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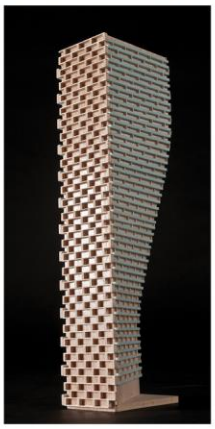
ENGINEERS & SCIENTISTS

PEDESTRIAN LEVEL WIND STUDY

805 Dundas Street East
Mississauga, Ontario

REPORT: GWE22-164-WTPLW



September 2, 2022

PREPARED FOR

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EXECUTIVE SUMMARY

This report describes a wind tunnel pedestrian level wind study undertaken to assess wind conditions for a proposed mixed-use development located at 805 Dundas Street East in Mississauga, Ontario. Two configurations were studied: (i) *existing scenario*, including all approved, surrounding developments and without the proposed development, and (ii) *proposed scenario* with the proposed development in place. The study involves wind tunnel measurements of pedestrian wind speeds using a physical scale model, combined with meteorological data integration, to assess pedestrian comfort at key areas within and surrounding the study site. Grade-level areas investigated include sidewalks, driveways, parking areas, landscaped spaces, private recreation areas, transit stops, and building access points. Wind comfort is also evaluated over the Level 2 outdoor amenity space. The results and recommendations derived from these considerations are summarized in the following paragraphs and detailed in the subsequent report.

Our work is based on industry standard wind tunnel testing and data analysis procedures, architectural drawings provided by KIRKOR Architects and Planners in July and September 2022, surrounding street layouts, as well as existing and approved future building massing, and recent site imagery.

A complete summary of the predicted wind conditions is provided in Section 5.2 of this report and is also illustrated in Figures 2A through 4B, as well as Tables A1-A2 and B1-B3 in the appendices. Based on wind tunnel test results, meteorological data analysis, and experience with similar developments in Mississauga, we conclude that the future wind conditions over all grade-level pedestrian wind-sensitive areas within and surrounding the study site will be acceptable for the intended uses on a seasonal basis. Additionally, the Level 2 outdoor amenity will experience wind conditions comfortable for sitting or more sedentary activities throughout the warmer months, without the need for mitigation.

Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no areas over the study site were found to experience conditions too windy for walking, or that could be considered unsafe.

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1. INTRODUCTION

This report describes a wind tunnel pedestrian level wind (PLW) study undertaken to assess wind conditions for a proposed mixed-use development located at 805 Dundas Street East in Mississauga, Ontario. Two configurations were studied: (i) *existing scenario*, including all approved, surrounding developments and without the proposed development, and (ii) *proposed scenario* with the proposed development in place. The study was performed in accordance with industry standard wind tunnel testing techniques, architectural drawings provided by KIRKOR Architects and Planners in July and September 2022, surrounding street layouts and existing and approved future building massing information, as well as recent site imagery.

2. TERMS OF REFERENCE

The focus of this wind tunnel pedestrian wind study is the proposed mixed-use development located at 805 Dundas Street East in Mississauga, Ontario. The study site is situated on a plot of land bounded by Dundas Street East to the southeast, Cedar Creek Lane to the southwest, Haines Road to the northeast, and existing three-storey townhouses to the northwest.

The proposed development comprises a 12-storey mixed-use residential building (Building 'A') and three 3-storey townhouse buildings (Buildings 'B', 'C', and 'D' which comprise of 6, 8, and 6 townhouse units respectively) located to the north of Building A (relative to project north). All developments are accessible via a driveway connecting to Haines Road. Surface parking, two levels of below-grade parking, and a loading zone are also accessible via the noted driveway. The residential lobby is located near the northeast corner of Building A, with retail entrances along the inner north façade and the south façade. Buildings B, C, and D are all accessed through private residential entrances along the south elevation. At Level 2 the building steps back from the inner north façade to provide an outdoor amenity terrace. The outdoor amenity terrace is accompanied by an attached indoor amenity space, while the rest of the floor, and the remainder of the building above, comprises residential occupancy. Above Level 2 the building rises with a uniform floor plate to Level 12 with additional step backs from the northeast and northwest segments at Levels 8 and 10. Above Level 12, the building is topped with two mechanical penthouses on the southwest and southeast corners of the building.

Regarding wind exposures, the near-field surroundings of the development (defined as an area falling within a 200-metre radius of the site) comprise of low-rise suburban exposure in all directions with open spaces to the northeast across Haines Road, and to the west across Cedar Creek Lane (St. john's Dixie Cemetery). The far-field surroundings (defined as the area beyond the near-field and within a two-kilometer radius) continues the low-rise suburban exposure in all directions.

Grade-level areas investigated include sidewalks, driveways, parking areas, landscaped spaces, private recreation areas, transit stops, and building access points. Wind comfort is also evaluated over the Level 2 outdoor amenity space. Figures 1A and 1B illustrates the *existing* and *proposed* study sites and surrounding context, respectively, and Photographs 1 through 6 depict the wind tunnel model used to conduct the study.

3. OBJECTIVES

The principal objectives of this study are to (i) determine pedestrian level wind comfort and safety conditions at key areas within and surrounding the development site; (ii) identify areas where wind conditions may interfere with the intended uses of outdoor spaces; (iii) recommend suitable mitigation measures, where required; and (iv) evaluate the influence of the proposed development on the existing wind conditions.

4. METHODOLOGY

The approach followed to quantify pedestrian wind conditions over the site is based on wind tunnel measurements of wind speeds at selected locations on a reduced-scale physical model, meteorological analysis of the Mississauga area wind climate and synthesis of wind tunnel data with industry-accepted guidelines[1]. The following sections describe the analysis procedures, including a discussion of the pedestrian comfort and safety guidelines.

4.1 Wind Tunnel Context Modelling

A detailed PLW study is performed to determine the influence of local winds at the pedestrian level for a proposed development. The physical model of the proposed development and relevant surroundings,

[1] Pedestrian Level Wind Study Terms of Reference Guide, 2022

illustrated in Photographs 1 through 6 following the main text, was constructed at a scale of 1:400. The wind tunnel model includes all existing buildings and approved future developments within a full-scale diameter of approximately 840 metres. The general concept and approach to wind tunnel modelling is to provide building and topographic detail in the immediate vicinity of the study site on the surrounding model, and to rely on a length of wind tunnel upwind of the model to develop wind properties consistent with known turbulent intensity profiles that represent the surrounding terrain.

An industry standard practice is to omit trees, vegetation, and other existing and planned landscape elements from the wind tunnel model due to the difficulty of providing accurate seasonal representation of vegetation. The omission of trees and other landscaping elements produces slightly more conservative wind speed values.

4.2 Wind Speed Measurements

The PLW study was performed by testing a total of 74 sensor locations on the scale model in Gradient Wind's wind tunnel. Of these 74 sensors, 72 were located at grade and the remaining two sensors were located over the Level 2 amenity terrace. Wind speed measurements were performed for each of the 74 sensors for 36 wind directions at 10° intervals. Figures 1A and 1B illustrates the *existing* and *proposed* study sites and surrounding context, respectively, while sensor locations used to investigate wind conditions are illustrated in Figures 2A through 4B.

Mean and peak wind speed values for each location and wind direction were calculated from real-time pressure measurements, recorded at a sample rate of 500 samples per second, and taken over a 60-second time period. This period at model-scale corresponds approximately to one hour in full-scale, which matches the time frame of full-scale meteorological observations. Measured mean and gust wind speeds at grade were referenced to the wind speed measured near the ceiling of the wind tunnel to generate mean and peak wind speed ratios. Ceiling height in the wind tunnel represents the depth of the boundary layer of wind flowing over the earth's surface, referred to as the gradient height. Within this boundary layer, mean wind speed increases up to the gradient height and remains constant thereafter. Appendices C and D provide greater detail of the theory behind wind speed measurements. Wind tunnel measurements for this project, conducted in Gradient Wind's wind tunnel facility, meet or exceed

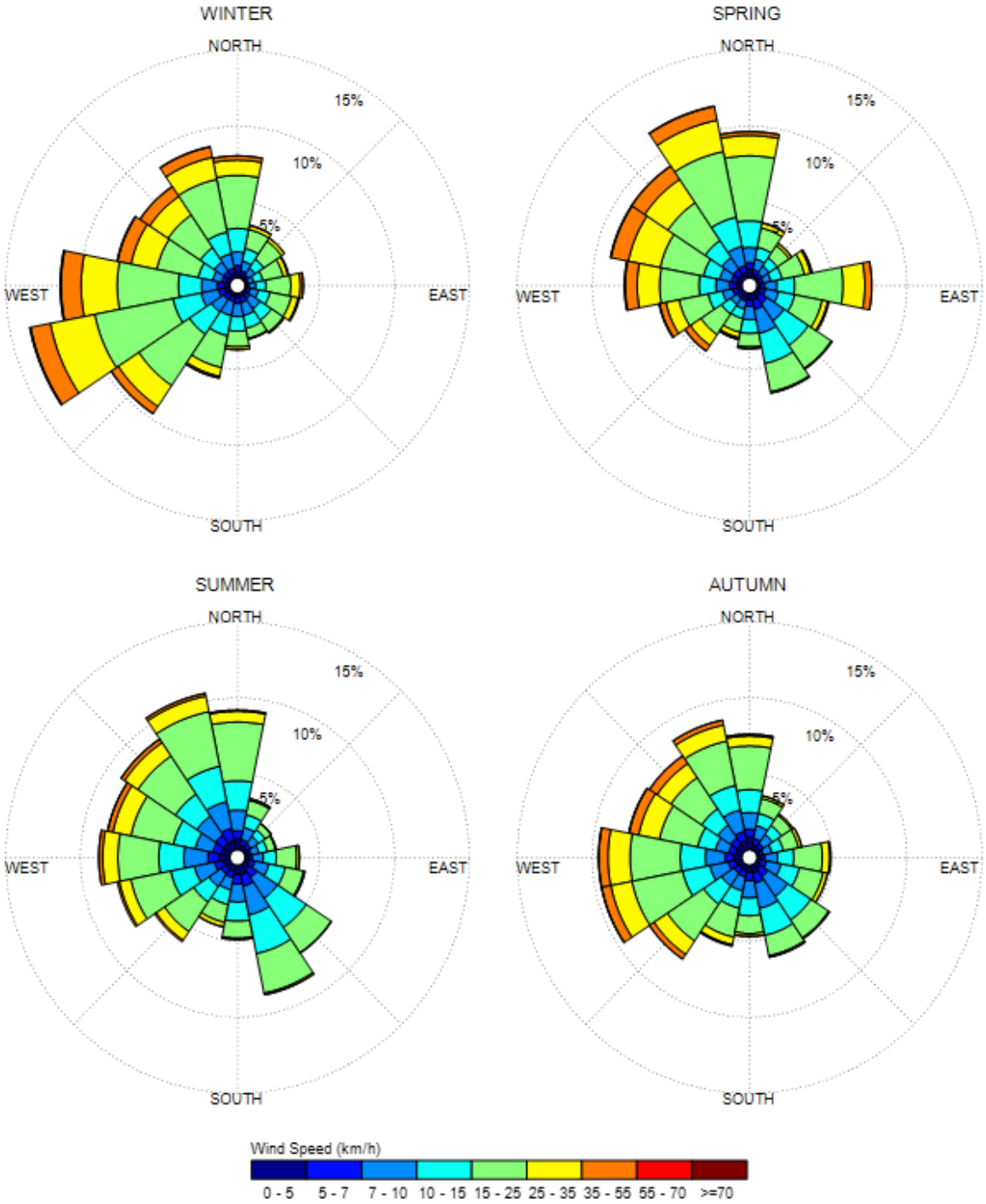
guidelines found in the National Building Code of Canada 2015 and of 'Wind Tunnel Studies of Buildings and Structures', ASCE Manual 7 Reports on Engineering Practice No 67.

4.3 Meteorological Data Analysis - Pearson International Airport

A statistical model for winds in Mississauga, was developed from over 50 years of hourly meteorological wind data recorded at Pearson International Airport. Wind speed and direction data were analyzed for each month of the year in order to determine the statistically prominent wind directions and corresponding speeds, and to characterize similarities between monthly weather patterns. Based on this portion of the analysis, the four seasons are represented by grouping data from consecutive months based on similarity of weather patterns, and not according to the traditional calendar method.

The statistical model of the Mississauga area wind climate, which indicates the directional character of local winds on a seasonal basis, is illustrated on the following page. The plots illustrate seasonal distribution of measured wind speeds and directions in km/h. Probabilities of occurrence of different wind speeds are represented as stacked polar bars in sixteen azimuth divisions. The radial direction represents the percentage of time for various wind speed ranges per wind direction during the measurement period. The preferred wind speeds and directions can be identified by the longer length of the bars. For Pearson International Airport, the most common winds concerning pedestrian comfort occur from the southwest clockwise to the north, as well as those from the east. The directional preference and relative magnitude of the wind speed varies somewhat from season to season, with the summer months displaying the calmest winds relative to the remaining seasonal periods.

SEASONAL DISTRIBUTION OF WINDS FOR VARIOUS PROBABILITIES
PEARSON INTERNATIONAL AIRPORT, TORONTO, ONTARIO



Notes:

1. Radial distances indicate percentage of time of wind events.
2. Wind speeds are mean hourly in km/h, measured at 10 m above the ground.

4.4 Pedestrian Comfort and Safety Guidelines

Pedestrian comfort and safety guidelines are based on the mechanical effects of wind without consideration of other meteorological conditions (i.e. temperature, relative humidity). The comfort guidelines assume that pedestrians are appropriately dressed for a specified outdoor activity during any given season. Four pedestrian comfort classes are based on 80% non-exceedance Guest Equivalent Mean (GEM) wind speed ranges, which include (i) Sitting; (ii) Standing; (iii) Walking; and (iv) Uncomfortable. More specifically, the comfort classes and associated GEM wind speed ranges are summarized as follows:

(i) **Sitting** – A wind speed below 10 km/h (i.e. 0 – 10 km/h) would be considered acceptable for sedentary activities, including sitting.

(ii) **Standing** – A wind speed below 15 km/h (i.e. 10 km/h – 15 km/h) is acceptable for activities such as standing or leisurely strolling.

(iii) **Walking** – A wind speed below 20 km/h (i.e. 15 km/h – 20 km/h) is acceptable for walking or more vigorous activities.

(iv) **Uncomfortable** – A wind speed over 20 km/h is classified as uncomfortable from a pedestrian comfort standpoint. Brisk walking and exercise, such as jogging, would be acceptable for moderate excesses of this criterion.

The pedestrian safety wind speed guideline is based on the approximate threshold that would cause a vulnerable member of the population to fall. A 0.1% exceedance gust wind speed of greater than 90 km/h is classified as dangerous.

Experience and research on people's perception of mechanical wind effects has shown that if the wind speed levels are exceeded for more than 20% of the time, the activity level would be judged to be uncomfortable by most people. For instance, if wind speeds of 10 km/h were exceeded for more than 20% of the time most pedestrians would judge that location to be too windy for sitting or more sedentary activities. Similarly, if 20 km/h at a location were exceeded for more than 20% of the time, walking or less vigorous activities would be considered uncomfortable. As most of these criteria are based on subjective reactions of a population to wind forces, their application is partly based on experience and judgment.

Once the pedestrian wind speed predictions have been established at tested locations, the assessment of pedestrian comfort involves determining the suitability of the predicted wind conditions for their

associated spaces. This step involves comparing the predicted comfort class to the desired comfort class, which is dictated by the location type represented by the sensor (i.e. a sidewalk, building entrance, amenity space, or other). An overview of common pedestrian location types and their desired comfort classes are summarized below.

DESIRED PEDESTRIAN COMFORT CLASSES FOR VARIOUS LOCATION TYPES

Location Types	Desired Comfort Classes
Primary Building Entrance	Standing
Secondary Building Access Point	Walking
Public Sidewalks / Pedestrian Walkways	Walking
Outdoor Amenity Spaces	Sitting / Standing
Cafés / Patios / Benches / Gardens	Sitting / Standing
Plazas	Standing / Walking
Transit Stops	Standing
Public Parks	Sitting / Walking
Garage / Service Entrances	Walking
Vehicular Drop-Off Zones	Walking
Laneways / Loading Zones	Walking

5. RESULTS AND DISCUSSION

Tables A1 through A2 in Appendix A provide a summary of seasonal comfort predictions for each sensor location under the *existing* massing scenario. Similarly, Tables B1 through B3 in Appendix B provide the seasonal comfort predictions for under the *proposed* massing scenario. The tables indicate the 80% non-exceedance GEM wind speeds and corresponding comfort classifications as defined in Section 4.4. In other words, a wind speed threshold of 19.1 for the summer season indicates that 80% of the measured data falls at or below 19.1 km/h during the summer months and conditions are therefore suitable for walking, as the 80% threshold value falls within the exceedance range of 15-20 km/h for walking. The tables include the predicted threshold values for each sensor location during each season, accompanied by the corresponding predicted comfort class (i.e. sitting, standing, walking, etc.).

The most significant findings of the PLW study are summarized in Sections 5.1 and 5.2. To assist with understanding and interpretation, predicted conditions for the proposed development are also illustrated in colour-coded format in Figures 2A through 4B. Conditions suitable for sitting are represented by the colour blue, while standing is represented by green, and walking by yellow.

5.1 Pedestrian Comfort Suitability – *Existing Scenario*

Based on the analysis of the measured data, consideration of local climate data, and the suitability descriptors provided in Tables A1-A2 in Appendix A and illustrated in Figures 2A through 2B, this section summarizes the significant findings of the PLW study with respect to the *existing scenario*, as follows:

1. All public sidewalks, driveways, surface parking, and landscaped areas within and surrounding the proposed development currently experience wind conditions suitable for walking or better during each seasonal period, which is acceptable for the intended uses of the spaces.
2. All transit stops surrounding the development (Sensors 10, and 15) currently experience wind conditions suitable for standing throughout all seasonal periods, which is appropriate.
3. Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no areas over the study site were found to experience wind conditions that are considered unsafe.

5.2 Pedestrian Comfort Suitability – *Proposed Scenario*

Based on the analysis of the measured data, consideration of local climate data, and the suitability descriptors provided in Tables B1-B3 in Appendix B and illustrated in Figures 3A through 4B, this section summarizes the significant findings of the PLW study with respect to the *proposed scenario*, as follows:

1. All public sidewalks, driveways, surface parking, and landscaped areas within and surrounding the proposed development will experience wind conditions suitable for walking or better during each seasonal period, which is acceptable for the intended uses of the spaces.
2. The residential lobby entrance (Sensor 65) as well as all retail entrance locations will experience wind conditions suitable for standing or better throughout the year, which is acceptable.
3. All secondary access points (including stairwell exits, vehicle entrances, and private access points) will experience wind conditions suitable for walking or better throughout all seasonal periods which is appropriate.
4. The future private recreation space to the west of the building (Sensors 2-4) will be comfortable for standing during the summer and for a mix of standing and walking during the winter months. If seating areas will be provided within this space, it is recommended to provide vertical wind barriers upwind of designated spaces to deflect prominent northwesterly wind directions.
5. All transit stops surrounding the development (Sensors 10, and 15) will experience wind conditions suitable for standing throughout all seasonal periods, which is appropriate.
6. The Level 2 outdoor amenity terrace will experience wind conditions suitable for sitting or more sedentary activities, throughout the summer months, without the need for mitigation.
7. Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no areas over the study site were found to experience wind conditions that are considered unsafe.

6. CONCLUSIONS AND RECOMMENDATIONS

This report summarizes the methodology, results, and recommendations related to a pedestrian level wind study for the proposed mixed-use development located at 805 Dundas Street East in Mississauga,

Ontario. The study was performed in accordance with industry standard wind tunnel testing and data analysis procedures.

A complete summary of the predicted wind conditions is provided in Section 5 of this report and is also illustrated in Figures 2A through 4B, as well as Tables A1-A2 and B1-B3 in the appendices. Based on wind tunnel test results, meteorological data analysis, and experience with similar developments in Mississauga, we conclude that the future wind conditions over all grade-level pedestrian wind-sensitive areas within and surrounding the study site will be acceptable for the intended uses on a seasonal basis. Additionally, the Level 2 outdoor amenity will experience wind conditions comfortable for sitting or more sedentary activities throughout the warmer months, without the need for mitigation.

Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no areas over the study site were found to experience conditions too windy for walking, or that could be considered unsafe.

This concludes our pedestrian level wind study and report. Please advise the undersigned of any questions or comments.

Sincerely,

Gradient Wind Engineering Inc.

Logan McFadden, B.Eng.,
Junior Wind Scientist

Nick Petersen, P.Eng.,
Wind Engineer

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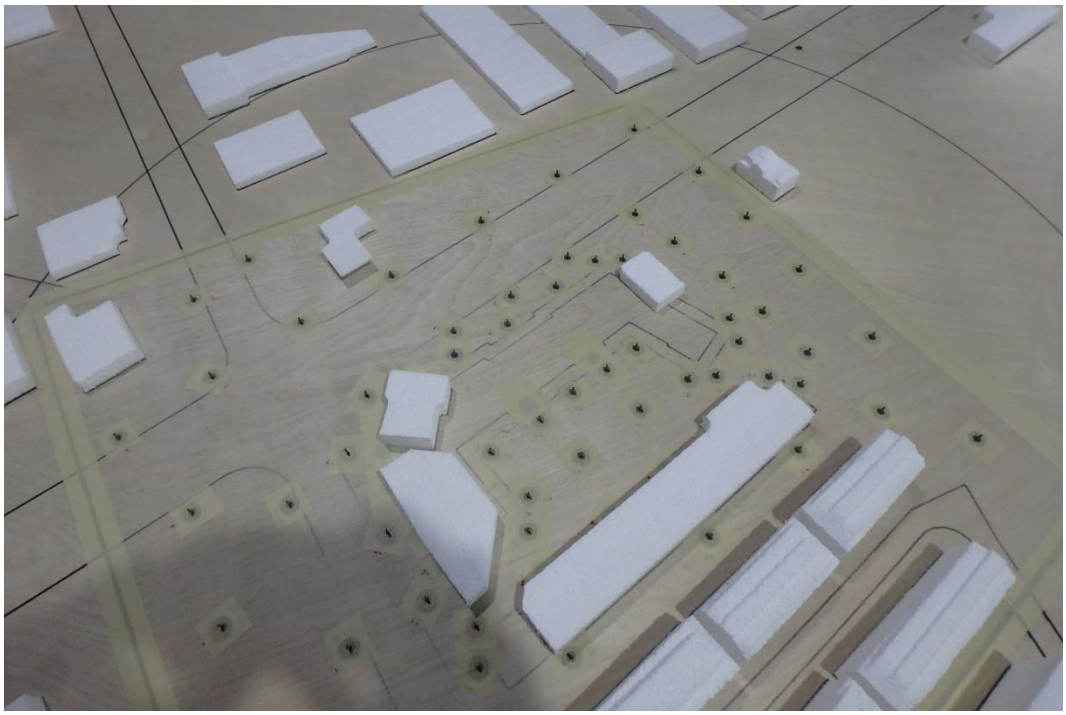
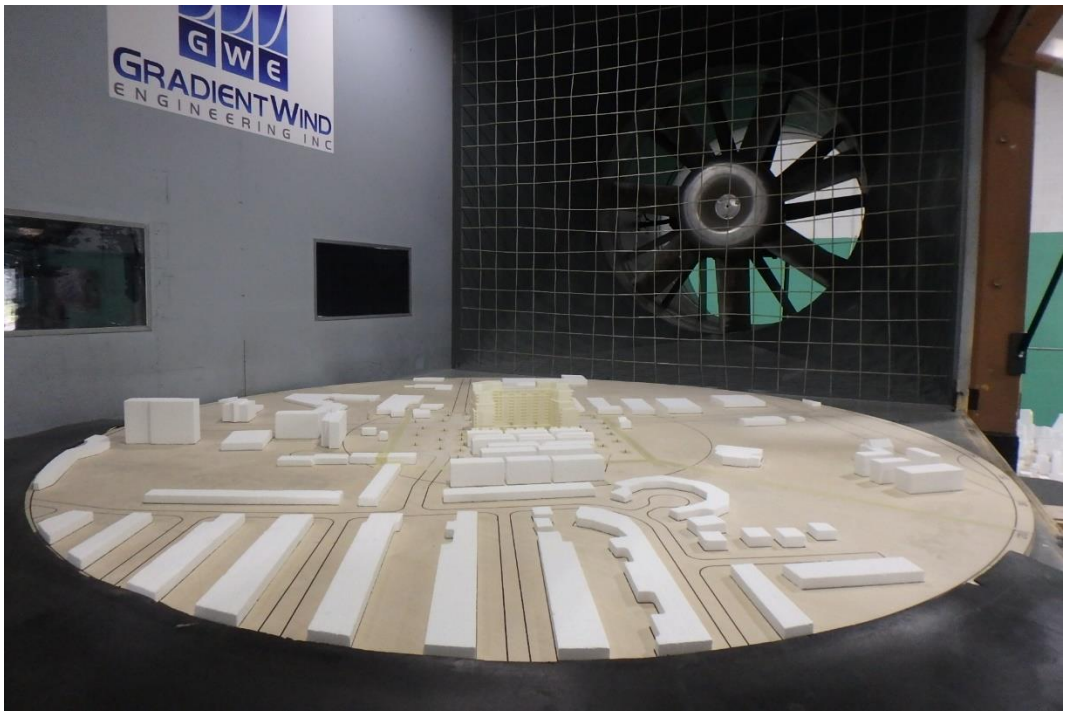


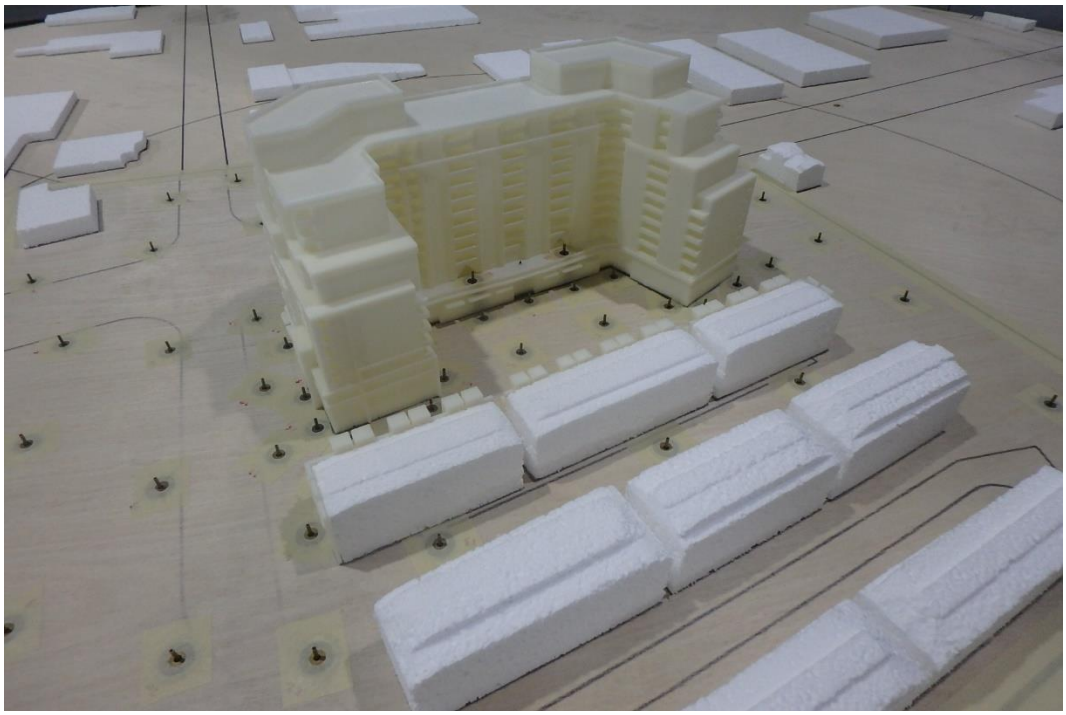
PHOTOGRAPH 1: CLOSE-UP VIEW OF EXISTING CONTEXT MODEL LOOKING SOUTH

PHOTOGRAPH 2: CLOSE-UP VIEW OF EXISTING CONTEXT MODEL LOOKING NORTH

PHOTOGRAPH 3: STUDY MODEL INSIDE THE GWE WIND TUNNEL LOOKING DOWNWIND

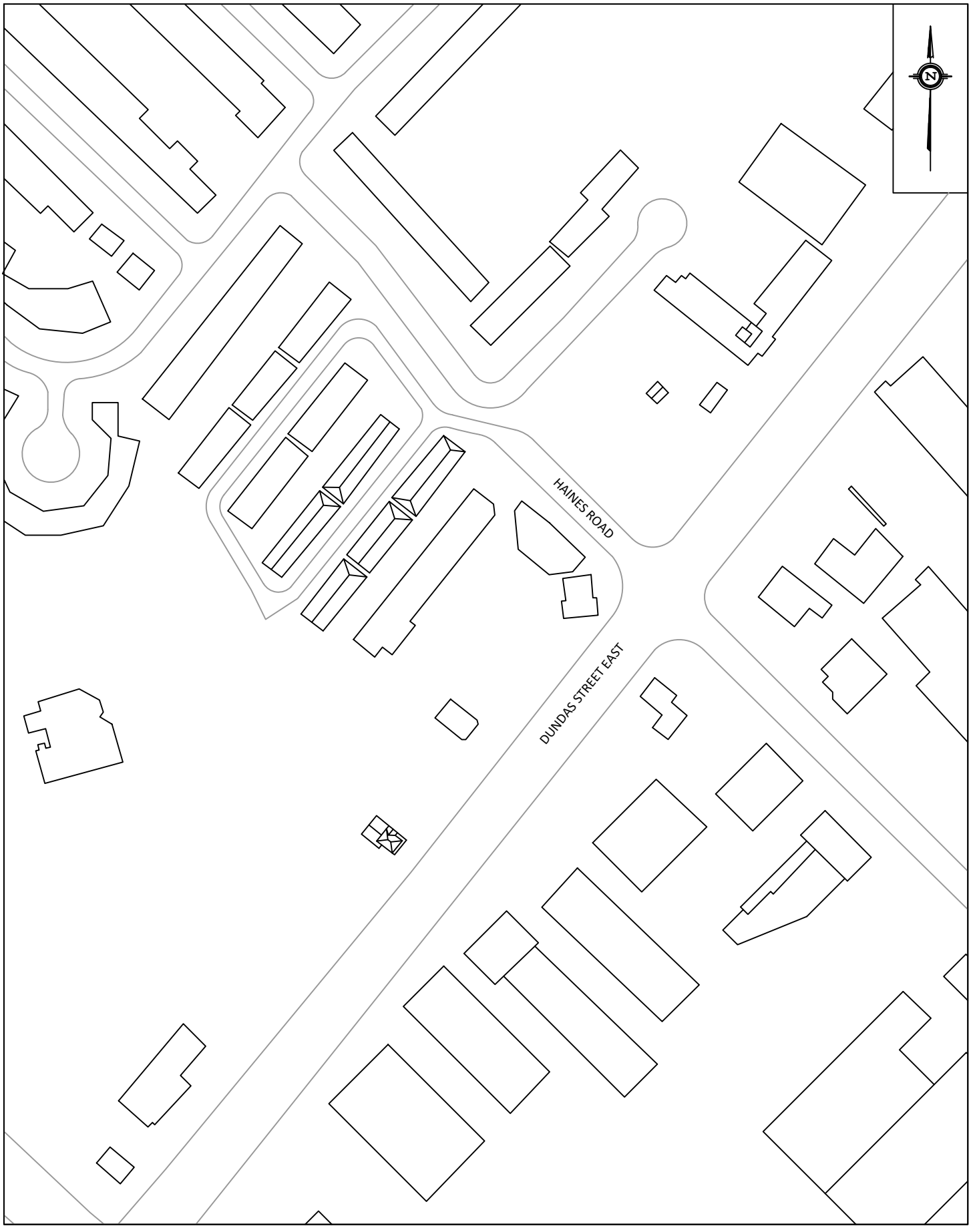


PHOTOGRAPH 4: STUDY MODEL INSIDE THE GWE WIND TUNNEL LOOKING UPWIND



PHOTOGRAPH 5: CLOSE-UP VIEW OF STUDY MODEL LOOKING SOUTH

PHOTOGRAPH 6: CLOSE-UP VIEW OF STUDY MODEL LOOKING NORTH



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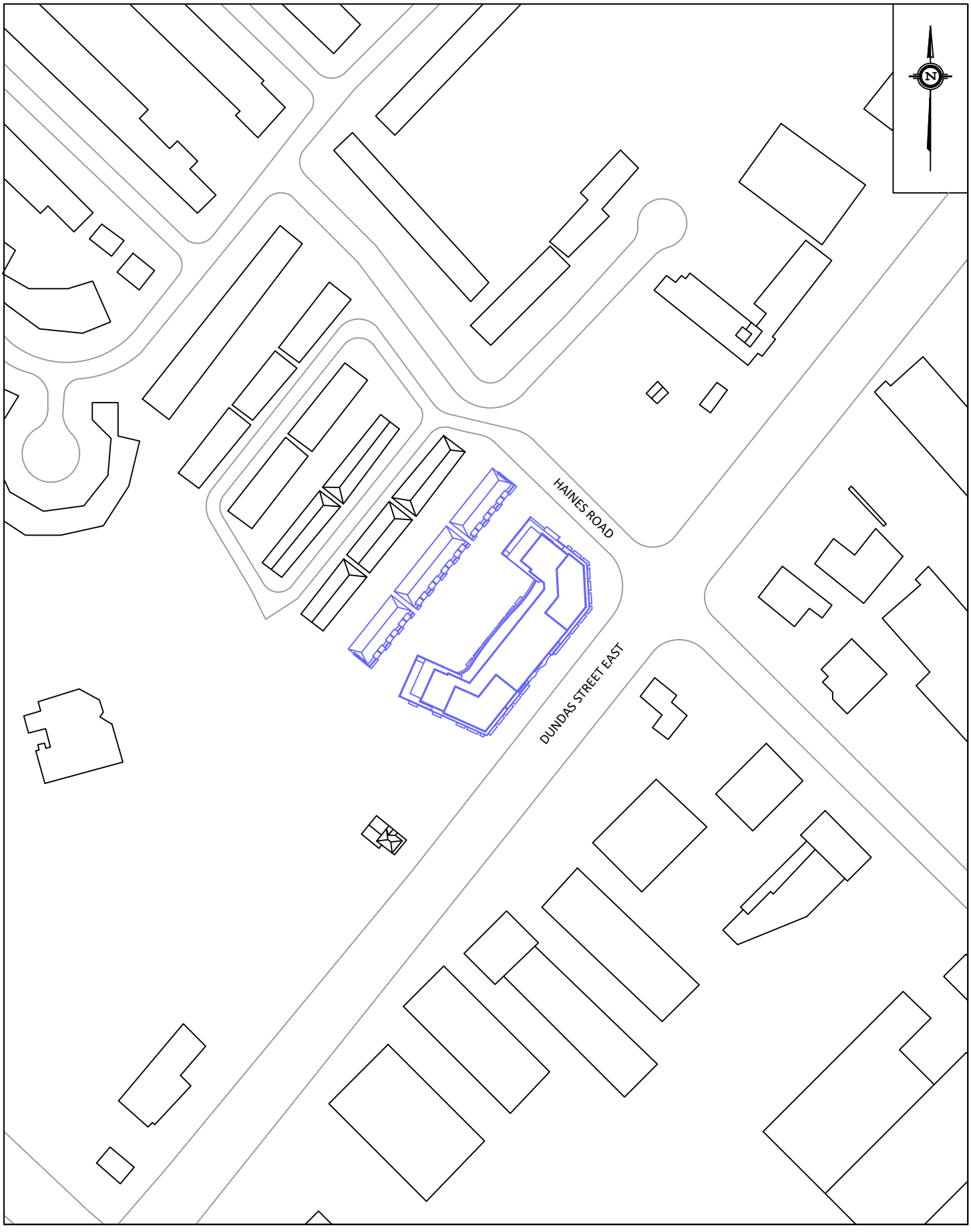
PROJECT	805 DUNDAS STREET EAST, MISSISSAUGA PEDESTRIAN LEVEL WIND STUDY
SCALE	1:2500 (APPROX.)
DRAWING NO.	GW22-164-PLW-1A
DATE	SEPTEMBER 2, 2022
DRAWN BY	C.E.

DESCRIPTION

FIGURE 1A:
EXISTING SITE PLAN
AND SURROUNDING CONTEXT



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DATE	SEPTEMBER 2, 2022
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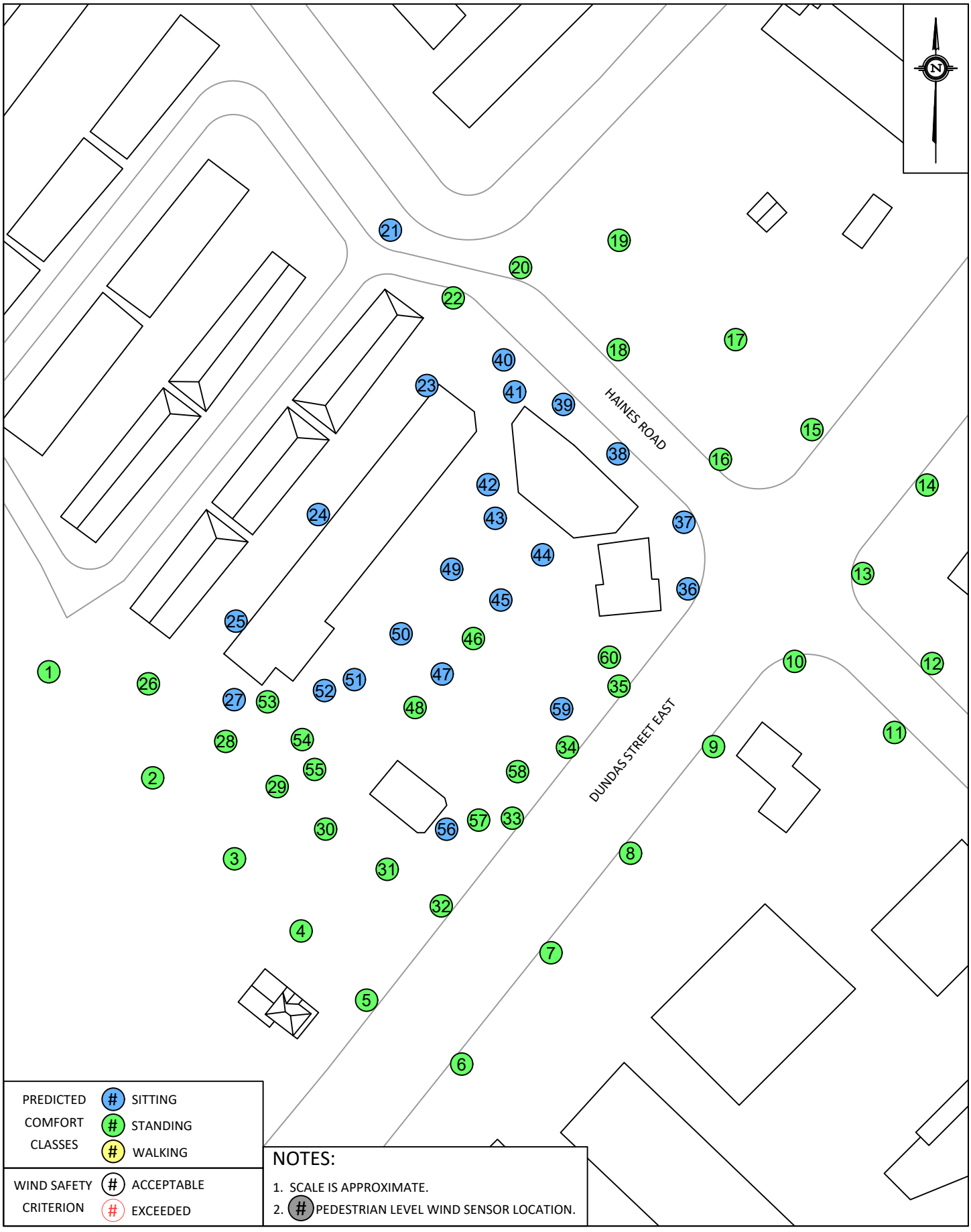
DESCRIPTION

FIGURE 1B:
PROPOSED SITE PLAN
AND SURROUNDING CONTEXT



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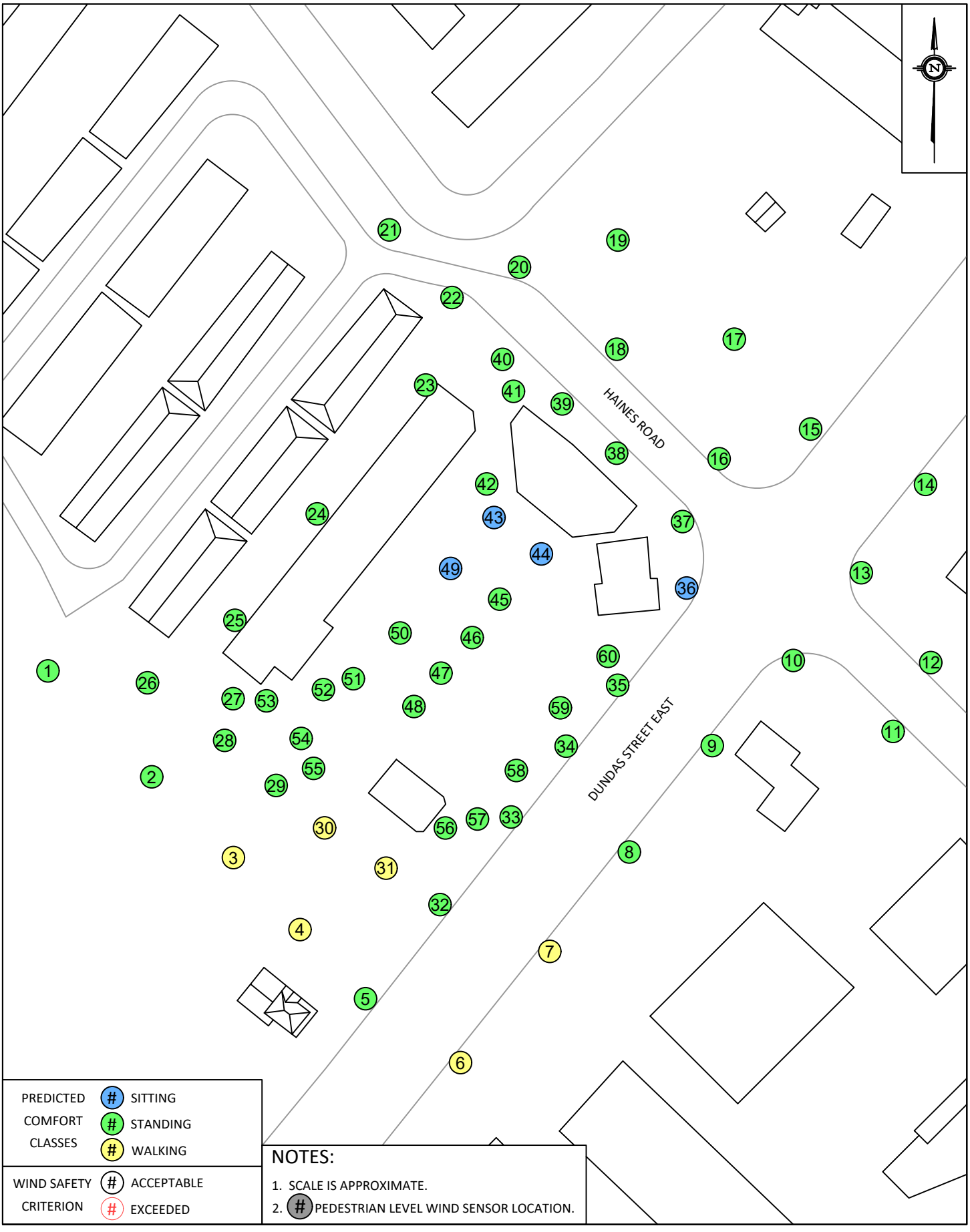
DESCRIPTION

FIGURE 2A: SUMMER
EXISTING GROUND FLOOR PLAN
PEDESTRIAN COMFORT PREDICTIONS



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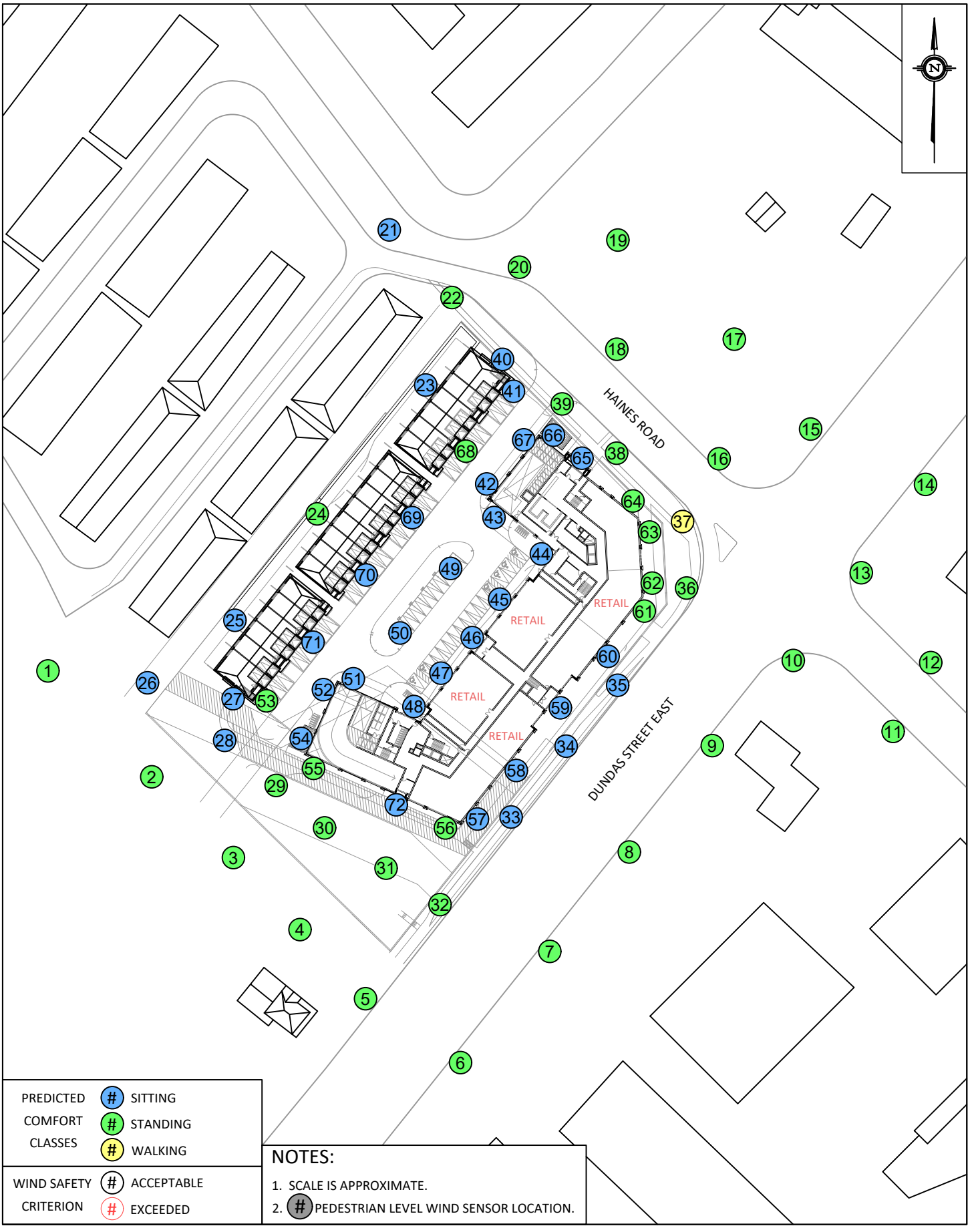
DRAWN BY	C.E.

DESCRIPTION

FIGURE 2B: WINTER
EXISTING GROUND FLOOR PLAN
PEDESTRIAN COMFORT PREDICTIONS



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DESCRIPTION

FIGURE 3A: SUMMER
PROPOSED GROUND FLOOR PLAN
PEDESTRIAN COMFORT PREDICTIONS

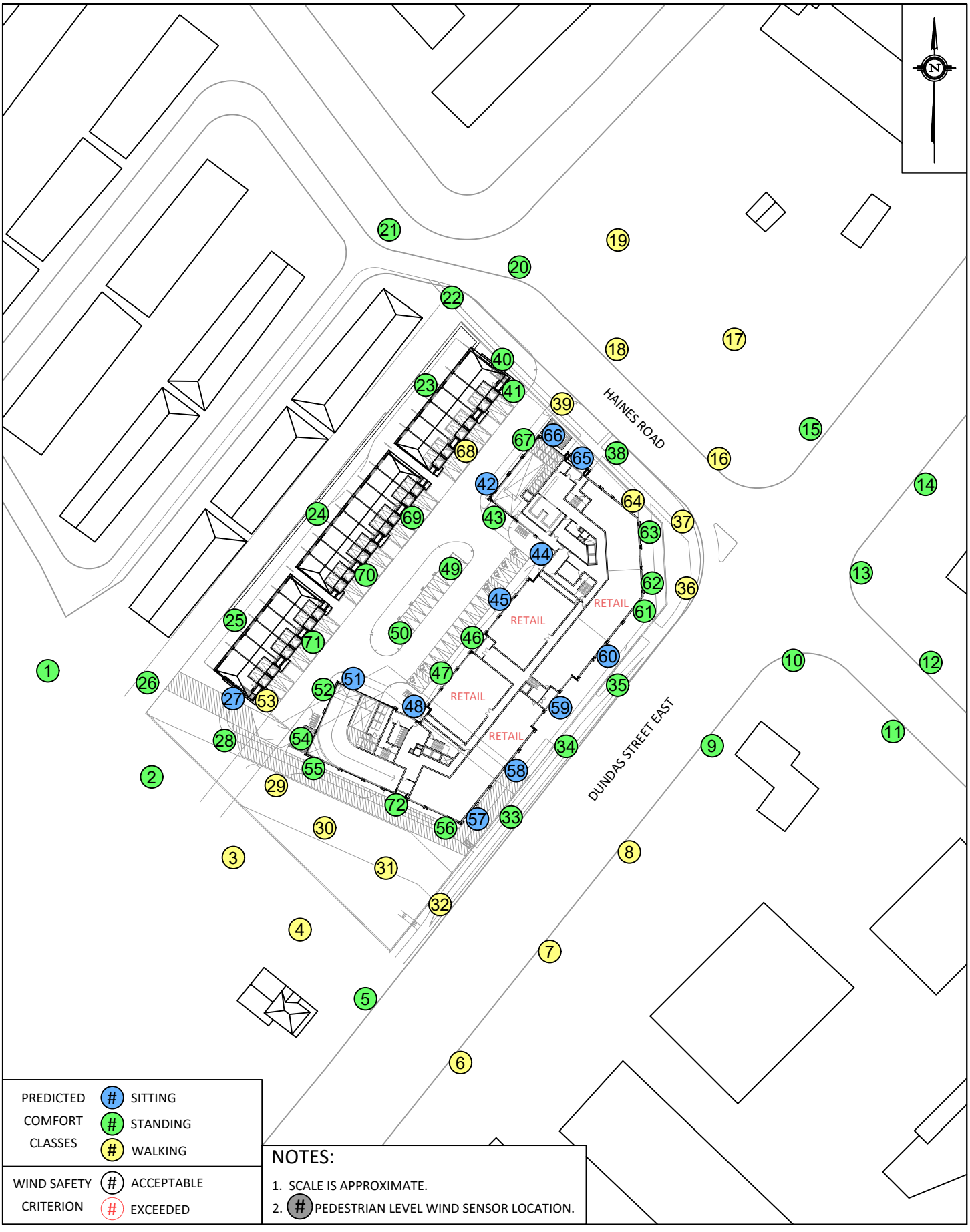

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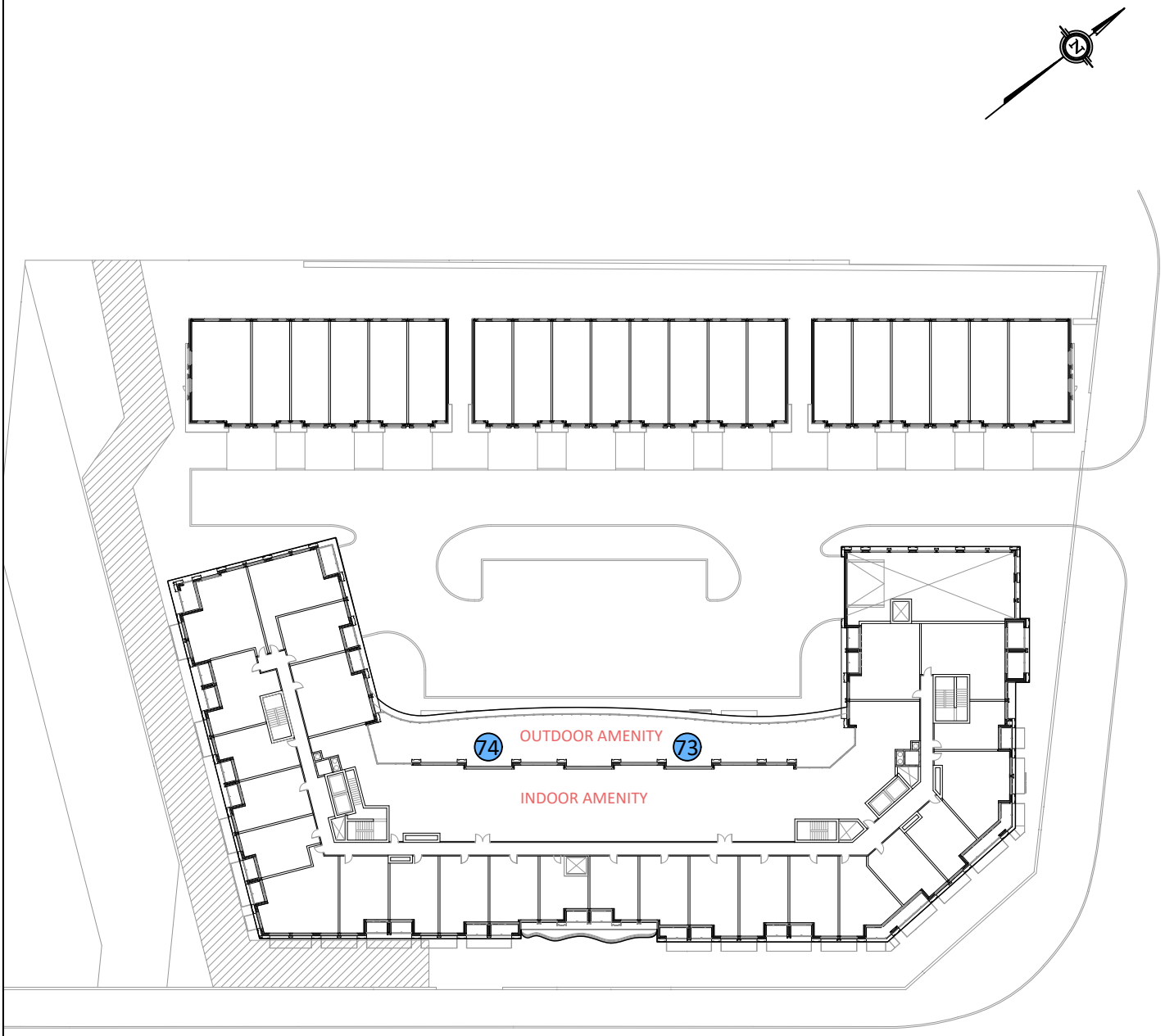
FIGURE 3B: WINTER
PROPOSED GROUND FLOOR PLAN
PEDESTRIAN COMFORT PREDICTIONS



PREDICTED COMFORT CLASSES	#	SITTING
	#	STANDING
	#	WALKING
WIND SAFETY CRITERION	#	ACCEPTABLE
	#	EXCEEDED

NOTES:

1. SCALE IS APPROXIMATE.
2. # PEDESTRIAN LEVEL WIND SENSOR LOCATION.

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DATE	SEPTEMBER 2, 2022
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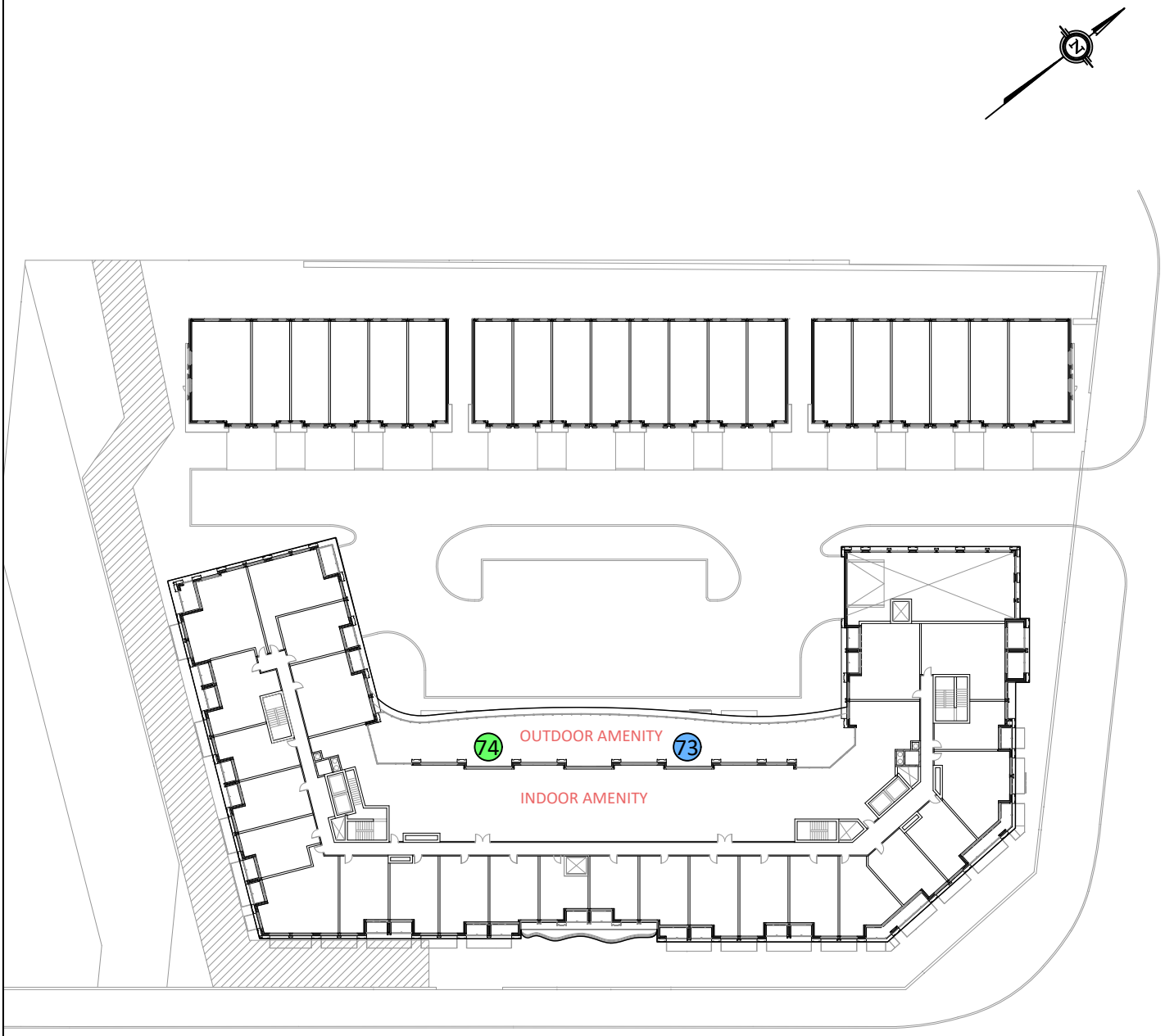
DESCRIPTION

FIGURE 4A: SUMMER
PROPOSED LEVEL 2 AMENITY PLAN
PEDESTRIAN COMFORT PREDICTIONS



PREDICTED COMFORT CLASSES	#	SITTING
	#	STANDING
	#	WALKING
WIND SAFETY CRITERION	#	ACCEPTABLE
	#	EXCEEDED

NOTES:

1. SCALE IS APPROXIMATE.
2. # PEDESTRIAN LEVEL WIND SENSOR LOCATION.

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DESCRIPTION

FIGURE 4B: WINTER
PROPOSED LEVEL 2 AMENITY PLAN
PEDESTRIAN COMFORT PREDICTIONS

APPENDIX A

PEDESTRIAN COMFORT SUITABILITY, TABLES A1-A2 (EXISTING SCENARIO)

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Guidelines	
Pedestrian Comfort	**20% exceedance wind speed** 0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable
Pedestrian Safety	**0.1% exceedance wind speed** 0-90 km/h = Safe

TABLE A1: SUMMARY OF PEDESTRIAN COMFORT (EXISTING SCENARIO)

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
1	11.3	Standing	13.5	Standing	46.1	Safe
2	11.3	Standing	14.7	Standing	52.3	Safe
3	12.0	Standing	15.6	Walking	52.8	Safe
4	12.1	Standing	16.3	Walking	57.5	Safe
5	11.2	Standing	13.7	Standing	45.9	Safe
6	12.7	Standing	16.5	Walking	53.3	Safe
7	12.5	Standing	16.2	Walking	53.0	Safe
8	11.1	Standing	14.2	Standing	47.7	Safe
9	10.5	Standing	13.2	Standing	44.6	Safe
10	11.1	Standing	14.0	Standing	47.6	Safe
11	11.7	Standing	14.5	Standing	49.3	Safe
12	12.0	Standing	15.0	Standing	51.4	Safe
13	11.5	Standing	13.9	Standing	47.2	Safe
14	10.4	Standing	13.4	Standing	48.7	Safe
15	11.3	Standing	14.2	Standing	51.0	Safe
16	11.1	Standing	13.3	Standing	48.3	Safe
17	11.8	Standing	14.9	Standing	51.9	Safe
18	10.8	Standing	13.1	Standing	45.9	Safe
19	11.6	Standing	13.5	Standing	47.9	Safe
20	10.3	Standing	12.2	Standing	42.5	Safe
21	9.5	Sitting	13.0	Standing	51.0	Safe
22	10.6	Standing	12.3	Standing	47.1	Safe
23	9.0	Sitting	11.1	Standing	44.6	Safe
24	8.5	Sitting	10.1	Standing	38.8	Safe
25	8.1	Sitting	11.0	Standing	57.5	Safe
26	10.2	Standing	13.4	Standing	49.9	Safe
27	8.4	Sitting	11.5	Standing	47.4	Safe
28	10.4	Standing	14.2	Standing	53.6	Safe
29	11.1	Standing	14.7	Standing	53.0	Safe
30	11.7	Standing	15.2	Walking	50.9	Safe
31	11.3	Standing	15.3	Walking	53.6	Safe
32	11.6	Standing	15.0	Standing	51.1	Safe
33	11.5	Standing	14.3	Standing	47.9	Safe
34	11.5	Standing	14.5	Standing	48.1	Safe
35	10.3	Standing	13.2	Standing	46.8	Safe

Guidelines	
Pedestrian Comfort	**20% exceedance wind speed** 0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable
Pedestrian Safety	**0.1% exceedance wind speed** 0-90 km/h = Safe

TABLE A2: SUMMARY OF PEDESTRIAN COMFORT (EXISTING SCENARIO)

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
36	8.2	Sitting	9.4	Sitting	38.8	Safe
37	9.3	Sitting	11.1	Standing	46.8	Safe
38	9.2	Sitting	11.8	Standing	43.1	Safe
39	8.5	Sitting	10.5	Standing	41.0	Safe
40	9.5	Sitting	11.7	Standing	43.7	Safe
41	9.5	Sitting	12.2	Standing	44.3	Safe
42	8.8	Sitting	10.6	Standing	39.0	Safe
43	7.7	Sitting	9.1	Sitting	33.0	Safe
44	7.8	Sitting	9.6	Sitting	35.9	Safe
45	9.3	Sitting	11.3	Standing	40.0	Safe
46	10.2	Standing	12.5	Standing	42.6	Safe
47	9.5	Sitting	11.9	Standing	42.8	Safe
48	10.2	Standing	13.3	Standing	46.9	Safe
49	7.5	Sitting	9.0	Sitting	35.2	Safe
50	8.6	Sitting	10.7	Standing	39.9	Safe
51	8.9	Sitting	11.5	Standing	42.2	Safe
52	9.6	Sitting	12.6	Standing	47.8	Safe
53	10.8	Standing	15.0	Standing	55.8	Safe
54	10.9	Standing	14.6	Standing	52.8	Safe
55	11.4	Standing	14.6	Standing	50.9	Safe
56	8.2	Sitting	10.2	Standing	42.3	Safe
57	10.9	Standing	13.2	Standing	45.9	Safe
58	11.2	Standing	14.0	Standing	46.9	Safe
59	9.8	Sitting	12.4	Standing	44.2	Safe
60	10.8	Standing	14.7	Standing	51.9	Safe

APPENDIX B

PEDESTRIAN COMFORT SUITABILITY, TABLES B1-B3 (PROPOSED SCENARIO)

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Guidelines	
Pedestrian Comfort	**20% exceedance wind speed** 0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable
Pedestrian Safety	**0.1% exceedance wind speed** 0-90 km/h = Safe

TABLE B1: SUMMARY OF PEDESTRIAN COMFORT (PROPOSED SCENARIO)

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
1	10.6	Standing	12.3	Standing	45.0	Safe
2	12.1	Standing	14.6	Standing	49.4	Safe
3	13.4	Standing	16.7	Walking	55.8	Safe
4	13.4	Standing	18.0	Walking	62.1	Safe
5	11.2	Standing	14.5	Standing	54.6	Safe
6	13.6	Standing	17.6	Walking	55.1	Safe
7	13.8	Standing	18.2	Walking	61.8	Safe
8	13.9	Standing	18.4	Walking	67.8	Safe
9	12.2	Standing	15.0	Standing	57.6	Safe
10	11.8	Standing	14.8	Standing	54.9	Safe
11	10.6	Standing	12.9	Standing	51.9	Safe
12	10.1	Standing	12.4	Standing	51.9	Safe
13	11.7	Standing	14.2	Standing	55.0	Safe
14	10.5	Standing	13.1	Standing	50.0	Safe
15	12.4	Standing	15.0	Standing	59.1	Safe
16	14.1	Standing	16.3	Walking	61.4	Safe
17	13.1	Standing	16.3	Walking	55.7	Safe
18	13.3	Standing	16.3	Walking	55.2	Safe
19	12.5	Standing	15.3	Walking	48.9	Safe
20	11.1	Standing	13.9	Standing	46.8	Safe
21	9.4	Sitting	13.0	Standing	54.0	Safe
22	10.4	Standing	13.7	Standing	50.3	Safe
23	9.6	Sitting	12.2	Standing	44.9	Safe
24	11.0	Standing	13.0	Standing	45.0	Safe
25	9.2	Sitting	11.8	Standing	53.3	Safe
26	9.3	Sitting	10.5	Standing	40.4	Safe
27	7.4	Sitting	8.2	Sitting	36.1	Safe
28	9.8	Sitting	11.0	Standing	40.1	Safe
29	13.4	Standing	15.6	Walking	62.5	Safe
30	13.3	Standing	16.3	Walking	64.0	Safe
31	13.5	Standing	18.5	Walking	66.4	Safe
32	14.5	Standing	19.4	Walking	64.1	Safe
33	9.6	Sitting	12.5	Standing	62.8	Safe
34	8.3	Sitting	10.2	Standing	43.3	Safe
35	8.9	Sitting	10.2	Standing	41.2	Safe

Guidelines	
Pedestrian Comfort	**20% exceedance wind speed** 0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable
Pedestrian Safety	**0.1% exceedance wind speed** 0-90 km/h = Safe

TABLE B2: SUMMARY OF PEDESTRIAN COMFORT (PROPOSED SCENARIO)

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
36	15.0	Standing	16.7	Walking	65.0	Safe
37	15.6	Walking	17.7	Walking	66.1	Safe
38	11.3	Standing	13.9	Standing	55.6	Safe
39	13.4	Standing	17.6	Walking	62.4	Safe
40	8.1	Sitting	10.2	Standing	56.2	Safe
41	9.9	Sitting	14.0	Standing	61.7	Safe
42	7.6	Sitting	9.7	Sitting	39.7	Safe
43	7.8	Sitting	10.1	Standing	42.2	Safe
44	7.1	Sitting	9.6	Sitting	43.7	Safe
45	7.6	Sitting	9.9	Sitting	47.2	Safe
46	9.0	Sitting	11.4	Standing	48.4	Safe
47	8.6	Sitting	11.2	Standing	48.3	Safe
48	7.4	Sitting	9.8	Sitting	40.7	Safe
49	8.4	Sitting	10.8	Standing	45.4	Safe
50	10.0	Sitting	12.9	Standing	51.0	Safe
51	7.5	Sitting	9.6	Sitting	46.5	Safe
52	10.0	Sitting	13.0	Standing	50.7	Safe
53	13.1	Standing	15.3	Walking	64.6	Safe
54	9.2	Sitting	11.9	Standing	47.9	Safe
55	11.0	Standing	12.5	Standing	51.0	Safe
56	10.8	Standing	14.4	Standing	60.8	Safe
57	7.6	Sitting	9.4	Sitting	56.0	Safe
58	6.9	Sitting	8.7	Sitting	40.5	Safe
59	6.2	Sitting	7.7	Sitting	28.8	Safe
60	8.3	Sitting	9.6	Sitting	35.7	Safe
61	10.5	Standing	11.4	Standing	43.4	Safe
62	11.3	Standing	11.8	Standing	46.1	Safe
63	11.7	Standing	13.6	Standing	65.8	Safe
64	12.9	Standing	16.0	Walking	62.9	Safe
65	7.0	Sitting	9.0	Sitting	47.5	Safe
66	7.7	Sitting	9.9	Sitting	50.7	Safe
67	8.1	Sitting	10.2	Standing	40.6	Safe
68	12.6	Standing	17.6	Walking	69.4	Safe
69	9.2	Sitting	11.9	Standing	57.4	Safe
70	9.0	Sitting	11.0	Standing	51.2	Safe

Guidelines	
Pedestrian Comfort	**20% exceedance wind speed** 0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable
Pedestrian Safety	**0.1% exceedance wind speed** 0-90 km/h = Safe

TABLE B3: SUMMARY OF PEDESTRIAN COMFORT (PROPOSED SCENARIO)

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
71	10.0	Sitting	11.6	Standing	45.3	Safe
72	8.5	Sitting	10.9	Standing	50.4	Safe
73	7.5	Sitting	9.8	Sitting	50.9	Safe
74	7.6	Sitting	10.3	Standing	54.8	Safe

APPENDIX C

WIND TUNNEL SIMULATION OF THE NATURAL WIND

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WIND TUNNEL SIMULATION OF THE NATURAL WIND

Wind flowing over the surface of the earth develops a boundary layer due to the drag produced by surface features such as vegetation and man-made structures. Within this boundary layer, the mean wind speed varies from zero at the surface to the gradient wind speed at the top of the layer. The height of the top of the boundary layer is referred to as the gradient height, above which the velocity remains more-or-less constant for a given synoptic weather system. The mean wind speed is taken to be the average value over one hour. Superimposed on the mean wind speed are fluctuating (or turbulent) components in the longitudinal (i.e. along wind), vertical and lateral directions. Although turbulence varies according to the roughness of the surface, the turbulence level generally increases from nearly zero (smooth flow) at gradient height to maximum values near the ground. While for a calm ocean the maximum could be 20%, the maximum for a very rough surface such as the center of a city could be 100%, or equal to the local mean wind speed. The height of the boundary layer varies in time and over different terrain roughness within the range of 400 metres (m) to 600 m.

Simulating real wind behaviour in a wind tunnel requires simulating the variation of mean wind speed with height, simulating the turbulence intensity, and matching the typical length scales of turbulence. It is the ratio between wind tunnel turbulence length scales and turbulence scales in the atmosphere that determines the geometric scales that models can assume in a wind tunnel. Hence, when a 1:200 scale model is quoted, this implies that the turbulence scales in the wind tunnel and the atmosphere have the same ratios. Some flexibility in this requirement has been shown to produce reasonable wind tunnel predictions compared to full scale. In model scale the mean and turbulence characteristics of the wind are obtained with the use of spires at one end of the tunnel and roughness elements along the floor of the tunnel. The fan is located at the model end and wind is pulled over the spires, roughness elements and model. It has been found that, to a good approximation, the mean wind profile can be represented by a power law relation, shown below, giving height above ground versus wind speed.

$$U = U_g \left(\frac{Z}{Z_g} \right)^{\alpha}$$

Where; ***U*** = mean wind speed, U_g = gradient wind speed, ***Z*** = height above ground, Z_g = depth of the boundary layer (gradient height) and α is the power law exponent.

Figure B1 on the following page plots three velocity profiles for open country, and suburban and urban exposures.

The exponent α varies according to the type of upwind terrain; α ranges from 0.14 for open country to 0.33 for an urban exposure. Figure C2 illustrates the theoretical variation of turbulence for open country, suburban and urban exposures.

The integral length scale of turbulence can be thought of as an average size of gust in the atmosphere. Although it varies with height and ground roughness, it has been found to generally be in the range of 100 m to 200 m in the upper half of the boundary layer. Thus, for a 1:300 scale, the model value should be between 1/3 and 2/3 of a metre. Integral length scales are derived from power spectra, which describe the energy content of wind as a function of frequency. There are several ways of determining integral length scales of turbulence. One way is by comparison of a measured power spectrum in model scale to a non-dimensional theoretical spectrum such as the Davenport spectrum of longitudinal turbulence. Using the Davenport spectrum, which agrees well with full-scale spectra, one can estimate the integral scale by plotting the theoretical spectrum with varying L until it matches as closely as possible the measured spectrum:

$$f \times S(f) = \frac{\frac{4(Lf)^2}{U_{10}{}^2}}{\left[1 + \frac{4(Lf)^2}{U_{10}{}^2}\right]^{\frac{4}{3}}}$$

Where, f is frequency, S(f) is the spectrum value at frequency f, U10 is the wind speed 10 m above ground level, and L is the characteristic length of turbulence.

Once the wind simulation is correct, the model, constructed to a suitable scale, is installed at the center of the working section of the wind tunnel. Different wind directions are represented by rotating the model to align with the wind tunnel center-line axis.

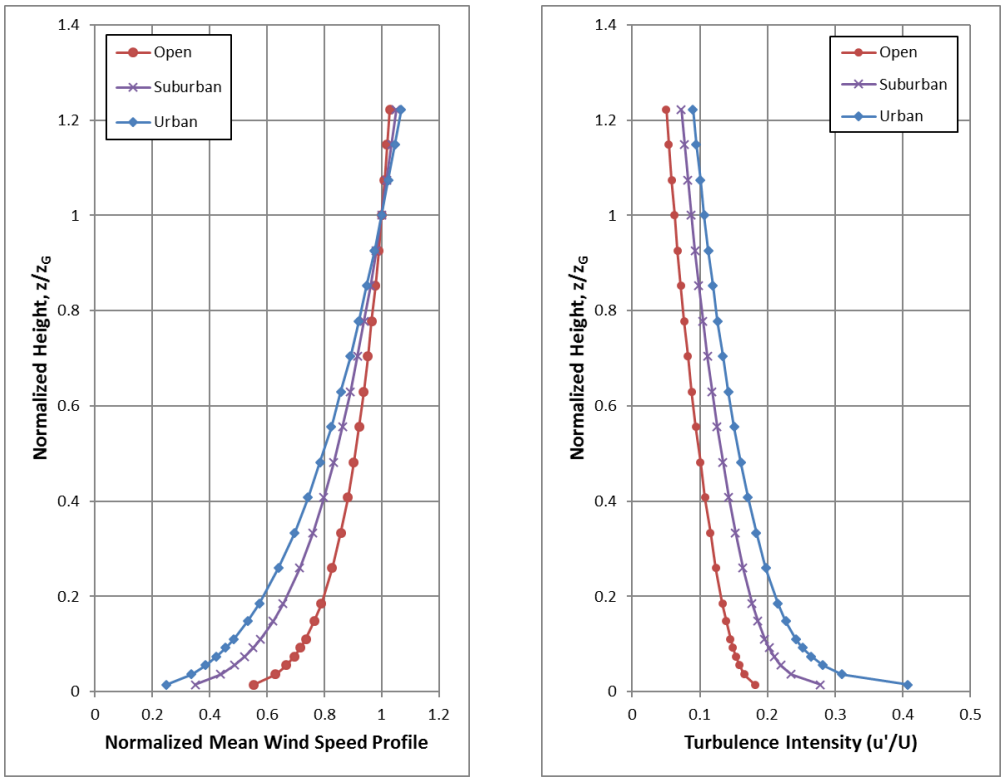

FIGURE C1 (LEFT): MEAN WIND SPEED PROFILES;
FIGURE C2 (RIGHT): TURBULENCE INTENSITY PROFILES

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APPENDIX D

PEDESTRIAN LEVEL WIND MEASUREMENT METHODOLOGY

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PEDESTRIAN LEVEL WIND MEASUREMENT METHODOLOGY

Pedestrian level wind studies are performed in a wind tunnel on a physical model of the study buildings at a suitable scale. Instantaneous wind speed measurements are recorded at a model height corresponding to 1.5 m full scale using either a hot wire anemometer or a pressure-based transducer. Measurements are performed at any number of locations on the model and usually for 36 wind directions. For each wind direction, the roughness of the upwind terrain is matched in the wind tunnel to generate the correct mean and turbulent wind profiles approaching the model.

The hot wire anemometer is an instrument consisting of a thin metallic wire conducting an electric current. It is an omni-directional device equally sensitive to wind approaching from any direction in the horizontal plane. By compensating for the cooling effect of wind flowing over the wire, the associated electronics produce an analog voltage signal that can be calibrated against velocity of the air stream. For all measurements, the wire is oriented vertically so as to be sensitive to wind approaching from all directions in a horizontal plane.

The pressure sensor is a small cylindrical device that measures instantaneous pressure differences over a small area. The sensor is connected via tubing to a transducer that translates the pressure to a voltage signal that is recorded by computer. With appropriately designed tubing, the sensor is sensitive to a suitable range of fluctuating velocities.

For a given wind direction and location on the model, a time history of the wind speed is recorded for a period of time equal to one hour in full-scale. The analog signal produced by the hot wire or pressure sensor is digitized at a rate of 400 samples per second. A sample recording for several seconds is illustrated in Figure D1. This data is analyzed to extract the mean, root-mean-square (rms) and the peak of the signal. The peak value, or gust wind speed, is formed by averaging a number of peaks obtained from sub-intervals of the sampling period. The mean and gust speeds are then normalized by the wind tunnel gradient wind speed, which is the speed at the top of the model boundary layer, to obtain mean and gust ratios. At each location, the measurements are repeated for 36 wind directions to produce normalized polar plots, which will be provided upon request.

In order to determine the duration of various wind speeds at full scale for a given measurement location the gust ratios are combined with a statistical (mathematical) model of the wind climate for the project site. This mathematical model is based on hourly wind data obtained from one or more meteorological stations (usually airports) close to the project location. The probability model used to represent the data is the Weibull distribution expressed as:

$$P\left(>U_g\right) = A_\theta \bullet \exp\left[\left(-\frac{U_g}{C_\theta}\right)^{K\theta}\right]$$

Where,

P (> U_g) is the probability, fraction of time, that the gradient wind speed ***U_g*** is exceeded; ***θ*** is the wind direction measured clockwise from true north, ***A***, ***C***, ***K*** are the Weibull coefficients, (Units: A - dimensionless, C - wind speed units [km/h] for instance, K - dimensionless). ***A_θ*** is the fraction of time wind blows from a 10° sector centered on ***θ***.

Analysis of the hourly wind data recorded for a length of time, on the order of 10 to 30 years, yields the ***A_θ***, ***C_θ*** and ***K_θ*** values. The probability of exceeding a chosen wind speed level, say 20 km/h, at sensor *N* is given by the following expression:

$$P_N(>20) = \Sigma_\theta P\left[\frac{(>20)}{\left(\frac{U_N}{U_g}\right)}\right]$$

P_N (> 20) = Σ_θ P { > 20/(U_N/Ug) }

Where, ***U_N/U_g*** is the gust velocity ratios, where the summation is taken over all 36 wind directions at 10° intervals.

If there are significant seasonal variations in the weather data, as determined by inspection of the C_θ and K_θ values, then the analysis is performed separately for two or more times corresponding to the groupings of seasonal wind data. Wind speed levels of interest for predicting pedestrian comfort are based on the comfort guidelines chosen to represent various pedestrian activity levels as discussed in the main text.

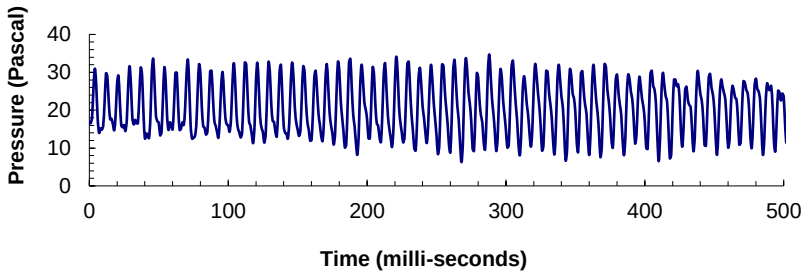

FIGURE D1: TIME VERSUS VELOCITY TRACE FOR A TYPICAL WIND SENSOR

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