# SERVICING AND STORMWATER MANAGEMENT REPORT

Prepared for: Miss BJL Corp.

9-Storey Mixed-Use Residential Building

21-51 Queen Street North Mississauga, Ontario L5N 1A2

SITEPLANTECH INC.

July 20, 2023 Project No.: 21-003



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	Submission History											
Submission	Date	<b>Issued For</b>	Issued To									
1	Dec. 6, 2021	RZA	City of Mississauga									
2	2 July 20, 2023		City of Mississauga									



## 1.0 INTRODUCTION

All *italicized* information listed below and all referenced documents are found in **Appendix A**.

## 1.1 Purpose

SITEPLANTECH was retained by Miss BJL Corp. to prepare a Servicing and Stormwater Management Report, in support of a Site Plan Application, to investigate water supply, sanitary sewerage and storm drainage for a proposed development located at 21-51 Queen Street North in Mississauga.

The purpose of this report is to provide site specific information for the municipality's review with respect to the adequacy of the existing infrastructure to support the proposed development.

## 1.2 Background Information

The following documents were requested and made available to SITEPLANTECH for our review and forms the basis of this report:

- Waldemar Golinski, KRCMAR (2017, December 13), Plan of Survey Showing Topographical Information (17-245BT01). [Technical drawing].
- Authors unknown, A& Architects Inc. (2023, June 19), 21-51 Queen St. N., Mississauga (A-002, A-003, A-102, A-151, A-209). [Technical digital drawings].
- Development Requirements Manual, City of Mississauga, dated January 2020.
- Public Works Design, Specifications & Procedures Manual, Region of Peel, Linear Infrastructure. Modified March 2017.
- Credit Valley Conservation (CVC) Stormwater Management Criteria, Dated august 2012.
- D. Marchese (1994, June 16), Mississauga Road Britannia Rd to Erin Mills Pkwy (C-29203). [Technical drawing].

## 1.3 Site Description

The subject site is approximately 9,676 square metres (0.97 hectares) and is currently occupied by a single storey multi-tenant retail building. The site is bounded by:

- An existing religious institution to the north;
- Existing low-density detached homes to the east;
- A commercial plaza to the south; and,
- Queen Street North to the west.



## **1.4 Proposed Development**

The proposed development will consist of a 9-storey mixed use residential building with ground floor retail fronting on Queen Street North. The mixed-use building will include approximately 1,424 m<sup>2</sup> of commercial space and a mix of studios, one-, two- and three-bedroom suites yielding 444 units. Access to the 2-level underground parking ramp and loading area will be provided from Queen Street North along the northern property line. Please refer to **Plan A-002** and **A-102** in for additional information.

#### **1.5 Easements and Land Conveyances**

The following easements are registered on title:

- Servicing easement as per instruments ST4623 and ST4624. This is easement is parallel to the western property line and provides sanitary, storm and water services between Matlock Avenue and Britannia Road West.
- Servicing easement as per instruments R01096667. This is easement is parallel to the southern property line and has a storm sewer connecting Queen Street North to the storm sewer in the easement described above.

No new easements will be required in order develop this property, nor has the City requested any land conveyances.



## 2.0 SERVICING TERMS OF REFERENCE AND METHODOLOGY

## 2.1 Terms of Reference

This report was prepared in accordance with the City of Mississauga's Development Requirements Manual, the Credit Valley Stormwater Management Criteria and the Region of Peel's Specifications & Procedures Manual.

## 2.2 Methodology: Stormwater Management

The modified rational method will be used to calculate runoff rates and target release rates from the site based on Intensity-Duration-Frequency (IDF) rainfall curves from the City of Mississauga Development Requirements. We will provide a detailed account of the pre- and postdevelopment conditions and demonstrate how the proposed development will meet the design requirements. The requirements for developments located within the CVC's Credit River subwatershed (Norval to Port Credit) are summarized as follows:

- Erosion: The minimum on-site runoff detention of 5mm is required;
- Water quality: Long-term average of 80% TSS removal is required; and,
- Water quantity: No control required for all storms.

Detailed servicing and grading plans were prepared based on the recommendations of this report and are included in **Appendix E**.

## 2.3 Methodology: Sanitary Drainage

The sanitary sewage discharge from the site will be determined using sanitary sewer design sheets that consider the land use and building statistics as supplied by the design team. The calculated values provide peak sanitary flow discharge that considers infiltration.

The existing and proposed sanitary flows will be calculated based on the Region's criteria shown in **Table 1** below, based on a population density found in the Region of Peel's 202 DC Background Study:

	Table 1. Sanitary now Design Criteria										
Use	Population	Flow									
Studio / 1-bdrm (<750 ft <sup>2</sup> )	1.6	302.8 L/c/d									
2-bdrm (<750 ft <sup>2</sup> )	1.6	302.8 L/c/d									
2-bdrm (>750 ft <sup>2</sup> )	3.0	302.8 L/c/d									
3-bdrm (>750 ft <sup>2</sup> )	3.0	302.8 L/c/d									
Commercial	50 p/Ha	302.8 L/c/d									

#### Table 1: Sanitary Flow Design Criteria



The existing and proposed site generated flows will be compared, and recommendations will be made to address capacity issues identified, if applicable.

## 2.4 Methodology: Water Supply

The existing and proposed domestic water demands from the site will be determined in accordance with the Region's criteria as per **Table 2** below:

Use	Flow	Max Day Factor	Peak Hour Factor
Residential	280 L/c/d	2.0	3.0
Commercial	300 L/c/d	1.4	3.0

Table 2	2: Water	Demand	Criteria
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The development will be fully sprinklered in accordance with OBC and NFPA 13 requirements.

Pressure and flow testing was conducted at hydrants on Queen Street North. Fire suppression calculations, in accordance with the Fire Underwriters Survey (FUS) Guidelines, will be undertaken to determine the minimum flow required at 140 KPa for fire protection, the results of which will be compared to the hydrant flow test to confirm adequate supply.



## 3.0 STORMWATER MANAGEMENT

All calculations and figures pertaining to the information summarized in the following sections are found in **Appendix B** unless otherwise noted.

## 3.1 Existing Drainage System

The site is bound by a 525mm concrete storm sewer located on the west side of Queen Street North which drains south then east through an easement (instruments R01096667) and ultimately connects to the 825mm storm sewer located near the centreline of the easement (instruments ST4623 and ST4624), along the east side of the property, which drains south to Britannia Drive and ultimately outlets directly to the Credit River.

Surface drainage from the site is conveyed to private storm infrastructure that connects to the 525mm storm sewer within the southern easement. Refer to **Figure 201** for details.

## 3.2 Existing Runoff

The pre-development runoff conditions were calculated based on the City's criteria and will be used to determine run-off conditions. The pre-development runoff from the site is summarized in **Table 3** below:

Return Period	Drainage Area (Ha)	Runoff C	Q (L/s)								
2-Year	0.968	0.90	144.9								
5-Year	0.968	0.90	194.8								
10-Year	0.968	0.90	240.0								
100-Year	0.968	0.90	340.5								

Table 3: Pre-Development Runoff

## 3.3 Allowable Release Rate

As noted in **Section 2.2** above, quantity controls are not required for sites being developed within the Credit River sub-watershed (Norval to Port Credit). It is noted however that storm sewer capacity constraints may govern, stormwater management will be designed such that post-development flows do not exceed pre-development flows noted in **Section 3.2**.

## 3.4 Quantity Control

As per the requirements for developments located within the CVC's Credit River sub-watershed (Norval to Port Credit) water quantity controls are not required. Run-off from the site will be capture by surface area drains and the storm sewer connection (refer to **Section 3.9**) will be sized to convey the 10-year flow.



## 3.5 Quality Control

As per CVC's requirements quality controls must achieve a minimum of 80% total suspended solids (TSS) removal. The development will consist of green roofs, rooftop/terraces, perimeter landscaped and asphalt surfaces each having an effective removal rate as outlined in **Table 4** below:

Surface Type	Effective
	Removal Rate
Asphalt	0%
Roof	95%
Green roof/Landscape	100%

Based on the Effective TSS removal calculations, the proposed development will achieve a net TSS pre-treatment removal of 70%, therefore it is proposed to treat run-off from the asphalted areas with a filtration system (Upflo UFF-3). This runoff will be treated by the filtration system prior to entering the water balance component of the SWM chamber.

The proposed filtration system has documented evidence that it can achieve a TSS removal rate of 81% from the treated area (refer to NJDEP certification included). Based on this removal rate and our calculations, the proposed treatment train approach combined with the filtration system will achieve an overall net TSS removal of 80%. Refer to **Plan 101** for details.

## 3.6 Erosion Control

Based on the site area of 0.97 hectare, the required on-site water retention volume is 48.4m<sup>3</sup>. An initial abstraction of 1mm and 5mm from the roof ballast and the green roofs respectively, will provide a volume reduction of 16.9m<sup>3</sup>. Therefore, a net water balance volume of 31.2m<sup>3</sup> will be needed to meet CVC's requirements. Due to various site constraints, meeting the water balance criteria will require a multi-faceted approach. The following options were considered:

## <u>Infiltration:</u>

Since the proposed footprint of the building is such that the foundations are less than 4.0m from the property limits, infiltration is not recommended and thus was not considered.

## Green roof and Landscape Irrigation:

Approximately 23.5m<sup>3</sup> of the water balance volume will be used for the proposed green-roof irrigation within a period of 72 hours as per the water irrigation report prepared by Next Level included in **Appendix B**.



#### <u>Gray water re-use:</u>

In addition to the proposed green roof irrigation, a rainwater harvesting system will be implemented for use as grey-water within the building. A portion of the roof water from the stormwater management tank water balance bay will be directed to the grey-water system, the details of which will be provided by the mechanical consultant at the building permit stage. In order to achieve the Erosion Control target, a total of 7,700L (7.7m<sup>3</sup>) will need to be re-used as part of a gray-water system within a period of 72 hours.

The required 31.2m<sup>3</sup> water balance volume will be provided as a separate compartment within the stormwater chamber. **Plan 101** for details. Details of the pumping and rainwater re-use system will be provided by the mechanical consultant as part of the building permit application.

## 3.7 100-Year Capture

As noted in **Section 3.4** stormwater controls are not required and thus 100-year capture points do not need to be designed provided that overland flow is directed away from the proposed building towards the municipal right-of-way.

We note however that there are proposed private patios along the southern and eastern façade as well as area drains within the main access. To ensure that the 100-year flow is captured from the sunken patios, area drains within the private patios and the drive aisles were modelled as horizontal orifice plates assuming a 50% blockage. A summary of the design flows and inlet capacity is summarized in **Table 5** below:

Drainage ID	Drain Type	Area (m <sup>2</sup> )	100-Year Flow (L/s)	Max Head (m)	Inlet Q (L/s)		
AD (Patio)	Z611	30	1.3	0.05	5.2		
AD (Driveway)			10.0	0.15	35.4		

 Table 5: 100-Year Capture Points

The area drain specified in the above table (or approved equal) will capture the 100-year flow adequately when 50% blockage has occurred.

The 100-year capture from the roof areas will be performed by uncontrolled roof drains outleting to the SWM chamber.



## 3.8 Proposed Drainage System

It is proposed to connect the building's storm outlet to the existing infrastructure located within the easement east of the site. The development will connect to the existing 825mm concrete storm sewer via a 375mm diameter storm sewer service connection with a grade of 3.0%, designed to convey the captured 10-year storm. Since the proposed service connection is less than half the diameter of the main sewer, connection at the main will be made with a riser as per the Region of Peel Standard 2-4-3. Refer to **Drawing 002** and **101** found in **Appendix E** for the details related to the service connection.



## 4.0 SANITARY DRAINAGE

All calculations pertaining to the information summarized in the following sections are found in **Appendix C** unless otherwise noted.

## 4.1 Existing Sanitary Drainage System

There is an existing 450mm concrete sanitary sewer located within the easement on the east side of the site and a 250mm PVC sanitary sewer along the frontage of the site on Queen Street North. Both sewers drain south to Britannia Drive.

## 4.2 Existing Sanitary Flows

Based on the Region of Peel criteria outlined in **Section 2.3**, the site contributes a peak sanitary flow of approximately 1.0L/s to the local infrastructure. It is noted however, based on a population per hectare equivalent of less then 1,000 persons as per Peel Region Standards 2-9-2, that the site is estimated to contribute 13.3L/s to the local infrastructure. Given the current land use, the calculated flow of 1.0 L/s is a more appropriate assessment of existing conditions.

## 4.3 **Proposed Sanitary Flows**

The sanitary discharge flows from the site were calculated based on the Region of Peel criteria outlined in **Section 2.3**, the proposed building and site information. A total peak design flow of 10.3 L/s was calculated for the subject property.

## 4.4 Proposed Sanitary Connection

The sanitary effluent from the above-grade portion of the development will discharge by gravity, while all sanitary flows from below grade portion of the development (i.e. parking garage) will be pumped to the outlet.

All sanitary flow from the proposed development will outlet into the existing 450mm concrete sanitary sewer in the easement east of the site. A 200mm sanitary sewer service connection with a grade of 2.0% will be adequate to convey the calculated design flow of 10.3 L/s. Since the proposed service connection is less than half the diameter of the main sewer, connection at the main will be made with a riser as per Region of Peel standard 2-4-3. Refer to **Drawing 002** and **101** found in **Appendix E** for the details related to the service connection.



## 5.0 WATER SUPPLY

All calculations pertaining to the information summarized in the following sections are found in **Appendix D**.

## 5.1 Existing System

An existing 200 mm diameter watermain is located within the easement located on the east side of the side and a 300mm diameter watermain is located on Queen Street North along the frontage of the site.

It is currently unknown where the existing building is serviced from as no visible/surveyed water valves were noted on site.

A hydrant flow tests was carried out within the vicinity of the site to determine flow and pressure conditions for each existing watermains. The tests were carried out by LHS Inc. on May 12, 2021. The test results indicate the watermain is operating at a static pressure of approximately 365 KPa (53 PSI), and that the available flow at 140 KPa (20 PSI) is approximately 14,200L/min (3750 USPGM).

## 5.2 Existing Water Demands

The existing water consumption was calculated as per the criteria outlined in **Section 2.4** above. Based on the gross floor area, the existing development requires an estimated average of 14,600 L/d (0.17L/s) from the municipal infrastructure.

## 5.3 **Proposed Water Supply Requirements**

The estimated water consumption was calculated as per the criteria outlined in **Section 2.4** above. The proposed average day domestic water consumption rate is estimated to be 2.3 L/s (maximum day demand of approximately 405,200L/d).

Water Supply for Public Fire Protection calculations, as provided by the Fire Underwriters Survey (FUS), were undertaken to determine the minimum requirement to provide adequate fire suppression. According to our calculations, a minimum fire suppression flow of approximately 9,900 L/min (2,600 USGPM) at a pressure of 140 KPa (20 PSI) will be required for the subject development. The Max Day + Fire Flow rate of approximately 10,300 L/min (2,690 USGPM) is available at a pressure which exceeds the minimum FUS requirements.

The municipal water system therefore has adequate flow and pressure to satisfy the water demands of the proposed development.



## 5.4 Proposed Water Connection

As the height of the proposed building does not exceed 84.0m, the development may be serviced by a single fire supply. Therefore the proposed building will be serviced with a combined fire and domestic water connection in accordance with the Region of Peel standard 1-8-3.

It is proposed to connect the 200 mm water service to the existing 300 mm diameter watermain at Queen Street North with a 300 mm X 200 mm tapping sleeve and valve. The 200 mm fire service line will be equipped with a detector check valve and the 150 mm domestic service with a meter and backflow preventor.

Refer to **Drawing 101** found in **Appendix E** for additional details.



## 6.0 SITE GRADING

All plans and figures pertaining to the information summarized in the following sections are found in **Appendix E** unless otherwise noted.

## 6.1 Existing Grades

The site consists of asphalt surfaces and by roofs from an existing commercial building which appears to be connected to the municipal storm infrastructure leading to the easement (refer to **Section 3.1** above). Generally, drainage is capture by private storm sewer infrastructure that drain to the storm sewer infrastructure located in the south easement draining to the east easement. The topography of the surrounding areas suggests that the lots from the east drain towards a non-defined swale along the east easement while a portion of the southern property drains to local catchbasins located along the southern property line.

Generally, the site is graded below the existing Queen Street North Centreline and tends to slope towards the east easement and has an approximate 1.5m grade difference from high to low point.

## 6.2 Proposed Grades

A review of the perimeter site grades suggests that the first-floor elevation of the residential lobby and retail is proposed to be set at 166.60 while the finished floor elevation for the townhouse units along the south and east side of the proposed building will be at 164.60. The underground parking garage ramp high point will be set at 166.15 to ensure overland flow is directed to Queen Street North. The proposed finished floor elevations and grading of the site perimeter will be compatible with the adjacent developments. Please refer to **Drawing 401** for additional information.

Existing catchbasins along the southern property line, picking drainage from the commercial development to the south, will be relocated to maintain existing drainage from the commercial property and ensure existing drainage patterns are maintained. In addition, rear-lot catchbasins will be constructed along the east side of the easement to ensure the rear yards of the existing residential lots are adequately drained.

Boulevard grades are designed to produce moderate grades in the range of 2.0% to 3.0% throughout the site frontages and existing grades will be met at the edge of pavement as the existing sidewalks will be replaced as per the landscaping plan.

The development of this site and will not adversely impact adjacent lands.



## 7.0 EROSION AND SEDIMENT CONTROL

In accordance with the City requirements (Section 6.01.08) for sites less than 1.0 hectare located more than 30m from a watercourse, an ESC permit will not be required.

To ensure stormwater runoff during the construction phase does not transport sediment to the existing municipal infrastructure, temporary catch basin sediment control devices are proposed on Queen Street North and all capture points within the adjacent easements. In addition, a temporary sediment control fence will be erected around the site perimeter and a temporary construction access (mud mat) will be built at the construction entrance on Queen Street North.

These measures will be designed and constructed in accordance with the "Erosion and Sediment Control Guideline for Urban Construction" document (December 2006). These measures, as well as any additional information pertaining to ESC Controls, are detailed on **Drawing 601** found in **Appendix E**. All reasonable measures will be taken to ensure sediment loading to the adjacent properties and municipal right-of-way is minimized both during and following construction.



## 8.0 CONCLUSIONS AND RECOMMENDATIONS

This report is to be read in conjunction with the application submission material for the project proposal known as 21-51 Queen Street North. We conclude and recommend the following:

## 8.1 STORMWATER MANAGEMENT

No quantity controls are required to develop this property.

Quality controls will be provided by a filtration system that will achieve 80% net total suspended solids removal.

A Volume of 31.2m<sup>3</sup> will be retained within the SWM chamber and will be reused as part of landscape irrigation and greywater re-use system, thereby meeting the CVC's erosion control requirements.

## 8.2 SANITARY DRAINAGE

The sanitary discharge from the proposed development will be directed to the infrastructure within the easement located along the east property limit.

## 8.3 WATER SUPPLY

According to the calculations and hydrant flow tests presented in this report, the existing municipal infrastructure is adequate to support the proposed development.

## 8.4 SITE GRADING

The proposed grading is compatible with existing elevations at the property limit, and will not adversely affect adjacent properties.

## 8.5 EROSION AND SEDIMENT CONTROL

ESC measures will be designed as per the "Erosion and Sediment Control Guideline for Urban Construction" document (December 2006). Provided that these measures are well maintained during construction, these will be adequate to keep sediments from entering the municipal infrastructure during construction.



Respectfully submitted,

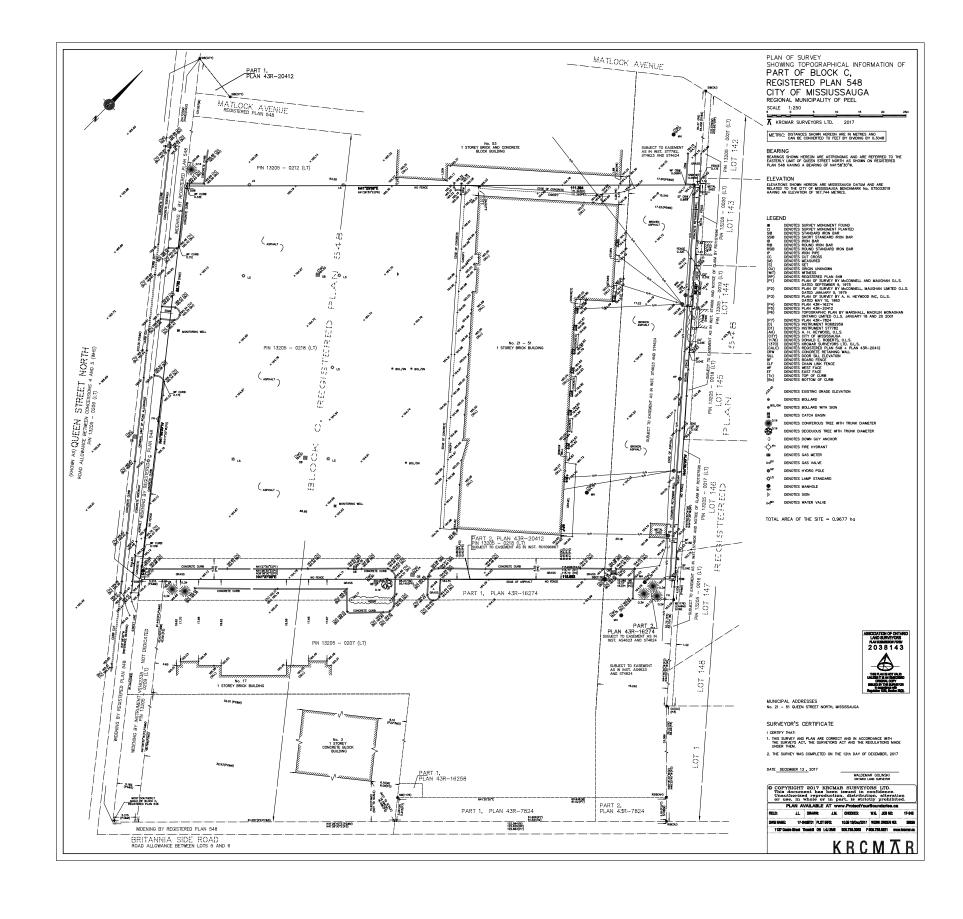
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Appendix A

**Background Information** 



SIT	E STATISTIC	CS INCLUDIN	IG EASEMENT	AREA
Area	Building Foot Print	TOTAL GFA	COVERAGE	FSI
9,676 m <sup>2</sup>	6,009 m <sup>2</sup>	28,238 m <sup>2</sup>	0.62	2.92

**GROSS FLOOR AREA (GFA) - APARTMENT ZONE** MEANS THE SUM OF THE AREAS OF EACH STOREY OF A BUILDING ABOVE OR BELOW ESTABLISHED GRADE, MEASURED FROM THE EXTERIOR OF OUTSIDE WALLS OF THE BUILDING INCLUDING FLOOR AREA OCCUPIED BY INTERIOR WALLS BUT EXCLUDING ANY PART OF THE BUILDING USED FOR MECHANICAL FLOOR AREA, STAIRWELLS, ELEVATORS, MOTOR VEHICLE PARKING, BICYCLE PARKING, STORAGE LOCKERS, BELOW-GRADE STORAGE, ANY ENCLOSED AREA USED FOR THE COLLECTION OR STORAGE OF DISPOSABLE OR RECYCLABLE WASTE GENERATED WITHIN THE BUILDING, COMMON FACILITIES FOR THE USE OF THE RESIDENTS OF THE BUILDING, A DAY CARE AND AMENITY AREA. \*AVERAGE GRADE= 165.55 + 165.05 /2 = 165.30

STATISTICS/TOTAL																		
		GCA (ABOVE	E GRADE)- TOTAL		DEDUCTION										GFA	GFA-TOTAL		
LEVEL	NUMBER OF REPEATED FLOOR	GCA	GCA sf	PARKING	STORAGE / BIKE	GARBAGE CHUTE	FI EVATOR	MECH PH		STAIR	GARBAGE LOADING	RESIDENTIAL GARBAGE LOADING	RETAIL GARBAGE	GARBAGE RETAIL	INDOOR AMENITY	TOTAL DEDUCTION	GFA	GFA sf
EVEL 1	1	5,648.6 m <sup>2</sup>	60,801.1 SF	247.2 m <sup>2</sup>	406.5 m <sup>2</sup>	0.3 m <sup>2</sup>	34.0 m <sup>2</sup>	0 m <sup>2</sup>	1.2 m <sup>2</sup>	63.0 m <sup>2</sup>	285.2 m <sup>2</sup>	216.1 m <sup>2</sup>	22.2 m <sup>2</sup>	138.6 m <sup>2</sup>	313.5 m <sup>2</sup>	1,727.6 m <sup>2</sup>	3,921 m <sup>2</sup>	42,205.4 SF
_EVEL 2	1	3,442.1 m <sup>2</sup>	37,050.7 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	25.3 m <sup>2</sup>	0 m <sup>2</sup>	359.4 m <sup>2</sup>	101.5 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	906.9 m <sup>2</sup>	1,393.6 m <sup>2</sup>	2,048.5 m <sup>2</sup>	22,049.8 SF
LEVEL 3	1	4,052.4 m <sup>2</sup>	43,619.9 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	11.8 m <sup>2</sup>	55.8 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	258.2 m <sup>2</sup>	349.2 m <sup>2</sup>	3,703.2 m <sup>2</sup>	39,861.4 SF
LEVEL 4	1	4,052.9 m <sup>2</sup>	43,624.5 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	11.8 m <sup>2</sup>	55.9 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0 m <sup>2</sup>	91 m²	3,961.8 m <sup>2</sup>	42,644.5 SF
LEVEL 5	1	3,171.9 m <sup>2</sup>	34,142.3 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	9.4 m <sup>2</sup>	53.1 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0 m <sup>2</sup>	85.8 m²	3,086.1 m <sup>2</sup>	33,218.3 SF
LEVEL 6	1	3,201.3 m <sup>2</sup>	34,458 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	9.4 m <sup>2</sup>	53.1 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0 m <sup>2</sup>	85.9 m²	3,115.4 m <sup>2</sup>	33,533.9 SF
LEVEL 7-8	2	5,883.4 m <sup>2</sup>	63,328.6 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	1.2 m <sup>2</sup>	45.5 m <sup>2</sup>	0 m <sup>2</sup>	18.8 m <sup>2</sup>	102.7 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0 m <sup>2</sup>	168.2 m <sup>2</sup>	5,715.2 m <sup>2</sup>	61,518 SF
LEVEL 9	1	2,772.8 m <sup>2</sup>	29,845.9 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	9.5 m <sup>2</sup>	53.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0 m <sup>2</sup>	85.9 m²	2,686.9 m <sup>2</sup>	28,921.7 SF
MPH	1	478 m <sup>2</sup>	5,145.6 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	32.5 m <sup>2</sup>	410.4 m <sup>2</sup>	0.0 m <sup>2</sup>	35.1 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0 m <sup>2</sup>	478 m²	0 m <sup>2</sup>	0 SF
		32,703.4 m <sup>2</sup>	352,016.7 SF	247.2 m <sup>2</sup>	406.5 m <sup>2</sup>	5.0 m <sup>2</sup>	251.0 m <sup>2</sup>	410.4 m <sup>2</sup>	431.3 m <sup>2</sup>	573.3 m <sup>2</sup>	285.2 m <sup>2</sup>	216.1 m <sup>2</sup>	22.2 m <sup>2</sup>	138.6 m <sup>2</sup>	1,478.6 m <sup>2</sup>	4,465.3 m <sup>2</sup>	28,238.2 m <sup>2</sup>	303,953 SF

								51A	TISTICS/ RESI	DENTIAL								
		GCA(ABO)	/E GRADE)- RES.							DEDUCTIO	N						GFA- RE	SIDENTIAL
	NUMBER OF											RESIDENTIAL	RETAIL GARBAGE	GARBAGE	INDOOR	TOTAL		
LEVEL	REPEATED FLOOR	GCA	GCA sf	PARKING	STORAGE / BIKE	GARBAGE CHUTE	ELEVATOR	MECH.PH	MECH./ELEC.	STAIR	GARBAGE LOADING	GARBAGE LOADING	LOADING	RETAIL	AMENITY	DEDUCTION	GFA	GFA sf
LEVEL 1	1	4,064.2 m <sup>2</sup>	43,747 SF	247.2 m <sup>2</sup>	406.5 m <sup>2</sup>	0.3 m <sup>2</sup>	34.0 m <sup>2</sup>	0 m²	1.2 m <sup>2</sup>	63.0 m <sup>2</sup>	285.2 m <sup>2</sup>	216.1 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	313.5 m <sup>2</sup>	1,566.8 m <sup>2</sup>	2,497.4 m <sup>2</sup>	26,881.7 SF
LEVEL 2	1	3,442.1 m <sup>2</sup>	37,050.7 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	25.3 m <sup>2</sup>	0 m²	359.4 m <sup>2</sup>	101.5 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	906.9 m <sup>2</sup>	1,393.6 m <sup>2</sup>	2,048.5 m <sup>2</sup>	22,049.8 SF
LEVEL 3	1	4,052.4 m <sup>2</sup>	43,619.9 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	11.8 m <sup>2</sup>	55.8 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	258.2 m <sup>2</sup>	349.2 m <sup>2</sup>	3,703.2 m <sup>2</sup>	39,861.4 SF
LEVEL 4	1	4,052.9 m <sup>2</sup>	43,624.5 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	11.8 m <sup>2</sup>	55.9 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	91 m²	3,961.8 m <sup>2</sup>	42,644.5 SF
LEVEL 5	1	3,171.9 m <sup>2</sup>	34,142.3 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	9.4 m <sup>2</sup>	53.1 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	85.8 m²	3,086.1 m <sup>2</sup>	33,218.3 SF
LEVEL 6	1	3,201.3 m <sup>2</sup>	34,458 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m <sup>2</sup>	9.4 m <sup>2</sup>	53.1 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	85.9 m²	3,115.4 m <sup>2</sup>	33,533.9 SF
LEVEL 7-8	2	5,883.4 m <sup>2</sup>	63,328.6 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	1.2 m <sup>2</sup>	45.5 m <sup>2</sup>	0 m <sup>2</sup>	18.8 m <sup>2</sup>	102.7 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	168.2 m <sup>2</sup>	5,715.2 m <sup>2</sup>	61,518 SF
LEVEL 9	1	2,772.8 m <sup>2</sup>	29,845.9 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.6 m <sup>2</sup>	22.8 m <sup>2</sup>	0 m²	9.5 m <sup>2</sup>	53.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	85.9 m²	2,686.9 m <sup>2</sup>	28,921.7 SF
MPH	1	478 m <sup>2</sup>	5,145.6 SF	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	32.5 m <sup>2</sup>	410.4 m <sup>2</sup>	0 m²	35.1 m²	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	478 m²	0 m <sup>2</sup>	0 SF
		31,119 m <sup>2</sup>	334,962.5 SF	247.2 m <sup>2</sup>	406.5 m <sup>2</sup>	5.0 m <sup>2</sup>	251.0 m <sup>2</sup>	410.4 m <sup>2</sup>	431.3 m <sup>2</sup>	573.3 m <sup>2</sup>	285.2 m <sup>2</sup>	216.1 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	1478.6 m <sup>2</sup>	4,304.5 m <sup>2</sup>	26,814.5 m <sup>2</sup>	288,629.3 SF

	STATISTICS/ RETAIL																	
GCA(ABOVE GRADE)- RETAIL DEDUCTION										GFA-	- RETAIL							
	NUMBER OF CENTIAL RETAIL GARBAGE GARBAGE INDOOR							TOTAL										
LEVEL	REPEATED FLOOR	GCA	GCA sf	PARKING	Area Storage/ Bike	GARBAGE CHUTE	ELEVATOR	MECH.PH	MECH./ELEC.	STAIR	GARBAGE LOADING	GARBAGE LOADING	LOADING	RETAIL	AMENITY	DEDUCTION	GFA	GFA sf
LEVEL 1	1	1,584.4 m²	17,054.2 SF	0.0 m²	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0.0 m <sup>2</sup>	0 m²	0 m²	0.0 m²	0 m <sup>2</sup>	0.0 m <sup>2</sup>	22.2 m <sup>2</sup>	138.6 m²	0.0 m <sup>2</sup>	160.8 m <sup>2</sup>	1,423.6 m <sup>2</sup>	15,323.7 SF
		1,584.4 m²	17,054.2 SF	0.0 m <sup>2</sup>	0.0 m²	0.0 m²	0.0 m <sup>2</sup>	0 m²	0 m²	0.0 m²	0 m²	0.0 m <sup>2</sup>	22.2 m <sup>2</sup>	138.6 m²	0.0 m²	160.8 m <sup>2</sup>	1,423.6 m <sup>2</sup>	15,323.7 SF

LOADING AREA	REQUIRED	REQUIRED	PROVIDED		GCA (BELOW GRADE	PARKING AF	REA)	REQUIRED PARKING (Zoning)					
RETAIL:	BETWEEN 2,350 sm UP TO 7,500 sm	2	N/A	Level	NUMBER OF REPEATED FLOOR	GCA	GCA sf	STUDIO (X 1) 1B- 175 236		2B+2BD (X 1.4) 109	· · · · ·		TOTAL 612.8
RETAIL:	BETWEEN 250 sm UP TO 2,350 sm	1	1	Not Placed	1	0 m²	0 SF						
				P2	1	7,240 m <sup>2</sup>	77,931 SF						
RESIDENTIAL APARTMENT MORE THAN 30 UNITS		1	1	P1	1	7,296.5 m <sup>2</sup>	78,539 SF	**RETAIL PARKING RE	QUIRED:	ACCESSIBLE	PARKING R	EQUIREM	IENT 4%
						14,536.5 m <sup>2</sup>	156,470 SF	4.3 SPACES PER 100sr		OF NON RESI			

RESIDENTIAL UNIT COUNT										
			RE	SIDENT	IAL UNIT	COUN	Т		ST	
LEVEL	NUMBER OF REPEATED FLOOR	STUDIO	1B	1BD	2B	2BD	3B	TOTAL UNIT	E 26.	
LEVEL 1	1	8	1	2	10	0	0	21		
LEVEL 2	1	20	0	1	10	0	0	31		
LEVEL 3	1	23	2	32	8	0	0	65		
LEVEL 4	1	27	2	33	9	0	0	71		
LEVEL 5	1	22	2	22	9	0	0	55		
LEVEL 6	1	20	2	24	9	0	0	55		
LEVEL 7-8	2	36	4	44	16	0	0	100		
LEVEL 9	1	19	1	17	5	2	2	46		
MPH	1	0	0	0	0	0	0	0		
L		175	14	175	76	2	2	444		

TUDIO\_ BF % 3.25

# ΙΛΤΟΤ /20ΙΤ2ΙΤΑΤ2

# STATISTICS/ RESIDENTIAL

# STATISTICS/ DETAIL

NOTE: 90% OF LOADING AREA HAS BEEN DEDUCTED FOR RESIDENTIAL GFA CALCULATION 10% OF LOADING AREA HAS BEEN DEDUCTED FOR RETAIL GFA CALCULATION

RE	QUIRED BF	UNITS 15	%		UNIT COUNT									
DIO_	1 B+ 1BD	2B+2BD_	3B_BF	STUDIO	1B	1BD	2B	2E	BD	3B	Т	OTAL I	JNIT	
= %	_BF%	BF %	%	175	14 ′	175	76	2	2	4	444			
5	28.35	11.7	0											
				*UNIT BREAKDOWN %										
				NUMBER	NUMBER OF UNITS STUDIO 1B 1 BD 2B 2BD 3B TOT							TOTAL	. %	
				444		39.4%	6 3.2	%	39.4%	17.1%	6 0.5%	0.5%	100.0	
						*UN	NIT BRE	AKDO	OWN C	OUNT%	6			
				NUMBER	R OF UNIT	S STU	DIO	1B+′	1BD	28	3+2BD+	+3B	TOTAL	. %
				444		39.49	% 42.	42.6%			18.0%			
							*AVERAGE UNIT							
				NUMBER	R OF UNIT	S SAI	SALEABLE AVERAGE UNITS AVERAGE UN			E UNIT S	SF			
				444		23,02	23 m²	52	2 m²		558	8 SF		

# MIN AMENITY AREA IS THE GR sm PER UNIT OR 10% OF THE

REQUIR	ED AMENITY							
NET UNITS	TC							
444	2,486.4							
TOTAL F	PROVIDED AI							
LEVEL	A							
LEVEL 1	313 m²							
LEVEL 2	907 m²							
LEVEL 3	1,098 m <sup>2</sup>							
LEVEL 3	258 m²							
Grand total	2,576 m²							

TOTAL OPEN TO BELOW AREA IS NOT							
	INCLUDED IN GCA						
LEVEL	Area						
LEVEL 2	2,229 m²						

TOTA	TOTAL PROPOSED PARKING (NOT INCLUD TANDEM)								
Level Count									
P2	189								
P1 169									
Grand total 358									

	PROVI	DED INTERIOR AMENITY						
	LEVEL	Area						
	LEVEL 1	313 m <sup>2</sup>						
GREATER OF 5.6 E SITE AREA	LEVEL 2	907 m²						
_	LEVEL 3	258 m <sup>2</sup>						
TY AREA	Grand total	1,479 m²						
FOTAL								
	INTERIOR AMENITY RATIO: TOTAL AREA / NUMBER							
	OF UNIS = 1,469 /444=3.3							
AMENITY	MIN EXTERIO	DR AMENITY 55 sm						
Area	PROVIE	DED EXTERIOR AMENITY						
	LEVEL	Area						
	LEVEL 3	1,098 m <sup>2</sup>						
	Grand total	1,098 m <sup>2</sup>						
		MENITY RATIO: TOTAL AREA / 098/444=2.47	NUMBER					



	RESIDENTIAL UNIT COUNT B.F								
			F	RESIDEN	TIAL UNI	T COUI	NT		
	NUMBER OF							TOTAL	
LEVEL	REPEATED FLOOR	STUDIO	1B	1BD	2B	2BD	3B	UNIT	
LEVEL 1	1	0	0	0	1	0	0	1	
LEVEL 2	1	3	0	0	0	0	0	3	
LEVEL 3	1	4	0	5	1	0	0	10	
LEVEL 4	1	4	0	5	1	0	0	10	
LEVEL 5	1	3	0	5	2	0	0	10	
LEVEL 6	1	3	0	5	2	0	0	10	
LEVEL 7-8	2	6	0	10	4	0	0	20	
LEVEL 9	1	4	0	0	1	0	2	7	
		27	0	30	12	0	2	71	

	SALEABLE AREA								
	NUMBER OF	SALEABLE (I	RESIDENTIAL)	SALEABLE	(RETAIL)				
/	REPEATED				RETAIL				
LEVEL	FLOOR	SALEABLE	SALEABLE sf	RETAIL LEASABLE	LEASABLE sf				
LEVEL 1	1	1,205.3 m <sup>2</sup>	12,973 SF	1,423.6 m <sup>2</sup>	15,324 SF				
LEVEL 2	1	1,416 m²	15,242 SF	0 m²	0 SF				
LEVEL 3	1	3,364.3 m <sup>2</sup>	36,213 SF	0 m <sup>2</sup>	0 SF				
LEVEL 4	1	3,622.9 m <sup>2</sup>	38,997 SF	0 m <sup>2</sup>	0 SF				
LEVEL 5	1	2,838.6 m <sup>2</sup>	30,554 SF	0 m <sup>2</sup>	0 SF				
LEVEL 6	1	2,867.9 m <sup>2</sup>	30,870 SF	0 m <sup>2</sup>	0 SF				
LEVEL 7-8	2	5,250 m²	56,510 SF	0 m <sup>2</sup>	0 SF				
LEVEL 9	1	2,458.4 m <sup>2</sup>	26,462 SF	0 m <sup>2</sup>	0 SF				
MPH	1	0 m <sup>2</sup>	0 SF	0 m <sup>2</sup>	0 SF				
		23,023.4 m <sup>2</sup>	247,822 SF	1,423.6 m <sup>2</sup>	15,324 SF				

# UNIT SIZE:

	SM	SF
STUDIO	29	313
	43	458
1B-1B+D	43	458
	63	681
2B-2B+D	61	661
	83	893
3B	87	941
	94	1,013

*GARBAGE	GARBAGE ROOM	REQUIRED sm	PROVIDED sm
	RESIDENTIAL	127.5	188.31
	RETAIL		138.58
	BULKROOM	10	41
	STAGING	44.4	55.85
	TOTAL (SM)	181.9	423.74

TOTAL RETAIL GARBAGE			
LEVEL	RETAIL GARBAGE		
LEVEL 1	138.58 m <sup>2</sup>		
138.58 m <sup>2</sup>			
TC	TAL GARBAGE AREA		
TC LEVEL	TAL GARBAGE AREA GARBAGE AREA		
LEVEL	GARBAGE AREA		

GARBAGE ROOM: MIN. 25 sm FOR THE FIRST 50 UNITS AND 13 sm FOR ADDITIONAL 50 STAGING: 5 sm FOR EVERY 50 UNITS

GARBAGE (1/50) RECYCLE (1/50) ORGANIC (1/100)

\* MIN. CLEAR HEIGHT FOR LOADING = 7.5m

REQUIRED RESIDENTIAL BIKE			
RESIDENTIAL LONG-TERM(X0.6)	RESIDENTIAL SHORT-TERM (X0.15)	TOTAL	
266.4	67	333	

PROVIDED RESIDENTIAL SHORT-TERM BIKE			
LEVEL	TYPE	COUNT	
Level 1	<varies></varies>	48	
		48	

PROVIDED RESIDENTIAL LONG-TERM BIKE				
LEVEL	TYPE	COUNT		
Level 1	RES. 1525X450 STACK BIKE	274		
Level 1	RES. 1700X450 STACK BIKE	52		
		326		

PROVIDED TOTAL RESIDENTIAL SHORT/LONG-TERM BIKE			
LEVEL	EL TYPE COUN		
Level 1	RES. 1525X450 STACK BIKE	274	
Level 1	RES. 1700X450 STACK BIKE	52	
Level 1	VIS. 1525X450 STACK BIKE	28	
Level 1	VIS. 1700X450 STACK BIKE	20	
		374	

TOTAL RETAIL PARKING				
LEVEL	PARKING TYPE	COUNT		
P1	RETAIL REGULAR PARKING	24		
P1	RETAIL BARRIER FREE PARKING	2		
		26		

TOTAL VISITOR PARKING		
LEVEL	PARKING TYPE	COUNT
P1	VISITOR REGULAR PARKING	21
P1	VISITOR BARRIER FREE PARKING	1
	•	22

TOTAL RESIDENTIAL				
LEVEL	PARKING TYPE	COUNT		
P2	RESIDENTIAL REGULAR PARKING	182		
P1	RESIDENTIAL REGULAR PARKING	116		
P2	RESIDENTIAL BARRIER FREE TYPE A PARKING	7		
P1	RESIDENTIAL BARRIER FREE TYPE A PARKING	5		
	•	310		

TOTAL PROPOSED PARKING (TANDEM)			
LEVEL	PARKING TYPE	COUNT	
P2	TANDEM REGULAR PARKING (SMALL CAR)	6	
		6	

TOTAL PROPOSED PARKING(INCLUDING TANDEM)				
LEVEL	PARKING TYPE	COUNT		
P2	RESIDENTIAL BARRIER FREE TYPE A PARKING	7		
P1	RESIDENTIAL BARRIER FREE TYPE A PARKING	5		
		12		
P2	RESIDENTIAL REGULAR PARKING	182		
P1	RESIDENTIAL REGULAR PARKING	116		
		298		
P1	RETAIL BARRIER FREE PARKING	2		
		2		
P1	RETAIL REGULAR PARKING	24		
		24		
P2	TANDEM REGULAR PARKING (SMALL CAR)	6		
		6		
P1	VISITOR BARRIER FREE PARKING	1		
		1		
P1	VISITOR REGULAR PARKING	21		
		21		
		364		

REQUIRED RETAIL BIKE				
RETAIL LONG-TERM (X0.085/100 sm)RETAIL SHORT-TERM (X0.25)		TOTAL		
1.21		3.56	4.77	
	PRO	VIDED RETAIL SHORT-TERM BIKE		
LEVEL		TYPE	COUNT	
Level 1	RETAIL SH	IORT-TERM BIKE	4	
			4	
	PRC	VIDED RETAIL LONG-TERM BIKE		
LEVEL		TYPE		
Level 1	RETAIL LONG-TERM BIKE 2		2	
	L		2	
	PROVIDED	TOTAL RETAIL SHORT/LONG-TERM BI	KE	
LEVEL		TYPE	COUNT	
Level 1	RETAIL LONG-TERM BIKE 2		2	
Level 1	RETAIL SHORT-TERM BIKE		4	
	-		6	
	PF	ROVIDED RESIDENTIAL LOCKER		
LEVEL		LOCKER TYPE	COUNT	
P2	RES. 1830	X915 LOCKER	80	
P1	RES. 1830	X915 LOCKER	81	
Level 1	RES. 1830	X915 LOCKER	34	
			195	

REQUIRED RETAIL BIKE					
( X0.085	DNG-TERM /100 sm)	RETAIL SHORT-TERM (X0.25)	TOTAL		
1.21		3.56	4.77		
	PRO	/IDED RETAIL SHORT-TERM BIKE			
LEVEL		TYPE	COUNT		
Level 1	RETAIL SH	ORT-TERM BIKE	4		
			4		
	PRC	VIDED RETAIL LONG-TERM BIKE			
LEVEL		COUNT			
Level 1	RETAIL LONG-TERM BIKE 2				
2					
	PROVIDED	TOTAL RETAIL SHORT/LONG-TERM	BIKE		
LEVEL		TYPE	COUNT		
Level 1	RETAIL LC	NG-TERM BIKE	2		
Level 1	RETAIL SH	IORT-TERM BIKE	4		
	-		6		
	PR	OVIDED RESIDENTIAL LOCKER			
LEVEL		LOCKER TYPE	COUNT		
P2	RES. 1830	X915 LOCKER	80		
P1	RES. 1830	X915 LOCKER	81		
Level 1	RES. 1830	X915 LOCKER	34		
			195		

# Low Impact Design Features List

- Development Density
- while minimizing urban sprawl
- 2. Public Transportation Access
- Walkability
- connected to pedestrian pathways.
- Bicycle Storage
- an alternative form of transportation
- 5. Green Roof System
- serve as outdoor amenity and recreation areas. 6. New Trees
  - volume.
- proposed building.
- Erosion And Sediment Control
- contain dust within the site.
- Green Site Maintenance
- A comprehensive site maintenance program will be implemented. Heat Island Effect (Non-Roof and Roof)
- effect which results from exposed surface parking lots
- 10. Indoor Water Use Reduction
- 11. Tri-Sorter Recycling
- disposal of recyclables and refuse.
- 12. Regional Material
- shipment of materials.
- 13. Pedestrian Walkways (Incorporated)
  - Private sidewalks and walkways are cor within immediate site vicinity have a buf
  - New sidewalks and pathways are propo
- Walkways will have various shaded, res
- 14. Site and Building Lighting (Incorporated)
- properties.
- to a heritage structure.

• The proposed development serves to maximize the permitted density on the land, maximizing efficient use of the lands

• 21-51 Queen Street North will be located adjacent to several Mississauga Transit bus lines. Furthermore, it is a short bus ride to the GO Train, therefore encouraging mass transit and consequently reducing the carbon footprint.

• 21-51 Queen Street North will be situated within walking distance to public transit and retail, therefore encouraging mass transit. All the public and private walkways are continuous, accessible, and barrier-free. All the building entries are

• Conveniently located bicycle parking spaces for residents and visitors have been proposed to encourage bicycle use as

• Where feasible, all portions of the roof will have either a high solar reflectance surface, outdoor amenity areas or a "green roof" created through the use of plant material, reducing temperature extremes inside the buildings and providing attractive views from suites. These areas will not only help to reduce energy use and the heat island effect but will also

• New shade trees along all street frontages and public walkways will be provided in areas with sufficient soil quality and

• Previous hardscape areas will be converted to landscape areas and act as a buffer between existing residents and the

• The erosion and sediment control plan for the site will be designed in conformance with the City of Mississauga and Credit Valley Conservation Authority guidelines. Construction management will be taking erosion and sediment control measures as well as following the requirements of the grading plan to prevent loss of topsoil, while also working to

• Of the vehicular parking provided, all will be contained within underground parking levels. This will reduce the heat island

• To reduce water consumption, high-efficiency toilets and water reducing fixtures will be provided.

• A tri-sorter system will be installed and made accessible to each residential floor, allowing for convenient separation and

• Construction materials where available will be sourced from the GTA to minimize the carbon footprint associated with the

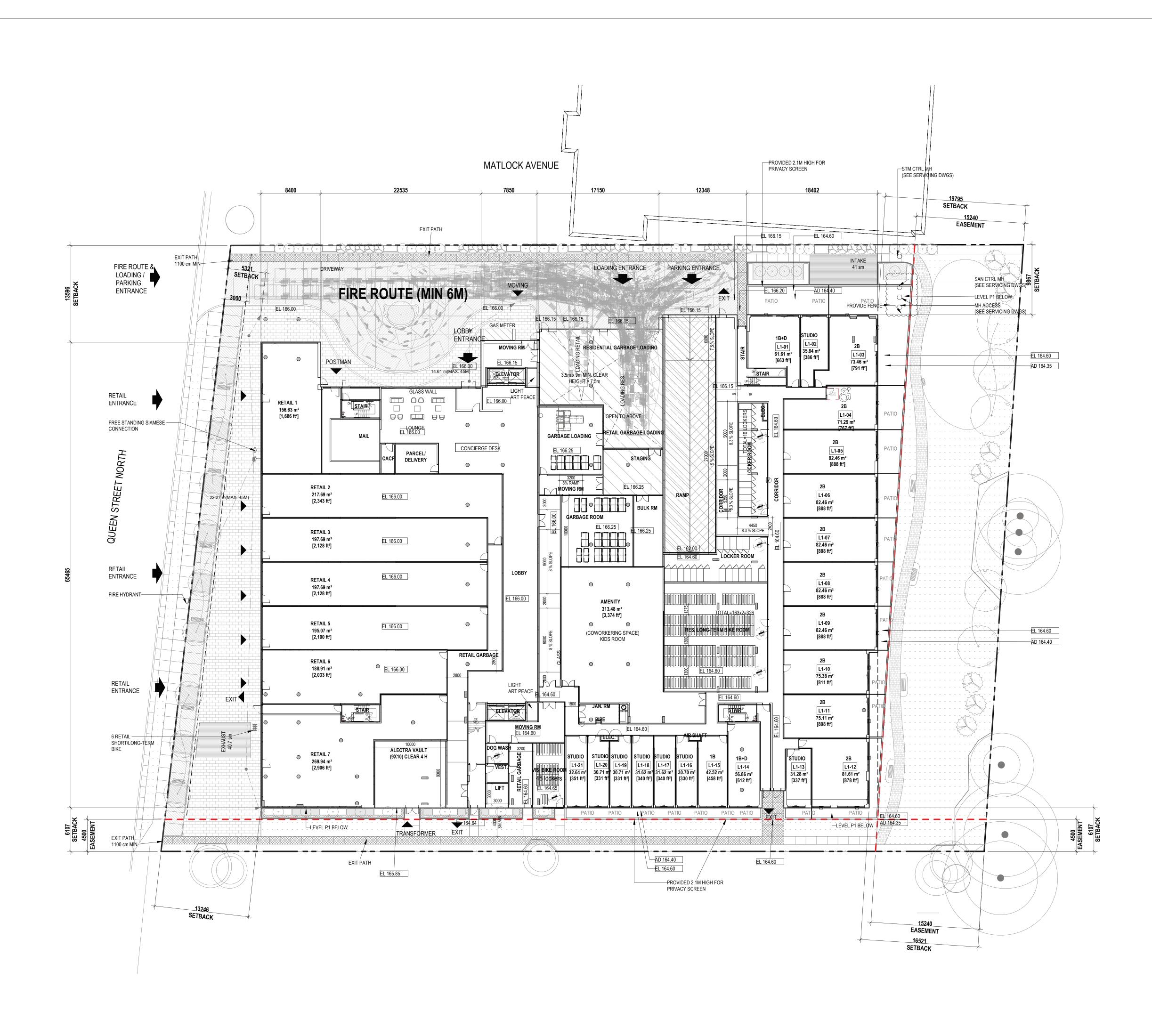
ntinuous, universally accessible, barrier-free, and clearly designated. Signated.	dewalks
ffer of vegetation between traffic and the walkway.	
osed intended for the enjoyment of residents.	
sting spots for relaxation and recreation	

• Install exterior light fixtures that are properly shielded to prevent glare and/or light to trespass onto any neighbouring

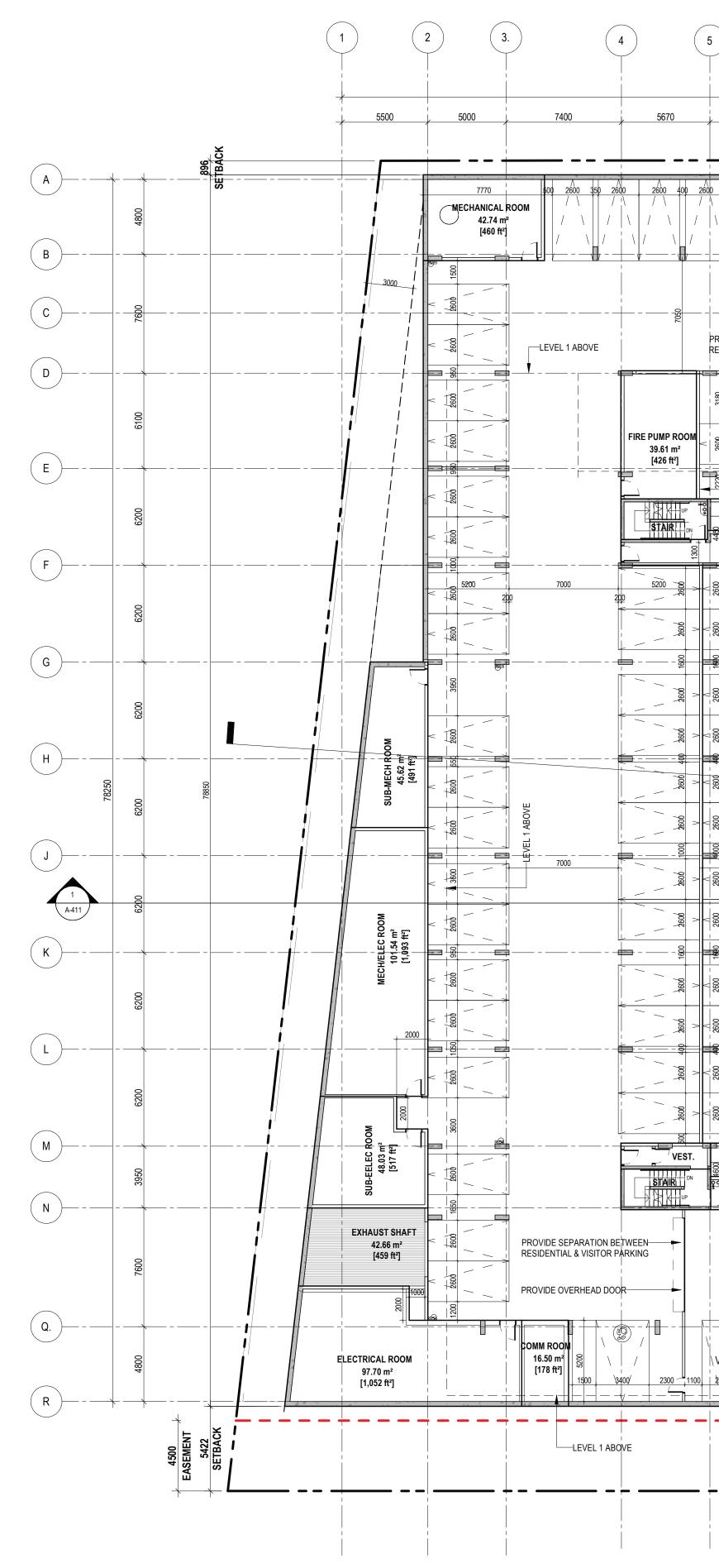
• Avoid up-lighting from exterior light fixtures mounted on buildings unless they are designated as an integral component

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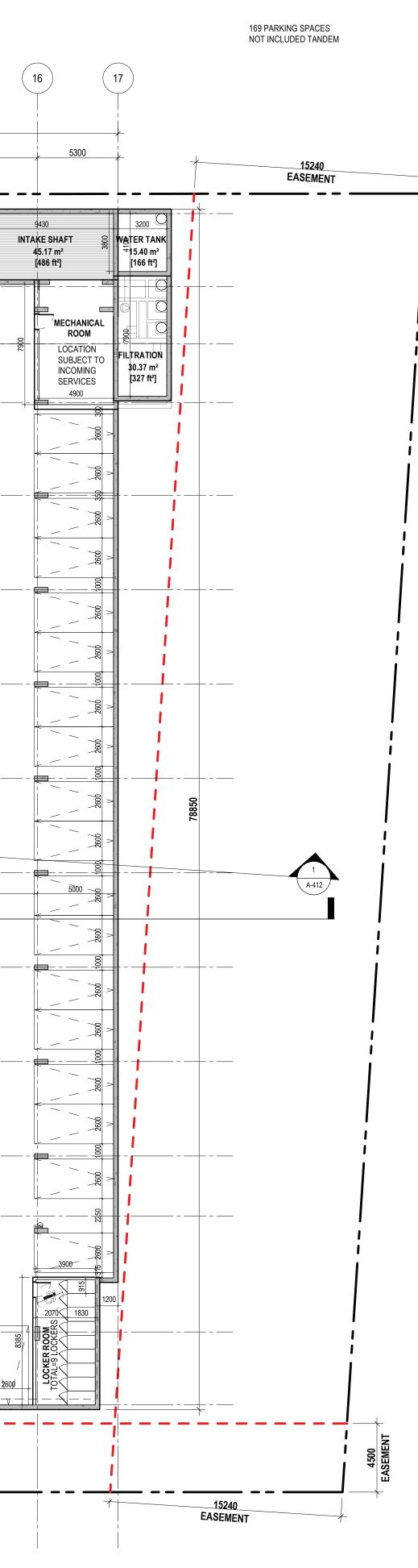






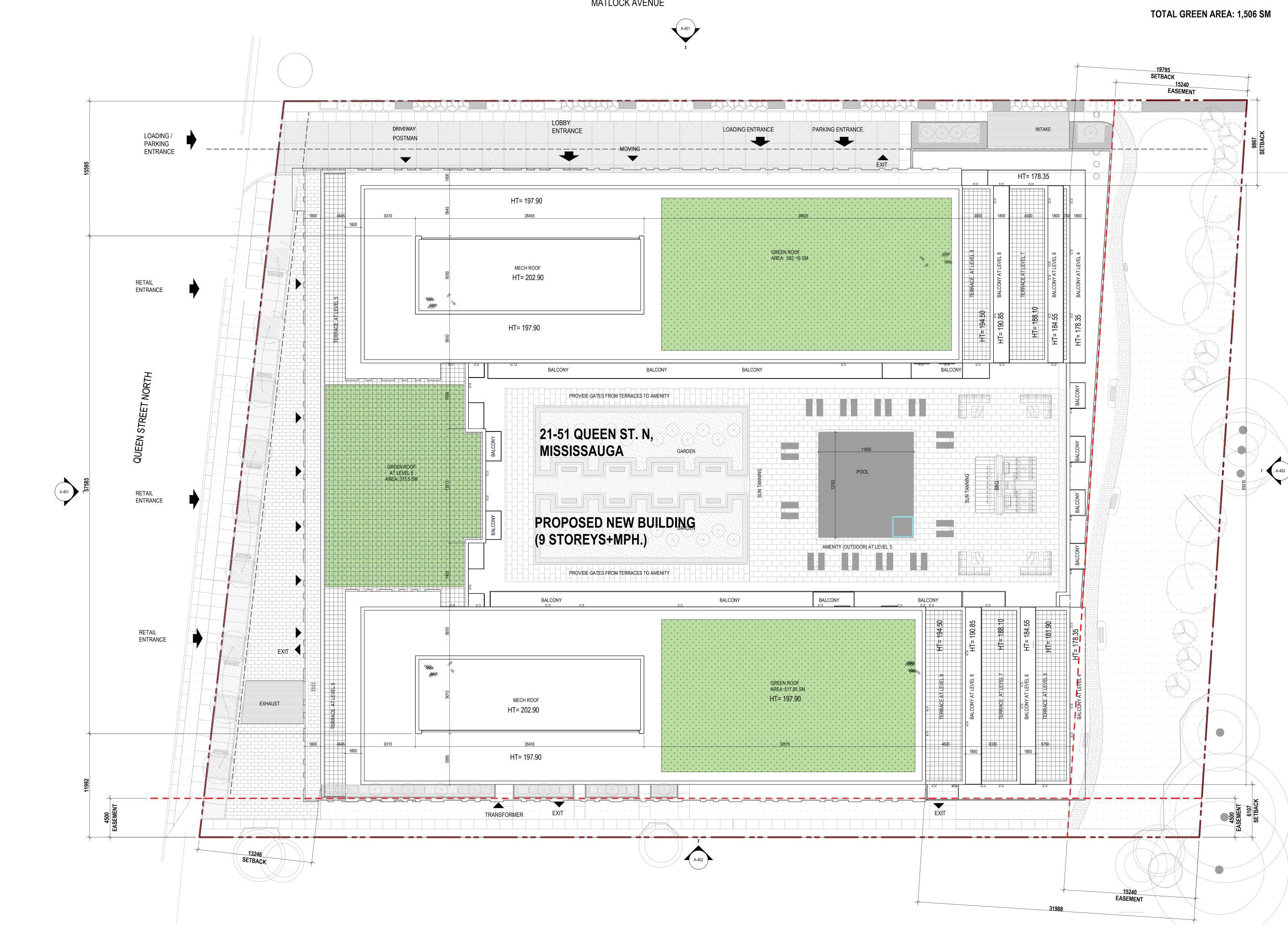
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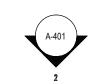






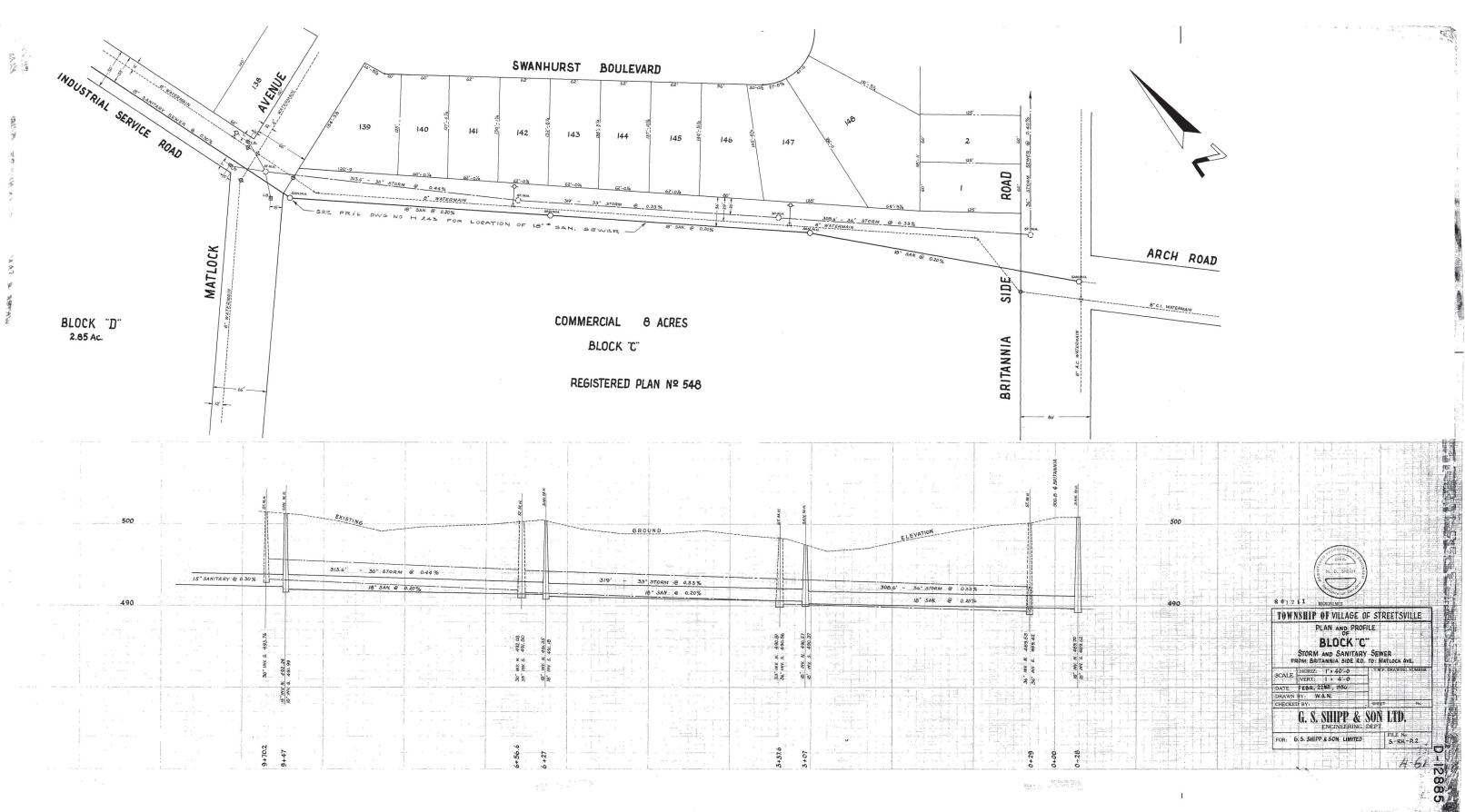


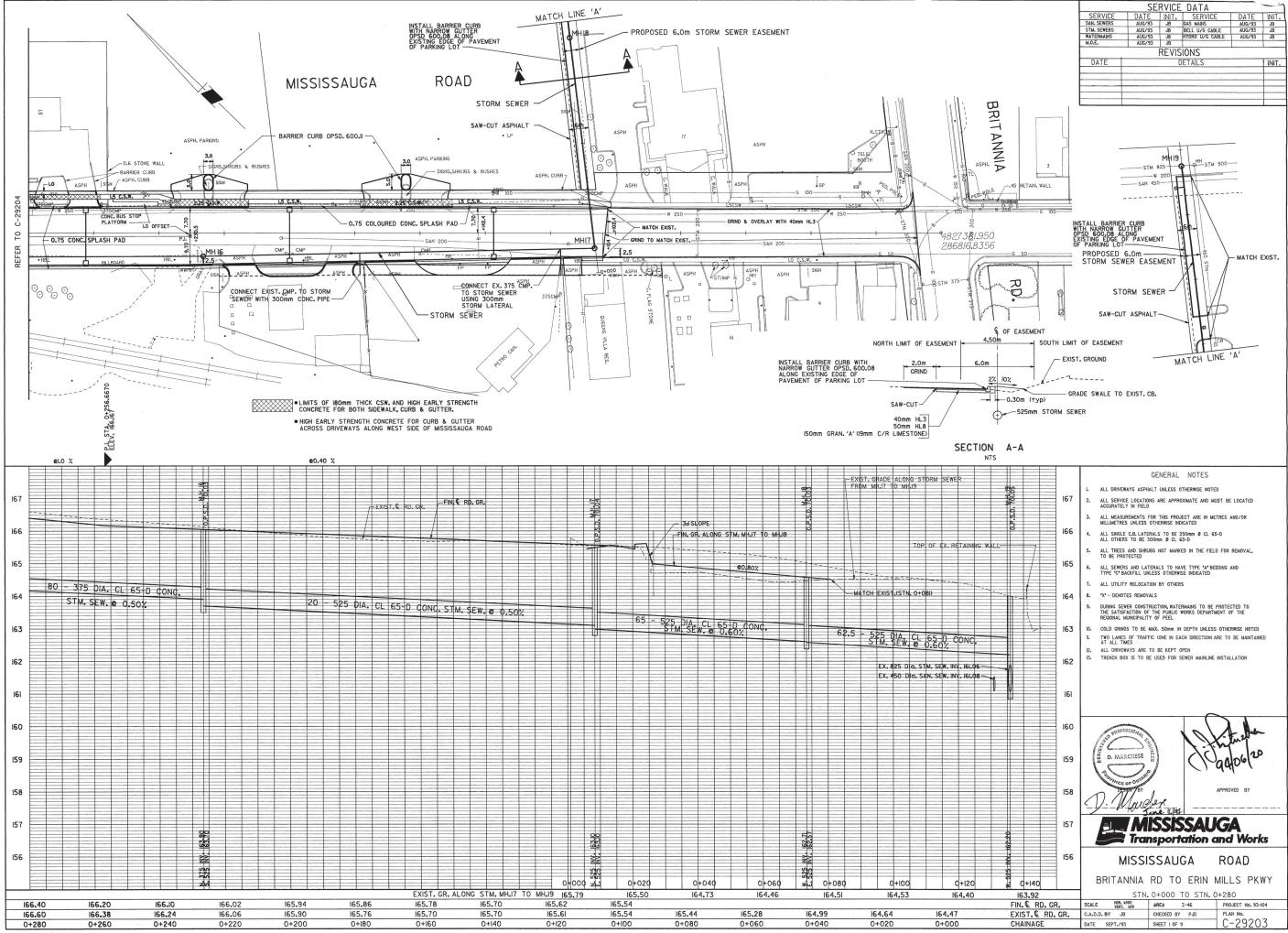
MATLOCK AVENUE



BUILDING HEIGHT





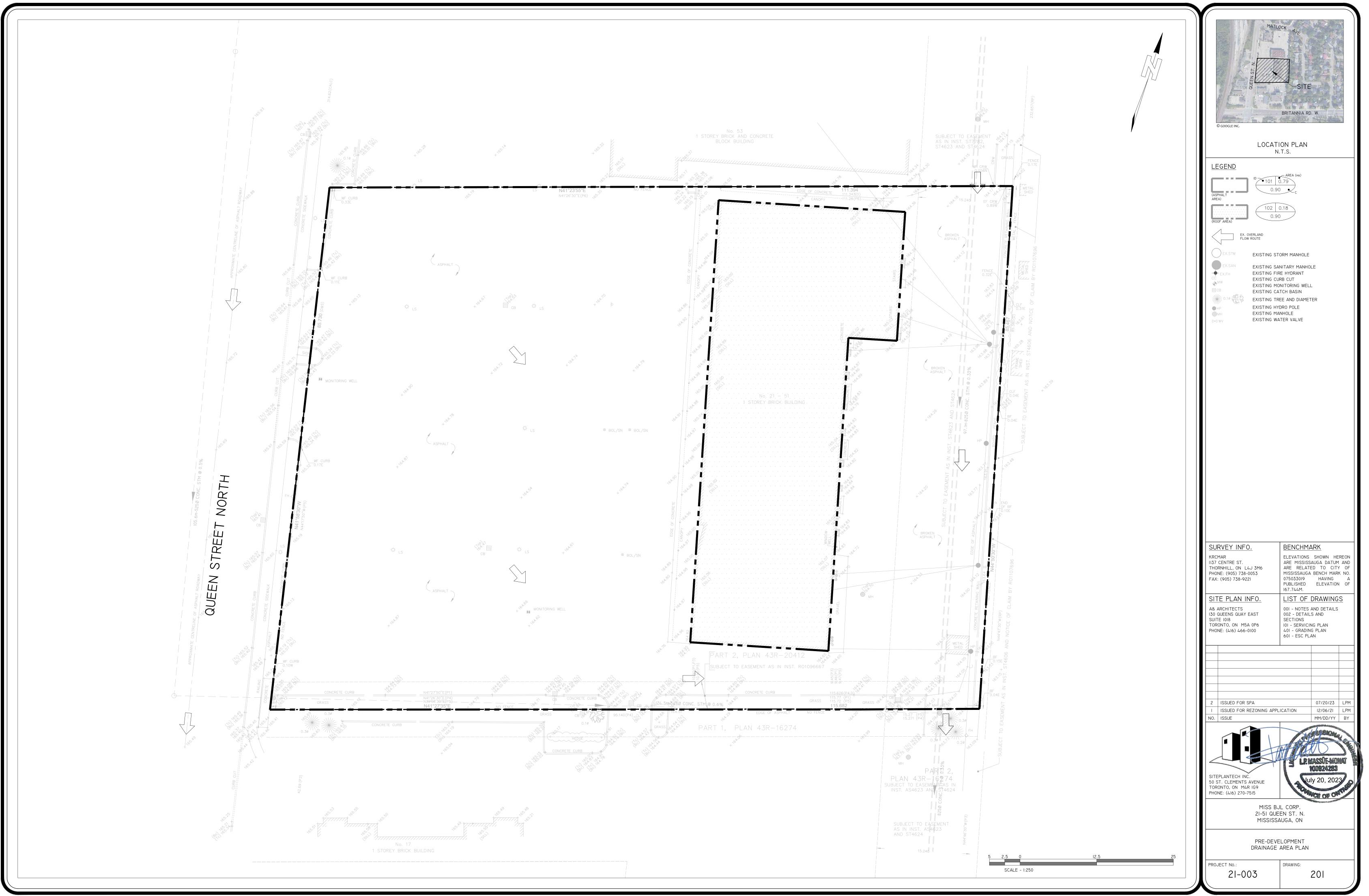


	SE	RVICE	DATA		
SERVICE	DATE	INIT.	SERVICE	DATE	INIT.
SAN. SEWERS	AUG/93	JB	GAS MAINS	AUG/93	JB
STM. SEWERS	AUG/93	JB	BELL U/G CABLE	AUG/93	JB
WATERMAINS	AUG/93	JB	HYDRO U/G CABLE	AUG/93	JB
M.O.E.	AUG/93	JB			
		REVIS	SIONS		
DATE		[	DETAILS		INIT.
					-

Appendix B

**Storm Data** 





#### PRE-DEVELOPMENT RUNOFF COEFFICIENT

	Drainage Area	a 101	
Surface Type	С	A (Ha)	A*C
Roof	0.90	0.180	0.162
Asphalt	0.90	0.788	0.709
Composite C		0.968	0.900

	Sum	nmary	
Drainage Area	С	A (Ha)	A*C
101	0.90	0.968	0.871
TOTAL		0.968	0.900



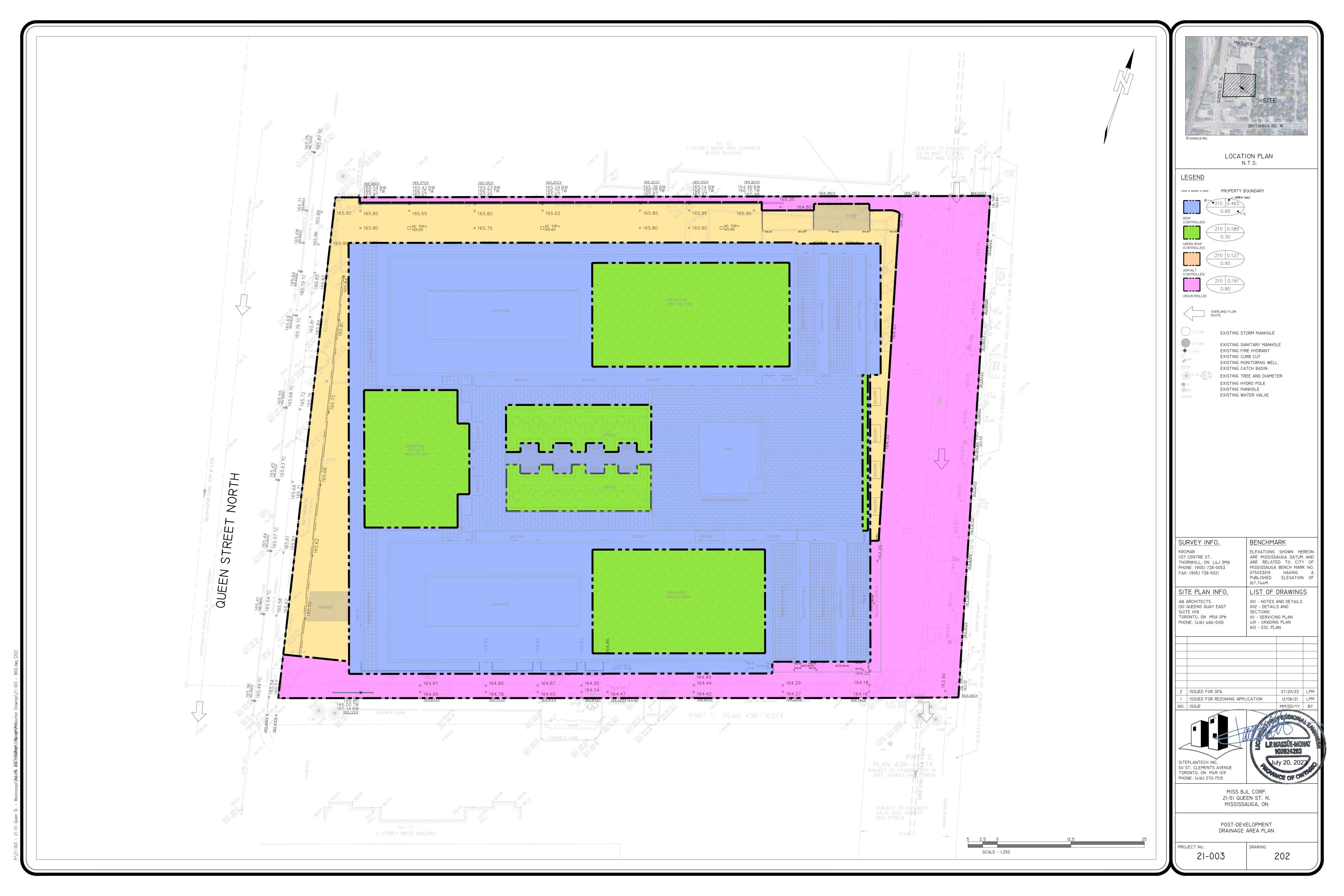
#### **ALLOWABLE RELEASE RATE CALCULATION**

IDF set: Mississauaga					
а	T <sub>c</sub>	Ь	с		
610.0	15	4.6	0.780		
820.0	15	4.6	0.780		
1450.0	15	4.9	0.780		
	610.0 820.0	610.0 15 820.0 15	610.0154.6820.0154.6		

 $I = \frac{a}{(t_c + b)^c}$ Where:

Pre-Development ID 101						
<b>Return Period</b>	Area (Ha)	Composite C	l (mm/hr)*	Q (L/s)		
2-year	0.968	0.900	59.89	144.9		
5-year	0.968	0.900	80.51	194.8		
10-year	0.968	0.900	99.17	240.0		
100-year	0.968	0.900	140.69	340.5		





#### POST-DEVELOPMENT RUNOFF COEFFICIENT

Dra	inage	Area	210

Surface Type	С	A (Ha)	A*C
Hardscape	0.90	0.127	0.114
Roof	0.90	0.462	0.416
Green Roof	0.30	0.189	0.057
Composite C		0.777	0.754

#### Drainage Area 220

Surface Type	С	A (Ha)	A*C
Hardscape	0.90	0.191	0.172
Composite C		0.191	0.900

	Summa	ary	
Drainage Area	С	A (Ha)	A*C
210	0.75	0.777	0.586
220	0.90	0.191	0.172
TOTAL		0.968	0.783



#### STORMWATER MANAGEMENT QUANTITY CONTROL SUMMARY

Drainage Area	ROOF	210	220	Total
Bldg ID				
C <sub>2</sub>	0.00	0.75	0.90	-
A (Ha)	0.000	0.78	0.191	0.97
<b>Q</b> <sub>Release (L/s)</sub>	0.0	97.6	28.6	126.2
Storage (m <sup>3</sup> )	0.0	0.0	0.0	0.0
Vol. Avail. (m <sup>3</sup> )	-	-	-	0.0
Orifice	Uncontrolled	Uncontrolled	Uncontrolled	-
<b>Q</b> Orifice (L/s)	-	-	-	-
Unctrled Q (L/s)	0.0	97.6	28.6	-
Orifice type	-	-	-	-

5-year Summary Matrix					
Drainage Area	ROOF	210	220	Total	
Bldg ID					
C₅	0.00	0.75	0.90	-	
A (Ha)	0.000	0.78	0.191	0.97	
<b>Q</b> <sub>Release (L/s)</sub>	0.0	131.2	38.4	169.7	
Storage (m <sup>3</sup> )	0.0	0.0	0.0	0.0	
Vol. Avail. (m <sup>3</sup> )	-	-	-	0.0	
Orifice	Uncontrolled	Uncontrolled	Uncontrolled	-	
<b>Q</b> <sub>Orifice (L/s)</sub>	-	-	-	-	
Unctrled Q (L/s)	0.0	131.2	38.4	-	
Orifice type	-	-	-	-	



#### STORMWATER MANAGEMENT QUANTITY CONTROL SUMMARY

10-Year Summary Matrix					
Drainage Area	EXT1	210	220	Total	
Bldg ID					
C <sub>10</sub>	0.00	0.75	0.90	-	
A (Ha)	0.000	0.78	0.191	0.97	
<b>Q</b> <sub>Release (L/s)</sub>	6.3	168.0	47.3	215.3	
Storage (m <sup>3</sup> )	0.0	0.0	0.0	0.0	
Vol. Avail. (m <sup>3</sup> )	-	72.2	-	72.2	
Orifice	Uncontrolled	Uncontrolled	Uncontrolled	-	
<b>Q</b> <sub>Orifice (L/s)</sub>	-	-	-	-	
Unctrled Q (L/s)	6.3	168.0	47.3	-	
Orifice type	-	-	-	-	

100-Year Summary						
Drainage Area	ROOF	210	220	Total		
Bldg ID						
C <sub>100</sub>	0.00	0.75	0.90	-		
A (Ha)	0.000	0.78	0.191	0.97		
<b>Q</b> <sub>Release (L/s)</sub>	0.0	229.3	67.2	296.5		
Storage (m <sup>3</sup> )	0.0	0.0	0.0	0.0		
Vol. Avail. (m <sup>3</sup> )	-	67.8	-	67.8		
Orifice	Uncontrolled	Uncontrolled	Uncontrolled	-		
<b>Q</b> <sub>Orifice (L/s)</sub>	-	-	-	-		
Unctrled Q (L/s)	0.0	229.3	67.2	-		
Orifice type	-	-	-	-		



Drainage	Area 210
Area (Ha)	0.78
C <sub>2</sub>	0.75
AC	0.59
T <sub>c</sub> (min)	15.0
T incr. (min)	5
Q <sub>1</sub> (l/s)	97.6
Req. vol. (m <sup>3</sup> )	0.0

Mississauaga	2-year
a=	610
b=	4.6
C=	0.780

T (min)	l (mm/hr)	Q (I/s)	Total Vol.	Ext. Vol. (m <sup>3</sup> )	Rel. Vol. (m <sup>3</sup> )	Storage (m <sup>3</sup> )
15	59.9	97.6	87.9	0.0	87.9	-
20	50.2	81.8	98.1	0.0	117.1	-
25	43.4	70.8	106.2	0.0	146.4	-
30	38.4	62.7	112.8	0.0	175.7	-
35	34.6	56.4	118.4	0.0	205.0	-
40	31.5	51.4	123.4	0.0	234.3	-
45	29.0	47.3	127.7	0.0	263.6	-
50	26.9	43.9	131.7	0.0	292.8	-
55	25.2	41.0	135.3	0.0	322.1	-
60	23.6	38.5	138.6	0.0	351.4	-
65	22.3	36.3	141.7	0.0	380.7	-
70	21.1	34.4	144.5	0.0	410.0	-
75	20.1	32.7	147.2	0.0	439.3	-
80	19.1	31.2	149.7	0.0	468.5	-
85	18.3	29.8	152.1	0.0	497.8	-
90	17.5	28.6	154.4	0.0	527.1	-
95	16.9	27.5	156.6	0.0	556.4	-
100	16.2	26.4	158.6	0.0	585.7	-
105	15.6	25.5	160.6	0.0	615.0	-
110	15.1	24.6	162.5	0.0	644.2	-
115	14.6	23.8	164.3	0.0	673.5	-
120	14.2	23.1	166.1	0.0	702.8	-
125	13.7	22.4	167.8	0.0	732.1	-
130	13.3	21.7	169.4	0.0	761.4	-
135	13.0	21.1	171.0	0.0	790.7	-
140	12.6	20.5	172.5	0.0	819.9	-
145	12.3	20.0	174.0	0.0	849.2	-
150	12.0	19.5	175.4	0.0	878.5	-
155	11.7	19.0	176.8	0.0	907.8	-
160	11.4	18.6	178.2	0.0	937.1	-
165	11.1	18.1	179.5	0.0	966.4	-
170	10.9	17.7	180.8	0.0	995.6	-



Drainage	Area 210
Area (Ha)	0.78
C <sub>5</sub>	0.75
AC	0.59
T <sub>c</sub> (min)	15.0
T incr. (min)	5
Q <sub>1</sub> (l/s)	131.2
Req. vol. (m <sup>3</sup> )	0.0

Mississauaga	5-year
a=	820
b=	4.6
C=	0.780

T (min)	l (mm/hr)	Q (l/s)	Total Vol.		Rel. Vol. (m <sup>3</sup> )	Storage (m <sup>3</sup> )
15	80.5	131.2	118.1	0.0	118.1	0.0
20	67.4	109.9	131.9	0.0	157.5	-
25	58.4	95.1	142.7	0.0	196.8	-
30	51.7	84.2	151.6	0.0	236.2	-
35	46.5	75.8	159.2	0.0	275.6	-
40	42.4	69.1	165.8	0.0	314.9	-
45	39.0	63.6	171.7	0.0	354.3	-
50	36.2	59.0	177.0	0.0	393.7	-
55	33.8	55.1	181.9	0.0	433.0	-
60	31.8	51.8	186.3	0.0	472.4	-
65	30.0	48.8	190.4	0.0	511.7	-
70	28.4	46.3	194.3	0.0	551.1	-
75	27.0	44.0	197.9	0.0	590.5	-
80	25.7	41.9	201.3	0.0	629.8	-
85	24.6	40.1	204.5	0.0	669.2	-
90	23.6	38.4	207.6	0.0	708.6	-
95	22.7	36.9	210.5	0.0	747.9	-
100	21.8	35.5	213.2	0.0	787.3	-
105	21.0	34.3	215.9	0.0	826.7	-
110	20.3	33.1	218.4	0.0	866.0	-
115	19.6	32.0	220.9	0.0	905.4	-
120	19.0	31.0	223.2	0.0	944.8	-
125	18.4	30.1	225.5	0.0	984.1	-
130	17.9	29.2	227.7	0.0	1023.5	-
135	17.4	28.4	229.8	0.0	1062.9	-
140	16.9	27.6	231.9	0.0	1102.2	-
145	16.5	26.9	233.9	0.0	1141.6	-
150	16.1	26.2	235.8	0.0	1181.0	-
155	15.7	25.6	237.7	0.0	1220.3	-
160	15.3	25.0	239.6	0.0	1259.7	-
165	15.0	24.4	241.3	0.0	1299.0	-
170	14.6	23.8	243.1	0.0	1338.4	-



Drainage	Area 210
Area (Ha)	0.78
C <sub>10</sub>	0.75
AC	0.59
T <sub>c</sub> (min)	15.0
T incr. (min)	5
Q <sub>1</sub> (l/s)	168.0
Req. vol. (m <sup>3</sup> )	0.0

Mississauaga	10-year
a=	1010
b=	4.6
c=	0.780

T (min)	l (mm/hr)	Q (l/s)	Total Vol.	Ext. Vol. (m <sup>3</sup> )	Rel. Vol. (m <sup>3</sup> )	Storage (m <sup>3</sup> )
15	99.2	161.6	145.5	5.7	151.2	0.0
20	83.1	135.4	162.4	5.7	201.6	-
25	71.9	117.2	175.8	5.7	251.9	-
30	63.7	103.7	186.7	5.7	302.3	-
35	57.3	93.4	196.1	5.7	352.7	-
40	52.2	85.1	204.3	5.7	403.1	-
45	48.1	78.3	211.5	5.7	453.5	-
50	44.6	72.7	218.1	5.7	503.9	-
55	41.7	67.9	224.0	5.7	554.3	-
60	39.1	63.7	229.5	5.7	604.7	-
65	36.9	60.1	234.6	5.7	655.1	-
70	35.0	57.0	239.3	5.7	705.5	-
75	33.2	54.2	243.8	5.7	755.8	-
80	31.7	51.7	247.9	5.7	806.2	-
85	30.3	49.4	251.9	5.7	856.6	-
90	29.0	47.3	255.7	5.7	907.0	-
95	27.9	45.5	259.2	5.7	957.4	-
100	26.9	43.8	262.6	5.7	1007.8	-
105	25.9	42.2	265.9	5.7	1058.2	-
110	25.0	40.8	269.1	5.7	1108.6	-
115	24.2	39.4	272.1	5.7	1159.0	-
120	23.4	38.2	275.0	5.7	1209.4	-
125	22.7	37.0	277.8	5.7	1259.7	-
130	22.1	36.0	280.5	5.7	1310.1	-
135	21.4	34.9	283.1	5.7	1360.5	-
140	20.9	34.0	285.6	5.7	1410.9	-
145	20.3	33.1	288.1	5.7	1461.3	-
150	19.8	32.3	290.5	5.7	1511.7	-
155	19.3	31.5	292.8	5.7	1562.1	-
160	18.9	30.7	295.1	5.7	1612.5	-
165	18.4	30.0	297.3	5.7	1662.9	-
170	18.0	29.4	299.4	5.7	1713.3	-



Drainage Area	
Area (Ha)	0.78
C <sub>100</sub>	0.75
AC	0.59
T <sub>c</sub> (min)	15.0
T incr. (min)	5
Q <sub>1</sub> (l/s)	229.3
Req. vol. (m³)	0.0

Mississauaga	100-year
a=	1450
b=	4.9
C=	0.780

T (min)	l (mm/hr)	Q (l/s)	Total Vol.		Rel. Vol. (m <sup>3</sup> )	Storage (m <sup>3</sup> )
15	140.7	229.3	206.4	0.0	206.4	0.0
20	118.1	192.5	231.0	0.0	275.2	-
25	102.4	166.9	250.4	0.0	343.9	-
30	90.8	147.9	266.3	0.0	412.7	-
35	81.8	133.3	279.9	0.0	481.5	-
40	74.6	121.5	291.7	0.0	550.3	-
45	68.7	111.9	302.2	0.0	619.1	-
50	63.8	103.9	311.7	0.0	687.9	-
55	59.6	97.1	320.3	0.0	756.7	-
60	56.0	91.2	328.3	0.0	825.5	-
65	52.8	86.1	335.6	0.0	894.3	-
70	50.0	81.5	342.5	0.0	963.0	-
75	47.6	77.5	348.9	0.0	1031.8	-
80	45.4	74.0	355.0	0.0	1100.6	-
85	43.4	70.7	360.7	0.0	1169.4	-
90	41.6	67.8	366.1	0.0	1238.2	-
95	40.0	65.1	371.3	0.0	1307.0	-
100	38.5	62.7	376.2	0.0	1375.8	-
105	37.1	60.5	380.9	0.0	1444.6	-
110	35.8	58.4	385.5	0.0	1513.4	-
115	34.7	56.5	389.8	0.0	1582.1	-
120	33.6	54.7	394.0	0.0	1650.9	-
125	32.6	53.1	398.1	0.0	1719.7	-
130	31.6	51.5	402.0	0.0	1788.5	-
135	30.7	50.1	405.7	0.0	1857.3	-
140	29.9	48.7	409.4	0.0	1926.1	-
145	29.1	47.5	412.9	0.0	1994.9	-
150	28.4	46.3	416.4	0.0	2063.7	-
155	27.7	45.1	419.7	0.0	2132.5	-
160	27.0	44.1	423.0	0.0	2201.2	-
165	26.4	43.0	426.2	0.0	2270.0	-
170	25.8	42.1	429.3	0.0	2338.8	-



Drainage	Area 220
Area (Ha)	0.191
C <sub>2</sub>	0.90
AC	0.172
T <sub>c</sub> (min)	15.0
T incr. (min)	5
Q <sub>1</sub> (l/s)	28.6
Req. vol. (m³)	0.0

Mississauaga	2-year
a=	610
b=	4.6
C=	0.780

Required	Storage	Summary
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T (min)	l (mm/hr)	Q (l/s)	Total Vol.		Rel. Vol. (m <sup>3</sup> )	Storage (m <sup>3</sup> )
15	59.9	28.6	25.7	0.0	25.7	-
20	50.2	23.9	28.7	0.0	34.3	-
25	43.4	20.7	31.1	0.0	42.9	-
30	38.4	18.4	33.0	0.0	51.5	-
35	34.6	16.5	34.7	0.0	60.0	-
40	31.5	15.1	36.1	0.0	68.6	-
45	29.0	13.9	37.4	0.0	77.2	-
50	26.9	12.9	38.6	0.0	85.8	-
55	25.2	12.0	39.6	0.0	94.4	-
60	23.6	11.3	40.6	0.0	102.9	-
65	22.3	10.6	41.5	0.0	111.5	-
70	21.1	10.1	42.3	0.0	120.1	-
75	20.1	9.6	43.1	0.0	128.7	-
80	19.1	9.1	43.9	0.0	137.2	-
85	18.3	8.7	44.6	0.0	145.8	-
90	17.5	8.4	45.2	0.0	154.4	-
95	16.9	8.0	45.9	0.0	163.0	-
100	16.2	7.7	46.5	0.0	171.5	-
105	15.6	7.5	47.0	0.0	180.1	-
110	15.1	7.2	47.6	0.0	188.7	-
115	14.6	7.0	48.1	0.0	197.3	-
120	14.2	6.8	48.6	0.0	205.9	-
125	13.7	6.6	49.1	0.0	214.4	-
130	13.3	6.4	49.6	0.0	223.0	-
135	13.0	6.2	50.1	0.0	231.6	-
140	12.6	6.0	50.5	0.0	240.2	-
145	12.3	5.9	51.0	0.0	248.7	-
150	12.0	5.7	51.4	0.0	257.3	-
155	11.7	5.6	51.8	0.0	265.9	-
160	11.4	5.4	52.2	0.0	274.5	-
165	11.1	5.3	52.6	0.0	283.1	-
170	10.9	5.2	53.0	0.0	291.6	-



Drainage	Area 220
Area (Ha)	0.191
C <sub>5</sub>	0.90
AC	0.172
T <sub>c</sub> (min)	15.0
T incr. (min)	5
Q <sub>1</sub> (l/s)	38.4
Req. vol. (m³)	0.0

Mississauaga	5-year
a=	820
b=	4.6
C=	0.780

T (min)	l (mm/hr)	Q (l/s)	Total Vol.	Ext. Vol. (m <sup>3</sup> )	Rel. Vol. (m <sup>3</sup> )	Storage (m <sup>3</sup> )
15	80.5	38.4	34.6	0.0	34.6	0.0
20	67.4	32.2	38.6	0.0	46.1	-
25	58.4	27.9	41.8	0.0	57.7	-
30	51.7	24.7	44.4	0.0	69.2	-
35	46.5	22.2	46.6	0.0	80.7	-
40	42.4	20.2	48.6	0.0	92.2	-
45	39.0	18.6	50.3	0.0	103.8	-
50	36.2	17.3	51.9	0.0	115.3	-
55	33.8	16.1	53.3	0.0	126.8	-
60	31.8	15.2	54.6	0.0	138.4	-
65	30.0	14.3	55.8	0.0	149.9	-
70	28.4	13.6	56.9	0.0	161.4	-
75	27.0	12.9	58.0	0.0	173.0	-
80	25.7	12.3	59.0	0.0	184.5	-
85	24.6	11.7	59.9	0.0	196.0	-
90	23.6	11.3	60.8	0.0	207.5	-
95	22.7	10.8	61.6	0.0	219.1	-
100	21.8	10.4	62.5	0.0	230.6	-
105	21.0	10.0	63.2	0.0	242.1	-
110	20.3	9.7	64.0	0.0	253.7	-
115	19.6	9.4	64.7	0.0	265.2	-
120	19.0	9.1	65.4	0.0	276.7	-
125	18.4	8.8	66.1	0.0	288.3	-
130	17.9	8.6	66.7	0.0	299.8	-
135	17.4	8.3	67.3	0.0	311.3	-
140	16.9	8.1	67.9	0.0	322.8	-
145	16.5	7.9	68.5	0.0	334.4	-
150	16.1	7.7	69.1	0.0	345.9	-
155	15.7	7.5	69.6	0.0	357.4	-
160	15.3	7.3	70.2	0.0	369.0	-
165	15.0	7.1	70.7	0.0	380.5	-
170	14.6	7.0	71.2	0.0	392.0	-



Drainage A	rea 220
Area (Ha)	0.191
C <sub>10</sub>	0.90
AC	0.172
T <sub>c</sub> (min)	15.0
T incr. (min)	5
Q <sub>1</sub> (l/s)	47.3
Req. vol. (m³)	0.0

Mississauaga	10-year
a=	1010
b=	4.6
C=	0.780

T (min)	l (mm/hr)	Q (l/s)	Total Vol.		Rel. Vol. (m <sup>3</sup> )	Storage (m <sup>3</sup> )
15	99.2	47.3	42.6	0.0	42.6	-
20	83.1	39.7	47.6	0.0	56.8	-
25	71.9	34.3	51.5	0.0	71.0	-
30	63.7	30.4	54.7	0.0	85.2	-
35	57.3	27.4	57.4	0.0	99.4	-
40	52.2	24.9	59.8	0.0	113.6	-
45	48.1	22.9	62.0	0.0	127.8	-
50	44.6	21.3	63.9	0.0	142.0	-
55	41.7	19.9	65.6	0.0	156.2	-
60	39.1	18.7	67.2	0.0	170.4	-
65	36.9	17.6	68.7	0.0	184.6	-
70	35.0	16.7	70.1	0.0	198.8	-
75	33.2	15.9	71.4	0.0	213.0	-
80	31.7	15.1	72.6	0.0	227.2	-
85	30.3	14.5	73.8	0.0	241.4	-
90	29.0	13.9	74.9	0.0	255.6	-
95	27.9	13.3	75.9	0.0	269.8	-
100	26.9	12.8	76.9	0.0	284.0	-
105	25.9	12.4	77.9	0.0	298.2	-
110	25.0	11.9	78.8	0.0	312.4	-
115	24.2	11.5	79.7	0.0	326.6	-
120	23.4	11.2	80.5	0.0	340.8	-
125	22.7	10.8	81.4	0.0	355.0	-
130	22.1	10.5	82.2	0.0	369.3	-
135	21.4	10.2	82.9	0.0	383.5	-
140	20.9	10.0	83.7	0.0	397.7	-
145	20.3	9.7	84.4	0.0	411.9	-
150	19.8	9.5	85.1	0.0	426.1	-
155	19.3	9.2	85.8	0.0	440.3	-
160	18.9	9.0	86.4	0.0	454.5	-
165	18.4	8.8	87.1	0.0	468.7	-
170	18.0	8.6	87.7	0.0	482.9	-



Drainage	Area 220
Area (Ha)	0.191
C <sub>100</sub>	0.90
AC	0.172
T <sub>c</sub> (min)	15.0
T incr. (min)	5
Q <sub>1</sub> (l/s)	67.2
Req. vol. (m³)	0.0

Mississauaga	100-year
a=	1450
b=	4.9
C=	0.780

T (min)	l (mm/hr)	Q (l/s)	Total Vol.		Rel. Vol. (m <sup>3</sup> )	Storage (m <sup>3</sup> )
15	140.7	67.2	60.4	0.0	60.4	0.0
20	118.1	56.4	67.7	0.0	80.6	-
25	102.4	48.9	73.3	0.0	100.7	-
30	90.8	43.3	78.0	0.0	120.9	-
35	81.8	39.0	82.0	0.0	141.0	-
40	74.6	35.6	85.4	0.0	161.2	-
45	68.7	32.8	88.5	0.0	181.3	-
50	63.8	30.4	91.3	0.0	201.5	-
55	59.6	28.4	93.8	0.0	221.6	-
60	56.0	26.7	96.2	0.0	241.8	-
65	52.8	25.2	98.3	0.0	261.9	-
70	50.0	23.9	100.3	0.0	282.1	-
75	47.6	22.7	102.2	0.0	302.2	-
80	45.4	21.7	104.0	0.0	322.4	-
85	43.4	20.7	105.7	0.0	342.5	-
90	41.6	19.9	107.2	0.0	362.7	-
95	40.0	19.1	108.8	0.0	382.8	-
100	38.5	18.4	110.2	0.0	403.0	-
105	37.1	17.7	111.6	0.0	423.1	-
110	35.8	17.1	112.9	0.0	443.3	-
115	34.7	16.5	114.2	0.0	463.4	-
120	33.6	16.0	115.4	0.0	483.6	-
125	32.6	15.5	116.6	0.0	503.7	-
130	31.6	15.1	117.7	0.0	523.9	-
135	30.7	14.7	118.8	0.0	544.0	-
140	29.9	14.3	119.9	0.0	564.2	-
145	29.1	13.9	121.0	0.0	584.3	-
150	28.4	13.6	122.0	0.0	604.5	-
155	27.7	13.2	122.9	0.0	624.6	-
160	27.0	12.9	123.9	0.0	644.8	-
165	26.4	12.6	124.8	0.0	664.9	-
170	25.8	12.3	125.7	0.0	685.1	-



#### VOLUME CONTROL CALCULATIONS

Runoff Volume Summary								
Surface typeA (Ha)Depth (mm)Vol. (m³)IA depth (mm)Runoff Vol. (m³)(m³)(m³)(m³)(m³)								
Hardscape	0.317	5	15.9	1	3.2	12.7		
Roof	0.462	5	23.1	1	4.6	18.5		
Green Roof	0.189	5	9.4	5	9.4	0.0		
Total	0.968		48.4		17.2	31.2		



#### **EFFECTIVE TSS REMOVAL** CALCULATIONS

TSS Pre-Treatment Summary							
Drainage	Surface	A (Ha)	Removal	Net for	Treatment	Rate	Effective
Area	Туре	A (Па)	Rate	Treatment	Туре	Kate	Removal
210	Hardscape	0.127	0%	100%		0%	0%
	Rooftops	0.462	95%	5%	-	10%	96%
	Green roof	0.189	100%	0%	-	0%	100%
220	Hardscape	0.191	25%	75%	-	0%	25%
Total		0.968					70%

#### TCC Des Te ~

#### **TSS Removal Summary**

Drainage	Surface	A (Ha)	Removal	Net for	Treatment	Rate	Effective
Area	Туре	A (⊓a)	Rate	Treatment	Туре	Rate	Removal
210	Hardscape	0.127	0%	100%	4	81%	81%
	Rooftops	0.462	95%	5%	1	0%	95%
	Green roof	0.189	100%	0%	2	0%	100%
220	Hardscape	0.191	25%	75%	3	0%	25%
Total		0.968					80%

Treatment Type Legend:

- 1 Inherently clean runoff
- 2 Green roof
- 3 Untreated
- 4 Up-Flo Filter



#### 100-YEAR CAPTURE CALCULATIONS

IDF set: Mississauga							
Return Period	а	T <sub>c</sub>	b	с			
100-year	1450.0	15	4.90	0.780			
Where: $I = \frac{a}{(t_c + b)^c}$							
Driveway Typical Flow							

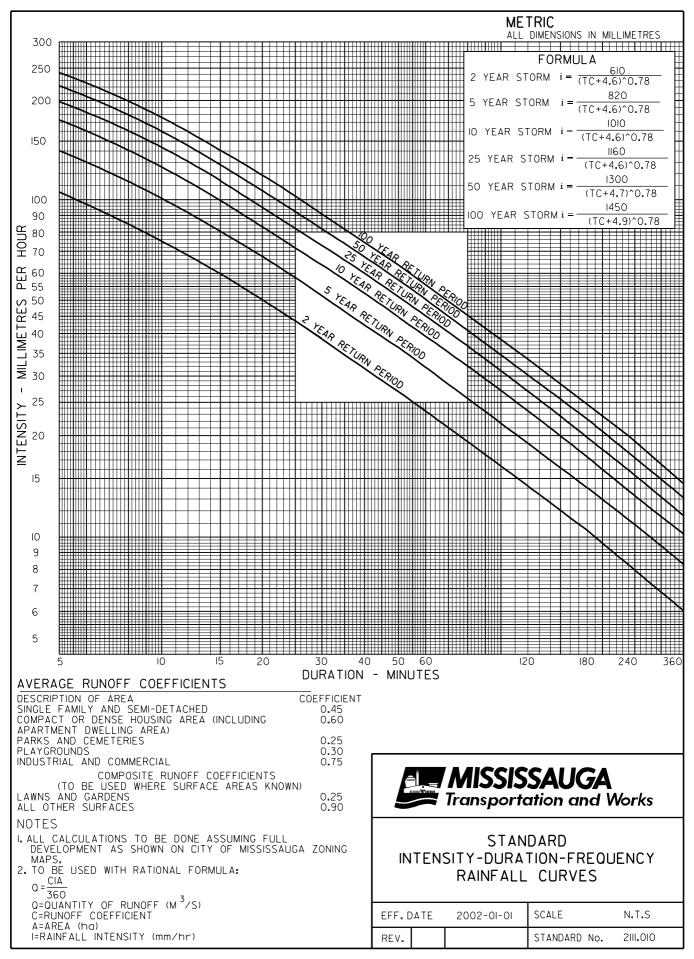
Driveway Typical Flow						
Drainage ID	Area (m <sup>2</sup> )	Composite C	l (mm/hr)*	Q (L/s)		
AD	284	0.90	140.69	10.0		
Where:	$Q = \frac{CIA}{360}$					

$Q_{Orifice} = C_d A (2gh)^{1/2}$			
Туре	PLATE		
Model	Zurn Z662-HF		
Grate Open Area (cm <sup>2</sup> )	665		
1/2 Area* (m <sup>2</sup> )	0.033		
C <sub>d</sub>	0.62		

Drainage ID	AD Elev. (m)	Max W.L.	h (m)	Q <sub>in</sub> (L/s)
AD1 (Zurn Z662)	165.60	165.75	0.15	35.4

\* Assumes 50% blockage





					Location:	21-51 Queent Stree				
Nov+1	ovol				Date:	21-51 Queent Stree	t worth			
STORMWATER N	-evel					2023-07-18				
STORMWATER N	ANAGEMENT				Contact:	sasha Aguilera   Sas	sha@nlsm.ca   647-466	-5595		
18 King Street East, Su	ite 1400, Toronto, ON M5C 1C4	416 637 5772   info@r	nlsm.ca   nlsm.ca							
CALCULAT	IONS - LANDS	CAPE IRRIG	<b>GATION RE</b>	QUIREME	NTS FOR V	<b>VATER RE</b>	USE			
Methodology	Estimate the landscape irrig	gation water needs u	ising the landscape co	pefficient method wit	th the following equa	ations:				
	WR = (ET <sub>0</sub> *K <sub>L</sub> - R <sub>e</sub> ) *A / IE		Equation 1			K <sub>L</sub> = K <sub>S</sub> * K <sub>D</sub> * K <sub>MC</sub>		Equation 2		
	where					where				
	WR = Water Requireme ET <sub>o</sub> = Local Reference E		nm/month)				Coefficient (dimension tor (dimensionless)	ess)		
	K <sub>L</sub> = Landscape Coefficie		ining montunj				tor (dimensionless)			
	R <sub>e</sub> = Effective Rainfall (r		as 25% of average of	ak monthly rainfall			ate Factor (dimensionless)	ess)		
	A = Area (m2)	,		,		-mc microcilli		/		
	IE = Irrigation Efficiency	(dimensionless)								
pecies Factor (K <sub>s</sub> ) -	account for differences in spe		.g. succulents vs. turf	grass.						
	Water Needs	Ks	_							
	Very low	<0.1	-							
	Low	0.1 - 0.3	-							
	Moderate High	0.4 - 0.6 0.7 - 0.9	-							
	пвп	0.7 - 0.5								
ensity Factor (K <sub>D</sub> ) -	account for differences in ve	getation density, e.g	pre-vegetated mat v	s plant plugs.						
	Density	KD	Examples							
	Low	0.5 - 0.9	tree with <70% can							
	Average	1	Groundcover with >							
	High	1.1 - 1.3	Mixed planting type	es or tiered plantings						
diana dina da Farris	W ) and the difference		a bish wind as	an and astrony has the						
viicrociimate Factoi	(K <sub>MC</sub> ) - account for difference Density	es in microclimate, e. K <sub>D</sub>	g. high wind on rooft Examples	op, reflected heat fro	om claddings					
	Low	0.5 - 0.9	shaded or protecter	d from wind						
	Average	0.5 - 0.9	similar to ET <sub>o</sub> cond							
	High	1.1 - 1.4		ing or reflective surfa	aces, exposed to win	ndy conditions				
Reference Evapotra	nspiration (ET <sub>o</sub> ) in July for the			PA WaterSense Wate	er Budget Data Finde	er)				
	ET <sub>0</sub> =		mm							
	R <sub>e</sub> =	16	mm							
				CDC)						
Irrigation Efficiency	(IE) based on average values	of different irrigation	i systems (Source: US	GBC)						
rrigation Efficiency	(IE) based on average values	of different irrigatior	i systems (Source: US	GBC)						
		of different irrigatior	i systems (Source: US	(GBC)						
		of different irrigatior	i systems (Source: US	(BC)						
		of different irrigatior	systems (Source: US				Landscape			
Water Requirem			Species Factor K <sub>s</sub>		Microclimate	Landscape	Landscape Evapotranspiration	Irrigation Type	Irrigation Efficiency	
	ent Calculations	of different irrigation		Density Factor K <sub>D</sub>	Microclimate Factor K <sub>MC</sub>	Landscape Coefficient K <sub>L</sub>	Landscape Evapotranspiration ET <sub>L</sub> (mm/month)	Irrigation Type	Irrigation Efficiency IE	
Water Requirem	ent Calculations						Evapotranspiration	Irrigation Type Drip		
Water Requirem Landscape Type Landscape Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0 315.0	Species Factor K <sub>S</sub> 0.5 0.7	Density Factor K <sub>D</sub>	Factor K <sub>MC</sub>	Coefficient K <sub>L</sub> 0.55 0.84	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121	Drip Drip	IE 0.8 0.8	
Water Requirem Landscape Type Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0	Species Factor K <sub>s</sub>	Density Factor K <sub>D</sub>	Factor K <sub>MC</sub>	Coefficient K <sub>L</sub> 0.55	Evapotranspiration ET <sub>L</sub> (mm/month) 79	Drip	IE 0.8	
Water Requirem Landscape Type Landscape Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0 315.0	Species Factor K <sub>S</sub> 0.5 0.7	Density Factor K <sub>D</sub>	Factor K <sub>MC</sub> 1.1 1.2 1.2	Coefficient K <sub>L</sub> 0.55 0.84 0.72	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121 103	Drip Drip Drip	IE 0.8 0.8 0.8	
Water Requirem Landscape Type Landscape Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0 315.0	Species Factor K <sub>5</sub> 0.5 0.7 0.6	Density Factor K <sub>D</sub> 1 1 Trees/	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs	Coefficient K <sub>L</sub> 0.55 0.84 0.72	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121 103	Drip Drip Drip Alpine I	IE 0.8 0.8 0.8 0.8	Total
Vater Requirem Landscape Type Landscape Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0 315.0	Species Factor K <sub>S</sub> 0.5 0.7 0.6	Density Factor K <sub>D</sub> 1 1 1 Vertex Vert	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I)	Coefficient K <sub>L</sub> 0.55 0.84 0.72 WR (m <sup>3</sup> )	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121 103 Sod WR (I)	Drip Drip Drip Alpine I WR (m <sup>3</sup> )	IE 0.8 0.8 0.8	WR (m <sup>3</sup> )
Vater Requirem Landscape Type Landscape Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0 315.0	Species Factor K <sub>5</sub> 0.5 0.7 0.6	Density Factor K <sub>0</sub> 1 1 Trees/. WR (m <sup>3</sup> ) 59.0	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I) 58,951	Coefficient K <sub>L</sub> 0.55 0.84 0.72 WR (m <sup>3</sup> ) 29.2	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121 103 Sod WR (I) 29,249	Drip Drip Drip Malpine I WR (m <sup>3</sup> ) 113.8	IE 0.8 0.8 0.8 <b>Aeadow</b> WR (I) 113,796	WR (m <sup>3</sup> ) 202.0
Vater Requirem Landscape Type Landscape Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0 315.0	Species Factor K <sub>S</sub> 0.5 0.7 0.6	Density Factor K <sub>D</sub> 1 1 1 Vertex Vert	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I) 58,951 75,156	Coefficient K <sub>L</sub> 0.55 0.84 0.72 WR (m <sup>3</sup> )	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121 103 Sod WR (I) 29,249 36,369	Drip Drip Drip Alpine I WR (m <sup>3</sup> )	IE 0.8 0.8 0.8 Meadow WR (I) 113,796 142,537	WR (m <sup>3</sup> ) 202.0 254.1
Water Requirem Landscape Type Landscape Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0 315.0	Species Factor Ks 0.5 0.7 0.6	Density Factor K <sub>0</sub> 1 1 Trees/' WR (m <sup>3</sup> ) 59.0 75.2	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I) 58,951	Coefficient K <sub>L</sub> 0.55 0.84 0.72 WR (m <sup>3</sup> ) 29.2 36.4	Evapotranspiration ET <sub>4</sub> (mm/month) 79 121 103 Sod WR (I) 29,249 36,369 41,115	Drip Drip Drip Alpine I WR (m <sup>3</sup> ) 113.8 142.5	IE 0.8 0.8 0.8 <b>Aeadow</b> WR (I) 113,796	WR (m <sup>3</sup> ) 202.0
Vater Requirem Landscape Type Landscape Landscape	System Name Trees/Shrubs Sod	Area (m <sup>2</sup> ) 1095.0 315.0	Species Factor K <sub>5</sub> 0.5 0.7 0.6	Density Factor K <sub>0</sub> 1 1 Tress/7 WR (m <sup>3</sup> ) 59.0 75.2 86.0	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I) 58,951 75,156 85,960	Coefficient K <sub>L</sub> 0.55 0.84 0.72 WR (m <sup>3</sup> ) 29.2 36.4 41.1	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121 103 sod WR (I) 29,249 36,369 41,115 36,369	Drip Drip Drip MR (m <sup>3</sup> ) 113.8 142.5 161.7	IE 0.8 0.8 0.8 Meadow WR (I) 113,796 142,537 161,698	WR (m <sup>3</sup> ) 202.0 254.1 288.8
Vater Requirem Landscape Type Landscape Landscape	ent Calculations System Name Trees/Shrubs Sod Alpine Meadow	Area (m <sup>2</sup> ) 1095.0 3315.0 1483.5	Species Factor K <sub>5</sub> 0.5 0.7 0.6 Irrigation Month May June July August	Density Factor K <sub>0</sub> 1 1 Trees/ WR (m <sup>3</sup> ) 59.0 75.2 59.0	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I) 58,951 75,156 85,960 75,156 58,951	Coefficient K <sub>L</sub> 0.55 0.84 0.72 WR (m <sup>3</sup> ) 29.2 36.4 41.1 36.4 29.2	Evapotranspiration ET <sub>i</sub> (mm/month) 79 121 103 Sod WR (I) 29,249 36,369 41,115 36,369 29,249	Drip Drip Drip WR (m <sup>3</sup> ) 113.8 142.5 161.7 142.5 113.8	IE 0.8 0.8 0.8 Meadow WR (I) 113,796 142,537 161,698 142,537 113,796	WR (m <sup>3</sup> ) 202.0 254.1 288.8 254.1 202.0
Water Requirem Landscape Type Landscape Landscape	Ent Calculations System Name Trees/Shrubs Sod Alpine Meadow Total irrigation water use p	Area (m <sup>2</sup> ) 1095.0 315.0 1483.5 1483.5	Species Factor K <sub>5</sub> 0.5 0.7 0.6 Irrigation Month May June July August	Density Factor K <sub>0</sub> 1 1 1 1 WR (m <sup>3</sup> ) 59.0 75.2 86.0 75.2 59.0 354.2	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I) 58,951 75,156 85,960 75,156 58,951 58,951 354,172	Coefficient K, 0.55 0.84 0.72 29.2 36.4 41.1 36.4 29.2 36.4 29.2 172.3	Evapotranspiration ET <sub>4</sub> (mm/month) 79 121 103 Sod WR (I) 29,249 36,369 41,115 36,369 29,249 172,350	Drip Drip Drip WR (m <sup>3</sup> ) 113.8 142.5 161.7 142.5 113.8 674.4	IE 0.8 0.8 0.8 VR (I) 113,796 142,537 161,698 142,537 113,796 674,366	WR (m <sup>3</sup> ) 202.0 254.1 288.8 254.1 202.0 1,200.9
Water Requirem Landscape Type Landscape Landscape	System Name         Trees/Shrubs         Sod         Alpine Meadow	Area (m <sup>2</sup> ) 1095.0 315.0 1483.5 per year se per month	Species Factor K <sub>5</sub> 0.5 0.7 0.6 Irrigation Month May June July August	Density Factor K <sub>0</sub> 1 1 Trees/7 WR (m <sup>3</sup> ) 59.0 75.2 86.0 0 75.2 59.0 354.2 70.8	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I) 58,951 75,156 85,960 75,156 58,951 	Coefficient K <sub>1</sub> 0.55 0.84 0.72 WR (m <sup>3</sup> ) 29.2 36.4 41.1 36.4 29.2 172.3 34.5	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121 103 30 00 29,249 36,369 41,115 36,369 29,249 172,350 34,470	Drip Drip Drip WR (m <sup>3</sup> ) 113.8 142.5 161.7 142.5 113.8 142.5 113.8	IE 0.8 0.8 0.8 WR (I) 113,796 142,537 161,698 142,537 113,796 743,656 134,873	WR (m <sup>3</sup> ) 202.0 254.1 288.8 254.1 202.0 1,200.9 240.2
Water Requirem Landscape Type Landscape Landscape	Ent Calculations System Name Trees/Shrubs Sod Alpine Meadow Total irrigation water use p	Area (m <sup>2</sup> ) 1095.0 3315.0 1483.5 1483.5 per year se per month se for 72 hours	Species Factor K <sub>5</sub> 0.5 0.7 0.6 Irrigation Month May June July August	Density Factor K <sub>0</sub> 1 1 1 1 WR (m <sup>3</sup> ) 59.0 75.2 86.0 75.2 59.0 354.2	Factor K <sub>MC</sub> 1.1 1.2 1.2 Shrubs WR (I) 58,951 75,156 85,960 75,156 58,951 58,951 354,172	Coefficient K, 0.55 0.84 0.72 29.2 36.4 41.1 36.4 29.2 36.4 29.2 172.3	Evapotranspiration ET <sub>L</sub> (mm/month) 79 121 103 500 WR (I) 29,249 36,369 41,115 36,369 29,249 172,350 34,470 3,379	Drip Drip Drip WR (m <sup>3</sup> ) 113.8 142.5 161.7 142.5 113.8 674.4	IE 0.8 0.8 0.8 WR (I) 113,796 142,537 161,698 142,537 113,796 743,656 134,873	WR (m <sup>3</sup> ) 202.0 254.1 288.8 254.1 202.0 1,200.9



# **ADS UFF Sizing Summary**

Project Name:	Mississauga Project		
Consulting Engineer:	Siteplantech Inc		
Location:	Mississauga, ON		
Sizing Completed By:	Haider Nasrullah	Email:	haider.nasrullah@ads-pipe.com

Recommended Unit			
Recommended Model:	UFF-3		
TSS Removal Percentage:	81.1%		
Total Site Volume Treated:	90.2%		

Site Details				
Site Area:	0.23 ha			
% Impervious:	100%			
Rational C:	0.90			
Rainfall Station:	Toronto, ONT			
Particle Size Distribution:	ETV / NJDEP			

Unit Specifications:			
Number of Filter Modules:	3		
Maximum Treatment Flowrate:	4.8 L/s		
Inlet - Outlet Drop:	240 mm		
Max. Pipe Diameter:	600 mm		
Operating Head:	760 mm		

Site Elevat	ions:
Rim Elevation:	0.00
Inlet Pipe Elevation:	0.00
Outlet Pipe Elevation:	0.00

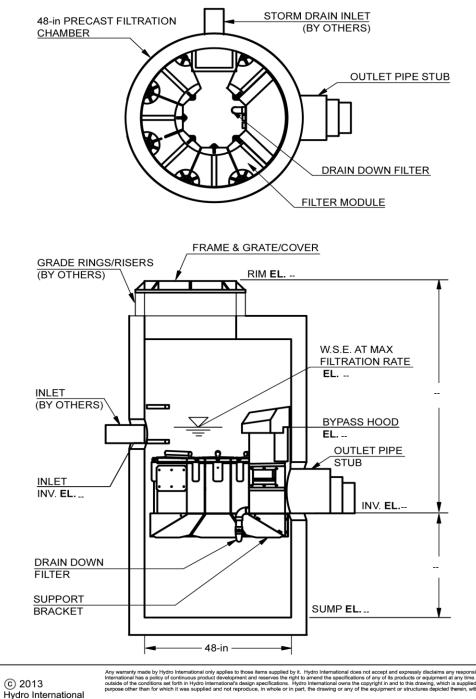
Consult approved shop drawings for final elevations. Riser sections (and/or grade rings) may be required to reach final grade on site.

Removal efficiencies are based on NJDEP Test Protocols and independently verified.

All units supplied by ADS have numerous local, provincial, and international certifications (copies of which can be provided upon request). The design engineer is responsible for ensuring compliance with applicable regulations.

Rainfall Intensity <sup>(1)</sup>	Fraction of Rainfall <sup>(1)</sup>	Removal Efficiency <sup>(2)</sup>	Weighted Net- Annual Removal Efficiency
mm/hr	%	%	%
0.50	0.2%	92.3%	0.2%
1.00	14.8%	91.4%	13.5%
1.50	15.1%	90.4%	13.6%
2.00	13.6%	89.5%	12.2%
2.50	3.9%	88.6%	3.5%
3.00	1.3%	87.7%	1.1%
3.50	8.9%	86.7%	7.7%
4.00	5.3%	85.8%	4.5%
4.50	1.2%	84.9%	1.0%
5.00	5.2%	84.0%	4.3%
6.00	4.2%	82.1%	3.5%
7.00	4.6%	80.3%	3.7%
8.00	3.1%	78.4%	2.4%
9.00	2.3%	76.6%	1.7%
10.00	2.2%	74.7%	1.6%
20.00	9.3%	56.2%	5.2%
30.00	2.7%	37.7%	1.0%
40.00	1.1%	19.2%	0.2%
50.00	0.5%	0.7%	0.0%
100.00	0.6%	0.0%	0.0%
150.00	0.1%	0.0%	0.0%
			<b>A</b> 4 101
	nnual Trea	81.1%	
Total Rui	90.2%		

Rainfall Data: 1953:2007, HLY03, Toronto , ON, 6158350 & 6158355



Treatment System Specifica	tions
Filtration Chamber Diameter (DIA)	
No. Filter Modules	
Max.Filtration Rate Per Filter Module	
Peak Internal Bypass Flow Rate	
Operating Head at Max. Filtration Rate	
Sediment Storage	
Oil Storage	
Outlet Pipe Diameter (Max.15-in)	

#### **Specification Requirements:**

CAPACITIES:

- 1. Minimum performance: 80% removal of Sil-Co-Sil 106 (d50=22 microns) at the max. filtration rate.
- 2. Maximum number of modules for vault size: 6

3. Peak treatment flow: --

#### ADDITIONAL DESIGN INFORMATION:

- 1. Normal operating W.S.E. is 29.5" (2.46') above the outlet invert at the max. filtration rate. For a given flow the head requirement can be reduced by adding additional Filter Modules.
- 2. Treatment flows that require more than 6 modules will require a larger vault design.
- 3. Drop required from inlet pipe invert to outlet pipe invert is 9".
- 4. Filter Media:

#### **Detail Notes:**

Outside Diameter: 10.5", 12.5" or 15.3" OD Concrete Penetration: Pipe Boot (by Hydro) Hook-up: Fernco-type coupling (by others)

#### DO NOT USE FOR CONSTRUCTION **OR FABRICATION**

#### 1. THIS IS A STANDARD DETAIL AND IS NOT SITE SPECIFIC. ACTUAL INLET PIPE DIAMETER AND ANGLE MAY BE DIFFERENT THAN SHOWN. 2. REFER TO SUBMITTAL OR FABRICATION DRAWINGS FOR FINAL RIM AND INVERT ELEVATIONS. 3. CONTACT HYDRO INTERNATIONAL FOR SITE SPECIFIC DRAWINGS AND INSTALLATION REQUIREMENTS. **REVISION HISTORY** REV BY DATE DESCRIPTION A JL 5/23/13 PARTS LIST Date Scale 03/30/12 3/8" = 1'0" Checked Approved Drawn MJ 4-FT DIAMETER **UP-FLO® FILTER** Hydro S Stormwater Solutions 94 Hutchins Drive Portland, Maine 04102 Tel: (207) 756-6200 Fax: (207) 756-6212 stormwateringuiry@hydro-int.com

Notes

Any warranty made by Hydro International only applies to those items supplied by it. Hydro International does not accept and expressly disclaims any responsibility or liability for any structure, plant or equipment (or the performance thereof) designed, built, manufactured or supplied by any third-party. Hydr International has a policy of continuous product development and reserves the right to amend the specifications of any of its products or equipment at any time. Hydro International expressly disclaims any liability for the performance of its equipment (or ran y and thereof) used or made subject to conditions outside of the conditions set forth in Hydro International expression of the cavity in the subject or conditions of the subject or conditions of the subject or conditions at the CAD Ref: SIZING CALC DWG Project No. purpose other than for which it was supplied and not reproduce, in whole or in part, the drawing or any of the equipment or structures depicted therein, without prior written permission of Hydro Interr DrawingNo. Rev. A



#### State of New Jersey

Division of Water Quality Bureau of Nonpoint Pollution Control 401 East State Street P.O. Box 420 Mail Code 401-02B Trenton, New Jersey 08625-0420 Phone: 609-633-7021 / Fax: 609-777-0432 http://www.state.nj.us/dep/dwq/bnpc\_home.htm CATHERINE R. McCABE Commissioner

August 15, 2018

David Scott, CPSWQ Technical Product Manager Hydro International 94 Hutchins Drive Portland, ME 04102

Re: MTD Laboratory Certification Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media by Hydro International Off-line Installation

#### **TSS Removal Rate 80%**

Dear Mr. Scott:

The Stormwater Management rules under N.J.A.C. 7:8-5.5(b) and 5.7(c) allow the use of manufactured treatment devices (MTDs) for compliance with the design and performance standards at N.J.A.C. 7:8-5 if the pollutant removal rates have been verified by the New Jersey Corporation for Advanced Technology (NJCAT) and have been certified by the New Jersey Department of Environmental Protection (NJDEP). Hydro International has requested a Laboratory Certification for the Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media.

This project falls under the "Procedure for Obtaining Verification of a Stormwater Manufactured Treatment Device from New Jersey Corporation for Advanced Technology" dated January 25, 2013. The applicable protocol is the "New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device" dated January 25, 2013.

NJCAT verification documents submitted to the NJDEP indicate that the requirements of the aforementioned protocol have been met or exceeded. The NJCAT letter also included a recommended certification TSS removal rate and the required maintenance plan. The NJCAT Verification Report with the Verification Appendix (dated June 2018) for this device is published online at http://www.njcat.org/uploads/newDocs/UPFLO450RVerificationReportFinal.pdf.

PHILIP D. MURPHY Governor

SHEILA Y. OLIVER Lt. Governor

# The NJDEP certifies the use of the Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media by Hydro International at a TSS removal rate of 80%, when designed, operated and maintained in accordance with the information provided in the Verification Appendix and subject to the following conditions:

- 1. The maximum treatment flow rate (MTFR) for the manufactured treatment device (MTD) is calculated using the New Jersey Water Quality Design Storm (1.25 inches in 2 hrs) in N.J.A.C. 7:8-5.5. The MTFR is calculated based on a verified loading rate of 0.533 gpm/sf of effective filtration treatment area.
- 2. The Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media shall be installed using the same configuration as the unit verified by NJCAT and sized in accordance with the criteria specified in item 6 below.
- 3. This device cannot be used in series with another MTD or a media filter (such as a sand filter), to achieve an enhanced removal rate for total suspended solids (TSS) removal under N.J.A.C. 7:8-5.5.
- 4. Additional design criteria for MTDs can be found in Chapter 9.6 of the New Jersey Stormwater Best Management Practices (NJ Stormwater BMP) Manual which can be found on-line at <u>www.njstormwater.org</u>.
- 5. The maintenance plan for a site using this device shall incorporate, at a minimum, the maintenance requirements for the Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media, which is attached to this document. However, it is recommended to review the maintenance website at

<u>https://www.hydro-int.com/sites/default/files/nj\_uff\_inspection\_and\_maintnenance.pdf</u> for any changes to the maintenance requirements.

6. Sizing Requirements:

The example below demonstrates the sizing procedure for an Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media. After determining the number of filter modules necessary, the corresponding model selection must be appropriate to hold at least that minimum number of filters.

Example: A 0.25-acre impervious site is to be treated to 80% TSS removal using an Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media. The impervious site runoff (Q) based on the New Jersey Water Quality Design Storm was determined to be 0.79 cfs or 354.58 gpm.

The selection of configuration for use in the Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media is based upon both the MTFR and the maximum inflow drainage area. It is necessary to select the configuration using both methods and to rely on the method that results in the larger configuration determined by the two methods.

#### Inflow Drainage Area Evaluation:

The drainage area to the Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media in this example is 0.25 acres. Based upon the information in Tables 1 and 2 below, the following minimum configuration is required for an Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media to treat the impervious area without exceeding the maximum drainage area:

Drainage area = 0.25 acres Max Allowable Inflow Area per Filter Module = 0.0245 acres/filter (Table 2 below) 0.25/0.0245 = 10.2 Filter Modules = 11 Filter Modules

Using Table 1 below, Model size UFF-ZV-25-450R with 11 filter modules and maximum allowable inflow drainage area of 0.27 acres may be used.

#### Maximum Treatment Flow Rate (MTFR) Evaluation:

The site runoff (Q) was determined based on the following: time of concentration = 10 minutes i=3.2 in/hr (page 5-8, Fig. 5-3 of the NJ Stormwater BMP Manual) c=0.99 (runoff coefficient for impervious) Q=ciA=0.99x3.2x0.25=0.79 cfs=0.79x448.83 gpm/cfs=354.58 gpm

Based on a flow rate of 354.58 gpm, the following minimum configuration is required for an Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media to treat the impervious area without exceeding the MTFR:

Flow rate = 354.58 gpm Max. Flow Rate per Filter Module = 10 gpm/Filter Module (Table 2 below) 354.58/10 = 35.46 Filter Modules = 36 Filter Modules

Using Table 1 below, Model size UFF-MH-25-450R with 36 filter modules, which would have an MTFR of 360 gpm, may be used.

The MTFR evaluation results will be used since that method results in the higher minimum configuration determined by the two methods.

The sizing table corresponding to the available system models are noted below:

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Configuration	Model Size	Maximum Number of Filter Modules	Max. Filtration Rate (gpm)	Minimum Sedimentation Area (sq.ft.)	Minimum Wet Volume (cu.ft.)	Total Filtration Area (sq.ft.)	Total Mass Capture (lbs)	Maximum Allowable Inflow Area (acres)
Manhole	UFF-MH-450R	6	60	12.48	48.6	112.5	88.0	0.15
Vault	UFF-ZV-25-450R	50	500	104	405	937.5	733	1.22
Vault	UFF-ZV-50-450R	100	1000	208	810	1875	1466	2.44
Vault	UFF-ZV-75-450R	150	1500	312.0	1215	2813	2199	3.67

Table 1: Up-Flo<sup>®</sup> Filter with 450R Filter Ribbon Media Configurations and NJDEP Sizing Table

 Table 2: Up-Flo<sup>®</sup> with 450R Filter Ribbon Media Design Specifications

Ribbon Model	Max. Flow per Filter Module (gpm/cfs)	Max. Allowable Inflow Area per Filter Module (acres)
450R	10/0.022	0.0245

Be advised a detailed maintenance plan is mandatory for any project with a Stormwater BMP subject to the Stormwater Management Rules, N.J.A.C. 7:8. The plan must include all of the items identified in Stormwater Management Rules, N.J.A.C. 7:8-5.8. Such items include, but are not limited to, the list of indication of problems in the system, and training of maintenance personnel. Additional information can be found in Chapter 8: Maintenance and Retrofit of Stormwater Management Measures.

If you have any questions regarding the above information, please contact Nicholas Grotts of my office at (609) 633-7021.

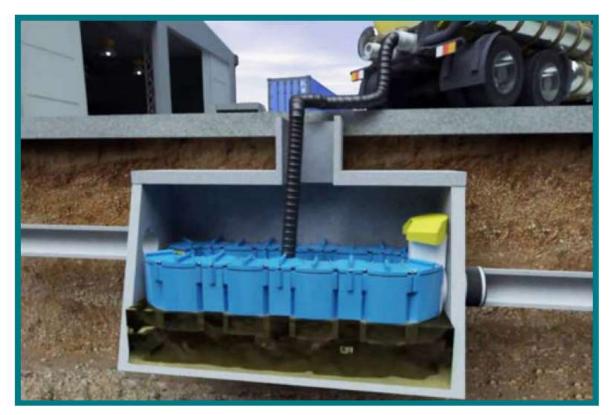
Sincerely,

Yames J. Murphy, Chief Bureau of Nonpoint Pollution Control

Attachment: Maintenance Plan

cc: Chron File Richard Magee, NJCAT Vince Mazzei, NJDEP - DLUR Ravi Patraju, NJDEP - BES Gabriel Mahon, NJDEP - BNPC Brian Salvo NJDEP - BNPC Nicholas X. Grotts NJDEP - BNPC





# **Operation and Maintenance Manual**

#### Stormwater Solutions

#### Up-Flo® Filter

Filtration System for Stormwater Treatment

94 Hutchins Drive Portland, ME 04102

Tel: (207) 756-6200 Fax: (207) 756-6212 stormwaterinquiry@hydro-int.com

www.hydro-int.com



### **Overview & Product Description**

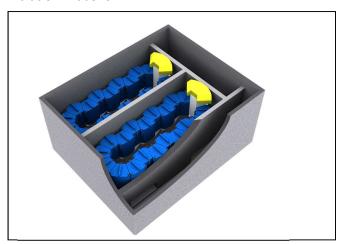
DON'T WANT TO GO IT ALONE? CALL HYDRO AND WE'LL TAKE CARE OF INSPECTION, REPLACEMENT MEDIA AND CLEANOUT.

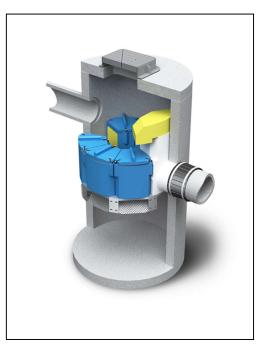
CALL 1 (888) 382-7808 FOR A QUOTE

The Up-Flo<sup>®</sup> Filter is a modular high-rate stormwater filtration device designed to capture trash, oil, sediment and remove fine pollutants such as dissolved and particulate metals and nutrients from stormwater runoff. In general, a minimum of two inspections are required per year to monitor sediment and gross pollutant accumulations.

In order to sustain expected flow and removal rates for the Up-Flo<sup>®</sup> Filter, annual replacement of the Media Pack and removal of accumulated sediment from the sump is required. Depending on site use and pollutant characteristics, annual rainfall, design and functionality of the stormdrain conveyance system, annual replacement and clean out may be more or less often.

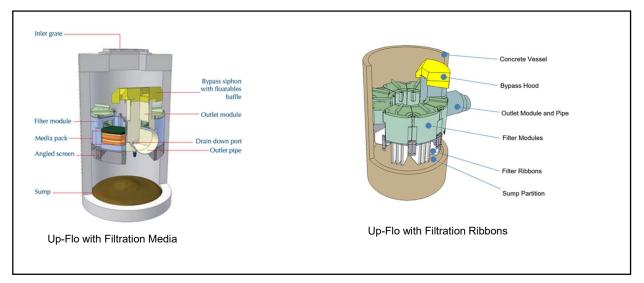
The Up-Flo Filter has modular components that connect together to form a ring of 1-6 Filter Modules or linearly to fit into rectangular precast structures with filter bays. Each filter bay can house 1-19 Filter Modules and precast structures can be constructed with multiple filter bays. Each Filter Module will have either a filtration Media Pack or filtration Ribbons.







It does not matter what type of media is used, the Filter Modules house the filtration medium and the precast structure is used to suspend the Filter Modules to provide a sedimentation sump. Stainless steel support frames are used to support the Filter Modules and attach them to the precast structure. An Outlet Module (with hood) is used to connect the Filter Modules to a discharge pipe and convey filtered water away from the treatment area. A Draindown Filter and screen are provided when filtration media is used but not with filtration Ribbons.



Maintenance activities can be categorized by those that can be performed from outside the Up-Flo<sup>®</sup> vessel and those that are performed inside the vessel. Maintenance performed from outside the vessel includes removal of floatables and oils that have accumulated on the water surface and removal of sediment from the sump. Maintenance performed inside the vessel includes removal and replacement of Media Packs (Filter Bags, flow Distribution Media and Draindown) or filtration Ribbons. A vactor truck is required for removal of oils, water, sediment, and to enter the vessel for performing inside maintenance. OSHA Confined Space Entry procedures need to be followed when entering the Up-Flo<sup>®</sup> vessel.

#### Inspection

The frequency of inspection and maintenance can be determined in the field after installation. Based on site characteristics such as contributing area, types of surfaces (e.g., paved and/or landscaped), site activities (e.g., short-term or long-term parking), and site maintenance (e.g., sanding and sweeping), inspection and maintenance should be conducted at intervals of no more than six months during the first year of operation. Typically, maintenance is recommended once per year thereafter.



By removing the manhole cover during a storm and monitoring the water level in the manhole or vault, site personnel can determine whether the filter is in bypass. A properly-sized filter that is in bypass during a storm that is producing runoff at, or below, the filter's design filtration rate needs maintenance. Otherwise, scheduled inspections will determine when one or more of the following maintenance thresholds have been reached:

Sediment depth at sump storage capacity. Up-Flo Filter with Filtration Media - Minimum 8"

- should separate the Draindown filter inlet from stored sediment in the sump. Up-Flo® Filter with Ribbon 285R Minimum 6" should separate the bottom of the filtration Ribbons and sump floor. Up-Flo® Filter with Ribbon 450R Minimum 1" should separate the bottom of the filtration Ribbons and sump floor. A simple probe, such as the Sludge-Judge®, can be used to determine the depth of the solids in the sump.
- Clogging of the Media Bags. Minimum filtration rate is generally reached when: Up-Flo® Filter with Filtration Media have accumulated approximately 20 lbs of sediment. Up-Flo® Filter with Ribbon 285R have accumulated approximately 8 lbs of sediment. Up-Flo® Filter with Ribbon 450R have accumulated approximately 15 lbs of sediment. Determining the amount of accumulated sediment will be accomplished by removing both of the Media Bags from one of the Media Packs and weighing the bags separately or removing the filter Ribbon assembly for weighing. A spent Media Bag weighs approximately 50 lbs wet. A 285R filter Ribbon assembly from one module weighs approximately 15 lbs wet and a 450R filter Ribbon assembly from one module weighs approximately 30 lbs.
- Draindown filter clogged. With modules supplied with filtration media, the Drain Down Filter is designed to lower the water level in the Up-Flo<sup>®</sup> vessel to an elevation below the bottom of the Filter Modules between storm events. If inspection one to two days after a storm event indicates otherwise, the Drain Down Filter has likely become clogged with sediment.
- Slime and debris covering the flow distribution media, angled screens or filtration Ribbons. After removal of the Media Bags or filtration Ribbons, the bottom flow distribution media should be removed and inspected to determine if it is coated with slime or debris. Similarly, the angled screen should be inspected for blockages and ragging.
- Oil forming a measureable thickness on the surface of the water. Since water in the Up-Flo<sup>®</sup> vessel drains down to an elevation below the bottom of the Filter Modules when the system is idle, the amount of accumulated oils must be minimized so that oils are not entrained into the Media Pack when stormwater begins to fill the vessel at the start of a storm event.
- Floatables completely covering the surface of the water. Similar to oils, the amount of accumulated floatables must be minimized to prevent trash and loose debris from becoming trapped on the angled screens when stormwater begins to fill the Up-Flo<sup>®</sup> vessel at the start of a storm event.



The site-specific solids loading rate in the sump and in the Media Packs will be determined during the first year of Up-Flo<sup>®</sup> Filter operation. Starting with a clean sump, the solids loading rate in the sump will be calculated by measuring the sediment depth in the sump and dividing the depth by the correlating interval of time since it was cleaned. Similarly, starting with fresh Media Bags or Ribbons, the solids loading rate in the Media Packs and Ribbons will be calculated by weighing the Media Bags or Ribbons and dividing the weights by the respective time interval since they were installed. The wet weight of the heaviest bag or Ribbon assembly from a single module will be used to determine the loading rate.

After completion of the first year of operation, the inspection and maintenance intervals for cleaning the sump and replacing Media Bags or Ribbons will be established to keep the solids loading within the respective limits of the sump and filter medium. Replacement of the Draindown Filter, replacement of flow Distribution Media, and removal of oils and floatables will occur at the same frequency unless the first year of operation indicates otherwise. Keeping to the established maintenance intervals will keep treatment flow rates at, or above, the design flow rate.

#### Maintenance

The access port located at the top of the manhole or vault provides access to the Up-Flo<sup>®</sup> vessel for maintenance personnel to enter the vessel and comfortably remove and replace Media Packs or Ribbon assemblies. The same access would be used for maintenance personnel working from the surface to net or skim debris and floatables or to vactor out sediment, oil, and water. Unless the Up-Flo<sup>®</sup> Filter has been installed in a very shallow unit, it is necessary to have personnel with OSHA-confined space entry performing the maintenance that occurs inside the vessel.

Maintenance activities include inspection, floatables removal, oil removal, sediment removal, Media Pack and Ribbon assembly replacement, and Draindown Filter replacement. Filtration medium housed in the Filter Modules is easily accessed by loosening three latches used to secure the Filter Module Lid. Maintenance intervals are determined from monitoring the Up-Flo<sup>®</sup> Filter during its first year of operation. Depending on the site, some maintenance activities may have to be performed on a more frequent basis than others. In the case of floatables removal, a vactor truck is not required. Otherwise, a vactor truck is normally required for oil removal, removal of sediment from the sump, and to dewater the vessel for replacement of the Media Packs and Draindown Filter. All inspection and maintenance activities would be recorded in an Inspection and Maintenance Log.

Good housekeeping practices upstream of the Up-Flo<sup>®</sup> Filter can significantly extend Media Bag life. For example, sweeping paved surfaces, collecting leaves and grass trimmings, and protecting bare ground from the elements will reduce loading to the system. Media Packs should not be installed in the Filter Modules until construction activities are complete and site stabilization is effective.



### **Up-Flo Filter Inspection & Maintenance Logs**

SITE REFERENCE NAME OR NUMB	ER FOR THIS UP-FLO® FILTER LOCATION:
SITE NAME:	
SITE LOCATION:	
OWNER:	SITE CONTRACTOR:
CONTACT NAME:	CONTACT NAME:
COMPANY NAME:	COMPANY NAME:
ADDRESS:	ADDRESS:
TELEPHONE:	TELEPHONE:
FAX:	FAX:

INSTALLATION DATE: / /

CONFIGURATION (CIRCLE ONE): MANHOLE VAULT SYSTEM

TOTAL NUMBER OF UP-FLO® FILTER MODULES:



#### **UP-FLO®** FILTER INSPECTION LOG

Site Name:		Owner Change since last inspection? Y N
Location:		<u></u>
Owner Name:		
Address:		Phone Number:
Site Status:		
Date:	Time:	Site conditions*:

Inspection Frequency Key: A=annual; M=monthly; S=after major storms

Inspection Items	Inspection Frequency	Inspected? (Yes/No)	Maintenance Needed? (Yes/No)	Comments/Description
Debris Removal				
Adjacent area free of debris?	M			
Inlets and Outlets free of debris?	M			
Facility (internally) free of debris?	M			
Vegetation			· ·	
Surrounding area fully stabilized? (no evidence of eroding material into Up-Flo® Filter)	A			
Grass mowed?	M			
Water retention where required		10		12. 191
Water holding chamber(s) at normal pool?	A			
Evidence of erosion?	A			
Sediment Deposition				
Filtration Chamber free of sediments?	A			
Sedimentation sump not more than 50% full?	A			
Structural Components				- X
Any evidence of structural deterioration?	A			
Grates in good condition?	A			
Spalling or cracking of structural parts?	A			
Outlet/Overflow Spillway	A			
Other	2.4		1.v.	
Noticeable odors?	A			
Any evidence of filter(s) clogging?	M	1		
Evidence of flow bypassing facility?	A			



Inspector Comments:		
Overall Condition of Up-Flo® Filter**:	Acceptable	Unacceptable
**"Acceptable" would mean properly fu	nctioning; "unacceptable" wo	ould mean damaged or required further maintenance.
		ance Needed", list Maintenance actions and their completion dates
below or on the Maintenance Log provi	ded on page 15 of the Up-Fl	lo® Filter Operation & Maintenance Manual:

Maintenance Action Needed	Due Date

The next routine inspection is schedule for approximately: (date)

Inspected by: (signature)

Inspected by: (printed)



#### UP-FLO® FILTER MAINTENANCE LOG

Site Name:			Owner Change since last inspection? Y N
Location:			
Owner Name:	2		
Address:			Phone Number:
Site Status:			
Date:	Time:		
		*(Stable, Under	Construction, Needing Maintenance, etc.)
Estimated volu	me of oil/floatable trash	removed:	
Sediment dept	h measured in sump pri	or to removal:	
Number of Filte	er Modules fitted with ne	ew media packs:	
			12
Inspector Com	iments:		17
5			
2		211-210	
Overall Condit	ion of Up-Flo® Filter:	Acceptable	Unacceptable
**"Acceptable"	' would mean properly fi	unctioning; "unacceptable" w	ould mean damaged or required further maintenance.
Maintained by:	: (signature)		
Maintained by	(printed)		

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Appendix C

Sanitary Data

#### SANITARY FLOW CALCULATIONS

	E	xisting Flow	S	
Commercial Flow Det				
Site area	ermination			0.97 Ha
Population eq.	50 PPU / Ha			48 POP
Harmon Peaking Fac				4.3
Average flow				308.2 L/c/d
Existing Peak Flow				0.7 L/s
Existing Feak flow				0.7 4/3
I/I Flow Determinatio	n			
Site Area				0.97 ha
Infiltration (22,500 L/da	ay/ha or 0.26 L/s/ha)			0.3 L/s
Total Existing Peak Fl	ow (Pop. Eq. <1,000)			1.0 L/s
	Drono	sed Develop	mont	
	Γιορο	sed Develop	ment	
Commercial Populati	on			2
Commercial GFA				1,424 m <sup>2</sup>
Population eq.	50 PPU / Ha			7 Persons
Residential Populatio	n			
	Unit type	<u>No. Unit</u>	<u>Pop. / Unit</u>	Population
	Studio (<750 ft <sup>2</sup> )	175	1.6	280
	1 Bdrm (<750 ft <sup>2</sup> )	189	1.6	302
	2 Bdrm (<750 ft <sup>2</sup> )	76	1.6	122
	2 Bdrm (>750 ft <sup>2</sup> )	2	3.0	6
	3 Bdrm (>750 ft <sup>2</sup> )	2	3.0	6
	Total	444	5.0	716 Persons
Sanitary Flow Determ	nination			722 Deveces
Total population				723 Persons
Eq. Pop/ha	4			747 Pop/Ha
Harmon Peaking Fac	tor			3.9
Average flow				308.2 L/c/d
Proposed Residential F	reak Flow			10.0 L/s
I/I Flow Determinatio	n			
Site Area				0.97 ha
Infiltration (22,500 L/da	ay/ha or 0.26 L/s/ha)			0.25 L/s
Long-term dewatering	contribution			0.00 L/s
Total Proposed Peak	Flow			10.3 L/s



#### SANITARY FLOW CALCULATIONS

Pipe Data							
LENGTH (m)	PIPE DIA. (mm)	SLOPE (%)	FULL FLOW CAP.	FULL FLOW VEL.	ACTUAL VEL.	% Full	
			(L/s)	(m/s)	(m/s)	78 T UII	
10.0	250	2.0%	87.7	1.8	1.2	12%	



Appendix D

Water Data

#### EXISTING DOMESTIC FLOW CALCULATION WORKSHEET

Other Uses							
Uses	GFA	Population Eq.	L/c/d	Avg. Day (L/d)			
Commercial	215	48	300	14,400			
Other Use Avg. Day (L/d)				14,400			

#### Peak Flows (Per Region Standards)

Criteria	Peaking Factor	Flow
Avg. day (L/s)	1.00	0.17
Max Hr (L/hr)	3.00	1,800
Max Day (L/d)	1.40	20,160



#### PROPOSED DOMESTIC FLOW CALCULATION WORKSHEET

Residential Use									
Unit Type	No. of Units	PPU	L/c/d	Avg. Day (L/d)					
Studio (<750 ft <sup>2</sup> )	175	1.6	280	78,400					
1 Bdrm (<750 ft <sup>2</sup> )	189	1.6	280	84,672					
2 Bdrm (<750 ft <sup>2</sup> )	76	1.6	280	34,048					
2 Bdrm (>750 ft <sup>2</sup> )	2	3.0	280	1,680					
3 Bdrm (>750 ft <sup>2</sup> )	2	3.0	280	1,680					
Residential Use Avg. Day (L/d) 200,480									

Other Uses							
Uses	GFA	Population Eq.	L/c/d	Avg. Day (L/d)			
Commercial	1,424	7	300	2,136			
Other Use Avg. Day (L/d)				2,136			

Criteria	Peaking Factor	Flow
Avg. day (L/s)	1.00	2.3
Max Hr (L/hr)	3.00	25,327
Max Day (L/d)	2.00	405,232



#### WATERMAIN SIZING AND HEADLOSS CALCULATION WORKSHEET

					FI	re watern	nain Sizing ai	па неаа	loss Calculat	lion					
P (kPa)	EL. (m)	HGL (m)	<b>Q (m</b> <sup>3</sup> /s)	D (mm)	<b>A (m</b> <sup>2</sup> )	V (m/s)	Fitting	L (m)	K (unitless)	<b>H</b> <sub>f</sub> (kPa)	<b>Η</b> <sub>L</sub> (m)	EL. (m)	HGL (m)	P (kPa)	P (PSI)
365.4	164.40	201.65	0.165	200	0.031	5.3	-	0.5			0.09	164.40	201.56	364.5	52.9
							Gate Valve		0.2	0.28				364.2	52.8
364.2	164.40	201.53	0.165	200	0.031	5.3	-	5.5			1.04	164.40	200.49	354.0	51.4
							In line T		0.35	0.49				353.6	51.3
353.6	164.40	200.44	0.165	200	0.031	5.3		1.2			0.23	164.40	200.21	351.3	51.0
							Gate Valve		0.2	0.28				351.1	50.9
351.1	164.40	200.19	0.165	200	0.031	5.3		3.0			0.57	164.40	199.62	345.5	50.1

#### Fire Watermain Sizing and Headloss Calculation

#### **Domestic Watermain Sizing**

Use	Q <sub>avg day</sub> (L/s)	Q <sub>min</sub> (L/s)	Q <sub>max</sub> (L/s)	Q <sub>min</sub> (m <sup>3</sup> /s)	Q <sub>max</sub> (m <sup>3</sup> /s)	Dia. (mm)	A (m <sup>2</sup> )	V <sub>min</sub> (m/s)	V <sub>max</sub> (m/s)
Res.	2.35	1.97	7.04	0.002	0.007				
I/C/I	-	-	-	-	-				
Total	2.35	1.97	7.04	0.00	0.01	100	0.01	0.25	0.90

Volume of Watermains								
Dia	Volume							
(mm)	(m <sup>2</sup> )	(m)	(m <sup>3</sup> )	(L)				
200	0.03	10.2	0.320	320.4				
150	0.02	3.0	0.053	53.0				
Total wate	rmain volu	0.373	373.5					

#### 0.04 Hours for water turnover

2.65 Minutes for water turnover

#### FIRE FLOW CALCULATION WORKSHEET

	PROJECT INFORMATION								
Address	21-51 Qi	ueen St. N.	Notes:	Assumes properly protected					
	Toronto,	ON		vertical openings					
				Effective area "A" calculated as:					
NBC Occu	upancy			A= L7+1/4 L8 + 1/4 L6					
Building F	ootprint								
No. of Sto	oreys	9 plus mechanical penthouse							

BASE FLOW CALCULATION					CHARGES	Q (L/min)
A= Effective area C= Fire-resistive F= Required fire "F" Rounded to near	e flow	F=220C $\sqrt{A}$	8,156 m <sup>2</sup> 0.6 11,921 L/min. 12,000 L/min.			12,000
FLO	OW 'F' AD	JUSTMENTS		CREDITS	CHARGES	Q (L/min)
Occupancy Adjustments Non-combustible	5 (F')	% -25%	-3,000	-3000		9,000
Exposure Adjustments (I	E)					
Exposure	Sep. (m)	Charge				
N	3	25%				
E	35	5%				
S	20	15%				
W	45	5%				
E = Total Exposure Char	ge	50%	4,500		4,500	13,500
Sprinkler Adjusments (S)	)					
Sprinklered as per NFPA	13	Yes	-2,700	-2700		10,800
Standard Water Supply		Yes	-900	-900		9,900
Fully supervised watersu	ipply	No	0			9,900
REQUIRED FLOW (F"=I	F'+E+S)		(L/min) (USGPM)			9,900 2,615



#### MUNICIPAL SUPPLY CALCULATION WORKSHEET

	Hydrant Flow Test Input								
Location	Test No.	P <sub>s</sub> (PSI)	P <sub>r</sub> (PSI)	Q <sub>r</sub> (USGPM)					
21-51 Queen St. N.	1	53	51	1,138					
	2	53	45	1743					

# Theoretical Flow CalculationLocationTest No.Pf (PSI)Qf (USGPM)21-51 Queen St. N.1205,1712203,747

Where  $Q_f = Q_r \left[ \frac{P_s - P_f}{P_s - P_r} \right]^{0.54}$ 

Max Day + Fire Check						
Max Day (USGPM) F'' (USGPM) Max Day + F'' (USGPM) Q <sub>20</sub> (USGPM) Che						
74	2,615	2,690	3,747	OK		





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GREEN - A 1000-1500

BLUE - AA >1500

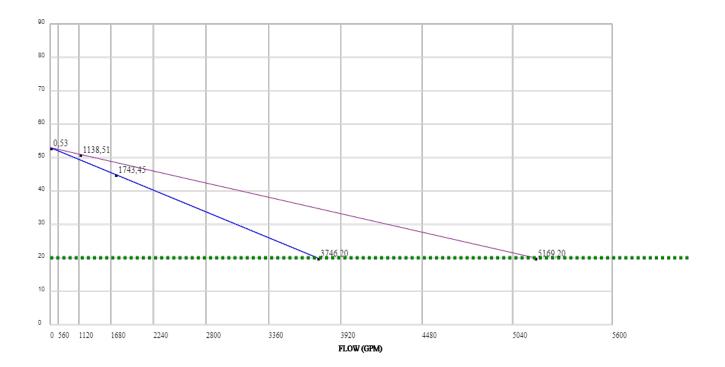
Client Siteplantech Inc. (Test #6) Site 21-51 Queen St. Mississauga, On 336-16 Elgin St. Markham, On Site Contact Pascal Monat Phone 416-270-7515 **FIRE FLOW TEST** Fire Flow Date May 12, 2021 - 12:00 pm RED - C 0-500 Site 21-51 Queen St. Mississauga, On ORANGE - B 500-1000 **Hydrant Colours** Static Hydrant Corner Queen St. & Matlock

#### Single Port

Flow Hydrant 21-51 Queen St.N

Static	53 psi	Static	53 psi
Residual 1	51 psi	Residual 2	45 psi
Flow	46 psi	Flow 2 (x2)	27 psi
Observed	<b>1138 US GPM</b> 947 IMP GPM 4306 L / MIN	Observed	<b>1743 US GPM</b> 1451IMP GPM 6598 L / MIN
Projected @ 20psi	<b>5169 US GPM</b> 4304 IMP GPM 19567 I/min.	Projected @ 20psi	<b>3746 US GPM</b> 3119 IMP GPM 14180 I/min.

**Two Port** 



Appendix E

**Engineering Drawings** 

# GENERAL NOTES

#### STORM SEWERS: ALL CONCRETE PIPE SMALLER THAN 450MM DIAMETER SHALL BE C-14, CLASS 2 CONCRETE PIPE 450MM DIAMETER AND LARGER SHALL BE C-76, CLASS 65-D, UNLESS OTHERWISE NOTED.

- 2. ALL POLYVINYL CHLORIDE (PVC.) PIPE SHALL MEET THE C.S.A. REQUIREMENTS AS NOTED WITHIN OPSS. THE PIPE MATERIAL SHALL HAVE A CELL CLASSIFICATION OF 12454-B OR 12454-C OR ASTM. STD. D-3034 & OPSS. 1841.
- 3. ALL CONCRETE SEWER PIPES SHALL HAVE RUBBER GASKET JOINTS.
- CLASS "B" BEDDING IS TO BE USED AS PER CITY STANDARD 2112.08 SEWER BEDDING AND COVER MATERIAL SHALL CONFIRM WITH CITY STANDARDS 2112.09 AND 2112.10. IF WATER IS PRESENT IN THE TRENCH EXCAVATION THEN 19MM. CLEAR STONE IS TO BE USED FOR BEDDING IN ACCORDANCE WITH CITY STANDARD 2112.11 AND 2112.14 RESPECTIVELY. WHERE WET OR SOFT TRENCH SUBGRADE CONDITIONS ARE ENCOUNTERED, FURTHER ON-SITE GEOTECHNICAL ASSESSMENT MAY BE REQUIRED TO DETERMINE THE APPROPRIATE BEDDING IN ORDER TO STABILIZE THE SUBGRADE FOR SEWER CONSTRUCTION.
- 5. MANHOLE STEPS SHALL BE AS PER OPSD. 405.010.
- 6. MANHOLE COVERS AND FRAMES SHALL BE AS PER OPSD. 401.010.
- SINGLE CATCHBASINS WITHIN ROAD ALLOWANCES SHALL BE AS PER OPSD. 705.010, WITH A 250MM DIAMETER LEAD, DOUBLE CATCHBASINS WITHIN ROAD ALLOWANCES SHALL BE AS PER OPSD. 705.020, WITH A 300MM DIAMETER LEAD.
- 8. ALL CATCHBASIN FRAME AND GRATES SHALL BE AS PER OPSD. 400.020.
- THE TRENCH WIDTH AT THE TOP OF PIPE SHALL BE AS PER STD. 2112.08. IF THE MAXIMUM TRENCH WIDTH IS EXCEEDED, THE CONTRACTOR SHALL BE RESPONSIBLE FOR SUPPLYING EXTRA BEDDING AND/OR STRONGER PIPE AS REQUIRED.
- 10. ALL STORM SEWER AND APPURTENANCES SHALL BE CONSTRUCTED IN ACCORDANCE WITH CURRENT CITY OF MISSISSAUGA STANDARDS AND SPECIFICATIONS.
- STORM SERVICE CONNECTION IS TO BE ON THE LEFT OF SANITARY SERVICE FACING THE HOUSE. (EXCEPT AS NOTED)
- 12. SERVICE CONNECTION AT THE STREET LINE IS TO BE HIGHER THAN THE SANITARY CONNECTION AT THAT POINT.
- 13. ALL CATCHBASINS ARE TO BE PLACED ON GRANULAR BEDDING (MINIMUM DEPTH 150MM).
- 14. TRENCH BACKFILLING ON PROPOSED ROADS SHALL WITH CITY'S ENGINEERING POLICY STATEMENT AS PROVIDED IN THE "DEVELOPMENT REQUIREMENTS MANUAL" (SECTION 4.02.06-TRENCH BACKFILLING ON ROADS). TRENCH BACKFILL SHALL BE COMPACTED TO A MINIMUM OF 95% S.P.D. WITHIN 2.0% OF THE OPTIMUM CONTENT
- 15. SAND BACKFILLING IS REQUIRED ADJACENT TO MANHOLES, CATCHBASINS AND SERVICE CROSSING
- GENERAL THE SUBJECT LANDS, IS TO BE UNDERTAKEN AT DEVELOPER'S EXPENSE
- 2. ALL UNDERGROUND SERVICE CONNECTIONS WITHIN PAVED PORTION OF ANY 8. ALL BOREHOLES SHOWN ON DRAWING ARE FOR INFORMATION ONLY. REFER TO EXISTING ROAD TO BE BACKFILLED WITH UNSHRINKABLE FILL TO THE LATEST CITY OF MISSISSAUGA OR REGION OF PEEL SPECIFICATIONS.
- SNOW FENCE AND SEDIMENT TRAP CONTROL FENCE ARE TO BE INSTALLED PRIOR TO THE COMMENCEMENT OF ANY SITE CONSTRUCTION AND SHALL REMAIN IN SANITARY SEWER NOTES: PLACE AND IN GOOD REPAIR THROUGHOUT THE CONSTRUCTION AND GRADING I. ALL SANITARY SEWER BEDDING AS PER STD. 2-3-1 PHASES.
- PRIOR TO THE START OF CONSTRUCTION, SNOW FENCING IS TO BE ERECTED ALONG THE PROPERTY BOUNDARIES ADJACENT TO ALL EXISTING RESIDENTIAL LOTS, PARKS AND ALL EXISTING SCHOOL BLOCKS.
- THE LOCATION AND ELEVATION OF ALL EXISTING SERVICES AND UTILITIES ARE TO BE VERIFIED IN THE FIELD BY THE CONTRACTOR. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE RESTORATION TO THE REPAIR OF EXISTING UTILITIES DISTURBED DURING CONSTRUCTION.
- ALL AREAS BEYOND THE PLAN OF SUBDIVISION WHICH ARE DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO THE SATISFACTION OF THE AUTHORITY 5. ALL MANHOLES SHALL BE AS PER REGION STD. DWG. 2-5-2, 2-5-3, 2-5-4, 2-5-5 HAVING JURISDICTION AT THE CONTRACTOR'S EXPENSE.
- "UNIFORM TRAFFIC CONTROL DEVICES".
- 8. ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH THE "OCCUPATIONAL HEALTH AND SAFETY ACT". THE GENERAL CONTRACTOR SHALL BE DEEMED TO 8. BE THE CONSTRUCTOR AS DEFINED IN THE ACT.
- BOREHOLES: BOREHOLE LOGS SHOWN ARE FOR GENERAL INFORMATION ONLY AND LOCATIONS ARE APPROXIMATE. CONTRACTOR IS TO VERIFY AND SATISFY HIMSELF AS TO THE NATURE OF THE SUBSURFACE CONDITIONS.

#### **ROADWORKS:**

- ALL FILL WITHIN ROAD ALLOWANCE TO BE COMPACTED TO A MINIMUM OF 95% STANDARD PROCTOR DENSITY. THE SUITABILITY AND COMPACTION OF ALL FILL MATERIALS ARE TO BE CONFIRMED BY A RECOGNIZED SOIL CONSULTANT TO THE CITY ENGINEER PRIOR TO THE INSTALLATION OF ANY ROAD BASE MATERIALS.
- ALL CONNECTIONS WITHIN PAVED PORTION OF ANY EXISTING ROAD TO BE WATERMAIN NOTES: BACKFILLED WITH GRANULAR MATERIAL AND/OR UNSHRINKABLE FILL AS PER I. THE REGION OF PEEL SHALL CONDUCT THE OPERATION OF EXISTING VALVES THE LATEST OF CITY OF MISSISSAUGA STANDARDS AND SPECIFICATIONS.
- A. TRENCH BACKFILLING ON PROPOSED ROADS SHALL COMPLY WITH THE CITY'S ENGINEERING POLICY STATEMENTS PROVIDED IN THE "DEVELOPMENT REQUIREMENTS MANUAL" (SECTION 4.02.06 - TRENCH BACKFILLING ON ROADS).
- B. ALL BACKFILL FOR SEWERS, WATERMAINS AND UTILITIES WITHIN ROAD ALLOWANCE SHALL BE COMPACTED TO 95% STANDARD PROCTOR DENSITY WITHIN 2% OF THE OPTIMUM MOISTURE CONTENT.
- C. THE TOP 1000MM OF THE SUB-GRADE IS TO BE COMPACTED TO A MINIMUM 98% STANDARD PROCTOR DENSITY WITHIN 2% OF THE OPTIMUM MOISTURE CONTENT.
- ALL ROADWORKS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE CITY OF MISSISSAUGA STANDARDS AND SPECIFICATIONS.
- ALL INTERSECTING ROADS SHALL BE PROVIDED WITH AN ADDITIONAL 150MM THICKNESS OF OPSS. GRANULAR "B". THIS EXTRA DEPTH SHALL EXTEND FOR A MINIMUM OF 15M BEYOND PROPERTY LINE OF INTERSECTING STREET, AS NOTED.
- SUB-DRAINS ARE TO BE INSTALLED AS PER CITY STANDARD 2220.04 ALONG THE ENTIRE LENGTH OF THE ROAD.
- PAVEMENT THICKNESS AND COMPOSITION TO BE AS SHOWN ON INDIVIDUAL PLAN AND PROFILE DRAWINGS.

ROADWORKS (CONT'D): 8. CONCRETE CURB & GUTTER OPSD. 600.070.

- 9. SAND BACKFILL IS TO BE USED ADJACENT TO MANHOLES, CATCHBASINS AND SERVICE CROSSINGS.
- EXISTING WATERCOURSE/GREENBELT:
- PRIOR TO COMMENCEMENT OF ANY GRADING OR CONSTRUCTION, TEMPORARY SNOW FENCE AND SILT FENCE TO BE ERECTED ALONG ALL LOTS AND BLOCKS 10. FIRE HYDRANTS TO BE INSTALLED AS PER REGION STD. DWG. I-6-I AND I-6-2 ADJACENT TO THE EXISTING WATERCOURSE/GREENBELT, PARKS AND WITH FLANGE SET BETWEEN 50MM AND 150MM ABOVE FINISHED GRADE. MAINTAINED UNTIL COMPLETION OF CONSTRUCTION.
- II. ALL HYDRANTS SHALL HAVE I.2M MINIMUM HORIZONTAL CLEARANCE FROM ALL 2. NO STOCKPILES OF FILL MATERIAL ARE TO BE PLACED WITHIN 10.0M OF THE OTHER UTILITIES AND STRUCTURES MEASURED FROM THE NEAREST POINT OF EXISTING WATERCOURSE BLOCK. THE STRUCTURE.
- TOPSOIL STOCKPILE PROTECTION: ALL TOPSOIL STOCKPILE CONTAINING MORE THAN 100M<sup>3</sup> OF MATERIAL SHALL BE LOCATED A MINIMUM OF IOM AWAY FROM A ROADWAY, DRAINAGE CHANNEL OR AN OCCUPIED RESIDENTIAL LOT. THE MAXIMUM SIDE SLOPES FOR TOPSOIL

STOCKPILES SHALL BE 1.5 HORIZONTAL TO 1.0 VERTICAL.

2. RUNOFF FROM ALL TOPSOIL STOCKPILES SHALL BE CONTROLLED BY A SEDIMENT 30 DAYS, TOPSOIL STOCKPILES SHALL BE STABILIZED BY VEGETATIVE COVER, OR OTHER MEANS

#### REGION OF PEEL

GENERAL NOTES:

- THE APPLICANT, APPLICANT'S REPRESENTATIVE, CONSULTANT, CONTRACTOR AND SUB CONTRACTORS ARE RESPONSIBLE TO ENSURE THAT THEIR DESIGN MATERIALS AND CONSTRUCTION PRACTICES CONFORM TO THE LATEST REGION OF PEEL'S WEBSITE (WWW.PEELREGION.CA/PW/STANDARDS). IN THE ABSENCE OF REGION SPECIFICATIONS, THE ONTARIO PROVINCIAL STANDARDS SPECIFICATIONS (OPSS) SHALL APPLY.
- 2. ALL WORKS SHALL BE COMPLETED IN ACCORDANCE WITH THE "OCCUPATIONAL HEALTH AND SAFETY ACT". THE GENERAL CONTRACTOR SHALL BE DEEMED TO BE THE CONSTRUCTOR AS DEFINED IN THE ACT.
- 18. PROVISION FOR FLUSHING OF NEW WATERMAINS PRIOR TO TESTING MUST BE PROVIDED WITH AT LEAST A 50MM OUTLET ON WATERMAINS SMALLER THAN FOR ROAD PROJECTS THAT WILL NOT BE COMPLETED PRIOR TO THE END OF THE 3. THE CONTRACTOR AT THEIR EXPENSE SHALL VERIFY THE LOCATION, DIMENSION 300MM IN DIAMETER, AND MINIMUM 100MM OUTLET ON WATERMAINS 300MM AND CONSTRUCTION SEASON, THE FOLLOWING WILL NEED TO BE CONSIDERED IN AND ELEVATION OF ALL EXISTING SERVICES AND UTILITIES IN THE FIELD. LARGER. COPPER WATERMAINS ARE TO HAVE FLUSHING POINTS AT THE END, ORDER TO WINTERIZE THE CONSTRUCTION PROJECT TO ENSURE SAFE THE SAME SIZE AS THE WATERMAIN, AS PER STD. DWG. I-7-7 AND I-7-8. CONDITIONS DURING WINTER:
- 4. PRIOR TO EXCAVATION OR BORING CONTRACTOR AT THEIR EXPENSE SHALL EXPOSE AND VERIFY THE LOCATION AND ELEVATION OF ALL EXISTING UTILITIES AND SERVICES TO BE CROSSED AND MUST NOTIFY THE DESIGN ENGINEER AND THE AGENCY FIELD INSPECTOR AND/OR PROJECT MANAGER IMMEDIATELY, IN WRITING, OF ANY CONFLICTS OR DISCREPANCIES. CONTRACTOR SHALL BE RESPONSIBLE FOR EXPOSING THE EXISTING UTILITIES FAR ENOUGH IN ADVANCE OF CONSTRUCTION TO MAKE NECESSARY DESIGN MODIFICATIONS FOR REVIEW AND APPROVAL, IF REQUIRED, WITHOUT DELAYING THE WORK
- 5. THE CONTRACTOR, AT THEIR EXPENSE AND TO THE SATISFACTION OF THE REGION OF PEEL, SHALL BE RESPONSIBLE FOR THE RESTORATION AND THE REPAIR OF THE EXISTING UTILITIES AND ALL AREAS BEYOND THE PLAN OF SUBDIVISION DISTURBED DURING CONSTRUCTION.
- 6. THE SUPPORT OF ALL UTILITIES SHALL BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE AUTHORITY HAVING JURISDICTION.
- ANY RELOCATION OF EXISTING UTILITIES REQUIRED BY THE DEVELOPMENT OF 7. ALL BACKFILL FOR SEWERS, WATERMAINS AND UTILITIES ON THE ROAD ALLOWANCE MUST BE MECHANICALLY COMPACTED.
  - GEOTECHNICAL REPORT.
  - 9. ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE SPECIFIED.

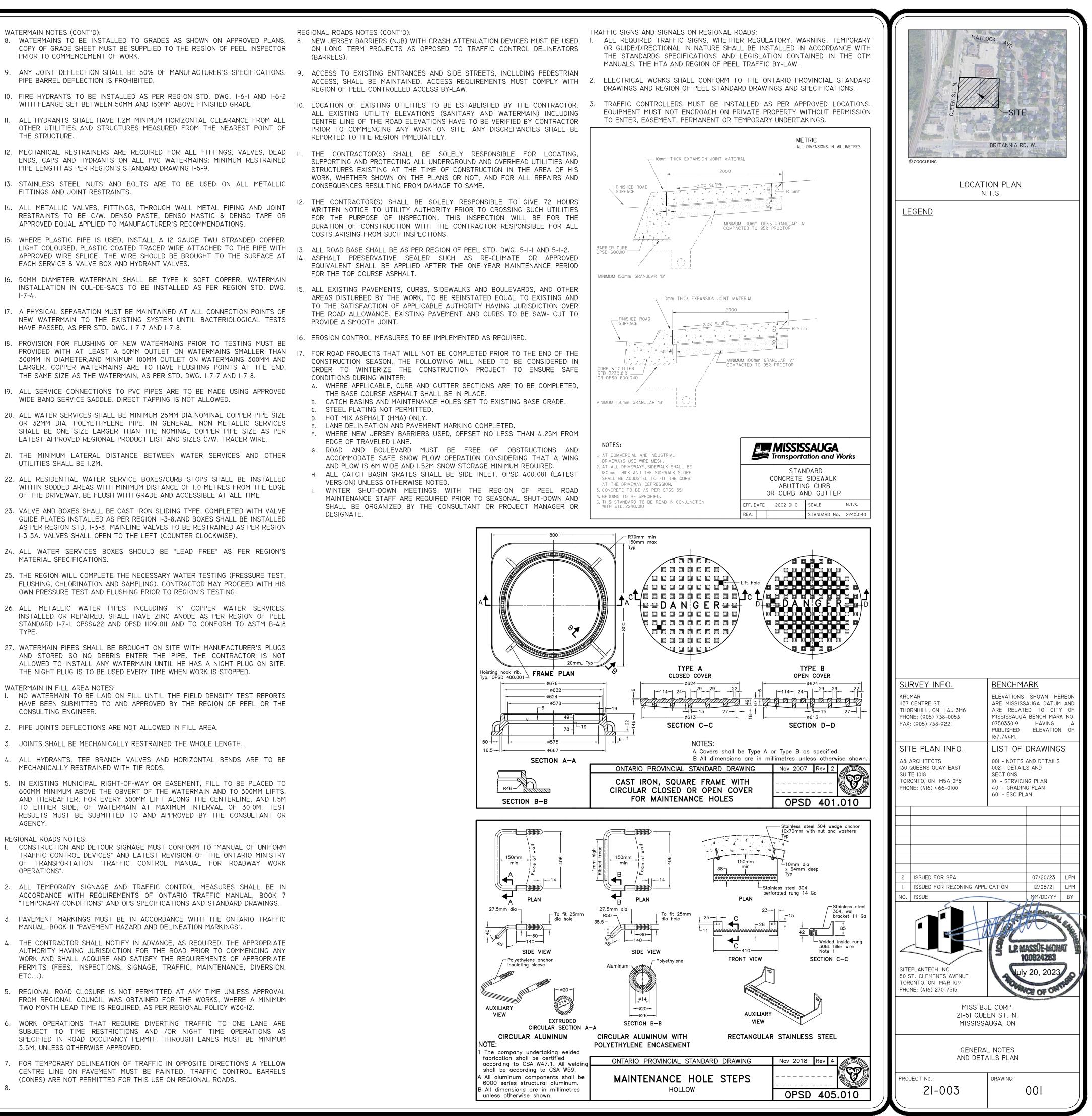
  - 2. MAINLINE SANITARY SEWER PIPE SIZE SHALL BE MINIMUM 250MM DIAMETER INSTALLED AT THE APPROVED DESIGN GRADE. PIPE CLASS AND APPURTENANCES AS PER REGION'S SPECIFICATIONS.
  - 3. ALL SEWERS CONSTRUCTED WITH GRADES 0.5% OR LESS SHALL BE APPROVED BY THE ENGINEER AND THE AGENCY PROJECT MANAGER OR DESIGNATED AND BE 27. WATERMAIN PIPES SHALL BE BROUGHT ON SITE WITH MANUFACTURER'S PLUGS INSTALLED WITH LASER AND CHECKED PRIOR TO BACKFILL.
  - 4. MINIMUM SANITARY SEWER PIPE SLOPE FOR LAST LEG SHALL BE 1% AND DESIRABLE SLOPE 2%.
  - AND 2-5-6 AND BENCHING AS PER STD. DWG. 2-5-20.
- 7. ALL CONSTRUCTION SIGNING MUST CONFORM TO THE M.T.O. MANUAL OF 6. FRAME AND COVERS SHALL BE AS PER REGION STD. DWG. 2-5-13, 2-6-1 TO 2-6-8
  - 7. MANHOLE STEPS OR LADDERS TO BE AS PER REGION STD. DWG. 2-6-9 TO 2-6-II.
  - MANHOLES DEEPER THAN 5.0M MUST BE EQUIPPED WITH SAFETY PLATFORMS, AS PER STD. 2-6-13 AND 2-6-14.
  - 9. MANHOLE DROP STRUCTURES SHALL BE AS PER REGION STD. DWG. 2-5-26 AND 2-5-27.
  - 10. SANITARY SERVICE LATERALS SHALL BE MINIMUM 125MM DIAMETER AND, A. SANITARY SERVICE SHALL BE LOWER THAN AND TO THE RIGHT OF THE STORM SERVICE AT THE PROPERTY LINE WHEN FACING THE LOT FROM THE STREET.
  - B. CONNECTIONS TO SEWERS SHALL BE MADE WITH MANUFACTURED TEES OR WYES WHERE APPLICABLE AND SHALL BE COLOUR CODED AS NON-WHITE, AS PER STD. DWG. 2-4-I, TO 2-4-7.

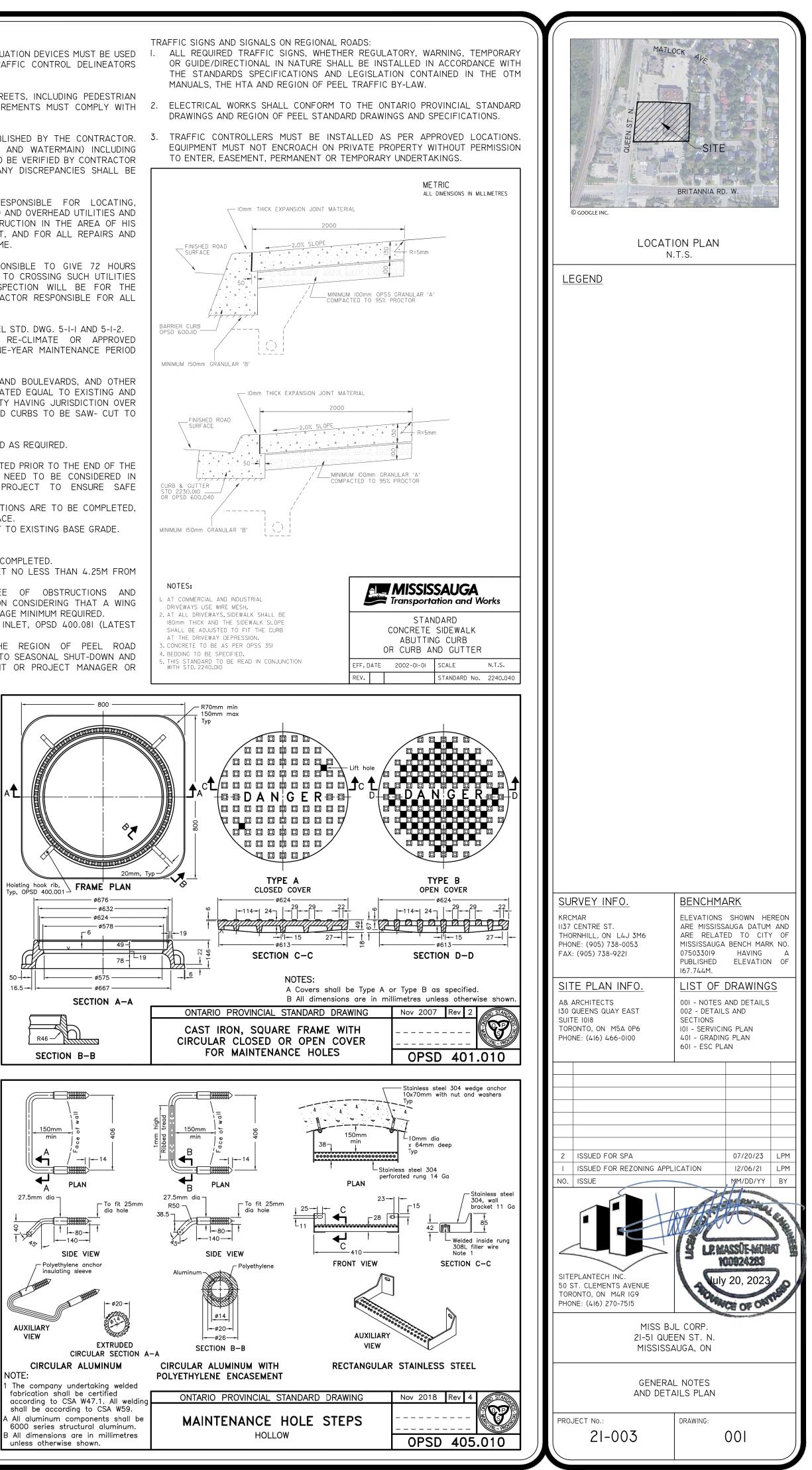
- AND HYDRANTS IF REQUIRED.
- 2. CONTRACTOR MUST USE BATTER BOARD OR ROD-AND-LEVEL METHOD FOR WATERMAIN INSTALLATION.
- 3. ALL WATERMAINS SHALL HAVE I.70M MINIMUM COVER FOR URBAN ROAD DESIGN 3. PAVEMENT MARKINGS MUST BE IN ACCORDANCE WITH THE ONTARIO TRAFFIC AND 2.IM MINIMUM COVER FOR RURAL ROAD DESIGN. MANUAL, BOOK II "PAVEMENT HAZARD AND DELINEATION MARKINGS".
- 4. ALL WATERMAINS SHALL MAINTAIN A MINIMUM 1.5M CLEARANCE FROM ALL THE CONTRACTOR SHALL NOTIFY IN ADVANCE, AS REQUIRED, THE APPROPRIATE MANHOLES AND CATCH BASINS, WHERE APPLICABLE. AUTHORITY HAVING JURISDICTION FOR THE ROAD PRIOR TO COMMENCING ANY WORK AND SHALL ACQUIRE AND SATISFY THE REQUIREMENTS OF APPROPRIATE 5. FOR WATERMAIN CROSSING OVER OR UNDER SEWERS A MINIMUM 0.5M VERTICAL PERMITS (FEES, INSPECTIONS, SIGNAGE, TRAFFIC, MAINTENANCE, DIVERSION, CLEARANCE SHALL BE PROVIDED. ETC...).
- FOR WATERMAIN CROSSING A SANITARY SEWER, WATERMAIN JOINTS ARE TO BE REGIONAL ROAD CLOSURE IS NOT PERMITTED AT ANY TIME UNLESS APPROVAL OFFSET A MINIMUM OF 2.5M HORIZONTALLY FROM THE CENTERLINE OF THE FROM REGIONAL COUNCIL WAS OBTAINED FOR THE WORKS, WHERE A MINIMUM SANITARY SEWER. TWO MONTH LEAD TIME IS REQUIRED, AS PER REGIONAL POLICY W30-12.
- 7. WATERMAIN BEDDING SHOULD BE AS PER TRENCH DETAIL ON THE PLAN AND PROFILE DRAWING AND COMPACTED TO 100% SPD.

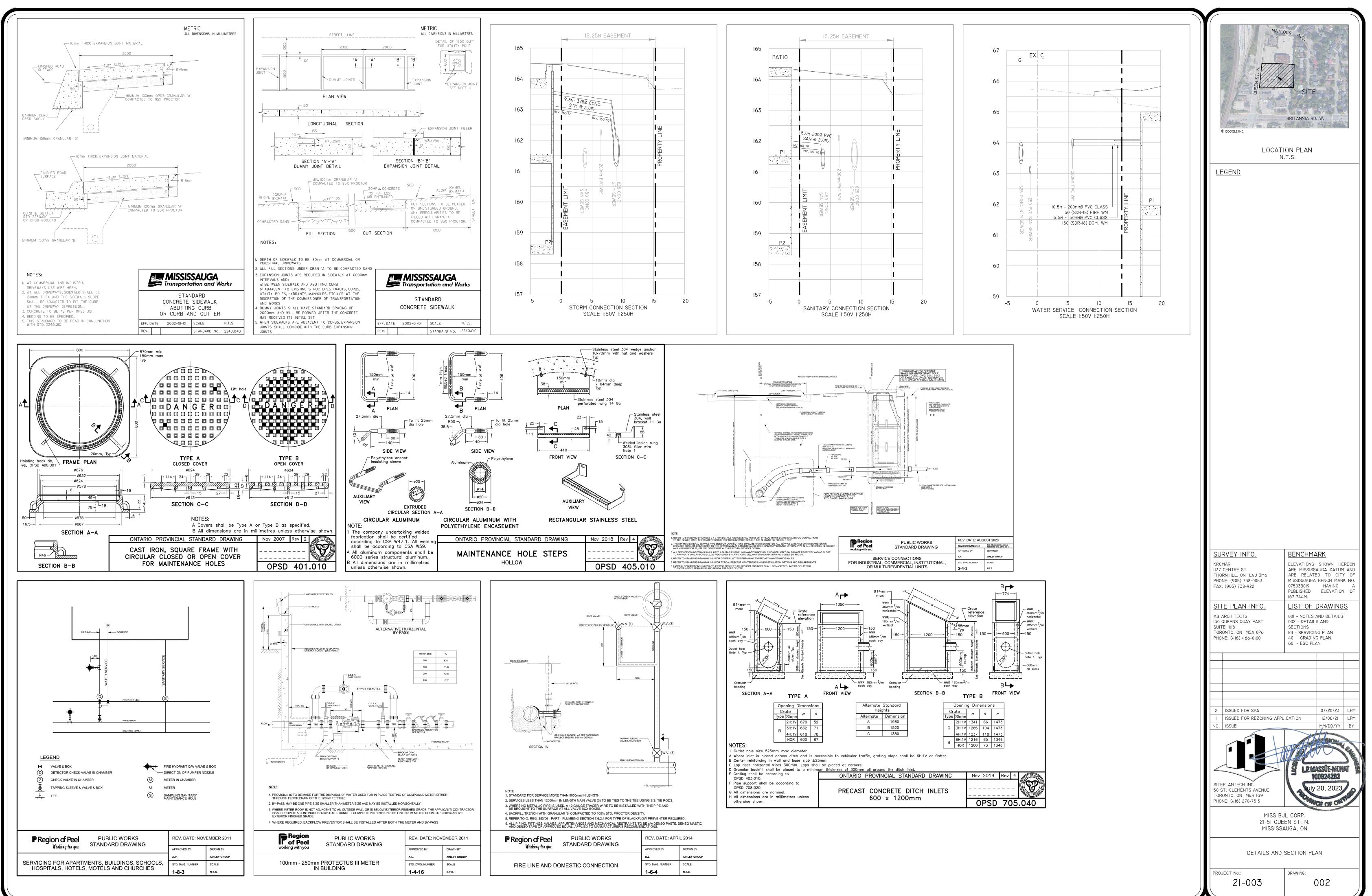
- WATERMAIN NOTES (CONT'D): COPY OF GRADE SHEET MUST BE SUPPLIED TO THE REGION OF PEEL INSPECTOR PRIOR TO COMMENCEMENT OF WORK.
- PIPE BARREL DEFLECTION IS PROHIBITED.
- 12. MECHANICAL RESTRAINERS ARE REQUIRED FOR ALL FITTINGS, VALVES, DEAD 11. THE CONTRACTOR(S) SHALL BE SOLELY RESPONSIBLE FOR LOCATING, ENDS, CAPS AND HYDRANTS ON ALL PVC WATERMAINS; MINIMUM RESTRAINED PIPE LENGTH AS PER REGION'S STANDARD DRAWING 1-5-9.
- 13. STAINLESS STEEL NUTS AND BOLTS ARE TO BE USED ON ALL METALLIC FITTINGS AND JOINT RESTRAINTS.
- CONTROL FENCE OR OTHER APPROVED DEVICES. IF REMAINING FOR MORE THAN 14. ALL METALLIC VALVES, FITTINGS, THROUGH WALL METAL PIPING AND JOINT RESTRAINTS TO BE C/W. DENSO PASTE, DENSO MASTIC & DENSO TAPE OR APPROVED EQUAL APPLIED TO MANUFACTURER'S RECOMMENDATIONS.
  - 15. WHERE PLASTIC PIPE IS USED, INSTALL A 12 GAUGE TWU STRANDED COPPER LIGHT COLOURED, PLASTIC COATED TRACER WIRE ATTACHED TO THE PIPE WITH APPROVED WIRE SPLICE. THE WIRE SHOULD BE BROUGHT TO THE SURFACE AT EACH SERVICE & VALVE BOX AND HYDRANT VALVES.
  - 50MM DIAMETER WATERMAIN SHALL BE TYPE K SOFT COPPER. WATERMAIN INSTALLATION IN CUL-DE-SACS TO BE INSTALLED AS PER REGION STD. DWG. 1-7-4.
  - 17. A PHYSICAL SEPARATION MUST BE MAINTAINED AT ALL CONNECTION POINTS OF NEW WATERMAIN TO THE EXISTING SYSTEM UNTIL BACTERIOLOGICAL TESTS HAVE PASSED, AS PER STD. DWG. I-7-7 AND I-7-8.
  - 19. ALL SERVICE CONNECTIONS TO PVC PIPES ARE TO BE MADE USING APPROVED WIDE BAND SERVICE SADDLE. DIRECT TAPPING IS NOT ALLOWED.
  - 20. ALL WATER SERVICES SHALL BE MINIMUM 25MM DIA.NOMINAL COPPER PIPE SIZE OR 32MM DIA. POLYETHYLENE PIPE. IN GENERAL, NON METALLIC SERVICES SHALL BE ONE SIZE LARGER THAN THE NOMINAL COPPER PIPE SIZE AS PER LATEST APPROVED REGIONAL PRODUCT LIST AND SIZES C/W. TRACER WIRE.
  - 21. THE MINIMUM LATERAL DISTANCE BETWEEN WATER SERVICES AND OTHER UTILITIES SHALL BE 1.2M.
  - 22. ALL RESIDENTIAL WATER SERVICE BOXES/CURB STOPS SHALL BE INSTALLED WITHIN SODDED AREAS WITH MINIMUM DISTANCE OF 1.0 METRES FROM THE EDGE OF THE DRIVEWAY, BE FLUSH WITH GRADE AND ACCESSIBLE AT ALL TIME.
  - 23. VALVE AND BOXES SHALL BE CAST IRON SLIDING TYPE, COMPLETED WITH VALVE GUIDE PLATES INSTALLED AS PER REGION I-3-8.AND BOXES SHALL BE INSTALLED AS PER REGION STD. I-3-8. MAINLINE VALVES TO BE RESTRAINED AS PER REGION I-3-3A. VALVES SHALL OPEN TO THE LEFT (COUNTER-CLOCKWISE).
  - 24. ALL WATER SERVICES BOXES SHOULD BE "LEAD FREE" AS PER REGION'S MATERIAL SPECIFICATIONS.
  - 25. THE REGION WILL COMPLETE THE NECESSARY WATER TESTING (PRESSURE TEST FLUSHING, CHLORINATION AND SAMPLING). CONTRACTOR MAY PROCEED WITH HIS OWN PRESSURE TEST AND FLUSHING PRIOR TO REGION'S TESTING.
  - ALL METALLIC WATER PIPES INCLUDING 'K' COPPER WATER SERVICES INSTALLED OR REPAIRED, SHALL HAVE ZINC ANODE AS PER REGION OF PEEL STANDARD I-7-I, OPSS422 AND OPSD II09.011 AND TO CONFORM TO ASTM B-418 TYPE.
  - AND STORED SO NO DEBRIS ENTER THE PIPE. THE CONTRACTOR IS NOT ALLOWED TO INSTALL ANY WATERMAIN UNTIL HE HAS A NIGHT PLUG ON SITE. THE NIGHT PLUG IS TO BE USED EVERY TIME WHEN WORK IS STOPPED.
  - WATERMAIN IN FILL AREA NOTES: NO WATERMAIN TO BE LAID ON FILL UNTIL THE FIELD DENSITY TEST REPORTS HAVE BEEN SUBMITTED TO AND APPROVED BY THE REGION OF PEEL OR THE CONSULTING ENGINEER.
  - PIPE JOINTS DEFLECTIONS ARE NOT ALLOWED IN FILL AREA.
  - JOINTS SHALL BE MECHANICALLY RESTRAINED THE WHOLE LENGTH.
  - 4. ALL HYDRANTS, TEE BRANCH VALVES AND HORIZONTAL BENDS ARE TO BE MECHANICALLY RESTRAINED WITH TIE RODS.
  - 5. IN EXISTING MUNICIPAL RIGHT-OF-WAY OR EASEMENT, FILL TO BE PLACED TO 600MM MINIMUM ABOVE THE OBVERT OF THE WATERMAIN AND TO 300MM LIFTS; AND THEREAFTER, FOR EVERY 300MM LIFT ALONG THE CENTERLINE, AND 1.5M TO EITHER SIDE, OF WATERMAIN AT MAXIMUM INTERVAL OF 30.0M. TEST RESULTS MUST BE SUBMITTED TO AND APPROVED BY THE CONSULTANT OR AGENCY.
  - REGIONAL ROADS NOTES: CONSTRUCTION AND DETOUR SIGNAGE MUST CONFORM TO "MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES" AND LATEST REVISION OF THE ONTARIO MINISTRY OF TRANSPORTATION "TRAFFIC CONTROL MANUAL FOR ROADWAY WORK OPERATIONS".
  - ALL TEMPORARY SIGNAGE AND TRAFFIC CONTROL MEASURES SHALL BE IN ACCORDANCE WITH REQUIREMENTS OF ONTARIO TRAFFIC MANUAL, BOOK 7 "TEMPORARY CONDITIONS" AND OPS SPECIFICATIONS AND STANDARD DRAWINGS.
  - WORK OPERATIONS THAT REQUIRE DIVERTING TRAFFIC TO ONE LANE ARE SUBJECT TO TIME RESTRICTIONS AND /OR NIGHT TIME OPERATIONS AS SPECIFIED IN ROAD OCCUPANCY PERMIT. THROUGH LANES MUST BE MINIMUM 3.5M, UNLESS OTHERWISE APPROVED.
  - 7. FOR TEMPORARY DELINEATION OF TRAFFIC IN OPPOSITE DIRECTIONS A YELLOW CENTRE LINE ON PAVEMENT MUST BE PAINTED. TRAFFIC CONTROL BARRELS (CONES) ARE NOT PERMITTED FOR THIS USE ON REGIONAL ROADS.

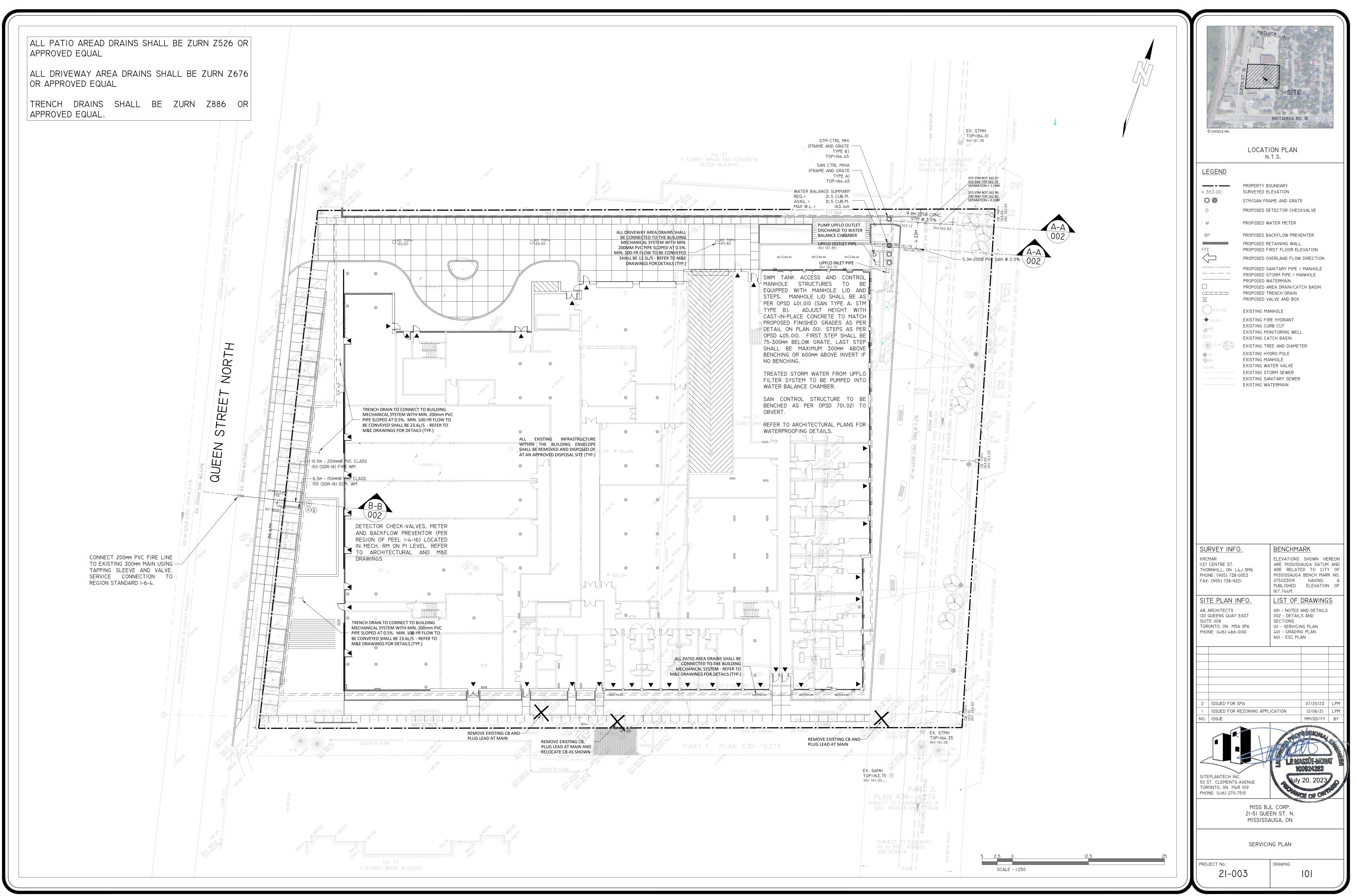
REGIONAL ROADS NOTES (CONT'D):

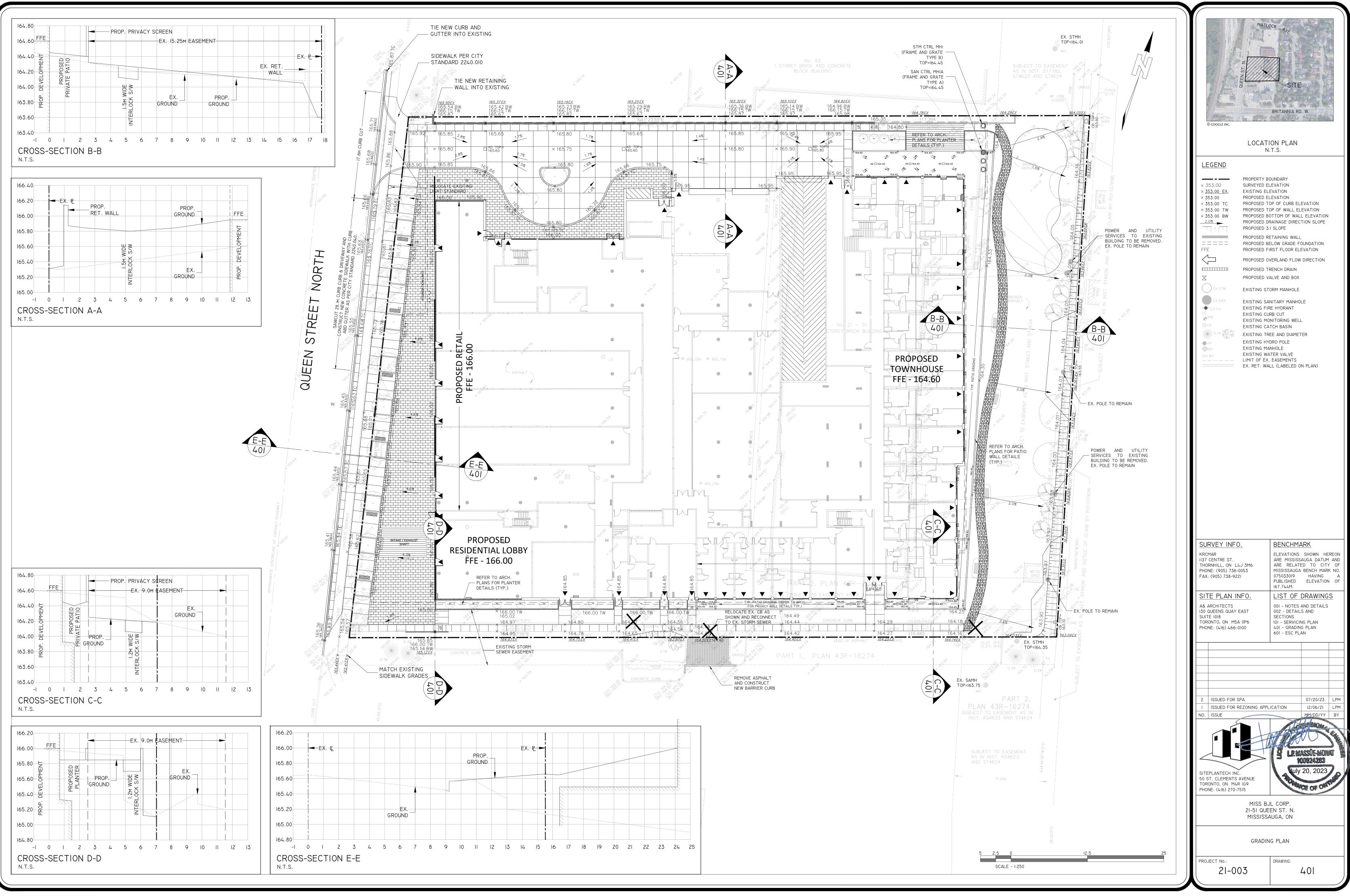
- ON LONG TERM PROJECTS AS OPPOSED TO TRAFFIC CONTROL DELINEATORS (BARRELS).
- 9. ANY JOINT DEFLECTION SHALL BE 50% OF MANUFACTURER'S SPECIFICATIONS. 9. ACCESS TO EXISTING ENTRANCES AND SIDE STREETS, INCLUDING PEDESTRIAN ACCESS, SHALL BE MAINTAINED. ACCESS REQUIREMENTS MUST COMPLY WITH 2 REGION OF PEEL CONTROLLED ACCESS BY-LAW.
  - ALL EXISTING UTILITY ELEVATIONS (SANITARY AND WATERMAIN) INCLUDING CENTRE LINE OF THE ROAD ELEVATIONS HAVE TO BE VERIFIED BY CONTRACTOR PRIOR TO COMMENCING ANY WORK ON SITE. ANY DISCREPANCIES SHALL BE REPORTED TO THE REGION IMMEDIATELY.
  - SUPPORTING AND PROTECTING ALL UNDERGROUND AND OVERHEAD UTILITIES AND STRUCTURES EXISTING AT THE TIME OF CONSTRUCTION IN THE AREA OF HIS WORK, WHETHER SHOWN ON THE PLANS OR NOT, AND FOR ALL REPAIRS AND CONSEQUENCES RESULTING FROM DAMAGE TO SAME.
  - 12. THE CONTRACTOR(S) SHALL BE SOLELY RESPONSIBLE TO GIVE 72 HOURS WRITTEN NOTICE TO UTILITY AUTHORITY PRIOR TO CROSSING SUCH UTILITIES FOR THE PURPOSE OF INSPECTION. THIS INSPECTION WILL BE FOR THE DURATION OF CONSTRUCTION WITH THE CONTRACTOR RESPONSIBLE FOR ALL COSTS ARISING FROM SUCH INSPECTIONS.
  - 13. ALL ROAD BASE SHALL BE AS PER REGION OF PEEL STD. DWG. 5-I-I AND 5-I-2. ASPHALT PRESERVATIVE SEALER SUCH AS RE-CLIMATE OR APPROVED EQUIVALENT SHALL BE APPLIED AFTER THE ONE-YEAR MAINTENANCE PERIOD FOR THE TOP COURSE ASPHALT.
  - 15. ALL EXISTING PAVEMENTS, CURBS, SIDEWALKS AND BOULEVARDS, AND OTHER AREAS DISTURBED BY THE WORK, TO BE REINSTATED EQUAL TO EXISTING AND TO THE SATISFACTION OF APPLICABLE AUTHORITY HAVING JURISDICTION OVER THE ROAD ALLOWANCE. EXISTING PAVEMENT AND CURBS TO BE SAW- CUT TO PROVIDE A SMOOTH JOINT.
  - EROSION CONTROL MEASURES TO BE IMPLEMENTED AS REQUIRED.
  - A. WHERE APPLICABLE, CURB AND GUTTER SECTIONS ARE TO BE COMPLETED, THE BASE COURSE ASPHALT SHALL BE IN PLACE.
  - B. CATCH BASINS AND MAINTENANCE HOLES SET TO EXISTING BASE GRADE.
  - STEEL PLATING NOT PERMITTED. HOT MIX ASPHALT (HMA) ONLY.
  - LANE DELINEATION AND PAVEMENT MARKING COMPLETED.
  - WHERE NEW JERSEY BARRIERS USED, OFFSET NO LESS THAN 4.25M FROM EDGE OF TRAVELED LANE.
  - G. ROAD AND BOULEVARD MUST BE FREE OF OBSTRUCTIONS AND ACCOMMODATE SAFE SNOW PLOW OPERATION CONSIDERING THAT A WING AND PLOW IS 6M WIDE AND 1.52M SNOW STORAGE MINIMUM REQUIRED.
  - H. ALL CATCH BASIN GRATES SHALL BE SIDE INLET, OPSD 400.081 (LATEST VERSION) UNLESS OTHERWISE NOTED.
  - WINTER SHUT-DOWN MEETINGS WITH THE REGION OF PEEL ROAD MAINTENANCE STAFF ARE REQUIRED PRIOR TO SEASONAL SHUT-DOWN AND SHALL BE ORGANIZED BY THE CONSULTANT OR PROJECT MANAGER OR DESIGNATE

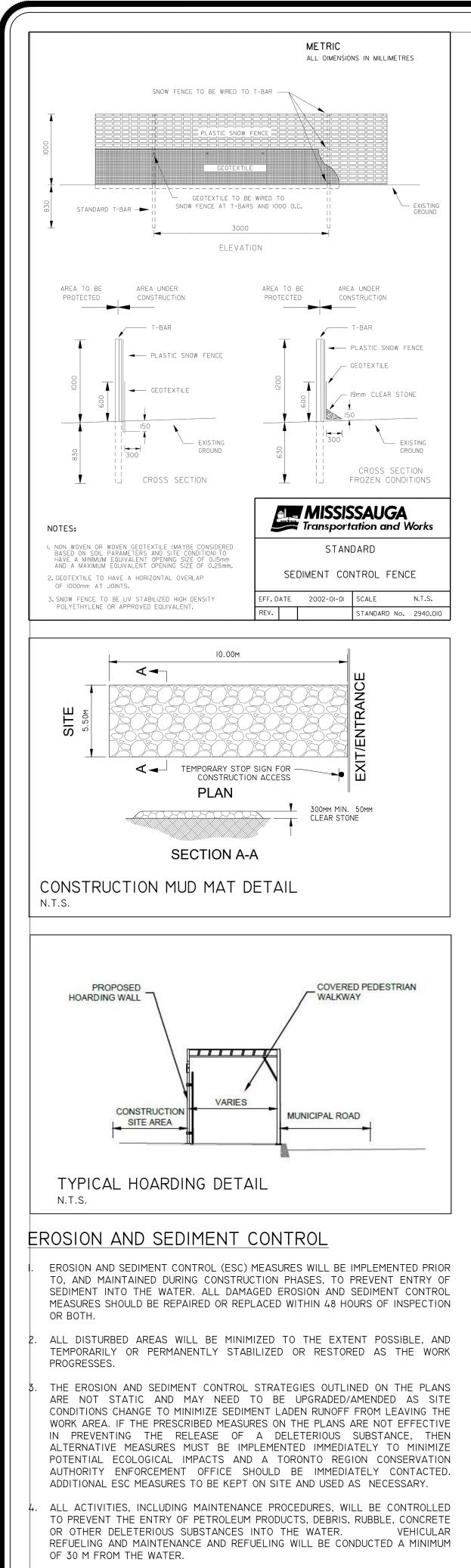












ALL GRADES WITHIN THE REGULATORY FLOOD PLAN WILL BE MAINTAINED OR MATCHED.

