

# HYDROGEOLOGICAL REVIEW REPORT

**PREPARED FOR:**

ACLP - Dundas Street E  
25 Watline Ave. Suite 501  
Mississauga ON, L4Z 2Z1

**ATTENTION:**

Jodi Shpigel

**60 Dundas St East,  
Mississauga, Ontario**

**Grounded Engineering Inc.**

**File No.** 21-067

**Issued** November 9, 2022



## Executive Summary

Grounded Engineering Inc. (Grounded) was retained by ACLP - Dundas Street E to conduct a Hydrogeological Review for the proposed redevelopment of 60 Dundas St East in Mississauga, Ontario (site). The conclusions of the investigation are summarized as follows:

### Development Information

Current Development					
Development Phase	Above Grade Levels	Below Grade Levels			
		Level #	Lowest Finished Floor		Approximate Base of Footings (masl)
			Depth (m)	Elevation (masl)	
60 Dundas St E	1	0	0	111.0 (approx.)	Unknown

Proposed Development					
Development Phase	Above Grade Levels	Below Grade Levels			
		Level #	Lowest Finished Floor		Approximate Base of Footings (masl)
			Depth (m)	Elevation (masl)	
60 Dundas St E – Tower A	40				
60 Dundas St E – Tower B	35	P5	17	94.0 (approx.)	93.0 (approx.)
60 Dundas St E – Tower C	32				

### Site Conditions

Site Stratigraphy				
Stratum/Formation	Aquifer or Aquitard	Depth Range (mbgs)	Elevation Range (masl)	Hydraulic Conductivity (m/s)
Earth Fill	Aquifer	0.1 – 4.0	110.8 – 106.0	$1.0 \times 10^{-5**}$
Clayey Silt Glacial Till	Aquitard	1.7 – 7.2	108.9 – 102.7	$6.8 \times 10^{-8*}$
Weathered Bedrock	Aquifer	4.4 – 10.1	104.6 – 99.7	$1.0 \times 10^{-7**}$
Sound Bedrock	Aquitard	6.6 – 10.1	101.9 – 99.7	$1.1 \times 10^{-8*}$

\*Indicates conductivity was calculated by Slug Test

\*\*Indicates conductivity was estimated using typical published values from Freeze and Cherry (1979)

Maximum Groundwater Elevation		
Monitoring Well ID	Depth Below Grade (m)	Elevation (masl)
101	3.2	108.1
102	3.8	106.3
103	4.0	105.7
201	2.4	105.4
202	3.1	106.3



Maximum Groundwater Elevation		
203	2.8	103.4
204	3.5	106.8
205	4.6	103.3
206	3.2	105.2
207	3.9	105.1

Groundwater Quality				
Sample ID	Sample Date	Sample Expiry Date	City of Mississauga Storm Sewer Limits	Region of Peel Sanitary Sewer Limits
SW-UF-BH205	23 Mar 2022	23 Dec 2022	Exceeds	Meets

### Groundwater Control

Stored Groundwater (pre-excavation/dewatering)					
Volume of Excavation (m <sup>3</sup> )	Volume of Excavation Below Water Table (m <sup>3</sup> )	Volume of Stored Groundwater		Volume of Available Groundwater	
		(m <sup>3</sup> )	(L)	(m <sup>3</sup> )	(L)
170,520	142,262	12,600	12,600,000	8,400	8,400,000

Short Term (Construction) Groundwater Quantity – Safety Factor of 2.0 Used					
Groundwater Seepage		Design Rainfall Event (25mm)		Total Daily Water Takings	
L/day	L/min	L/day	L/min	L/day	L/min
90,000	62.5	244,000	169.4	334,000	231.9

Long Term (Permanent) Groundwater Quantity – Safety Factor of 2.0 Used					
Groundwater Seepage		Infiltration Design Rainfall Event (25mm)		Total Daily Water Takings	
L/day	L/min	L/day	L/min	L/day	L/min
90,000	62.5	21,000	14.6	111,000	77.1

Zone of Influence	
Zone of Influence (m)	Maximum Potential Settlement (mm)
23	13



<b>Regulatory Requirements</b>	
Environmental Activity and Sector Registry (EASR) Posting	Required
Short Term Permit to Take Water (PTTW)	Not Required
Long Term Permit to Take Water (PTTW)	Required
Short Term Discharge Agreement City of Mississauga/Region of Peel	Required
Long Term Discharge Agreement City of Mississauga/Region of Peel	Required





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## **FIGURES**

Figure 1 – Study Area Map

Figure 2 – Borehole and Monitoring Well Location Plan

Figure 3 – Subsurface Cross-Section

## **APPENDICES**

Appendix A – Borehole Logs

Appendix B – Aquifer Response Tests

Appendix C – Grain Size Analysis

Appendix D – HydrogeoSieveXL Data

Appendix E – Laboratory Certificate of Analysis

Appendix F – Finite Element Model

Appendix G – Dewatering Calculations



# 1 Introduction

ACLPL - Dundas Street E has retained Grounded Engineering Inc. ("Grounded") to provide hydrogeological engineering design advice for their proposed development at 60 Dundas St East, in Mississauga, Ontario.

## Property Information

Location of Property	60 Dundas St East, Mississauga, Ontario, L5A 1W4
Ownership of Property	Gold Star Plaza Ltd.
Property Dimensions (m)	110 x 114 (irregular shape)
Property Area (m <sup>2</sup> )	10,724

## Existing Development

Number of Building Structures	1
Number of Above Grade Levels	1
Number of Underground Levels	0
Sub-Grade Depth of Development (m)	0
Sub-Grade Area (m <sup>2</sup> )	0
Land Use Classification	Commercial

## Proposed Development

Number of Building Structures	3
Number of Above Grade Levels	Building A = 40 Building B = 35 Building C = 32
Number of Underground Levels	5
Sub-Grade Depth of Development (m)	17
Sub-Grade Area (m <sup>2</sup> )	9,685
Land Use Classification	Residential



### Qualified Person and Hydrogeological Review Information

Qualified Person	Matthew Bielaski, P.Eng., QP <sub>RA-ESA</sub>
Consulting Firm	Grounded Engineering Inc.
Date of Hydrogeological Review	November 9, 2022
Scope of Work	<ul style="list-style-type: none"> <li>▪ Review of MECP Water Well Records for the area</li> <li>▪ Review of geological information for the area</li> <li>▪ Review of topographic information for the area</li> <li>▪ Advancement of 10 boreholes to a depth of 5.1 to 23.7 m, which were instrumented with monitoring wells</li> <li>▪ Completion of slug tests in all available monitoring wells</li> <li>▪ Ground water sampling and analysis to the City of Mississauga and Region of Peel Sewer Use Limits</li> <li>▪ Assessment of groundwater controls and potential impacts</li> <li>▪ Report preparation in accordance with Ontario Water Resources Act, Ontario Regulation 387/04</li> </ul>

### General Hydrogeological Characterization

Property Topography	The site has an approximate ground surface elevation of 111.0± to 108± masl.
Local Physiographic Features	The site subsurface is composed of earth fill, clayey silt glacial till and bedrock.
Regional Physiographic Features	The West St Lawrence Lowland consists of a limestone plain (elevation 200–250 masl) that is separated by a broad, shale lowland from a broader dolomite and limestone plateau west of Lake Ontario. This plateau is bounded by the Niagara Escarpment. From the escarpment the plateau slopes gently southwest to lakes Huron and Erie (elevation 173 masl). Glaciation has mantled this region with several layers of glacial till (i.e., an unsorted mixture of clay, sand, etc.), the youngest forming extensive, undulating till plains, often enclosing rolling drumlin fields.
Watershed	The site is located within the Credit River Watershed. Locally, groundwater is anticipated to flow southeast towards Lake Ontario.
Surface Drainage	Surface water is expected to flow towards municipal catch basins located on the site.



## 2 Study Area Map

A map has been enclosed which shows the following information:

- All monitoring wells identified on site
- All monitoring wells identified off site within the study area
- All boreholes identified on site
- All buildings identified on site and within the study area
- The property boundaries of the site
- Any watercourses and drainage features within the study area.

## 3 Geology and Physical Hydrogeology

The site stratigraphy, including soil materials, composition and texture are presented in detail on the borehole logs in Appendix A. A summary of stratigraphic units that were encountered at the site are as follows:

Site Stratigraphy				
Stratum/Formation	Aquifer or Aquitard	Depth Range (mbgs)	Elevation Range (masl)	Hydraulic Conductivity (m/s)
Earth Fill	Aquifer	0.1 – 4.0	110.8 – 106.0	$1.0 \times 10^{-5}$
Clayey Silt Glacial Till	Aquitard	1.7 – 7.2	108.9 – 102.7	$6.8 \times 10^{-8}$

Bedrock			
Stratum	Depth Range (mbgs)	Elevation Range (masl)	Hydraulic Conductivity (m/s)
Weathered	4.4 – 10.1	104.6 – 99.7	$1.0 \times 10^{-7}$
Sound	6.6 – 10.1	101.9 – 99.7	$1.1 \times 10^{-8}$

Surface Water		
Surface Water Body	Distance from site (m)	Hydraulically Connected to Property (yes/no)
Cooksville Creek	Adjacent to east boundary of site	No – the creek has been channelized hydraulically cut off from the site by a concrete retaining wall



## 4 Monitoring Well Information

Well ID	Well Diameter (mm)	Ground Surface (masl)	Top of Screen (masl)	Bottom of Screen (masl)	Screened Geological Unit
101	50	110.9	106.3	104.8	Clayey Silt Glacial Till
102	50	110.0	105.4	103.9	Clayey Silt Glacial Till /Bedrock
103	50	109.4	106.0	104.5	Clayey Silt Glacial Till
201	50	110.5	90.4	87.3	Bedrock
202	50	109.4	106.4	104.9	Clayey Silt Glacial Till
203	50	110.3	89.7	86.6	Bedrock
204	50	109.9	106.2	103.1	Clayey Silt Glacial Till /Bedrock
205	50	109.8	89.6	86.6	Bedrock
206	50	108.1	105.1	102.1	Clayey Silt Glacial Till /Bedrock
207	50	108.8	105.8	102.7	Glacial Till

## 5 Groundwater Elevations

Well ID	Groundwater Elevation (masl)								
	May 4, 2021	May 10, 2021	May 21, 2021	March 21, 2022	March 22, 2022	April 17, 2022	April 29, 2022	May 13, 2022	September 26, 2022
101	106.2	107.6	107.7	n/a	n/a	107.5	108.1	107.6	107.9
102	105.3	106.2	106.2	n/a	n/a	105.1	105.1	105.1	106.3
103	104.8	105.3	105.4	n/a	n/a	105.2	105.3	105.3	105.7
201	n/a	n/a	n/a	108.1	102.1	105.2	105.4	105.4	103.8
202	n/a	n/a	n/a	105.1	n/a	106.3	105.7	106.3	106.3
203	n/a	n/a	n/a	107.5	89.5	98.9	101.2	102.6	103.4
204	n/a	n/a	n/a	106.2	106.3	106.4	106.1	106.6	106.8
205	n/a	n/a	n/a	105.2	101.2	103.1	103.3	103.1	103.2
206	n/a	n/a	n/a	104.9	104.8	104.9	104.9	105	105.2
207	n/a	n/a	n/a	104.9	104.5	104.8	104.9	104.9	105.1

The groundwater table fluctuates from about 2.8 to 4.0 metres below grade, in the clayey silt till at Elev. 104.9 to 108.1 m with the groundwater sloping downwards from the west to the east towards Cooksville Creek. For design purposes, the groundwater table is assumed to be at



Elev. 108.1 m. The clayey silt till has a moderate to low permeability and will yield only minor seepage in the long term. There is also perched water in the earth fill, and groundwater within discrete fractures in the bedrock.

Groundwater levels fluctuate with time depending on the amount of precipitation and surface runoff and may be influenced by known or unknown dewatering activities at nearby sites.

## 6 Aquifer Testing

### 6.1 Single Well Response Test (Slug Test)

The hydraulic conductivities from the monitoring wells were determined based on slug tests (single-well response tests). These tests involve rapid removal of water or addition of a “slug” which displaces a known volume of water from a single well, and then monitoring the water level in the well until it recovers. The results of the slug tests were analyzed using the Bouwer and Rice method (1976).

The hydraulic properties of the strata applicable to the site are as follows:

Well ID	Well Screen Elevation (masl)	Screened Geological Unit	Hydraulic Conductivity (m/s)
101	106.3 - 104.8	Clayey Silt Glacial Till	$6.8 \times 10^{-8}$
102	105.4 - 103.9	Clayey Silt Glacial Till /Bedrock	$1.7 \times 10^{-8}$
103	106.0 - 104.5	Clayey Silt Glacial Till	$6.2 \times 10^{-8}$
201	90.4 - 87.3	Bedrock	$1.1 \times 10^{-8}$
202	106.4 - 104.8	Clayey Silt Glacial Till	$1.5 \times 10^{-8}$
203	89.7 - 86.6	Bedrock	$5.3 \times 10^{-9}$
204	106.2 - 103.1	Clayey Silt Glacial Till /Bedrock	$1.1 \times 10^{-8}$
205	89.6 - 86.6	Bedrock	$3.8 \times 10^{-9}$
206	105.1 - 102.0	Clayey Silt Glacial Till /Bedrock	$6.8 \times 10^{-8}$
207	105.8 - 102.7	Glacial Till	$2.0 \times 10^{-8}$

### 6.2 Soil Grain Size Distribution

The hydraulic conductivities of various soil types can also be estimated from grain size analyses. An assessment of the grain sizes was conducted using the excel-based tool, HydrogeoSieve XL (*HydrogeoSieve XL ver.2.2, J.F. Devlin, University of Kansas, 2015*). HydrogeoSieve XL compares the results of the grain size analyses against fifteen (15) different analytical methods.





Given our experience in the area as well as published literature, some of the geometric means provided for the soil were biased low by one or more methods. In these instances, the values determined by these methods were excluded from the mean. The table below illustrates the hydraulic conductivity values estimated from the mean of the analytical methods where the soil met the applicable analysis criteria.

Sample ID	Soil Description	Applicable Analysis Methods	Hydraulic Conductivity (m/s)
BH103-SS4	Clayey silt glacial till	Alyamani and Sen, Barr, Sauerbrei	$4.2 \times 10^{-9}$
BH201-SS5	Clayey silt glacial till	Alyamani and Sen, Barr, Sauerbrei	$1.6 \times 10^{-8}$
BH202-SS6	Clayey silt glacial till	Alyamani and Sen, Barr, Kruger, Krumbein and Monk, Sauerbrei	$5.1 \times 10^{-7}$
BH203-SS3	Sand	Alyamani and Sen, Barr, Krumbein and Monk, Sauerbrei	$2.9 \times 10^{-6}$
BH204-SS2	Silty sand	Alyamani and Sen, Barr, Krumbein and Monk, Sauerbrei	$5.9 \times 10^{-8}$
BH205-SS2	Silty sand	Alyamani and Sen, Barr, Krumbein and Monk, Sauerbrei	$3.4 \times 10^{-7}$
BH206-SS4	Clayey silt glacial till	Alyamani and Sen, Barr, Sauerbrei	$5.1 \times 10^{-9}$
BH207-SS4	Clayey silt glacial till	Alyamani and Sen, Barr, Sauerbrei	$2.9 \times 10^{-9}$

The results of the analyses are presented in Appendix D.

### 6.3 Literature

According to Freeze and Cherry (1979), the typical hydraulic conductivity of the strata investigated at the site are:

Stratum/Formation	Hydraulic Conductivity (m/s)
Earth Fill	$1 \times 10^{-3}$ to $1 \times 10^{-7}$
Clayey Silt Glacial Till	$1 \times 10^{-7}$ to $1 \times 10^{-10}$
Weathered Shale Bedrock	$1 \times 10^{-6}$ to $1 \times 10^{-12}$
Sound Shale Bedrock	$1 \times 10^{-7}$ to $1 \times 10^{-12}$

## 7 Water Quality

One (1) unfiltered groundwater sample was collected and analyzed by a Canadian laboratory accredited and licensed by Standards Council of Canada and or Canadian Association for Laboratory Accreditation.

The sample was collected directly from monitoring well BH205 on March 23, 2022. The sample was analyzed for the following parameters:



- City of Mississauga Storm Sewer By-Law 0046-2022 – Limits for Storm Sewers Discharge
- Region of Peel By-Law 53-2010 Table 1 – Limits for Sanitary Sewer Discharge

The groundwater sample **exceeded** the **Limits for Storm Sewer Discharge** for the following parameters:

- Total Suspended Solids (Limit 15 mg/L, Result 38.2 mg/L)
- Copper (Limit 0.04 mg/L, Result <0.040 mg/L)
- Manganese (Limit 2.0 mg/L, Result 2.09 mg/L)
- Zinc (Limit 0.3 mg/L, Result <0.30 mg/L)

The groundwater sample **met** the **Limits for Sanitary Sewer Discharge** for all parameters analyzed.

A true copy of the analysis report, Certificate of Analysis and a chain of custody record for the sample are enclosed.

## 8 Proposed Construction Method

The proposed shoring methodology at the site is currently undetermined. For the purposes of this report, numerical analyses were conducted employing conventional soldier piling and lagging in order to determine a “worst-case scenario” with respect to dewatering volumes and groundwater seepage at the site.

For design purposes, the stabilized groundwater table is at about Elev. 108.1± m. The water table is present in the clayey silt till soil units. The lowest (P5) FFE is at about Elev. 94± m. Therefore,

- Bulk excavation will extend down to the elevation of the prevailing groundwater table;
- Foundation excavations will extend below the prevailing groundwater table; and
- Foundation excavations will penetrate sound bedrock yielding minor seepage.

The groundwater table is in the clayey silt till deposits and bedrock. There is perched water in the earth fill above the clayey silt till. Dewatering will take some time to accomplish prior to the start of excavation. Stored water within the excavation will need to be considered prior to excavation/dewatering. The clayey silt till deposit has a moderate to low permeability and will yield minor seepage. Positive dewatering of soils may not be feasible at this site due to permeability of the soils present. Dewatering could potentially be achieved through conventional sump pump arrangements. Dewatering of the bedrock is not required, seepage can be allowed to drain into the excavation and pumped accordingly. Failure to dewater prior to excavation may result in unrecoverable disturbance of the subgrade, which will render advice provided for undisturbed subgrade conditions inapplicable.

It is recommended that a professional dewatering contractor be consulted to review the subsurface conditions and to design a site-specific dewatering system. It is the dewatering contractor’s responsibility to assess the factual data and to provide recommendations on dewatering system requirements.



The proposed structures will consist of drained foundations. The City of Mississauga and/or the Region of Peel will require Discharge Agreements in the short and long terms, if any water is to be discharged to the storm or sanitary sewers. It should be noted that securing a permit to take water on a permanent basis may not be supported by regulatory agencies.

## **9 Private Water Drainage System (PWDS)**

If the proposed development consists of drained foundations, then a private water drainage system will be required. The total sub floor drain area will be approximately 9,685 m<sup>2</sup> based on the drawings which have been provided.

If the development is designed with a private water drainage system, the drainage system is a critical structural element since it keeps water pressure from acting on the basement walls and floor slab. As such, the sump that ensures the performance of this system must have a duplexed pump arrangement for 100% pumping redundancy and these pumps must be on emergency power. The size of the sump should be adequate to accommodate the estimated groundwater seepage. It is anticipated that the groundwater seepage can be controlled with typical, widely available, commercial/residential sump pumps.

If the proposed development is designed as a leak tight structure, then a private water drainage system will not be required. However, the structure must then be designed to resist hydrostatic pressure and uplift forces.

## **10 Groundwater Extraction and Discharge**

Numerical analyses were conducted for both short-term and long-term dewatering scenarios. The modeling was conducted using computer software, which deploys the finite element modelling method. The Finite Element Model (FEM) for groundwater seepage indicates the short term (construction) and long term (permanent) dewatering requirements as provided below. The finite element model results are presented in Appendix E.

The groundwater seepage estimates, which have been provided, represent the steady state groundwater seepage. There will be an initial drawdown of the groundwater before a steady state condition is reached. The rate of the initial drawdown, and therefore discharge, is dependent on the dewatering contractor and how the groundwater is being dealt with at the site. An estimated initial volume of stored groundwater which will require removal before steady state is reached has been provided below.

Please note that if excavation is exposed to the elements, storm water will have to be managed. The short-term control of groundwater should consider stormwater management from rainfall events. A dewatering system should be designed to consider the removal of rainfall from excavation. A design storm of 25 mm has been used in the quantity estimates.



As required by Ontario Regulation 63/16, a plan for discharge must consider the conveyance of storm water from a 100-year storm. The additional volume that will be generated in the occurrence of a 100-year storm event is approximately 916,000 L.

<b>Stored Groundwater (pre-excavation/dewatering)</b>					
Volume of Excavation (m <sup>3</sup> )	Volume of Excavation Below Water Table (m <sup>3</sup> )	Volume of Stored Groundwater		Volume of Available Groundwater	
		(m <sup>3</sup> )	(L)	(m <sup>3</sup> )	(L)
170,520	142,262	12,600	12,600,000	8,400	8,400,000

<b>Short Term (Construction) Groundwater Quantity – Safety Factor of 2.0 Used</b>					
Groundwater Seepage		Design Rainfall Event (25mm)		Total Daily Water Takings	
L/day	L/min	L/day	L/min	L/day	L/min
90,000	62.5	244,000	169.4	334,000	231.9

<b>Long Term (Permanent) Groundwater Quantity – Safety Factor of 2.0 Used</b>					
Groundwater Seepage		Infiltration Design Rainfall Event (25mm)		Total Daily Water Takings	
L/day	L/min	L/day	L/min	L/day	L/min
90,000	62.5	21,000	14.6	111,000	77.1

<b>Regulatory Requirements</b>	
Environmental Activity and Sector Registry (EASR) Posting	Required
Short Term Permit to Take Water (PTTW)	Not Required
Long Term Permit to Take Water (PTTW)	Required
Short Term Discharge Agreement City of Mississauga/Region of Peel	Required
Long Term Discharge Agreement City of Mississauga/Region of Peel	Required



Please note:

- The proposed pump schedule for short term construction dewatering has not been completed. As such, the actual peak short term discharge rate is not available at the time of writing this report. The pump schedule must be specified by either the dewatering contractor retained or the mechanical consultant.
- The proposed pump schedule for long term permanent drainage has not been completed. As such the actual peak long term discharge rate is not available at the time writing of this report. The pump schedule must be specified by the mechanical consultant.
- A leak-tight structure (structure that has not included a private water drainage system) has not been considered as part of the proposed development at this time.
- On-site containment (infiltration gallery/dry well etc.) has not been considered as part of the proposed development at this time. If this option is considered, additional work will have to be conducted (i.e. infiltration testing).

## 11 Evaluation of Impact

### 11.1 Zone of Influence (ZOI)

The Zone of Influence (ZOI) with respect to groundwater was calculated based on the estimated groundwater taking rate and the hydraulic conductivity of the unit which water will be taken at the Property.

The ZOI was calculated using the Sichardt equation below.

Equation:  $R_0 = 3000 * dH * K^{0.5}$

Where:

dH is the dewatering thickness (m)

K is the hydraulic conductivity (m/s)

Calculation:

Geological Unit	dH (m)	K (m/s)	ZOI (m)
Earth Fill	2.1	$1 \times 10^{-5}$	20
Clayey Silt Glacial Till	3.3	$6.8 \times 10^{-8}$	3

The ZOI with respect to groundwater seepage at the site is 23 m.



## 11.2 Land Stability

The impacts to land stability of the proposed short term and long term dewatering at the site on adjacent structures are summarized as follows:

- The proposed dewatering at the subject site locally lowers the groundwater table within the ZOI by a maximum of 5.4 m. This drawdown would create an increase in effective stress of approximately  $53 \pm$  kPa in the native soils.
- Based on the change in effective stress and the compressibility of the soil subjected to that change, the proposed dewatering activities will induce a theoretical maximum 5-10 mm of additional settlement in the adjacent lands.
- The maximum induced settlement occurs directly adjacent to the proposed excavation and decreases in a nonlinear fashion with distance away from the excavation.
- For the structures within the public realm adjacent to the site, the theoretical dewatering-induced settlement is calculated to be 2-4 mm or less (depending on the depth of the structure).

On this basis, the impact of the proposed dewatering on the existing adjacent structures is considered by Grounded to be within acceptable limits.

## 11.3 City's Sewage Works

Negative impacts to City's sewage works may occur in terms of the quantity or quality of the groundwater discharged. This report provided the estimated quantity of the water discharge. However, this report does not speak to the sewer capacities. The sewer capacity analysis is provided under a separate cover by the civil consultant.

The quality of the proposed groundwater discharge is provided in Section 7. As noted in that section, the groundwater sample exceeded the Limits for Storm Sewer Discharge and met the Limits for Sanitary Sewer Discharge.

As such, additional treatment will be required before the water can be discharged to the Storm Sewer to avoid impacts to the City's sewage works caused by groundwater quality. Additional treatment will not be required before the water can be discharged to the Sanitary Sewer.

## 11.4 Natural Environment

Cooksville Creek is located adjacent to east boundary of site but is hydraulically cut off from the site by a concrete retaining wall that appears to be bearing on relatively low hydraulic conductivity clayey silt till or bedrock. Therefore, the creek will likely not be affected by the proposed construction and long-term dewatering. There are no other natural waterbodies within the ZOI that will be affected by the proposed construction dewatering or permanent drainage. Any groundwater which will be taken from the site will be discharged (if required) into the City's sewer systems and not into any natural water body. As such, there will be no impact to the natural environment caused by the water takings at the site.



## **11.5 Local Drinking Water Wells**

The site is located within the municipal boundaries of the City of Mississauga. The site and surrounding area are provided with municipal piped water and sewer supply. There is no use of the groundwater for water supply in this area of Mississauga. As such, there will be no impact to drinking water wells.

## **11.6 Contamination Source**

The site and immediately surrounding area currently consist mostly of residential and commercial areas. These land uses are anticipated to be a source of potential contamination and are expected to provide an Area of Potential Environmental Concern for the site. As such, the pumping of groundwater at the site is anticipated to facilitate the movement of potential contaminants onto the site. Evaluation of the environmental condition of the site has been completed under a separate cover.

## **12 Proposed Mitigation Measures and Monitoring Plan**

The extent of the negative impact identified in previous sections will be limited to the ZOI caused by the groundwater taking at the site.

As a result of dewatering and draining the soil, changes in groundwater level have the potential to cause settlement based on the change in the effective stresses within the ZOI.

If adjacent buildings or municipal infrastructure are within the ZOI and will undergo settlement that may be considered unacceptable as identified the Land Stability Section, consideration should be given to implement a monitoring and mitigation program during dewatering activities.

Both the temporary construction dewatering system and the permanent building drainage system must be properly installed and screened to ensure sediments and fines will not be removed, which is typically a primary cause of dewatering related settlement.

## **13 Limitations**

Natural occurrences, the passage of time, local construction, and other human activity all have the potential to directly or indirectly alter the subsurface conditions at or near the project site. Contractual obligations related to groundwater or stormwater control must be considered with attention and care as they relate this potential site alteration.

The hydrogeological engineering advice provided in this report is based on the factual observations made from the site investigations as reported. It is intended for use by the owner and their retained design team. If there are changes to the features of the development or to the scope, the interpreted subsurface information, geotechnical engineering design parameters, advice, and discussion on construction considerations may not be relevant or complete for the





project. Grounded should be retained to review the implications of such changes with respect to the contents of this report.

Any use which a third party makes of this report, or any reliance on or decisions to be made based on it, are the responsibility of such third parties. Grounded accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this report, including consequential financial effects on transactions or property values, or requirements for follow-up actions and costs.

### 13.1 Report Use

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## 14 Closure

If there are any questions regarding the discussion and advice provided, please do not hesitate to contact our office. We trust that this report meets your requirements at present.

For and on behalf of our team,



A handwritten signature in black ink, appearing to read "Nico Piers".

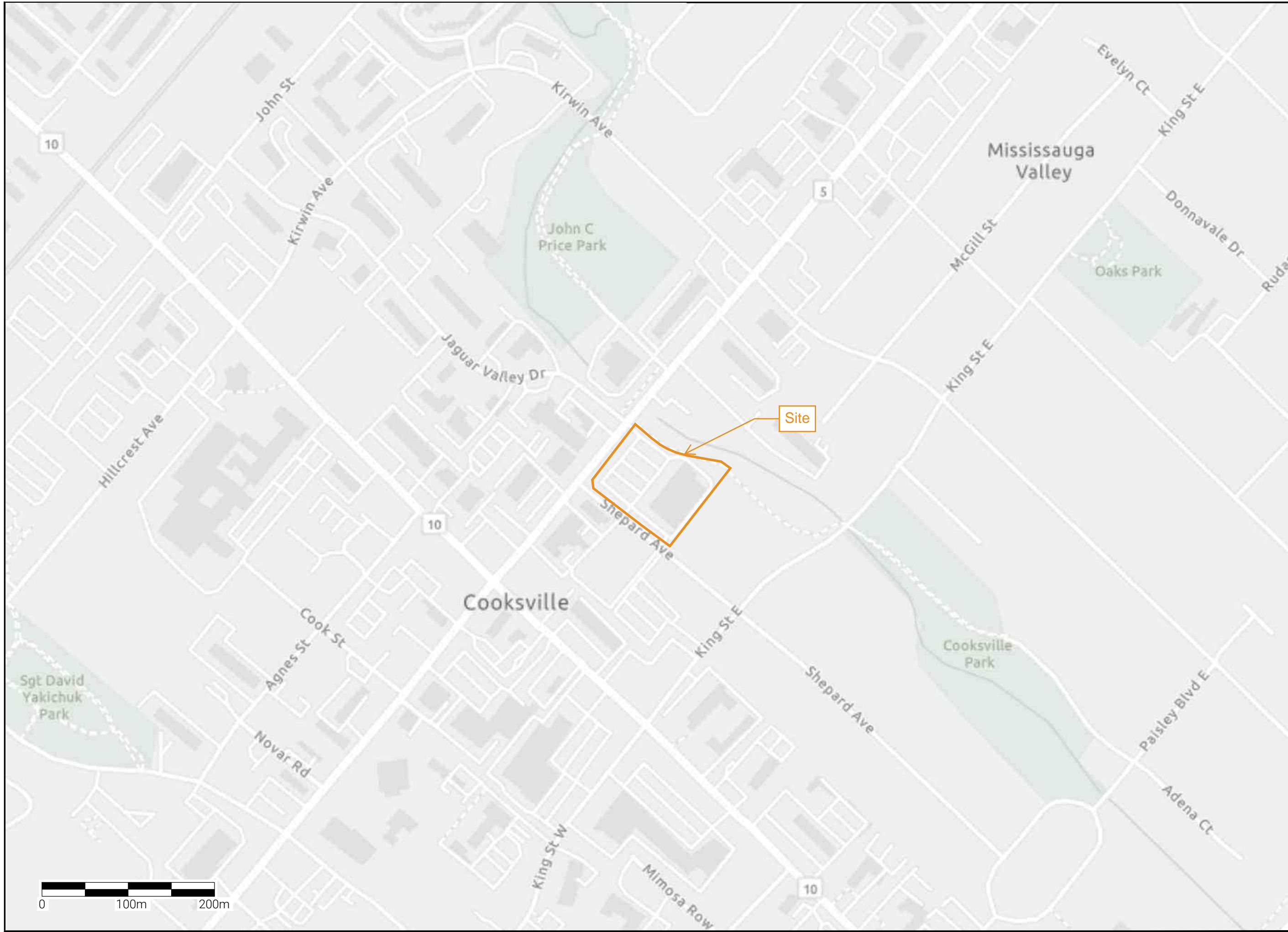
Nico Piers, BAsC  
Project Coordinator



Matthew Bielaski, P.Eng., QP<sub>RA-ESA</sub>  
Principal

# FIGURES





**GROUNDED**  
ENGINEERING

1 BANIGAN DRIVE, TORONTO, ONT., M4H 1G3  
www.grounedeng.ca

**LEGEND**

— APROXIMATE PROPERTY BOUNDARY

Note

Reference

ArcGIS Map 2021

Project

**60 DUNDAS STREET EAST, MISSISSAUGA, ON**

Figure Title

**SITE LOCATION PLAN**

North



Date

NOVEMBER 2022

Scale

AS INDICATED

Job No

21-067

Figure No

**FIGURE 1**



**GROUND  
ENGINEERING**

1 BANIGAN DRIVE, TORONTO, ONT., M4H 1G3  
www.groundedeng.ca

**LEGEND**

- APPROXIMATE PROPERTY BOUNDARY
- EXISTING BUILDING STRUCTURE
- MONITORING WELL BY GROUND
- CATCHBASIN
- MAINTENANCE HOLE

**Note**

**Reference**

Survey Drawing no. 20-21-14108-00.  
Prepared by Aksan Piller Corporation Ltd.  
Dated April 5, 2021.

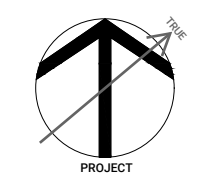
**Project**

**60 DUNDAS STREET  
EAST, MISSISSAUGA, ON**

**Figure Title**

**BOREHOLE LOCATION  
PLAN**

**North**



**Date**

NOVEMBER 2022

**Scale**

AS INDICATED

**Job No**

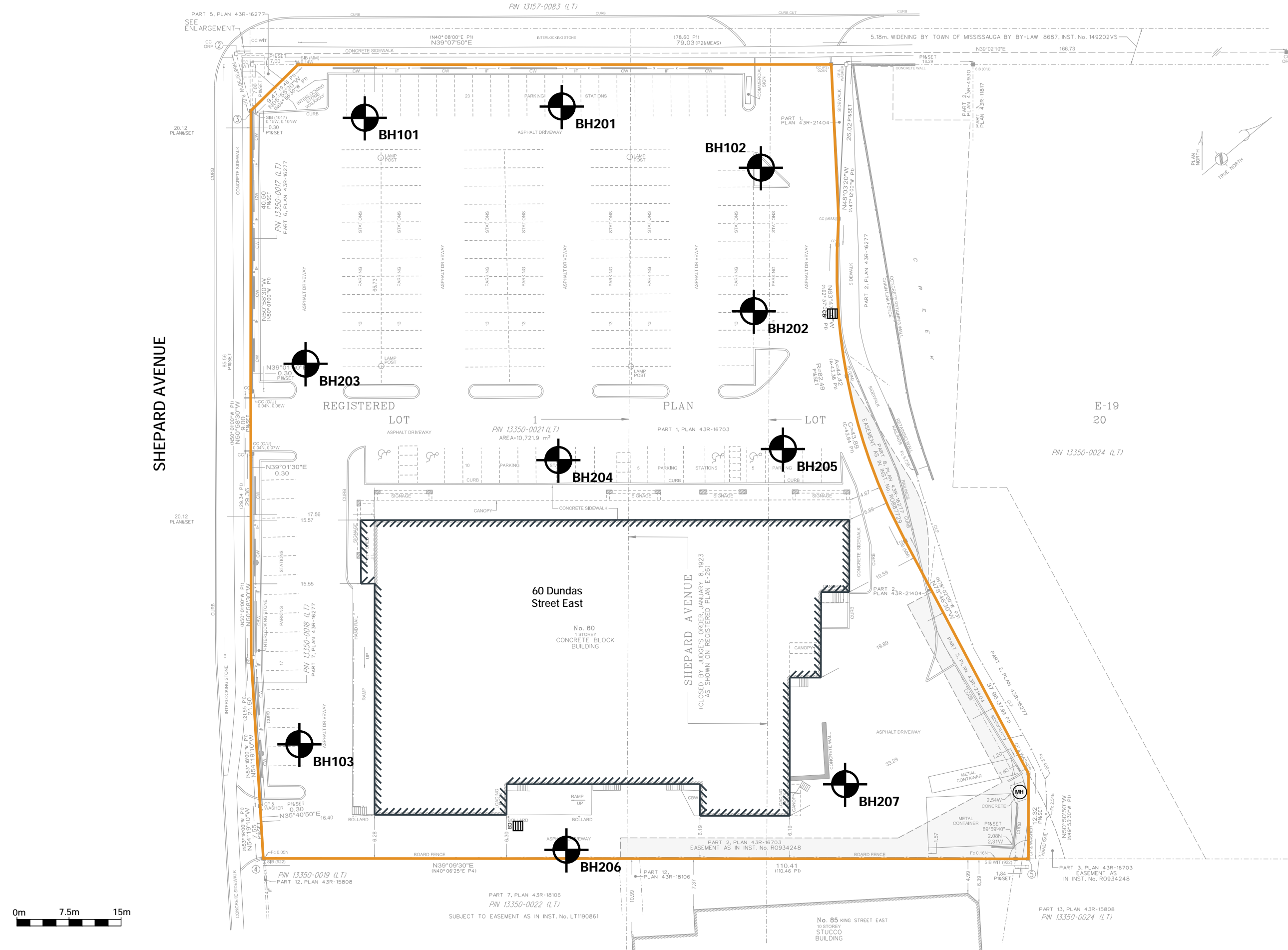
21-067

**Figure No**

**FIGURE 2**

**DUNDAS STREET EAST**

**SHEPARD AVENUE**



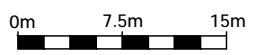
E-19  
20

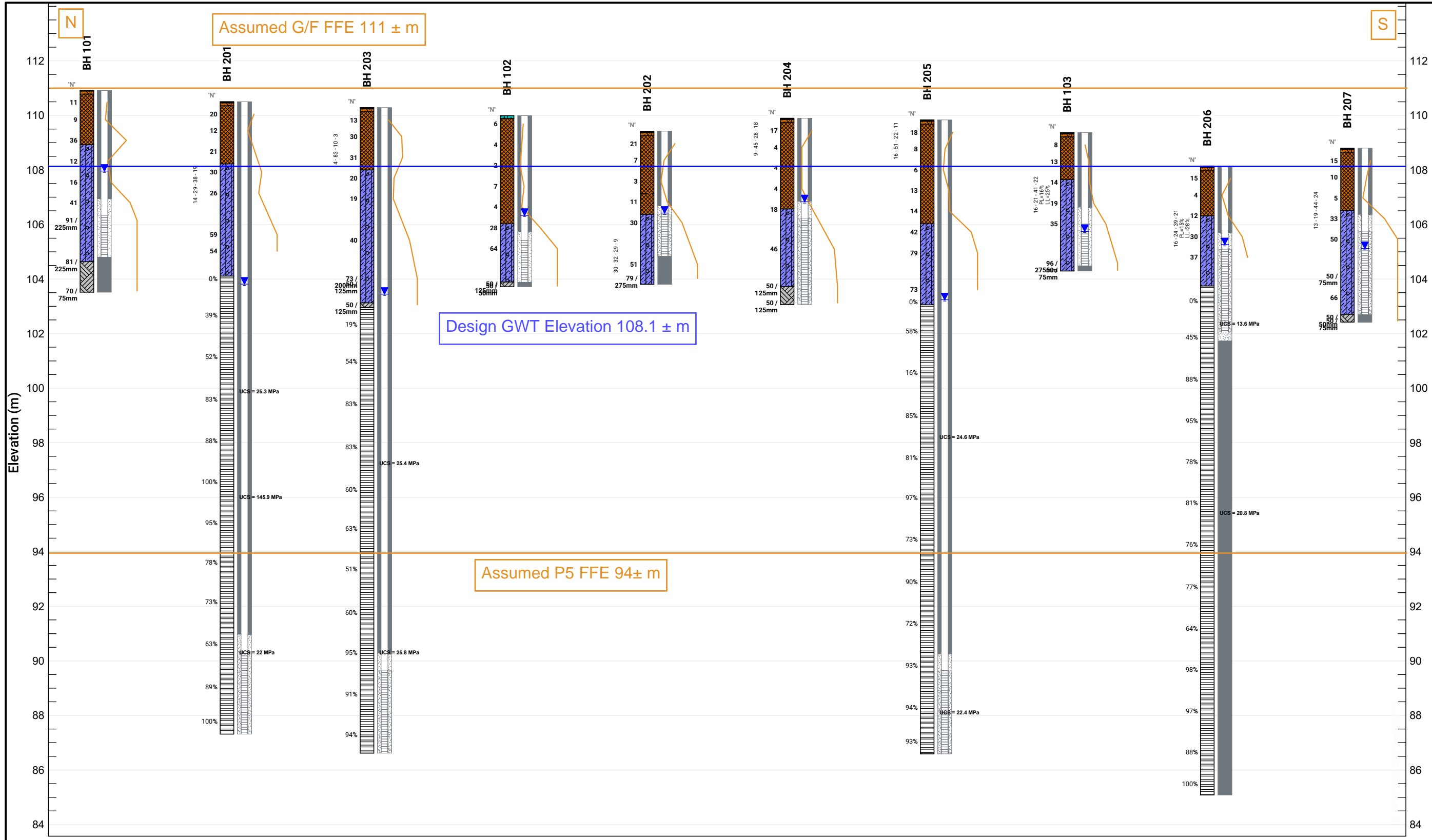
PIN 13350-0024 (LT)

**60 Dundas  
Street East**

No. 60  
1 STOREY  
CONCRETE BLOCK  
BUILDING

**SHEPARD AVENUE**  
(CLOSED BY JUDGE'S ORDER JANUARY 8, 1923  
AS SHOWN ON REGISTERED PLAN E-26)





**LEGEND**

- FILL
- GRAVELS (gravel to gravelly sand)
- SILT TO SAND (not till)
- COHESIONLESS TILLS
- COHESIVE SOILS (clayey silt to clay, incl. tills)
- DISTURBED/REWORKED/ORGANIC

▽ water level, unstabilized  
▽ water level, stabilized (latest)  
▽ water level, stabilized (highest)

Project  
**60 DUNDAS STREET EAST  
MISSISSAUGA, ON**

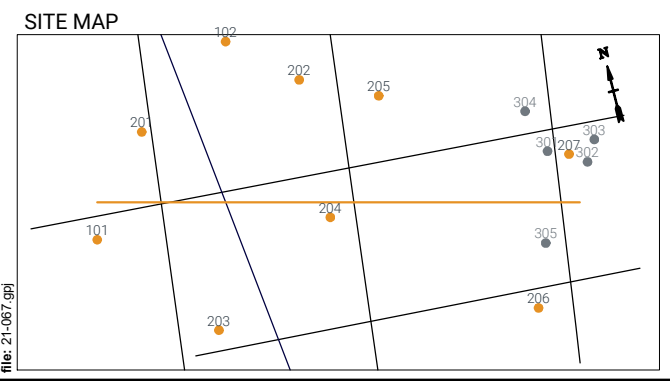
Figure Title  
**SUBSURFACE PROFILE**

Date  
NOVEMBER 2022

Scale  
AS INDICATED

Job No  
21-067

Figure No  
**FIGURE 3**



**LITHOLOGY GRAPHIC LEGEND**

<span style="display: inline-block; width: 15px; height: 15px; background-color: black; border: 1px solid black; margin-right: 5px;"></span> Asphalt	<span style="display: inline-block; width: 15px; height: 15px; border: 1px solid black; border-style: dashed; margin-right: 5px;"></span> Bedrock (inferred)
<span style="display: inline-block; width: 15px; height: 15px; background-color: #cccccc; border: 1px solid black; margin-right: 5px;"></span> Aggregate	<span style="display: inline-block; width: 15px; height: 15px; border: 1px solid black; border-style: dotted; margin-right: 5px;"></span> Topsoil
<span style="display: inline-block; width: 15px; height: 15px; background-color: #8B4513; border: 1px solid black; margin-right: 5px;"></span> Fill	<span style="display: inline-block; width: 15px; height: 15px; border: 1px solid black; border-style: solid; margin-right: 5px;"></span> Shale
<span style="display: inline-block; width: 15px; height: 15px; background-color: #66B3FF; border: 1px solid black; margin-right: 5px;"></span> Clayey Silt Till	

Boreholes Equally Spaced

# APPENDIX A





## SAMPLING/TESTING METHODS

SS: split spoon sample  
 AS: auger sample  
 GS: grab sample  
 FV: shear vane  
 DP: direct push  
 PMT: pressuremeter test  
 ST: shelby tube  
 CORE: soil coring  
 RUN: rock coring

## SYMBOLS & ABBREVIATIONS

MC: moisture content  
 LL: liquid limit  
 PL: plastic limit  
 NP: non-plastic  
 $\gamma$ : soil unit weight (bulk)  
 $G_s$ : specific gravity  
 $S_u$ : undrained shear strength  
 unstabalized water level  
 1st water level measurement  
 2nd water level measurement most recent  
 water level measurement

## ENVIRONMENTAL SAMPLES

M&I: metals and inorganic parameters  
 PAH: polycyclic aromatic hydrocarbon  
 PCB: polychlorinated biphenyl  
 VOC: volatile organic compound  
 PHC: petroleum hydrocarbon  
 BTEX: benzene, toluene, ethylbenzene and xylene  
 PPM: parts per million

## FIELD MOISTURE (based on tactile inspection)

**DRY:** no observable pore water  
**MOIST:** inferred pore water, not observable (i.e. grey, cool, etc.)  
**WET:** visible pore water

## COHESIONLESS

Relative Density	N-Value
Very Loose	<4
Loose	4 - 10
Compact	10 - 30
Dense	30 - 50
Very Dense	>50

## COHESIVE

Consistency	N-Value	Su (kPa)
Very Soft	<2	<12
Soft	2 - 4	12 - 25
Firm	4 - 8	25 - 50
Stiff	8 - 15	50 - 100
Very Stiff	15 - 30	100 - 200
Hard	>30	>200

## COMPOSITION

Term	% by weight
trace silt	<10
some silt	10 - 20
silty	20 - 35
sand and silt	>35

## ASTM STANDARDS

### ASTM D1586 Standard Penetration Test (SPT)

Driving a 51 mm O.D. split-barrel sampler ("split spoon") into soil with a 63.5 kg weight free falling 760 mm. The blows required to drive the split spoon 300 mm ("bpf") after an initial penetration of 150 mm is referred to as the N-Value.

### ASTM D3441 Cone Penetration Test (CPT)

Pushing an internal still rod with a outer hollow rod ("sleeve") tipped with a cone with an apex angle of 60° and a cross-sectional area of 1000 mm<sup>2</sup> into soil. The resistance is measured in the sleeve and at the tip to determine the skin friction and the tip resistance.

### ASTM D2573 Field Vane Test (FVT)

Pushing a four blade vane into soil and rotating it from the surface to determine the torque required to shear a cylindrical surface with the vane. The torque is converted to the shear strength of the soil using a limit equilibrium analysis.

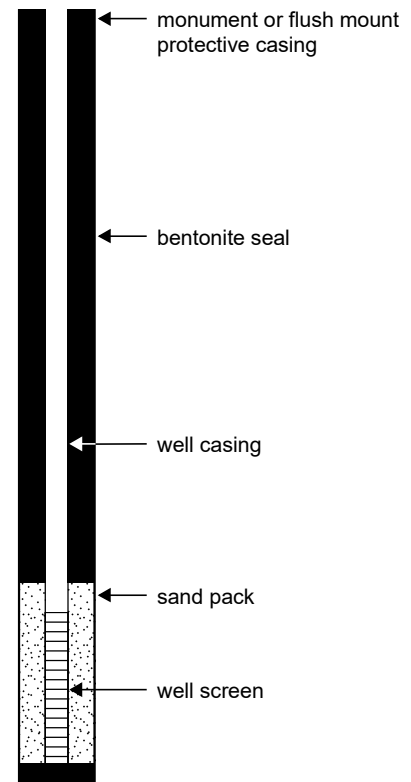
### ASTM D1587 Shelby Tubes (ST)

Pushing a thin-walled metal tube into the in-situ soil at the bottom of a borehole, removing the tube and sealing the ends to prevent soil movement or changes in moisture content for the purposes of extracting a relatively undisturbed sample.

### ASTM D4719 Pressuremeter Test (PMT)

Place an inflatable cylindrical probe into a pre-drilled hole and expanding it while measuring the change in volume and pressure in the probe. It is inflated under either equal pressure increments or equal volume increments. This provides the stress-strain response of the soil.

## WELL LEGEND

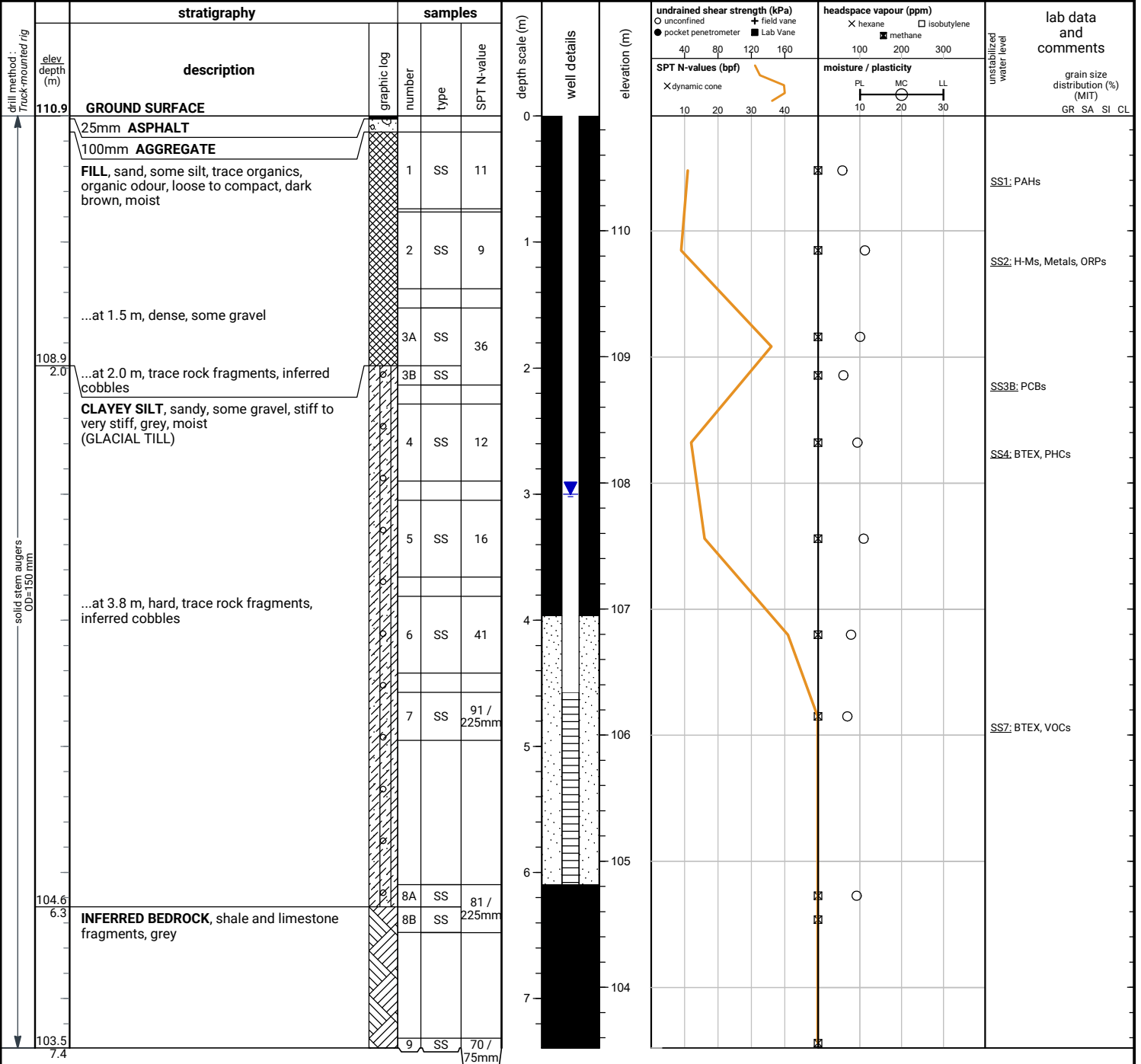




File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



END OF BOREHOLE

Dry and open upon completion of drilling.  
 50 mm dia. monitoring well installed.  
 No. 10 screen

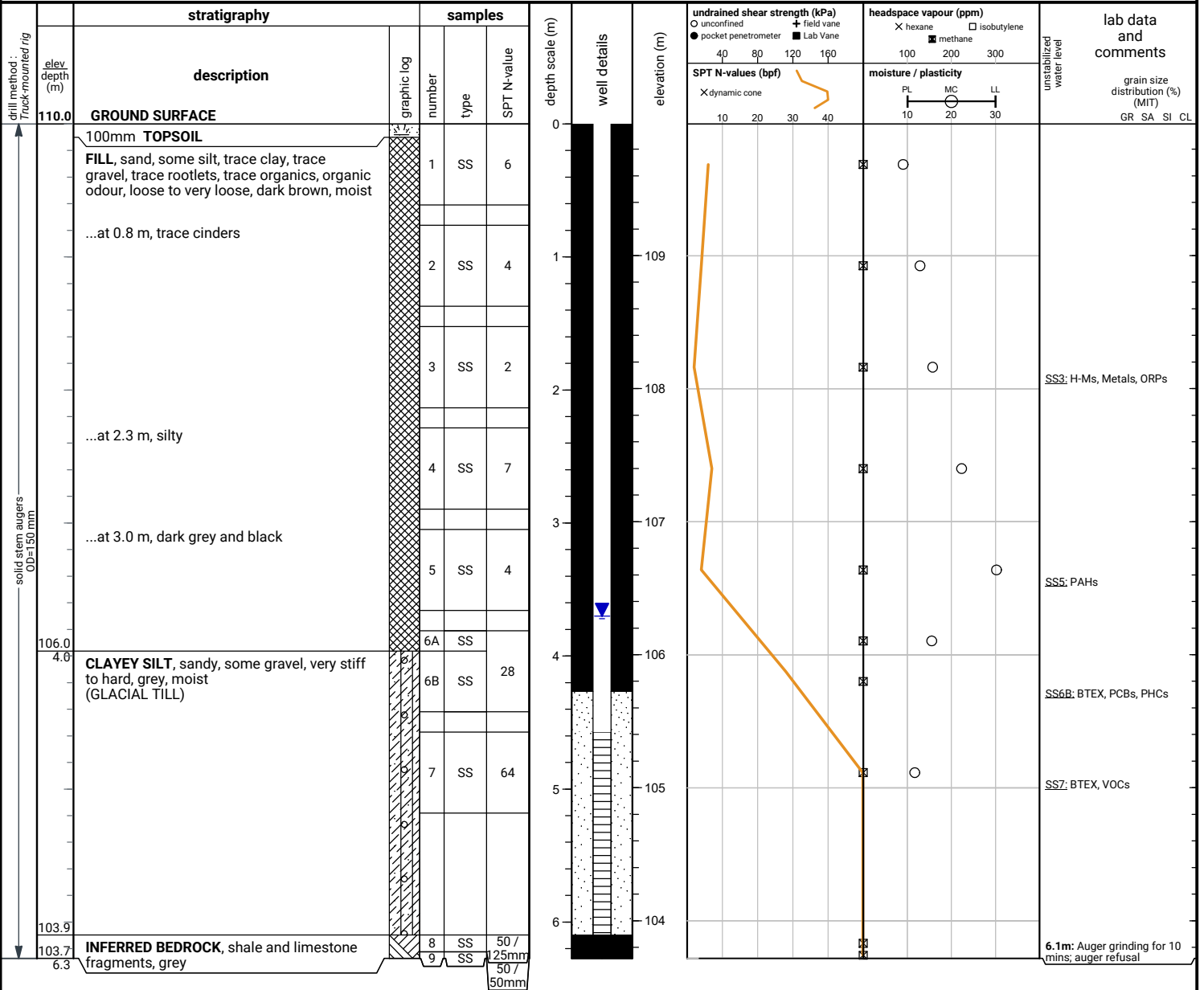
GROUNDWATER LEVELS

date	depth (m)	elevation (m)
May 4, 2021	4.7	106.2
May 6, 2021	3.5	107.4
May 10, 2021	3.3	107.6
May 21, 2021	3.2	107.7
Apr 17, 2022	3.4	107.5
Apr 29, 2022	2.8	108.1
May 13, 2022	3.3	107.6
Sep 26, 2022	3.0	107.9

File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



**END OF BOREHOLE**  
Auger refusal on inferred bedrock

Dry and open upon completion of drilling.

50 mm dia. monitoring well installed.  
No. 10 screen

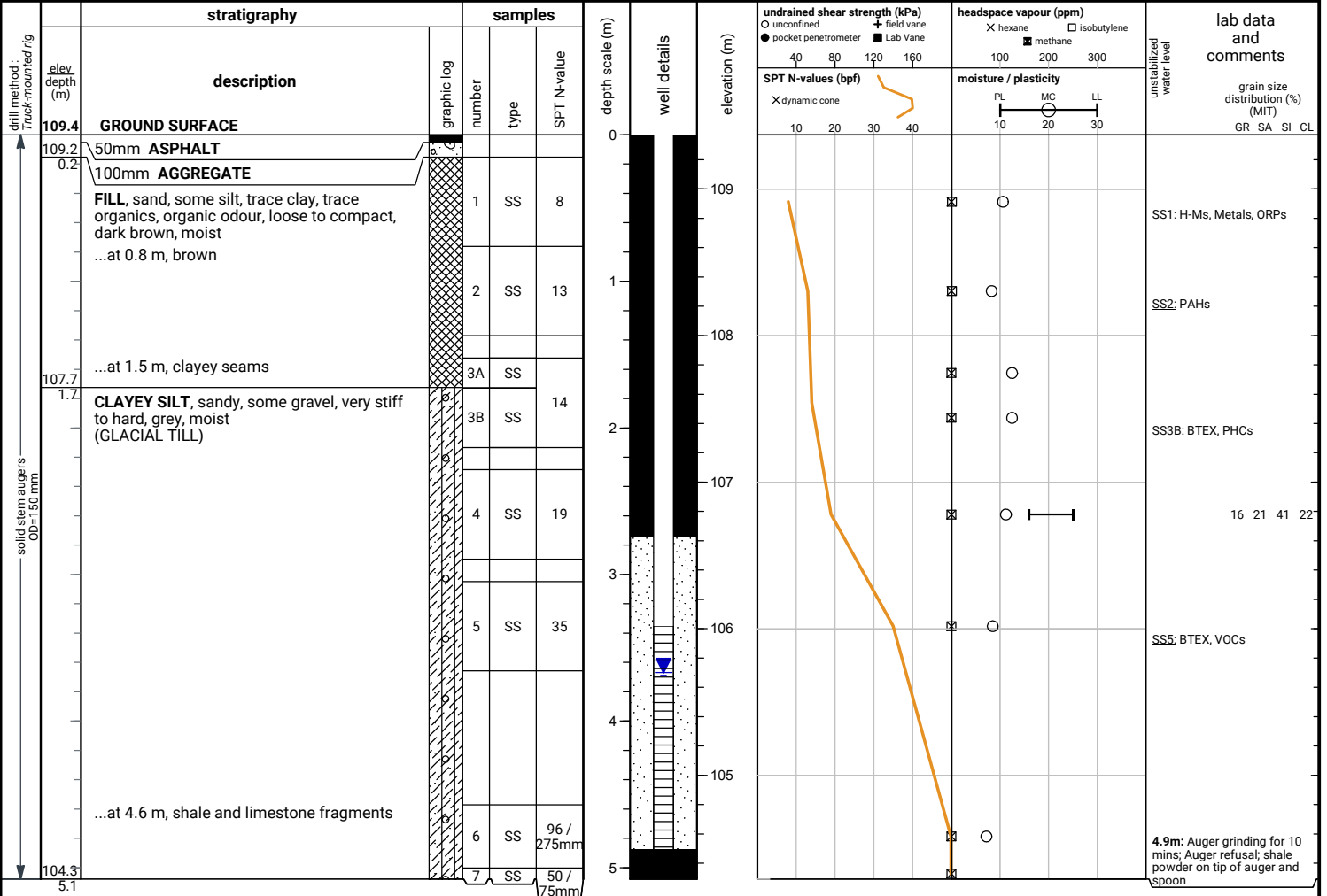
**GROUNDWATER LEVELS**

date	depth (m)	elevation (m)
May 4, 2021	4.7	105.3
May 6, 2021	4.0	106.0
May 10, 2021	3.8	106.2
May 21, 2021	3.8	106.2
Apr 17, 2022	4.9	105.1
Apr 29, 2022	4.9	105.1
May 13, 2022	4.9	105.1
Sep 26, 2022	3.7	106.3

File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



**END OF BOREHOLE**  
Auger refusal on inferred bedrock

Dry and open upon completion of drilling.

50 mm dia. monitoring well installed.  
No. 10 screen

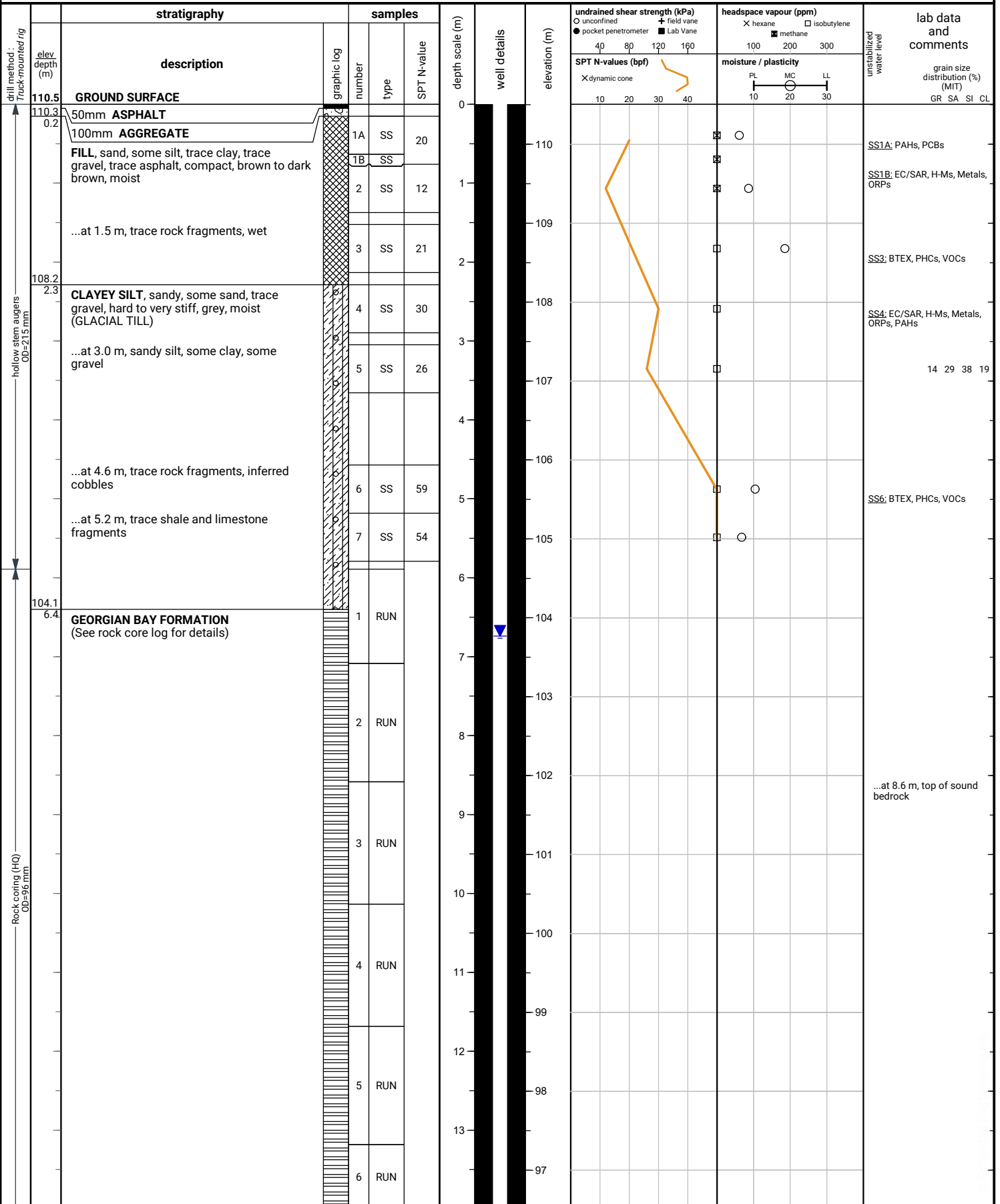
**GROUNDWATER LEVELS**

date	depth (m)	elevation (m)
May 4, 2021	4.6	104.8
May 6, 2021	4.1	105.3
May 10, 2021	4.1	105.3
May 21, 2021	4.0	105.4
Apr 17, 2022	4.2	105.2
Apr 29, 2022	4.1	105.3
May 13, 2022	4.1	105.3
Sep 26, 2022	3.7	105.7

File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



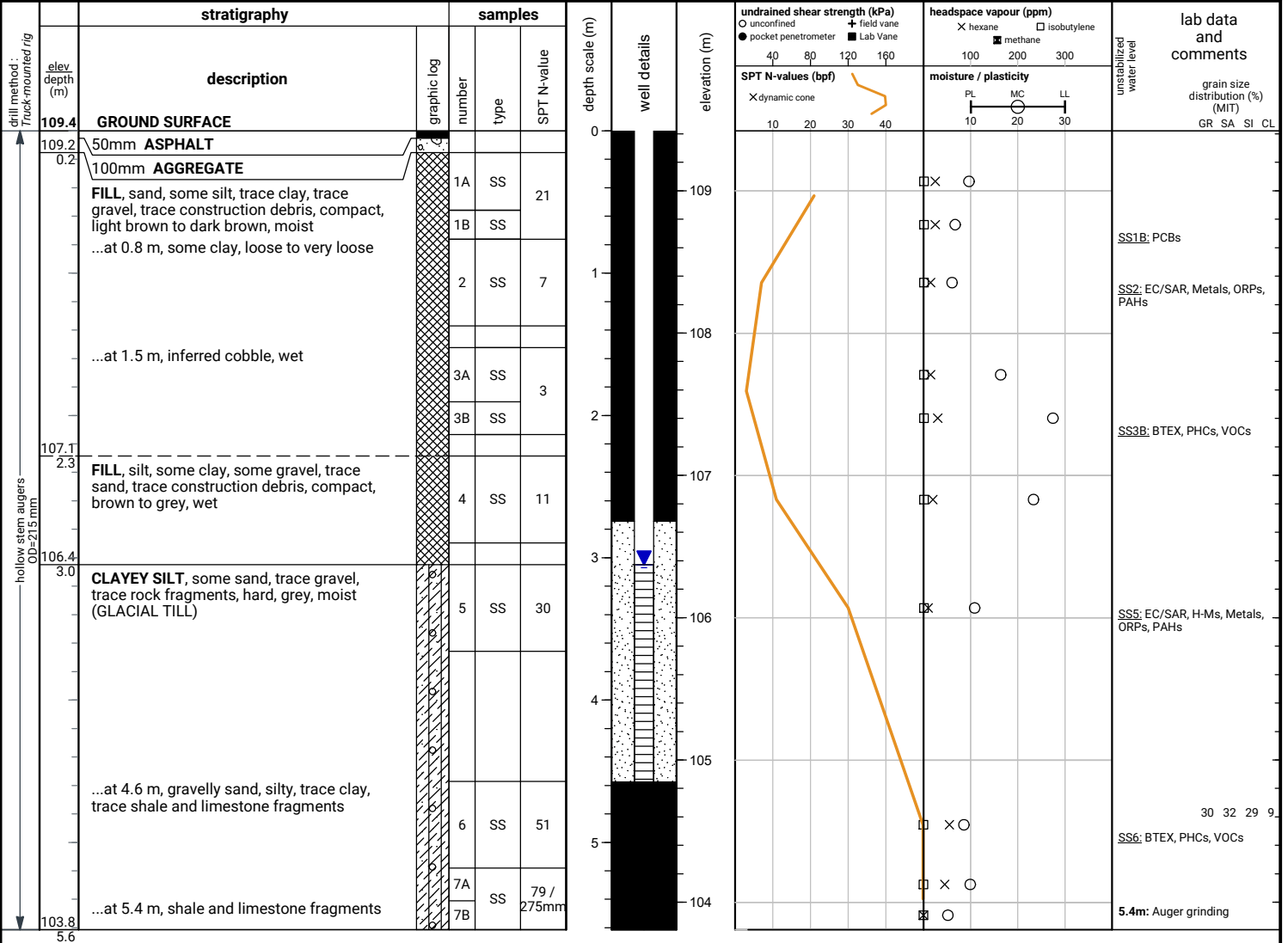
file: 21-067.gpj



File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



**END OF BOREHOLE**  
Auger refusal on inferred bedrock

Water level and cave not measured upon completion of drilling.

50 mm dia. monitoring well installed.  
No. 10 screen

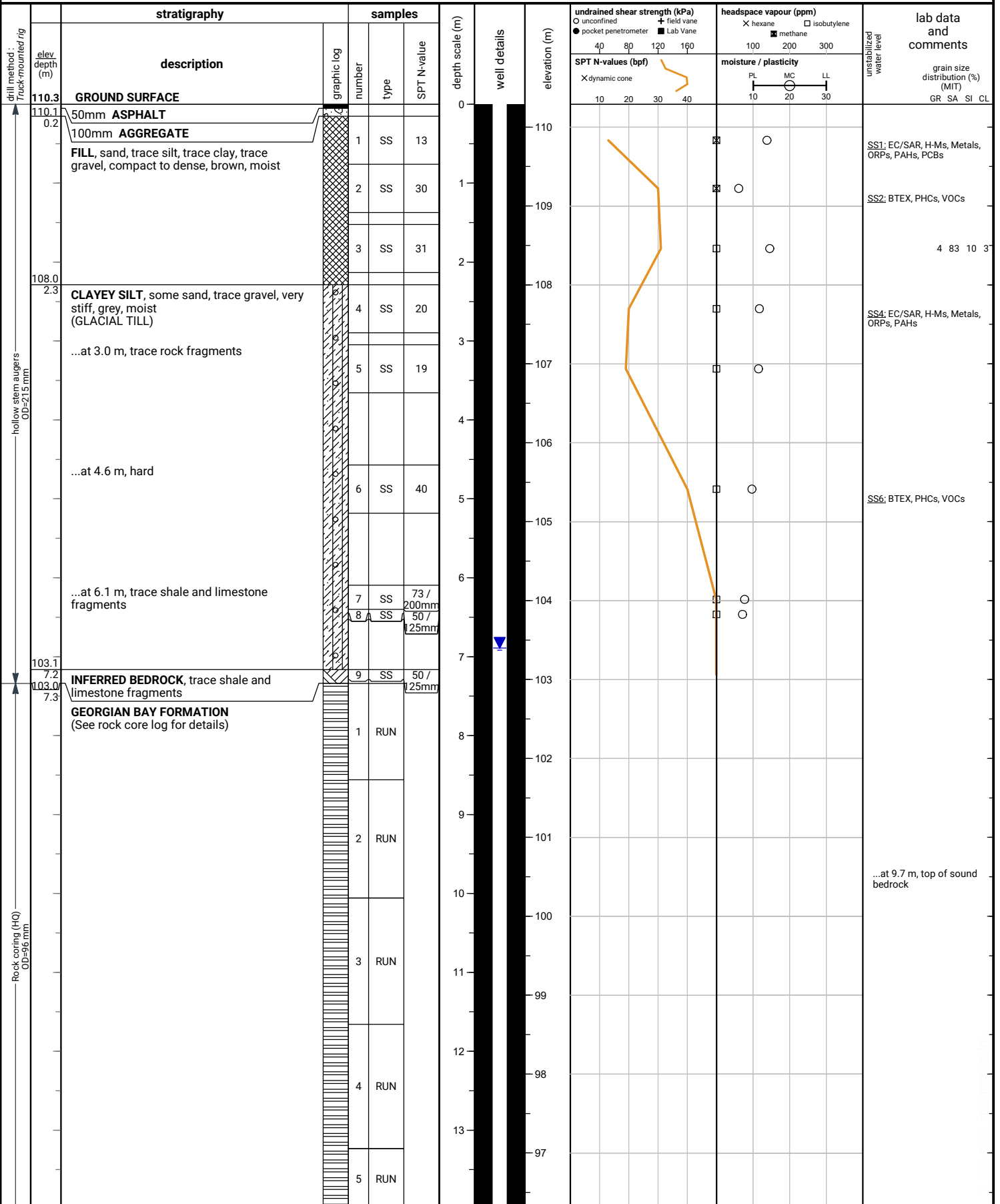
**GROUNDWATER LEVELS**

date	depth (m)	elevation (m)
Mar 21, 2022	4.3	105.1
Apr 17, 2022	3.1	106.3
Apr 29, 2022	3.7	105.7
May 13, 2022	3.1	106.3
Sep 26, 2022	3.1	106.3

File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



file: 21-067.gpj



File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E

drill method : Truck-mounted rig	stratigraphy		samples			depth scale (m)	well details	elevation (m)	undrained shear strength (kPa) ○ unconfined    + field vane ● pocket penetrometer    ■ Lab Vane	headspace vapour (ppm) X hexane    □ isobutylene methane	lab data and comments grain size distribution (%) (MIT) GR SA SI CL
	elev. depth (m)	description	graphic log	number	type						
	(continued)	<b>GEORGIAN BAY FORMATION</b> (See rock core log for details) (continued)									
				5	RUN						
				6	RUN						
				7	RUN						
				8	RUN						
				9	RUN						
				10	RUN						
				11	RUN						

**END OF BOREHOLE**

Borehole was filled with drill water upon completion of drilling.

50 mm dia. monitoring well installed.  
No. 10 screen

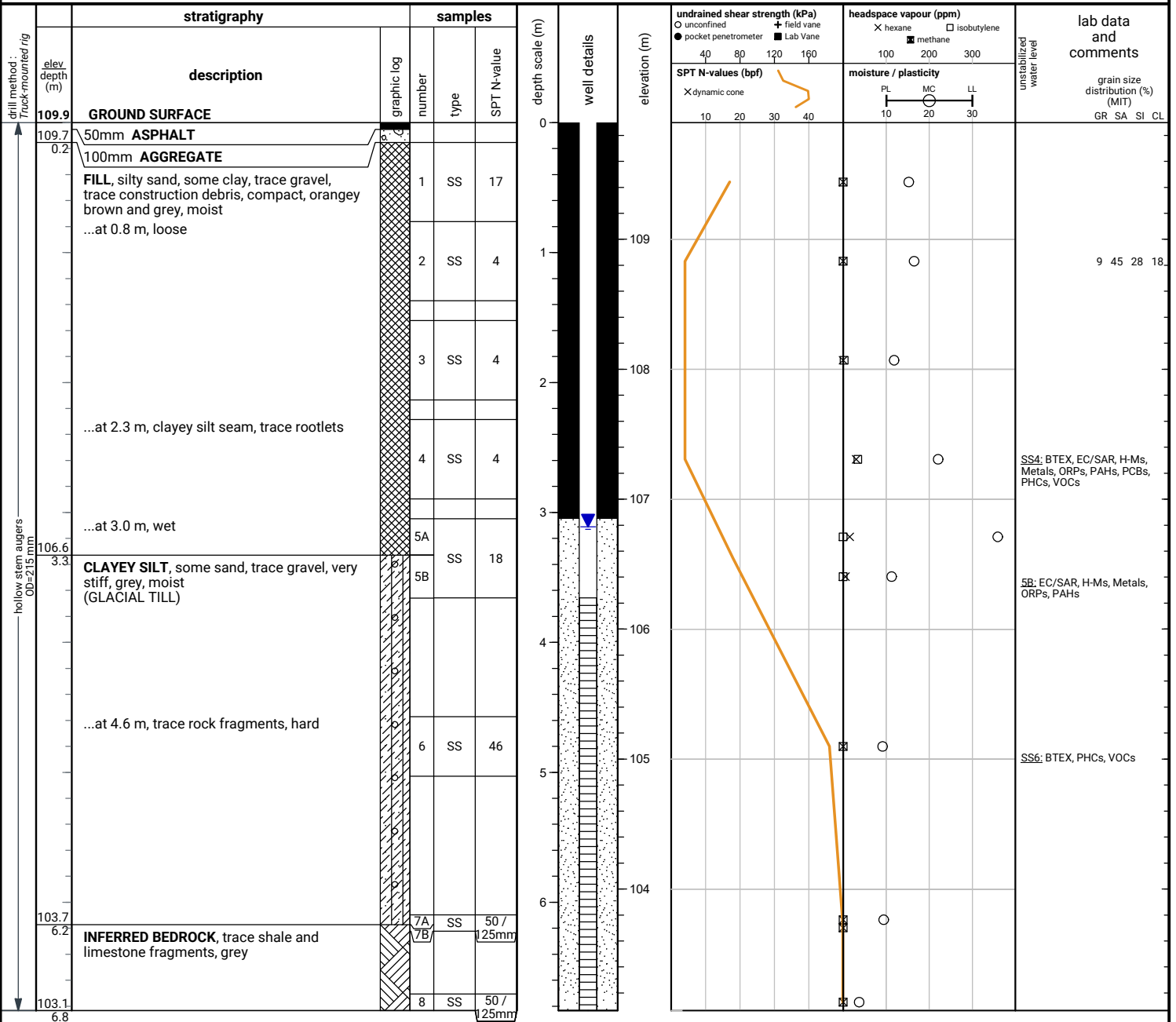
**GROUNDWATER LEVELS**

date	depth (m)	elevation (m)
Apr 17, 2022	11.4	98.9
Apr 29, 2022	9.1	101.2
May 13, 2022	7.7	102.6
Sep 26, 2022	6.9	103.4

File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



**END OF BOREHOLE**

Water level and cave not measured upon completion of drilling.

50 mm dia. monitoring well installed.  
 No. 10 screen

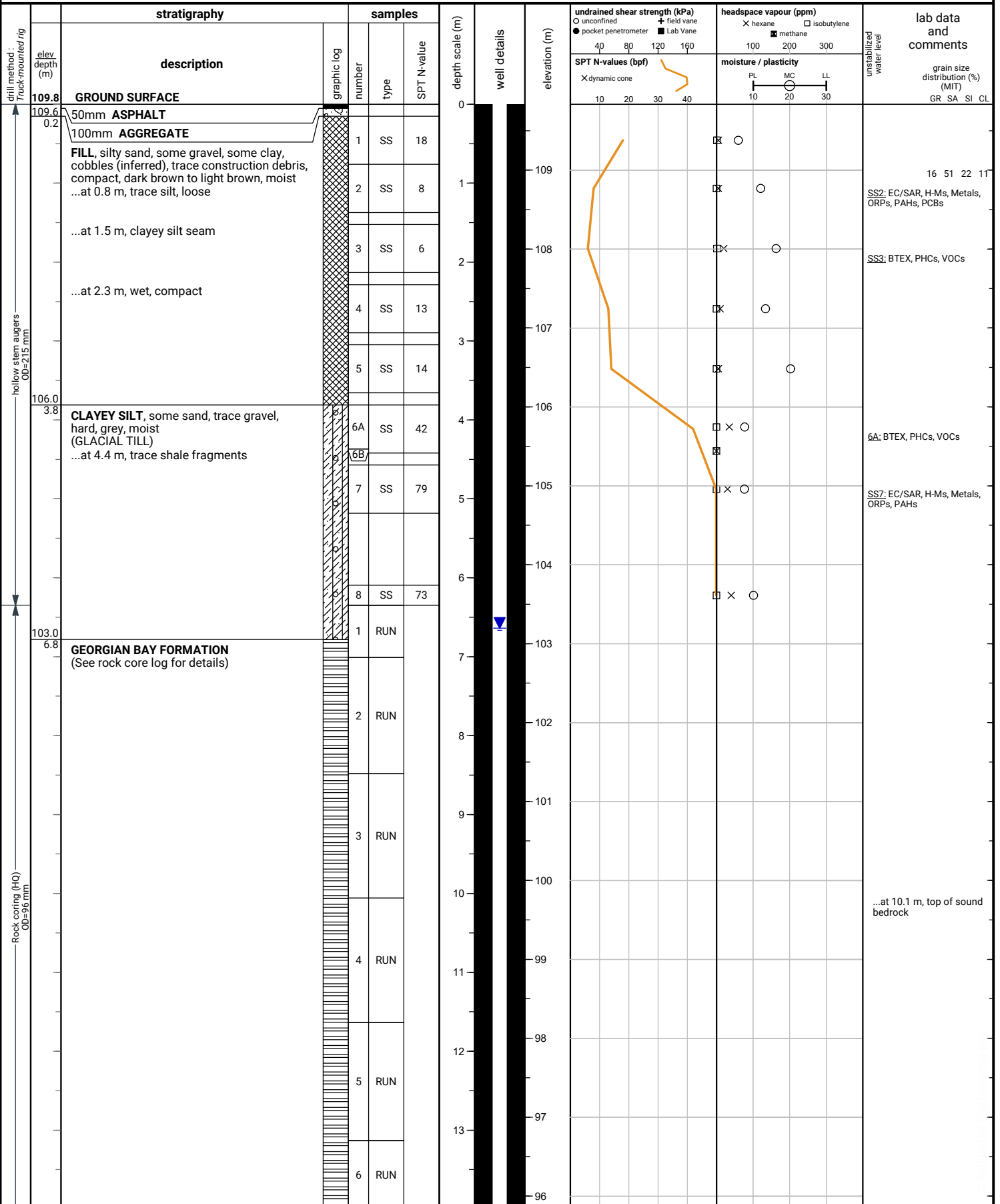
**GROUNDWATER LEVELS**

date	depth (m)	elevation (m)
Mar 21, 2022	3.7	106.2
Mar 22, 2022	3.6	106.3
Apr 17, 2022	3.5	106.4
Apr 29, 2022	3.8	106.1
May 13, 2022	3.3	106.6
Sep 26, 2022	3.1	106.8

File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



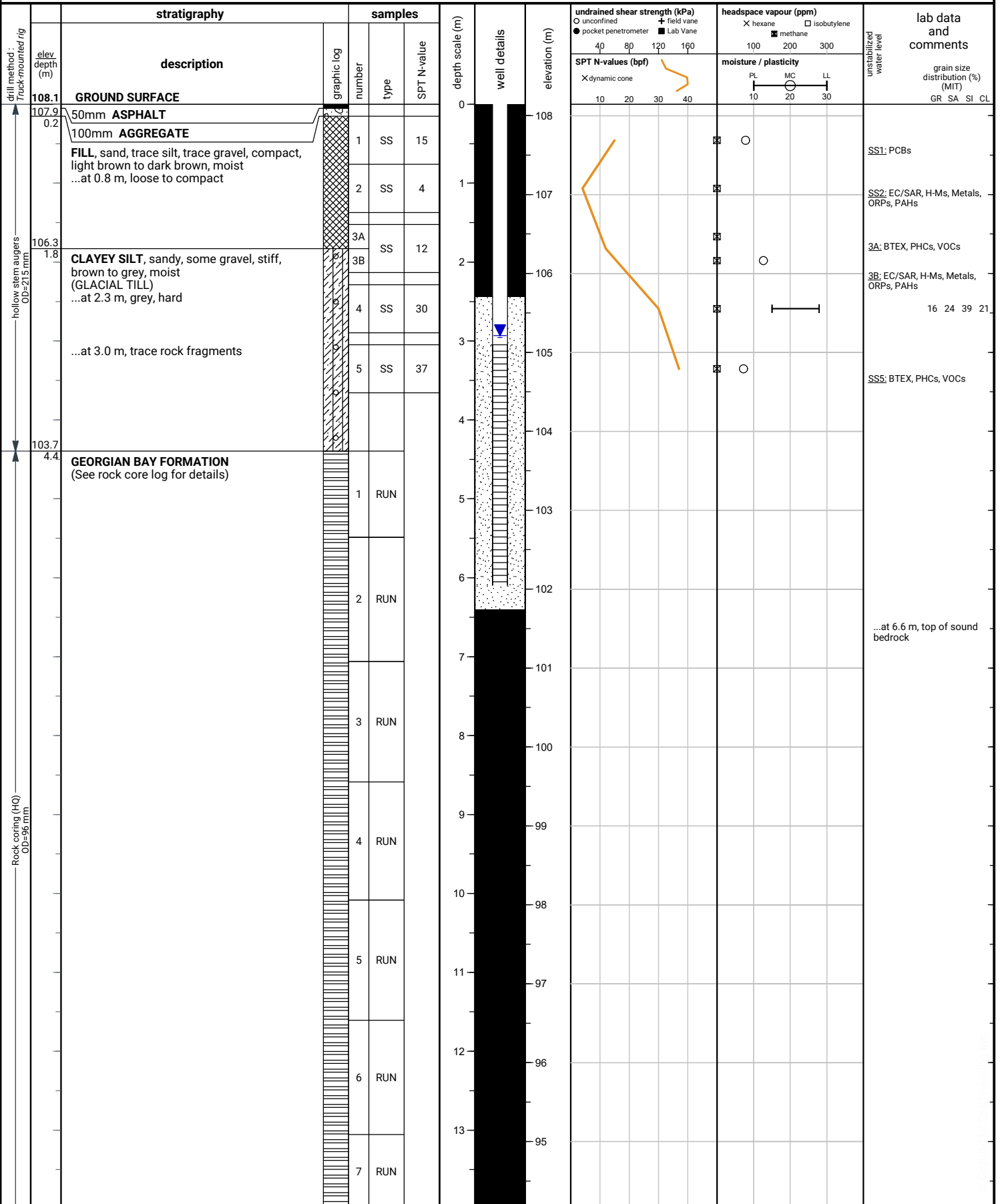
file: 21-067.gpj



File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



file: 21-067.gpj

File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E

drill method : Truck-mounted rig	stratigraphy		samples			depth scale (m)	well details	elevation (m)	undrained shear strength (kPa)		headspace vapour (ppm)			lab data and comments
	elev. depth (m)	description	graphic log	number	type				SPT N-value	○ unconfined ● pocket penetrometer X dynamic cone	+ field vane ■ Lab Vane	X hexane □ isobutylene	■ methane	
	(continued)													
	<b>GEORGIAN BAY FORMATION</b> (See rock core log for details) (continued)													
				7	RUN			94						
				8	RUN			93						
				9	RUN			92						
				10	RUN			91						
				11	RUN			90						
				12	RUN			89						
				13	RUN			88						
								87						
								86						
								23						

**END OF BOREHOLE**

Borehole was filled with drill water upon completion of drilling.

50 mm dia. monitoring well installed.  
No. 10 screen

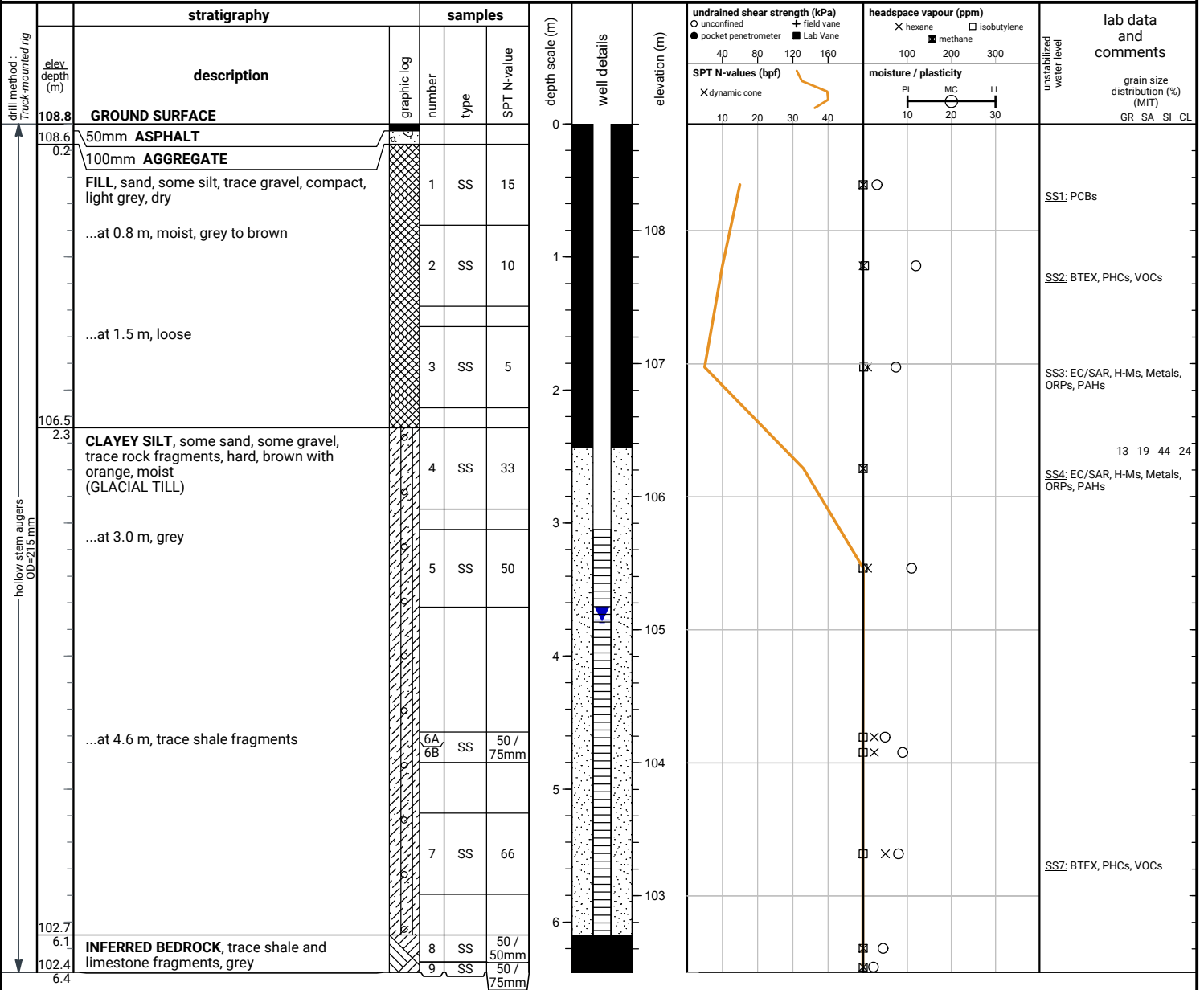
**GROUNDWATER LEVELS**

date	depth (m)	elevation (m)
Mar 22, 2022	3.3	104.8
Apr 17, 2022	3.2	104.9
Apr 29, 2022	3.2	104.9
May 13, 2022	3.1	105.0
Sep 26, 2022	2.9	105.2

File No. : 21-067

Project : 60 Dundas Street East, Mississauga, ON

Client : ACLP - Dundas St E



**END OF BOREHOLE**

Water level and cave not measured upon completion of drilling.

50 mm dia. monitoring well installed.  
 No. 10 screen

**GROUNDWATER LEVELS**

date	depth (m)	elevation (m)
Mar 21, 2022	3.9	104.9
Mar 22, 2022	4.3	104.5
Apr 17, 2022	4.0	104.8
Apr 29, 2022	3.9	104.9
May 13, 2022	3.9	104.9
Sep 26, 2022	3.7	105.1

# APPENDIX B







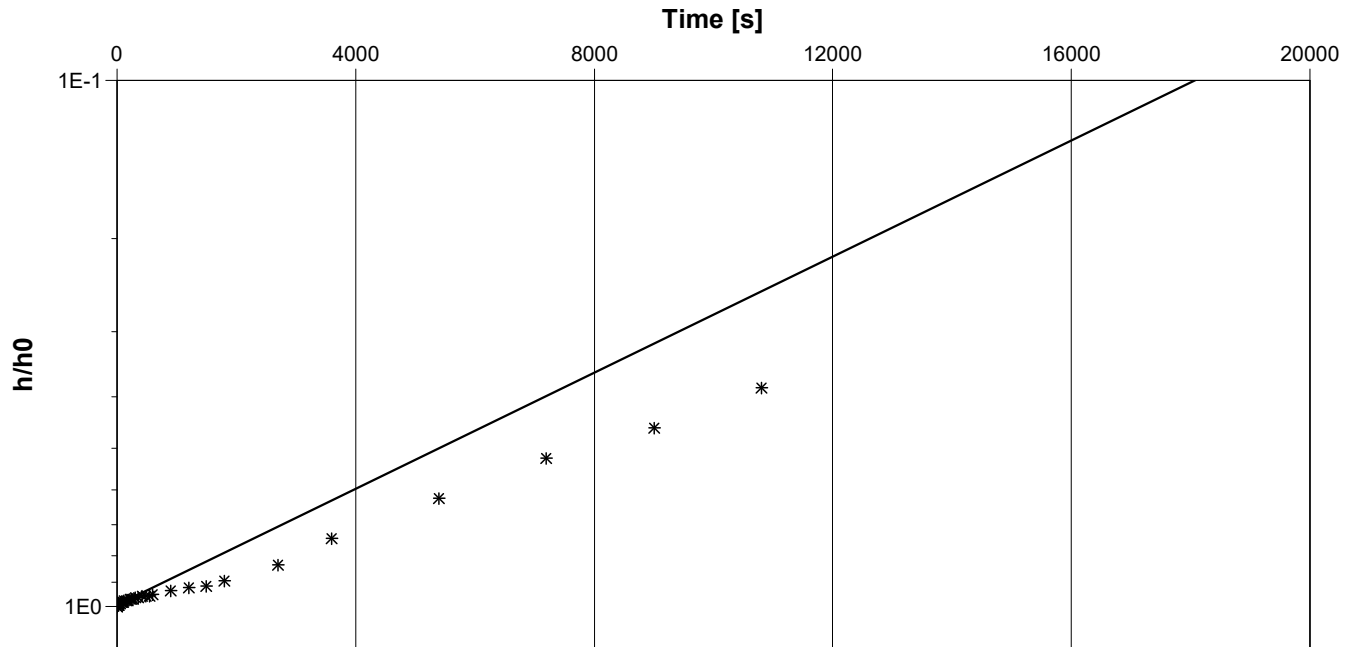
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH101	Test Well: BH207
Test Conducted by: OM		Test Date: 2021-05-10
Analysis Performed by: DK	RHT-BH101	Analysis Date: 2021-05-13
Aquifer Thickness: 6.30 m		



Calculation using Bouwer & Rice

Observation Well	Hydraulic Conductivity [m/s]
BH207	$6.78 \times 10^{-8}$



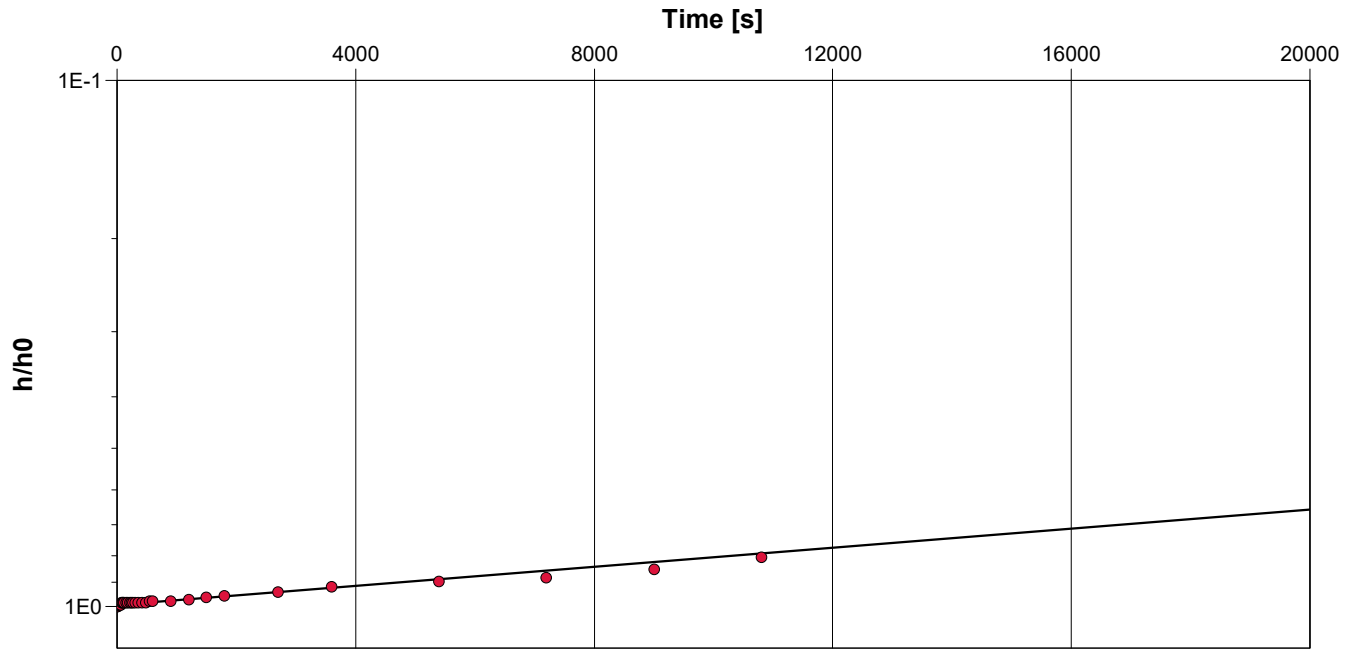
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH102	Test Well: BH102
Test Conducted by: OM		Test Date: 2021-05-10
Analysis Performed by: DK	RHT-BH102	Analysis Date: 2021-05-13
Aquifer Thickness: 6.30 m		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [m/s]	
BH102	$1.65 \times 10^{-8}$	



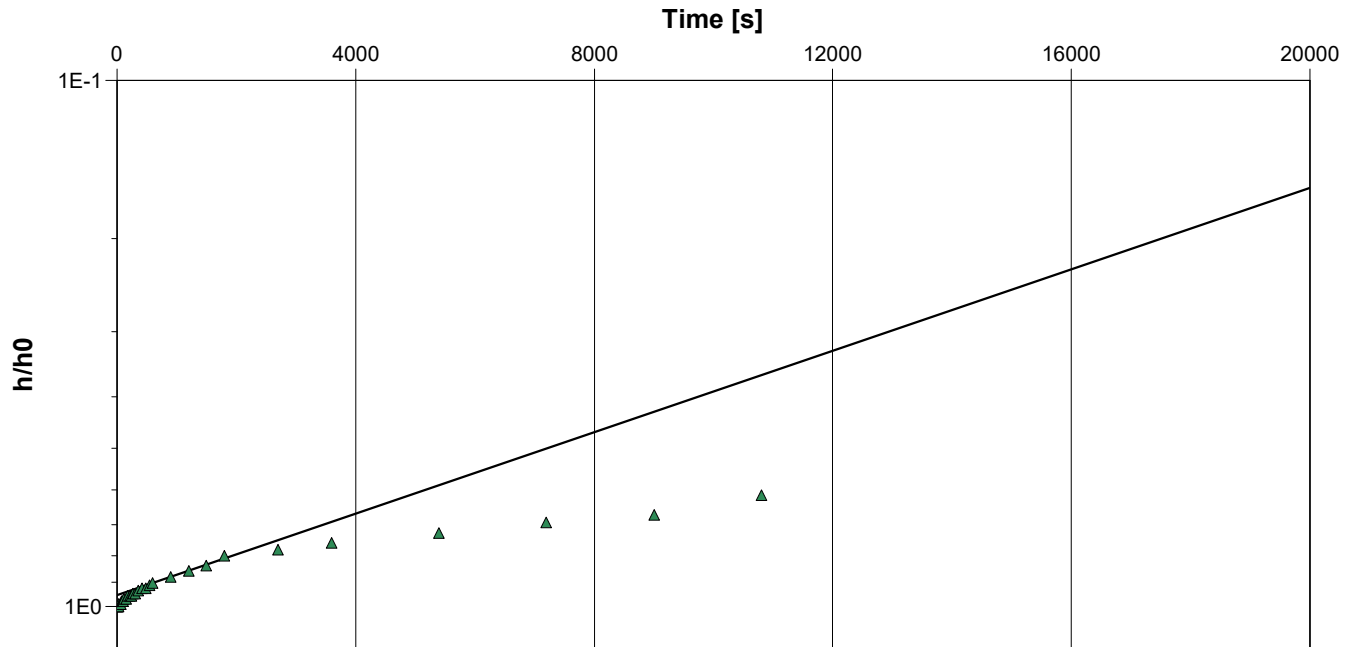
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH103	Test Well: BH103
Test Conducted by: OM		Test Date: 2021-05-11
Analysis Performed by: DK	RHT-BH103	Analysis Date: 2021-05-13
Aquifer Thickness: 6.30 m		



Calculation using Bouwer & Rice

Observation Well	Hydraulic Conductivity [m/s]
BH103	$6.23 \times 10^{-8}$



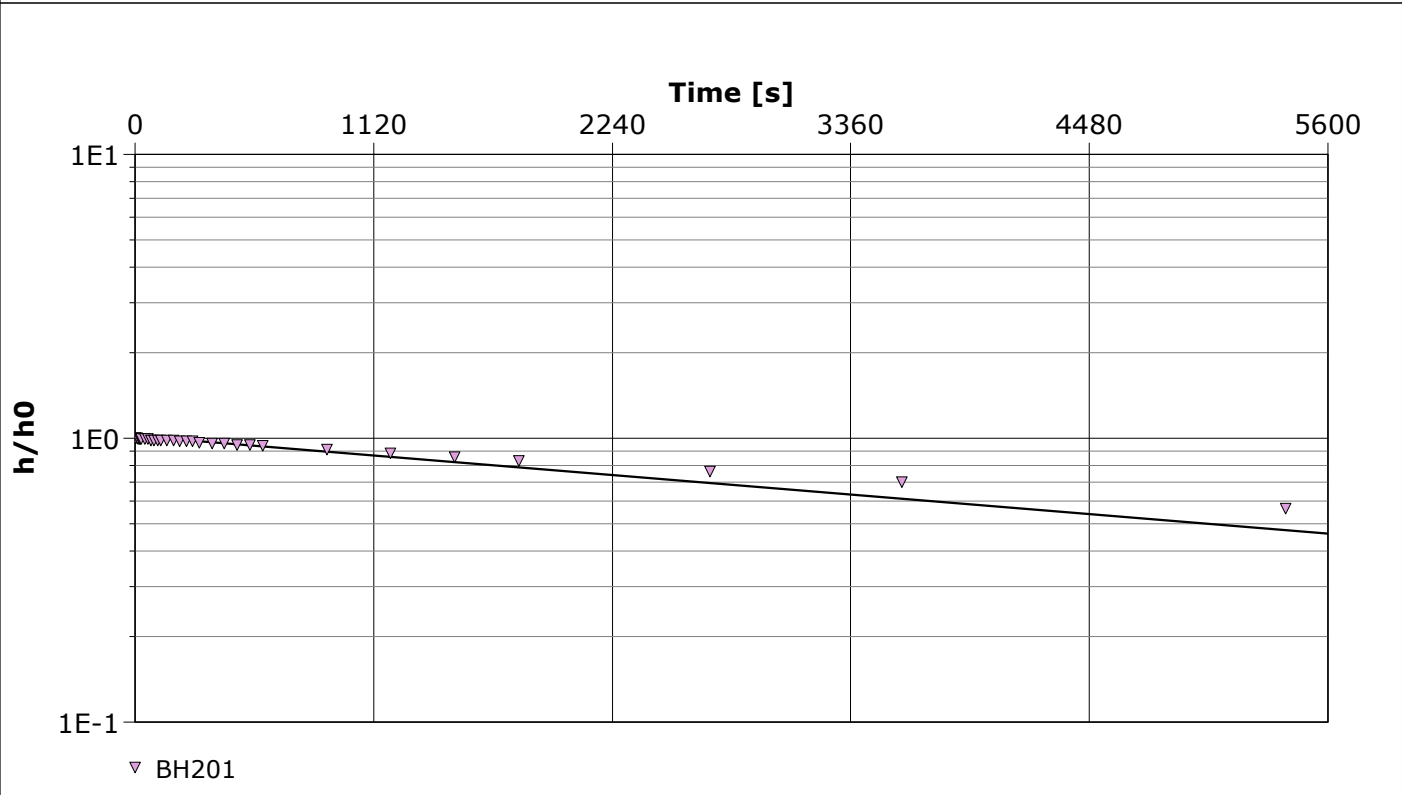
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH201	Test Well: BH201
Test Conducted by: FR		Test Date: 2022-03-30
Analysis Performed by: NP	BH201 RHT	Analysis Date: 2022-04-04
Aquifer Thickness: 25.00 m		



Calculation using Bouwer & Rice

Observation Well	Hydraulic Conductivity [m/s]
BH201	$1.14 \times 10^{-8}$



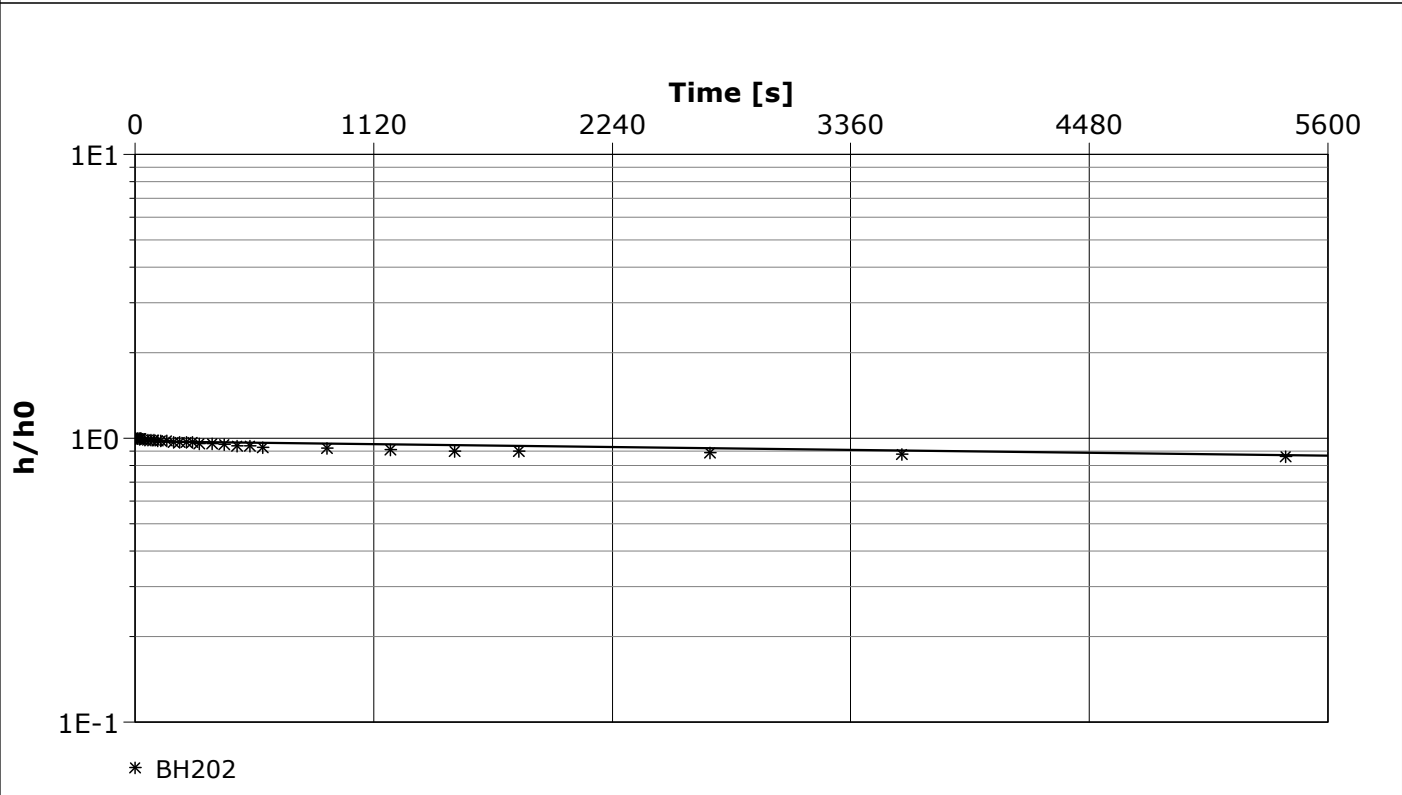
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH202	Test Well: BH202
Test Conducted by: NP		Test Date: 2022-04-04
Analysis Performed by: NP	BH202 RHT	Analysis Date: 2022-04-04
Aquifer Thickness: 4.70 m		



Calculation using Bouwer & Rice

Observation Well	Hydraulic Conductivity [m/s]
BH202	$1.54 \times 10^{-8}$



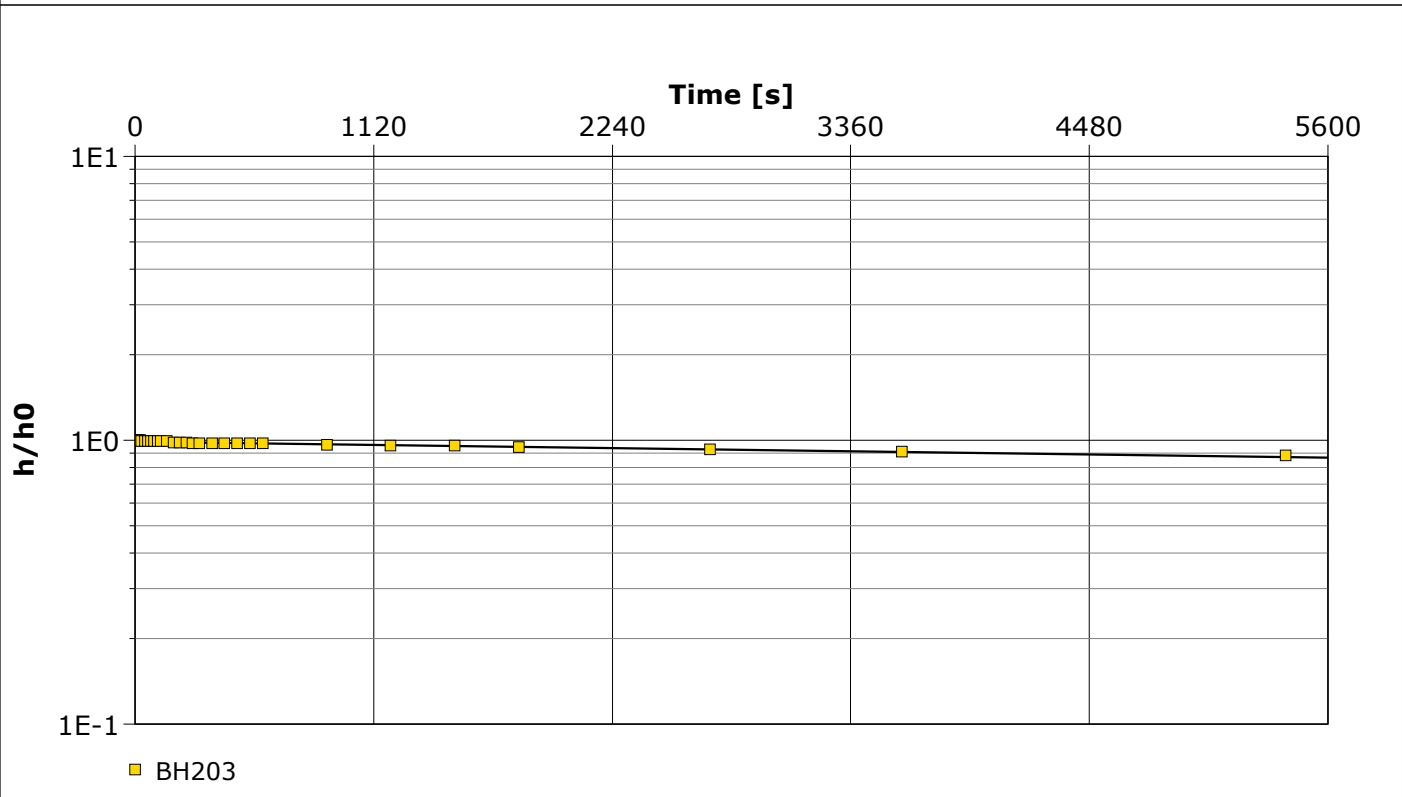
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH203	Test Well: BH203
Test Conducted by:		Test Date: 2022-03-31
Analysis Performed by: NP	BH203 RHT	Analysis Date: 2022-04-04
Aquifer Thickness: 25.00 m		



Calculation using Bouwer & Rice

Observation Well	Hydraulic Conductivity [m/s]
BH203	$5.33 \times 10^{-9}$



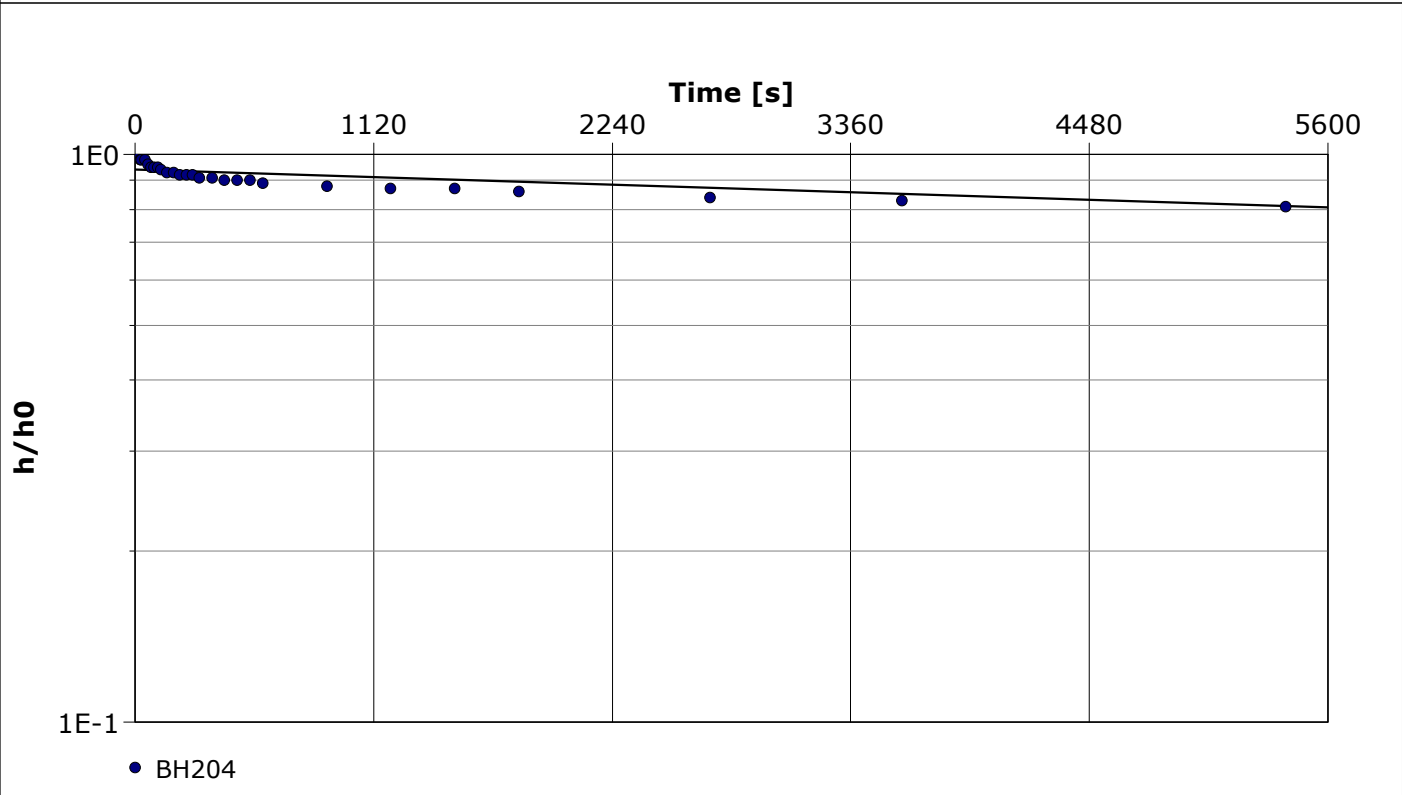
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH204	Test Well: BH204
Test Conducted by: DI		Test Date: 2022-03-31
Analysis Performed by: NP	B204 RHT	Analysis Date: 2022-04-04
Aquifer Thickness: 7.00 m		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [m/s]	
BH204	$1.05 \times 10^{-8}$	



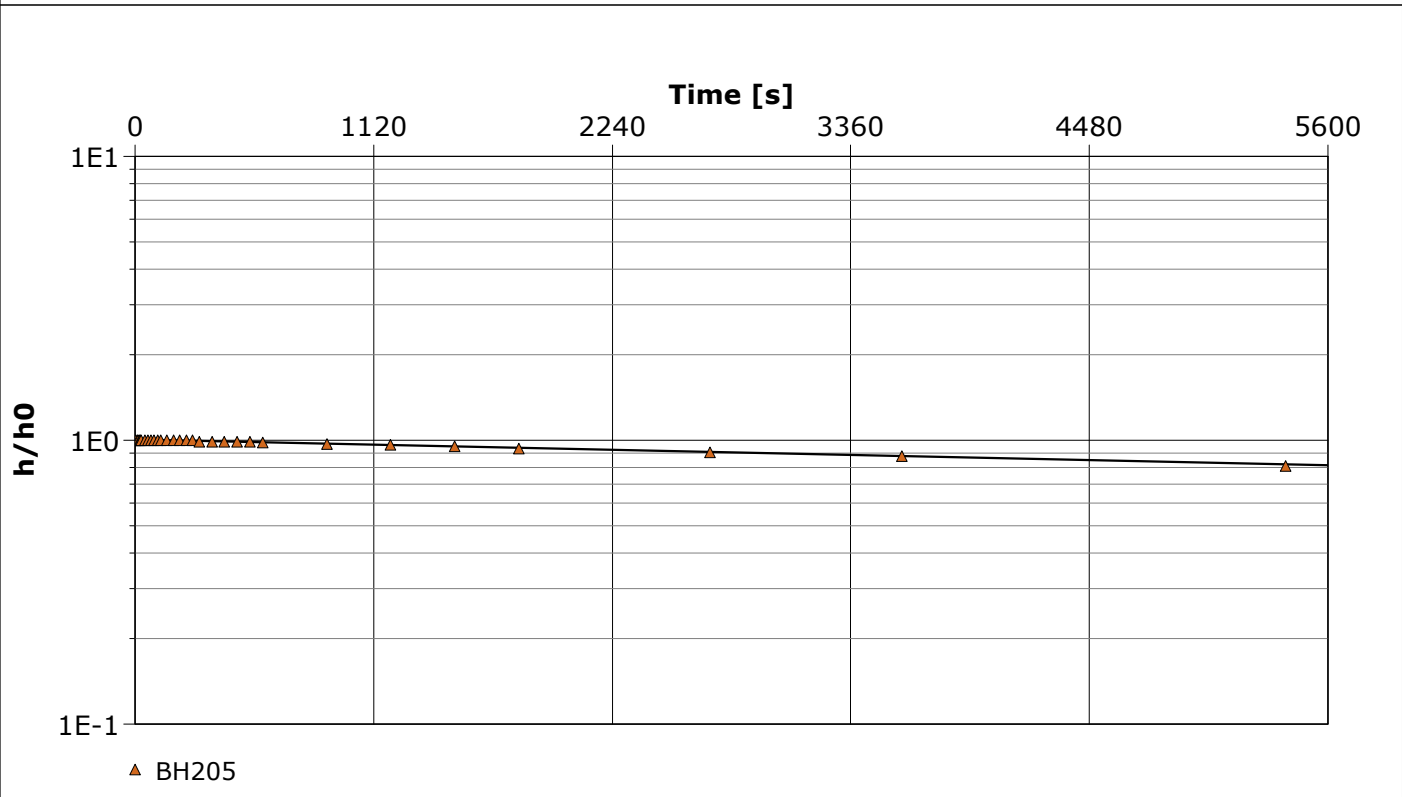
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH205	Test Well: BH205
Test Conducted by: DI		Test Date: 2022-03-31
Analysis Performed by: NP	BH205 RHT	Analysis Date: 2022-04-04
Aquifer Thickness: 25.00 m		



Calculation using Bouwer & Rice

Observation Well	Hydraulic Conductivity [m/s]	
BH205	$3.82 \times 10^{-9}$	





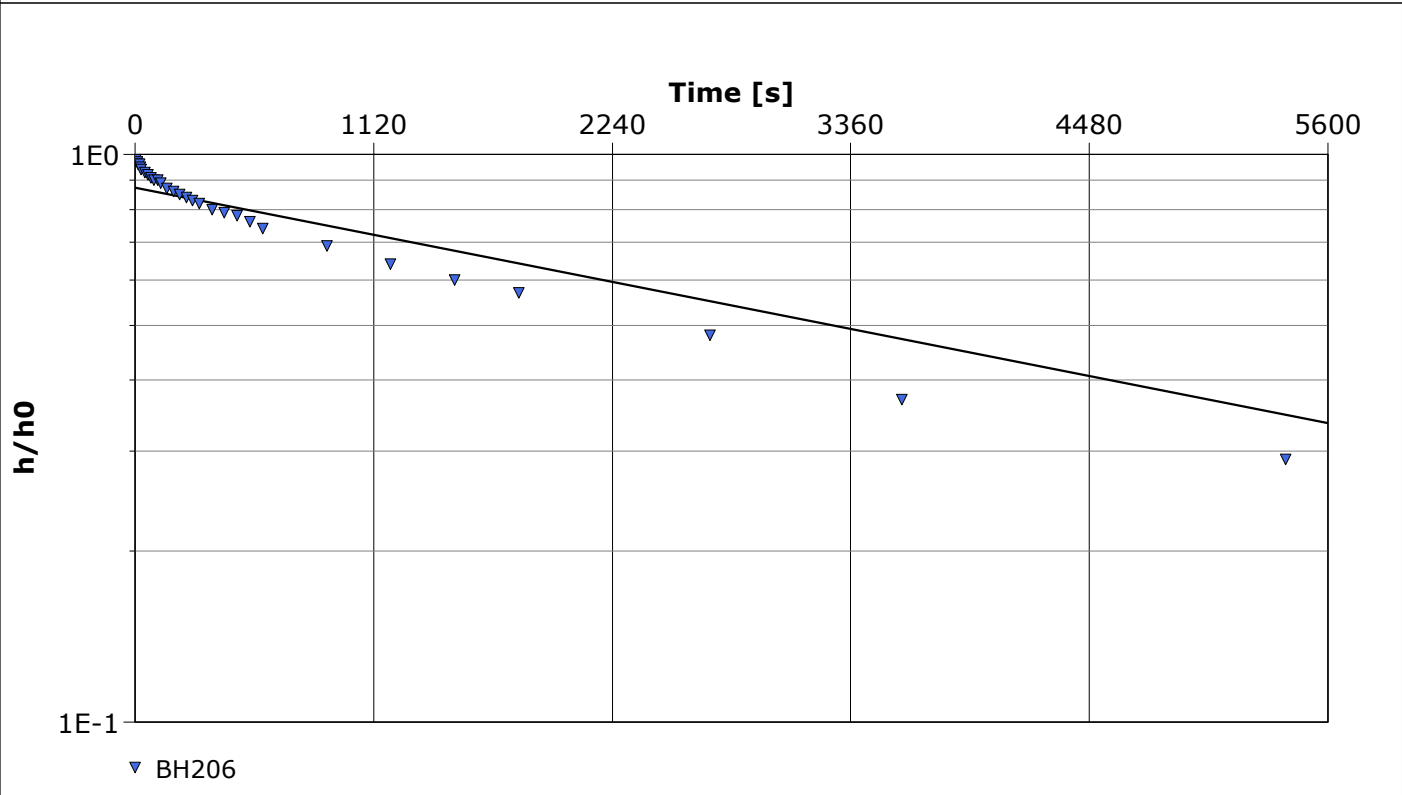
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH206	Test Well: BH206
Test Conducted by: DI		Test Date: 2022-03-31
Analysis Performed by: NP	BH206 RHT	Analysis Date: 2022-04-04
Aquifer Thickness: 6.50 m		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [m/s]	
BH206	$6.83 \times 10^{-8}$	



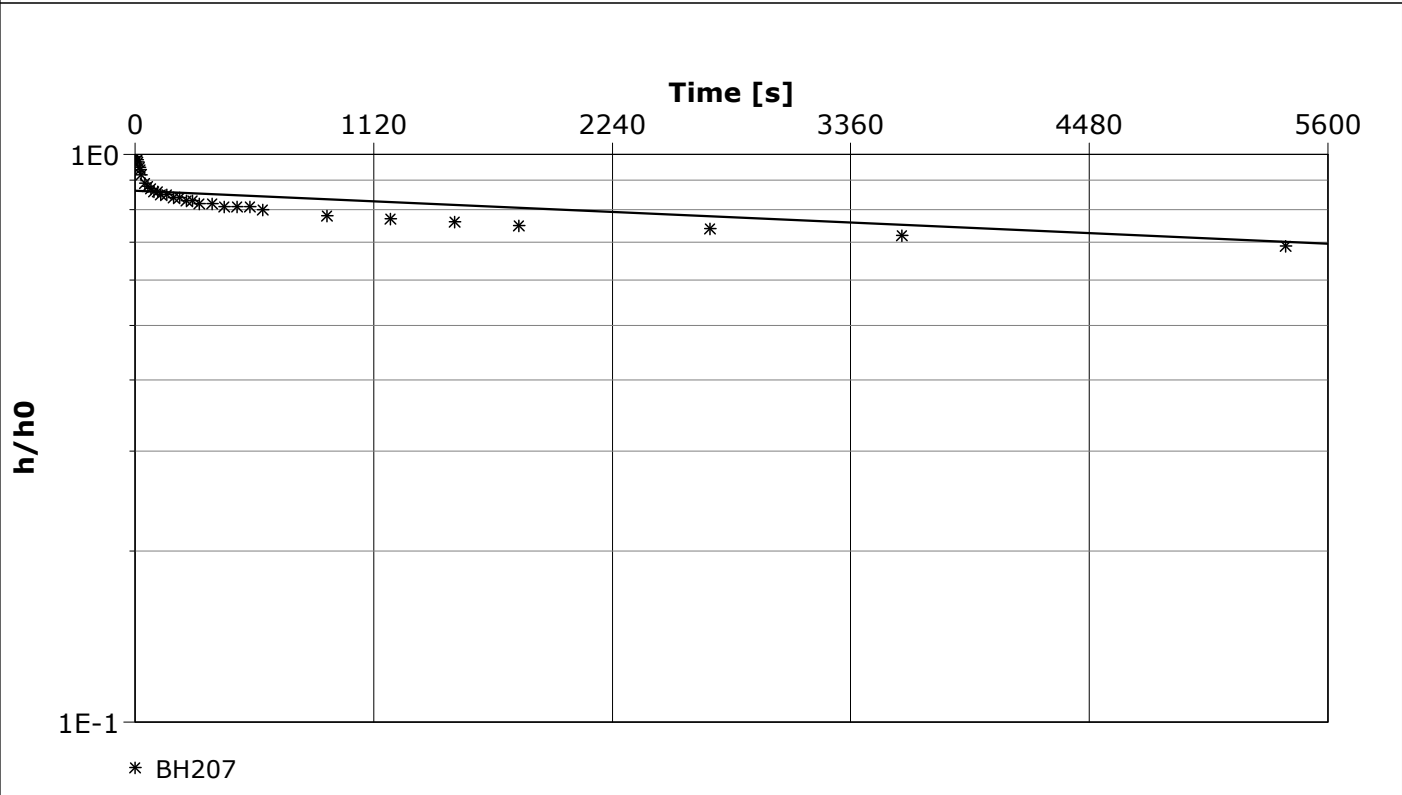
**Slug Test Analysis Report**

Project: 60 Dundas St E, Mississauga

Number: 21-067

Client: ACLP - Dundas Street E

Location: 60 Dundas St E, Mississauga	Slug Test: BH207	Test Well: BH207
Test Conducted by: DI		Test Date: 2022-03-31
Analysis Performed by: NP	BH207 RHT	Analysis Date: 2022-04-04
Aquifer Thickness: 7.00 m		



Calculation using Bouwer & Rice

Observation Well	Hydraulic Conductivity [m/s]
BH207	$1.97 \times 10^{-8}$

# APPENDIX C



## ATTERBERG LIMITS - LIQUID AND PLASTIC

LABORATORY NO.:	2102782 B	PROJECT NO.:	21TM720	DATE:	May 18, 2021
BOREHOLE NO.:	103	SAMPLE NO.:	SS4	TESTED BY:	L. Gowry
SAMPLE DEPTH:	7.5-9 ft	DESCRIPTION:		CHECKED BY:	J. Noor

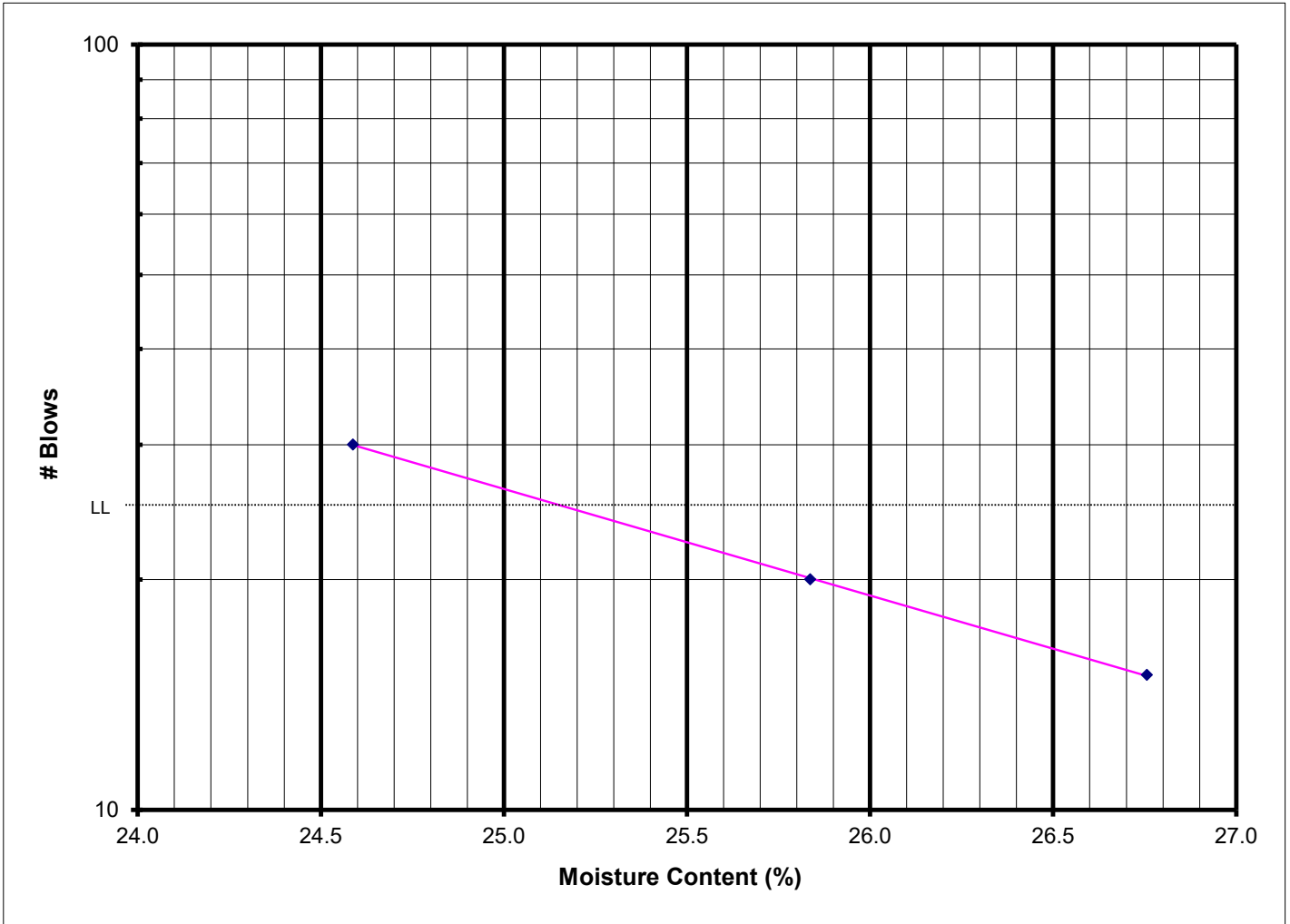
<b>LIQUID LIMIT</b>					
TRIAL	1	2	3	4	5
NUMBER OF BLOWS	30	20	15		
TARE NUMBER	H1	P4	N4		
WT. TARE & WET SOIL	43.42	42.92	39.09		
WT. TARE & DRY SOIL	38.79	38.21	35.09		
WT. OF WATER	4.63	4.71	4.00		
WT. OF TARE	19.96	19.98	20.14		
WT. OF DRY SAMPLE	18.83	18.23	14.95		
MOISTURE CONTENT	24.6	25.8	26.8		

<b>ATTERBERG LIMITS</b>		<b>PLASTIC LIMIT</b>		
LIQUID LIMIT	25	TRIAL	1	2
PLASTIC LIMIT	16	TARE NUMBER	P10	x23
PLASTICITY INDEX	9	WT. TARE & WET SOIL	27.75	27.57
		WT. TARE & DRY SOIL	26.65	26.53
		WT. OF WATER	1.10	1.04
		WT. OF TARE	19.83	20.03
		WT. OF DRY SAMPLE	6.82	6.50
		MOISTURE CONTENT	16.1	16.0

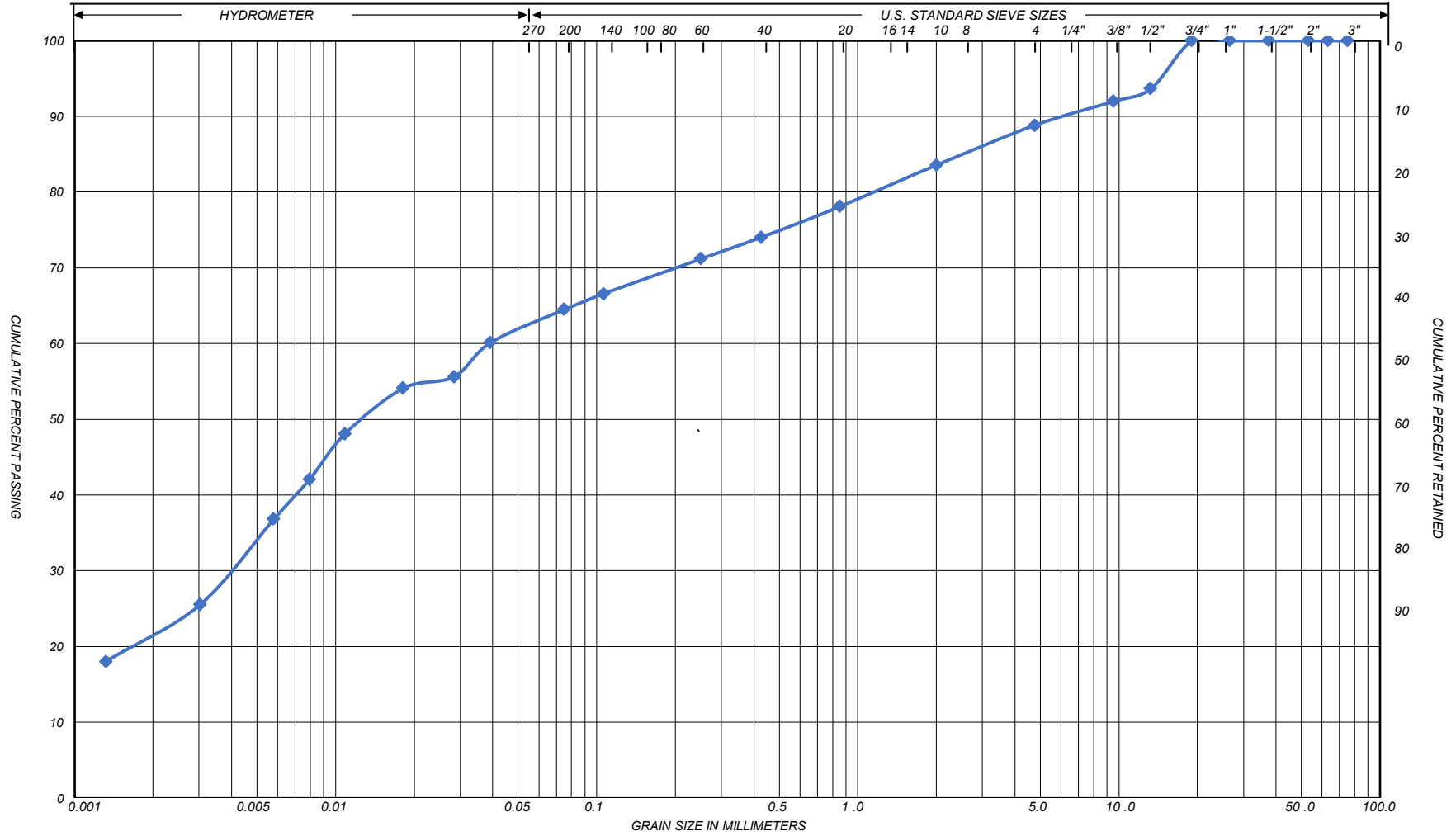
<b>LIQUID LIMIT BEST-LINE CALCULATION &amp; ASSESSMENT</b>						
LOG OF BLOWS	MOISTURE CONTENTS		ERROR EVALUATION			
			BLOW COUNT	MOISTURE CONTENT	DIFFERENCE	WITHIN 1%?
1.4771213	24.6					
1.30103	25.8		30	24.6	0.0	TRUE
1.1760913	26.8		20	25.8	0.0	TRUE
			15	26.7	0.0	TRUE
SLOPE	INTERCEPT					
-7.19268	35.20747		ERROR ASSESSMENT		PASSES	

**ATTERBERG LIMITS - LIQUID AND PLASTIC**

LABORATORY NO.:	2102782 B	PROJECT NO.:	21TM720	DATE:	May 18, 2021
BOREHOLE NO.:	103	SAMPLE NO.:	SS4	TESTED BY:	L. Gowry
SAMPLE DEPTH:	7.5-9 ft	DESCRIPTION:		CHECKED BY:	J. Noor

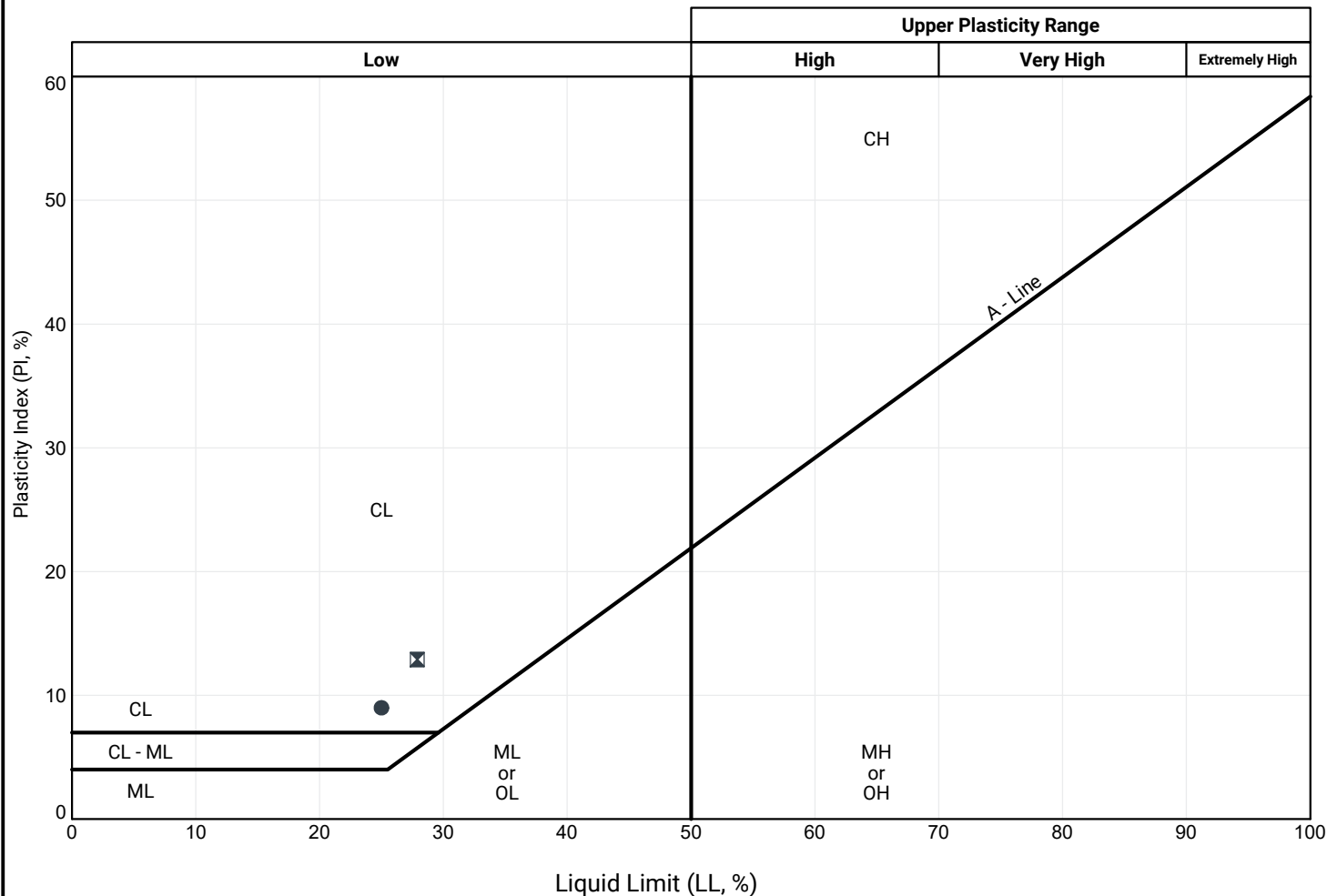


## PARTICLE SIZE DISTRIBUTION CHART

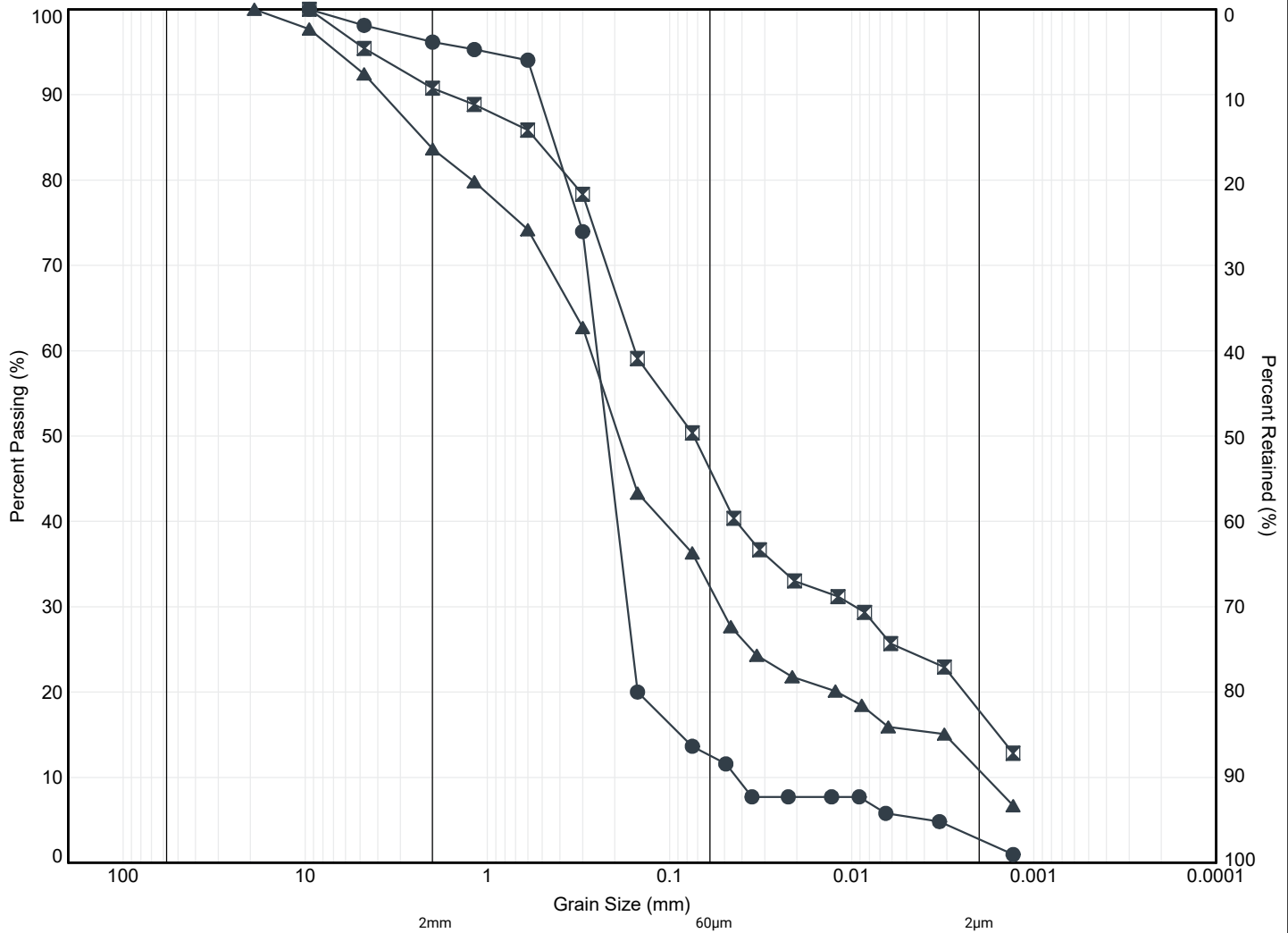


SILT & CLAY				FINE SAND			COARSE SAND	GRAVEL		COBBLES	UNIFIED
CLAY	FINE SILT	MEDIUM SILT	COARSE SILT	FINE SAND	MEDIUM SAND	COARSE SAND	GRAVEL		COBBLES	M.I.T.	
CLAY	SILT			VERY FINE SAND	FINE SAND	MEDIUM SAND	COARSE SAND	GRAVEL		U.S. BUREAU	

REMARKS Bore Hole 103, Sample No.SS4, Depth 7.5-9, Lab No.2102782-B,  
\_\_\_\_\_  
\_\_\_\_\_



Borehole	Sample	Depth (m)	Elev. (m)	LL (%)	PL (%)	PI (%)
● <b>103</b>	SS4	2.6	106.8	25	16	9
⊠ <b>206</b>	SS4	2.6	105.6	28	15	13



MIT SYSTEM	COBBLES	GRAVEL			SAND			SILT	CLAY
		COARSE	MEDIUM	FINE	COARSE	MEDIUM	FINE		

MIT SYSTEM								
Borehole	Sample	Depth (m)	Elev. (m)	Gravel (%)	Sand (%)	Silt (%)	Clay (%)	
● 203	SS3	1.8	108.5	4	83	10	3	
☒ 204	SS2	1.1	108.8	9	45	28	18	
▲ 205	SS2	1.1	108.8	16	51	22	11	

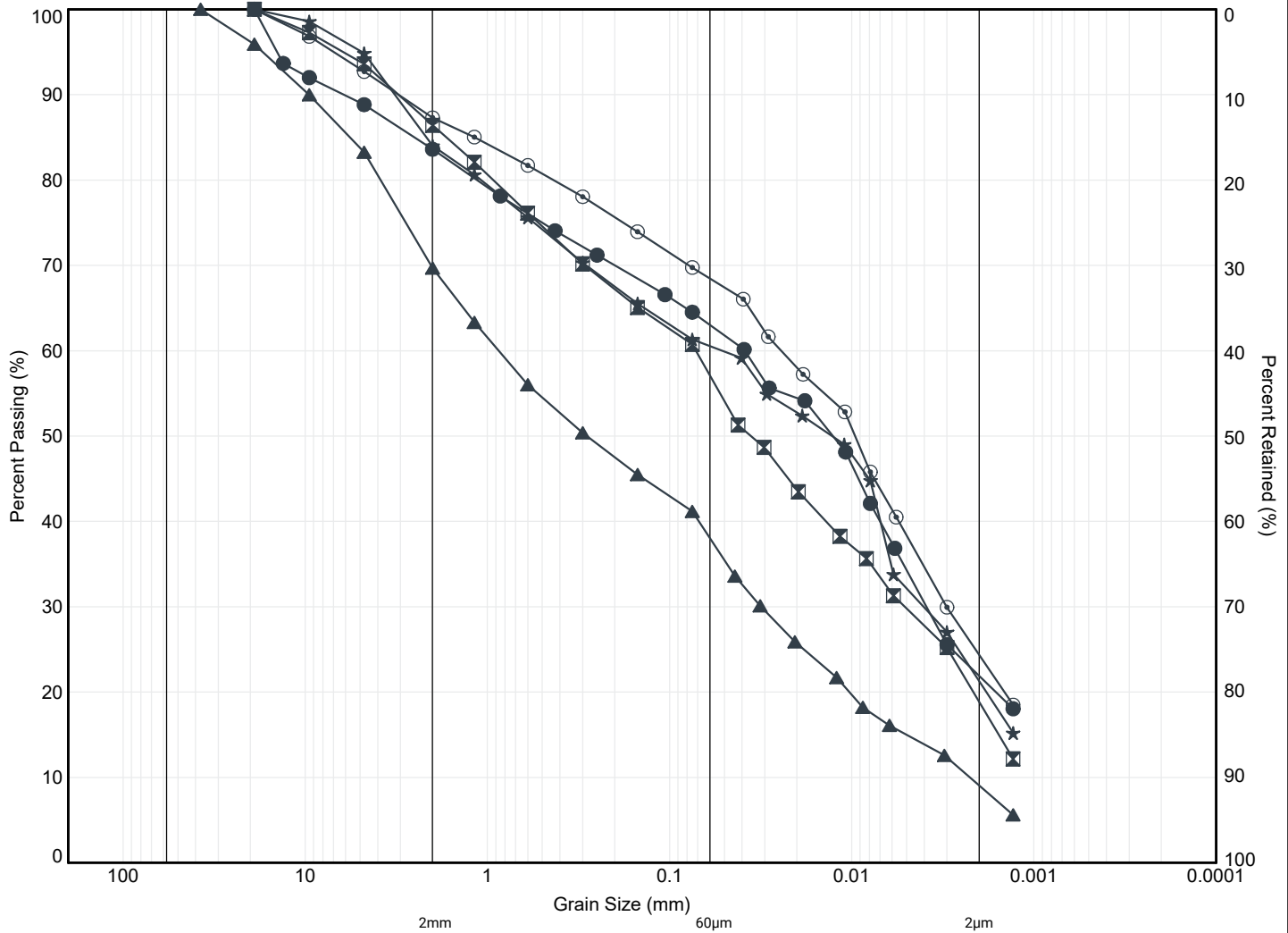
file: 21-067.gpj



Title: **GRAIN SIZE DISTRIBUTION - FILL**

File No.: **21-067**





MIT SYSTEM	COBBLES	GRAVEL			SAND			SILT	CLAY
		COARSE	MEDIUM	FINE	COARSE	MEDIUM	FINE		

MIT SYSTEM

Borehole	Sample	Depth (m)	Elev. (m)	Gravel (%)	Sand (%)	Silt (%)	Clay (%)
● 103	SS4	2.6	106.8	16	21	41	22
⊠ 201	SS5	3.4	107.2	14	29	38	19
▲ 202	SS6	4.9	104.5	30	32	29	9
★ 206	SS4	2.6	105.6	16	24	39	21
⊙ 207	SS4	2.6	106.2	13	19	44	24



Title: **GRAIN SIZE DISTRIBUTION - GLACIAL TILL**

File No.: **21-067**

# APPENDIX D





Grain Size Analysis Report

Date:

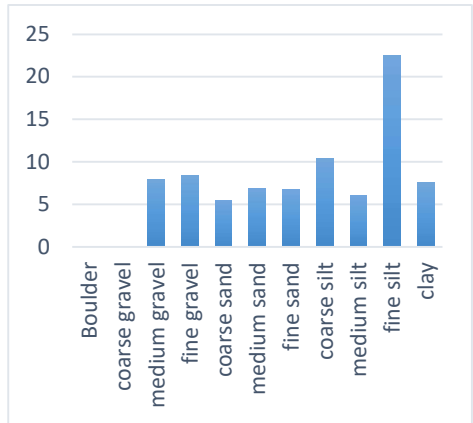
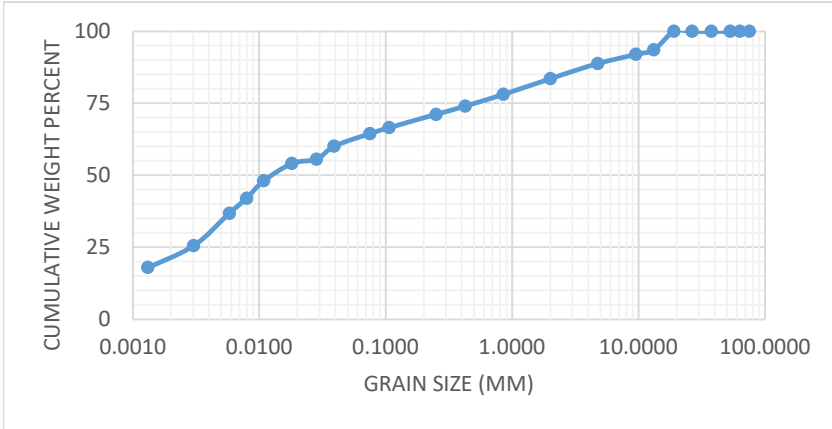
May 18, 2021

Sample Name: BH103-SS4

Mass Sample (g): 100

T (oC) 20

Poorly sorted clay with fines



Sieve opening (ps) di (mm)	Mass of retained (mr) (g)	mass fraction (mf)	Percent Passing (pp)
75	0	0	100
63	0	0	100
53	0	0	100
37.5	0	0	100
26.5	0	0	100
19	0	0	100
13.2	6.343888	0.063439	93.65611193
9.5	1.66053	0.016605	91.99558174
4.75	3.166421	0.031664	88.82916053
2	5.231959	0.05232	83.59720177
0.85	5.474125	0.054741	78.12307656
0.425	4.075182	0.040752	74.04789446
0.25	2.843504	0.028435	71.20439053
0.106	4.637801	0.046378	66.56659001
0.075	2.052797	0.020528	64.51379305
0.039035	4.369257	0.043693	60.14453568
0.028373	4.51084	0.045108	55.6336955
0.018105	1.503613	0.015036	54.13008211
0.01084	6.014454	0.060145	48.11562854
0.007931	6.014454	0.060145	42.10117498
0.005785	5.262647	0.052626	36.8385281
0.003019	11.2771	0.112771	25.56142766

Effective Grain Diameters (mm)		Other Useful Parameters	
d10	0.001	Uniformity Coef.	53.04
d17	0.001	n computed	0.26
d20	0.002	g (cm/s <sup>2</sup> )	980.00
d50	0.013	ρ (g/cm <sup>3</sup> )	0.9981
d60	0.039	μ (g/cm s)	0.0098
de (Krugler)	0.012	ρg/μ (1/cm s)	9.9327E+04
de (Kozeny)	0.005	tau (Sauerbrei)	1.053
de (Zunker)	0.005	d <sub>geometric mean</sub>	0.127
de (Zamarin)	0.005	σ <sub>φ</sub>	5.036
lo (Alyameni)	-0.002		
	mm	0	% in sample
	>64	Boulder	0
	16 - 64	coarse gravel	0
	8 - 16	medium gravel	8.004418262
	2 - 8	fine gravel	8.398379971
	0.5 - 2	coarse sand	5.474125209
	0.25 - 0.5	medium sand	6.918686028
	0.063 - 0.25	fine sand	6.690597478
	0.016 - 0.063	coarse silt	10.38371094
	0.008 - 0.016	medium silt	6.014453568
	0.002 - 0.008	fine silt	22.55420088
	<0.002	clay	7.51806696

Data continue, additional pages required ...



K from Grain Size Analysis Report

Date: 20-May-21

Sample Name:

BH103 SS4

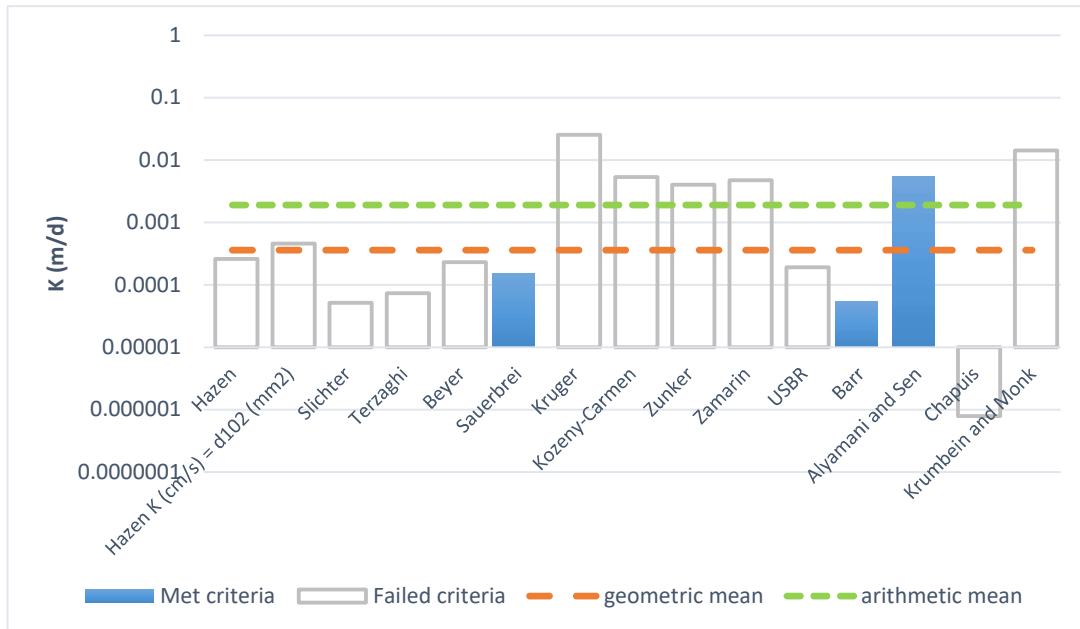
Mass Sample (g):

100

T (oC)

20

Poorly sorted clay with fines



Estimation of Hydraulic Conductivity	cm/s	m/s	m/d	de
Hazen	3.0E-07	3.0E-09	0.00	
Hazen K (cm/s) = d <sub>10</sub> (mm)	5.3E-07	5.3E-09	0.00	
Slichter	5.9E-08	5.9E-10	0.00	
Terzaghi	8.4E-08	8.4E-10	0.00	
Beyer	2.7E-07	2.7E-09	0.00	
Sauerbrei	1.8E-07	1.8E-09	0.00	
Kruger	3.0E-05	3.0E-07	0.03	
Kozeny-Carmen	6.1E-06	6.1E-08	0.01	
Zunker	4.7E-06	4.7E-08	0.00	
Zamarrin	5.5E-06	5.5E-08	0.00	
USBR	2.2E-07	2.2E-09	0.00	
Barr	6.4E-08	6.4E-10	0.00	
Alyamani and Sen	6.4E-06	6.4E-08	0.01	
Chapuis	9.1E-10	9.1E-12	0.00	
Krumbein and Monk	1.6E-05	1.6E-07	0.01	
geometric mean	4.2E-07	4.2E-09	0.00	
arithmetic mean	2.2E-06	2.2E-08	0.00	



Grain Size Analysis Report

Date:

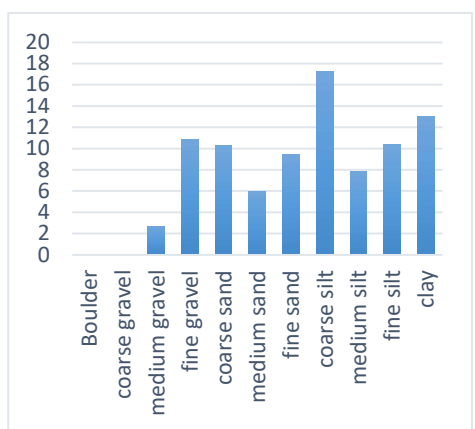
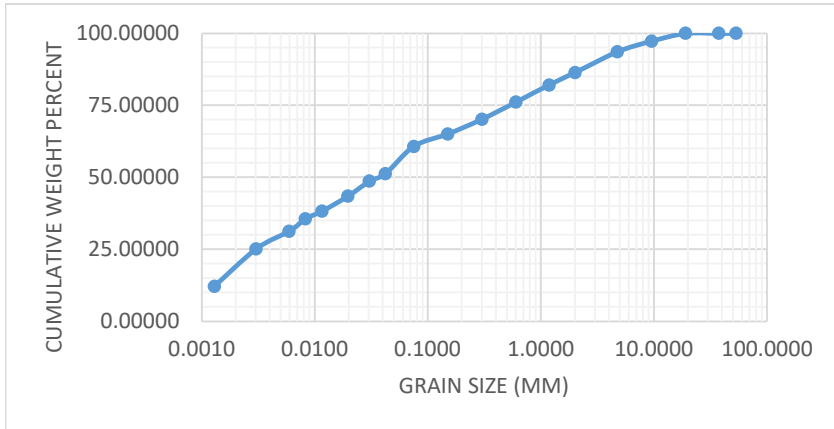
12-Apr-22

Sample Name: BH201-SS5

Mass Sample (g): 278.45

T (oC) 20

Poorly sorted sandy gravelly silt with fines



Sieve opening (ps) di (mm)	Mass of retained (mr) (g)	mass fraction (mf)	Percent Passing (pp)
53	0	0	100
37.5	0	0	100
19	0	0	100
9.5	7.56	0.02715	97.28497037
4.75	10.26	0.036847	93.6002873
2	20.01	0.071862	86.41407793
1.18	12.031	0.043207	82.09337403
0.6	16.60278	0.059626	76.13080266
0.3	16.60278	0.059626	70.16823128
0.15	14.19658	0.050984	65.06980068
0.075	12.031	0.043207	60.74909679
0.042081	26.34265	0.094605	51.28863886
0.030324	7.261689	0.026079	48.68074197
0.019601	14.52338	0.052158	43.46494819
0.011555	14.52338	0.052158	38.2491544
0.008254	7.261689	0.026079	35.64125751
0.005933	12.10281	0.043465	31.29476269
0.003033	16.94394	0.060851	25.20966995
0.001294	36.30844	0.130395	12.17018549

Effective Grain Diameters (mm)		Other Useful Parameters	
d10	0.001	Uniformity Coef.	68.07
d17	0.002	n computed	0.26
d20	0.002	g (cm/s <sup>2</sup> )	980.00
d50	0.036	ρ (g/cm <sup>3</sup> )	0.9981
d60	0.072	μ (g/cm s)	0.0098
de (Krugler)	0.011	ρg/μ (1/cm s)	9.9327E+04
de (Kozeny)	0.006	tau (Sauerbrei)	1.053
de (Zunker)	0.006	d <sub>geometric mean</sub>	0.105
de (Zamarin)	0.006	σ <sub>φ</sub>	4.494
lo (Alyameni)	-0.008		
	mm	0	% in sample
	>64	Boulder	0
	16 - 64	coarse gravel	0
	8 - 16	medium gravel	2.715029628
	2 - 8	fine gravel	10.87089244
	0.5 - 2	coarse sand	10.28327527
	0.25 - 0.5	medium sand	5.962571377
	0.063 - 0.25	fine sand	9.419134495
	0.016 - 0.063	coarse silt	17.2841486
	0.008 - 0.016	medium silt	7.823690673
	0.002 - 0.008	fine silt	10.43158756
	<0.002	clay	13.03948446



K from Grain Size Analysis Report

Date: 12-Apr-22

Sample Name:

BH201-SS5

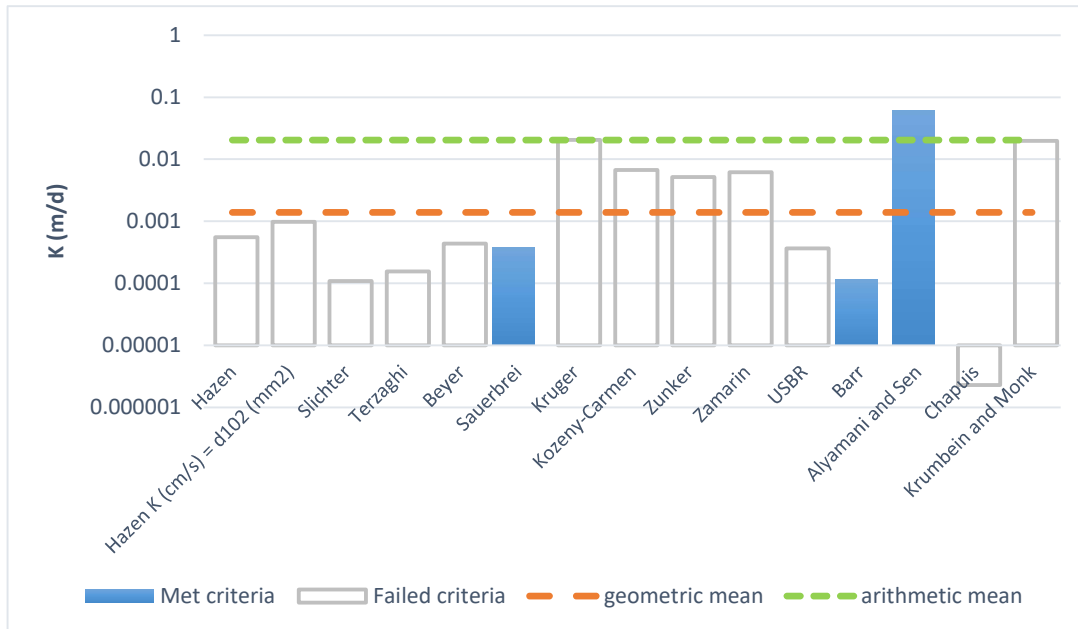
Mass Sample (g):

278.45

T (oC)

20

Poorly sorted sandy gravelly silt with fines



Estimation of Hydraulic Conductivity	cm/s	m/s	m/d	de
Hazen	6.4E-07	6.4E-09	0.00	
Hazen K (cm/s) = d <sub>10</sub> (mm)	1.1E-06	1.1E-08	0.00	
Slichter	1.3E-07	1.3E-09	0.00	
Terzaghi	1.8E-07	1.8E-09	0.00	
Beyer	5.1E-07	5.1E-09	0.00	
Sauerbrei	4.4E-07	4.4E-09	0.00	
Kruger	2.4E-05	2.4E-07	0.02	
Kozeny-Carmen	7.7E-06	7.7E-08	0.01	
Zunker	6.0E-06	6.0E-08	0.01	
Zamarin	7.2E-06	7.2E-08	0.01	
USBR	4.2E-07	4.2E-09	0.00	
Barr	1.3E-07	1.3E-09	0.00	
Alyamani and Sen	7.1E-05	7.1E-07	0.06	
Chapuis	2.6E-09	2.6E-11	0.00	
Krumbein and Monk	2.3E-05	2.3E-07	0.02	
geometric mean	1.6E-06	1.6E-08	0.00	
arithmetic mean	2.4E-05	2.4E-07	0.02	



Grain Size Analysis Report

Date:

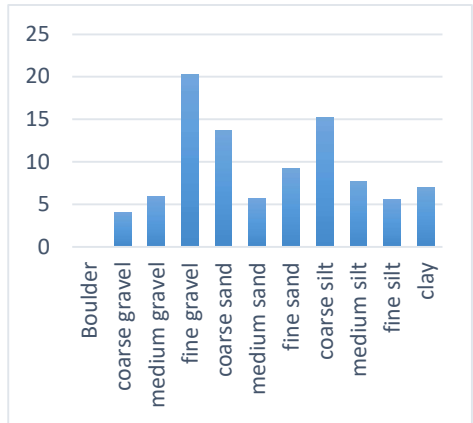
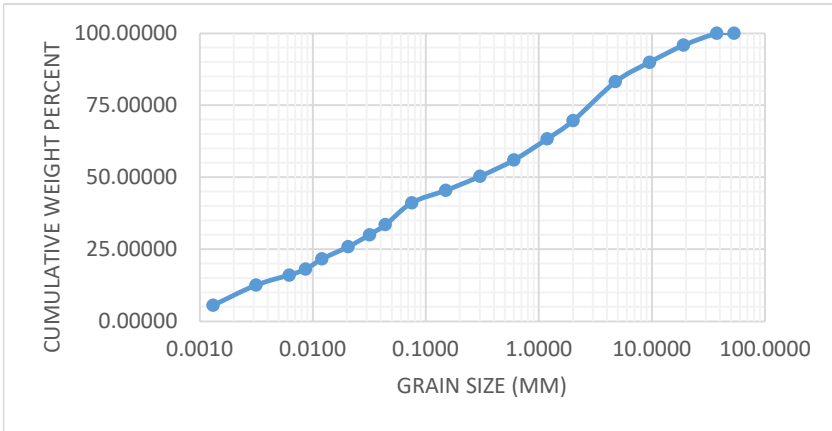
12-Apr-22

Sample Name: BH202-SS6

Mass Sample (g): 214.37

T (oC) 20

Poorly sorted gravelly sand with fines



Sieve opening (ps) di (mm)	Mass of retained (mr) (g)	mass fraction (mf)	Percent Passing (pp)
53	0	0	100
37.5	0	0	100
19	8.77	0.040911	95.90894248
9.5	12.72	0.059337	89.97527639
4.75	14.39	0.067127	83.26258338
2	29.14	0.135933	69.66926342
1.18	13.59085	0.063399	63.32936045
0.6	15.68175	0.073153	56.01408779
0.3	12.09735	0.056432	50.37087745
0.15	10.4545	0.048768	45.49402902
0.075	9.2597	0.043195	41.17453468
0.043829	16.24654	0.075787	33.59579741
0.031753	7.502012	0.034996	30.09623518
0.020486	9.002414	0.041995	25.89676051
0.012056	9.002414	0.041995	21.69728583
0.008658	7.502012	0.034996	18.1977236
0.006177	4.501207	0.020997	16.09798626
0.003134	7.502012	0.034996	12.59842403
0.001316	15.00402	0.069991	5.599299569

Effective Grain Diameters (mm)		Other Useful Parameters	
d10	0.002	Uniformity Coef.	372.47
d17	0.007	n computed	0.26
d20	0.010	g (cm/s <sup>2</sup> )	980.00
d50	0.289	ρ (g/cm <sup>3</sup> )	0.9981
d60	0.916	μ (g/cm s)	0.0098
de (Kruger)	0.019	ρg/μ (1/cm s)	9.9327E+04
de (Kozeny)	0.011	tau (Sauerbrei)	1.053
de (Zunker)	0.011	d <sub>geometric mean</sub>	0.306
de (Zamarin)	0.011	σ <sub>φ</sub>	4.540
lo (Alyameni)	-0.069		
	mm	0	% in sample
	>64	Boulder	
	16 - 64	coarse gravel	4.091057517
	8 - 16	medium gravel	5.933666091
	2 - 8	fine gravel	20.30601297
	0.5 - 2	coarse sand	13.65517563
	0.25 - 0.5	medium sand	5.643210337
	0.063 - 0.25	fine sand	9.196342772
	0.016 - 0.063	coarse silt	15.27777418
	0.008 - 0.016	medium silt	7.699036908
	0.002 - 0.008	fine silt	5.599299569
	<0.002	clay	6.999124461



K from Grain Size Analysis Report

Date: 12-Apr-22

Sample Name:

BH202-SS6

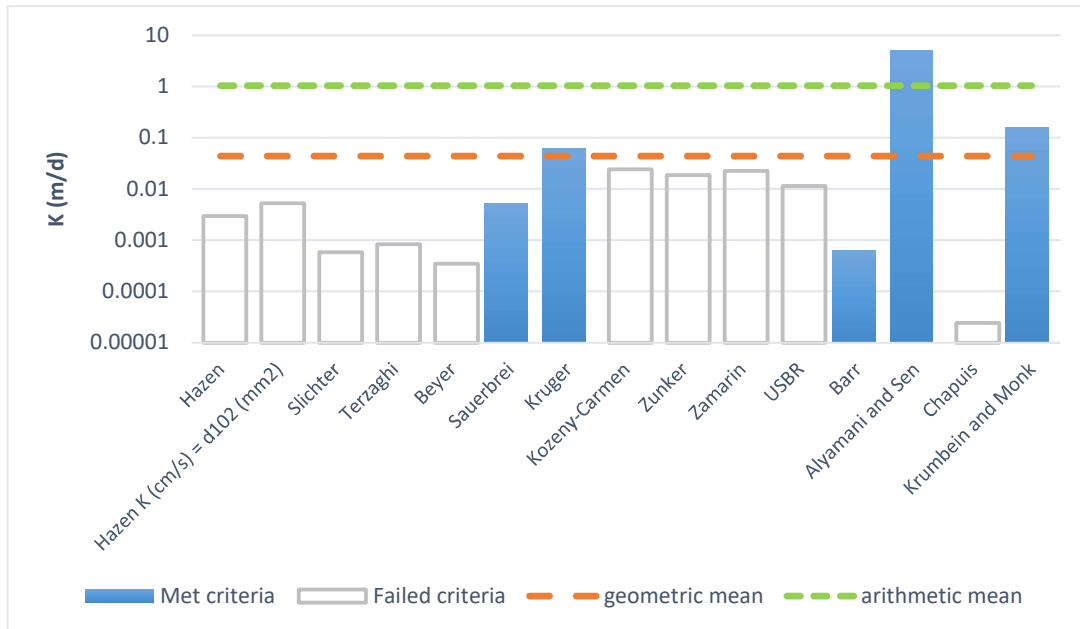
Mass Sample (g):

214.37

T (oC)

20

Poorly sorted gravelly sand with fines



Estimation of Hydraulic Conductivity	cm/s	m/s	m/d	de
Hazen	3.4E-06	3.4E-08	0.00	
Hazen K (cm/s) = d <sub>10</sub> (mm)	6.0E-06	6.0E-08	0.01	
Slichter	6.7E-07	6.7E-09	0.00	
Terzaghi	9.6E-07	9.6E-09	0.00	
Beyer	4.0E-07	4.0E-09	0.00	
Sauerbrei	6.1E-06	6.1E-08	0.01	
Kruger	7.2E-05	7.2E-07	0.06	
Kozeny-Carmen	2.8E-05	2.8E-07	0.02	
Zunker	2.2E-05	2.2E-07	0.02	
Zamarin	2.6E-05	2.6E-07	0.02	
USBR	1.3E-05	1.3E-07	0.01	
Barr	7.2E-07	7.2E-09	0.00	
Alyamani and Sen	5.8E-03	5.8E-05	4.98	
Chapuis	2.8E-08	2.8E-10	0.00	
Krumbein and Monk	1.8E-04	1.8E-06	0.16	
geometric mean	5.1E-05	5.1E-07	0.04	
arithmetic mean	1.2E-03	1.2E-05	1.04	





Grain Size Analysis Report

Date:

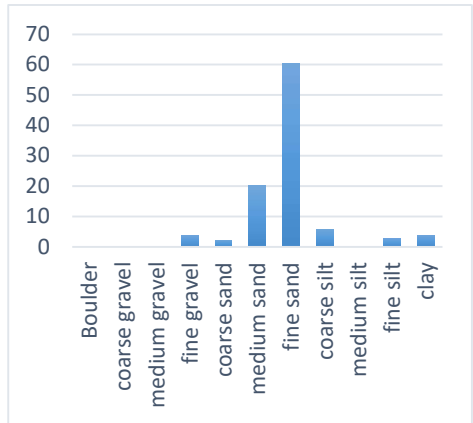
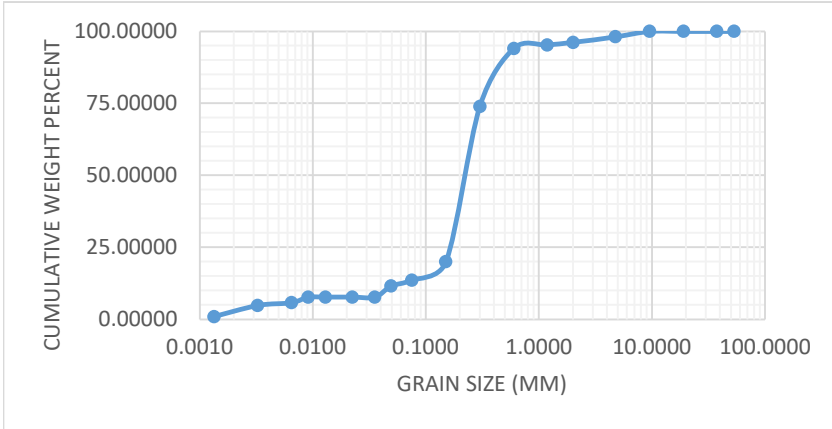
12-Apr-22

Sample Name: BH203-SS3

Mass Sample (g): 164.57

T (oC) 20

Poorly sorted sand with fines



Sieve opening (ps) di (mm)	Mass of retained (mr) (g)	mass fraction (mf)	Percent Passing (pp)
53	0	0	100
37.5	0	0	100
19	0	0	100
9.5	0	0	100
4.75	3.09	0.018776	98.12237953
2	3.23	0.019627	96.15968889
1.18	1.42425	0.008654	95.29425169
0.6	2.05725	0.012501	94.04417573
0.3	33.07425	0.200974	73.94680075
0.15	88.77825	0.539456	20.00121529
0.075	10.4445	0.063465	13.65467582
0.049116	3.419259	0.020777	11.57698333
0.035315	6.350747	0.03859	7.717988889
0.022335	0	0	7.717988889
0.012895	0	0	7.717988889
0.009118	0	0	7.717988889
0.006483	3.175374	0.019295	5.788491667
0.00325	1.587687	0.009647	4.823743056
0.001341	6.350747	0.03859	0.964748611

Effective Grain Diameters (mm)		Other Useful Parameters	
d10	0.043	Uniformity Coef.	6.01
d17	0.115	n computed	0.34
d20	0.150	g (cm/s <sup>2</sup> )	980.00
d50	0.233	ρ (g/cm <sup>3</sup> )	0.9981
d60	0.261	μ (g/cm s)	0.0098
de (Kruger)	0.039	ρg/μ (1/cm s)	9.9327E+04
de (Kozeny)	0.028	tau (Sauerbrei)	1.053
de (Zunker)	0.029	d <sub>geometric mean</sub>	0.191
de (Zamarin)	0.030	σ <sub>φ</sub>	1.758
lo (Alyameni)	-0.004		
	mm	0	% in sample
	>64	Boulder	
	16 - 64	coarse gravel	0
	8 - 16	medium gravel	0
	2 - 8	fine gravel	3.840311114
	0.5 - 2	coarse sand	2.115513155
	0.25 - 0.5	medium sand	20.09737498
	0.063 - 0.25	fine sand	60.29212493
	0.016 - 0.063	coarse silt	5.936686933
	0.008 - 0.016	medium silt	0
	0.002 - 0.008	fine silt	2.894245833
	<0.002	clay	3.858994444



K from Grain Size Analysis Report

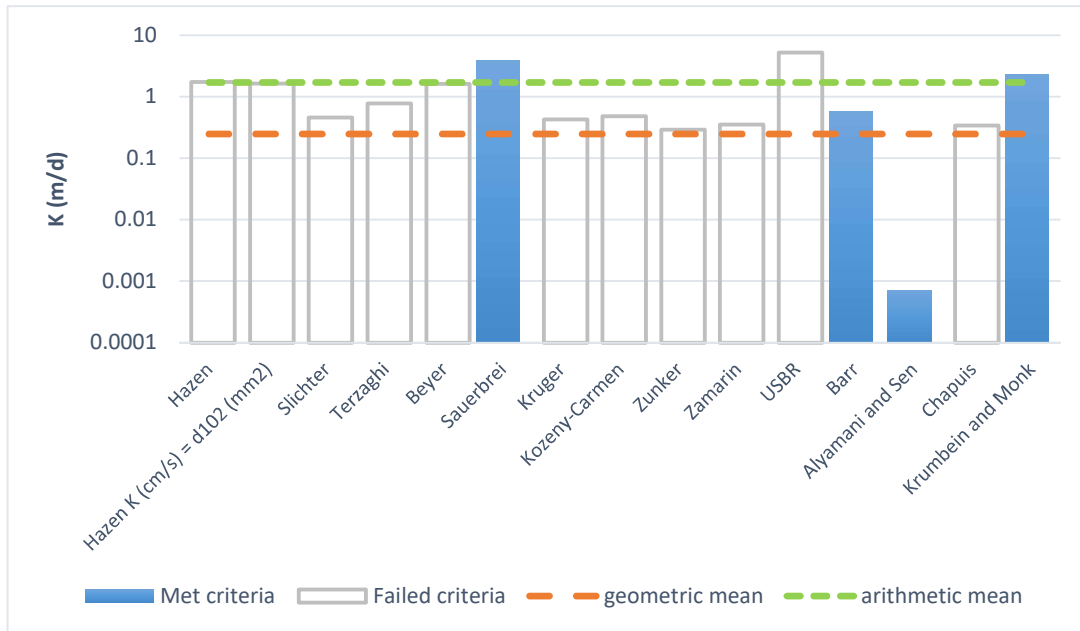
Date: 12-Apr-22

Sample Name: BH203-SS3

Mass Sample (g): 164.57

T (oC) 20

Poorly sorted sand with fines



Estimation of Hydraulic Conductivity	cm/s	m/s	m/d	de
Hazen	2.0E-03	2.0E-05	1.73	
Hazen K (cm/s) = d <sub>10</sub> (mm)	1.9E-03	1.9E-05	1.63	
Slichter	5.3E-04	5.3E-06	0.46	
Terzaghi	9.0E-04	9.0E-06	0.78	
Beyer	1.9E-03	1.9E-05	1.62	
Sauerbrei	4.5E-03	4.5E-05	3.93	
Kruger	5.0E-04	5.0E-06	0.43	
Kozeny-Carmen	5.6E-04	5.6E-06	0.48	
Zunker	3.4E-04	3.4E-06	0.29	
Zamarin	4.1E-04	4.1E-06	0.35	
USBR	6.1E-03	6.1E-05	5.24	
Barr	6.7E-04	6.7E-06	0.58	
Alyamani and Sen	8.3E-07	8.3E-09	0.00	
Chapuis	3.9E-04	3.9E-06	0.34	
Krumbein and Monk	2.7E-03	2.7E-05	2.34	
geometric mean	2.9E-04	2.9E-06	0.25	
arithmetic mean	2.0E-03	2.0E-05	1.71	



Grain Size Analysis Report

Date:

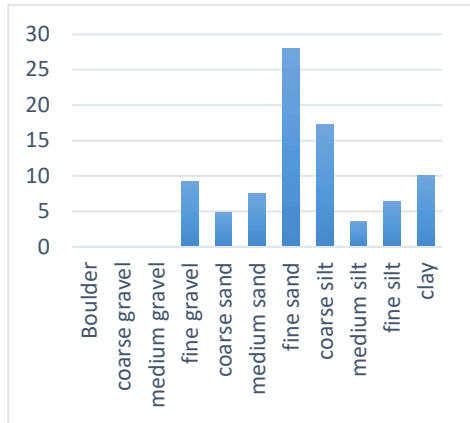
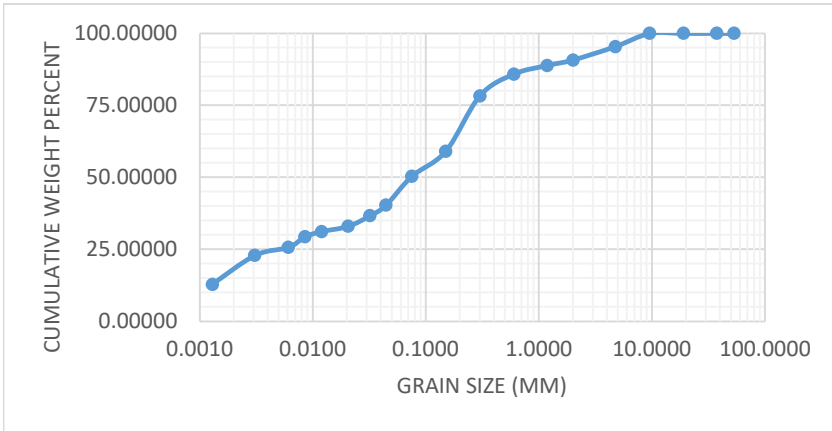
12-Apr-22

Sample Name: BH204-SS2

Mass Sample (g): 185.97

T (oC) 20

Poorly sorted sand with fines



Sieve opening (ps) di (mm)	Mass of retained (mr) (g)	mass fraction (mf)	Percent Passing (pp)
53	0	0	100
37.5	0	0	100
19	0	0	100
9.5	0	0	100
4.75	8.5	0.045706	95.42937033
2	8.7	0.046782	90.75119643
1.18	3.54417	0.019058	88.8454213
0.6	5.56941	0.029948	85.85063182
0.3	14.00791	0.075323	78.31828252
0.15	35.77924	0.192393	59.07902888
0.075	16.20192	0.087121	50.36691402
0.044448	18.61292	0.100086	40.3583535
0.032074	6.82313	0.036689	36.68941227
0.020553	6.82313	0.036689	33.02047104
0.011943	3.411565	0.018345	31.18600043
0.008498	3.411565	0.018345	29.35152982
0.006085	6.82313	0.036689	25.68258859
0.00307	5.117348	0.027517	22.93088267
0.001294	18.76361	0.100896	12.84129429

Effective Grain Diameters (mm)		Other Useful Parameters	
d10	0.001	Uniformity Coef.	155.94
d17	0.002	n computed	0.26
d20	0.003	g (cm/s <sup>2</sup> )	980.00
d50	0.074	ρ (g/cm <sup>3</sup> )	0.9981
d60	0.157	μ (g/cm s)	0.0098
de (Kruger)	0.015	ρg/μ (1/cm s)	9.9327E+04
de (Kozeny)	0.007	tau (Sauerbrei)	1.053
de (Zunker)	0.007	d <sub>geometric mean</sub>	0.126
de (Zamarin)	0.007	σ <sub>φ</sub>	4.026
lo (Alyameni)	-0.017		
	mm	0	% in sample
	>64	Boulder	
	16 - 64	coarse gravel	0
	8 - 16	medium gravel	0
	2 - 8	fine gravel	9.24880357
	0.5 - 2	coarse sand	4.900564607
	0.25 - 0.5	medium sand	7.532349304
	0.063 - 0.25	fine sand	27.9513685
	0.016 - 0.063	coarse silt	17.34644297
	0.008 - 0.016	medium silt	3.668941227
	0.002 - 0.008	fine silt	6.420647147
	<0.002	clay	10.08958837



K from Grain Size Analysis Report

Date: 12-Apr-22

Sample Name:

BH204-SS2

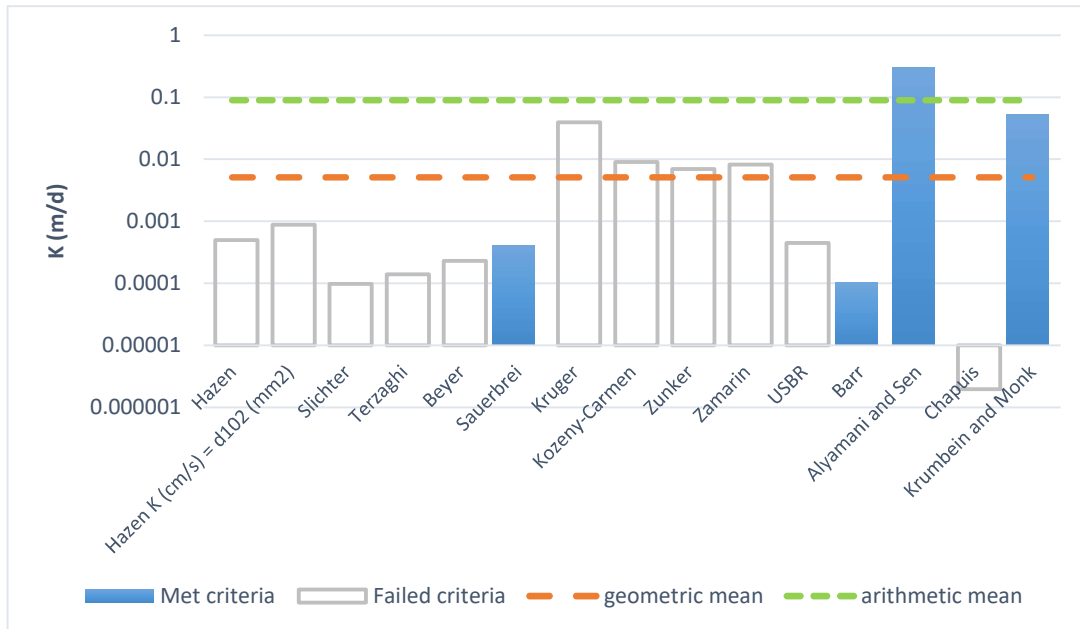
Mass Sample (g):

185.97

T (oC)

20

Poorly sorted sand with fines



Estimation of Hydraulic Conductivity	cm/s	m/s	m/d	de
Hazen	5.8E-07	5.8E-09	0.00	
Hazen K (cm/s) = d <sub>10</sub> (mm)	1.0E-06	1.0E-08	0.00	
Slichter	1.1E-07	1.1E-09	0.00	
Terzaghi	1.6E-07	1.6E-09	0.00	
Beyer	2.7E-07	2.7E-09	0.00	
Sauerbrei	4.8E-07	4.8E-09	0.00	
Kruger	4.5E-05	4.5E-07	0.04	
Kozeny-Carmen	1.0E-05	1.0E-07	0.01	
Zunker	8.0E-06	8.0E-08	0.01	
Zamarin	9.5E-06	9.5E-08	0.01	
USBR	5.2E-07	5.2E-09	0.00	
Barr	1.2E-07	1.2E-09	0.00	
Alyamani and Sen	3.6E-04	3.6E-06	0.31	
Chapuis	2.3E-09	2.3E-11	0.00	
Krumbein and Monk	6.0E-05	6.0E-07	0.05	
geometric mean	5.9E-06	5.9E-08	0.01	
arithmetic mean	1.0E-04	1.0E-06	0.09	



Grain Size Analysis Report

Date:

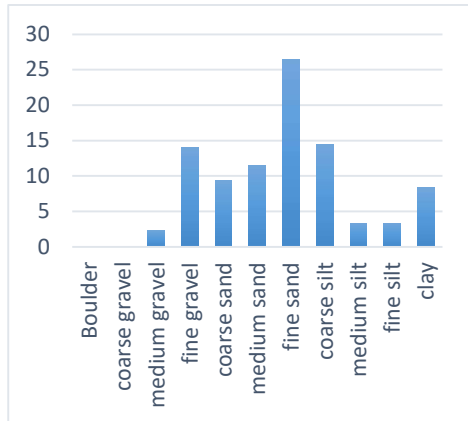
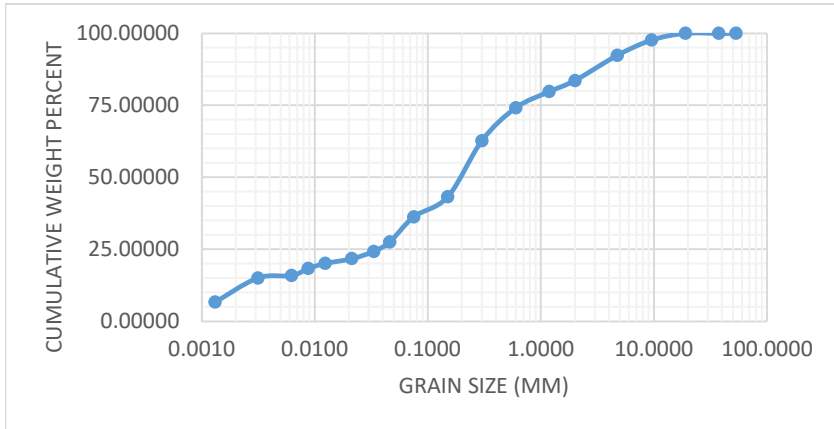
12-Apr-22

Sample Name: BH205-SS2

Mass Sample (g): 157.26

T (oC) 20

Poorly sorted gravelly sand with fines



Sieve opening (ps) di (mm)	Mass of retained (mr) (g)	mass fraction (mf)	Percent Passing (pp)
53	0	0	100
37.5	0	0	100
19	0	0	100
9.5	3.64	0.023146	97.68536182
4.75	8.27	0.052588	92.42655475
2	13.82	0.08788	83.63856035
1.18	6.05038	0.038474	79.79118657
0.6	8.81251	0.056038	74.18740303
0.3	18.01961	0.114585	62.72892026
0.15	30.51496	0.194041	43.32477426
0.075	11.04852	0.070256	36.29913519
0.046106	13.59504	0.086449	27.65419325
0.033224	5.271392	0.03352	24.30216983
0.021207	3.953544	0.02514	21.78815226
0.012318	2.635696	0.01676	20.11214055
0.008762	2.635696	0.01676	18.43612883
0.006251	3.953544	0.02514	15.92211127
0.003134	1.317848	0.00838	15.08410541
0.001316	13.17848	0.083801	6.704046849

Effective Grain Diameters (mm)		Other Useful Parameters	
d10	0.002	Uniformity Coef.	137.31
d17	0.007	n computed	0.26
d20	0.012	g (cm/s <sup>2</sup> )	980.00
d50	0.202	ρ (g/cm <sup>3</sup> )	0.9981
d60	0.279	μ (g/cm s)	0.0098
de (Kruger)	0.020	ρg/μ (1/cm s)	9.9327E+04
de (Kozeny)	0.010	tau (Sauerbrei)	1.053
de (Zunker)	0.010	d <sub>geometric mean</sub>	0.208
de (Zamarin)	0.011	σ <sub>φ</sub>	4.038
lo (Alyameni)	-0.048		
	mm	0	% in sample
	>64	Boulder	0
	16 - 64	coarse gravel	2.314638179
	8 - 16	medium gravel	14.04680148
	2 - 8	fine gravel	9.451157319
	0.5 - 2	coarse sand	11.45848277
	0.25 - 0.5	medium sand	26.42978507
	0.063 - 0.25	fine sand	14.51098293
	0.016 - 0.063	coarse silt	3.352023425
	0.008 - 0.016	medium silt	3.352023425
	0.002 - 0.008	fine silt	8.380058561
	<0.002	clay	



K from Grain Size Analysis Report

Date: 12-Apr-22

Sample Name:

BH205-SS2

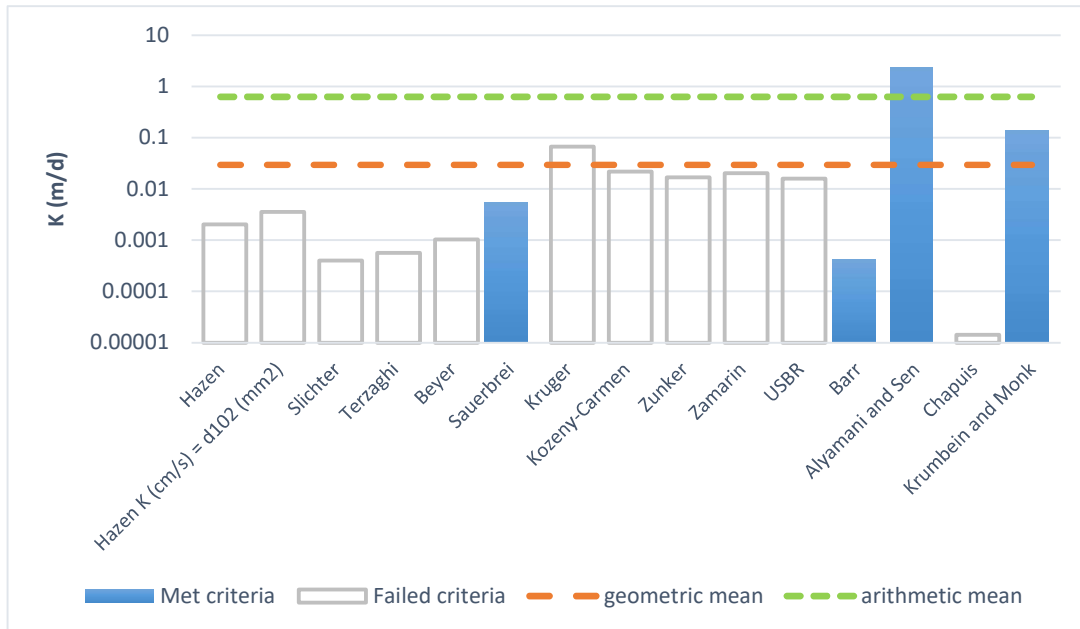
Mass Sample (g):

157.26

T (oC)

20

Poorly sorted gravelly sand with fines



Estimation of Hydraulic Conductivity	cm/s	m/s	m/d	de
Hazen	2.3E-06	2.3E-08	0.00	
Hazen K (cm/s) = d <sub>10</sub> (mm)	4.1E-06	4.1E-08	0.00	
Slichter	4.6E-07	4.6E-09	0.00	
Terzaghi	6.5E-07	6.5E-09	0.00	
Beyer	1.2E-06	1.2E-08	0.00	
Sauerbrei	6.3E-06	6.3E-08	0.01	
Kruger	7.8E-05	7.8E-07	0.07	
Kozeny-Carmen	2.5E-05	2.5E-07	0.02	
Zunker	2.0E-05	2.0E-07	0.02	
Zamarin	2.4E-05	2.4E-07	0.02	
USBR	1.8E-05	1.8E-07	0.02	
Barr	4.9E-07	4.9E-09	0.00	
Alyamani and Sen	2.8E-03	2.8E-05	2.39	
Chapuis	1.6E-08	1.6E-10	0.00	
Krumbein and Monk	1.6E-04	1.6E-06	0.14	
geometric mean	3.4E-05	3.4E-07	0.03	
arithmetic mean	7.3E-04	7.3E-06	0.63	



Grain Size Analysis Report

Date:

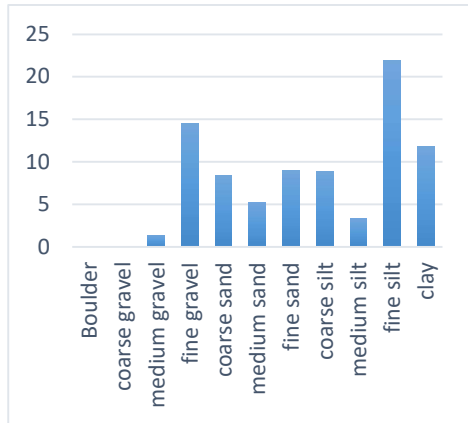
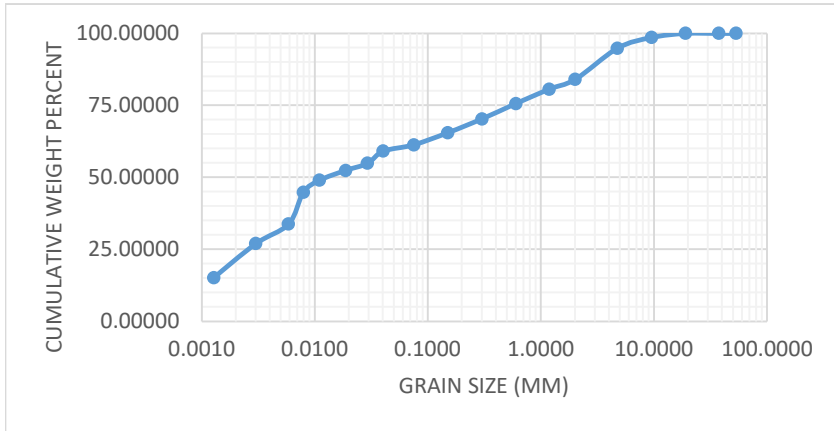
12-Apr-22

Sample Name: BH206-SS4

Mass Sample (g): 225.5

T (oC) 20

Poorly sorted clay with fines



Sieve opening (ps) di (mm)	Mass of retained (mr) (g)	mass fraction (mf)	Percent Passing (pp)
53	0	0	100
37.5	0	0	100
19	0	0	100
9.5	3.18	0.014102	98.58980044
4.75	8.38	0.037162	94.87361419
2	24.51	0.108692	84.00443459
1.18	7.5772	0.033602	80.64425721
0.6	11.3658	0.050403	75.60399113
0.3	11.93409	0.052923	70.31171175
0.15	10.79751	0.047883	65.52345898
0.075	9.4715	0.042002	61.32323725
0.040257	4.891385	0.021691	59.15410866
0.029293	9.528037	0.042253	54.92881518
0.018747	5.716822	0.025352	52.3936391
0.01099	7.622429	0.033802	49.01340432
0.007916	9.528037	0.042253	44.78811084
0.005856	24.7729	0.109858	33.8023478
0.003005	15.24486	0.067605	27.04187824
0.00128	26.6785	0.118308	15.21105651

Effective Grain Diameters (mm)		Other Useful Parameters	
d10	0.001	Uniformity Coef.	63.96
d17	0.002	n computed	0.26
d20	0.002	g (cm/s <sup>2</sup> )	980.00
d50	0.013	ρ (g/cm <sup>3</sup> )	0.9981
d60	0.054	μ (g/cm s)	0.0098
de (Kruger)	0.010	ρg/μ (1/cm s)	9.9327E+04
de (Kozeny)	0.005	tau (Sauerbrei)	1.053
de (Zunker)	0.005	d <sub>geometric mean</sub>	0.103
de (Zamarin)	0.005	σ <sub>φ</sub>	4.668
lo (Alyameni)	-0.002		
	mm	0	% in sample
	>64	Boulder	
	16 - 64	coarse gravel	0
	8 - 16	medium gravel	1.410199557
	2 - 8	fine gravel	14.58536585
	0.5 - 2	coarse sand	8.400443459
	0.25 - 0.5	medium sand	5.292279379
	0.063 - 0.25	fine sand	8.988474501
	0.016 - 0.063	coarse silt	8.929598154
	0.008 - 0.016	medium silt	3.38023478
	0.002 - 0.008	fine silt	21.97152607
	<0.002	clay	11.83082173



K from Grain Size Analysis Report

Date: 12-Apr-22

Sample Name:

BH206-SS4

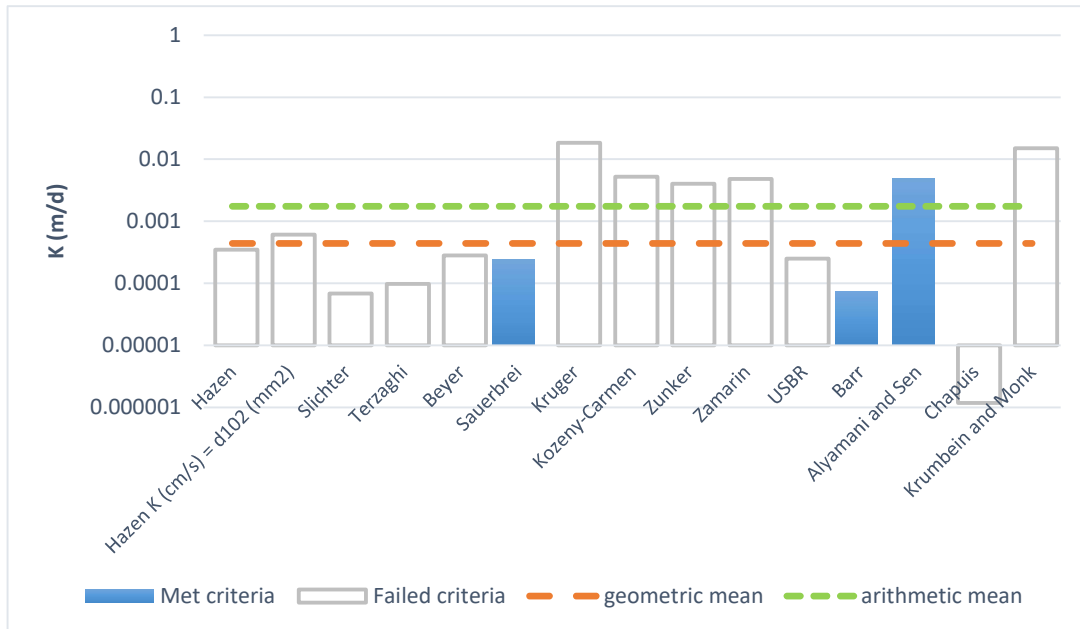
Mass Sample (g):

225.5

T (oC)

20

Poorly sorted clay with fines



Estimation of Hydraulic Conductivity	cm/s	m/s	m/d	de
Hazen	4.0E-07	4.0E-09	0.00	
Hazen K (cm/s) = d <sub>10</sub> (mm)	7.1E-07	7.1E-09	0.00	
Slichter	7.9E-08	7.9E-10	0.00	
Terzaghi	1.1E-07	1.1E-09	0.00	
Beyer	3.3E-07	3.3E-09	0.00	
Sauerbrei	2.8E-07	2.8E-09	0.00	
Kruger	2.1E-05	2.1E-07	0.02	
Kozeny-Carmen	6.1E-06	6.1E-08	0.01	
Zunker	4.7E-06	4.7E-08	0.00	
Zamarin	5.5E-06	5.5E-08	0.00	
USBR	2.9E-07	2.9E-09	0.00	
Barr	8.4E-08	8.4E-10	0.00	
Alyamani and Sen	5.7E-06	5.7E-08	0.00	
Chapuis	1.4E-09	1.4E-11	0.00	
Krumbein and Monk	1.7E-05	1.7E-07	0.01	
geometric mean	5.1E-07	5.1E-09	0.00	
arithmetic mean	2.0E-06	2.0E-08	0.00	





Grain Size Analysis Report

Date:

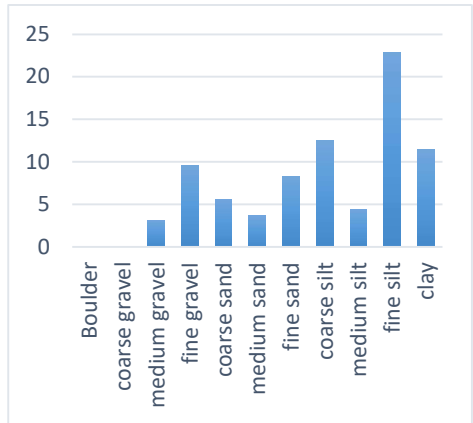
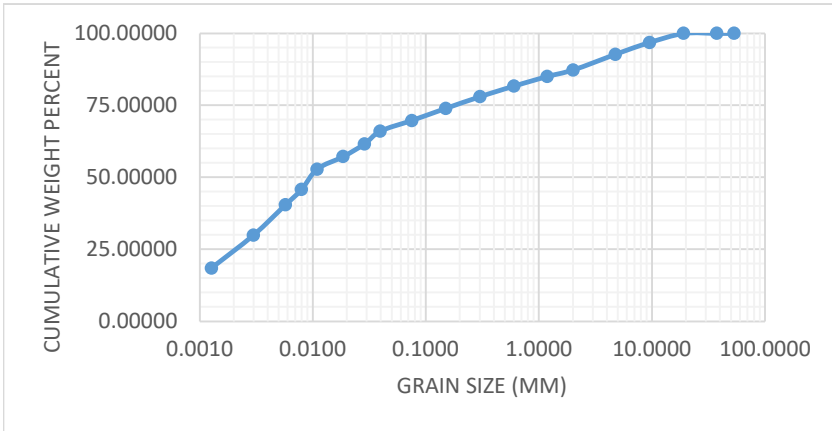
12-Apr-22

Sample Name: BH207-SS4

Mass Sample (g): 172.38

T (oC) 20

Poorly sorted clay with fines



Sieve opening (ps) di (mm)	Mass of retained (mr) (g)	mass fraction (mf)	Percent Passing (pp)
53	0	0	100
37.5	0	0	100
19	0	0	100
9.5	5.47	0.031732	96.82677805
4.75	7.09	0.04113	92.7137719
2	9.34	0.054183	87.29550992
1.18	3.91248	0.022697	85.02582666
0.6	5.71824	0.033172	81.70859729
0.3	6.32016	0.036664	78.04218587
0.15	7.07256	0.041029	73.9392969
0.075	7.22304	0.041902	69.74911243
0.0394	6.394439	0.037095	66.03961096
0.028705	7.589272	0.044026	61.63697023
0.018527	7.589272	0.044026	57.2343295
0.010907	7.589272	0.044026	52.83168877
0.007945	12.14284	0.070442	45.7874636
0.005738	9.107127	0.052832	40.50429472
0.002986	18.21425	0.105663	29.93795697
0.001268	19.73211	0.114469	18.49109107

Effective Grain Diameters (mm)		Other Useful Parameters	
d10	0.001	Uniformity Coef.	36.33
d17	0.001	n computed	0.26
d20	0.001	g (cm/s <sup>2</sup> )	980.00
d50	0.010	ρ (g/cm <sup>3</sup> )	0.9981
d60	0.025	μ (g/cm s)	0.0098
de (Krugler)	0.010	ρg/μ (1/cm s)	9.9327E+04
de (Kozeny)	0.004	tau (Sauerbrei)	1.053
de (Zunker)	0.005	d <sub>geometric mean</sub>	0.085
de (Zamarin)	0.005	σ <sub>φ</sub>	4.639
lo (Alyameni)	-0.002		
	mm	0	% in sample
	>64	Boulder	0
	16 - 64	coarse gravel	0
	8 - 16	medium gravel	3.173221952
	2 - 8	fine gravel	9.531268129
	0.5 - 2	coarse sand	5.586912635
	0.25 - 0.5	medium sand	3.666411417
	0.063 - 0.25	fine sand	8.293073442
	0.016 - 0.063	coarse silt	12.51478293
	0.008 - 0.016	medium silt	4.402640731
	0.002 - 0.008	fine silt	22.8937318
	<0.002	clay	11.4468659



K from Grain Size Analysis Report

Date: 12-Apr-22

Sample Name:

BH207-SS4

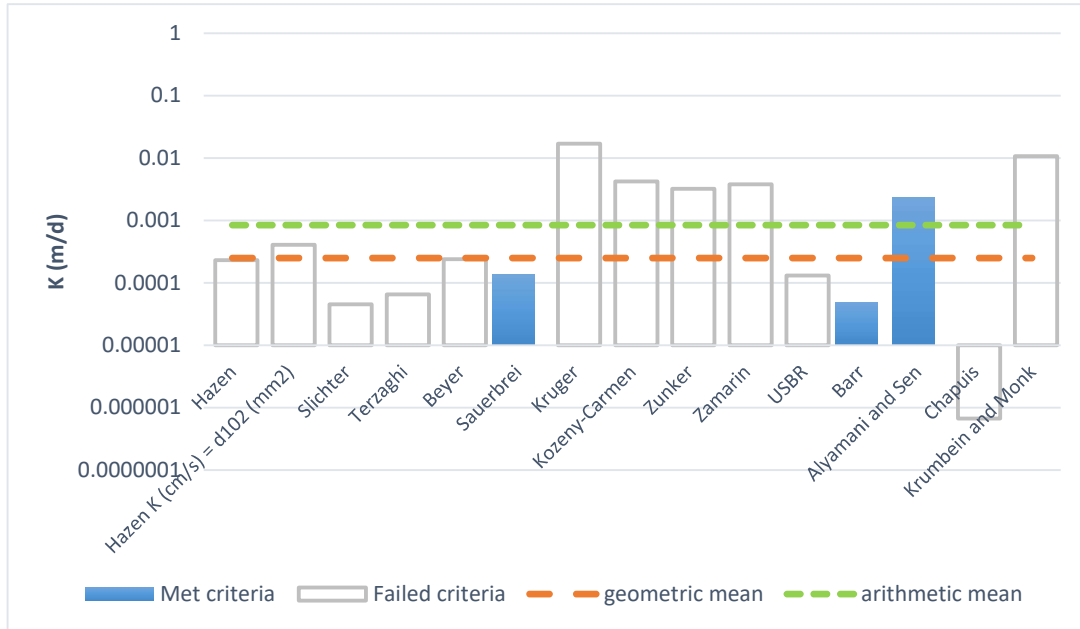
Mass Sample (g):

172.38

T (oC)

20

Poorly sorted clay with fines



Estimation of Hydraulic Conductivity	cm/s	m/s	m/d	de
Hazen	2.7E-07	2.7E-09	0.00	
Hazen K (cm/s) = d <sub>10</sub> (mm)	4.7E-07	4.7E-09	0.00	
Slichter	5.3E-08	5.3E-10	0.00	
Terzaghi	7.5E-08	7.5E-10	0.00	
Beyer	2.8E-07	2.8E-09	0.00	
Sauerbrei	1.6E-07	1.6E-09	0.00	
Kruger	2.0E-05	2.0E-07	0.02	
Kozeny-Carmen	4.9E-06	4.9E-08	0.00	
Zunker	3.7E-06	3.7E-08	0.00	
Zamarin	4.4E-06	4.4E-08	0.00	
USBR	1.5E-07	1.5E-09	0.00	
Barr	5.6E-08	5.6E-10	0.00	
Alyamani and Sen	2.7E-06	2.7E-08	0.00	
Chapuis	7.7E-10	7.7E-12	0.00	
Krumbein and Monk	1.2E-05	1.2E-07	0.01	
geometric mean	2.9E-07	2.9E-09	0.00	
arithmetic mean	9.8E-07	9.8E-09	0.00	

# APPENDIX E





Grounded Engineering Inc  
ATTN: Nicholas Piers  
1 Banigan Drive  
TORONTO ON M4H 1G3

Date Received: 24-MAR-22  
Report Date: 19-APR-22 08:37 (MT)  
Version: FINAL REV. 2

Client Phone: 647-264-7932

## Certificate of Analysis

Lab Work Order #: L2694356  
Project P.O. #: NOT SUBMITTED  
Job Reference: 21-067  
C of C Numbers: 20-954694  
Legal Site Desc: 60 DUNDAS ST. E.

Comments: 14-APR-22 Report revision to compare to City of Mississauga Storm Sewer and Region of Peel Sanitary Sewer per client request. -A.Overholster

Amanda Overholster  
Account Manager

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ADDRESS: 5730 Coopers Avenue, Unit #26, Mississauga, ON L4Z 2E9 Canada | Phone: +1 905 507 6910 | Fax: +1 905 507 6927  
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## Summary of Guideline Exceedances

Guideline		Grouping	Analyte	Result	Guideline Limit	Unit
ALS ID	Client ID					
<b>Ontario Sewer Use Bylaws - Peel Sanitary Sewer (53-2010)</b>						
(No parameter exceedances)						
<b>Ontario Sewer Use Bylaws - Mississauga Storm Sewer (0046-2022)</b>						
L2694356-1	SW-UF-BH205	Physical Tests	Total Suspended Solids	38.2	15	mg/L
		Total Metals	Copper (Cu)-Total	<0.050	0.04	mg/L
			Manganese (Mn)-Total	2.09	2.0	mg/L
			Zinc (Zn)-Total	<0.30	0.2	mg/L

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Physical Tests - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
pH	pH units	5.5-10	6-9	7.63
Total Suspended Solids	mg/L	350	15	38.2

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.

Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Anions and Nutrients - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
Fluoride (F)	mg/L	10	-	<2.0 <sup>DLDS</sup>
Total Kjeldahl Nitrogen	mg/L	100	-	13.3 <sup>DLHC</sup>
Phosphorus, Total	mg/L	10	0.4	0.0165
Sulfate (SO4)	mg/L	1500	-	813 <sup>DLDS</sup>

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

- Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.
- Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Cyanides - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

**Guide Limits**

Analyte	Unit	#1	#2	<0.0020
Cyanide, Total	mg/L	2	0.02	

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.

Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.



## Bacteriological Tests - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	0
E. Coli	CFU/100m L	-	200	0
Fecal Coliforms	CFU/100m L	-	-	0

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

- Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.
- Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Total Metals - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
Aluminum (Al)-Total	mg/L	50	1.0	0.52 <sup>DLHC</sup>
Antimony (Sb)-Total	mg/L	5	-	<0.010 <sup>DLHC</sup>
Arsenic (As)-Total	mg/L	1	0.02	<0.010 <sup>DLHC</sup>
Cadmium (Cd)-Total	mg/L	0.7	0.008	<0.00050 <sup>DLHC</sup>
Chromium (Cr)-Total	mg/L	5	0.08	<0.050 <sup>DLHC</sup>
Cobalt (Co)-Total	mg/L	5	-	<0.010 <sup>DLHC</sup>
Copper (Cu)-Total	mg/L	3	0.04	<0.050 <sup>DLHC</sup>
Lead (Pb)-Total	mg/L	3	0.120	<0.0050 <sup>DLHC</sup>
Manganese (Mn)-Total	mg/L	5	2.0	2.09 <sup>DLHC</sup>
Mercury (Hg)-Total	mg/L	0.01	0.0004	<0.0000050
Molybdenum (Mo)-Total	mg/L	5	-	0.0087 <sup>DLHC</sup>
Nickel (Ni)-Total	mg/L	3	0.08	<0.050 <sup>DLHC</sup>
Selenium (Se)-Total	mg/L	1	0.02	<0.0050 <sup>DLHC</sup>
Silver (Ag)-Total	mg/L	5	0.12	<0.0050 <sup>DLHC</sup>
Tin (Sn)-Total	mg/L	5	-	<0.010 <sup>DLHC</sup>
Titanium (Ti)-Total	mg/L	5	-	<0.030 <sup>DLHC</sup>
Zinc (Zn)-Total	mg/L	3	0.2	<0.30 <sup>DLHC</sup>

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

  Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.

  Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Aggregate Organics - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
BOD Carbonaceous	mg/L	300	-	19.3
Oil and Grease, Total	mg/L	-	-	<5.0
Animal/Veg Oil & Grease	mg/L	150	-	<5.0
Mineral Oil and Grease	mg/L	15	-	<2.5
Phenols (4AAP)	mg/L	1	0.008	<0.0010

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

- Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.
- Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Volatile Organic Compounds - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
Acetone	ug/L	-	-	<20
Benzene	ug/L	10	2	<0.50
Bromodichloromethane	ug/L	-	-	1.3
Bromoform	ug/L	-	-	<1.0
Bromomethane	ug/L	-	-	<0.50
Carbon Disulfide	ug/L	-	-	<1.0
Carbon tetrachloride	ug/L	-	-	<0.20
Chlorobenzene	ug/L	-	-	<0.50
Dibromochloromethane	ug/L	-	-	<1.0
Chloroethane	ug/L	-	-	<1.0
Chloroform	ug/L	40	-	2.4
Chloromethane	ug/L	-	-	<2.0
1,2-Dibromoethane	ug/L	-	-	<0.20
1,2-Dichlorobenzene	ug/L	50	5.6	<0.50
1,3-Dichlorobenzene	ug/L	-	-	<0.50
1,4-Dichlorobenzene	ug/L	80	6.8	<0.50
Dichlorodifluoromethane	ug/L	-	-	<1.0
1,1-Dichloroethane	ug/L	-	-	<0.50
1,2-Dichloroethane	ug/L	-	-	<0.50
1,1-Dichloroethylene	ug/L	-	-	<0.50
cis-1,2-Dichloroethylene	ug/L	4000	-	<0.50
trans-1,2-Dichloroethylene	ug/L	-	-	<0.50
Dichloromethane	ug/L	2000	5.2	<2.0
1,2-Dichloropropane	ug/L	-	-	<0.50
cis-1,3-Dichloropropene	ug/L	-	-	<0.30
trans-1,3-Dichloropropene	ug/L	140	-	<0.30
Ethylbenzene	ug/L	160	2	<0.50
n-Hexane	ug/L	-	-	<0.50
2-Hexanone	ug/L	-	-	<20
Methyl Ethyl Ketone	ug/L	8000	-	<20

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**  
**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Volatile Organic Compounds - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
Methyl Isobutyl Ketone	ug/L	-	-	<20
MTBE	ug/L	-	-	<0.50
Styrene	ug/L	200	-	<0.50
1,1,1,2-Tetrachloroethane	ug/L	-	-	<0.50
1,1,2,2-Tetrachloroethane	ug/L	1400	-	<0.50
Tetrachloroethylene	ug/L	1000	4.4	<0.50
Toluene	ug/L	270	2	0.40
1,1,1-Trichloroethane	ug/L	-	-	<0.50
1,1,2-Trichloroethane	ug/L	-	-	<0.50
Trichloroethylene	ug/L	400	7.6	<0.50
Trichlorofluoromethane	ug/L	-	-	<1.0
Vinyl chloride	ug/L	-	-	<0.50
o-Xylene	ug/L	-	-	<0.30
m+p-Xylenes	ug/L	-	-	<0.40
Xylenes (Total)	ug/L	1400	4.4	<0.50
Surrogate: 4-Bromofluorobenzene	%	-	-	89.5
Surrogate: 1,4-Difluorobenzene	%	-	-	97.5

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.

Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Phthalate Esters - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
Bis(2-ethylhexyl)phthalate	ug/L	12	-	<2.0
Surrogate: 2-fluorobiphenyl	%	-	-	88.9
Surrogate: p-Terphenyl d14	%	-	-	83.4

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.

Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Semi-Volatile Organics - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
Di-n-butylphthalate	ug/L	80	-	<1.0
Surrogate: 2-Fluorobiphenyl	%	-	-	88.9
Surrogate: p-Terphenyl d14	%	-	-	83.4

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.

Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

## Polychlorinated Biphenyls - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits		
		#1	#2	
Aroclor 1242	ug/L	-	-	<0.020
Aroclor 1248	ug/L	-	-	<0.020
Aroclor 1254	ug/L	-	-	<0.020
Aroclor 1260	ug/L	-	-	<0.020
Surrogate: Decachlorobiphenyl	%	-	-	107.5
Total PCBs	ug/L	1	0.4	<0.040
Surrogate: Tetrachloro-m-xylene	%	-	-	91.8

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

- Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.
- Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.



## Organic Parameters - WATER

**Lab ID** L2694356-1  
**Sample Date** 23-MAR-22  
**Sample ID** SW-UF-BH205

Analyte	Unit	Guide Limits	
		#1	#2
Nonylphenol	ug/L	20	- 3.8
Nonylphenol Diethoxylates	ug/L	-	- <0.10
Total Nonylphenol Ethoxylates	ug/L	200	- <2.0
Nonylphenol Monoethoxylates	ug/L	-	- <2.0

**Guide Limit #1: Peel Sanitary Sewer (53-2010)**

**Guide Limit #2: Mississauga Storm Sewer (0046-2022)**

- Detection Limit for result exceeds Guideline Limit. Assessment against Guideline Limit cannot be made.
- Analytical result for this parameter exceeds Guide Limits listed. See Summary of Guideline Exceedances.

\* Please refer to the Reference Information section for an explanation of any qualifiers noted.

# Reference Information

## Qualifiers for Individual Parameters Listed:

Qualifier	Description
DLDS	Detection Limit Raised: Dilution required due to high Dissolved Solids / Electrical Conductivity.
DLHC	Detection Limit Raised: Dilution required due to high concentration of test analyte(s).

## Methods Listed (if applicable):

ALS Test Code	Matrix	Test Description	Method Reference**
<b>625-BIS-2-PHTH-WT</b>	Water	Bis(2-ethylhexyl)phthalate	SW846 8270
Aqueous samples are extracted and extracts are analyzed on GC/MSD.			
<b>625-DNB-PHTH-WT</b>	Water	Di-n-Butyl Phthalate	SW846 8270
Aqueous samples are extracted and extracts are analyzed on GC/MSD.			
<b>BOD-C-WT</b>	Water	BOD Carbonaceous	APHA 5210 B (CBOD)
This analysis is carried out using procedures adapted from APHA Method 5210B - "Biochemical Oxygen Demand (BOD)". All forms of biochemical oxygen demand (BOD) are determined by diluting and incubating a sample for a specified time period, and measuring the oxygen depletion using a dissolved oxygen meter. Dissolved BOD (SOLUBLE) is determined by filtering the sample through a glass fibre filter prior to dilution. Carbonaceous BOD (CBOD) is determined by adding a nitrification inhibitor to the diluted sample prior to incubation.			
<b>CN-TOT-WT</b>	Water	Cyanide, Total	ISO 14403-2
Total cyanide is determined by the combination of UV digestion and distillation. Cyanide is converted to cyanogen chloride by reacting with chloramine-T, the cyanogen chloride then reacts with a combination of barbituric acid and isonicotinic acid to form a highly colored complex.			
When using this method, high levels of thiocyanate in samples can cause false positives at ~1-2% of the thiocyanate concentration. For samples with detectable cyanide analyzed by this method, ALS recommends analysis for thiocyanate to check for this potential interference			
<b>EC-SCREEN-WT</b>	Water	Conductivity Screen (Internal Use Only)	APHA 2510
Qualitative analysis of conductivity where required during preparation of other tests - e.g. TDS, metals, etc.			
<b>EC-WW-MF-WT</b>	Water	E. Coli	SM 9222D
A 100 mL volume of sample is filtered through a membrane, the membrane is placed on mFC-BCIG agar and incubated at 44.5 – 0.2 °C for 24 – 2 h. Method ID: WT-TM-1200			
<b>F-IC-N-WT</b>	Water	Fluoride in Water by IC	EPA 300.1 (mod)
Inorganic anions are analyzed by Ion Chromatography with conductivity and/or UV detection.			
<b>FC-WW-MF-WT</b>	Water	Fecal Coliforms	APHA 9223B
<b>FC-WW-MF-WT</b>	Water	Fecal Coliforms	SM 9222D
<b>HG-T-CVAA-WT</b>	Water	Total Mercury in Water by CVAAS	EPA 1631E (mod)
Water samples undergo a cold-oxidation using bromine monochloride prior to reduction with stannous chloride, and analyzed by CVAAS.			
<b>MET-T-CCMS-WT</b>	Water	Total Metals in Water by CRC ICPMS	EPA 200.2/6020A (mod)

Water samples are digested with nitric and hydrochloric acids, and analyzed by CRC ICPMS.

Method Limitation (re: Sulfur): Sulfide and volatile sulfur species may not be recovered by this method.

# Reference Information

**Methods Listed (if applicable):**

ALS Test Code	Matrix	Test Description	Method Reference**
<p>Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011).</p>			
<b>NP,NPE-LCMS-WT</b>	Water	Nonylphenols and Ethoxylates by LC/MS-MS	J. Chrom A849 (1999) p.467-482
<p>Water samples are filtered and analyzed on LCMS/MS by direct injection.</p>			
<b>OGG-SPEC-CALC-WT</b>	Water	Speciated Oil and Grease A/V Calc	CALCULATION
<p>Sample is extracted with hexane, sample speciation into mineral and animal/vegetable fractions is achieved via silica gel separation and is then determined gravimetrically.</p>			
<b>OGG-SPEC-WT</b>	Water	Speciated Oil and Grease-Gravimetric	APHA 5520 B
<p>The procedure involves an extraction of the entire water sample with hexane. Sample speciation into mineral and animal/vegetable fractions is achieved via silica gel separation and is then determined gravimetrically.</p>			
<b>P-T-COL-WT</b>	Water	Total P in Water by Colour	APHA 4500-P PHOSPHORUS
<p>This analysis is carried out using procedures adapted from APHA Method 4500-P "Phosphorus". Total Phosphorus is determined colourimetrically after persulphate digestion of the sample.</p>			
<b>PCB-WT</b>	Water	Polychlorinated Biphenyls	EPA 8082
<p>PCBs are extracted from an aqueous sample at neutral pH with aliquots of dichloromethane using a modified separatory funnel technique. The extracts are analyzed by GC/MSD.</p>			
<b>PH-WT</b>	Water	pH	APHA 4500 H-Electrode
<p>Water samples are analyzed directly by a calibrated pH meter.</p>			
<p>Analysis conducted in accordance with the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act (July 1, 2011). Holdtime for samples under this regulation is 28 days</p>			
<b>PHENOLS-4AAP-WT</b>	Water	Phenol (4AAP)	EPA 9066
<p>An automated method is used to distill the sample. The distillate is then buffered to pH 9.4 which reacts with 4AAP and potassium ferricyanide to form a red complex which is measured colorimetrically.</p>			
<b>SO4-IC-N-WT</b>	Water	Sulfate in Water by IC	EPA 300.1 (mod)
<p>Inorganic anions are analyzed by Ion Chromatography with conductivity and/or UV detection.</p>			
<b>SOLIDS-TSS-WT</b>	Water	Suspended solids	APHA 2540 D-Gravimetric
<p>A well-mixed sample is filtered through a weighed standard glass fibre filter and the residue retained is dried in an oven at 104–1°C for a minimum of four hours or until a constant weight is achieved.</p>			
<b>TKN-F-WT</b>	Water	TKN in Water by Fluorescence	J. ENVIRON. MONIT., 2005,7,37-42,RSC
<p>Total Kjeldahl Nitrogen is determined using block digestion followed by Flow-injection analysis with fluorescence detection</p>			
<b>VOC-ROU-HS-WT</b>	Water	Volatile Organic Compounds	SW846 8260
<p>Aqueous samples are analyzed by headspace-GC/MS.</p>			

# Reference Information

## Methods Listed (if applicable):

ALS Test Code	Matrix	Test Description	Method Reference**
<b>XYLENES-SUM-CALC-WT</b>	Water	Sum of Xylene Isomer Concentrations	CALCULATION

Total xylenes represents the sum of o-xylene and m&p-xylene.

\*\*ALS test methods may incorporate modifications from specified reference methods to improve performance.

## Chain of Custody Numbers:

20-954694

The last two letters of the above test code(s) indicate the laboratory that performed analytical analysis for that test. Refer to the list below:

Laboratory Definition Code	Laboratory Location
WT	ALS ENVIRONMENTAL - WATERLOO, ONTARIO, CANADA

## GLOSSARY OF REPORT TERMS

Surrogates are compounds that are similar in behaviour to target analyte(s), but that do not normally occur in environmental samples. For applicable tests, surrogates are added to samples prior to analysis as a check on recovery. In reports that display the D.L. column, laboratory objectives for surrogates are listed there.

mg/kg - milligrams per kilogram based on dry weight of sample

mg/kg wwt - milligrams per kilogram based on wet weight of sample

mg/kg lwt - milligrams per kilogram based on lipid-adjusted weight

mg/L - unit of concentration based on volume, parts per million.

< - Less than.

D.L. - The reporting limit.

N/A - Result not available. Refer to qualifier code and definition for explanation.

Test results reported relate only to the samples as received by the laboratory.

UNLESS OTHERWISE STATED, ALL SAMPLES WERE RECEIVED IN ACCEPTABLE CONDITION.

Analytical results in unsigned test reports with the DRAFT watermark are subject to change, pending final QC review.

Application of guidelines is provided "as is" without warranty of any kind, either expressed or implied, including, but not limited to, fitness for a particular purpose, or non-infringement. ALS assumes no responsibility for errors or omissions in the information. Guideline limits are not adjusted for the hardness, pH or temperature of the sample (the most conservative values are used). Measurement uncertainty is not applied to test results prior to comparison with specified criteria values.



## Quality Control Report

Workorder: L2694356

Report Date: 19-APR-22

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Client: Grounded Engineering Inc  
 1 Banigan Drive  
 TORONTO ON M4H 1G3

Contact: Nicholas Piers

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>625-BIS-2-PHTH-WT</b> <b>Water</b>								
Batch      R5750578								
<b>WG3709937-2</b> <b>LCS</b>								
	Bis(2-ethylhexyl)phthalate		108.0		%		50-140	26-MAR-22
<b>WG3709937-1</b> <b>MB</b>								
	Bis(2-ethylhexyl)phthalate		<2.0		ug/L		2	26-MAR-22
	Surrogate: 2-fluorobiphenyl		78.0		%		40-130	26-MAR-22
	Surrogate: p-Terphenyl d14		94.2		%		40-130	26-MAR-22
<b>625-DNB-PHTH-WT</b> <b>Water</b>								
Batch      R5750578								
<b>WG3709937-2</b> <b>LCS</b>								
	Di-n-butylphthalate		95.0		%		50-150	26-MAR-22
<b>WG3709937-1</b> <b>MB</b>								
	Di-n-butylphthalate		<1.0		ug/L		1	26-MAR-22
	Surrogate: 2-Fluorobiphenyl		78.0		%		40-130	26-MAR-22
	Surrogate: p-Terphenyl d14		94.2		%		40-130	26-MAR-22
<b>BOD-C-WT</b> <b>Water</b>								
Batch      R5751353								
<b>WG3709807-2</b> <b>DUP</b>								
	BOD Carbonaceous	<b>L2694213-1</b>	<3.0	RPD-NA	mg/L	N/A	30	24-MAR-22
<b>WG3709807-3</b> <b>LCS</b>								
	BOD Carbonaceous		92.4		%		85-115	24-MAR-22
<b>WG3709807-1</b> <b>MB</b>								
	BOD Carbonaceous		<2.0		mg/L		2	24-MAR-22
<b>CN-TOT-WT</b> <b>Water</b>								
Batch      R5750806								
<b>WG3710141-3</b> <b>DUP</b>								
	Cyanide, Total	<b>WG3710141-5</b>	0.0100		mg/L	2.4	20	25-MAR-22
<b>WG3710141-2</b> <b>LCS</b>								
	Cyanide, Total		105.5		%		80-120	25-MAR-22
<b>WG3710141-1</b> <b>MB</b>								
	Cyanide, Total		<0.0020		mg/L		0.002	25-MAR-22
<b>WG3710141-4</b> <b>MS</b>								
	Cyanide, Total	<b>WG3710141-5</b>	102.7		%		70-130	25-MAR-22
<b>EC-WW-MF-WT</b> <b>Water</b>								
Batch      R5750580								
<b>WG3709707-1</b> <b>MB</b>								
	E. Coli		0		CFU/100mL		1	24-MAR-22



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Client: Grounded Engineering Inc  
 1 Banigan Drive  
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Contact: Nicholas Piers

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>F-IC-N-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5750845</b>							
<b>WG3710310-19</b>	<b>DUP</b>	<b>WG3710310-18</b>						
Fluoride (F)		0.053	0.052		mg/L	2.8	20	25-MAR-22
<b>WG3710310-17</b>	<b>LCS</b>							
Fluoride (F)			102.7		%		90-110	25-MAR-22
<b>WG3710310-16</b>	<b>MB</b>							
Fluoride (F)			<0.020		mg/L		0.02	25-MAR-22
<b>WG3710310-20</b>	<b>MS</b>	<b>WG3710310-18</b>						
Fluoride (F)			97.8		%		75-125	25-MAR-22
<b>FC-WW-MF-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5750576</b>							
<b>WG3709714-1</b>	<b>MB</b>							
Fecal Coliforms			0		CFU/100mL		1	24-MAR-22
<b>HG-T-CVAA-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5750289</b>							
<b>WG3709889-7</b>	<b>DUP</b>	<b>WG3709889-9</b>						
Mercury (Hg)-Total		<0.0000050	<0.0000050	RPD-NA	mg/L	N/A	20	25-MAR-22
<b>WG3709889-6</b>	<b>LCS</b>							
Mercury (Hg)-Total			89.4		%		80-120	25-MAR-22
<b>WG3709889-5</b>	<b>MB</b>							
Mercury (Hg)-Total			<0.0000050		mg/L		0.000005	25-MAR-22
<b>WG3709889-8</b>	<b>MS</b>	<b>WG3709889-10</b>						
Mercury (Hg)-Total			87.0		%		70-130	25-MAR-22
<b>MET-T-CCMS-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5749909</b>							
<b>WG3709877-4</b>	<b>DUP</b>	<b>WG3709877-3</b>						
Aluminum (Al)-Total		<0.0050	<0.0050	RPD-NA	mg/L	N/A	20	24-MAR-22
Antimony (Sb)-Total		<0.00010	<0.00010	RPD-NA	mg/L	N/A	20	24-MAR-22
Arsenic (As)-Total		0.00016	0.00016		mg/L	2.6	20	24-MAR-22
Cadmium (Cd)-Total		<0.0000050	<0.0000050	RPD-NA	mg/L	N/A	20	24-MAR-22
Chromium (Cr)-Total		0.00064	0.00057		mg/L	11	20	24-MAR-22
Cobalt (Co)-Total		<0.00010	<0.00010	RPD-NA	mg/L	N/A	20	24-MAR-22
Copper (Cu)-Total		<0.00050	<0.00050	RPD-NA	mg/L	N/A	20	24-MAR-22
Lead (Pb)-Total		0.000099	0.000100		mg/L	1.2	20	24-MAR-22
Manganese (Mn)-Total		0.0121	0.0123		mg/L	1.6	20	24-MAR-22
Molybdenum (Mo)-Total		0.000697	0.000692		mg/L	0.8	20	24-MAR-22



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Contact: Nicholas Piers

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>MET-T-CCMS-WT</b>								
	<b>Water</b>							
<b>Batch</b>	<b>R5749909</b>							
<b>WG3709877-4</b>	<b>DUP</b>	<b>WG3709877-3</b>						
Nickel (Ni)-Total		<0.00050	<0.00050	RPD-NA	mg/L	N/A	20	24-MAR-22
Selenium (Se)-Total		<0.000050	<0.000050	RPD-NA	mg/L	N/A	20	24-MAR-22
Silver (Ag)-Total		<0.000050	<0.000050	RPD-NA	mg/L	N/A	20	24-MAR-22
Tin (Sn)-Total		<0.00010	<0.00010	RPD-NA	mg/L	N/A	20	24-MAR-22
Titanium (Ti)-Total		<0.00030	<0.00030	RPD-NA	mg/L	N/A	20	24-MAR-22
Zinc (Zn)-Total		0.0639	0.0641		mg/L	0.4	20	24-MAR-22
<b>WG3709877-2</b>	<b>LCS</b>							
Aluminum (Al)-Total			105.8		%		80-120	24-MAR-22
Antimony (Sb)-Total			99.6		%		80-120	24-MAR-22
Arsenic (As)-Total			105.1		%		80-120	24-MAR-22
Cadmium (Cd)-Total			101.1		%		80-120	24-MAR-22
Chromium (Cr)-Total			101.7		%		80-120	24-MAR-22
Cobalt (Co)-Total			99.3		%		80-120	24-MAR-22
Copper (Cu)-Total			102.0		%		80-120	24-MAR-22
Lead (Pb)-Total			97.6		%		80-120	24-MAR-22
Manganese (Mn)-Total			101.5		%		80-120	24-MAR-22
Molybdenum (Mo)-Total			95.9		%		80-120	24-MAR-22
Nickel (Ni)-Total			101.9		%		80-120	24-MAR-22
Selenium (Se)-Total			103.5		%		80-120	24-MAR-22
Silver (Ag)-Total			91.2		%		80-120	24-MAR-22
Tin (Sn)-Total			98.7		%		80-120	24-MAR-22
Titanium (Ti)-Total			101.9		%		80-120	24-MAR-22
Zinc (Zn)-Total			105.0		%		80-120	24-MAR-22
<b>WG3709877-1</b>	<b>MB</b>							
Aluminum (Al)-Total			<0.0050		mg/L		0.005	24-MAR-22
Antimony (Sb)-Total			<0.00010		mg/L		0.0001	24-MAR-22
Arsenic (As)-Total			<0.00010		mg/L		0.0001	24-MAR-22
Cadmium (Cd)-Total			<0.0000050		mg/L		0.000005	24-MAR-22
Chromium (Cr)-Total			<0.00050		mg/L		0.0005	25-MAR-22
Cobalt (Co)-Total			<0.00010		mg/L		0.0001	24-MAR-22
Copper (Cu)-Total			<0.00050		mg/L		0.0005	24-MAR-22
Lead (Pb)-Total			<0.000050		mg/L		0.00005	24-MAR-22
Manganese (Mn)-Total			<0.00050		mg/L		0.0005	24-MAR-22
Molybdenum (Mo)-Total			<0.000050		mg/L		0.00005	24-MAR-22



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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>MET-T-CCMS-WT</b>								
	Water							
<b>Batch</b>	<b>R5749909</b>							
<b>WG3709877-1</b>	<b>MB</b>							
Nickel (Ni)-Total			<0.00050		mg/L		0.0005	24-MAR-22
Selenium (Se)-Total			<0.000050		mg/L		0.00005	24-MAR-22
Silver (Ag)-Total			<0.000050		mg/L		0.00005	24-MAR-22
Tin (Sn)-Total			<0.00010		mg/L		0.0001	24-MAR-22
Titanium (Ti)-Total			<0.00030		mg/L		0.0003	24-MAR-22
Zinc (Zn)-Total			<0.0030		mg/L		0.003	24-MAR-22
<b>WG3709877-5</b>	<b>MS</b>	<b>WG3709877-6</b>						
Aluminum (Al)-Total			96.8		%		70-130	24-MAR-22
Antimony (Sb)-Total			93.8		%		70-130	24-MAR-22
Arsenic (As)-Total			99.2		%		70-130	24-MAR-22
Cadmium (Cd)-Total			95.6		%		70-130	24-MAR-22
Chromium (Cr)-Total			95.0		%		70-130	24-MAR-22
Cobalt (Co)-Total			91.9		%		70-130	24-MAR-22
Copper (Cu)-Total			85.8		%		70-130	24-MAR-22
Lead (Pb)-Total			88.9		%		70-130	24-MAR-22
Manganese (Mn)-Total			N/A	MS-B	%		-	24-MAR-22
Molybdenum (Mo)-Total			90.1		%		70-130	24-MAR-22
Nickel (Ni)-Total			72.0		%		70-130	24-MAR-22
Selenium (Se)-Total			98.9		%		70-130	24-MAR-22
Silver (Ag)-Total			70.3		%		70-130	24-MAR-22
Tin (Sn)-Total			91.5		%		70-130	24-MAR-22
Titanium (Ti)-Total			96.6		%		70-130	24-MAR-22
Zinc (Zn)-Total			89.9		%		70-130	24-MAR-22
<b>NP,NPE-LCMS-WT</b>								
	Water							
<b>Batch</b>	<b>R5750387</b>							
<b>WG3709872-3</b>	<b>DUP</b>	<b>L2694288-1</b>						
Nonylphenol			<1.0		ug/L	N/A	30	24-MAR-22
Nonylphenol Monoethoxylates			<2.0		ug/L	N/A	30	24-MAR-22
Nonylphenol Diethoxylates			0.36		ug/L	19	30	24-MAR-22
<b>WG3709872-2</b>	<b>LCS</b>							
Nonylphenol			98.4		%		75-125	24-MAR-22
Nonylphenol Monoethoxylates			93.9		%		75-125	24-MAR-22
Nonylphenol Diethoxylates			99.1		%		75-125	24-MAR-22
<b>WG3709872-1</b>	<b>MB</b>							







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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>PCB-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5750900</b>							
<b>WG3709840-1</b>	<b>MB</b>							
Aroclor 1248			<0.020		ug/L		0.02	28-MAR-22
Aroclor 1254			<0.020		ug/L		0.02	28-MAR-22
Aroclor 1260			<0.020		ug/L		0.02	28-MAR-22
Surrogate: Decachlorobiphenyl			113.2		%		50-150	28-MAR-22
Surrogate: Tetrachloro-m-xylene			82.8		%		50-150	28-MAR-22
<b>PH-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5750564</b>							
<b>WG3710133-4</b>	<b>DUP</b>	<b>WG3710133-3</b>						
pH		8.15	8.01	J	pH units	0.14	0.2	25-MAR-22
<b>WG3710133-2</b>	<b>LCS</b>		6.99		pH units		6.9-7.1	25-MAR-22
<b>PHENOLS-4AAP-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5750872</b>							
<b>WG3710102-3</b>	<b>DUP</b>	<b>L2694356-1</b>						
Phenols (4AAP)		<0.0010	<0.0010	RPD-NA	mg/L	N/A	20	25-MAR-22
<b>WG3710102-2</b>	<b>LCS</b>		95.3		%		85-115	25-MAR-22
Phenols (4AAP)								
<b>WG3710102-1</b>	<b>MB</b>		<0.0010		mg/L		0.001	25-MAR-22
Phenols (4AAP)								
<b>WG3710102-4</b>	<b>MS</b>	<b>L2694356-1</b>						
Phenols (4AAP)			106.1		%		75-125	25-MAR-22
<b>SO4-IC-N-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5750845</b>							
<b>WG3710310-19</b>	<b>DUP</b>	<b>WG3710310-18</b>						
Sulfate (SO4)		8.28	8.28		mg/L	0.0	20	25-MAR-22
<b>WG3710310-17</b>	<b>LCS</b>		104.0		%		90-110	25-MAR-22
Sulfate (SO4)								
<b>WG3710310-16</b>	<b>MB</b>		<0.30		mg/L		0.3	25-MAR-22
Sulfate (SO4)								
<b>WG3710310-20</b>	<b>MS</b>	<b>WG3710310-18</b>						
Sulfate (SO4)			103.3		%		75-125	25-MAR-22
<b>SOLIDS-TSS-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5751303</b>							
<b>WG3710756-3</b>	<b>DUP</b>	<b>L2694778-1</b>						
Total Suspended Solids		680	660		mg/L	3.0	20	29-MAR-22
<b>WG3710756-2</b>	<b>LCS</b>							



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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>SOLIDS-TSS-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5751303</b>							
<b>WG3710756-2</b>	<b>LCS</b>							
Total Suspended Solids			87.7		%		85-115	29-MAR-22
<b>WG3710756-1</b>	<b>MB</b>							
Total Suspended Solids			<3.0		mg/L		3	29-MAR-22
<b>TKN-F-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5751694</b>							
<b>WG3711026-3</b>	<b>DUP</b>	<b>L2695017-1</b>						
Total Kjeldahl Nitrogen		51.4	49.3		mg/L	4.1	20	30-MAR-22
<b>WG3711026-2</b>	<b>LCS</b>							
Total Kjeldahl Nitrogen			114.9		%		75-125	29-MAR-22
<b>WG3711026-1</b>	<b>MB</b>							
Total Kjeldahl Nitrogen			<0.050		mg/L		0.05	29-MAR-22
<b>WG3711026-4</b>	<b>MS</b>	<b>L2695017-1</b>						
Total Kjeldahl Nitrogen			N/A	MS-B	%		-	30-MAR-22
<b>VOC-ROU-HS-WT</b>		<b>Water</b>						
<b>Batch</b>	<b>R5751540</b>							
<b>WG3711016-4</b>	<b>DUP</b>	<b>WG3711016-3</b>						
1,1,1,2-Tetrachloroethane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,1,2,2-Tetrachloroethane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,1,1-Trichloroethane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,1,2-Trichloroethane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,2-Dibromoethane		<0.20	<0.20	RPD-NA	ug/L	N/A	30	30-MAR-22
1,1-Dichloroethane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,1-Dichloroethylene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,2-Dichlorobenzene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,2-Dichloroethane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,2-Dichloropropane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,3-Dichlorobenzene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
1,4-Dichlorobenzene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
2-Hexanone		<20	<20	RPD-NA	ug/L	N/A	30	30-MAR-22
Acetone		<20	<20	RPD-NA	ug/L	N/A	30	30-MAR-22
Benzene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
Bromodichloromethane		<1.0	<1.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Bromoform		<1.0	<1.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Bromomethane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22



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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>VOC-ROU-HS-WT</b>								
	<b>Water</b>							
<b>Batch</b>	<b>R5751540</b>							
<b>WG3711016-4</b>	<b>DUP</b>	<b>WG3711016-3</b>						
Carbon Disulfide		<1.0	<1.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Carbon tetrachloride		<0.50	<0.20	RPD-NA	ug/L	N/A	30	30-MAR-22
Chlorobenzene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
Chloroethane		<1.0	<1.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Chloroform		1.1	<1.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Chloromethane		<2.0	<2.0	RPD-NA	ug/L	N/A	30	30-MAR-22
cis-1,2-Dichloroethylene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
cis-1,3-Dichloropropene		<0.30	<0.30	RPD-NA	ug/L	N/A	30	30-MAR-22
Dibromochloromethane		<1.0	<1.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Dichlorodifluoromethane		<1.0	<1.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Dichloromethane		<2.0	<2.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Ethylbenzene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
m+p-Xylenes		<0.40	<0.40	RPD-NA	ug/L	N/A	30	30-MAR-22
Methyl Ethyl Ketone		<20	<20	RPD-NA	ug/L	N/A	30	30-MAR-22
Methyl Isobutyl Ketone		<20	<20	RPD-NA	ug/L	N/A	30	30-MAR-22
n-Hexane		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
MTBE		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
o-Xylene		<0.30	<0.30	RPD-NA	ug/L	N/A	30	30-MAR-22
Styrene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
Tetrachloroethylene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
trans-1,2-Dichloroethylene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
trans-1,3-Dichloropropene		<0.30	<0.30	RPD-NA	ug/L	N/A	30	30-MAR-22
Trichloroethylene		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
Trichlorofluoromethane		<1.0	<1.0	RPD-NA	ug/L	N/A	30	30-MAR-22
Vinyl chloride		<0.50	<0.50	RPD-NA	ug/L	N/A	30	30-MAR-22
<b>WG3711016-1</b>	<b>LCS</b>							
1,1,1,2-Tetrachloroethane			97.0		%		70-130	30-MAR-22
1,1,1,2,2-Tetrachloroethane			94.0		%		70-130	30-MAR-22
1,1,1-Trichloroethane			106.1		%		70-130	30-MAR-22
1,1,2-Trichloroethane			102.9		%		70-130	30-MAR-22
1,2-Dibromoethane			99.8		%		70-130	30-MAR-22
1,1-Dichloroethane			100.1		%		70-130	30-MAR-22
1,1-Dichloroethylene			103.4		%		70-130	30-MAR-22



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Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>VOC-ROU-HS-WT</b>								
	<b>Water</b>							
<b>Batch</b>	<b>R5751540</b>							
<b>WG3711016-1</b>	<b>LCS</b>							
1,2-Dichlorobenzene			109.1		%		70-130	30-MAR-22
1,2-Dichloroethane			104.5		%		70-130	30-MAR-22
1,2-Dichloropropane			108.3		%		70-130	30-MAR-22
1,3-Dichlorobenzene			109.9		%		70-130	30-MAR-22
1,4-Dichlorobenzene			109.7		%		70-130	30-MAR-22
2-Hexanone			102.1		%		60-140	30-MAR-22
Acetone			107.0		%		60-140	30-MAR-22
Benzene			100.9		%		70-130	30-MAR-22
Bromodichloromethane			110.2		%		70-130	30-MAR-22
Bromoform			102.4		%		70-130	30-MAR-22
Bromomethane			97.0		%		60-140	30-MAR-22
Carbon Disulfide			93.2		%		70-130	30-MAR-22
Carbon tetrachloride			103.9		%		70-130	30-MAR-22
Chlorobenzene			99.2		%		70-130	30-MAR-22
Chloroethane			111.4		%		70-130	30-MAR-22
Chloroform			107.2		%		70-130	30-MAR-22
Chloromethane			101.0		%		60-140	30-MAR-22
cis-1,2-Dichloroethylene			107.8		%		70-130	30-MAR-22
cis-1,3-Dichloropropene			100.6		%		70-130	30-MAR-22
Dibromochloromethane			98.2		%		70-130	30-MAR-22
Dichlorodifluoromethane			93.5		%		50-140	30-MAR-22
Dichloromethane			102.6		%		70-130	30-MAR-22
Ethylbenzene			103.5		%		70-130	30-MAR-22
m+p-Xylenes			105.9		%		70-130	30-MAR-22
Methyl Ethyl Ketone			98.9		%		60-140	30-MAR-22
Methyl Isobutyl Ketone			103.9		%		50-150	30-MAR-22
n-Hexane			97.6		%		70-130	30-MAR-22
MTBE			108.3		%		70-130	30-MAR-22
o-Xylene			102.5		%		70-130	30-MAR-22
Styrene			94.7		%		70-130	30-MAR-22
Tetrachloroethylene			97.9		%		70-130	30-MAR-22
trans-1,2-Dichloroethylene			105.1		%		70-130	30-MAR-22
trans-1,3-Dichloropropene			98.1		%		70-130	30-MAR-22



## Quality Control Report

Workorder: L2694356

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Client: Grounded Engineering Inc  
 1 Banigan Drive  
 TORONTO ON M4H 1G3

Contact: Nicholas Piers

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>VOC-ROU-HS-WT</b>								
	<b>Water</b>							
<b>Batch</b>	<b>R5751540</b>							
<b>WG3711016-1</b>	<b>LCS</b>							
Trichloroethylene			103.8		%		70-130	30-MAR-22
Trichlorofluoromethane			101.8		%		60-140	30-MAR-22
Vinyl chloride			95.7		%		60-140	30-MAR-22
<b>WG3711016-2</b>	<b>MB</b>							
1,1,1,2-Tetrachloroethane			<0.50		ug/L		0.5	30-MAR-22
1,1,1,2,2-Tetrachloroethane			<0.50		ug/L		0.5	30-MAR-22
1,1,1-Trichloroethane			<0.50		ug/L		0.5	30-MAR-22
1,1,1,2-Trichloroethane			<0.50		ug/L		0.5	30-MAR-22
1,2-Dibromoethane			<0.20		ug/L		0.2	30-MAR-22
1,1-Dichloroethane			<0.50		ug/L		0.5	30-MAR-22
1,1-Dichloroethylene			<0.50		ug/L		0.5	30-MAR-22
1,2-Dichlorobenzene			<0.50		ug/L		0.5	30-MAR-22
1,2-Dichloroethane			<0.50		ug/L		0.5	30-MAR-22
1,2-Dichloropropane			<0.50		ug/L		0.5	30-MAR-22
1,3-Dichlorobenzene			<0.50		ug/L		0.5	30-MAR-22
1,4-Dichlorobenzene			<0.50		ug/L		0.5	30-MAR-22
2-Hexanone			<20		ug/L		20	30-MAR-22
Acetone			<20		ug/L		20	30-MAR-22
Benzene			<0.50		ug/L		0.5	30-MAR-22
Bromodichloromethane			<1.0		ug/L		1	30-MAR-22
Bromoform			<1.0		ug/L		1	30-MAR-22
Bromomethane			<0.50		ug/L		0.5	30-MAR-22
Carbon Disulfide			<1.0		ug/L		1	30-MAR-22
Carbon tetrachloride			<0.20		ug/L		0.2	30-MAR-22
Chlorobenzene			<0.50		ug/L		0.5	30-MAR-22
Chloroethane			<1.0		ug/L		1	30-MAR-22
Chloroform			<1.0		ug/L		1	30-MAR-22
Chloromethane			<2.0		ug/L		2	30-MAR-22
cis-1,2-Dichloroethylene			<0.50		ug/L		0.5	30-MAR-22
cis-1,3-Dichloropropene			<0.30		ug/L		0.3	30-MAR-22
Dibromochloromethane			<1.0		ug/L		1	30-MAR-22
Dichlorodifluoromethane			<1.0		ug/L		1	30-MAR-22
Dichloromethane			<2.0		ug/L		2	30-MAR-22
Ethylbenzene			<0.50		ug/L		0.5	30-MAR-22



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Client: Grounded Engineering Inc  
 1 Banigan Drive  
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Contact: Nicholas Piers

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>VOC-ROU-HS-WT</b>								
	<b>Water</b>							
<b>Batch</b>	<b>R5751540</b>							
<b>WG3711016-2 MB</b>								
m+p-Xylenes			<0.40		ug/L		0.4	30-MAR-22
Methyl Ethyl Ketone			<20		ug/L		20	30-MAR-22
Methyl Isobutyl Ketone			<20		ug/L		20	30-MAR-22
n-Hexane			<0.50		ug/L		0.5	30-MAR-22
MTBE			<0.50		ug/L		0.5	30-MAR-22
o-Xylene			<0.30		ug/L		0.3	30-MAR-22
Styrene			<0.50		ug/L		0.5	30-MAR-22
Tetrachloroethylene			<0.50		ug/L		0.5	30-MAR-22
trans-1,2-Dichloroethylene			<0.50		ug/L		0.5	30-MAR-22
trans-1,3-Dichloropropene			<0.30		ug/L		0.3	30-MAR-22
Trichloroethylene			<0.50		ug/L		0.5	30-MAR-22
Trichlorofluoromethane			<1.0		ug/L		1	30-MAR-22
Vinyl chloride			<0.50		ug/L		0.5	30-MAR-22
Surrogate: 1,4-Difluorobenzene			99.8		%		70-130	30-MAR-22
Surrogate: 4-Bromofluorobenzene			92.8		%		70-130	30-MAR-22
<b>WG3711016-5 MS</b>		<b>WG3711016-3</b>						
1,1,1,2-Tetrachloroethane			95.4		%		50-150	30-MAR-22
1,1,2,2-Tetrachloroethane			99.0		%		50-150	30-MAR-22
1,1,1-Trichloroethane			106.3		%		50-150	30-MAR-22
1,1,2-Trichloroethane			107.8		%		50-150	30-MAR-22
1,2-Dibromoethane			103.3		%		50-150	30-MAR-22
1,1-Dichloroethane			104.2		%		50-150	30-MAR-22
1,1-Dichloroethylene			104.5		%		50-150	30-MAR-22
1,2-Dichlorobenzene			109.4		%		50-150	30-MAR-22
1,2-Dichloroethane			112.4		%		50-150	30-MAR-22
1,2-Dichloropropane			112.5		%		50-150	30-MAR-22
1,3-Dichlorobenzene			109.1		%		50-150	30-MAR-22
1,4-Dichlorobenzene			109.4		%		50-150	30-MAR-22
2-Hexanone			107.1		%		50-150	30-MAR-22
Acetone			116.0		%		50-150	30-MAR-22
Benzene			102.1		%		50-150	30-MAR-22
Bromodichloromethane			114.2		%		50-150	30-MAR-22
Bromoform			99.8		%		50-150	30-MAR-22
Bromomethane			94.8		%		50-150	30-MAR-22



# Quality Control Report

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Client: Grounded Engineering Inc  
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Contact: Nicholas Piers

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
<b>VOC-ROU-HS-WT</b>								
	<b>Water</b>							
<b>Batch</b>	<b>R5751540</b>							
<b>WG3711016-5</b>	<b>MS</b>	<b>WG3711016-3</b>						
Carbon Disulfide			91.4		%		50-150	30-MAR-22
Carbon tetrachloride			99.7		%		50-150	30-MAR-22
Chlorobenzene			98.9		%		50-150	30-MAR-22
Chloroethane			111.4		%		50-150	30-MAR-22
Chloroform			110.0		%		50-150	30-MAR-22
Chloromethane			100.3		%		50-150	30-MAR-22
cis-1,2-Dichloroethylene			109.1		%		50-150	30-MAR-22
cis-1,3-Dichloropropene			100.7		%		50-150	30-MAR-22
Dibromochloromethane			97.3		%		50-150	30-MAR-22
Dichlorodifluoromethane			89.2		%		50-150	30-MAR-22
Dichloromethane			104.4		%		50-150	30-MAR-22
Ethylbenzene			103.4		%		50-150	30-MAR-22
m+p-Xylenes			106.8		%		50-150	30-MAR-22
Methyl Ethyl Ketone			100.1		%		50-150	30-MAR-22
Methyl Isobutyl Ketone			108.3		%		50-150	30-MAR-22
n-Hexane			96.1		%		50-150	30-MAR-22
MTBE			110.1		%		50-150	30-MAR-22
o-Xylene			103.2		%		50-150	30-MAR-22
Styrene			93.1		%		50-150	30-MAR-22
Tetrachloroethylene			90.6		%		50-150	30-MAR-22
trans-1,2-Dichloroethylene			105.8		%		50-150	30-MAR-22
trans-1,3-Dichloropropene			97.7		%		50-150	30-MAR-22
Trichloroethylene			98.9		%		50-150	30-MAR-22
Trichlorofluoromethane			100.1		%		50-150	30-MAR-22
Vinyl chloride			94.3		%		50-150	30-MAR-22
<b>Batch</b>	<b>R5751668</b>							
<b>WG3711510-4</b>	<b>DUP</b>	<b>WG3711510-3</b>						
Toluene		<0.40	<0.40	RPD-NA	ug/L	N/A	30	31-MAR-22
<b>WG3711510-1</b>	<b>LCS</b>							
Toluene			93.2		%		70-130	30-MAR-22
<b>WG3711510-2</b>	<b>MB</b>							
Toluene			<0.40		ug/L		0.4	30-MAR-22
<b>WG3711510-5</b>	<b>MS</b>	<b>WG3711510-3</b>						
Toluene			89.6		%		50-150	31-MAR-22



# Quality Control Report

Workorder: L2694356

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## Legend:

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Limit ALS Control Limit (Data Quality Objectives)  
DUP Duplicate  
RPD Relative Percent Difference  
N/A Not Available  
LCS Laboratory Control Sample  
SRM Standard Reference Material  
MS Matrix Spike  
MSD Matrix Spike Duplicate  
ADE Average Desorption Efficiency  
MB Method Blank  
IRM Internal Reference Material  
CRM Certified Reference Material  
CCV Continuing Calibration Verification  
CVS Calibration Verification Standard  
LCSD Laboratory Control Sample Duplicate

## Sample Parameter Qualifier Definitions:

---

Qualifier	Description
J	Duplicate results and limits are expressed in terms of absolute difference.
MS-B	Matrix Spike recovery could not be accurately calculated due to high analyte background in sample.
RPD-NA	Relative Percent Difference Not Available due to result(s) being less than detection limit.
RRQC	Refer to report remarks for information regarding this QC result.

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## Hold Time Exceedances:

All test results reported with this submission were conducted within ALS recommended hold times.

ALS recommended hold times may vary by province. They are assigned to meet known provincial and/or federal government requirements. In the absence of regulatory hold times, ALS establishes recommendations based on guidelines published by the US EPA, APHA Standard Methods, or Environment Canada (where available). For more information, please contact ALS.

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The ALS Quality Control Report is provided to ALS clients upon request. ALS includes comprehensive QC checks with every analysis to ensure our high standards of quality are met. Each QC result has a known or expected target value, which is compared against pre-determined data quality objectives to provide confidence in the accuracy of associated test results.

Please note that this report may contain QC results from anonymous Sample Duplicates and Matrix Spikes that do not originate from this Work Order.



# APPENDIX F



Excavation Dimensions: 112 m x 90 m

Section Cut: E-W

P5 Level Finished Floor: Elev. 94± m

P5 Base of Excavation/Drainage Layer: Elev. 93.5± m

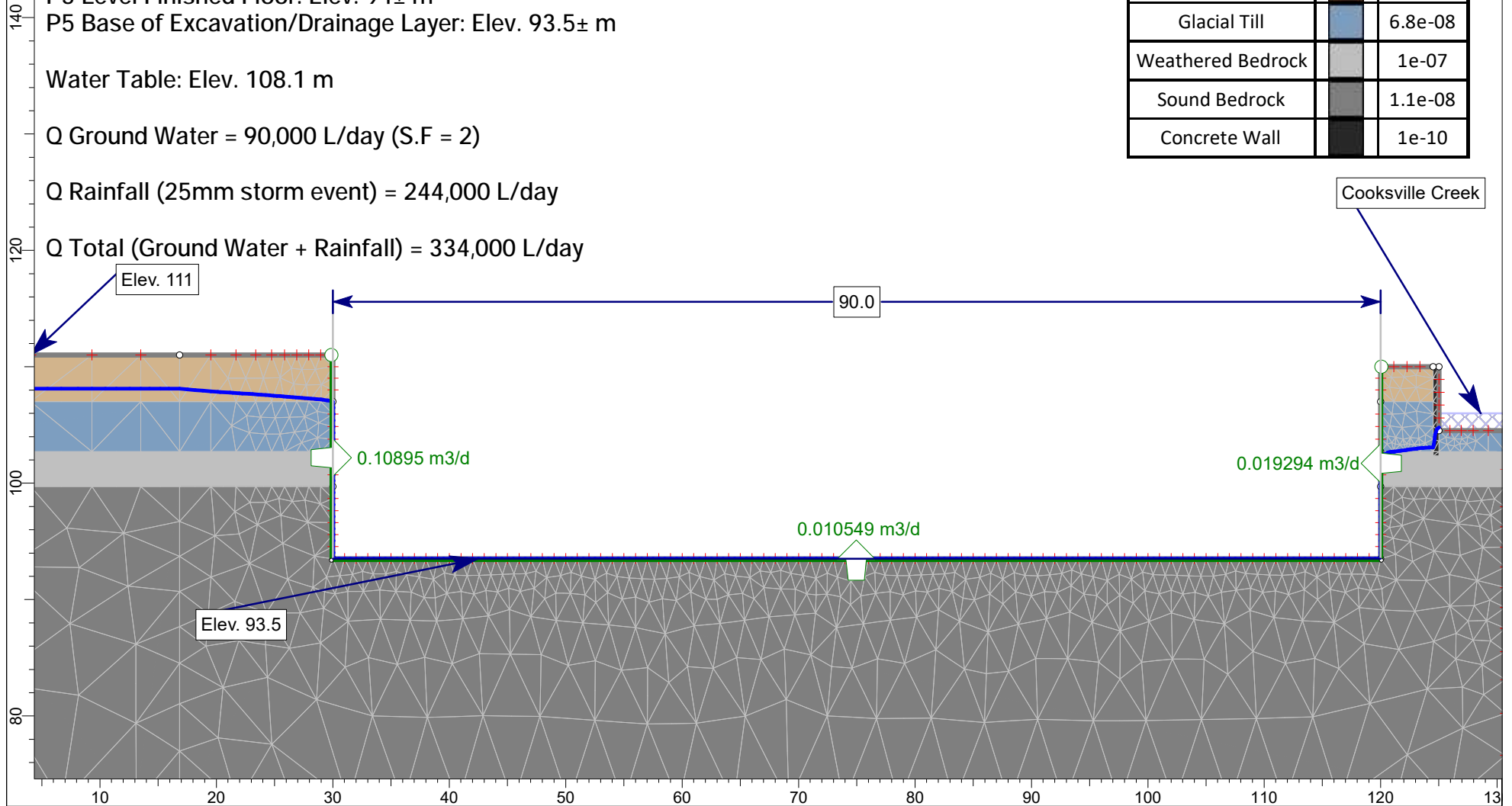
Water Table: Elev. 108.1 m


Q Ground Water = 90,000 L/day (S.F = 2)

Q Rainfall (25mm storm event) = 244,000 L/day

Q Total (Ground Water + Rainfall) = 334,000 L/day

Material Name	Color	KS (m/s)
Fill		1e-05
Glacial Till		6.8e-08
Weathered Bedrock		1e-07
Sound Bedrock		1.1e-08
Concrete Wall		1e-10



	File	21-067 60 Dundas St E			
	Analysis	Seepage model: Group 5			
	Ref.				
	RS2 File	21-067 60 Dundas St E Seepage model.slmd	Scale	1:495	Eng

# APPENDIX G



### SHORT TERM - PERMEABLE SHORING

Excavation Dimensions [m]		Rainfall Data		
N-S	112	Year	2	100
E-W	87	Hour	3	12
Area (m <sup>2</sup> )	9744	Depth (mm)	25	94
Perimeter (m)	398	Depth (m)	0.025	0.094
<b>Section</b>				
Base		Flow [m <sup>3</sup> /day]	Length [m]	Volume [L/day]
		0.010549	112	1,181
Sides		0.10895	398	43,362
Total				44,544
Factor of Safety	2.0			89,087
<b>Storm Events</b>				
2 Year [L/day]	100 Year [L/day]	Summary	L/day	L/min
243,600	916,000	Groundwater	90,000	62.5
		Rainfall	244,000	169.4
		Total	334,000	231.9

### LONG TERM - DRAINED FOUNDATIONS

Excavation Dimensions [m]		Rainfall Data		
N-S	112	Year	2	100
E-W	90	Hour	3	12
Area (m <sup>2</sup> )	10080	Depth (mm)	25	94
Perimeter (m)	404	Depth (m)	0.025	0.094
<b>Section</b>				
Base		Flow [m <sup>3</sup> /day]	Length [m]	Volume [L/day]
		0.010549	112	1,181
Sides		0.10895	398	43,362
Total				44,544
Factor of Safety	2.0			89,087
<b>Infiltration [L/day]</b>				
20319		Summary	L/day	L/min
		Groundwater	90,000	62.5
		Infiltration	21,000	14.6
		Total	111,000	77.1