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## 21-51 Queen Street North Proposed Mixed-Use Development

Urban Transportation Considerations Update<br>Zoning By-law Amendment Application<br>City of Mississauga

Prepared For: Miss BJL Corporation
July 2023


MOVEMENT IN URBAN ENVIRONMENTS
© BA Consulting Group Ltd.
45 St. Clair Avenue West, Suite 300
Toronto, ON M4V 1K9
www.bagroup.com

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### 1.0 INTRODUCTION

BA Group has been retained by Miss BJL Corporation to provide transportation consulting services in relation to the proposed mixed-use development at the property municipally addressed as 21-51 Queen Street North (referred to herein as "the Site").

The Site is located north from the Britannia Road West and Queen Street North intersection. The Site is bounded by the Portuguese Cultural Centre of Mississauga to the north, a commercial plaza to the south, a row of residential homes of one to two-storeys in height along Swanhurst Boulevard to the east and Queen Street North to the west.

A Zoning By-law Amendment (ZBA) and Official Plan Amendment (OPA) application is being made to permit the proposed development of a 9-storey mixed-used building consisting of 444 residential units and retail / commercial space with a GFA of $1,584 \mathrm{~m}^{2}$ located at-grade by the west frontage of the building. A total of 358 parking spaces and six (6) tandem parking spaces are proposed to be located within a two-level underground parking garage.

The existing sidewalk along Queen Street north will be retained to provide connections to the Site for pedestrian access. The following report provides a review of the transportation-related impacts of the proposed development, a parking justification for the reduced parking supply, and outlines the proposed strategies to facilitate movement by all transportation modes to and from the Site.

The following sections of the report detail the findings of BA Group's review.

### 1.1 BACKGROUND

BA Group previously prepared a transport study entitled "21-51 Queen Street North Proposed Mixed-Use Development, Urban Transportation Considerations, Zoning By-law Amendment Application, City of Mississauga", dated December 2021 (herein referred to as "December 2021 Report"), which was submitted to the City of Mississauga as part of the initial ZBA and OPA application for the Site.

Following the December 2021 Report, comments have been received from the City of Mississauga and Region of Peel in relation to the Project's transportation related items, through a consolidated matrix dated August 25, 2022.

A resubmission is now being made to the City of Mississauga providing refined development plans, and supplementary materials that respond to the City of Mississauga and Region of Peel's staff comments that are in relation to the transportation related items.

We note that the development programme has slightly changed since the initial submission. The proposed development now consists of a 9 -storey mixed-use building with approximately 444 residential units and a retail component with a GFA of $1,423 \mathrm{~m}^{2}$ at grade, whereas the initial submission contained 390 residential units and a retail component with a GFA of $1,198 \mathrm{~m}^{2}$ at grade.

### 1.2 SCOPE OF REVIEW

BA Group has undertaken an updated review of the key transportation related aspects (i.e. traffic, parking, loading and bicycles) of the proposed ZBA and OPA application being submitted to the City of Mississauga to permit the proposed development. Key transportation related aspects reviewed include:

## Transportation Context

- A description of the existing transportation context of the Site considering the area road network, transit system and other non-automobile dependent travel options;
- A description of any future transportation related changes / improvements to the area context (i.e. transit improvements, other non-automobile dependent travel options, etc.);


## Development Plan

- An overview of the integrated on-Site and area physical and operational transportation elements and strategies that enable the minimization of automobile-dependent travel for prospective residents, and visitors while meeting the practical and operational needs of mixed-use development;
- A review of the transportation elements of the proposed development plan including vehicular access and circulation, loading, and parking facilities;


## Site Planning

- A review of the adequacy of the vehicular parking supply provisions of the proposed development plans;
- A review of the adequacy of the loading space provisions for the proposed development plans;
- A review of the bicycle parking supply provisions for the proposed development plans;
- A review of the functionality and appropriateness of the proposed vehicular facilities incorporated into the Site Plan including access, pick-up/drop-off and loading / garbage collection facility arrangements;


## Travel Demand Forecasting

- Assessment of the existing traffic activity patterns and volumes in the study area during the key weekday morning and afternoon peak periods;
- A comprehensive review of traffic changes that may occur in the area in the future with the development of a number of other area development projects;
- An assessment of the traffic and other trip generation characteristics of the proposed development;


## Traffic Operations Review

- A review of traffic operations at intersections in the area under existing and future conditions including an assessment of the operational impacts of the proposed development; and
- A review of community related traffic impacts of the proposed redevelopment.

Responses to public agency transportation related comments on the application are also provided in Section
4.0.

### 2.0 EXISTING SITE CONTEXT

The Site is currently known as the "Streetsville Plaza". The Streetsville Plaza contains the following stores and services: Qasimul Uloom (Islamic Culture) Centre, Erum's Creations, Evan’s Variety store, Streetsville Martial Arts Karate, Belmonte Unisex Salon Hairstylists, Tulipz Spa, Queen Street Burger and Taters, Mediterranean Meats \& Deli, Smart Vacuum Plus, Baghad Pastries \& Catering, Offside Sports Bar and Roti Vybz. In addition to the stores and services located within the commercial plaza, there is an existing parking lot in front of the retail frontage that can be accessed from Queen Street North.

There is currently one driveway onto Queen Street North today. Internal vehicular connections are also provided to the properties to the north and south. Currently, there are sidewalks provided along both sides of Queen Street North in front of the parking lot.

The Site location and context are illustrated in Figure 1 and Figure 2.


FIGURE 1 SITE LOCATION


FIGURE 2 SITE CONTEXT

## $3.0 \quad$ PROPOSED DEVELOPMENT

### 3.1 DEVELOPMENT OVERVIEW

The proposed development is a 9-storey mixed-use building with approximately 444 residential units and a retail component with a GFA of $1,423 \mathrm{~m}^{2}$ at grade. The Site Plan is illustrated in Figure 3, and reduced scale architectural plans are included in Appendix A.

The following section provides an overview of the development programme that is currently being proposed for the Site.

### 3.2 PARKING PROVISIONS

### 3.2.1 Vehicular Parking

The applicant is proposing to provide a total parking supply of 359 parking spaces, including 311 residential parking spaces, 22 residential visitor parking spaces, 26 retail parking spaces. In addition to the overall parking supply, six (6) tandem parking spaces are proposed. Parking is provided in an underground two-level parking garage.

A total of 170 parking spaces, including 26 retail spaces, 22 residential visitors and 122 residential spaces are located in the P1 level. A total of 189 residential spaces are located in the P2 level. In addition, the six (6) tandem spaces are located in the P2 level of the garage.

In addition to the total parking supply, a pick-up / drop-off loop is proposed which can accommodate approximately $3-4$ vehicles. The PUDO area is provided at-grade adjacent to the residential lobby and the northern retail store of the Site.

### 3.2.2 Bicycle Parking

A total of 386 bicycle parking spaces, including 330 long-term residential bicycle parking spaces and 56 shortterm bicycle parking spaces are proposed for the Site. From the long-term bicycle parking supply, 326 are residential long-term spaces and four (4) are for retail long term spaces. From the short-term bicycle parking supply, 48 are residential short-term spaces, and eight (8) are short-term spaces.

All bicycle parking is provided on the ground floor. The total residential long-term bicycle parking spaces are located in a secure bicycle parking room located at-grade. The total residential short-term bicycle parking spaces are located in another separate bicycle parking room located at-grade. Access to the residential longterm and short-term bicycle storage rooms are provided from the path provided south of the site. The pathway connects east of Queen Street North.

The 12 retail bicycle parking spaces including the four (4) long-term and eight (8) short-term bicycle parking spaces are located outdoors at-grade in front of one of the southern retail spaces along the site frontage of Queen Street North.

### 3.3 LOADING AND GARBAGE COLLECTIONS FACILITIES

Two loading spaces are proposed to be located at-grade adjacent to the planned northeast driveway. A garbage room is proposed to be located in front of the loading space closest to the driveway.

### 3.4 SITE ACCESS

### 3.4.1 Vehicular Access

Vehicular access is currently provided via a driveway onto Queen Street North roughly mid-block. The proposed access would shift the access to the north end of the property. This is opposite to an existing driveway to the Petro Canada Gas Station located on the west side of Queen Street North. The proposed driveway would extend into the Site providing connections to the consolidated loading area and the ramp to the underground parking garage.

### 3.4.2 Bicycle Access

Access to the residential long-term and short-term bicycle storage rooms are provided from the path provided south of the site. The pathway connects east of Queen Street North.

Access to the six (6) retail bicycle parking spaces is provided from the sidewalks along Queen Street North.

### 3.4.3 Pedestrian Access

Pedestrian access to retail entrances and the residential lobby is provided through sidewalk connections along Queen Street North. and the perimeter of the building such as the pathway provided south of the Building.

### 3.5 CHANGES TO THE DEVELOPMENT PROPOSAL

Since the initial submission presented in the December 2021 Report, the development proposal has slightly changed. Key differences from the initial submission to the current development proposal presented in this Report herein is listed below:

- Unit Change: Increase of 54 units
- Retail GFA: Increase of $227 \mathrm{~m}^{2}$
- Vehicle Parking Supply: Decrease of 216 parking spaces (not including tandem spaces)
- Bicycle Parking Supply: Increase of 86 bicycle parking spaces

A comparison of the initial development proposal is summarized in Table 1.

## TABLE 1 DeVELOPMENT PROPOSAL SuMMARY

| Use |  | December 2021 Proposal ${ }^{1}$ | Current Development Proposal ${ }^{2}$ | Differences |
| :---: | :---: | :---: | :---: | :---: |
| 曲 | Residential Units | 390 units | 444 units | + 54 units |
| IIIII | Retail | 1,196 m ${ }^{2}$ | 1,423 m ${ }^{2}$ | + $227 \mathrm{~m}^{2}$ |
|  | Vehicular Parking | 453 residential spaces 79 visitor spaces <br> 43 retail spaces <br> 26 tandem spaces <br> Total:575 spaces (not including tandem spaces) | 311 residential spaces 22 visitor spaces <br> 26 retail spaces <br> 6 tandem spaces <br> Total: 359 spaces (not including tandem spaces) | -142 residential spaces -57 visitor spaces -17 retail spaces -20 spaces <br> Total: -216 spaces (not including tandem spaces) |
| cto | Bicycle Parking | 236 long-term spaces 64 short-term spaces <br> Total: 300 spaces | 330 long-term spaces 56 short-term spaces <br> Total: 386 spaces | +94 long-term spaces -8 short-term spaces <br> Total: +86 spaces |
|  | Loading | 1 retail space <br> 1 residential space <br> Total: 2 loading spaces | 1 retail space 1 residential space <br> Total: 2 loading spaces | No difference |
| $A$ | Vehicular Access | Vehicular access is provided from the driveway extending from Queen Street North. | Vehicular access is provided from the driveway extending from Queen Street North. | No difference |
| $\dot{x}$ | Pedestrian Access | Pedestrian access is provided along the existing sidewalks on Queen Street North. | Pedestrian access is provided along the existing sidewalks on Queen Street North. | No difference |
| Based on Site statistics provided by A\&Architects Inc. dated December 1, 2021. Based on Site statistics provided by A\&Architects Inc. dated June 19, 2023. |  |  |  |  |



FIGURE 3 PROPOSED SITE PLAN

### 4.0 RESPONSE TO COMMENTS

A consolidated comment matrix was received with a compilation of comments received from the City of Mississauga and the Region of Peel in regards to the OPA and ZBA application for the Site, dated August 25, 2022. Within the comment matrix, it's been noted that different departments of the City of Mississauga and the Region of Peel have provided comments on different dates.

The following section provides a response to the OPA / ZBA comments in relation to the transportation related elements of the application. These comments are addressed in the following sections, and responses have been organized by comment with a summary discussion provided in each case which refers, as appropriate, to technical materials provided within this report.

### 4.1 CITY OF MISSISSAUGA

City of Mississauga staff have provided comments on the following dates identified in the consolidated comment matrix:

- Fire Prevention Plan Examination - May 4, 2022
- Parking - May 26, 2022
- Planner, Development Design - June 27, 2022
- Traffic - December 23, 2021


### 4.1.1 Fire Prevention Plan Examination

## Comment 9:

Please show the roadway and curbs on the site plan (to confirm 15m distance to primary entrance).

## BA Group Response:

The Site Plan has been revised to indicate curb locations. Refer to the ground floor plan in the architectural plans attached in Appendix A.

### 4.1.2 Parking

## Comment 46:

Subject to the Applicant addressing the comments provided above, staff see merit in the reduced parking standards and staff can support the proposed rates of:

- 1.16 residential parking spaces per condominium apartment unit
- 0.20 visitor parking spaces per condominium apartment unit
- 3.67 commercial parking spaces per $100 m^{2}$ non-residential GFA for retail use.


## BA Group Response:

Noted. The proposed development is seeking a reduced parking supply less than those noted by City Staff and Zoning By-law 0225-2207 (amended) considering the Site's transit context, TDM measures, survey data and other approvals. This is further discussed in Section 7.2 of the report.

## Comment 47:

Staff request the Applicant provide clarification, specific details, and the use of the tandem parking spaces proposed.

## BA Group Response:

In the development programme, six (6) tandem parking spaces are proposed. Spaces in tandem would be owned by a single unit. This allows for cars to be 'jockeyed' to exit and enter the spaces.

## Comment 48:

Staff note that the Parking Regulations Study and the associated new parking rates have been approved by PDC and endorsed by City Council but are not currently in effect. The updated by-law is expected to come into effect in mid-July 2022.

## BA Group Response:

Noted. Refer to Section 7.1.1 which contains the application of the newly amended parking requirements outlined by Zoning By-law 0225-2007 (amended by Zoning By-law 0118-2022) to the Site.

## Comment 49:

Staff note that per the Council endorsed Parking Regulations Study, May 2022, that a minimum required number of Electric Vehicle Ready parking spaces will need to be provided. The associated rates for these are noted in Table 3.1.1.12, Minimum Required Number of Electric Vehicle Ready Parking Spaces, of the draft Zoning By-law Amendment included as part of the Parking Regulations Study.

## BA Group Response:

Noted. Electric vehicle (EV) ready parking spaces have been provided in accordance with the requirements outlined in Zoning By-law 0225-2007 (amended by Zoning By-law 0118-2022). Refer to Section 7.2.2 that speaks upon the proposed EV ready parking spaces with relation to the proposed parking supply. The Site's EV ready parking supply exceeds the minimum requirement.

## Comment 50:

Staff commend the Applicant for considering the provision of TDM measures on site; however, staff request further details. Staff request the Applicant provide clarification, specific details and commitments as to how these measures will be provided and implemented on site.

## BA Group Response:

Noted. TDM Measures will be used to support mobility on Site through various travel modes and reduce auto dependency and the necessity for parking. These include: good pedestrian connections, bicycle parking, bicycle repair stations, a transit screen, transit passes, travel brochure, lowered parking rates, access to ridesharing programs, and smart lockers. Further details regarding the TDM strategy are included in Section 6.0 of the report.

### 4.1.3 Planner - Development Design

## Comment 118:

Proximity to entrance underground ramp and garbage collection area is such that conflicts could arise with vehicles exiting the underground while waste collection is occurring. The applicant is encourage to revisit the proximity of these features to alleviate that conflict.

## BA Group Response:

A warning system is proposed to alert motorists exiting the parking garage of loading activity as discussed in Section 9.2. Please refer to the pavement marking and signage plan in Appendix B for more information.

## Comment 126:

MTSA: The Streetsville GO Station is a Planned Major Transit Station Area (MTSA) and the boundaries have not yet been delineated. Further study is required to determine the boundaries of the MTSA. Regardless of the ultimate delineation these lands are outside of the 800 m radius of the Streetsville GO Station.

## BA Group Response:

Noted. The Region of Peel's Official Plan (2022) indicates that an 800 -metre radius around stations is used as the initial area to be assessed when MTSAs are identified and to guide delineation. The Site is located within a 2 -kilometre radius of the Streetsville GO Station, and thus falls outside the typical 800 -metre radius of a MTSA.

### 4.1.4 Traffic

## Comment 92 A - General:

(i) The report must be stamped, dated, and signed by a Professional Engineer Licensed in the Province of Ontario (P. Eng).
(ii) All traffic volume figures are to be revised to illustrate northbound left volumes at the intersection of Britannia Rd \& Earl St.

## BA Group Response:

(i) The revised report has been stamped by a Professional Engineer.
(ii) All traffic volume figures have been revised to illustrate northbound left-turn volumes at the intersection of Britannia Road/ Earl Street.

## Comment 92 B - Site Access:

(i) As per the Terms of Reference, the report is required to review proposed site access and ensure that it conforms to all TAC standards (e.g. corner clearances, clear throat lengths, vehicular \& pedestrian sight line distances, proximity/alignment to other driveways/roads, ensuring appropriate driveway/intersection offsets to avoid interlocking left-turns, etc.). Provide confirmation within the report on whether the site access will operate safely.

## BA Group Response:

The site access was reviewed against design parameters provided in the Geometric Design Guide for Canadian roads produced by TAC. Corner clearances, sight lines, and alignment with opposing driveways are
appropriate. The minimum clear throat length to the pick-up/ drop-off facility is below the TAC guidelines values. We believe this is reasonable in this context given the low volumes associated with the pick-up / drop-off area and its queuing capacity. This is further discussed in Section 10.0.

## Comment 92 C - Existing Conditions:

(i) Area Road Network Some of the information within Table 1 is incorrect. For example, Queen Street North and Queen Street South should be noted as Major Collector and Major Collector (Scenic Route) roads, respectively. Matlock Avenue and Swanhurst Boulevard should be noted as Local roads. Queen Street North becomes Mississauga Road north of the OQ railway tracks and becomes Queen Street South, south of Britannia Road. Queen Street South becomes Mississauga Road at the CP railway tracks. The posted speed limit for Matlock Avenue and Swanhurst Boulevard should be noted as 40km/h. Please review all information contained in Table 1 and revise accordingly. Likewise, please update Figure 4 such that the road classifications are consistent with the Official Plan.

## BA Group Response:

Noted. Table 2 has been revised in accordance with Comment 92 C. Figure 4 has also been updated to match Table 2. Its noteworthy to mention that in the City of Mississauga's Official Plan's Schedule 5: LongTerm Road Network Plan, Matlock Avenue and Swanhurst Boulevard are illustrated as minor collector roads.

## Comment 92 D - Future Background Conditions:

(i) Background Developments 6, 10 and 12 Queen Street South, 16 James Street, 2 William Street and 0 William Street (OZ/OPA 21 14) must be considered as a background development.

## BA Group Response:

Noted. the background developments located at 6, 10 and 12 Queen Street South, 16 James Street, 2 William Street and 0 William Street (OZ/OPA 21 14) have been considered as part of the background development traffic in the revised traffic analysis. Refer to Section 11.2.2 in the report for more details.

## Comment 92 E - Site Traffic:

(i) Trip Distribution The report notes that existing traffic survey patterns were considered. However, its unclear why such a small percentage of trips are assigned to/from Britannia Road, particularly for the retail traffic component.
(ii) Existing site traffic - Existing site trips should be removed from the background traffic volumes, rather than the proposed development trip generation / site traffic volumes. Please revise the report accordingly.
(iii) Retail Trip Generation Please justify the appropriateness of using LUC 822 to calculate the projected retail component of the site traffic.
(iv) Modal Split \%s Did the TTS mode split query only include Apartment dwelling types? If not, why?
(v) Modal Split Reduction Why was a non-auto modal split reduction not applied to the vehicular trip generation?

## BA Group Response:

(i) The retail trip distribution has been revised as part of the updated analysis and is based on afternoon existing traffic patterns as there are more retail-based trips occurring than in the morning peak hour.
(ii) The future background scenario represents the 'do nothing' case for the Site. Existing site trips, where were captured in traffic counts prepared on behalf of BA Group, are removed for the future total scenario only. (iii) Land use code 822 (Strip Retail Plaza <40k sqft) was chosen as the land use that could most closely represent the retail provided on Site. Given the gross floor area of the on-Site retail is well below 40,000 sqft, other land use codes such as 820 (Shopping Center) and 821 (Strip Retail >40k sqft) are not appropriate. Other land use codes, including 814 (Variety Store) and 851 (Convenience Store) were considered for this, however the distribution of rates ( $R^{2}$ value) was very low or not available - indicating insufficient trends in the data to provide an accurate projection. Land use code 231 (Mid-Rise Residential with Ground-Floor Commercial) was also considered, however, no data was available for vehicular trips (walk + bike + transit only). Therefore, land use code 822 was considered the closest match for this site and is generally considered to be conservative.
(iv) The modal split TTS query included all home-based trips and was not apartment specific. This was due to only 20 data points being available for apartment specific trips in this area. Generally, 100 datapoints is considered a good minimum to obtain accurate results.
(v) The revised traffic analysis includes updated trip generation in accordance with the method outlined in the ITE Trip Generation Handbook (3 $3^{\text {rd }}$ Edition). Accordingly, a mode split reduction was applied to the baseline selected ITE trip generation calculations, to adjust the baseline vehicle trip generation for the local area. Updated trip generation projections are included in Section 11.3.3.

## Comment 92 F - TDM:

(i) Section 4 includes a list of Potential and Recommended Site TDM Measures. However, the report needs to specify which TDM measures are proposed as part of the development. The TDM measures need to be specific and included in the Conclusion/Recommendation Section. All TDM measures shall be the responsibility of the Owner. (Refer to Traffic Comment \#93 for additional TIS comments)

## BA Group Response:

Noted. Section 6.0 of the report discusses the recommended TDM measures proposed for the Site, and implementation details per measure. All proposed TDM measures shall be the responsibility of the Developer / Applicant.

## Comment 93 G - Truck Access \& Circulation:

(i) As per the Terms of Reference, it must be ensured that truck traffic (garbage/loading) can enter and exit the site in a forward motion and access to the garbage and loading areas are functional. Truck turning movements are to be illustrated with one continuous path with AutoTURN and right-turns in and out of the proposed site access shall be analyzed.
(ii) The site must be able to accommodate the largest design vehicles which will be accessing the property. It appears that there are multiple instances of the design vehicles mounting/striking curbs. Please revise the site design accordingly.
(iii) An evaluation of the parking areas and ramps using a PTAC design vehicle should also be included.
(iv) As revisions to the site design/layout is required, please update the turning movement diagrams in the TIS accordingly.
(v) Please replace the TAC SU analysis with a TAC MSU design vehicle.
(vi) Include a section in the report which details the results of the truck access \& circulation analysis.

## BA Group Response:

(i) Noted. BA Group has prepared vehicle manoeuvring diagrams (VMDs) that confirm the truck traffic can enter and exit the site in a forward motion, and that the access to the loading facilities are functional. Please refer to Section 9.0. Associated vehicle manoeuvring diagrams attached in Appendix C.
(ii) The largest design vehicle accessing the property is a TAC Heavy Single Unit Truck (HSU). Please refer to the vehicle manoeuvring diagrams attached in Appendix C for more information.
(iii) PTAC design vehicle have been tested travelling through the pick-up/drop-off loop and accessing the parking ramp. Please refer to the vehicle manoeuvring diagrams attached in Appendix Cor more information.
(iv) Noted.
(v) Noted. The TAC SU vehicle was replaced with a TAC MSU. Please refer to the vehicle manoeuvring diagrams attached in Appendix C for more information.
(vi) The design vehicles tested within the site are further discussed in Section 9.0.

## Comment 93 H - Additional Comments:

(i) Community Impacts The TIS shall include a section in the report to address Community Impacts. This section shall include summary statements outlining the resulting traffic increases to the critical streets, movements and intersections. Comments or concerns from the community through future public meetings and engagements that are related to traffic shall also be addressed in this section.
(ii) Please submit a revised TIS report addressing all of the TIS comments in PDF format.
(iii) Due to the number and significance of the comments, further comments may be provided in the subsequent submission(s).

## BA Group Response:

(i) A community impact review has been included in Section 13.0. As the Site driveway is onto Queen Street North, there are anticipated to be minimal impacts to local streets. It is further noted that the existing Site contains a retail plaza which generates traffic.
(ii) Noted.
(iii)Noted.

## Comment 94 - Site Access:

(a) The proposed access shall be relocated to align centreline to centreline with the opposing access at 40 Queen Street North. The opposing access shall be illustrated on the plans to demonstrate proper alignment.
(b) The Owner shall ensure the proposed access provides sufficient sight lines such that views are not obstructed at the intersection (street trees, retaining walls, fences, building structures, etc.). This shall be analysed within the revised TIS.
(c) The Owner shall provide for a sufficient clear throat length within the driveway access to ensure the roadway and internal driveway can operate efficiently. The TAC Manual indicates a minimum clear throat length requirement of 25 m for this scenario, whereas a 20 m clear throat length is proposed. No intersecting drive aisles or parking spaces are permitted within the clear throat length. At a minimum, please remove the parking space located closest to the site access.
(d) The site access design shall be revised to ensure that the curb radius does not extend beyond the projection of the property line. Curb radii dimensions must conform to OPSD 350.010 standards.
(e) The site access width shall be revised to be a minimum of 7.0 m .

## BA Group Response:

(a) The proposed site access has been relocated along the north property line and aligns approximately centreline to centreline with the opposing access at 40 Queen Street North.
(b) Compliance with sight lines is further discussed in Section 10.0.
(c) Compliance with the clear throat length is further discussed in Section 10.0.
(d) The site access has been relocated along the north property line so that it aligns approximately centreline to centreline with the opposing access at 40 Queen Street N. The driveway has been designed to conform with the specifications noted in OPSD 350.010. Please refer to the reduced scale architectural plans in Appendix A for more information.
(e) A minimum 7.0m width is proposed for the site access. Please refer to the reduced scale architectural plans in Appendix A for more information.

## Comment 95 - Internal Site Circulation:

(a) Revised turning movement diagrams will be required within the updated TIS to depict the internal site circulation.
(b) Additional provisions to aid in the safety and operation of these features may be required.
(c) Detailed turning movements are to be provided for ingress and egress through the access point for the site.
(d) Confirmation from Fire and Emergency Services that the internal road is acceptable from an emergency response perspective.
(e) Confirmation from the Region of Peel that the internal road is acceptable from a waste collection perspective.

## BA Group Response:

(a) Revised vehicle manoeuvring diagrams are attached in Appendix C.
(b) A warning system that alerts motorists exiting the parking garage to watch for large trucks is provided. Please refer to the pavement marking and signage plan in Appendix B for more information.
(c) Vehicle manoeuvring diagrams entering and exiting the site have been provided. Please refer to the vehicle manoeuvring diagrams attached in Appendix Cor more information.
(d) Noted.
(e) Noted.

## Comment 98-Cycling Facilities:

The Owner will be required to provide accessible and secure short term (outdoor) and long term (indoor) bicycle storage facilities on site. The Site Plan shall be revised to identify the cycling facility locations and to specify the facility detail(s), including quantity of spaces proposed for each. The following rates are to be used:(a) Apartment Mississauga - A minimum of 0.60 long term spaces and 0.05 (6 spaces min.) short term spaces per residential unit. (b) Retail (Per 100 sq.m. GFA of retail area) Mississauga A minimum of 0.10 long term spaces and 0.20 short term spaces.

## BA Group Response:

Noted. A total of 386 bicycle parking spaces are proposed to serve the development, including 326 resident long-term spaces, 48 resident short-term spaces, four (4) retail long-term spaces and eight (8) short-term spaces. The proposed bicycle parking supply meets and exceeds the requirements outlined by Zoning By-law 0225-2007 (amended by Zoning By-law 0118-2022). Refer to Section 8.2 of the report for more details about the proposed bicycle parking supply.

### 4.2 REGION OF PEEL

Region of Peel staff provided comments in a consolidated comment matrix dated May 12, 2022 in relation to the proposed ZBA / OPA application. ZBA/OPA comments are addressed in the following sections, and responses have been organized by the comment number identified in the matrix, with a summary discussion provided in each case which refers, as appropriate, to technical materials provided within this updated report.

## Comment 63:

For the Residential Units - The Region of Peel will provide front-end collection of garbage and recyclable materials subject to Sections 2.0, 4.0, and 5.0 of the WCDSM - Waste Collection Design Standards Manual and the following conditions being met and labeled on the Waste Management Plan Prior to OZ approval: Waste Collection Vehicle Access and Egress Route 1.The turning radius from the centre line must be a minimum of 13 metres and must be shown and labelled on all turns on the revised submission. This includes the turning radii to the entrance and exit of the site, and into and out of the Collection Point. Collection Point Requirements2.The Collection Point should not require the jockeying of front-end bins (i.e. manually positioning one front-end bin at a time for the waste collection vehicle to pick up) by property management staff. Please see Appendix 4 of the WCDSM Waste Collection Design Standards Manual for suggested positioning of bins.3.Bins must be shown staged for collection, only the maximum number of front-end bins to be collected at a time (either garbage or recycling) will need to be shown in the collection area. Please refer to WCDSM Appendix 4 Indoor Waste Collection Point Specifications and recalculate the required area for staging with the specified bin arrangement. For 3 cubic yard front-end bin, the minimum width required is 3 metres for every front-end bin present, with a minimum depth of 2 metres. For 4 cubic yard front-end bins, a minimum depth of 3 metres is required. Indoor Storage Requirements4. Please show and label the Bin type (garbage/recycling) and size in the indoor waste storage room on Waste management plan drawing. The bin calculation must be shown and labelled on subsequent submissions. Please refer to WCDSM Appendix 7 Waste bin calculation or refer to Table 1. Maximum Number of Dwelling Units per Front-End Bin for Garbage by Bin Size and Table 2. Maximum Number of Dwelling Units per Front-End Bin for Recyclable Materials by Bin Size in the Peel Region Waste Collection Design Standards Manual.

## BA Group Response:

Details regarding the waste collection areas are provided in the architectural plans. Supporting truck manoeuvring diagrams are provided in Appendix C.

## Comment 65:

The site design is on its way to contributing to a healthy built form. For further opportunities to enhance the site, we recommend the following for consideration on the future site plan:

- A well designed streetscape improves the safety, the comfort and the convenience of travelling by foot or bike and makes the public space more inviting. We support the design of the entrance's points from the proposed buildings to face the streetscape. A recommendation within our health assessment suggests that this built form design will promote walkability for pedestrians within the neighbourhood. Similarly, the locations and design of sidewalks and pathways should be strategically located to connect to community amenities and surrounding sidewalks.
- We recommend the inclusion of secure long and short-term bicycle parking on site for residents and visitors.
- Please consider reduced parking in favour of car share and carpool spots.


## BA Group Response:

Noted. The proposed development contains a well-designed streetscape along Queen Street North and provides a pedestrian pathway south of the building that connects to Queen Street North for cyclists to access the bicycle storage room conveniently located at-grade and pedestrians can access the building's interior corridor. This pathway will be well-lit for cyclists and pedestrians to promote safety and visibility. The retail frontage contains entry points from Queen Street North. The residential lobby is located in front to the PUDO area and contains a connection to the existing sidewalk along the Site's frontages.

Bicycle parking including long-term and short-term spaces that meets and exceeds the bicycle parking requirements outlined in the Zoning By-law is also being proposed as part of this updated submission. Refer to Section 8.2 that speaks upon the proposed bicycle parking for the Site.

As part of this proposed development programme, a reduced parking supply from the Zoning By-law 02252007 is being proposed, which is supported by the TDM plan in place and existing area transportation context.

## Comment 66:

The Sustainable Transportation Strategy recognizes and identifies Peels role in increasing the proportion of trips made by walking, cycling, transit, carpooling Please refer to the Regions Healthy Development Assessment and the City of Mississauga Bicycle Parking Zoning By-Law for recommended short term and long-term bike parking for retail and residential purposes Provide sidewalk and cycling route connections (curbs are cut) through the property and suggest confirming lighting conditions meet current standards for pedestrian/cycling ways and walkways to make walkers/cyclists visible to vehicle users and provides a safer environment. Suggest the installation of EV charging stations for micro-mobility devices (e-scooter, e-bike, ecar) in public spaces and designate micro-mobility parking area so devices do not impede the pedestrian clearway.

## BA Group Response:

Noted. A strong, robust TDM plan is in place to support the proposed development, which includes the provision of long-term and short-term bicycle parking for both residential and retail uses, safe pedestrian connections, and more. Refer to Section 7.2.2of this Report for further details outlined in the proposed TDM plan.

In addition, EV parking has been provided to meet the EV ready parking standards outlined in the by-law. The location of the EV ready parking spaces are annotated in the underground parking plans in the architectural plans, which are attached in Appendix A for reference.

### 5.0 TRANSPORTATION CONTEXT

The existing area street network, transit and cycling context, and planned cycling context are provided in the following sections.

### 5.1 AREA ROAD NETWORK

### 5.1.1 Existing Area Road Network

A description of the existing roads within the local area road network is provided in Table 2.
Figure 4 illustrates the existing road network, and Figure 5 shows the existing lane configuration and traffic control.

## Table 2 Area Road Network

| Street Name |  | Road Cross Section | Parking Regulations | Posted Speed | Description |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 5 lanes (including the centre two-way left turn lanes) | No parking at any time. | $60 \mathrm{~km} / \mathrm{h}$ | Queen Street North is a north-south major collector road which runs from the CP railway tracks in the north to Britannia Road in the south. Queen Street North becomes Mississauga Road in the north at the CP railway tracks. |
|  |  | 2 lanes (with the addition of turn lanes) | No parking at any time. | $40 \mathrm{~km} / \mathrm{h}$ | Queen Street South is a north-south major collector road that extends from Queen Street North to the north and Reid Drive to the south. Queen Street South becomes Mississauga Road in the south at the CP railway tracks. <br> Generally, Queen Street South is a 2-lane road. At the Britannia Road West / Queen Street South and North intersection, the road cross section for Queen Street South is a fivelane road with the addition of a left turn lane, and a shared through and right turn lane. |
|  |  | 2 lanes | On-street parking is permitted. | $40 \mathrm{~km} / \mathrm{h}$ | Matlock Avenue is an east-west local road that runs from Queen Street north to the west and Swanhurst Boulevard to the east. |
|  |  | 2 lanes | On-street parking is permitted. | $40 \mathrm{~km} / \mathrm{h}$ | Swanhurst Boulevard is a north-south local road that runs from Ellesboro Drive to the south and Suburban Drive to the north. |
|  |  | 4 lanes (with the addition of turn lanes) | No parking at any time. | $50 \mathrm{~km} / \mathrm{h}$ | Britannia Road West is an east-west regional arterial road that runs from Milburough Line to the west and Kennedy Road to the east. <br> Generally, Britannia Road West is a 4-lane road. At the Britannia Road West / Queen Street South and North intersection, the road cross section for Britannia Road West is a sixlane road with the addition of a left turn lane, and a right turn lane. |



FIGURE 4 EXISTING AREA ROAD NETWORK


FIGURE 5 EXISTING LANE CONFIGURATION AND TRAFFIC CONTROL

### 5.2 AREA TRANSIT NETWORK

### 5.2.1 Existing Transit Network

The City of Mississauga municipal transit provider is MiWay. The Site is currently well served by various MiWay bus routes. In addition, the Streetsville GO station is located approximately 2 kilometres from the Site and can be easily reached within approximately 14 minutes by taking the 44 bus. The Site is located approximately:

- 180 metres from Queen Street North at Matlock Avenue bus stop for the 43 and 44 bus route;
- 210 metres from Britannia Road at Queen Street North bus stop for the 10, 39 and 87 bus route; and
- 240 metres from Queen Street South at Britannia Road bus stop for the 306 bus route.

A summary of the transit services operating in the area is provided in Table 3. The area transit services are illustrated in Figure 6.

## Table 3 Area Transit Network

| Route | Nearby Stops | Headways | Route Description |
| :---: | :---: | :---: | :---: |
| Mi-Way |  |  |  |
| 43 | Queen Street North at Matlock Avenue <br> (~180 m / 2 minute walking distance) | Approximately 45 minutes during all periods | The 43 bus route begins from Commerce Boulevard at Renforth Station and ends in Meadowvale Town Centre Drop Off. The bus route operates from Monday - Friday and does not operates on weekends. For the northbound route, the operational time periods are from 5:15 AM 10:12 AM and for the southbound route the operational routes are from 2:42 PM - 7:34 PM. |
| 44 | Queen Street North at Matlock Avenue <br> (~180 m / 2 minute walking distance) | Approximately 22 minutes during all periods | The 44 bus route begins from University of Toronto at Mississauga Campus and ends in Meadowvale Town Centre Drop Off. Operates every day of the week. |
| 10 | Britannia Road at Queen Street North (~210 m / 3 minute walking distance) | Peak Hours: 18 minutes <br> Off-Peak: 25 minutes | The 10 bus route begins from City Centre Transit Terminal Platform J ending in Meadowvale Town Centre Drop Off. Operates every day of the week. |
| 39 | Britannia Road at Queen Street North <br> (~210 m / 3 minute walking distance) | Peak Hours: 23-25 minutes <br> Off Peak: 25-30 minutes | The 39 bus route begins from Meadowvale Town Centre Bus Terminal Platform E and F, and ends in Renforth Station East Platform 7. Operates every day of the week. |
| 87 | Britannia Road at Queen Street North (~210 m / 3 minute walking distance) | Approximately 42 minutes during all periods | The 87 bus route begins from Skymark Hub and ends in Meadowvale Town Centre Drop Off. Operates Monday Friday from 3:46 PM - 8:01 PM and does not operates on weekends. |
| 306 | Queen Street South at Britannia Road (~240 m / 3 minute walking distance) | No headways available as there is only one bus per day. | The 306 bus route begins from Winterton Way at Mavis Road and ends at Joymar Drive at Tannery Street. Operates Monday - Friday only at 7:27 am. |
| GO Transit |  |  |  |
| 21 Route / Milton Line | Streetsville GO Station (~2 km / 27 minute walking distance) | Peak Hours: 30 minutes <br> Off-Peak: 1 hour | The 21 GO bus Route begins at Milton GO and ends at Union Station in Toronto and operates during off-peak periods. During peak periods, the Milton train runs a similar route with a stop at Streetsville GO station. The train operates on weekdays and the bus route operates both on weekdays and weekends. |



FIGURE 6 EXISTING TRANSIT CONTEXT

### 5.3 AREA CYCLING NETWORK

### 5.3.1 Existing Cycling Infrastructure

The Site is well-connected from a cycling perspective as multiple cycling routes exist within an 800 metre radius of the Site. Cycling facilities include bike lanes, signed routes and multi-use trails. Table 4 lists the characteristics of cycling routes within the local area of the proposed development.

Table 4 Area Cycling Network

| Route | Cycling Infrastructure | Description | Image ${ }^{1}$ |
| :---: | :---: | :---: | :---: |
| North-South Bicycle Connections |  |  |  |
| Queen Street South <br> From Queen Street South / Britiannia Road West to Plaza's Driveway / Queen Street South | Buffered Bike Lane with a painted buffer to separate cyclists and vehicular traffic | A bike lane is provided along both sides of Queen Street South. Bike lanes travelling southbound and northbound are extended from Britannia Road West to a plaza's driveway right before the Tannery Street / Queen Street South intersection. | Bike lane along Queen Street South facing South |
| Joymar Drive <br> From <br> Britannia <br> Road West / Joymar Drive to Joymar Drive / <br> Thomas Street | Signed Route | The signed route is provided along both sides of Joymar Drive from Britannia Road West / Joymar Drive to Joymar Drive / Thomas Street. |  |
| Riverview <br> Park Trail <br> From <br> Britannia <br> Road West to <br> Pine Cliff <br> Drive | Multi-use Trail | This multi-use trail provided in Riverview Park connects from Britannia Road West to Pine Cliff Drive. Within this trail, there are bicycle friendly roads that connect the trail to Shady Lawn Court and Sir Monty's Drive. | Multi-use Trail's entrance from Britannia Road West |


| Route | Cycling Infrastructure | Description | Image ${ }^{1}$ |
| :---: | :---: | :---: | :---: |
| East - West Bicycle Connections |  |  |  |
| Britannia Road West <br> From <br> Britannia <br> Road West / <br> Queen Street <br> South to <br> Britannia <br> Road West / <br> Hurontario <br> Street | Multi-use Trail | A multi-use trail is provided along the south side of Britannia Road West and extends to Hurontario Street. The multi-use trail is shared with pedestrians. | Multi-use trail along Britannia Road West facing East |

Notes:

1. Images obtained from Google Maps Street View, 2021.

### 5.3.2 Planned Cycling Infrastructure

In 2018, the City of Mississauga has approved the update to the Cycling Master Plan from 2010. This updated Master Plan provides a recommended bicycle route network of shared roadways (signed bicycle routes and sharrows), conventional bicycle lanes, boulevard multi-use trails, and off-road trails. In addition, this updated plan recommends policies and programs that will support cycling by all types of cyclists. This Cycling Master Plan is also aligned with the approved Vision Zero plan in which aids in designing a comfortable cycling network that is suitable for cyclists of all ages.

Within an 800 metre radius, the existing cycling network is further connected through the proposed cycling infrastructure as recommended in the City of Mississauga Cycling Master Plan (2018). The existing multi-use trail along Britannia Road West which begins from Britannia Road West / Queen Street South is planned to be extended to the existing multi-use Trail along Britannia Road West beginning from Britannia Road West / Erin Mills Pkwy. Cycle tracks are proposed to be extended north from Queen Street South / Britannia Road West along Queen Street North and Mississauga Road. A new bicycle lane is proposed along Falconer Drive connecting from the new cycle track along Queen Street North. Another cycle track is proposed along Mill Creek Drive connecting from the signed bike route along Joymar Dr. The proposed cycling infrastructure mentioned above will improve connectivity for cyclists in the area.

The existing and planned area cycling network is shown in Figure 7.


FIGURE 7 EXISTING AND PROPOSED CYCLING CONTEXT

### 5.4 AREA PEDESTRIAN CONSIDERATIONS

## Surrounding Area

The Site is surrounded by various commercial stores, services, restaurants, schools and parks. The Site is located along Queen Street North which offers a strip of various pedestrian destinations such as commercial stores, restaurants and services. In addition, the Site is surrounded by residential homes to the northeast and southeast. The following is a list of the pedestrian destinations located within 500 metres of the Site:

- Streetsville Square (Prestige Pools, Big Slick Bar \& Billards, AAA Teen Drivers, Carolyn's model \& talent agency, Matthew Oberc Accounting and Taxation, UK Insurance, Hot Hounds Outfitters \& Spa, RR Supermarket, Randhawa Law Office and Asian \& Indian Groceries)
- Streetsville Home Hardware;
- Several Restaurants (Latin Super Chicken, Chinese Restaurant Wings, Shawarma Hut, Traditional Fish \& Chips, Bobby's Hideaway, and Dairy Queen Grill \& Chill);
- Portuguese Cultural Centre of Mississauga;
- Streetsville Denture Clinic;
- The Beer Store;
- The Church in Mississauga;
- Schools (Ray Underhill Public School and Dolphin Senior Public School) and
- Parks (Riverview Park and Frank Dowling Park).


## Pedestrian Crossings

Adjacent to the Site, there is a signalized intersection at Queen Street North / Britannia Road West with marked pedestrian crossings adequately facilitating pedestrian movement in a safe manner. Within 500 metres of the Site, there are several signalized intersections with pedestrian movement at all four approaches. Other intersections surrounding the Site are unsignalized with crossings in most situations provided in the north-south direction; such intersections include Matlock Avenue / Queen Street North.

## Sidewalks

Most roads within the Site vicinity have sidewalks along both sides of the road, except along the plaza's driveway. The sidewalks on Queen Street North within the immediate Site vicinity have a buffer of vegetation between traffic and the sidewalk, providing a degree of safety for pedestrians.

The area pedestrian context is illustrated in Figure 8.


FIGURE 8 AREA PEDESTRIAN DESTINATIONS

### 5.5 CAR SHARE AVAILABILITY

There are two primary car sharing companies operating in the City of Mississauga (Zip Car and Enterprise CarShare) which each offer their members access to vehicles. Both of these programs have acquired parking spaces for their vehicles either in private garages or public parking lots. Vehicles rented from either of these programs must be picked up and returned from the same parking space.

There are no Zipcar nor Enterprise vehicles available within a close walking distance to the Site. However, within 2 km of the Site, there is an Enterprise location with 19 vehicles available.

### 5.6 AREA TRAVEL BEHAVIOUR - MODE SHARE

To understand existing travel characteristics and patterns of the Site surrounding area, Transportation Tomorrow Survey data has been reviewed for the general Site area. The Transportation Tomorrow Survey (TTS) is a comprehensive travel survey that is conducted in the Greater Toronto and Hamilton Area (GTHA) once every five years. The data set used for analysis is based upon information from the 2016 survey year.

A review of the travel characteristics of residential trips being made to / from the area during weekday peak periods is provided in the following sections. Travel behaviour characteristics for resident (home-based) travel during peak periods are summarized in Table 5.

Table 5 Area Residential Mode Split (2016 TTS Zones - 3715, 3717, 3718 and 3836)

| Mode | Morning Peak Period <br> Outbound | Afternoon Peak Period <br> Inbound |
| :--- | :---: | :---: |
| Auto Driver | $64 \%$ | $67 \%$ |
| Auto Passenger | $17 \%$ | $19 \%$ |
| Transit | $13 \%$ | $10 \%$ |
| Cycle | $0 \%$ | $0 \%$ |
| Walk | $6 \%$ | $4 \%$ |

Notes:

1. Based on 2016 TTS results for morning (6:00-8:59) and afternoon (15:00-17:59) peak traffic periods for TTS 2006 GTA Zones 3715, 3717, 3718 and 3836.
2. Auto passenger trips (includes auto passengers, school bus passengers and taxi passengers).

The 2016 TTS survey confirms a substantial proportion of travel is undertaken by using an automobile during the weekday morning and afternoon peak periods with approximately $81 \%$ and $86 \%$ residential trips being undertaken by an automobile. The existing travel mode characteristics present an opportunity to shift travel patterns away from auto dependency towards active and sustainable modes of travel. This shift can be supported through a Travel Demand Strategy for the Site as discussed in Section 6.0 as well as the continuing improvement of cycling and transit services and infrastructure in the area.

Detailed TTS queries for travel characteristics are attached in Appendix D.

### 6.0 TRANSPORTATION DEMAND MANAGEMENT

A central element of the transportation strategy for the proposed development will be the adoption of a sustainable transportation demand management (TDM) Plan for the project that will attempt to influence the way people travel to and from the site through a comprehensive suite of TDM strategies.

These measures will include the application of various Site design elements, alternative transportation offerings, property management, and operational policies, each of which have the goal of redistributing and reducing the travel demand of the project. Specifically, the primary goal is to reduce the overall reliance on single-occupant vehicles (SOV) while promoting the use of more active and sustainable modes of transportation.

Generally, this TDM Plan has three primary objectives:

1. Reduce car dependence and the need for everyday SOV travel;
2. Improve pedestrian / cycling convenience to encourage non-automobile modes of transportation; and
3. Promote low-carbon modes of transportation, such as car-sharing and transit.

The Site has the potential to set a sustainable precedent of urban development in Mississauga. The City of Mississauga's strategic plan - Our Future Mississauga - states the aspiration for the City to be one where people can travel without an automobile, where transit is promoted as a preferred, affordable, and accessible choice, and to provide all people with the choice to walk, cycle, or use transit because these options will be desirable and convenient. The TDM Plan aims to leverage the advantages imbedded within the design of the proposed development (i.e. it will be a compact, mixed-use development) to achieve its objectives.

### 6.1 TDM PLAN STRATEGIES AND INITIATIVES

The TDM Plan will serve as an initial guide for the design, development and implementation of the Site, as well as the ultimate operation of the facilities over time to maximize the travel demand sustainability of the project and allow the development to fully leverage its location relative to the growing range of employment, retail, recreation and residential uses in the vicinity of the Site. Strategies have been developed to support the use of non-auto modes of travel, and to encourage a change in travel behaviour that reduces automobile travel.

The proposed TDM strategies and its implementation are outlined in Table 6.

## Table 6 Recommended Site TDM Measures

| TDM Measure | Overview | Impact | Implementation |
| :---: | :---: | :---: | :---: |
| Pedestrian and Cycling Related |  |  |  |
| Pedestrian Connections | Provide public pedestrian sidewalks on all new public streets within the Project's boundaries. <br> A pedestrian / cyclist pathway is provided south of the building to provide pedestrians with a safe access to the bicycle parking facilities on-site. The pathway will contain adequate lighting. | Improve pedestrian and cycling convenience to encourage non-automobile modes of transportation. | Integrated into the building. |
| Provision of Bicycle Parking | As outlined in Section 8.2, a total of 386 bicycle parking spaces, including 330 longterm bicycle parking spaces and 56 shortterm bicycle parking spaces are proposed for the Site. The proposed bicycle parking supply meets and exceeds the applicable bicycle parking standards as per the amended Zoning By-law 0225-2007. | Improve pedestrian and cycling convenience to encourage non-automobile modes of transportation. | Integrated into the building. |
| Bicycle Repair Stations | Two bicycle repair/ maintenance stations will be provided on-site. This allows residents to change tires, inflate tires, adjust seat, etc. | Improve pedestrian and cycling convenience to encourage non-automobile modes of transportation. | Integrated into the building. |
| Transit Related |  |  |  |
| Transit Screen | The implementation of a transit information screen which will be displayed in the building's residential lobby. It provides realtime information on transit schedules, walking and cycling routes amongst other items. | Promote car-sharing and transit. | To be purchased by the Developer and be placed strategically in the lobbies. |
| Provision of Transit Pass | Provide pre-loaded Presto Cards with a value of $\$ 50$ to each first-time unit owner. | Promote car-sharing and transit. | To be purchased by the Developer and be distributed to the first-time owners at the time of occupancy. |
| Travel Information Brochures | Provide a travel information brochure to residents providing an overview of transportation (walk, cycle, car-share, transit, and car-pool opportunities) in the area. | Reduce car dependence and the need for everyday travel. <br> Improve pedestrian and cycling convenience to encourage non-automobile modes of transportation. <br> Promote car-sharing and transit. | To be prepared by the Developer and be distributed to the first-time owners at the time of occupancy. |
| Automobile Infrastructure |  |  |  |
| Lower Parking Rates | A reduced parking rate on-site is proposed. | Reduce car dependence and the need for everyday travel. | Secured through rezoning process. |


| Ride-Sharing Program | Explore opportunities to offer ride-sharing programs such as Smart Commute on Site. Online services are freely available and can be promoted on the site to facilitate carpooling activity. | Reduce car dependence and the need for everyday travel. <br> Promote car-sharing and transit. | Developer to enroll in a ride-sharing program and provide information to the owners at the time of occupancy. |
| :---: | :---: | :---: | :---: |
| Services |  |  |  |
| Smart Lockers | Provide smart lockers to facilitate convenient deliveries such as groceries and personal packages. | Reduce car dependence and the need for everyday SOV travel. | Integrated into the building. |

### 7.0 VEHICULAR PARKING

### 7.1 MINIMUM VEHICLE PARKING REQUIREMENTS

### 7.1.1 Zoning By-law 0225-2007 (Amended by Zoning By-law 0118-2022)

In accordance with the recommendations of the newly amended Zoning By-law 0225-2007 by Zoning By-law 0118-2022, the site is located within Precinct 4. As outlined in Table 7 application of this Zoning By-law results a total requirement of 576 parking spaces, inclusive of 488 resident spaces and 88 non-resident spaces to be shared between resident visitors and retail visitors.

Table 7 Zoning By-Law 0225-2007 (Amended by Zoning By-law 0118-2022) Minimum Parking Requirements - Precinct 4

| Use | Units / GFA | Zoning By-law 0117-2022 Minimum Rate | Minimum Requirement (spaces) |
| :---: | :---: | :---: | :---: |
| Resident Rates |  |  |  |
| Resident - Condominium Apartment | 444 units | 1.1 spaces / unit | 488 |
| Resident Subtotal |  |  | 488 |
| Non-resident Rates |  |  |  |
| Visitor - Condominium Apartment | 444 units | 0.2 spaces / unit | 88 |
| Retail Store | 1,423 m² GFA | 5 spaces / $100 \mathrm{~m}^{2}$ GFA | 71 |
| Non-resident Subtotal (before sharing) |  |  | 159 |
| Non-resident Shared Parking Arrangement ${ }^{3}$ |  |  | 88 |
| Non-resident Subtotal (after sharing) |  |  | 88 |
| SITE TOTAL (with sharing) |  |  | 576 |

Notes:

1. Based on site statistics provided by A\&Architects Inc dated June 19, 2023.
2. For the calculation of the required residential parking, the appropriate resident and / or visitor rate or ratio shall be calculated for each component and then rounded. Fractions of less than 0.5 shall be rounded down to the nearest whole number. Fractions equal to or greater than 0.5 shall be rounded up to the nearest whole number.
3. As per Zoning By-law 0118-2022, for the purpose of Article 3.1.2.1, a shared parking arrangement may be used for the calculation of required visitor/non-residential parking in accordance with the greater of 0.2 visitor spaces per unit or required retail parking rate of 5 spaces $/ 100 \mathrm{~m}^{2}$ of GFA.

### 7.2 PROPOSED PARKING SUPPLY

It is proposed to provide slightly less parking than is required by the Zoning By-law 0118-2022 in accordance with the following parking supply standards:

- $\quad 311$ parking spaces for the use of residents ( 0.70 spaces / unit)
- 22 parking spaces for the use of residential visitors ( 0.05 spaces / unit)
- 26 parking spaces to serve the retail component ( 1.80 spaces / $100 \mathrm{~m}^{2}$ GFA)
- 6 tandem parking spaces

Total: 359 parking spaces (not including tandem parking spaces)
The appropriateness of the proposed parking supply is discussed in Section 7.3.
A total parking supply of 359 parking spaces and six (6) tandem parking spaces are proposed for the Site. The total parking supply (including the 6 tandem parking spaces) is proposed to be located within the twolevel underground parking garage. Access to the parking garage and the parking located at-grade is provided from the Site driveway off Queen Street North.

In addition to the total parking supply, a pick-up / drop-off loop is proposed which can accommodate approximately 3-4 vehicles. The PUDO area is provided at-grade adjacent to the residential lobby and the northern retail store of the Site.

Based on the foregoing, the proposed residential, residential visitor and retail parking supply is slightly lower than the requirements of the prevailing and applicable City of Mississauga Zoning By-law 0118-2022.

### 7.2.1 Accessible Parking

The City's Zoning By-law 0225-2007 requires that accessible spaces be provided for non-residential / visitor uses at a minimum rate of $4 \%$ for a supply within the range of $13-100$ parking spaces.

Furthermore, the By-law states that for lots with an even number of total accessible parking spaces, an equal number of Type 'A' (non-residential uses) and Type 'B' (residential uses) spaces must be provided. The two types of spaces must adhere to the following dimensions:

- Type A space:
5.2 metres (length) x 3.4 metres (width)
- Type B space:
5.2 metres (length) x 2.4 metres (width)

Both types must include a 1.5-metre pedestrian aisle adjacent to the accessible space.

The minimum accessible parking requirements are summarized in Table 8.

## Table 8 Zoning By-law 0225-2007 Accessible Parking Requirements

| Non-residential <br> Parking Supply | Category | Minimum Rate | Minimum <br> Requirement | Type Allocation |
| :--- | :---: | :---: | :---: | :---: |
| 26 spaces | $13-100$ spaces | $4 \%$ of total parking <br> supply | 2 spaces | 1 Type A <br> 1 Type B |

Notes:

1. As per Section 3.1.3.1.3 of the Zoning By-Law 0225-2017, it's stated that "Where a shared parking arrangement is used for the calculation of required visitor/ non-residential parking, the required accessible parking space requirement will be calculated on either the visitor component or non-residential component". Therefore, the non-residential parking supply was based on the retail parking supply of 26 spaces.
2. As per Section 3.1.1.1.4 of Zoning By-law 0225-2017, it's stated that "for accessible parking spaces, all numeric fractions shall be rounded up to the nearest whole number".

Application of the Zoning By-law accessible parking space standards to the proposed non-residential parking supply would require a minimum of two (2) accessible parking spaces.

A total of six (6) accessible parking spaces are provided, including one (1) retail space and five (5) resident spaces, which meets and exceeds the minimum requirements. The proposed accessible parking supply complies with the Zoning By-law dimensional requirements. Furthermore, three (3) accessible parking spaces are proposed to be provided in the P1 level and the remaining three (3) accessible parking spaces are proposed to be provided in the P2 level of the underground parking facility.

Based on the above, the proposed accessible parking supply meets the requirements of Zoning By-law 02252007 requirements and will meet the practical needs of the Site.

### 7.2.2 Electric Vehicle (EV) Parking

City of Mississauga Zoning By-law 0225-2007 (amended by Zoning By-law 0118-2022) requires a minimum number of electric vehicle ready parking spaces for new condominiums. A summary of the minimum EV ready parking spaces requirement applied to the proposed parking supply is provided in Table 9.

Table 9 Zoning By-law 0225-2007 (Amended by Zoning By-Law 0118-2022) EV Parking Requirements

| Type of Use | Proposed Parking Supply | Minimum EV Parking Requirement Rate | Minimum EV Parking Requirement Supply | Proposed EV Parking Supply |
| :---: | :---: | :---: | :---: | :---: |
| Condominium resident parking | 310 parking spaces | $20 \%$ of the total required parking spaces | 62 EV ready parking spaces | 98 ready parking spaces |
| Condominium -visitor parking | 22 parking spaces | $10 \%$ of the total required parking spaces | 2 EV ready parking spaces | 9 ready parking spaces |
| Non-residential uses with 10 or parking spaces | 26 parking spaces | $10 \%$ of the total required parking spaces | 3 EV ready parking spaces | 7 ready parking spaces |
| TOTAL | 358 parking spaces |  | 67 EV ready parking spaces | 114 ready parking spaces |

Application of this minimum rate to the proposed parking supply of 358 parking spaces results is a total minimum requirement of 67 EV ready parking spaces including 62 spaces for residents, two (2) for visitors and two (2) for retail users.

A total of 114 parking spaces located in the P1 level of the underground parking garage are equipped to be EV ready, including 98 resident parking spaces, nine (9) residential visitor parking spaces, and seven (7) retail parking spaces. The proposed EV parking supply meets and exceeds the minimum requirements outlined in Zoning By-law 0225-2007.

The surplus of EV-ready parking spaces, when compared to the requirements set by the By-law, can be attributed to the intentional design aimed at accommodating the future demand for electric vehicles. Specifically, the P1 level of the underground parking garage has been designed to offer flexibility in embracing the growing popularity of electric vehicles over time.

### 7.3 APPROPRIATENESS OF THE REDUCED PARKING SUPPLY

It is proposed to adopt a reduced parking supply standard for both residents and non-residential (including residential visitors and retail) in comparison to the minimum requirements of Zoning By-law 0225-2007 (amended by Zoning By-law 0118-2022).

A discussion and rationale are provided within the following sections regarding the appropriateness of the reduced parking supply for each use.

### 7.3.1 Resident Parking Rationale

In our opinion, the resident parking standards outlined in the Zoning By-law 0225-2007 (amended by Zoning By-law 0118-2022) continue to overstate the parking needs of contemporary residential buildings located within an urban context in close proximity to transit routes, pedestrian destinations and cycling facilities in the City of Mississauga. This section provides an overview of the contextual factors influencing parking demand in the area and the appropriateness of the proposed resident parking supply in this instance.

Adoption of a reduced series of parking standards are considered appropriate based upon the following considerations:

- The subject Site is in close proximity to existing transit services including the MiWay bus routes (i.e. $43,44,10,39,87$, and 306 bus routes), the Streetsville GO station, and bicycle route facilities that provide non-automobile dependent travel connections across the City;
- A series of Transportation Demand Management (TDM) measures proposed to be incorporated in the development to support the use of non-automobile travel modes;
- A review of parking demands observed / recorded by BA Group at another residential condominium in the City of Mississauga with similar transit context; and
- Range of approvals for reductions in resident parking supply ratios for developments with less proximate access to a GO Station.

The following provides an overview of the contextual factors influencing parking demand at residential buildings in the City of Mississauga and the appropriateness of the proposed parking supply in this instance.

### 7.3.1.1 Existing Transportation Services

The location of the Site will provide future residents with options for transportation that will reduce the reliance on an automobile. The complete transportation context is provided in Section 4.0.

The Site is well-located relative to transit routes bus routes. The following transit options listed below are all attainable within less than a 3 -minute walk from the Site:

- 180 metres from Queen Street North at Matlock Avenue bus stop for the 43 and 44 bus route;
- 210 metres from Britannia Road at Queen Street North bus stop for the 10, 39 and 87 bus route; and
- 240 metres from Queen Street South at Britannia Road bus stop for the 306 bus route.

In addition to the available MiWay bus routes surrounding the Site, Streetsville GO is approximately 2 km walking distance (27-minute walk) from the Site. Alternatively, if the future resident does not desire to walk from/to the Streetsville GO station, the user can take the 44-bus route and reach the station/the Site within 14 minutes.

The Site is currently well served by cycling infrastructure including cycle tracks, bike lanes and multi-use trails. The Site is in close proximity to multiple north-south bicycle connections such as the Queen Street South bike lane, Joymar Drive signed route and Riverview Park Trail multi-use trail. An east-west bicycle connection in close proximity to the Site is the Britannia Road West multi-use trail.

In addition, the existing cycling network is further connected through the proposed cycling infrastructure as recommended in the City of Mississauga Cycling Master Plan (2018). The existing multi-use trail along Britannia Road West which begins from Britannia Road West / Queen Street South is planned to be extended to the existing multi-use Trail along Britannia Road West beginning from Britannia Road West / Erin Mills Pkwy. Cycle tracks are proposed to be extended north from Queen Street South / Britannia Road West along Queen Street North and Mississauga Road. A new bicycle lane is proposed along Falconer Drive connecting from the new cycle track along Queen Street North. Another cycle track is proposed along Mill Creek Drive connecting from the signed bike route along Joymar Drive The existing and proposed cycling infrastructure mentioned above will improve connectivity from the Site to the rest of the City.

### 7.3.1.2 Transportation Demand Management

As outlined in Section 6.0, a proposed transportation demand management (TDM) plan is proposed for the Site, both as a method to reduce vehicular traffic but also to reduce parking demand.

Highlights of the Plan, in addition to the proposed parking supply reductions, are provided below:

- Provision of public pedestrian sidewalks on all new public streets within the Project's boundaries including a new pedestrian / cyclist pathway south of the building with adequate lighting;
- Provision of 386 bicycle parking spaces including 330 long-term bicycle parking spaces and 56 shortterm spaces;
- Implementation of two bicycle repair/maintenance stations to be provided on-site;
- Implementation of a transit screen in the lobby;
- Provision of a pre-loaded PRESTO card with a value of $\$ 50$ to each first-time unit owner;
- Implementation of travel information brochures;
- A reduced parking rate is proposed on-site to reduce car dependence;
- Opportunities will be explored to offer ride-sharing programs on-site such as participation in the Smart Commute program; and
- Smart lockers will be provided to facilitate convenient deliveries for residents.


### 7.3.1.3 Proxy Site Observed Resident Parking Demand

In order to assess the residential parking demand at another similar building with a similar context in Mississauga. BA Group conducted an overnight resident parking survey at 4011 Brickstone Mews \& 510 Curran Place, which is located approximately 2.6 kilometres walking distance (33-minute walk) from Cooksville GO station and/or a bus away from Cooksvile GO Station, which is similar to the Site's context in relation to Streetsville GO station. The proxy location was surveyed during the following dates:

- Wednesday, February 26, 2020;
- Thursday, February 27, 2020;
- Friday, February 28, 2020; and
- Monday, March 2, 2020.

The surveys were completed at a time when most residents are likely to be home (i.e. at night). The results of this study are summarized in Table 10.

Table 10 Existing Residential Parking Demand Studies

| Address | Major Intersection | Study Date | Peak Hour | Occupied Units | Resident Parking |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Demand (spaces) | Ratio (spaces / unit) |
| 4011 <br> Brickstone <br> Mews \& 510 <br> Curran Place | Confederation Pkwy/ Burnhamthorpe Road W | Wed, Feb 26, 2020 | 1:30 am | 1008 units | 786 | 0.78 |
|  |  | Thurs, Feb 27, 2020 | 1:30 am |  | 784 | 0.78 |
|  |  | Fri, Feb 28, 2020 | 1:30 am |  | 784 | 0.78 |
|  |  | $\begin{aligned} & \text { Mon, March 2, } \\ & 2020 \end{aligned}$ | 3:00 am |  | 786 | 0.78 |

The observed overall resident parking demand at the proxy site is 0.78 spaces per unit. The proposed residential parking rate of 0.70 spaces per unit is sightly less than the observed 0.78 spaces per unit, however the Site is situated in a more urban context with more transit routes available in the immediate area in comparison to the proxy site.

### 7.3.1.4 Resident Parking Reduction Precedents

Within the site vicinity, there are no recent approved parking reductions, however BA Group reviewed areas such as Port Credit, and other comparable area within the cities of Pickering and Hamilton. Although the Site is not situated in the Port Credit area, it's similar in context to the Site's Location as there is a GO station in the area vicinity and it's not located in the City Centre of Mississauga.

In the Port Credit area, a reduced parking supply of 0.86 spaces per unit was approved for 70 Mississauga Road South. This decision was signed by committee on July 1, 2021, prior to the new parking standards in place as per Zoning By-law 0118-2022. 70 Mississauga Road South is situated approximately 1.2 kilometres from Port Credit GO Station. Other examples of recent approvals have also been included for sites with more limited access to higher order transit to demonstrate the willingness of multiple municipalities (Pickering and

Hamilton) to significantly reduce residential parking standards compared to the enforce Zoning By-law, recognizing a shift in travel behaviour and bigger emphasis placed on existing and future transit access. These approvals range from 0.47 to 0.86 spaces per unit for sites that are significantly further from a GO Station (between 575 metres to 2.2 km ).

Table 11 outlines a selection of reduced parking approvals for proxy sites with similar or less transit supportive contexts as the proposed development.

## Table 11 Residential Developments with Approved Resident Parking Reductions

| Address | Proximity to Transit | Municipality | Resident Standard Applied | Permission Through |
| :---: | :---: | :---: | :---: | :---: |
| Approvals with less proximate access to High Order Transit |  |  |  |  |
| 1496 Bayly Street | - 575 m from Pickering GO Station | Pickering | 0.71 spaces per unit | Site Specific Zoning Bylaw 7810/21 |
| 600 James Street North | ~900 m from West Harbour GO Station | Hamilton | 0.58 spaces / unit | LPAT Case No. PL190517 Site Specific Zoning Bylaw 21-053-LPAT |
| 70 Mississauga Road South | $\sim 1.2 \mathrm{~km}$ from Port Credit GO Station | Mississauga | 0.86 spaces / unit | CoA Decision - A226.21 |
| 98 James Street South | $\sim 1.5 \mathrm{~m}$ from West Harbour GO Station | Hamilton | 0.47 spaces / unit | City of Hamilton Zoning By-law 15-024 |
| 175 Catharine Street South and 117 Forest Avenue | ~2.2 km from West Harbour GO Station | Hamilton | 0.65 spaces / unit | City of Hamilton Zoning By-law 20-216 |

The cities of Mississauga, Pickering and Hamilton have shown flexibility and pragmatism in adapting to the evolving transportation landscape as options become available to residents that were not available at the time when the Zoning By-law was enacted. In this context, the proposed resident parking supply ratio of 0.70 spaces / unit is conservatively within the range of documented parking supply reduction approvals that are appropriate proxies for the site.

### 7.3.1.5 Residential Parking Assessment Summary

In summary, the proposed resident parking supply rate ( 0.70 spaces per unit) is considered to be appropriate based upon the following:

- The subject Site is in close proximity to existing transit services including the MiWay bus routes (i.e. $43,44,10,39,87$, and 306 bus routes), the Streetsville GO station, and bicycle route facilities that provide non-automobile dependent travel connections across the City;
- A series of Transportation Demand Management measures proposed to be incorporated in the development to support the use of non-automobile travel modes;
- A review of parking demands observed / recorded by BA Group at another residential condominium in the City of Mississauga with similar transit context; and
- Range of approvals for reductions in resident parking supply ratios for developments with less proximate access to a GO Station; and

Based on the above, an adoption of the proposed resident parking supply rate of 0.70 spaces / unit is considered to be appropriate and will enable the essential resident parking demands of Site to be met.

### 7.3.2 Resident Visitor Parking Rationale

As part of the proposed development, 48 non-residential parking spaces are proposed to serve the residential visitor and retail needs of the Site. The following non-residential provisions are being sought as part of this application:

- 22 parking spaces for the use of residential visitors ( 0.05 spaces / unit)
- 26 parking spaces to serve the retail component ( 1.80 spaces / $100 \mathrm{~m}^{2}$ GFA)

The proposed parking supply for the non-residential component of the Site is slightly less than the required Zoning By-law 0225-2007. Zoning By-law 0225-2007 requires 88 visitor parking spaces to be shared with both residential visitors and retail users. The total non-residential parking supply proposed for the Site is a total of 48 parking spaces ( 22 parking spaces for residential visitors and 26 parking spaces for retail users), which is less than the required 88 parking spaces.

It's been observed that the non-residential supply standards outlined in Zoning By-law 0225-2007 overstate the parking demands of a new building located in an urban setting in the City of Mississauga. Generally, parking demands across the GTA have been declining over recent years in response to the changing demographics, economic factors, policy and planning emphasis on transit and active modes of travel, and mobility choices of residents within newer buildings, in particular.

Given the above, a reduced non-residential parking supply (48 parking spaces) is being proposed for the Site. The following provides an overview of the residential visitor parking demand observed in proxy locations that is supportive of the resident visitor rate of 0.05 spaces per unit, and provides a rationale for the retail parking.

### 7.3.2.1 Observed Residential Visitor Parking Demand

BA Group conducted more recent proxy parking studies at residential developments in the Port Credit area in September 2022. Although the Site is not located in the Port Credit area, the subject site has a similar transit context being in close proximity to a GO station with surface MiWay bus routes available within the immediate area, and not being located in the City Centre of the City of Mississauga. These include 28 Park Street E, 28 Elizabeth Street, and 70 Park Street East.

In addition to the Port Credit proxy locations, BA Group has conducted a parking study at 1575 Lakeshore Road West, which is located in the Clarkson area, and is situated approximately 2 kilometers walking distance to Clarkson GO station, which is relatively similar to the Site's transit context.

Survey results are summarized in Table 12.

Table 12 BA Group Directed Visitor parking Proxy Survey Results

| Proxy Sites | Port Credit Area Locations |  |  | Clarkson Area Location |
| :---: | :---: | :---: | :---: | :---: |
|  | 28 Park Street E | 28 Elizabeth Street N | 70 Park Street East | 1575 Lakeshore Road West |
| Tuesday, October 26, 2021 | -- | -- | -- | 0.04 |
| Thursday, October 28, 2021 | -- | -- | -- | 0.04 |
| Tuesday, November 2, 2021 | -- | -- | -- | 0.04 |
| Thursday, November 4, 2021 | -- | -- | -- | 0.04 |
| Friday, September 23, 2022 | 0.04 | 0.01 | -- | -- |
| Saturday, September $24,2022$ | 0.10 | 0.01 | -- | -- |
| Friday, September 30, 2022 | 0.06 | 0.02 | -- | -- |
| Saturday October 1, 2022 | 0.08 | 0.02 | -- | -- |
| Friday, October 14, $2022$ | -- | -- | 0.05 | -- |
| Saturday, October 15, $2022$ | -- | -- | 0.04 | -- |

1. Parking surveys were conducted on Fridays from 6:00 PM to 11:00 PM, and on Saturdays from 12:00 PM to 8:00 PM. Table values represent absolute maximum
2. At 70 Park Street East, visitor parking demand surveys were conducted from 2:00pm to 11:00pm on a Friday and a Saturday. Based upon 204 leased units at the time of study.

The reviewed proxy sites are observed to have a residential visitor parking demand range of 0.01-0.08 spaces per unit. The proposed parking supply of 0.05 spaces per unit is well within this range, and is considered appropriate on this basis.

### 7.3.2.2 Ancillary Non-Residential Parking

As per the By-law, 88 parking spaces can be shared between the retail use and resident visitors. However, 26 parking spaces are proposed for retail uses. The proposed retail use for the Site is intended to serve the majority of the residents in the building and the surrounding community. Thus, the retail use is not anticipated to generate significant parking demand.

From this perspective, in the event that the retail uses generate a nominal vehicle need, these uses can be accommodated within the proposed 26 retail spaces which is more than appropriate for a mixed-use urban area.

### 7.3.2.3 Non-Residential Assessment Summary

In summary, the provision of a reduced non-residential parking standard for the proposed development is considered appropriate based upon the following considerations:

- The subject Site is in close proximity to existing transit services including the MiWay bus routes (i.e. $43,44,10,39,87$, and 306 bus routes), the Streetsville GO station, and bicycle route facilities that provide non-automobile dependent travel connections across the City;
- Consistent with the observed visitor parking rates for proxy sites with a similar transit context
- Retail employees can participate in the car-pool program such as Smart Commute which will reduce the single occupant vehicle trips
- The nature and size of the retail use will not generate a significant amount of parking demand and thus the 26 retail parking spaces will be appropriate to support the retail needs.


### 8.0 BICYCLE PARKING CONSIDERATIONS

### 8.1 BICYCLE PARKING REQUIREMENTS

### 8.1.1 The City of Mississauga Zoning By-law 0225-2007 (Amended by Zoning Bylaw 0118-2022)

Bicycle parking standards have been introduced in the newly amended Zoning By-law 0225-2007 by the bicycle parking requirements outlined in Zoning By-law 0118-2022. The applicable bicycle parking requirements outlined in Zoning By-law 0118-2022, now introduced in Zoning By-law 0225-2007, to the Site are summarized in Table 13.

Application of the bicycle parking standards to the Site will result in a total provision of 293 bicycle parking spaces, including five (5) spaces for retail and 288 spaces for residential.

Table 13 Zoning By-Law 0225-2007 (Amended by Zoning By-Law 0118-2022) Bicycle Parking Requirements

| Land Use | Class Type ${ }^{2}$ | Number of Units / GFA | Minimum Bicycle Parking Standard | Spaces Required ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: |
| Residential | Class A | 444 units | 0.60 spaces / unit | 266 spaces |
|  | Class B |  | The greater of 0.05 spaces per unit or 6.0 spaces | 22 spaces |
| Retail | Class A | 1,423 m ${ }^{2}$ | 0.15 spaces / $100 \mathrm{~m}^{2}$ | 2 spaces |
|  | Class B |  | 0.2 spaces / $100 \mathrm{~m}^{2}$ | 3 spaces |
|  | Total |  |  | 293 spaces |

## Notes

1. Based on site statistics provided by A\&Architects Inc dated June 19, 2023.
2. Class A means a bicycle parking space designed to provide long-term parking for employees or residents of the building. Bicycle Parking Space, Class B means a bicycle parking space designed to provide short-term transient parking for persons who are not residents or employees of the building.
3. In Article 3.1.1.1 of the By-law, it states the following: "Where the number of non-residential parking spaces and/or loading spaces and/or bicycle parking spaces is calculated on the basis of a rate or ratio and results in a numeric fraction, fractions of less than 0.5 shall be rounded clown to the nearest whole number and fractions equal to or greater than 0.5 shall be rounded up to the nearest whole number" and for residential parking and bicycle parking spaces, "if the calculation results in a fraction less than 0.5 , it shall be rounded down to the nearest whole number, and fractions equal to or greater than 0.5 shall be rounded up to the nearest whole number."

### 8.2 PROPOSED BICYCLE PARKING SUPPLY AND FACILITIES

A total of 386 bicycle parking spaces, including 330 long-term residential bicycle parking spaces and 56 shortterm bicycle parking spaces are proposed for the Site. From the long-term bicycle parking supply, 326 are residential long-term spaces and four (4) are for retail long term spaces. From the short-term bicycle parking supply, 48 are residential short-term spaces, and eight (8) are short-term spaces.

All bicycle parking is provided on the ground floor. The total residential long-term bicycle parking spaces are located in a secure bicycle parking room located at-grade. The total residential short-term bicycle parking spaces are located in another separate bicycle parking room located at-grade. Access to the residential long-
term and short-term bicycle storage rooms are provided from the path provided south of the site. The pathway connects east of Queen Street North.

The 12 retail bicycle parking spaces including the four (4) long-term and eight (8) short-term bicycle parking spaces are located outdoors at-grade in front of one of the southern retail spaces along the site frontage of Queen Street North.

Access to the residential long-term and short-term bicycle storage rooms are provided from the path provided south of the site. The pathway connects east of Queen Street North.

Access to the 12 retail bicycle parking spaces is provided from the sidewalks along Queen Street North.

The proposed bicycle parking supply meets and exceeds the requirements outlined in Zoning By-law 02252007, and is therefore an appropriate supply to serve the cycling needs of the proposed development. By providing a bicycle parking supply ( 386 bicycle parking spaces) that exceeds the By-law's requirement of 293 bicycle parking spaces, the applicant is not only ensuring compliance but also strategically supporting the reduced parking approach adopted for the development.

### 9.0 LOADING CONSIDERATIONS

### 9.1 MINIMUM LOADING REQUIREMENTS

Application of the prevailing City of Mississauga Zoning By-Law 0225-2007 to the proposed development results in a requirement of two loading spaces with minimum dimensions of 3.5 metres by 9.0 metres. The loading space requirements are summarized in Table 14.

Table 14 City of Mississauga Zoning By-Law 0225-2007 Loading Space Requirements

| Use |
| :--- |
| Residential |
| Units / GFA1 | Minimum Zoning By-law Requirement | Number of Required Spaces |  |
| :---: | :---: |
| Retail | 1 loading space for apartment <br> containing a minimum of 30 dwelling <br> units |

### 9.2 PROPOSED LOADING SUPPLY

Two (2) loading spaces are proposed at-grade with a dimension of 3.5 metres by 9.0 metres. The two (2) loading spaces are located adjacent to the proposed northeast driveway. A garbage loading room is proposed to be located in front of the loading space closest to the driveway. The loading area and adjacent parking ramp includes a warning system to advise motorists of loading activity. Associated signage and pavement markings are provided in Appendix B.

The Site plan can appropriately accommodate the needs of the design vehicles. Vehicle Maneuvering Diagrams (VMD's) illustrating the inbound and outbound manoeuvres of a Peel Region garbage collection vehicle, TAC Heavy Single Unit Truck (HSU) and TAC Medium Single Unit Truck Unit (MSU) truck are attached in Appendix C. These diagrams confirm that the proposed loading arrangements are appropriate and will facilitate the manoeuvring needs of the vehicles that will make deliveries to the proposed development.

### 10.0 SITE ACCESS

The new east-west Site driveway will operate as a full-movement access. No lane improvements are recommended on Queen Street North at the Site driveway.

The proposed Site driveway is located approximately 170 metres from the signalized intersection at Queen Street North and Britannia Road intersection (measured edge of driveway to edge of roadway).

The proposed spacing between the Site driveway and the signalized intersection at Queen Street North and Britannia Road is greater than the suggested minimum corner clearance requirements for a driveway as identified in The Transportation Association of Canada Design Guide for Canadian Roads 2017 (TAC Guidelines) Figure 8.8.2 (Suggested Minimum Corner Clearances to Accesses or Public Lanes at Major Intersections) - 70 metre from the signalized condition.

### 10.1 CLEAR THROAT LENGTH

The clear throat length requirement within the Site driveway is less than the suggested minimum clear throat length requirements as identified in The Transportation Association of Canada Design Guide for Canadian Roads 2017 (TAC Guidelines) Table 8.9.3 (Suggested Minimum Clear Throat Lengths for Major Driveways) 25m.

The clear throat length allotted for the site driveway is approximately 15 metres, measured from the end of the driveway curb return radii at the roadway to the edge of the inbound PUDO loop. It is not anticipated for the inbound vehicles to be obstructed by vehicles entering the PUDO loop since the PUDO loop has been sized appropriately and can accommodate a range of 1-4 vehicles. It is noteworthy that a clear throat length of more than 25 metres is provided between the end of the driveway curb return radii at the roadway to parking ramp and loading facility.

### 10.2 SIGHT DISTANCE REVIEW

A review of the available sight distance for the proposed Site driveway on Queen Street North was completed as part of this analysis and is attached in Appendix E.

The sight distance north and south of the Site driveway on Queen Street North meets the minimum intersection sight distance requirements as identified in the TAC Guidelines for a design speed of $70 \mathrm{~km} / \mathrm{h}$ ( 150 metres and 130 metres, respectively).

Therefore, there are no issues with the sight distance for the proposed Site driveway.

### 10.3 DRIVEWAY SPACING CONSIDERATIONS

The proposed Site driveway is aligned with the 40 Queen Street North driveway located directly opposite each other. This will help reduce conflicting movements within the centre two-way left-turn lane that currently exists on Queen Street North.

In addition, the proposed Site driveway is located approximately 25 metres south of the existing 53 Queen Street North driveway (measured edge of driveway to edge of driveway).

This driveway spacing is greater than the suggested minimum spacing as identified in the Transportation Association of Canada Design Guide for Canadian Roads 2017 (TAC Guidelines) Figure 8.9.2 (Driveway Spacing Guidelines - Locals and Collectors) - 3 metres for commercial land use.

### 11.0 TRAVEL DEMAND FORECAST

### 11.1 BASELINE EXISTING TRAFFIC VOLUMES

Undertaking accurate traffic field counts is not possible at the time of this study, given the unprecedented circumstances surrounding the COVID-19 pandemic (March 2020 onwards). The most current available traffic data (a combination of traffic surveys undertaken in 2019 and 2021), as described below, are used to develop existing baseline conditions for the traffic analysis.

Table 15 summarizes the range of survey data used for this analysis. Appendix F contains the raw survey data.

## Table 15 Existing Traffic Count Summary

| Intersection | Control Type | Date of Count |
| :--- | :---: | :---: |
| Britannia Road West / Queen <br> Street $^{1}$ | Signalized | Wednesday, October 2, 2019 |
| Britannia Road West / Arch Road | STOP Control | Wednesday, September 25, 2019 |
| Britannia Road West / Earl Street | STOP Control | Thursday, September 26, 2019 |
| Britannia Road West / Ellesboro <br> Drive | Signalized | Thursday, May 30, 2019 |
| Queen Street North / Petro Canada <br> South Driveway | STOP Control | Thursday, September 9, 2021 |
| Queen Street North / Petro Canada <br> North Driveway | STOP Control | Thursday, September 9, 2021 |
| Queen Street North / Site Driveway <br> (39 Queen Street North) | STOP Control | Thursday, September 9, 2021 |
| Queen Street North / 53 Queen <br> Street North Driveway | STOP Control | Thursday, September 9, 2021 |
| Queen Street North / Matlock <br> Avenue | STOP Control | Tuesday, February 9, 2021 |

Notes:

1. Primary intersection.

Volumes were balanced to the 'primary' intersection at Britannia Road West / Queen Street, as this intersection was surveyed in 2019 before the onset of the Covid-19 pandemic. Volumes were balanced in all four cardinal directions along each corridor, to ensure matching to the 2019 survey at the primary intersection.

Baseline existing traffic volumes are summarized in Figure 9.


### 11.2 BACKGROUND TRAFFIC VOLUMES

### 11.2.1 Corridor Growth

Based on forecasting model outputs from both the City of Mississauga (for Queen Street) and the Region of Peel (for Britannia Road West), compounding corridor growth rates were applied along both corridors. All corridor growth rates have been applied over 10 years and are compounded annually.

Corridor growth rates are based on the rates outlined in Table 16 below.

Table 16 Annual Corridor Growth Rates to 2031

|  | AM Peak Hour | PM Peak Hour | Source |
| :--- | :---: | :---: | :---: |
| Northbound on Queen Street | $+0.5 \%$ | $+0.5 \%$ | City of Mississauga |
| Southbound on Queen Street | $+1.5 \%$ | $+0.5 \%$ | City of Mississauga |
| Eastbound on Britannia Road West | $+0.5 \%$ | $+0.5 \%$ | Region of Peel |
| Westbound on Britannia Road West | $+0.5 \%$ | $+0.5 \%$ | Region of Peel |

Agency correspondence pertaining to corridor growth is attached in Appendix G.

### 11.2.2 Other Background Development

Mississauga's development applications map was reviewed to check for other development applications within the surrounding area that may impact traffic growth at the study intersections.

It was identified that the development at 6, 10, and 12 Queen Street South, 16 James Street, 2 William Street and 0 William Street (OZ/OPA 21 14) would impact the area street network and has therefore been considered as background traffic based on NexTrans transportation report dated August 2021. The development includes 77 townhomes with retail space fronting Queen Street.

### 11.2.3 Future Background Traffic

Future background traffic volumes reflect a combination of baseline existing traffic volumes, projected corridor growth allowance and any future area development related traffic activity. Study horizons of 5 and 10 years were considered for this analysis and future background volumes developed for each horizon year.

Future background traffic volumes on the area road network for the weekday morning and afternoon peak hours are summarized for the 5 -year and 10-year horizons in Figure 10 and Figure 11, respectively.


FIGURE 10 FUTURE BACKGROUND TRAFFIC VOLUMES -5 YEAR


FIGURE 11 FUTURE BACKGROUND TRAFFIC VOLUMES - 10 YEAR

### 11.3 SITE TRAFFIC

### 11.3.1 Trip Distribution and Assignment

Trip distribution patterns and traffic route assignment for the residential component of the Site are derived from a 2016 Transportation Tomorrow Survey (TTS) residential travel query for 2006 GTA Zones 3715, 3717, 3718 and 3836. Retail traffic distribution is derived from existing traffic survey patterns.

Table 17 presents adopted distribution of inbound and outbound vehicle traffic.

## Table 17 Site Trip Distribution

| Direction (to or from) | Residential Traffic |  | Retail Traffic |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Outbound | Inbound | Outbound | Inbound |
| North via Queen Street North | $35 \%$ | $30 \%$ | $40 \%$ | $35 \%$ |
| South via Queen Street South | $25 \%$ | $20 \%$ | $50 \%$ | $35 \%$ |
| East via Britannia Road West | $25 \%$ | $40 \%$ | $5 \%$ | $15 \%$ |
| West via Britannia Road West | $15 \%$ | $10 \%$ | $5 \%$ | $15 \%$ |
| Total | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ | $\mathbf{1 0 0 \%}$ |

### 11.3.2 Existing Site Traffic

Traffic surveys for the Site's existing driveway demonstrated the generation of some peak hour traffic. Future total conditions account for existing Site traffic removal based on the approximate trip distribution patterns realized within the existing survey data.

### 11.3.3 Site Vehicle Trip Forecast

The vehicle trip generation rates adopted for the purposes of this study are based on rates outlined within the ITE Trip Generation Manual $11^{\text {th }}$ Edition for Land Use Codes 221 (Mid-Rise Residential) and 822 (Strip Retail Plaza <40k).

Vehicle trip generation is extrapolated into multimodal person trips, based on methodology in Section 5.3 of the ITE Trip Generation Handbook (3rd Edition). The volumes are subsequently adjusted from ITE's baseline vehicle mode share to the vehicle mode share applicable to the Site. The below formulae demonstrate these calculations.

$$
\begin{gathered}
\text { baseline person trips }=\frac{\text { baseline vehicle trips } \times \text { baseline vehicle occupancy }}{\text { baseline person trip mode share in vehicles }} \\
\text { adjusted vehicle trips }=\frac{\text { person trips } \times \text { area vehicle mode share }}{\text { area average vehicle occupancy }}
\end{gathered}
$$

## Where:

- Baseline vehicle occupancy (morning peak) = 1.09
- Baseline vehicle occupancy (afternoon peak) $=1.21$
- Baseline mode share (morning peak) $=95 \%$
- Baseline mode share (afternoon peak) = 95\%
- Area vehicle occupancy (morning peak) $=1.26$
- Area vehicle occupancy (afternoon peak) $=1.29$
- Area mode share (morning peak) = 64\%
- Area mode share (afternoon peak) $=67 \%$
(ITE Trip Generation Manual, $3^{\text {rd }}$ Ed.)
(ITE Trip Generation Manual, $3^{\text {rd }}$ Ed.)
(ITE Trip Generation Manual, $3^{\text {rd }}$ Ed.)
(ITE Trip Generation Manual, $3^{\text {rd }}$ Ed.)
(TTS, 2016)
(TTS, 2016)
(TTS, 2016)
(TTS, 2016)

Table 18 is a summary of trip generation, including the rates utilized for each component and an existing site traffic removal allowance.

## Table 18 Vehicle Trip Generation

| Land Use / Land Use Code | Weekday Morning Peak Hour |  |  | Weekday Afternoon Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | 2-Way | In | Out | 2-Way |
| ITE Baseline Resident Trip Generation ${ }^{3,4}$ |  |  |  |  |  |  |
| Land Use Code 221 (Mid-Rise), Not Close to Rail Transit - trips per unit | 0.09 | 0.28 | 0.37 | 0.24 | 0.15 | 0.39 |
| Baseline New Residential Site Traffic (444 units) | 40 | 125 | 165 | 105 | 70 | 175 |
| Baseline New Residential Person Trips | 46 | 143 | 189 | 134 | 89 | 223 |
| Adjusted New Vehicle Trips (Resident) ${ }^{5}$ | 25 | 75 | 100 | 70 | 45 | 115 |
| Retail Trip Generation ${ }^{6}$ |  |  |  |  |  |  |
| Land Use Code 822 (Strip Retail Plaza <40k) - trips per 1,000 sqft GFA | 1.42 | 0.94 | 2.36 | 3.29 | 3.30 | 6.59 |
| New Retail Vehicle Trips ( $1,423 \mathrm{~m}^{2}$ or $15,317 \mathrm{ft}^{2}$ ) | 20 | 15 | 35 | 50 | 50 | 100 |
| Total Site Trip Generation |  |  |  |  |  |  |
| Total New Site Trips | 45 | 90 | 130 | 120 | 95 | 215 |
| Existing Site Trips to be Removed (based on survey data) ${ }^{2}$ | -15 | -5 | -20 | -40 | -50 | -90 |
| Net-New Site Trips | 30 | 85 | 115 | 80 | 45 | 125 |

Notes:

1. Trips rounded to the nearest five (5).
2. Traffic volumes based on counts conducted on September 9, 2021.
3. Baseline ITE vehicle occupancy is 1.09 people per vehicle for the morning peak hour and 1.21 people per vehicle in the afternoon peak hour, based on ITE Trip Generation Handbook ( $3^{\text {rd }}$ Ed.) Appendix D contains the calculations.
Baseline ITE automobile mode share is $95 \%$, based on ITE Trip Generation Handbook (3 ${ }^{\text {rd }}$ Ed.) Section 5.5.2.
4. Actual site mode split and vehicle occupancy based on TTS 2016 'home-based' survey data for 2006 GTA Zones 3715,3717
5. $\quad 3718$ \& 3836 . conservative.

Based on the trip generation methodology outlined above, the site is expected to generate in the order of $\mathbf{1 1 5}$ and $\mathbf{1 2 5}$ new two-way vehicle trips in the weekday morning and afternoon peak hours, respectively.

Net-new site traffic volumes are illustrated on Figure 13.

### 11.3.4 Mode Split

Modal share characteristics for resident (home-based) travel during the morning and afternoon peak periods are summarized in Table 19 and are based on a 2016 Transportation Tomorrow Survey (TTS) data query.

Table 19 Area Residential Mode Split (2016 TTS, Zones 3718, 3715, 3717 and 3836)

| Mode | Morning Peak Period <br> Outbound | Afternoon Peak Period <br> Inbound |
| :--- | :---: | :---: |
| Auto Driver | $64 \%$ | $67 \%$ |
| Auto Passenger | $17 \%$ | $19 \%$ |
| Transit | $13 \%$ | $10 \%$ |
| Cycle | $0 \%$ | $0 \%$ |
| Walk | $6 \%$ | $4 \%$ |

Notes:

1. Based on 2016 TTS results for morning (6:00-8:59) and afternoon (15:00-17:59) peak traffic periods for TTS 2006 GTA Zones 3715, 3717, 3718 and 3836.
2. Auto passenger trips (includes auto passengers, school bus passengers and taxi passengers).

Overall, the area has an auto driver mode share in the order of $64 \%$ and $67 \%$ for morning outbound and afternoon inbound home-based trips during the peak travel periods, respectively.

### 11.3.5 Site Multimodal Trips

A multimodal person trip forecast was undertaken through back-calculation of vehicular trip generation and modal split percentages. Table 20 summarizes net-new person trips forecast to result from the proposed development.

Table 20 Net-New Site Person Trips

|  | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | In | Out | 2-Way | In | Out | 2-Way |
| Area Mode Split <br> Driver <br> Passenger <br> Transit <br> Active (Walk/Cycle) |  | $64 \%$ $17 \%$ $13 \%$ $6 \%$ |  |  | $67 \%$ $19 \%$ $10 \%$ $4 \%$ |  |
| Multimodal Trips Generated |  |  |  |  |  |  |
| Trips <br> Driver <br> Passenger <br> Transit <br> Active (Walk/Cycle) <br> Total New Site Trips | $\begin{gathered} 30 \\ 10 \\ 5 \\ 5 \\ 50 \end{gathered}$ | $\begin{gathered} 85 \\ 25 \\ 15 \\ 10 \\ \mathbf{1 3 5} \end{gathered}$ | $\begin{gathered} 115 \\ 30 \\ 25 \\ 10 \\ 180 \end{gathered}$ | $\begin{gathered} 80 \\ 25 \\ 10 \\ 5 \\ 120 \end{gathered}$ | $\begin{gathered} 45 \\ 15 \\ 5 \\ 5 \\ 70 \end{gathered}$ | $\begin{gathered} 125 \\ 35 \\ 20 \\ 5 \\ \mathbf{1 8 5} \end{gathered}$ |

The proposed development is forecast to generate 180 and $\mathbf{1 8 5}$ net-new two-way person trips during the weekday morning and weekday afternoon peak hours, respectively.

It is envisioned that the relatively small number of new transit trips will utilize nearby transit options that are available within the study area, including the nearby GO rail and bus services.

### 11.4 FUTURE TOTAL TRAFFIC VOLUMES

Future total traffic volumes during the weekday morning and afternoon peak hours reflect the sum of future background traffic volumes and new site traffic volumes. Future total traffic volumes for the 5 -year and 10year study horizons are summarized in Figure 13 and Figure 14, respectively.


FIGURE 12 NET-NEW SITE TRAFFIC


FIGURE 13 FUTURE TOTAL TRAFFIC VOLUMES - 5 YEAR


FIGURE 14 FUTURE TOTAL TRAFFIC VOLUMES - 10 YEAR

### 12.0 TRAFFIC OPERATIONS ANALYSIS

### 12.1 ANALYSIS METHODOLOGY

### 12.1.1 Analysis Scenarios

Traffic operations analyses have been undertaken during the weekday morning and afternoon street peak hours under the following traffic conditions:

- Baseline existing traffic conditions that reflect activity levels and patterns on the area road network in a "pre-COVID" context, based on the derived baseline existing traffic volumes;
- Future background traffic conditions that include general corridor growth over 5-year and 10-year planning periods and traffic activity generated by other new area developments; and
- Future total traffic conditions with the development of the Site as planned, which includes new traffic generated by the development proposal in addition to future background traffic volumes.

Traffic operations analyses were undertaken at the following locations in proximity of the proposed development Site:

Signalized:

- Britannia Road West / Queen Street
- Britannia Road West / Ellesboro Drive


## Unsignalized:

- Britannia Road West / Arch Road
- Britannia Road West / Earl Street
- Britannia Road West / Ellesboro Drive
- Queen Street North / Petro Canada South Driveway
- Queen Street North / Petro Canada North Driveway
- Queen Street North / 39 Queen Street North
- Queen Street North / 53 Queen Street North
- Queen Street North / Matlock Avenue

The traffic analysis of this study is based on Highway Capacity Manual (HCM) 2000 methodology. A brief overview of the software, analysis parameters and assumptions are provided below.

### 12.1.2 Analysis Software

The analysis has been completed using Synchro (version 11) capacity analysis software in accordance with the methodologies outlined in the Highway Capacity Manual (HCM 2000). The analysis is also in accordance with the City of Mississauga's Traffic Impact Study Guidelines for intersections along Queen Street North, and Peel Region's Regional Guidelines for Using Synchro (December 2010) for intersections along Britannia Road West.

For signalized intersections, two indicators are used to reflect an intersection's operation. The first is a volume to capacity ( $\mathrm{v} / \mathrm{c}$ ) ratio which is an indicator of the capacity utilization at an intersection or on specific movements at an intersection. A v/c of 1.00 indicates that a movement, or intersection as a whole, is operating at or near theoretical capacity, based on HCM 2000 methodology.

The second indicator is a Level of Service (LOS) designation for an intersection as a whole or for individual movements. The LOS designation ranges from LOS A to LOS F, providing an understanding of the relative time a motorist may have to wait, on average, to travel through an intersection and complete any movement. A LOS A designation is reflective of a condition where motorists may experience little delay, while a LOS F designation is reflective of extended delays.

### 12.1.3 Traffic Signal Timings

Analysis at signalized intersections were undertaken using the available signal timing parameters in an attempt to reflect how the signals were operating at the time of existing traffic data collection. Where signals have been optimized in future, existing signal cycle lengths and pedestrian minimum times were maintained.

Traffic signal timings adopted for this analysis were obtained for the area signalized intersections from the Region of Peel and are provided in Appendix H.

### 12.2 ANALYSIS PARAMETERS

### 12.2.1 Parameters and Assumptions

### 12.2.1.1 Peak Hour Factors

Where available, Peak Hour Factors (PHF's) were adopted for signalized intersections within the study area in accordance with observed survey data. Where data was not available, PHFs consistent with adjacent intersections were adopted. For intersections under Peel Region jurisdiction, a PHF of 1.00 was adopted in as per Peel's Regional Guidelines for Using Synchro (December 2010).

### 12.2.1.2 Lost Time Adjustment

A lost time adjustment of 0 seconds was adopted by default for all signalized intersection movements within the study area, consistent with the Region of Peel Synchro Guidelines.

### 12.3 SIGNALIZED INTERSECTIONS

This section contains an analysis of signalized intersections under existing, future background and future total traffic conditions for both the morning and afternoon peak hours. The results of the signalized intersection traffic operations analyses are summarized in Table 21 and briefly in the following sections.

Detailed capacity analysis calculation worksheets for signalized intersections are attached in Appendix I.

Overall, signalized intersections proximate to the site operate well, with the exception of selected movements that are already constrained under existing or future background conditions. The Site can be comfortably accommodated by the existing road network and no changes outside of signal timing adjustments are recommended for this development.

Table 21 Signalized Intersection Analysis Summary

|  | Existing |  | 5-Year Future Background |  | 5-Year Future Total |  | 10-Year Future Background |  | 10-Year Future Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V/C | LOS | V/C | LOS | V/C | LOS | V/C | LOS | V/C | LOS |
| Queen Street \& Britannia Rd West |  |  |  |  |  |  |  |  |  |  |
| EBL | $\begin{gathered} 0.43 \\ (0.72) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.44 \\ (0.77) \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.46 \\ (0.83) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.46 \\ (0.81) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ (\mathrm{E}) \end{gathered}$ | $\begin{gathered} 0.48 \\ (0.87) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ (\mathrm{E}) \end{gathered}$ |
| EBTR | $\begin{gathered} 0.86 \\ (0.70) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.87 \\ (0.75) \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.87 \\ (0.75) \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.91 \\ (0.74) \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.91 \\ (0.75) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{D} \\ \text { (D) } \end{gathered}$ |
| WBL | $\begin{gathered} 0.55 \\ (0.65) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (C) } \end{gathered}$ | $\begin{gathered} 0.62 \\ (0.67) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.62 \\ (0.69) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.56 \\ (0.73) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.57 \\ (0.74) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ |
| WBT | $\begin{gathered} 0.34 \\ (0.76) \\ \hline \end{gathered}$ | C <br> (D) | $\begin{gathered} 0.36 \\ (0.81) \end{gathered}$ | $\begin{gathered} \text { C } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.36 \\ (0.82) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.37 \\ (0.82) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.37 \\ (0.84) \\ \hline \end{gathered}$ | $\begin{gathered} \text { C } \\ \text { (D) } \end{gathered}$ |
| WBR | $\begin{gathered} 0.25 \\ (0.13) \end{gathered}$ | $\begin{gathered} \text { B } \\ \text { (B) } \end{gathered}$ | $\begin{gathered} 0.25 \\ (0.11) \end{gathered}$ | $\begin{gathered} \text { B } \\ \text { (B) } \end{gathered}$ | $\begin{gathered} 0.25 \\ (0.14) \end{gathered}$ | $\begin{gathered} \text { B } \\ \text { (C) } \end{gathered}$ | $\begin{gathered} 0.26 \\ (0.13) \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ \text { (C) } \end{gathered}$ | $\begin{gathered} 0.26 \\ (0.16) \end{gathered}$ | $\begin{gathered} \mathrm{B} \\ \text { (C) } \end{gathered}$ |
| NBL | $\begin{gathered} 0.47 \\ (0.91) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (F) } \end{gathered}$ | $\begin{gathered} 0.49 \\ (0.90) \end{gathered}$ | $\begin{gathered} E \\ \text { (F) } \end{gathered}$ | $\begin{gathered} 0.53 \\ (0.91) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (F) } \end{gathered}$ | $\begin{gathered} 0.52 \\ (0.95) \end{gathered}$ | $\begin{gathered} E \\ \text { (F) } \end{gathered}$ | $\begin{gathered} 0.58 \\ (0.97) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (F) } \end{gathered}$ |
| NBTR | $\begin{gathered} 0.82 \\ (0.49) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.89 \\ (0.59) \end{gathered}$ | $\begin{gathered} E \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.89 \\ (0.61) \\ \hline \end{gathered}$ | $\begin{gathered} \text { E } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.83 \\ (0.50) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.82 \\ (0.51) \\ \hline \end{gathered}$ | $\begin{gathered} E \\ \text { (D) } \end{gathered}$ |
| SBL | $\begin{gathered} 0.82 \\ (0.84) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.77 \\ (0.74) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.84 \\ (0.76) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.82 \\ (0.84) \end{gathered}$ | $\begin{gathered} E \\ (\mathrm{E}) \end{gathered}$ | $\begin{gathered} 0.91 \\ (0.86) \end{gathered}$ | $\begin{gathered} \text { F } \\ (\mathrm{E}) \end{gathered}$ |
| SBT | $\begin{gathered} 0.54 \\ (0.90) \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.57 \\ (0.92) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.61 \\ (0.93) \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.60 \\ (0.92) \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.64 \\ (0.93) \\ \hline \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (E) } \end{gathered}$ |
| SBR | $\begin{gathered} 0.10 \\ (0.55) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.10 \\ (0.49) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.11 \\ (0.51) \end{gathered}$ | $\begin{aligned} & \text { D } \\ & \text { (D) } \end{aligned}$ | $\begin{gathered} 0.10 \\ (0.54) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.11 \\ (0.55) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ |
| Overall | $\begin{gathered} 0.84 \\ (0.83) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.85 \\ (0.85) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.86 \\ (0.88) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.88 \\ (0.88) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ | $\begin{gathered} 0.91 \\ (0.92) \end{gathered}$ | $\begin{gathered} \text { D } \\ \text { (D) } \end{gathered}$ |
| Britannia Rd West \& Ellesboro Dr |  |  |  |  |  |  |  |  |  |  |
| EBL | $\begin{gathered} 0.07 \\ (0.06) \end{gathered}$ | $\begin{gathered} \mathrm{A} \\ (\mathrm{~A}) \end{gathered}$ | $\begin{gathered} 0.07 \\ (0.07) \end{gathered}$ | $\begin{gathered} \text { A } \\ (A) \end{gathered}$ | $\begin{gathered} 0.08 \\ (0.07) \end{gathered}$ | A <br> (A) | $\begin{gathered} 0.08 \\ (0.07) \end{gathered}$ | $\begin{gathered} \text { A } \\ (A) \end{gathered}$ | $\begin{gathered} 0.08 \\ (0.07) \end{gathered}$ | $\begin{gathered} \text { A } \\ (\mathrm{A}) \end{gathered}$ |
| EBT | $\begin{gathered} 0.59 \\ (0.45) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { A } \\ & \text { (A) } \end{aligned}$ | $\begin{gathered} 0.60 \\ (0.46) \\ \hline \end{gathered}$ | A <br> (A) | $\begin{gathered} 0.60 \\ (0.46) \\ \hline \end{gathered}$ | A <br> (A) | $\begin{gathered} 0.61 \\ (0.46) \\ \hline \end{gathered}$ | $\begin{aligned} & \text { A } \\ & \text { (A) } \end{aligned}$ | $\begin{gathered} 0.62 \\ (0.47) \\ \hline \end{gathered}$ | A <br> (A) |
| WBTR | $\begin{gathered} 0.36 \\ (0.50) \\ \hline \end{gathered}$ | $\begin{gathered} \text { A } \\ (\mathrm{A}) \end{gathered}$ | $\begin{gathered} 0.37 \\ (0.51) \\ \hline \end{gathered}$ | A <br> (A) | $\begin{gathered} 0.37 \\ (0.52) \\ \hline \end{gathered}$ | A <br> (A) | $\begin{gathered} 0.37 \\ (0.52) \\ \hline \end{gathered}$ | $\begin{gathered} \text { A } \\ (\mathrm{A}) \end{gathered}$ | $\begin{gathered} 0.38 \\ (0.53) \\ \hline \end{gathered}$ | A <br> (A) |
| SBL | $\begin{gathered} 0.50 \\ (0.59) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ (\mathrm{E}) \end{gathered}$ | $\begin{gathered} 0.50 \\ (0.59) \end{gathered}$ | $\begin{gathered} E \\ (E) \end{gathered}$ | $\begin{gathered} 0.50 \\ (0.59) \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.50 \\ (0.59) \end{gathered}$ | $\begin{gathered} E \\ (E) \end{gathered}$ | $\begin{gathered} 0.50 \\ (0.59) \end{gathered}$ | $\begin{gathered} E \\ (E) \end{gathered}$ |
| SBR | $\begin{gathered} 0.02 \\ (0.05) \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{E} \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.02 \\ (0.05) \\ \hline \end{gathered}$ | $\begin{gathered} E \\ (E) \end{gathered}$ | $\begin{gathered} 0.02 \\ (0.05) \\ \hline \end{gathered}$ | $\begin{gathered} E \\ \text { (E) } \end{gathered}$ | $\begin{gathered} 0.02 \\ (0.05) \\ \hline \end{gathered}$ | $\begin{gathered} E \\ (E) \end{gathered}$ | $\begin{gathered} 0.02 \\ (0.05) \\ \hline \end{gathered}$ | $\begin{gathered} E \\ (E) \\ \hline \end{gathered}$ |
| Overall | $\begin{gathered} 0.58 \\ (0.51) \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { (A) } \end{gathered}$ | $\begin{gathered} 0.59 \\ (0.52) \end{gathered}$ | A <br> (A) | $\begin{gathered} 0.60 \\ (0.53) \end{gathered}$ | A <br> (A) | $\begin{gathered} 0.60 \\ (0.53) \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { (A) } \end{gathered}$ | $\begin{gathered} 0.61 \\ (0.54) \end{gathered}$ | $\begin{gathered} \text { A } \\ \text { (A) } \end{gathered}$ |

Note:

1. $x x(x x)$ : Weekday morning peak hour (Weekday afternoon peak hour).

### 12.3.1 Britannia Road West / Queen Street

Under existing conditions, the Britannia Road West / Queen Street signalized intersection operates under acceptable conditions at all times. Overall volume to capacity (v/c) ratios are 0.84 and 0.83 for the weekday morning and afternoon peak hours, respectively.

With the addition of future background traffic in the 5 -year planning horizon, the intersection will remain within capacity, with an overall $\mathrm{v} / \mathrm{c}$ ratio of 0.85 in both peak hours. With the addition of site traffic for this horizon, the intersection will remain within capacity, with overall $\mathrm{v} / \mathrm{c}$ ratios of 0.86 and 0.88 in the weekday morning and afternoon peak hours, respectively.

With the addition of future background traffic in the 10-year planning horizon, the intersection will remain within capacity, with an overall $\mathrm{v} / \mathrm{c}$ ratio of 0.88 in both peak hours. With the addition of site traffic for this horizon, the intersection will remain within capacity, with overall v/c ratios of 0.91 and 0.92 in the weekday morning and afternoon peak hours, respectively.

With development of the Site as planned, the intersection can operate within capacity at all times.

### 12.3.2 Britannia Road West / Ellesboro Drive

Under existing conditions, the Britannia Road West / Ellesboro Drive signalized intersection operates under acceptable conditions at all times. Overall volume to capacity (v/c) ratios are 0.58 and 0.51 for the weekday morning and afternoon peak hours, respectively.

With the addition of future background traffic in the 5 -year planning horizon, the intersection will remain within capacity, with overall $\mathrm{v} / \mathrm{c}$ ratios of 0.59 and 0.52 in the weekday morning and weekday afternoon peak hours, respectively. With the addition of site traffic for this horizon, the intersection will remain within capacity, with overall $\mathrm{v} / \mathrm{c}$ ratios of 0.60 and 0.53 in the weekday morning and afternoon peak hours, respectively.

With the addition of future background traffic in the 10-year planning horizon, the intersection will remain within capacity, with overall $\mathrm{v} / \mathrm{c}$ ratios of 0.60 and 0.53 in the weekday morning and weekday afternoon peak hours, respectively. With the addition of site traffic for this horizon, the intersection will remain within capacity, with overall $\mathrm{v} / \mathrm{c}$ ratios of 0.61 and 0.54 in the weekday morning and afternoon peak hours, respectively.

With development of the Site as planned, the intersection can operate within capacity at all times.

### 12.4 UNSIGNALIZED INTERSECTIONS

Unsignalized intersection operations were analyzed under existing, future background and future total traffic conditions for both the morning and afternoon peak hours. Table 22 summarizes results of the unsignalized intersection traffic operations analyses, including the Site driveway.

Table 22 Unsignalized Intersection Analysis Summary


Table continued on following page.


All area unsignalized intersections, inclusive of the Site driveway, operate adequately today and will continue to operate well under future conditions with background traffic growth and redevelopment of the Site.

### 12.5 SIGNAL WARRANT - QUEEN STREET N \& MATLOCK AVENUE

A signal warrant analysis was undertaken for the intersection of Queen Street North and Matlock Avenue, under existing, 10-year future background and 10-year future total conditions. Ontario Traffic Manual Book 12 (March, 2012) was consulted for the warrant.

In the absence of 8-hour traffic volumes for the intersection, 'Justification 7 - Projected Volumes' was utilized to determine the future need for a traffic signal at the existing intersection. As part of the transportation study, peak hour volumes (PHV) are estimated and converted into average hourly volumes (AHV) which can be compared with traffic signal justification thresholds for projected volumes.

As all three scenarios failed to meet the traffic signal justification, a signal isn't warranted or required at the intersection at this time. Justification tables demonstrating further details are included in Appendix J.

Pedestrian crossing volumes across Queen Street North at this location are also very low (less than one per hour on average), as only a railway reserve lies opposite Matlock Drive on the west side of Queen Street North. Consequently, further to not explicitly meeting the signal warrant, a traffic signal would not have any value in enhancing pedestrian safety or connectivity at this location.

### 13.0 COMMUNITY IMPACTS

One of the key considerations in this study is the generation of traffic resulting from development of the Site. While it is anticipated that the project will generate additional vehicular activity, impacts on the community are expected to be minimal and generally localized to the arterial road network.

Nearby arterial roads are designed to handle higher traffic volumes and have sufficient capacity to accommodate the projected increase. Existing intersections near the proposed development have been evaluated and found to be capable of accommodating the additional traffic generated by the Site. Table 23 provides a summary of net-new two-way traffic volumes added to key road sections within the study area during peak hours.

## Table 23 Net-New Two-Way Traffic Volume Summary

| Road Name | Road Classification | Net-New Two-Way Volumes |
| :--- | :---: | :---: |
| Britannia Road West | Regional Arterial | $20(25)$ |
| Queen Street North | Major Collector | $75(85)$ |
| Queen Street South | Major Collector (Scenic Route) | $30(40)$ |
| Arch Road, Earl Street, Matlock <br> Avenue, Ellesboro Drive | Local | $<5$ |

Notes:

1. $\quad x x(x x)=$ weekday morning peak hour (weekday afternoon peak hour).

In summary, the immediate residential areas surrounding the development are unlikely to experience any noticeable impact on traffic flow or congestion.

### 14.0 SUMMARY AND CONCLUSIONS

Key findings of the transportation review are as follows:

## Context

1. The Site is currently known as the "Streetsville Plaza". The Streetsville Plaza contains the following stores and services: Qasimul Uloom (Islamic Culture) Centre, Erum's Creations, Evan's Variety store, Streetsville Martial Arts Karate, Belmonte Unisex Salon Hairstylists, Tulipz Spa, Queen Street Burger and Taters, Mediterranean Meats \& Deli, Smart Vaccum Plus, Baghad Pastries \& Catering, Offside Sports Bar and Roti Vybz. In addition to the stores and services located within the commercial plaza, there is a parking lot available in front of the strip of stores.
2. The subject Site is located in an area that contain sidewalks along Queen Street North and the surrounding roads to allow for pedestrian movement, cycling facilities, and MiWay services including the 10, 39, 43, 44, 87 and 306 bus routes.
3. There are various cycling facilities surrounding the site including the immediate bike lane along Queen Street South and a multi-use trail along Britannia Road West. The existing cycling network is planned to be further connected with the proposed new cycling facilities that will improve connectivity.

## Proposed Development

4. A Zoning By-law Amendment (ZBA) and Official Plan Amendment (OPA) application is being made to permit the proposed development of a 9-storey mixed-used building consisting of 444 residential units and a retail component with a GFA of $1,423 \mathrm{~m}^{2}$ located at-grade.
5. The applicant is proposing to provide a total parking supply of 359 parking spaces, including 311 residential parking spaces, 22 residential visitor parking spaces, 26 retail parking spaces. In addition to the overall parking supply, six (6) tandem parking spaces are proposed. Parking is provided in an underground two-level parking garage. A total of 170 parking spaces, including 26 retail spaces, 22 residential visitors and 122 residential spaces are located in the P1 level. A total of 189 residential spaces are located in the P2 level. In addition, the six (6) tandem spaces are located in the P2 level of the garage. Access to the underground parking garage is provided via the proposed driveway extending from Queen Street North.
6. A total of 386 bicycle parking spaces, including 330 long-term residential bicycle parking spaces and 56 short-term bicycle parking spaces are proposed for the Site. From the long-term bicycle parking supply, 326 are residential long-term spaces and four (4) are for retail long term spaces. From the short-term bicycle parking supply, 48 are residential short-term spaces, and eight (8) are short-term spaces. Access to the residential long-term and short-term bicycle storage rooms are provided from the path provided south of the site. The pathway connects east of Queen Street North.
7. Two loading spaces are proposed to be located at-grade adjacent to the proposed driveway extending from Queen Street North.

## Transportation Demand Management (TDM) Plan

8. A proposed transportation demand management (TDM) plan is proposed for the Site, both as a method to reduce vehicular traffic but also to reduce parking demand. Highlights of the Plan, in addition to the proposed parking supply reductions, are provided below:

- Provision of public pedestrian sidewalks on all new public streets within the Project's boundaries including a new pedestrian / cyclist pathway south of the building with adequate lighting;
- Provision of 386 bicycle parking spaces including 330 long-term bicycle parking spaces and 56 short-term spaces;
- Implementation of two bicycle repair/maintenance stations to be provided on-site;
- Implementation of a transit screen in the lobby;
- Provision of a pre-loaded PRESTO card with a value of $\$ 50$ to each first-time unit owner;
- Implementation of travel information brochures;
- A reduced parking rate is proposed on-site to reduce car dependence;
- Opportunities will be explored to offer ride-sharing programs on-site such as participation in the Smart Commute program; and
- Smart lockers will be provided to facilitate convenient deliveries for residents.


## Vehicular Parking

9. Application of the parking requirements outlined in the City of Mississauga's Zoning By-law 02252007 (amended by Zoning By-law 0118-2022) (Precinct 4) results a total requirement of 576 parking spaces, inclusive of 488 resident spaces and 88 non-resident spaces to be shared between resident visitors and retail visitors.
10. It is proposed to provide less parking than is required by the Zoning By-law 0225-2007 in accordance with 311 residential parking spaces ( 0.70 spaces per unit), 22 residential visitor parking spaces and 26 retail parking spaces resulting in a total parking supply of 359 parking spaces. In addition to the proposed parking supply, 6 tandem parking spaces will be provided.
11. In summary, the proposed resident parking supply rate ( 0.70 spaces per unit) and non-residential parking supply is considered to be appropriate based upon the following:

- The subject Site is in close proximity to existing transit services including the MiWay bus routes (i.e. $43,44,10,39,87$, and 306 bus routes), the Streetsville GO station, and bicycle route facilities that provide non-automobile dependent travel connections across the City;
- A series of Transportation Demand Management measures proposed to be incorporated in the development to support the use of non-automobile travel modes;
- A review of parking demands observed / recorded by BA Group at another residential condominium including resident and residential visitor supplies in the City of Mississauga with similar transit context; and
- Range of approvals for reductions in resident parking supply ratios for developments with less proximate access to a GO Station.


## Bicycle Parking

12. Bicycle parking standards have been introduced in the newly amended Zoning By-law 0225-2007 by the bicycle parking requirements outlined in Zoning By-law 0118-2022. Application of the bicycle parking standards to the Site will result in a total provision of 293 bicycle parking spaces, including five (5) spaces for retail and 288 spaces for residential.
13. A total of 386 bicycle parking spaces, including 330 long-term residential bicycle parking spaces and 56 short-term bicycle parking spaces are proposed for the Site. From the long-term bicycle parking supply, 326 are residential long-term spaces and four (4) are for retail long term spaces. From the short-term bicycle parking supply, 48 are residential short-term spaces, and eight (8) are short-term spaces. Access to the residential long-term and short-term bicycle storage rooms are provided from the path provided south of the site. The pathway connects east of Queen Street North.
14. The proposed bicycle parking supply meets and exceeds the requirements outlined in Zoning By-law 0225-2007, and is therefore an appropriate supply to serve the cycling needs of the proposed development. By providing a bicycle parking supply ( 386 bicycle parking spaces) that exceeds the By-law's requirement of 293 bicycle parking spaces, the applicant is not only ensuring compliance but also strategically supporting the reduced parking approach adopted for the development.

## Loading

15. Application of the City of Mississauga Zoning By-law 0225-2007 loading standards to the proposed development requires the provision of two (2) loading spaces, including one loading space for the residential use and one loading space for the retail component of the proposed development.
16. The development proposal includes two loading spaces located at-grade adjacent to the proposed northeast driveway. Loading access is provided from the proposed northeast driveway that extends from Queen Street North. The proposed loading supply meets the Zoning By-law 0225-2007 requirements.

## Multi-Modal Travel Demand Forecasts

17. Volumes were balanced to the 'primary' intersection at Britannia Road West / Queen Street, as this intersection was surveyed in 2019 before the onset of the Covid-19 pandemic. Volumes were balanced in all four cardinal directions along each corridor, to ensure matching to the 2019 survey at the master intersection.
18. Based on forecasting model outputs from both the City of Mississauga (for Queen Street) and the Region of Peel (for Britannia Road West), compounding corridor growth rates were applied along both corridors. All corridor growth rates have been applied over 10 years and are compounded annually.
19. Mississauga's development applications map was reviewed to check for other development applications within the surrounding area that may impact traffic growth at the study intersections. It was identified that the development at 6, 10, and 12 Queen Street South, 16 James Street, 2 William Street and 0 William Street (OZ/OPA 21 14) would impact the area street network and has therefore been considered as background traffic based on NexTrans' transportation report dated August 2021. The development includes 77 townhomes with retail space fronting Queen Street.
20. Traffic surveys for the Site's existing driveway demonstrated the generation of some peak hour traffic. Future total conditions account for existing Site traffic removal based on the approximate trip distribution patterns realized within the existing survey data.
21. The vehicle trip generation rates adopted for the purposes of this study are based on rates outlined within the ITE Trip Generation Manual 11th Edition for Land Use Codes 221 (Mid-Rise Residential) and 822 (Strip Retail Plaza <40k).
22. Vehicle trip generation is extrapolated into multimodal person trips, based on methodology in Section 5.3 of the ITE Trip Generation Handbook (3rd Edition). The volumes are subsequently adjusted from ITE's baseline vehicle mode share to the vehicle mode share applicable to the Site.
23. The Site is expected to generate in the order of $\mathbf{1 1 5}$ and $\mathbf{1 2 5}$ new two-way vehicle trips in the weekday morning and afternoon peak hours, respectively.
24. TTS data suggest that the area has an auto driver mode share in the order of $64 \%$ and $67 \%$ for morning outbound and afternoon inbound home-based trips during the peak travel periods, respectively.
25. The proposed development is forecast to generate $\mathbf{1 8 0}$ and $\mathbf{1 8 5}$ net-new two-way person trips during the weekday morning and weekday afternoon peak hours, respectively.

## Traffic Operations Analysis

26. Traffic operations analyses have been undertaken during the weekday morning and afternoon street peak hours under baseline existing, future background and future total conditions.
27. Overall, signalized intersections proximate to the Site operate well in all scenarios. The Site can be comfortably accommodated by the existing road network with no changes to signal timings required.
28. Unsignalized intersection operations were analyzed under existing, future background and future total traffic conditions for both the morning and afternoon peak hours.
29. All area unsignalized intersections, inclusive of the Site driveway, operate well today and will continue to operate acceptably under future conditions with background traffic growth and redevelopment of the Site.
30. A signal warrant analysis was undertaken for the intersection of Queen Street North and Matlock Avenue, under existing, 10-year future background and 10-year future total conditions. As all three scenarios failed to meet the traffic signal justification, a signal isn't warranted or required at the intersection at this time.

## Overall Conclusion

31. Based upon our review of the development proposal for 21-51 Queen Street North, including 444 residential units and $1,423 \mathrm{~m}^{2}$ GFA of retail space, can be reasonably accommodated on the surrounding area road network for all types of travel modes (i.e. transit, walking, cycling and vehicle).

Appendix A:
Reduced Scale Architectural Plans


GROSS FLOOR AREA (GFA) - APARTMENT ZONE
MEANS THE SUM OF THE AREAS OF EACH STOREY OF A BULDING ABOVE OR BELOW ESTABLISHED GRADE, MEASURED PROM THE EXTERIOR OF OUTSIDE WALLS OF THE BULLDING INCLUDING FLOOR

 LEVEL2 Area *AVERAGE GRADE $165.55+165.05 / 2=165.30$

| Statistics/ Total |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NUMBER OF REPEATED FLOOR | GCA (ABOVE GRADE)- TOTAL |  | DEDUCTION |  |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} \text { TOTAL } \\ \text { DEDUCTION } \end{gathered}$ | GFA-TOTAL |  |
| Level |  | GCA | GCAsf | PARKING | STORAGE/BIKE | GARBAGE CHUTE | Elevator | MECH.PH | MECH.JELEC. | STAR | GARBAGE LOADING | $\begin{array}{\|c\|} \hline \text { RESIDENTIAL } \\ \text { GARBAGE LOADING } \\ \hline \end{array}$ | RETALL GARBAGE <br> LOADING | GARBAGE RETAL | INDOOR AMENTY |  | GFA | GFAsf |
| LEVEL1 | 1 | $5.648 .6 \mathrm{~m}^{2}$ | 60,801.1 SF | 247.2m ${ }^{2}$ | $406.5 \mathrm{~m}^{2}$ | $0.3 \mathrm{~m}^{2}$ | $36.9 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $1.2 \mathrm{~m}^{2}$ | $63.1 \mathrm{~m}^{2}$ | $283.4 \mathrm{~m}^{2}$ | $216.1 \mathrm{~m}^{2}$ | $23.9 \mathrm{~m}^{2}$ | $135.4 \mathrm{~m}^{2}$ | $313.5 \mathrm{~m}^{2}$ | $1.777 .3 \mathrm{~m}^{2}$ | 3.921 .3 m ${ }^{\text {m }}$ | 42,20.3 SF |
| LEVEL2 | 1 | $3.442 .1 \mathrm{~m}^{2}$ | 37,050,7 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $25.3 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $359.4 \mathrm{~m}^{2}$ | $101.5 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $906.9 \mathrm{~m}^{2}$ | $1,393.6 \mathrm{~m}^{2}$ | 2,048.5 m ${ }^{\text {m }}$ | 22,049.8 SF |
| LEVEL3 | 1 | $4,052.4 \mathrm{~m}^{2}$ | 43,619.9 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $11.8 \mathrm{~m}^{2}$ | $55.8 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $258.2 \mathrm{~m}^{2}$ | $349.2 \mathrm{~m}^{2}$ | 3.703 .2 m ${ }^{\text {m }}$ | 3, $2,81.4 \mathrm{SF}$ |
| LEVEL4 | 1 | $4,052.9 \mathrm{~m}^{2}$ | 43,624.5SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $11.8 \mathrm{~m}^{2}$ | $55.9 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $91 \mathrm{~m}^{2}$ | $3.961 .8 \mathrm{~m}^{2}$ | 42,644.5 SF |
| LEVEL5 | 1 | $3,771.9 \mathrm{~m}^{2}$ | 34,142,3 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $9.4 \mathrm{~m}^{2}$ | $53.1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $85.8 \mathrm{~m}^{2}$ | $3.086 .1 \mathrm{~m}^{2}$ | 33,218.3 SF |
| LEVEL6 | 1 | $3.201 .3 \mathrm{~m}^{2}$ | 34,458 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $9.4 \mathrm{~m}^{2}$ | $53.1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $85.9 \mathrm{~m}^{2}$ | $3.115 .4 \mathrm{~m}^{2}$ | 33,533.9 SF |
| LEVEL 7.8 | 2 | 5,883.4 m ${ }^{\text {m }}$ | 63,328.6 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $1.2 \mathrm{~m}^{2}$ | $45.5 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $18.8 \mathrm{~m}^{2}$ | $102.7 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $168.2 \mathrm{~m}^{2}$ | $5.715 .2 \mathrm{~m}^{2}$ | 61,518 SF |
| LEVEL9 | 1 | $2.772 .8 \mathrm{~m}^{2}$ | 29,845.9 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | 0.6 m ${ }^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $9.5 \mathrm{~m}^{2}$ | $53.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $85.9 \mathrm{~m}^{2}$ | 2.686 .9 m ${ }^{\text {m }}$ | 28,921.7 SF |
| MPH | 1 | $478 \mathrm{~m}^{2}$ | 5,145.6 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $32.5 \mathrm{~m}^{2}$ | 410.4 m ${ }^{2}$ | $0.0 \mathrm{~m}^{2}$ | $35.1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $1 \mathrm{~m}^{2}$ | $478 \mathrm{~m}^{2}$ | $1 \mathrm{~m}^{2}$ | 0SF |
|  |  | $32,703.4 \mathrm{~m}^{2}$ | 352,016.7 SF | $24.2 \mathrm{~m}^{2}$ | $406.5 \mathrm{~m}^{2}$ | $5.0 \mathrm{~m}^{2}$ | $254.0 \mathrm{~m}^{2}$ | $410.4 \mathrm{~m}^{2}$ | $431.3 \mathrm{~m}^{2}$ | $573.3 \mathrm{~m}^{2}$ | $283.4 \mathrm{~m}^{2}$ | $216.1 \mathrm{~m}^{2}$ | 23.9 m | $135.4 \mathrm{~m}^{2}$ | $1,478.6 \mathrm{~m}^{2}$ | 4,465 m | 28,238.4 m ${ }^{2}$ | 303,955.9 |


| STATISTICS/ RESIDENTAL |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NUMBER OFREPEATED FLOOR | GCAAABOVE GRADE)-RES. |  | DEDUCTION |  |  |  |  |  |  |  |  |  |  |  | $\begin{gathered} \text { TOTAL } \\ \text { DEDUCTION } \\ \hline \end{gathered}$ | GFA RESIDENTIAL |  |
| LEVEL |  | GCA | GCAsf | PARKING | STORAGE/BIKE | GARBAGE CHUTE | Elevator | MECH.PH | MECH/ELEEC. | STAR | GARBAGE LOADING | $\begin{array}{c\|} \text { RESIDENTIAL } \\ \text { GARBAGE LOADING } \end{array}$ | RETAIL GARBAGE LOADING | GARBAGE RETALL | $\begin{aligned} & \text { INDOOR } \\ & \text { AMENITY } \end{aligned}$ |  |  | GFA sf |
| LEVEL 1 | 1 | 4,066.1 $\mathrm{m}^{2}$ | 43,767.2 SF | $247.2 \mathrm{~m}^{2}$ | $406.5 \mathrm{~m}^{2}$ | $0.3 \mathrm{~m}^{2}$ | $36.9 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $1.2 \mathrm{~m}^{2}$ | $63.0 \mathrm{~m}^{2}$ | $283.4 \mathrm{~m}^{2}$ | $216.1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $313.5 \mathrm{~m}^{2}$ | $1,568 \mathrm{~m}^{2}$ | $2.498 .1 \mathrm{~m}^{2}$ | 26,889,4 SF |
| LLVEL2 | 1 | $3.442 .1 \mathrm{~m}^{2}$ | 37,050,7 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $25.3 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $359.4 \mathrm{~m}^{2}$ | $101.5 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | 906.9 m ${ }^{\text {2 }}$ | $1,393.6 \mathrm{~m}^{2}$ | $2.048 .5 \mathrm{~m}^{2}$ | 22,049.8 SF |
| LEVEL 3 | 1 | 4,052.4 m ${ }^{2}$ | 43,619.9 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $11.8 \mathrm{~m}^{2}$ | $55.8 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $258.2 \mathrm{~m}^{2}$ | $349.2 \mathrm{~m}^{2}$ | 3,703.2 $\mathrm{m}^{2}$ | 39,861.4 SF |
| LEVEL 4 | 1 | 4,052.9 m ${ }^{\text {2 }}$ | 43,624.5 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $11.8 \mathrm{~m}{ }^{2}$ | $55.9 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $91 \mathrm{~m}^{2}$ | $3.961 .8 \mathrm{~m}^{2}$ | 42,644.5 SF |
| LEVEL5 | 1 | $3,171.9 \mathrm{~m}^{2}$ | 34,142.3 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $9.4 \mathrm{~m}^{2}$ | $53.1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $85.8 \mathrm{~m}^{2}$ | 3,086.1 $\mathrm{m}^{2}$ | 33,218,3 SF |
| LEVEL6 | 1 | $3.201 .3 \mathrm{~m}^{2}$ | 34,458 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $22.8 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $9.4 \mathrm{~m}^{2}$ | $53.1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $85.9 \mathrm{~m}^{2}$ | $3.115 .4 \mathrm{~m}^{2}$ | 33,533.9 SF |
| LEVEL 7-8 | 2 | 5,883.4 $\mathrm{m}^{2}$ | 63,328.6 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $1.2 \mathrm{~m}^{2}$ | $45.5 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | 18.8 m ${ }^{2}$ | $102.7 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $168.2 \mathrm{~m}^{2}$ | $5.715 .2 \mathrm{~m}^{2}$ | 61,518 SF |
| LEVEL 9 | 1 | $2,772.8 \mathrm{~m}^{2}$ | 29,845.9 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.6 \mathrm{~m}^{2}$ | $228 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $9.5 \mathrm{~m}^{2}$ | $53.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $85.9 \mathrm{~m}^{2}$ | $2,886.9 \mathrm{~m}^{2}$ | 28,921.7 SF |
| MPH | 1 | $478 \mathrm{~m}^{2}$ | 5,145.6 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $32.5 \mathrm{~m}^{2}$ | $410.4 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $35.1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $478 \mathrm{~m}^{2}$ | $1 \mathrm{~m}^{2}$ | OSF |
|  |  | $31,120.9 \mathrm{~m}^{2}$ | 334,982.8 SF | $247.2 \mathrm{~m}^{2}$ | $406.5 \mathrm{~m}^{2}$ | $5.0 \mathrm{~m}^{2}$ | $254.0 \mathrm{~m}^{2}$ | $410.4 \mathrm{~m}^{2}$ | $431.3 \mathrm{~m}^{2}$ | $573.3 \mathrm{~m}^{2}$ | $283.4 \mathrm{~m}^{2}$ | $216.1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $1478.6 \mathrm{~m}^{2}$ | 4,305.7 m² | 26,815.3 $\mathrm{m}^{2}$ | 288,637 |


| STATISTICS/ RETALL |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Level | NUMBER OF REPEATED FLOOR | GCAABOVE GRADE) RETAAL |  | DEDUCTION |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { TOTAL } \\ & \text { DEDUCTION } \end{aligned}$ | GFA-RETAL |  |
|  |  | GCA | GCAsf | PARKING | Area Storage/Bike | GARBAGE CHUTE | Elevator | MECH.PH | MECH.ELEC. | STAR | GARBAGE LOADING | RESIDENTIAL <br> GARBAGE LOADING | RETAIL GARBAGE LOADING | GARBAGE Retall | INDOOR |  | GFA | GFA sf |
| LEVEL1 | 1 | 1,582.5 m² | 17,033.9 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ |  | $1 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $23.9 \mathrm{~m}^{2}$ | $135.4 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $159.3 \mathrm{~m}^{2}$ | 1,423.2 | 15,318.9 SF |
|  |  | ${ }^{1,5882.5 \mathrm{~m}^{2}}$ | 17,033.9 SF | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $0 \mathrm{~m}^{2}$ | $0.0 \mathrm{~m}^{2}$ | $\begin{aligned} & \text { 23.9 } \mathrm{m}^{2} \\ & \text { NOTE: } 90 \% \text { OF LC } \\ & 10 \% \text { OF LC } \end{aligned}$ | $135.4 \mathrm{~m}^{2}$ OADING AREA OADING AREA | $0.0 \mathrm{~m}^{2}$ HAS BEEN HAS BEEN | $159.3 \mathrm{~m}^{2}$ EDUCTED FOR R EDUCTED FOR R | 1,423.2 ${ }^{2} \quad 15,318.9 \mathrm{SF}$ EIIDENTIAL GFA CALCULATION etall gfa calculation |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| LOADING AREA REQUIRED |  | REQUIRED <br> 2 | $\begin{gathered} \hline \text { PRoVIDED } \\ \hline \text { NA } \end{gathered}$ | GCA (BELOW GRADE PARKING AREA) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ReTALL: | BETWEEN 2,350 sm UP TO 7,500 sm |  |  | Level | NUMBER OF REPEATED FLOOR | GCA | GCAsf |
| RETAL: | BETWEEN 250 sm UP TO $2,350 \mathrm{sm}$ | 1 | 1 | P2 | 1 | $7,240 \mathrm{~m}^{2}$ | 77,931 SF |
| RESIDENTAL | APARTMENT MORE THAN 30 UNITS | 1 | 1 | P1 | 1 | 7,296.5 m² | 78,539 SF |


| RESIIENTIAL UNIT COUNT |  |  |  |  |  |  |  |  | UNT COUNT |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LevEL | NUMBER OF REPEATED FLOOR | RESIDENTAL UNIT COUNT |  |  |  |  |  |  | STUDIO | ${ }_{15}^{15}$ | $\begin{aligned} & \hline 1 \mathrm{BD} \\ & \hline 174 \\ & \hline \end{aligned}$ | ${ }_{76}^{28}$ | ${ }_{2}^{2 B D}$ |  | 3 B | TOTAL UNTT |  |  |
|  |  | STUDIO | 1 B | 1BD | 2 C | 2BD | 3B | $\begin{array}{\|c\|} \hline \text { TOTAL } \\ \text { UNIT } \\ \hline \end{array}$ | 175 |  |  |  |  |  | 444 |
| LEVEL 1 | 1 | 8 | 2 | 1 | 10 | 0 | 0 | 21 | 'UNTT BREAKDOWN\% |  |  |  |  |  |  |  |  |  |
| LEVEL2 | 1 | 20 | 0 | 1 | 10 | 0 | 0 | 31 | NUMBER | ROF UN |  | Studio |  | B 18D |  | 17.1\% | 2BD 0.5 |  | ${ }^{\text {3B }}$ - 5 TOTAL 100.0 |
| LEVEL 3 | 1 | 23 | 2 | 32 | 8 | 0 | 0 | 65 | 444 |  |  | 39.4\% | 3.4\% | 39.2\% |  |  |  |  |  |
| LEVEL 4 | 1 | 27 | 2 | 33 | 9 | 0 | 0 | 71 |  |  |  |  |  |  |  |  |  |  |  |
| LEVEL5 | 1 | 22 | 2 | 22 | 9 | 0 | 0 | 55 | *UNIT BREAKDOWN COUNT\% |  |  |  |  |  |  |  |  |  |  |
| LEVEL6 | 1 | 20 | 2 | 24 | 9 | 0 | 0 | 55 | NUMBER OF UNITS |  |  | STudo | 1B+1BD |  | $2 \mathrm{C}+28 \mathrm{~B}+3 \mathrm{~B}$ |  |  | TOTAL \% |  |
| LEVEL 7 -8 | 2 | 36 | 4 | 44 | 16 | 0 | 0 | 100 | 444 394\% |  |  |  | 42.6\% |  | 18.0\% |  |  | 100.0 |  |
| LEVEL9 | 1 | 19 | 1 | 17 | 5 | 2 | 2 | 46 |  |  |  |  | AVERAGE UNIT |  |  |  |  |  |  |  |  |  |
| MPH | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 175 | 15 | 174 | 76 |  | 2 | 444 | NUMBER OF UNITS |  |  | SALEABL |  | $\begin{array}{\|l\|} \hline \text { AVERAGE UNITS } \\ \hline 52 \mathrm{~m}^{2} \\ \hline \end{array}$ |  | AVERAGE UNIT SF |  |  |  |



MIN EXTERIOR AMENTY 55 sm MINEXROVIDED EXTERIOR AMENTY: \begin{tabular}{|c|c|}
\hline LEVEL \& Area <br>
\hline LVEIS \& $1098 \mathrm{~m}^{2}$ <br>
\hline

 

\hline LEVEL3 \& $1,098 \mathrm{~m}^{2}$ <br>
\hline Grand total \& $1,098 \mathrm{~m}^{2}$ <br>
\hline
\end{tabular}

exterior amenty ratio: total areal


| RESIDENTAL UNIT COUNT B.F |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LeVEL | NUMBER OF REPEATED FLOOR | RESIDENTIAL UNIT COUNT |  |  |  |  |  |  |
|  |  | STUDIO | 18 | 1BD | $2 \mathrm{2B}$ | 2 DB | 3 B | $\begin{array}{\|l\|l\|} \hline \text { TOTAL } \\ \text { UNNT } \end{array}$ |
| LLVEL1 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 1 |
| LEVEL2 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 3 |
| LEVEL 3 | 1 | 4 | 0 | 5 | 1 | 0 | 0 | 10 |
| LEVEL 4 | 1 | 4 | 0 | 5 | 1 | 0 | 0 | 10 |
| LEVEL 5 | 1 | 3 | 0 | 5 | 2 | 0 | 0 | 10 |
| LEVEL 6 | 1 | 3 | 0 | 5 | 2 | 0 | 0 | 10 |
| LEVEL 7.8 | 2 | 6 | 0 | 10 | 4 | 0 | 0 | 20 |
| LEVEL9 | 1 | 4 | 0 | 0 | 1 | 0 | 2 | 7 |


| SALEABLE AREA |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| LEVEL | $\begin{aligned} & \text { NUMBER OF } \\ & \text { REPEATED } \\ & \text { FLOOR } \end{aligned}$ | SALEABLE (RESIDENTIAL) |  | SALEABLE (RETAL) |  |
|  |  | SALEABLE | SALEABLE sf | RETAILLEASABLE | $\begin{array}{c\|} \text { RETAIL } \\ \text { LEASABLE sf } \\ \hline \end{array}$ |
| LEVEL1 | 1 | $1.204 .9 \mathrm{~m}^{2}$ | 12,969 SF | $1.423 .2 \mathrm{~m}^{2}$ | 15,319 SF |
| LEVEL2 | 1 | $1.416 \mathrm{~m}^{2}$ | 15,242 SF | $0 \mathrm{~m}^{2}$ | 0 SF |
| LEVEL3 | 1 | 3,364.3 m ${ }^{\text {2 }}$ | 36,213 SF | $0 \mathrm{~m}^{2}$ | OSF |
| LEVEL4 | 1 | $3.622 .9 \mathrm{~m}^{2}$ | 38,997 SF | $0 \mathrm{~m}^{2}$ | 0 SF |
| LEVEL5 | 1 | 2.838 .6 m ${ }^{\text {m }}$ | 30,554 SF | $0 \mathrm{~m}^{2}$ | 0 SF |
| LEVEL6 | 1 | $2.867 .9 \mathrm{~m}^{2}$ | 30,870 SF | $0 \mathrm{~m}^{2}$ | 0 SF |
| LEVEL 7.8 | 2 | $5,250 \mathrm{~m}^{2}$ | 56,510 SF | $0 \mathrm{~m}^{2}$ | 0 SF |
| LEVEL9 | 1 | $2.458 .4 \mathrm{~m}^{2}$ | 26,462 SF | $0 \mathrm{~m}^{2}$ | 0SF |
| MPH | 1 | $0 \mathrm{~m}^{2}$ | OSF | $0 \mathrm{~m}^{2}$ | 0 SF |
|  |  | 23,023 m ${ }^{\text {2 }}$ | 247,818 SF | 1.423 .2 m ${ }^{\text {2 }}$ | 15,319 SF |


| UNIT SIZE: SM SF |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| STUDIO | 29 | 313 |  |  |
|  | 43 | 458 |  |  |
| 1B-1B+D | 43 | 458 |  |  |
| $2 \mathrm{~B}-2 \mathrm{~B}+\mathrm{D}$ | $\begin{aligned} & 61 \\ & 8 \end{aligned}$ | $\begin{gathered} 661 \\ 893 \end{gathered}$ |  |  |
|  |  |  | TTTAL PROPOSED EV |  |
|  |  |  | EV PARKING TYPE | COUNT |
| 3B | $\begin{aligned} & 87 \\ & 94 \end{aligned}$ | $\begin{aligned} & 941 \\ & 1,013 \end{aligned}$ | RESIDENTIAL REGULAR PARKING | 98 |
|  |  |  | RETALL REGULAR PARKING | 7 |
|  |  |  | VISITOR REGULAR PARKING | 9 |


| EV PARKING REQUIREMENTS (PROVIDED BY BA GROUP) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| USE |  |  | PARKING REQUIREMENTS |  |  |
| RESIDENTIAL - CONDOMINUM APARTMENT RETALL STORE |  |  | 析 |  |  |
|  |  |  |  | 7 |  |
| VISTOR - CONDOMINUM APARTMENT |  |  | 114 |  |  |
| TOTAL |  |  |  |  |  |
| *GARBAGE | GARBAGE ROOM | $\begin{aligned} & \text { REQUIRED } \\ & \mathrm{sm} \end{aligned}$ | $\underset{s m}{\text { PROVIDED }}$ | total garbage area |  |
|  |  |  |  | LEVEL | GARBAGE AREA |
|  | RESIDENTAL | 127.5 | 188.31 | P1 | $75.40 \mathrm{~m}^{2}$ |
|  | Retall |  | 134.94 | LEVEL1 | $283.41 \mathrm{~m}^{2}$ |
|  | BuLKROOM | 10 | 41 |  |  |
|  | STAGING | 44.4 | 54.10 | TOTAL | Retall garbage |
|  |  |  |  | LEVEL | RETALL GARBAGE |
|  | TOTAL (SM) | 181.9 | 418.35 | LevEL1 | $135.39 \mathrm{~m}^{2}$ |
|  |  |  |  |  | $135.39 \mathrm{~m}^{2}$ |
| GARBAGE RO STAGING: 5 s GARBAGE | DOM: MIN. 25 sm F m FOR EVERY 50 50) RECYCLE (1/50 | OR THE FIRS UNTS ) ORGANIC | 50 UNITS AND <br> 100) | ITIONAL 50 |  |


©MIN. CLEAR HEIGHT FOR LOADING $=7.5 \mathrm{~m}$

| PARKING REQUIREMENTS (PROVIDED BY BA GROUP) |  |  |  |
| :---: | :---: | :---: | :---: |
| Resident Rate |  |  |  |
| USE | UNTTS / SQ.M | BY-LAW | PARKING REQUIREMENTS |
| RESIDENTIAL - CONDOMINUM APARTMENT | 444 UNITS | 1.1 SPACE/UNTS | 488 |
| RESIDENTAL SUBTOTAL |  |  | 488 |
| Rate NON - RESIDENTIAL RATE |  |  |  |
| USE | UNITS / SQ.M | BY-LAW | PARKING REQUIREMENTS |
| VIITOR - CONDOMINUM APARTMENT | 444 UNITS | 0.2 SPACE/ UNTS | 88 |
| Retail Store | 1,424 M2 GFA | 5 Space 1100 M2 GFA | 71 |
| NON- RESIDENTAL SUBTOTAL (BEFORE SHARRING) |  |  | 159 |
| NON- RESSIDENTIAL SHARED PARKING ARRAGEMENT |  |  | 88 |
| NON- RESIDENTAL SUBTOTAL (AFTER SHARING) |  |  | 88 |
| TOTAL |  |  |  |
| TOTAL RESIDENTAL +NON- RESIDENTIAL AFTER... |  |  | 576 |


| TOTAL RETAL PARKING |  |  |
| :---: | :---: | :---: |
| LevEL | PARKING TYPE | COUNT |
| P1 | Retall reGular parking | 25 |
| P1 | RETALL BARRIER FREE PARKING | 1 |
|  |  | 26 |


| TOTAL VISTOR PARKING |  |  |
| :---: | :---: | :---: |
| LEVEL | PARKING TYPE | COUNT |
| P1 | VISITOR REGULAR PARKING | 22 |
|  |  | 22 |
| TOTAL RESIDENTAL ( (NOT INCLUD TANDEM) |  |  |
| LEVEL | PARKING TYPE | COUNT |
| P2 | RESIDENTIAL REGULAR PARKING | 186 |
| P1 | RESIDENTAL REGULAR PARKING | 120 |
| P2 | RESIDENTIAL BARRIIER FREE TYPE A PARKING | 3 |
| P1 | RESIDENTIAL BARRIER FREE TYPE A PARKING | 2 |




## Low Impact Design Features List evelopment Density

The proposed development senves to maximize the permitted density on the land, maximizing efficient use of the lands while Mublin Trining gortatanan spraw

Public Transportation Access
$21-51$ Touen Street North will be located adjacent to several Misisissauga Transit bus lines. Furthermore, tits a short bus side to the
60 Train, therefore encouraging mass transit and consequequnty recucuing the carbon footprint.


| $\begin{array}{c}\text { pathways. } \\ \text { Bicycle torogege }\end{array}$ |
| :---: |

Convenienty located bicycle parking spaces for residents and visitors have been proposed to encourage bicycle use as an altemative Green Roof Syssem
 areas will not only help to reduce energy use and the heat island effect but will also senve as outcoor amenity and recreation areas.
areas will
New
Nees

busiding.
rosion Anc Sediment Control
The erosion and sediment controi plan for the site will be designed in conformance with the City of Mississauga and Credit Valley
Consenaion Aurity
Conseevation Authontity guidelines. Construction management will be taking erosion and sediment contol measures as well as
Green Sile Maintenance
Green Site Maintenanc


- Of he veticular parking provided, all will be contained within underground parking levels. This will reduce the heat sisland effect which results from exposeds surface parking lots
Indoor Water Use Reduction
- To reduce wated consumption, high-efficiency toiets and water reducing fixtures will be provided.
.Tri-Sotrer Recycling Atri-soret system will be installed and made accessibie to each residential floor, alowing for convenient separation and disposal of Rececycables and refuse.

12. Construction materials where available will be sourced from the GTA to minimize the carbon footpint associated with the stipment of meterials.

Private sidewalks and walkways are continuous, universally accessible, barier-free, and dlearly designated. Sidewalks within - immediate site vicinity have a buffer of vegetation between traffic and the walkway.

Wewsidewaks and patways are propossed
14. Site and Builiding Lighting (Incourporated)
 Avoid pp-Iighting from exterior light fixtures mounted on builingss unless they are designated as an integral component to a heritage
structure.



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THE MISS QuEEN
2.51 Quenenst. ., MISIISSAUGA, ontario
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STATISTICS



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Appendix B:
Signage Plan and Pavement Marking Plan


## Appendix C:

Vehicle Manoeuvring Diagrams (VMDs)







Appendix D:
Transportation Tomorrow Survey (TTS) Queries - Mode Splits

## TTS MODE SPLIT QUERY

Thu Sep 302021 13:54:11 GMT-0400 (Eastern Daylight Time)

Frequency Distribution Query Form - Trip - 2016 v1.1

Field: Primary travel mode of trip - mode_prime

Filters:
2006 GTA zone of origin - gta06_orig In 3718,3715,3717,3836
and
Trip purpose of origin - purp_orig $\ln \mathrm{H}$
and
Start time of trip - start_time In 600-859

Table: Trip 2016

| Row: | Count: | Expanded: $\%$ |  |
| :--- | ---: | ---: | ---: |
| Transit exclı | 12 | 296 | $7 \%$ |
| Cycle | 1 | 15 | $0 \%$ |
| Auto driver | 143 | 2886 | $64 \%$ |
| GO rail only | 14 | 171 | $4 \%$ |
| Joint GO rai | 8 | 126 | $3 \%$ |
| Auto passen | 30 | 600 | $13 \%$ |
| School bus | 8 | 133 | $3 \%$ |
| Taxi passen | 2 | 11 | $0 \%$ |
| Walk | 11 | 257 | $6 \%$ |
| Total: | 229 | 4493 | $100 \%$ |

Thu Sep 302021 13:54:54 GMT-0400 (Eastern Da

Frequency Distribution Query Form - Trip - 2016 v1

Field: Primary travel mode of trip - mode_prime

Filters:
2006 GTA zone of destination - gta06_dest In 371 \& and
Trip purpose of destination - purp_dest $\ln \mathrm{H}$
and
Start time of trip - start_time In 1500-1759

| Table: Trip 2016 | Count: |  |  |
| :--- | ---: | ---: | ---: |
| Row: | Expanded: $\%$ |  |  |
| Transit exclı | 5 | 98 | $2 \%$ |
| Auto driver | 149 | 2731 | $67 \%$ |
| GO rail only | 13 | 186 | $5 \%$ |
| Joint GO rai | 9 | 131 | $3 \%$ |
| Auto passen | 28 | 606 | $15 \%$ |
| School bus | 8 | 176 | $4 \%$ |
| Taxi passen | 1 | 7 | $0 \%$ |
| Walk | 6 | 165 | $4 \%$ |
| Total: | 219 | 4100 | $100 \%$ |


|  | AM | PM |
| :--- | :---: | :---: |
| Auto driver | $64 \%$ | $67 \%$ |
| Auto passe | $17 \%$ | $19 \%$ |
| Transit | $13 \%$ | $10 \%$ |
| Cycle | $0 \%$ | 0 |
| Walk | $6 \%$ | $4 \%$ |
|  | $100 \%$ | $100 \%$ |

Appendix E:
Sight Distance



## Appendix F:

 Traffic DataTurning Movement Count (24.BRITANNIA RD \& ARCH RD) CustID: 00305338 MioID:

|  | Westbound |  |  |  |  | Northbound |  |  |  |  | Eastbound |  |  |  |  | Int. Total (15 min) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | UTurn | Peds | Approach Total | Left | Right | UTurn | Peds | Approach Total | Thru | Right | UTurn | Peds | Approach Total |  |
| 07:00:00 | 2 | 146 | 0 | 0 | 148 | 0 | 2 | 0 | 1 | 2 | 429 | 0 | 0 | 0 | 429 | 579 |
| 07:15:00 | 2 | 171 | 0 | 0 | 173 | 0 | 0 | 0 | 4 | 0 | 510 | 2 | 0 | 0 | 512 | 685 |
| 07:30:00 | 5 | 198 | 0 | 0 | 203 | 2 | 3 | 0 | 6 | 5 | 553 | 2 | 0 | 0 | 555 | 763 |
| 07:45:00 | 5 | 285 | 0 | 0 | 290 | 0 | 5 | 0 | 0 | 5 | 560 | 0 | 0 | 0 | 560 | 855 |
| Hourly | 14 | 800 | 0 | 0 | 814 | 2 | 10 | 0 | 11 | 12 | 2052 | 4 | 0 | 0 | 2056 | 2882 |
| 08:00:00 | 4 | 268 | 0 | 0 | 272 | 2 | 1 | 0 | 2 | 3 | 640 | 2 | 0 | 0 | 642 | 917 |
| 08:15:00 | 0 | 275 | 0 | 0 | 275 | 1 | 4 | 0 | 1 | 5 | 674 | 1 | 0 | 0 | 675 | 955 |
| 08:30:00 | 1 | 357 | 0 | 0 | 358 | 2 | 3 | 0 | 3 | 5 | 593 | 0 | 0 | 0 | 593 | 956 |
| 08:45:00 | 3 | 291 | 0 | 0 | 294 | 2 | 4 | 0 | 1 | 6 | 572 | 1 | 0 | 0 | 573 | 873 |
| Hourly | 8 | 1191 | 0 | 0 | 1199 | 7 | 12 | 0 | 7 | 19 | 2479 | 4 | 0 | 0 | 2483 | 3701 |

***BREAK***

| 11:00:00 | 0 | 211 | 0 | 0 | 211 | 0 | 1 | 0 | 0 | 1 | 235 | 0 | 0 | 0 | 235 | 447 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11:15:00 | 1 | 211 | 0 | 0 | 212 | 1 | 1 | 0 | 0 | 2 | 253 | 2 | 0 | 0 | 255 | 469 |
| 11:30:00 | 0 | 181 | 0 | 0 | 181 | 2 | 0 | 0 | 0 | 2 | 226 | 4 | 1 | 0 | 231 | 414 |
| 11:45:00 | 0 | 231 | 0 | 0 | 231 | 0 | 2 | 0 | 0 | 2 | 249 | 1 | 0 | 0 | 250 | 483 |
| Hourly | 1 | 834 | 0 | 0 | 835 | 3 | 4 | 0 | 0 | 7 | 963 | 7 | 1 | 0 | 971 | 1813 |
| 12:00:00 | 0 | 239 | 0 | 0 | 239 | 1 | 0 | 0 | 2 | 1 | 282 | 0 | 0 | 0 | 282 | 522 |
| 12:15:00 | 4 | 231 | 0 | 0 | 235 | 2 | 0 | 0 | 0 | 2 | 246 | 4 | 0 | 0 | 250 | 487 |
| 12:30:00 | 0 | 217 | 0 | 0 | 217 | 0 | 2 | 0 | 1 | 2 | 262 | 0 | 0 | 0 | 262 | 481 |
| 12:45:00 | 3 | 232 | 0 | 0 | 235 | 0 | 1 | 0 | 0 | 1 | 290 | 1 | 0 | 0 | 291 | 527 |
| Hourly | 7 | 919 | 0 | 0 | 926 | 3 | 3 | 0 | 3 | 6 | 1080 | 5 | 0 | 0 | 1085 | 2017 |
| 13:00:00 | 1 | 240 | 0 | 0 | 241 | 1 | 1 | 0 | 2 | 2 | 233 | 0 | 0 | 0 | 233 | 476 |
| 13:15:00 | 0 | 224 | 0 | 0 | 224 | 1 | 1 | 0 | 2 | 2 | 257 | 1 | 0 | 0 | 258 | 484 |
| 13:30:00 | 0 | 240 | 0 | 0 | 240 | 1 | 0 | 0 | 0 | 1 | 217 | 0 | 0 | 0 | 217 | 458 |
| 13:45:00 | 0 | 264 | 0 | 0 | 264 | 0 | 1 | 0 | 2 | 1 | 253 | 1 | 0 | 0 | 254 | 519 |

Turning Movement Count
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| Hourly | 1 | 968 | 0 | 0 | 969 | 3 | 3 | 0 | 6 | 6 | 960 | 2 | 0 | 0 | 962 | 1937 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15:00:00 | 4 | 376 | 0 | 0 | 380 | 0 | 2 | 0 | 3 | 2 | 279 | 0 | 0 | 0 | 279 | 661 |
| 15:15:00 | 0 | 276 | 0 | 0 | 276 | 1 | 0 | 0 | 2 | 1 | 243 | 1 | 0 | 0 | 244 | 521 |
| 15:30:00 | 4 | 276 | 0 | 0 | 280 | 0 | 1 | 0 | 5 | 1 | 305 | 1 | 0 | 0 | 306 | 587 |
| 15:45:00 | 5 | 390 | 0 | 0 | 395 | 2 | 0 | 0 | 2 | 2 | 207 | 21 | 0 | 0 | 228 | 625 |
| Hourly | 13 | 1318 | 0 | 0 | 1331 | 3 | 3 | 0 | 12 | 6 | 1034 | 23 | 0 | 0 | 1057 | 2394 |
| 16:00:00 | 5 | 433 | 1 | 0 | 439 | 9 | 2 | 0 | 7 | 11 | 202 | 14 | 0 | 0 | 216 | 666 |
| 16:15:00 | 3 | 387 | 3 | 0 | 393 | 6 | 5 | 0 | 5 | 11 | 247 | 13 | 0 | 0 | 260 | 664 |
| 16:30:00 | 1 | 364 | 0 | 0 | 365 | 1 | 1 | 0 | 0 | 2 | 285 | 2 | 0 | 0 | 287 | 654 |
| 16:45:00 | 2 | 461 | 0 | 0 | 463 | 0 | 2 | 0 | 1 | 2 | 288 | 3 | 0 | 0 | 291 | 756 |
| Hourly | 11 | 1645 | 4 | 0 | 1660 | 16 | 10 | 0 | 13 | 26 | 1022 | 32 | 0 | 0 | 1054 | 2740 |
| 17:00:00 | 1 | 433 | 0 | 0 | 434 | 0 | 1 | 0 | 3 | 1 | 333 | 0 | 0 | 0 | 333 | 768 |
| 17:15:00 | 1 | 459 | 0 | 0 | 460 | 0 | 4 | 0 | 7 | 4 | 345 | 1 | 0 | 0 | 346 | 810 |
| 17:30:00 | 3 | 482 | 0 | 0 | 485 | 0 | 2 | 0 | 0 | 2 | 399 | 6 | 0 | 0 | 405 | 892 |
| 17:45:00 | 0 | 453 | 0 | 0 | 453 | 0 | 2 | 0 | 4 | 2 | 375 | 3 | 0 | 0 | 378 | 833 |
| Hourly | 5 | 1827 | 0 | 0 | 1832 | 0 | 9 | 0 | 14 | 9 | 1452 | 10 | 0 | 0 | 1462 | 3303 |
| Grand Total | 60 | 9502 | 4 | 0 | 9566 | 37 | 54 | 0 | 66 | 91 | 11042 | 87 | 1 | 0 | 11130 | 20787 |
| Approach\% | 0.6\% | 99.3\% | 0\% |  | - | 40.7\% | 59.3\% | 0\% |  | - | 99.2\% | 0.8\% | 0\% |  | - | - |
| Totals \% | 0.3\% | 45.7\% | 0\% |  | 46\% | 0.2\% | 0.3\% | 0\% |  | 0.4\% | 53.1\% | 0.4\% | 0\% |  | 53.5\% | - |
| Heavy | 0 | 291 | 0 |  | - | 3 | 5 | 0 |  | - | 285 | 5 | 0 |  | - | - |
| Heavy \% | 0\% | 3.1\% | 0\% |  | - | 8.1\% | 9.3\% | 0\% |  | - | 2.6\% | 5.7\% | 0\% |  | - | - |
| Bicycles | 0 | 1 | 0 |  | - | 0 | 0 | 0 |  | - | 4 | 0 | 0 |  | - | - |
| Bicycle \% | 0\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - |

## Peak Hour: 08:00 AM - 09:00 AM Weather: Mist $\left(13.18^{\circ} \mathrm{C}\right)$

| Start Time | Westbound |  |  |  |  | Northbound |  |  |  |  | Eastbound |  |  |  |  | Int. Total (15 min) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | UTurn | Peds | Approach Total | Left | Right | UTurn | Peds | Approach Total | Thru | Right | UTurn | Peds | Approach Total |  |
| 08:00:00 | 4 | 268 | 0 | 0 | 272 | 2 | 1 | 0 | 2 | 3 | 640 | 2 | 0 | 0 | 642 | 917 |
| 08:15:00 | 0 | 275 | 0 | 0 | 275 | 1 | 4 | 0 | 1 | 5 | 674 | 1 | 0 | 0 | 675 | 955 |
| 08:30:00 | 1 | 357 | 0 | 0 | 358 | 2 | 3 | 0 | 3 | 5 | 593 | 0 | 0 | 0 | 593 | 956 |
| 08:45:00 | 3 | 291 | 0 | 0 | 294 | 2 | 4 | 0 | 1 | 6 | 572 | 1 | 0 | 0 | 573 | 873 |
| Grand Total | 8 | 1191 | 0 | 0 | 1199 | 7 | 12 | 0 | 7 | 19 | 2479 | 4 | 0 | 0 | 2483 | 3701 |
| Approach\% | 0.7\% | 99.3\% | 0\% |  | - | 36.8\% | 63.2\% | 0\% |  | - | 99.8\% | 0.2\% | 0\% |  | - | - |
| Totals \% | 0.2\% | 32.2\% | 0\% |  | 32.4\% | 0.2\% | 0.3\% | 0\% |  | 0.5\% | 67\% | 0.1\% | 0\% |  | 67.1\% | - |
| PHF | 0.5 | 0.83 | 0 |  | 0.84 | 0.88 | 0.75 | 0 |  | 0.79 | 0.92 | 0.5 | 0 |  | 0.92 | - |
| Heavy | 0 | 55 | 0 |  | 55 | 0 | 1 | 0 |  | 1 | 44 | 1 | 0 |  | 45 | - |
| Heavy \% | 0\% | 4.6\% | 0\% |  | 4.6\% | 0\% | 8.3\% | 0\% |  | 5.3\% | 1.8\% | 25\% | 0\% |  | 1.8\% | - |
| Lights | 8 | 1136 | 0 |  | 1144 | 7 | 11 | 0 |  | 18 | 2435 | 3 | 0 |  | 2438 | - |
| Lights \% | 100\% | 95.4\% | 0\% |  | 95.4\% | 100\% | 91.7\% | 0\% |  | 94.7\% | 98.2\% | 75\% | 0\% |  | 98.2\% | - |
| Single-Unit Trucks | 0 | 17 | 0 |  | 17 | 0 | 1 | 0 |  | 1 | 13 | 1 | 0 |  | 14 | - |
| Single-Unit Trucks \% | 0\% | 1.4\% | 0\% |  | 1.4\% | 0\% | 8.3\% | 0\% |  | 5.3\% | 0.5\% | 25\% | 0\% |  | 0.6\% | - |
| Buses | 0 | 33 | 0 |  | 33 | 0 | 0 | 0 |  | 0 | 25 | 0 | 0 |  | 25 | - |
| Buses \% | 0\% | 2.8\% | 0\% |  | 2.8\% | 0\% | 0\% | 0\% |  | 0\% | 1\% | 0\% | 0\% |  | 1\% | - |
| Articulated Trucks | 0 | 5 | 0 |  | 5 | 0 | 0 | 0 |  | 0 | 6 | 0 | 0 |  | 6 | - |
| Articulated Trucks \% | 0\% | 0.4\% | 0\% |  | 0.4\% | 0\% | 0\% | 0\% |  | 0\% | 0.2\% | 0\% | 0\% |  | 0.2\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 7 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 100\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 2 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 12:00 PM-01:00 PM Weather: Broken Clouds ( $23.38^{\circ} \mathrm{C}$ )

| Start Time | Westbound |  |  |  |  | Northbound |  |  |  |  | Eastbound |  |  |  |  | Int. Total (15 min) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | UTurn | Peds | Approach Total | Left | Right | UTurn | Peds | Approach Total | Thru | Right | UTurn | Peds | Approach Total |  |
| 12:00:00 | 0 | 239 | 0 | 0 | 239 | 1 | 0 | 0 | 2 | 1 | 282 | 0 | 0 | 0 | 282 | 522 |
| 12:15:00 | 4 | 231 | 0 | 0 | 235 | 2 | 0 | 0 | 0 | 2 | 246 | 4 | 0 | 0 | 250 | 487 |
| 12:30:00 | 0 | 217 | 0 | 0 | 217 | 0 | 2 | 0 | 1 | 2 | 262 | 0 | 0 | 0 | 262 | 481 |
| 12:45:00 | 3 | 232 | 0 | 0 | 235 | 0 | 1 | 0 | 0 | 1 | 290 | 1 | 0 | 0 | 291 | 527 |
| Grand Total | 7 | 919 | 0 | 0 | 926 | 3 | 3 | 0 | 3 | 6 | 1080 | 5 | 0 | 0 | 1085 | 2017 |
| Approach\% | 0.8\% | 99.2\% | 0\% |  | - | 50\% | 50\% | 0\% |  | - | 99.5\% | 0.5\% | 0\% |  | - | - |
| Totals \% | 0.3\% | 45.6\% | 0\% |  | 45.9\% | 0.1\% | 0.1\% | 0\% |  | 0.3\% | 53.5\% | 0.2\% | 0\% |  | 53.8\% | - |
| PHF | 0.44 | 0.96 | 0 |  | 0.97 | 0.38 | 0.38 | 0 |  | 0.75 | 0.93 | 0.31 | 0 |  | 0.93 | - |
| Heavy | 0 | 30 | 0 |  | 30 | 0 | 0 | 0 |  | 0 | 30 | 0 | 0 |  | 30 | - |
| Heavy \% | 0\% | 3.3\% | 0\% |  | 3.2\% | 0\% | 0\% | 0\% |  | 0\% | 2.8\% | 0\% | 0\% |  | 2.8\% | - |
| Lights | 7 | 889 | 0 |  | 896 | 3 | 3 | 0 |  | 6 | 1050 | 5 | 0 |  | 1055 | - |
| Lights \% | 100\% | 96.7\% | 0\% |  | 96.8\% | 100\% | 100\% | 0\% |  | 100\% | 97.2\% | 100\% | 0\% |  | 97.2\% | - |
| Single-Unit Trucks | 0 | 15 | 0 |  | 15 | 0 | 0 | 0 |  | 0 | 12 | 0 | 0 |  | 12 | - |
| Single-Unit Trucks \% | 0\% | 1.6\% | 0\% |  | 1.6\% | 0\% | 0\% | 0\% |  | 0\% | 1.1\% | 0\% | 0\% |  | 1.1\% | - |
| Buses | 0 | 11 | 0 |  | 11 | 0 | 0 | 0 |  | 0 | 13 | 0 | 0 |  | 13 | - |
| Buses \% | 0\% | 1.2\% | 0\% |  | 1.2\% | 0\% | 0\% | 0\% |  | 0\% | 1.2\% | 0\% | 0\% |  | 1.2\% | - |
| Articulated Trucks | 0 | 4 | 0 |  | 4 | 0 | 0 | 0 |  | 0 | 5 | 0 | 0 |  | 5 | - |
| Articulated Trucks \% | 0\% | 0.4\% | 0\% |  | 0.4\% | 0\% | 0\% | 0\% |  | 0\% | 0.5\% | 0\% | 0\% |  | 0.5\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 3 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 100\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 1 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 1 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 05:00 PM - 06:00 PM Weather: Broken Clouds ( $25.35{ }^{\circ} \mathrm{C}$ )

| Start Time | Westbound |  |  |  |  | Northbound |  |  |  |  |  | Eastbound |  |  |  | Int. Total (15 min) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | UTurn | Peds | Approach Total | Left | Right | UTurn | Peds | Approach Total | Thru | Right | UTurn | Peds | Approach Total |  |
| 17:00:00 | 1 | 433 | 0 | 0 | 434 | 0 | 1 | 0 | 3 | 1 | 333 | 0 | 0 | 0 | 333 | 768 |
| 17:15:00 | 1 | 459 | 0 | 0 | 460 | 0 | 4 | 0 | 7 | 4 | 345 | 1 | 0 | 0 | 346 | 810 |
| 17:30:00 | 3 | 482 | 0 | 0 | 485 | 0 | 2 | 0 | 0 | 2 | 399 | 6 | 0 | 0 | 405 | 892 |
| 17:45:00 | 0 | 453 | 0 | 0 | 453 | 0 | 2 | 0 | 4 | 2 | 375 | 3 | 0 | 0 | 378 | 833 |
| Grand Total | 5 | 1827 | 0 | 0 | 1832 | 0 | 9 | 0 | 14 | 9 | 1452 | 10 | 0 | 0 | 1462 | 3303 |
| Approach\% | 0.3\% | 99.7\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | 99.3\% | 0.7\% | 0\% |  | - | - |
| Totals \% | 0.2\% | 55.3\% | 0\% |  | 55.5\% | 0\% | 0.3\% | 0\% |  | 0.3\% | 44\% | 0.3\% | 0\% |  | 44.3\% | - |
| PHF | 0.42 | 0.95 | 0 |  | 0.94 | 0 | 0.56 | 0 |  | 0.56 | 0.91 | 0.42 | 0 |  | 0.9 | - |
| Heavy | 0 | 13 | 0 |  | 13 | 0 | 0 | 0 |  | 0 | 24 | 0 | 0 |  | 24 | - |
| Heavy \% | 0\% | 0.7\% | 0\% |  | 0.7\% | 0\% | 0\% | 0\% |  | 0\% | 1.7\% | 0\% | 0\% |  | 1.6\% | - |
| Lights | 5 | 1814 | 0 |  | 1819 | 0 | 9 | 0 |  | 9 | 1428 | 10 | 0 |  | 1438 | - |
| Lights \% | 100\% | 99.3\% | 0\% |  | 99.3\% | 0\% | 100\% | 0\% |  | 100\% | 98.3\% | 100\% | 0\% |  | 98.4\% | - |
| Single-Unit Trucks | 0 | 4 | 0 |  | 4 | 0 | 0 | 0 |  | 0 | 8 | 0 | 0 |  | 8 | - |
| Single-Unit Trucks \% | 0\% | 0.2\% | 0\% |  | 0.2\% | 0\% | 0\% | 0\% |  | 0\% | 0.6\% | 0\% | 0\% |  | 0.5\% | - |
| Buses | 0 | 7 | 0 |  | 7 | 0 | 0 | 0 |  | 0 | 13 | 0 | 0 |  | 13 | - |
| Buses \% | 0\% | 0.4\% | 0\% |  | 0.4\% | 0\% | 0\% | 0\% |  | 0\% | 0.9\% | 0\% | 0\% |  | 0.9\% | - |
| Articulated Trucks | 0 | 2 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | 3 | 0 | 0 |  | 3 | - |
| Articulated Trucks \% | 0\% | 0.1\% | 0\% |  | 0.1\% | 0\% | 0\% | 0\% |  | 0\% | 0.2\% | 0\% | 0\% |  | 0.2\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 14 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 100\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 08:00 AM - 09:00 AM Weather: Mist $\left(13.18{ }^{\circ} \mathrm{C}\right)$


Peak Hour: 12:00 PM - 01:00 PM Weather: Broken Clouds ( $23.38^{\circ} \mathrm{C}$ )


Peak Hour: 05:00 PM - 06:00 PM Weather: Broken Clouds ( $25.35{ }^{\circ} \mathrm{C}$ )


Turning Movement Count (25. BRITANNIA RD \& EARL ST) CustID: 00305224 MioID:

| Start Time | Westbound |  |  |  |  | Northbound |  |  |  |  | Eastbound |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | UTurn | Peds | Approach Total | Left | Right | UTurn | Peds | Approach Total | Thru | Right | UTurn | Peds | Approach Total |  |
| 07:00:00 | 1 | 150 | 1 | 0 | 152 | 0 | 3 | 0 | 0 | 3 | 424 | 0 | 0 | 0 | 424 | 579 |
| 07:15:00 | 2 | 160 | 0 | 0 | 162 | 0 | 4 | 0 | 1 | 4 | 476 | 0 | 0 | 0 | 476 | 642 |
| 07:30:00 | 2 | 200 | 0 | 0 | 202 | 1 | 6 | 0 | 1 | 7 | 524 | 1 | 0 | 0 | 525 | 734 |
| 07:45:00 | 1 | 251 | 0 | 0 | 252 | 0 | 4 | 0 | 0 | 4 | 448 | 0 | 0 | 0 | 448 | 704 |
| Hourly | 6 | 761 | 1 | 0 | 768 | 1 | 17 | 0 | 2 | 18 | 1872 | 1 | 0 | 0 | 1873 | 2659 |
| 08:00:00 | 0 | 257 | 0 | 0 | 257 | 0 | 3 | 0 | 4 | 3 | 488 | 0 | 0 | 0 | 488 | 748 |
| 08:15:00 | 1 | 265 | 0 | 0 | 266 | 0 | 7 | 0 | 2 | 7 | 485 | 0 | 0 | 0 | 485 | 758 |
| 08:30:00 | 1 | 251 | 0 | 0 | 252 | 0 | 5 | 0 | 1 | 5 | 461 | 0 | 0 | 0 | 461 | 718 |
| 08:45:00 | 1 | 256 | 0 | 0 | 257 | 2 | 3 | 0 | 0 | 5 | 510 | 2 | 0 | 0 | 512 | 774 |
| Hourly | 3 | 1029 | 0 | 0 | 1032 | 2 | 18 | 0 | 7 | 20 | 1944 | 2 | 0 | 0 | 1946 | 2998 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00:00 | 0 | 159 | 0 | 0 | 159 | 0 | 3 | 0 | 3 | 3 | 210 | 0 | 0 | 1 | 210 | 372 |
| 11:15:00 | 3 | 210 | 0 | 0 | 213 | 0 | 4 | 0 | 0 | 4 | 247 | 0 | 0 | 0 | 247 | 464 |
| 11:30:00 | 0 | 212 | 0 | 0 | 212 | 1 | 2 | 0 | 1 | 3 | 213 | 0 | 0 | 0 | 213 | 428 |
| 11:45:00 | 2 | 231 | 0 | 0 | 233 | 0 | 2 | 0 | 0 | 2 | 242 | 2 | 1 | 0 | 245 | 480 |
| Hourly | 5 | 812 | 0 | 0 | 817 | 1 | 11 | 0 | 4 | 12 | 912 | 2 | 1 | 1 | 915 | 1744 |
| 12:00:00 | 2 | 218 | 0 | 0 | 220 | 0 | 6 | 0 | 3 | 6 | 256 | 0 | 1 | 0 | 257 | 483 |
| 12:15:00 | 0 | 206 | 0 | 0 | 206 | 1 | 1 | 0 | 3 | 2 | 248 | 2 | 0 | 0 | 250 | 458 |
| 12:30:00 | 0 | 236 | 0 | 0 | 236 | 0 | 1 | 0 | 1 | 1 | 225 | 0 | 0 | 0 | 225 | 462 |
| 12:45:00 | 3 | 283 | 0 | 0 | 286 | 0 | 1 | 0 | 1 | 1 | 253 | 1 | 0 | 0 | 254 | 541 |
| Hourly | 5 | 943 | 0 | 0 | 948 | 1 | 9 | 0 | 8 | 10 | 982 | 3 | 1 | 0 | 986 | 1944 |
| 13:00:00 | 2 | 216 | 0 | 0 | 218 | 1 | 3 | 0 | 1 | 4 | 217 | 0 | 0 | 0 | 217 | 439 |
| 13:15:00 | 2 | 273 | 0 | 0 | 275 | 0 | 2 | 0 | 2 | 2 | 233 | 0 | 0 | 0 | 233 | 510 |
| 13:30:00 | 1 | 233 | 0 | 0 | 234 | 0 | 4 | 0 | 0 | 4 | 225 | 0 | 1 | 0 | 226 | 464 |
| 13:45:00 | 1 | 296 | 0 | 0 | 297 | 0 | 3 | 0 | 1 | 3 | 260 | 0 | 0 | 0 | 260 | 560 |

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| Hourly | 6 | 1018 | 0 | 0 | 1024 | 1 | 12 | 0 | 4 | 13 | 935 | 0 | 1 | 0 | 936 | 1973 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15:00:00 | 1 | 341 | 0 | 0 | 342 | 1 | 1 | 0 | 0 | 2 | 274 | 0 | 0 | 0 | 274 | 618 |
| 15:15:00 | 6 | 315 | 0 | 0 | 321 | 0 | 4 | 0 | 0 | 4 | 258 | 1 | 0 | 0 | 259 | 584 |
| 15:30:00 | 2 | 378 | 0 | 0 | 380 | 0 | 4 | 0 | 7 | 4 | 259 | 1 | 1 | 0 | 261 | 645 |
| 15:45:00 | 2 | 367 | 0 | 0 | 369 | 0 | 2 | 0 | 1 | 2 | 281 | 3 | 0 | 0 | 284 | 655 |
| Hourly | 11 | 1401 | 0 | 0 | 1412 | 1 | 11 | 0 | 8 | 12 | 1072 | 5 | 1 | 0 | 1078 | 2502 |
| 16:00:00 | 7 | 392 | 0 | 0 | 399 | 1 | 9 | 0 | 2 | 10 | 291 | 1 | 0 | 0 | 292 | 701 |
| 16:15:00 | 3 | 383 | 0 | 0 | 386 | 1 | 3 | 0 | 1 | 4 | 269 | 0 | 0 | 0 | 269 | 659 |
| 16:30:00 | 2 | 342 | 1 | 0 | 345 | 0 | 2 | 0 | 6 | 2 | 305 | 0 | 0 | 0 | 305 | 652 |
| 16:45:00 | 0 | 370 | 0 | 0 | 370 | 0 | 6 | 0 | 2 | 6 | 293 | 1 | 0 | 0 | 294 | 670 |
| Hourly | 12 | 1487 | 1 | 0 | 1500 | 2 | 20 | 0 | 11 | 22 | 1158 | 2 | 0 | 0 | 1160 | 2682 |
| 17:00:00 | 1 | 357 | 0 | 0 | 358 | 0 | 7 | 0 | 0 | 7 | 351 | 0 | 0 | 0 | 351 | 716 |
| 17:15:00 | 0 | 336 | 0 | 0 | 336 | 0 | 4 | 0 | 1 | 4 | 343 | 3 | 0 | 0 | 346 | 686 |
| 17:30:00 | 1 | 383 | 0 | 0 | 384 | 0 | 2 | 0 | 0 | 2 | 384 | 1 | 0 | 0 | 385 | 771 |
| 17:45:00 | 3 | 363 | 0 | 0 | 366 | 0 | 7 | 0 | 4 | 7 | 378 | 3 | 0 | 0 | 381 | 754 |
| Hourly | 5 | 1439 | 0 | 0 | 1444 | 0 | 20 | 0 | 5 | 20 | 1456 | 7 | 0 | 0 | 1463 | 2927 |
| Grand Total | 53 | 8890 | 2 | 0 | 8945 | 9 | 118 | 0 | 49 | 127 | 10331 | 22 | 4 | 1 | 10357 | 19429 |
| Approach\% | 0.6\% | 99.4\% | 0\% |  | - | 7.1\% | 92.9\% | 0\% |  | - | 99.7\% | 0.2\% | 0\% |  | - | - |
| Totals \% | 0.3\% | 45.8\% | 0\% |  | 46\% | 0\% | 0.6\% | 0\% |  | 0.7\% | 53.2\% | 0.1\% | 0\% |  | 53.3\% | - |
| Heavy | 4 | 294 | 0 |  | - | 1 | 6 | 0 |  | - | 269 | 1 | 0 |  | - | - |
| Heavy \% | 7.5\% | 3.3\% | 0\% |  | - | 11.1\% | 5.1\% | 0\% |  | - | 2.6\% | 4.5\% | 0\% |  | - | - |
| Bicycles | 8 | 4 | 0 |  | - | 0 | 4 | 0 |  | - | 7 | 0 | 0 |  | - | - |
| Bicycle \% | 15.1\% | 0\% | 0\% |  | - | 0\% | 3.4\% | 0\% |  | - | 0.1\% | 0\% | 0\% |  | - | - |

## Peak Hour: 08:00 AM - 09:00 AM Weather: Moderate Rain ( $15.36^{\circ} \mathrm{C}$ )

| Start Time | Westbound |  |  |  |  | Northbound |  |  |  |  | Eastbound |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | UTurn | Peds | Approach Total | Left | Right | UTurn | Peds | Approach Total | Thru | Right | UTurn | Peds | Approach Total |  |
| 08:00:00 | 0 | 257 | 0 | 0 | 257 | 0 | 3 | 0 | 4 | 3 | 488 | 0 | 0 | 0 | 488 | 748 |
| 08:15:00 | 1 | 265 | 0 | 0 | 266 | 0 | 7 | 0 | 2 | 7 | 485 | 0 | 0 | 0 | 485 | 758 |
| 08:30:00 | 1 | 251 | 0 | 0 | 252 | 0 | 5 | 0 | 1 | 5 | 461 | 0 | 0 | 0 | 461 | 718 |
| 08:45:00 | 1 | 256 | 0 | 0 | 257 | 2 | 3 | 0 | 0 | 5 | 510 | 2 | 0 | 0 | 512 | 774 |
| Grand Total | 3 | 1029 | 0 | 0 | 1032 | 2 | 18 | 0 | 7 | 20 | 1944 | 2 | 0 | 0 | 1946 | 2998 |
| Approach\% | 0.3\% | 99.7\% | 0\% |  | - | 10\% | 90\% | 0\% |  | - | 99.9\% | 0.1\% | 0\% |  | - | - |
| Totals \% | 0.1\% | 34.3\% | 0\% |  | 34.4\% | 0.1\% | 0.6\% | 0\% |  | 0.7\% | 64.8\% | 0.1\% | 0\% |  | 64.9\% | - |
| PHF | 0.75 | 0.97 | 0 |  | 0.97 | 0.25 | 0.64 | 0 |  | 0.71 | 0.95 | 0.25 | 0 |  | 0.95 | - |
| Heavy | 2 | 47 | 0 |  | 49 | 0 | 1 | 0 |  | 1 | 46 | 0 | 0 |  | 46 | - |
| Heavy \% | 66.7\% | 4.6\% | 0\% |  | 4.7\% | 0\% | 5.6\% | 0\% |  | 5\% | 2.4\% | 0\% | 0\% |  | 2.4\% | - |
| Lights | 1 | 982 | 0 |  | 983 | 2 | 17 | 0 |  | 19 | 1898 | 2 | 0 |  | 1900 | - |
| Lights \% | 33.3\% | 95.4\% | 0\% |  | 95.3\% | 100\% | 94.4\% | 0\% |  | 95\% | 97.6\% | 100\% | 0\% |  | 97.6\% | - |
| Single-Unit Trucks | 0 | 10 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | 16 | 0 | 0 |  | 16 | - |
| Single-Unit Trucks \% | 0\% | 1\% | 0\% |  | 1\% | 0\% | 0\% | 0\% |  | 0\% | 0.8\% | 0\% | 0\% |  | 0.8\% | - |
| Buses | 2 | 35 | 0 |  | 37 | 0 | 1 | 0 |  | 1 | 28 | 0 | 0 |  | 28 | - |
| Buses \% | 66.7\% | 3.4\% | 0\% |  | 3.6\% | 0\% | 5.6\% | 0\% |  | 5\% | 1.4\% | 0\% | 0\% |  | 1.4\% | - |
| Articulated Trucks | 0 | 2 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | 2 | 0 | 0 |  | 2 | - |
| Articulated Trucks \% | 0\% | 0.2\% | 0\% |  | 0.2\% | 0\% | 0\% | 0\% |  | 0\% | 0.1\% | 0\% | 0\% |  | 0.1\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 7 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 100\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 1 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 1 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |


| Start Time | Peak Hour: 01:00 PM - 02:00 PM |  |  |  |  |  |  | Weather: Broken Clouds (16.94 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  | Int. Total (15 min) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Westbound |  |  |  | Left | Right | Northbound |  | Approach Total | Thru | Right | Eastbound |  | Approach Total |  |
|  |  | Thru | UTurn | Peds | Approach Total |  |  | UTurn | Peds |  |  |  | UTurn | Peds |  |  |
| 13:00:00 | 2 | 216 | 0 | 0 | 218 | 1 | 3 | 0 | 1 | 4 | 217 | 0 | 0 | 0 | 217 | 439 |
| 13:15:00 | 2 | 273 | 0 | 0 | 275 | 0 | 2 | 0 | 2 | 2 | 233 | 0 | 0 | 0 | 233 | 510 |
| 13:30:00 | 1 | 233 | 0 | 0 | 234 | 0 | 4 | 0 | 0 | 4 | 225 | 0 | 1 | 0 | 226 | 464 |
| 13:45:00 | 1 | 296 | 0 | 0 | 297 | 0 | 3 | 0 | 1 | 3 | 260 | 0 | 0 | 0 | 260 | 560 |
| Grand Total | 6 | 1018 | 0 | 0 | 1024 | 1 | 12 | 0 | 4 | 13 | 935 | 0 | 1 | 0 | 936 | 1973 |
| Approach\% | 0.6\% | 99.4\% | 0\% |  | - | 7.7\% | 92.3\% | 0\% |  | - | 99.9\% | 0\% | 0.1\% |  | - | - |
| Totals \% | 0.3\% | 51.6\% | 0\% |  | 51.9\% | 0.1\% | 0.6\% | 0\% |  | 0.7\% | 47.4\% | 0\% | 0.1\% |  | 47.4\% | - |
| PHF | 0.75 | 0.86 | 0 |  | 0.86 | 0.25 | 0.75 | 0 |  | 0.81 | 0.9 | 0 | 0.25 |  | 0.9 | - |
| Heavy | 0 | 56 | 0 |  | 56 | 0 | 0 | 0 |  | 0 | 35 | 0 | 0 |  | 35 | - |
| Heavy \% | 0\% | 5.5\% | 0\% |  | 5.5\% | 0\% | 0\% | 0\% |  | 0\% | 3.7\% | 0\% | 0\% |  | 3.7\% | - |
| Lights | 6 | 962 | 0 |  | 968 | 1 | 12 | 0 |  | 13 | 900 | 0 | 1 |  | 901 | - |
| Lights \% | 100\% | 94.5\% | 0\% |  | 94.5\% | 100\% | 100\% | 0\% |  | 100\% | 96.3\% | 0\% | 100\% |  | 96.3\% | - |
| Single-Unit Trucks | 0 | 27 | 0 |  | 27 | 0 | 0 | 0 |  | 0 | 23 | 0 | 0 |  | 23 | - |
| Single-Unit Trucks \% | 0\% | 2.7\% | 0\% |  | 2.6\% | 0\% | 0\% | 0\% |  | 0\% | 2.5\% | 0\% | 0\% |  | 2.5\% | - |
| Buses | 0 | 19 | 0 |  | 19 | 0 | 0 | 0 |  | 0 | 11 | 0 | 0 |  | 11 | - |
| Buses \% | 0\% | 1.9\% | 0\% |  | 1.9\% | 0\% | 0\% | 0\% |  | 0\% | 1.2\% | 0\% | 0\% |  | 1.2\% | - |
| Articulated Trucks | 0 | 10 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | 1 | 0 | 0 |  | 1 | - |
| Articulated Trucks \% | 0\% | 1\% | 0\% |  | 1\% | 0\% | 0\% | 0\% |  | 0\% | 0.1\% | 0\% | 0\% |  | 0.1\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 4 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 100\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 1 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 1 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |


| Peak Hour: 05:00 PM - 06:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Westbound |  |  |  |  | Northbound |  |  |  |  | Eastbound |  |  |  |  | Int. Total |
| Sta | Left | Thru | UTurn | Peds | Approach Total | Left | Right | UTurn | Peds | Approach Total | Thru | Right | UTurn | Peds | Approach Total | (15 min) |
| 17:00:00 | 1 | 357 | 0 | 0 | 358 | 0 | 7 | 0 | 0 | 7 | 351 | 0 | 0 | 0 | 351 | 716 |
| 17:15:00 | 0 | 336 | 0 | 0 | 336 | 0 | 4 | 0 | 1 | 4 | 343 | 3 | 0 | 0 | 346 | 686 |
| 17:30:00 | 1 | 383 | 0 | 0 | 384 | 0 | 2 | 0 | 0 | 2 | 384 | 1 | 0 | 0 | 385 | 771 |
| 17:45:00 | 3 | 363 | 0 | 0 | 366 | 0 | 7 | 0 | 4 | 7 | 378 | 3 | 0 | 0 | 381 | 754 |
| Grand Total | 5 | 1439 | 0 | 0 | 1444 | 0 | 20 | 0 | 5 | 20 | 1456 | 7 | 0 | 0 | 1463 | 2927 |
| Approach\% | 0.3\% | 99.7\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | 99.5\% | 0.5\% | 0\% |  | - | - |
| Totals \% | 0.2\% | 49.2\% | 0\% |  | 49.3\% | 0\% | 0.7\% | 0\% |  | 0.7\% | 49.7\% | 0.2\% | 0\% |  | 50\% | - |
| PHF | 0.42 | 0.94 | 0 |  | 0.94 | 0 | 0.71 | 0 |  | 0.71 | 0.95 | 0.58 | 0 |  | 0.95 | - |
| Heavy | 0 | 20 | 0 |  | 20 | 0 | 0 | 0 |  | 0 | 17 | 0 | 0 |  | 17 | - |
| Heavy \% | 0\% | 1.4\% | 0\% |  | 1.4\% | 0\% | 0\% | 0\% |  | 0\% | 1.2\% | 0\% | 0\% |  | 1.2\% | - |
| Lights | 5 | 1419 | 0 |  | 1424 | 0 | 20 | 0 |  | 20 | 1439 | 7 | 0 |  | 1446 | - |
| Lights \% | 100\% | 98.6\% | 0\% |  | 98.6\% | 0\% | 100\% | 0\% |  | 100\% | 98.8\% | 100\% | 0\% |  | 98.8\% | - |
| Single-Unit Trucks | 0 | 5 | 0 |  | 5 | 0 | 0 | 0 |  | 0 | 4 | 0 | 0 |  | 4 | - |
| Single-Unit Trucks \% | 0\% | 0.3\% | 0\% |  | 0.3\% | 0\% | 0\% | 0\% |  | 0\% | 0.3\% | 0\% | 0\% |  | 0.3\% | - |
| Buses | 0 | 11 | 0 |  | 11 | 0 | 0 | 0 |  | 0 | 10 | 0 | 0 |  | 10 | - |
| Buses \% | 0\% | 0.8\% | 0\% |  | 0.8\% | 0\% | 0\% | 0\% |  | 0\% | 0.7\% | 0\% | 0\% |  | 0.7\% | - |
| Articulated Trucks | 0 | 4 | 0 |  | 4 | 0 | 0 | 0 |  | 0 | 3 | 0 | 0 |  | 3 | - |
| Articulated Trucks \% | 0\% | 0.3\% | 0\% |  | 0.3\% | 0\% | 0\% | 0\% |  | 0\% | 0.2\% | 0\% | 0\% |  | 0.2\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 5 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 100\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 2 | 1 | 0 | 0 | - | 0 | 2 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 08:00 AM - 09:00 AM Weather: Moderate Rain (15.36 $\left.{ }^{\circ} \mathrm{C}\right)$



Peak Hour: 01:00 PM - 02:00 PM Weather: Broken Clouds (16.94 ${ }^{\circ} \mathrm{C}$ )


## Peak Hour: 05:00 PM - 06:00 PM Weather: Scattered Clouds (20.41 $\left.{ }^{\circ} \mathrm{C}\right)$



Turning Movement Count (14. BRITANNIA RD \& ELLESBORO DR) CustID: 00305155 MioID: 663715

| Start Time | Southbound ELLESBORO DR |  |  |  |  | Westbound BRITANNIA RD |  |  |  |  |  | Eastbound BRITANNIA RD |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Right | U-Turn | Peds | Approach Total | Thru | Right | U-Turn | Peds | Approach Total | Left | Thru | U-Turn | Peds | Approach Total |  |
| 07:00:00 | 4 | 2 | 0 | 0 | 6 | 139 | 5 | 0 | 0 | 144 | 0 | 362 | 0 | 0 | 362 | 512 |
| 07:15:00 | 9 | 2 | 0 | 0 | 11 | 158 | 10 | 0 | 0 | 168 | 0 | 421 | 0 | 2 | 421 | 600 |
| 07:30:00 | 9 | 10 | 0 | 3 | 19 | 212 | 7 | 0 | 0 | 219 | 2 | 502 | 0 | 0 | 504 | 742 |
| 07:45:00 | 14 | 11 | 0 | 2 | 25 | 268 | 19 | 0 | 0 | 287 | 0 | 476 | 0 | 3 | 476 | 788 |
| Hourly | 36 | 25 | 0 | 5 | 61 | 777 | 41 | 0 | 0 | 818 | 2 | 1761 | 0 | 5 | 1763 | 2642 |
| 08:00:00 | 12 | 6 | 0 | 0 | 18 | 212 | 17 | 0 | 0 | 229 | 6 | 487 | 0 | 1 | 493 | 740 |
| 08:15:00 | 26 | 9 | 0 | 3 | 35 | 266 | 22 | 0 | 1 | 288 | 7 | 448 | 0 | 7 | 455 | 778 |
| 08:30:00 | 13 | 9 | 0 | 1 | 22 | 220 | 6 | 0 | 0 | 226 | 3 | 475 | 0 | 3 | 478 | 726 |
| 08:45:00 | 11 | 5 | 0 | 0 | 16 | 282 | 24 | 0 | 0 | 306 | 13 | 401 | 0 | 1 | 414 | 736 |
| Hourly | 62 | 29 | 0 | 4 | 91 | 980 | 69 | 0 | 1 | 1049 | 29 | 1811 | 0 | 12 | 1840 | 2980 |

***BREAK***

| 11:00:00 | 3 | 4 | 0 | 0 | 7 | 172 | 8 | 0 | 0 | 180 | 5 | 237 | 0 | 0 | 242 | 429 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11:15:00 | 9 | 3 | 0 | 0 | 12 | 199 | 9 | 0 | 0 | 208 | 7 | 240 | 0 | 0 | 247 | 467 |
| 11:30:00 | 6 | 4 | 0 | 1 | 10 | 207 | 12 | 0 | 0 | 219 | 2 | 251 | 0 | 1 | 253 | 482 |
| 11:45:00 | 8 | 5 | 0 | 3 | 13 | 220 | 8 | 0 | 0 | 228 | 2 | 249 | 0 | 0 | 251 | 492 |
| Hourly | 26 | 16 | 0 | 4 | 42 | 798 | 37 | 0 | 0 | 835 | 16 | 977 | 0 | 1 | 993 | 1870 |
| 12:00:00 | 10 | 8 | 0 | 0 | 18 | 239 | 10 | 0 | 1 | 249 | 4 | 231 | 0 | 1 | 235 | 502 |
| 12:15:00 | 13 | 8 | 0 | 0 | 21 | 213 | 5 | 0 | 0 | 218 | 7 | 240 | 0 | 0 | 247 | 486 |
| 12:30:00 | 11 | 5 | 0 | 0 | 16 | 218 | 13 | 0 | 1 | 231 | 3 | 251 | 0 | 0 | 254 | 501 |
| 12:45:00 | 12 | 3 | 0 | 4 | 15 | 241 | 13 | 0 | 0 | 254 | 5 | 228 | 0 | 1 | 233 | 502 |
| Hourly | 46 | 24 | 0 | 4 | 70 | 911 | 41 | 0 | 2 | 952 | 19 | 950 | 0 | 2 | 969 | 1991 |
| 13:00:00 | 10 | 7 | 0 | 1 | 17 | 263 | 10 | 0 | 0 | 273 | 1 | 215 | 0 | 0 | 216 | 506 |
| 13:15:00 | 13 | 3 | 0 | 1 | 16 | 244 | 8 | 0 | 0 | 252 | 6 | 204 | 0 | 0 | 210 | 478 |
| 13:30:00 | 11 | 6 | 0 | 1 | 17 | 244 | 16 | 0 | 0 | 260 | 4 | 218 | 0 | 1 | 222 | 499 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | PEL19 |


| 13:45:00 | 8 | 5 | 0 | 0 | 13 | 279 | 7 | 0 | 0 | 286 | 5 | 234 | 0 | 0 | 239 | 538 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Hourly | 42 | 21 | 0 | 3 | 63 | 1030 | 41 | 0 | 0 | 1071 | 16 | 871 | 0 | 1 | 887 | 2021 |


| 15:00:00 | 3 | 4 | 0 | 3 | 7 | 341 | 22 | 0 | 0 | 363 | 7 | 273 | 0 | 4 | 280 | 650 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15:15:00 | 17 | 8 | 0 | 3 | 25 | 358 | 22 | 0 | 2 | 380 | 10 | 261 | 0 | 3 | 271 | 676 |
| 15:30:00 | 18 | 16 | 0 | 0 | 34 | 339 | 11 | 0 | 0 | 350 | 6 | 294 | 0 | 2 | 300 | 684 |
| 15:45:00 | 8 | 7 | 0 | 1 | 15 | 390 | 19 | 0 | 0 | 409 | 4 | 267 | 0 | 0 | 271 | 695 |
| Hourly | 46 | 35 | 0 | 7 | 81 | 1428 | 74 | 0 | 2 | 1502 | 27 | 1095 | 0 | 9 | 1122 | 2705 |
| 16:00:00 | 21 | 5 | 0 | 3 | 26 | 397 | 16 | 0 | 1 | 413 | 9 | 246 | 0 | 0 | 255 | 694 |
| 16:15:00 | 6 | 8 | 0 | 1 | 14 | 390 | 19 | 0 | 0 | 409 | 12 | 313 | 0 | 0 | 325 | 748 |
| 16:30:00 | 14 | 3 | 0 | 1 | 17 | 377 | 11 | 0 | 2 | 388 | 8 | 301 | 0 | 0 | 309 | 714 |
| 16:45:00 | 26 | 6 | 0 | 3 | 32 | 373 | 10 | 0 | 0 | 383 | 2 | 337 | 0 | 1 | 339 | 754 |
| Hourly | 67 | 22 | 0 | 8 | 89 | 1537 | 56 | 0 | 3 | 1593 | 31 | 1197 | 0 | 1 | 1228 | 2910 |
| 17:00:00 | 26 | 3 | 0 | 1 | 29 | 361 | 16 | 0 | 0 | 377 | 5 | 335 | 0 | 1 | 340 | 746 |
| 17:15:00 | 36 | 10 | 0 | 0 | 46 | 364 | 24 | 0 | 0 | 388 | 6 | 323 | 0 | 1 | 329 | 763 |
| 17:30:00 | 22 | 13 | 0 | 1 | 35 | 367 | 21 | 0 | 0 | 388 | 2 | 372 | 0 | 0 | 374 | 797 |
| 17:45:00 | 16 | 9 | 0 | 3 | 25 | 324 | 14 | 0 | 0 | 338 | 4 | 321 | 0 | 3 | 325 | 688 |
| Hourly | 100 | 35 | 0 | 5 | 135 | 1416 | 75 | 0 | 0 | 1491 | 17 | 1351 | 0 | 5 | 1368 | 2994 |
| Grand Total | 425 | 207 | 0 | 40 | 632 | 8877 | 434 | 0 | 8 | 9311 | 157 | 10013 | 0 | 36 | 10170 | 20113 |
| Approach\% | 67.2\% | 32.8\% | 0\% |  | - | 95.3\% | 4.7\% | 0\% |  | - | 1.5\% | 98.5\% | 0\% |  | - | - |
| Totals \% | 2.1\% | 1\% | 0\% |  | 3.1\% | 44.1\% | 2.2\% | 0\% |  | 46.3\% | 0.8\% | 49.8\% | 0\% |  | 50.6\% | - |
| Heavy | 6 | 15 | 0 |  | - | 296 | 23 | 0 |  | - | 11 | 259 | 0 |  | - | - |
| Heavy \% | 1.4\% | 7.2\% | 0\% |  | - | 3.3\% | 5.3\% | 0\% |  | - | 7\% | 2.6\% | 0\% |  | - | - |
| Bicycles | 0 | 2 | 0 |  | - | 1 | 2 | 0 |  | - | 0 | 1 | 0 |  | - | - |
| Bicycle \% | 0\% | 1\% | 0\% |  | - | 0\% | 0.5\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - |

## Peak Hour: 08:00 AM - 09:00 AM Weather: Fog $\left(11.77^{\circ} \mathrm{C}\right)$

| Start Time | Southbound ELLESBORO DR |  |  |  |  | Westbound BRITANNIA RD |  |  |  |  | Eastbound BRITANNIA RD |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Right | U-Turn | Peds | Approach Total | Thru | Right | U-Turn | Peds | Approach Total | Left | Thru | U-Turn | Peds | Approach Total |  |
| 08:00:00 | 12 | 6 | 0 | 0 | 18 | 212 | 17 | 0 | 0 | 229 | 6 | 487 | 0 | 1 | 493 | 740 |
| 08:15:00 | 26 | 9 | 0 | 3 | 35 | 266 | 22 | 0 | 1 | 288 | 7 | 448 | 0 | 7 | 455 | 778 |
| 08:30:00 | 13 | 9 | 0 | 1 | 22 | 220 | 6 | 0 | 0 | 226 | 3 | 475 | 0 | 3 | 478 | 726 |
| 08:45:00 | 11 | 5 | 0 | 0 | 16 | 282 | 24 | 0 | 0 | 306 | 13 | 401 | 0 | 1 | 414 | 736 |
| Grand Total | 62 | 29 | 0 | 4 | 91 | 980 | 69 | 0 | 1 | 1049 | 29 | 1811 | 0 | 12 | 1840 | 2980 |
| Approach\% | 68.1\% | 31.9\% | 0\% |  | - | 93.4\% | 6.6\% | 0\% |  | - | 1.6\% | 98.4\% | 0\% |  | - | - |
| Totals \% | 2.1\% | 1\% | 0\% |  | 3.1\% | 32.9\% | 2.3\% | 0\% |  | 35.2\% | 1\% | 60.8\% | 0\% |  | 61.7\% | - |
| PHF | 0.6 | 0.81 | 0 |  | 0.65 | 0.87 | 0.72 | 0 |  | 0.86 | 0.56 | 0.93 | 0 |  | 0.93 | - |
| Heavy | 0 | 2 | 0 |  | 2 | 55 | 4 | 0 |  | 59 | 1 | 37 | 0 |  | 38 | - |
| Heavy \% | 0\% | 6.9\% | 0\% |  | 2.2\% | 5.6\% | 5.8\% | 0\% |  | 5.6\% | 3.4\% | 2\% | 0\% |  | 2.1\% | - |
| Lights | 62 | 27 | 0 |  | 89 | 925 | 65 | 0 |  | 990 | 28 | 1774 | 0 |  | 1802 | - |
| Lights \% | 100\% | 93.1\% | 0\% |  | 97.8\% | 94.4\% | 94.2\% | 0\% |  | 94.4\% | 96.6\% | 98\% | 0\% |  | 97.9\% | - |
| Single-Unit Trucks | 0 | 0 | 0 |  | 0 | 17 | 1 | 0 |  | 18 | 0 | 14 | 0 |  | 14 | - |
| Single-Unit Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 1.7\% | 1.4\% | 0\% |  | 1.7\% | 0\% | 0.8\% | 0\% |  | 0.8\% | - |
| Buses | 0 | 2 | 0 |  | 2 | 30 | 3 | 0 |  | 33 | 1 | 20 | 0 |  | 21 | - |
| Buses \% | 0\% | 6.9\% | 0\% |  | 2.2\% | 3.1\% | 4.3\% | 0\% |  | 3.1\% | 3.4\% | 1.1\% | 0\% |  | 1.1\% | - |
| Articulated Trucks | 0 | 0 | 0 |  | 0 | 8 | 0 | 0 |  | 8 | 0 | 3 | 0 |  | 3 | - |
| Articulated Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 0.8\% | 0\% | 0\% |  | 0.8\% | 0\% | 0.2\% | 0\% |  | 0.2\% | - |
| Pedestrians | - | - | - | 4 | - | - | - | - | 1 | - | - | - | - | 12 | - | - |
| Pedestrians\% | - | - | - | 23.5\% |  | - | - | - | 5.9\% |  | - | - | - | 70.6\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 01:00 PM - 02:00 PM Weather: Haze ( $17.96{ }^{\circ} \mathrm{C}$ )

| Start Time | Southbound ELLESBORO DR |  |  |  |  | Westbound BRITANNIA RD |  |  |  |  | Eastbound BRITANNIA RD |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Right | U-Turn | Peds | Approach Total | Thru | Right | U-Turn | Peds | Approach Total | Left | Thru | U-Turn | Peds | Approach Total |  |
| 13:00:00 | 10 | 7 | 0 | 1 | 17 | 263 | 10 | 0 | 0 | 273 | 1 | 215 | 0 | 0 | 216 | 506 |
| 13:15:00 | 13 | 3 | 0 | 1 | 16 | 244 | 8 | 0 | 0 | 252 | 6 | 204 | 0 | 0 | 210 | 478 |
| 13:30:00 | 11 | 6 | 0 | 1 | 17 | 244 | 16 | 0 | 0 | 260 | 4 | 218 | 0 | 1 | 222 | 499 |
| 13:45:00 | 8 | 5 | 0 | 0 | 13 | 279 | 7 | 0 | 0 | 286 | 5 | 234 | 0 | 0 | 239 | 538 |
| Grand Total | 42 | 21 | 0 | 3 | 63 | 1030 | 41 | 0 | 0 | 1071 | 16 | 871 | 0 | 1 | 887 | 2021 |
| Approach\% | 66.7\% | 33.3\% | 0\% |  | - | 96.2\% | 3.8\% | 0\% |  | - | 1.8\% | 98.2\% | 0\% |  | - | - |
| Totals \% | 2.1\% | 1\% | 0\% |  | 3.1\% | 51\% | 2\% | 0\% |  | 53\% | 0.8\% | 43.1\% | 0\% |  | 43.9\% | - |
| PHF | 0.81 | 0.75 | 0 |  | 0.93 | 0.92 | 0.64 | 0 |  | 0.94 | 0.67 | 0.93 | 0 |  | 0.93 | - |
| Heavy | 0 | 1 | 0 |  | 1 | 38 | 2 | 0 |  | 40 | 0 | 26 | 0 |  | 26 | - |
| Heavy \% | 0\% | 4.8\% | 0\% |  | 1.6\% | 3.7\% | 4.9\% | 0\% |  | 3.7\% | 0\% | 3\% | 0\% |  | 2.9\% | - |
| Lights | 42 | 20 | 0 |  | 62 | 992 | 39 | 0 |  | 1031 | 16 | 845 | 0 |  | 861 | - |
| Lights \% | 100\% | 95.2\% | 0\% |  | 98.4\% | 96.3\% | 95.1\% | 0\% |  | 96.3\% | 100\% | 97\% | 0\% |  | 97.1\% | - |
| Single-Unit Trucks | 0 | 1 | 0 |  | 1 | 19 | 2 | 0 |  | 21 | 0 | 11 | 0 |  | 11 | - |
| Single-Unit Trucks \% | 0\% | 4.8\% | 0\% |  | 1.6\% | 1.8\% | 4.9\% | 0\% |  | 2\% | 0\% | 1.3\% | 0\% |  | 1.2\% | - |
| Buses | 0 | 0 | 0 |  | 0 | 14 | 0 | 0 |  | 14 | 0 | 13 | 0 |  | 13 | - |
| Buses \% | 0\% | 0\% | 0\% |  | 0\% | 1.4\% | 0\% | 0\% |  | 1.3\% | 0\% | 1.5\% | 0\% |  | 1.5\% | - |
| Articulated Trucks | 0 | 0 | 0 |  | 0 | 5 | 0 | 0 |  | 5 | 0 | 2 | 0 |  | 2 | - |
| Articulated Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 0.5\% | 0\% | 0\% |  | 0.5\% | 0\% | 0.2\% | 0\% |  | 0.2\% | - |
| Pedestrians | - | - | - | 3 | - | - | - | - | 0 | - | - | - | - | 1 | - | - |
| Pedestrians\% | - | - | - | 75\% |  | - | - | - | 0\% |  | - | - | - | 25\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 2 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |



Peak Hour: 08:00 AM-09:00 AM Weather: Fog $\left(11.77{ }^{\circ} \mathrm{C}\right)$


## Peak Hour: 01:00 PM-02:00 PM Weather: Haze (17.96 $\left.{ }^{\circ} \mathrm{C}\right)$



Peak Hour: 05:00 PM - 06:00 PM Weather: Broken Clouds (21.25 ${ }^{\circ} \mathrm{C}$ )


## Turning Movement Count (3. BRITANNIA RD \& QUEEN ST) CustID: 00305449 MioID:

| Start Time | Southbound |  |  |  |  |  |  | Westbound |  |  |  |  | Northbound |  |  |  |  |  | Eastbound |  |  |  |  |  | Int. Total (15 min) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total |  |
| 07:00:00 | 45 | 37 | 29 | 0 | 1 | 111 | 13 | 96 | 29 | 0 | 0 | 138 | 12 | 36 | 14 | 0 | 1 | 62 | 28 | 388 | 13 | 0 | 1 | 429 | 740 |
| 07:15:00 | 59 | 48 | 31 | 0 | 0 | 138 | 19 | 97 | 38 | 0 | 2 | 154 | 11 | 73 | 23 | 0 | 6 | 107 | 30 | 353 | 11 | 0 | 0 | 394 | 793 |
| 07:30:00 | 37 | 49 | 38 | 0 | 2 | 124 | 16 | 134 | 38 | 0 | 3 | 188 | 8 | 61 | 24 | 0 | 1 | 93 | 24 | 454 | 15 | 0 | 2 | 493 | 898 |
| 07:45:00 | 36 | 64 | 44 | 0 | 5 | 144 | 24 | 217 | 54 | 0 | 2 | 295 | 20 | 111 | 37 | 0 | 1 | 168 | 36 | 360 | 15 | 0 | 5 | 411 | 1018 |
| Hourly | 177 | 198 | 142 | 0 | 8 | 517 | 72 | 544 | 159 | 0 | 7 | 775 | 51 | 281 | 98 | 0 | 9 | 430 | 118 | 1555 | 54 | 0 | 8 | 1727 | 3449 |
| 08:00:00 | 31 | 67 | 46 | 0 | 7 | 144 | 23 | 151 | 59 | 0 | 4 | 233 | 25 | 92 | 29 | 0 | 10 | 146 | 56 | 401 | 27 | 0 | 5 | 484 | 1007 |
| 08:15:00 | 24 | 67 | 37 | 0 | 1 | 128 | 22 | 163 | 88 | 0 | 10 | 273 | 21 | 104 | 41 | 0 | 11 | 166 | 51 | 387 | 25 | 0 | 1 | 463 | 1030 |
| 08:30:00 | 43 | 81 | 28 | 0 | 3 | 152 | 24 | 138 | 86 | 0 | 1 | 248 | 22 | 150 | 30 | 0 | 2 | 202 | 60 | 346 | 20 | 0 | 5 | 426 | 1028 |
| 08:45:00 | 44 | 70 | 28 | 0 | 3 | 142 | 11 | 154 | 93 | 0 | 3 | 258 | 27 | 124 | 23 | 0 | 1 | 174 | 48 | 402 | 28 | 0 | 3 | 478 | 1052 |
| Hourly | 142 | 285 | 139 | 0 | 14 | 566 | 80 | 606 | 326 | 0 | 18 | 1012 | 95 | 470 | 123 | 0 | 24 | 688 | 215 | 1536 | 100 | 0 | 14 | 1851 | 4117 |


| 11:00:00 | 33 | 55 | 23 | 0 | 6 | 111 | 25 | 130 | 26 | 0 | 2 | 181 | 24 | 59 | 26 | 0 | 1 | 109 | 38 | 153 | 27 | 0 | 6 | 218 | 619 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11:15:00 | 27 | 59 | 26 | 0 | 2 | 112 | 18 | 118 | 29 | 0 | 0 | 165 | 26 | 57 | 28 | 0 | 1 | 111 | 25 | 190 | 31 | 0 | 2 | 246 | 634 |
| 11:30:00 | 24 | 47 | 16 | 0 | 1 | 87 | 17 | 120 | 22 | 0 | 0 | 159 | 29 | 68 | 28 | 0 | 0 | 125 | 24 | 181 | 33 | 0 | 1 | 238 | 609 |
| 11:45:00 | 49 | 107 | 39 | 0 | 1 | 195 | 37 | 167 | 39 | 0 | 0 | 243 | 37 | 64 | 35 | 0 | 0 | 136 | 41 | 162 | 30 | 0 | 2 | 233 | 807 |
| Hourly | 133 | 268 | 104 | 0 | 10 | 505 | 97 | 535 | 116 | 0 | 2 | 748 | 116 | 248 | 117 | 0 | 2 | 481 | 128 | 686 | 121 | 0 | 11 | 935 | 2669 |
| 12:00:00 | 42 | 68 | 41 | 0 | 3 | 151 | 27 | 151 | 25 | 0 | 0 | 203 | 28 | 46 | 32 | 0 | 4 | 106 | 35 | 218 | 34 | 0 | 2 | 287 | 747 |
| 12:15:00 | 38 | 73 | 32 | 0 | 3 | 143 | 22 | 144 | 32 | 0 | 0 | 198 | 26 | 64 | 29 | 0 | 0 | 119 | 35 | 167 | 23 | 0 | 3 | 225 | 685 |
| 12:30:00 | 28 | 55 | 34 | 0 | 3 | 117 | 24 | 156 | 30 | 0 | 0 | 210 | 26 | 67 | 28 | 0 | 2 | 121 | 30 | 174 | 28 | 0 | 3 | 232 | 680 |
| 12:45:00 | 47 | 68 | 40 | 0 | 0 | 155 | 23 | 170 | 32 | 0 | 2 | 225 | 35 | 73 | 37 | 0 | 1 | 145 | 44 | 179 | 24 | 0 | 1 | 247 | 772 |
| Hourly | 155 | 264 | 147 | 0 | 9 | 566 | 96 | 621 | 119 | 0 | 2 | 836 | 115 | 250 | 126 | 0 | 7 | 491 | 144 | 738 | 109 | 0 | 9 | 991 | 2884 |
| 13:00:00 | 26 | 58 | 47 | 0 | 1 | 131 | 33 | 160 | 36 | 0 | 4 | 229 | 38 | 81 | 41 | 0 | 3 | 160 | 32 | 140 | 25 | 0 | 2 | 197 | 717 |
| 13:15:00 | 36 | 53 | 32 | 0 | 1 | 121 | 21 | 166 | 23 | 0 | 4 | 210 | 13 | 58 | 34 | 0 | 2 | 105 | 32 | 162 | 26 | 0 | 1 | 220 | 656 |
| 13:30:00 | 38 | 72 | 32 | 0 | 3 | 142 | 28 | 156 | 36 | 0 | 4 | 220 | 34 | 76 | 28 | 0 | 3 | 138 | 28 | 149 | 26 | 0 | 5 | 203 | 703 |
| 13:45:00 | 36 | 62 | 40 | 0 | 5 | 138 | 37 | 174 | 34 | 0 | 2 | 245 | 31 | 75 | 19 | 0 | 2 | 125 | 26 | 137 | 28 | 0 | 3 | 191 | 699 |
| Hourly | 136 | 245 | 151 | 0 | 10 | 532 | 119 | 656 | 129 | 0 | 14 | 904 | 116 | 290 | 122 | 0 | 10 | 528 | 118 | 588 | 105 | 0 | 11 | 811 | 2775 |


| 15:00:00 | 53 | 61 | 48 | 0 | 1 | 162 | 23 | 281 | 52 | 0 | 5 | 356 | 43 | 84 | 34 | 0 | 1 | 161 | 28 | 176 | 21 | 0 | 0 | 225 | 904 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 15:15:00 | 54 | 77 | 63 | 0 | 1 | 194 | 27 | 245 | 27 | 0 | 8 | 299 | 38 | 99 | 35 | 0 | 7 | 172 | 37 | 197 | 31 | 0 | 1 | 265 | 930 |
| 15:30:00 | 54 | 74 | 72 | 0 | 1 | 200 | 35 | 272 | 27 | 0 | 4 | 334 | 42 | 84 | 30 | 0 | 7 | 156 | 35 | 170 | 26 | 0 | 1 | 231 | 921 |
| 15:45:00 | 41 | 73 | 43 | 0 | 0 | 157 | 29 | 295 | 25 | 0 | 9 | 349 | 35 | 66 | 24 | 0 | 4 | 125 | 37 | 193 | 33 | 0 | 0 | 263 | 894 |
| Hourly | 202 | 285 | 226 | 0 | 3 | 713 | 114 | 1093 | 131 | 0 | 26 | 1338 | 158 | 333 | 123 | 0 | 19 | 614 | 137 | 736 | 111 | 0 | 2 | 984 | 3649 |
| Movem | Coun |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 19J3 |

Date: Wed, Oct 02, 2019 Deployment Lead: Patrick Filopoulos

| 16:00:00 | 70 | 113 | 68 | 0 | 0 | 251 | 35 | 296 | 24 | 0 | 4 | 355 | 39 | 78 | 27 | 0 | 2 | 144 | 29 | 182 | 21 | 0 | 0 | 232 | 982 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 16:15:00 | 67 | 99 | 57 | 0 | 1 | 223 | 36 | 335 | 30 | 0 | 8 | 401 | 39 | 87 | 30 | 0 | 6 | 156 | 21 | 193 | 22 | 0 | 1 | 236 | 1016 |
| 16:30:00 | 61 | 104 | 67 | 0 | 3 | 232 | 25 | 308 | 18 | 0 | 4 | 351 | 37 | 66 | 22 | 0 | 3 | 125 | 28 | 203 | 29 | 0 | 1 | 260 | 968 |
| 16:45:00 | 61 | 128 | 77 | 0 | 2 | 266 | 27 | 355 | 19 | 0 | 5 | 401 | 48 | 92 | 25 | 0 | 11 | 165 | 39 | 186 | 25 | 0 | 3 | 250 | 1082 |
| Hourly | 259 | 444 | 269 | 0 | 6 | 972 | 123 | 1294 | 91 | 0 | 21 | 1508 | 163 | 323 | 104 | 0 | 22 | 590 | 117 | 764 | 97 | 0 | 5 | 978 | 4048 |
| 17:00:00 | 71 | 126 | 73 | 0 | 0 | 270 | 16 | 354 | 21 | 0 | 9 | 391 | 46 | 103 | 30 | 0 | 4 | 179 | 30 | 242 | 33 | 0 | 0 | 305 | 1145 |
| 17:15:00 | 86 | 145 | 121 | 0 | 6 | 352 | 30 | 327 | 18 | 0 | 8 | 375 | 39 | 81 | 37 | 0 | 1 | 157 | 29 | 214 | 44 | 0 | 3 | 287 | 1171 |
| 17:30:00 | 65 | 139 | 85 | 0 | 5 | 289 | 43 | 231 | 55 | 0 | 7 | 329 | 39 | 91 | 42 | 0 | 1 | 172 | 39 | 200 | 52 | 0 | 7 | 291 | 1081 |
| 17:45:00 | 57 | 100 | 68 | 0 | 1 | 225 | 49 | 273 | 29 | 0 | 0 | 351 | 40 | 73 | 29 | 0 | 3 | 142 | 49 | 267 | 38 | 0 | 0 | 354 | 1072 |
| Hourly | 279 | 510 | 347 | 0 | 12 | 1136 | 138 | 1185 | 123 | 0 | 24 | 1446 | 164 | 348 | 138 | 0 | 9 | 650 | 147 | 923 | 167 | 0 | 10 | 1237 | 4469 |
| Grand Total | 1483 | 2499 | 1525 | 0 | 72 | 5507 | 839 | 6534 | 1194 | 0 | 114 | 8567 | 978 | 2543 | 951 | 0 | 102 | 4472 | 1124 | 7526 | 864 | 0 | 70 | 9514 | 28060 |


| Approach\% | 26.9\% | 45.4\% | 27.7\% | 0\% | - | 9.8\% | 76.3\% | 13.9\% | 0\% | - | 21.9\% | 56.9\% | 21.3\% | 0\% | - | 11.8\% | 79.1\% | 9.1\% | 0\% | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Totals \% | 5.3\% | 8.9\% | 5.4\% | 0\% | 19.6\% | 3\% | 23.3\% | 4.3\% | 0\% | 30.5\% | 3.5\% | 9.1\% | 3.4\% | 0\% | 15.9\% | 4\% | 26.8\% | 3.1\% | 0\% | 33.9\% |
| Heavy | 35 | 52 | 93 | 0 | - | 24 | 226 | 44 | 0 | - | 26 | 59 | 17 | 0 | - | 34 | 190 | 8 | 0 | - |
| Heavy \% | 2.4\% | 2.1\% | 6.1\% | 0\% | - | 2.9\% | 3.5\% | 3.7\% | 0\% | - | 2.7\% | 2.3\% | 1.8\% | 0\% | - | 3\% | 2.5\% | 0.9\% | 0\% | - |
| Bicycles | 0 | 1 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 2 | 0 | 0 | - | 1 | 0 | 0 | 0 | - |
| Bicycle \% | 0\% | 0\% | 0\% | 0\% | - | 0\% | 0\% | 0\% | 0\% | - | 0\% | 0.1\% | 0\% | 0\% | - | 0.1\% | 0\% | 0\% | 0\% | - |

Peak Hour: 08:00 AM - 09:00 AM Weather: Light Rain (16.39 ${ }^{\circ} \mathrm{C}$ )

| Start Time |  |  |  |  |  |  | Peak Hour: 08:00 AM - 09:00 AM |  |  |  |  |  | Weather: Light Rain (16.39 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Southbound |  |  |  |  |  | Westbound |  |  |  |  |  | Northbound |  |  |  |  |  | Eastbound |  |  |  |  |  | Int. Total ( 15 min ) |
|  | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total |  |
| 08:00:00 | 31 | 67 | 46 | 0 | 7 | 144 | 23 | 151 | 59 | 0 | 4 | 233 | 25 | 92 | 29 | 0 | 10 | 146 | 56 | 401 | 27 | 0 | 5 | 484 | 1007 |
| 08:15:00 | 24 | 67 | 37 | 0 | 1 | 128 | 22 | 163 | 88 | 0 | 10 | 273 | 21 | 104 | 41 | 0 | 11 | 166 | 51 | 387 | 25 | 0 | 1 | 463 | 1030 |
| 08:30:00 | 43 | 81 | 28 | 0 | 3 | 152 | 24 | 138 | 86 | 0 | 1 | 248 | 22 | 150 | 30 | 0 | 2 | 202 | 60 | 346 | 20 | 0 | 5 | 426 | 1028 |
| 08:45:00 | 44 | 70 | 28 | 0 | 3 | 142 | 11 | 154 | 93 | 0 | 3 | 258 | 27 | 124 | 23 | 0 | 1 | 174 | 48 | 402 | 28 | 0 | 3 | 478 | 1052 |
| Grand Total | 142 | 285 | 139 | 0 | 14 | 566 | 80 | 606 | 326 | 0 | 18 | 1012 | 95 | 470 | 123 | 0 | 24 | 688 | 215 | 1536 | 100 | 0 | 14 | 1851 | 4117 |
| Approach\% | 25.1\% | 50.4\% | 24.6\% | 0\% |  | - | 7.9\% | 59.9\% | 32.2\% | 0\% |  | - | 13.8\% | 68.3\% | 17.9\% | 0\% |  | - | 11.6\% | 83\% | 5.4\% | 0\% |  | - | - |
| Totals \% | 3.4\% | 6.9\% | 3.4\% | 0\% |  | 13.7\% | 1.9\% | 14.7\% | 7.9\% | 0\% |  | 24.6\% | 2.3\% | 11.4\% | 3\% | 0\% |  | 16.7\% | 5.2\% | 37.3\% | 2.4\% | 0\% |  | 45\% | - |
| PHF | 0.81 | 0.88 | 0.76 | 0 |  | 0.93 | 0.83 | 0.93 | 0.88 | 0 |  | 0.93 | 0.88 | 0.78 | 0.75 | 0 |  | 0.85 | 0.9 | 0.96 | 0.89 | 0 |  | 0.96 | - |
| Heavy | 9 | 10 | 12 | 0 |  | 31 | 4 | 41 | 12 | 0 |  | 57 | 8 | 9 | 4 | 0 |  | 21 | 4 | 34 | 2 | 0 |  | 40 | - |
| Heavy \% | 6.3\% | 3.5\% | 8.6\% | 0\% |  | 5.5\% | 5\% | 6.8\% | 3.7\% | 0\% |  | 5.6\% | 8.4\% | 1.9\% | 3.3\% | 0\% |  | 3.1\% | 1.9\% | 2.2\% | 2\% | 0\% |  | 2.2\% | - |
| Lights | 133 | 275 | 127 | 0 |  | 535 | 76 | 565 | 314 | 0 |  | 955 | 87 | 461 | 119 | 0 |  | 667 | 211 | 1502 | 98 | 0 |  | 1811 | - |
| Lights \% | 93.7\% | 96.5\% | 91.4\% | 0\% |  | 94.5\% | 95\% | 93.2\% | 96.3\% | 0\% |  | 94.4\% | 91.6\% | 98.1\% | 96.7\% | 0\% |  | 96.9\% | 98.1\% | 97.8\% | 98\% | 0\% |  | 97.8\% | - |
| Single-Unit Trucks | 7 | 3 | 2 | 0 |  | 12 | 2 | 10 | 5 | 0 |  | 17 | 1 | 5 | 2 | 0 |  | 8 | 0 | 8 | 1 | 0 |  | 9 | - |
| Single-Unit Trucks \% | 4.9\% | 1.1\% | 1.4\% | 0\% |  | 2.1\% | 2.5\% | 1.7\% | 1.5\% | 0\% |  | 1.7\% | 1.1\% | 1.1\% | 1.6\% | 0\% |  | 1.2\% | 0\% | 0.5\% | 1\% | 0\% |  | 0.5\% | - |
| Buses | 0 | 7 | 10 | 0 |  | 17 | 0 | 29 | 7 | 0 |  | 36 | 7 | 4 | 2 | 0 |  | 13 | 4 | 26 | 1 | 0 |  | 31 | - |
| Buses \% | 0\% | 2.5\% | 7.2\% | 0\% |  | 3\% | 0\% | 4.8\% | 2.1\% | 0\% |  | 3.6\% | 7.4\% | 0.9\% | 1.6\% | 0\% |  | 1.9\% | 1.9\% | 1.7\% | 1\% | 0\% |  | 1.7\% | - |
| Articulated Trucks | 2 | 0 | 0 | 0 |  | 2 | 2 | 2 | 0 | 0 |  | 4 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 1.4\% | 0\% | 0\% | 0\% |  | 0.4\% | 2.5\% | 0.3\% | 0\% | 0\% |  | 0.4\% | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | - | 14 | - | - | - | - | - | 18 | - | - | - | - | - | 24 | - | - | - | - | - | 14 | - | - |
| Pedestrians\% | - | - | - | - | 20\% |  | - | - | - | - | 25.7\% |  | - | - | - | - | 34.3\% |  | - | - | - | - | 20\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 1 | 0 | 0 | 0 | - | 1 | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - |


| Start Time |  |  |  |  |  |  | Peak Hour: 12:00 PM - 01:00 PM |  |  |  |  |  | Weather: Light Rain (15.56 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Southbound |  |  |  |  |  | Westbound |  |  |  |  |  | Northbound |  |  |  |  |  | Eastbound |  |  |  |  |  | Int. Total ( 15 min ) |
|  | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total |  |
| 12:00:00 | 42 | 68 | 41 | 0 | 3 | 151 | 27 | 151 | 25 | 0 | 0 | 203 | 28 | 46 | 32 | 0 | 4 | 106 | 35 | 218 | 34 | 0 | 2 | 287 | 747 |
| 12:15:00 | 38 | 73 | 32 | 0 | 3 | 143 | 22 | 144 | 32 | 0 | 0 | 198 | 26 | 64 | 29 | 0 | 0 | 119 | 35 | 167 | 23 | 0 | 3 | 225 | 685 |
| 12:30:00 | 28 | 55 | 34 | 0 | 3 | 117 | 24 | 156 | 30 | 0 | 0 | 210 | 26 | 67 | 28 | 0 | 2 | 121 | 30 | 174 | 28 | 0 | 3 | 232 | 680 |
| 12:45:00 | 47 | 68 | 40 | 0 | 0 | 155 | 23 | 170 | 32 | 0 | 2 | 225 | 35 | 73 | 37 | 0 | 1 | 145 | 44 | 179 | 24 | 0 | 1 | 247 | 772 |
| Grand Total | 155 | 264 | 147 | 0 | 9 | 566 | 96 | 621 | 119 | 0 | 2 | 836 | 115 | 250 | 126 | 0 | 7 | 491 | 144 | 738 | 109 | 0 | 9 | 991 | 2884 |
| Approach\% | 27.4\% | 46.6\% | 26\% | 0\% |  | - | 11.5\% | 74.3\% | 14.2\% | 0\% |  | - | 23.4\% | 50.9\% | 25.7\% | 0\% |  | - | 14.5\% | 74.5\% | 11\% | 0\% |  | - | - |
| Totals \% | 5.4\% | 9.2\% | 5.1\% | 0\% |  | 19.6\% | 3.3\% | 21.5\% | 4.1\% | 0\% |  | 29\% | 4\% | 8.7\% | 4.4\% | 0\% |  | 17\% | 5\% | 25.6\% | 3.8\% | 0\% |  | 34.4\% | - |
| PHF | 0.82 | 0.9 | 0.9 | 0 |  | 0.91 | 0.89 | 0.91 | 0.93 | 0 |  | 0.93 | 0.82 | 0.86 | 0.85 | 0 |  | 0.85 | 0.82 | 0.85 | 0.8 | 0 |  | 0.86 | - |
| Heavy | 4 | 6 | 12 | 0 |  | 22 | 3 | 24 | 7 | 0 |  | 34 | 3 | 4 | 1 | 0 |  | 8 | 6 | 21 | 1 | 0 |  | 28 | - |
| Heavy \% | 2.6\% | 2.3\% | 8.2\% | 0\% |  | 3.9\% | 3.1\% | 3.9\% | 5.9\% | 0\% |  | 4.1\% | 2.6\% | 1.6\% | 0.8\% | 0\% |  | 1.6\% | 4.2\% | 2.8\% | 0.9\% | 0\% |  | 2.8\% | - |
| Lights | 151 | 258 | 135 | 0 |  | 544 | 93 | 597 | 112 | 0 |  | 802 | 112 | 246 | 125 | 0 |  | 483 | 138 | 717 | 108 | 0 |  | 963 | - |
| Lights \% | 97.4\% | 97.7\% | 91.8\% | 0\% |  | 96.1\% | 96.9\% | 96.1\% | 94.1\% | 0\% |  | 95.9\% | 97.4\% | 98.4\% | 99.2\% | 0\% |  | 98.4\% | 95.8\% | 97.2\% | 99.1\% | 0\% |  | 97.2\% | - |
| Single-Unit Trucks | 3 | 2 | 3 | 0 |  | 8 | 3 | 13 | 3 | 0 |  | 19 | 2 | 1 | 1 | 0 |  | 4 | 0 | 10 | 0 | 0 |  | 10 | - |
| Single-Unit Trucks \% | 1.9\% | 0.8\% | 2\% | 0\% |  | 1.4\% | 3.1\% | 2.1\% | 2.5\% | 0\% |  | 2.3\% | 1.7\% | 0.4\% | 0.8\% | 0\% |  | 0.8\% | 0\% | 1.4\% | 0\% | 0\% |  | 1\% | - |
| Buses | 1 | 4 | 8 | 0 |  | 13 | 0 | 10 | 0 | 0 |  | 10 | 1 | 3 | 0 | 0 |  | 4 | 6 | 9 | 1 | 0 |  | 16 | - |
| Buses \% | 0.6\% | 1.5\% | 5.4\% | 0\% |  | 2.3\% | 0\% | 1.6\% | 0\% | 0\% |  | 1.2\% | 0.9\% | 1.2\% | 0\% | 0\% |  | 0.8\% | 4.2\% | 1.2\% | 0.9\% | 0\% |  | 1.6\% | - |
| Articulated Trucks | 0 | 0 | 1 | 0 |  | 1 | 0 | 1 | 4 | 0 |  | 5 | 0 | 0 | 0 | 0 |  | 0 | 0 | 2 | 0 | 0 |  | 2 | - |
| Articulated Trucks \% | 0\% | 0\% | 0.7\% | 0\% |  | 0.2\% | 0\% | 0.2\% | $3.4 \%$ | 0\% |  | 0.6\% | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.3\% | 0\% | 0\% |  | 0.2\% | - |
| Pedestrians | - | - | - | - | 9 | - | - | - | - | - | 2 | - | - | - | - | - | 7 | - | - | - | - | - | 9 | - | - |
| Pedestrians\% | - | - | - | - | 33.3\% |  | - | - | - | - | 7.4\% |  | - | - | - | - | 25.9\% |  | - | - | - | - | 33.3\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - |


| Start Time | Peak Hour: 05:00 PM - 06:00 PM |  |  |  |  |  |  |  |  |  |  |  | Weather: Light Rain (14.01 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Southbound |  |  |  |  |  | Westbound |  |  |  |  |  | Northbound |  |  |  |  |  | Eastbound |  |  |  |  |  | Int. Total (15 min) |
|  | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total | Left | Thru | Right | UTurn | Peds | Approach Total |  |
| 17:00:00 | 71 | 126 | 73 | 0 | 0 | 270 | 16 | 354 | 21 | 0 | 9 | 391 | 46 | 103 | 30 | 0 | 4 | 179 | 30 | 242 | 33 | 0 | 0 | 305 | 1145 |
| 17:15:00 | 86 | 145 | 121 | 0 | 6 | 352 | 30 | 327 | 18 | 0 | 8 | 375 | 39 | 81 | 37 | 0 | 1 | 157 | 29 | 214 | 44 | 0 | 3 | 287 | 1171 |
| 17:30:00 | 65 | 139 | 85 | 0 | 5 | 289 | 43 | 231 | 55 | 0 | 7 | 329 | 39 | 91 | 42 | 0 | 1 | 172 | 39 | 200 | 52 | 0 | 7 | 291 | 1081 |
| 17:45:00 | 57 | 100 | 68 | 0 | 1 | 225 | 49 | 273 | 29 | 0 | 0 | 351 | 40 | 73 | 29 | 0 | 3 | 142 | 49 | 267 | 38 | 0 | 0 | 354 | 1072 |
| Grand Total | 279 | 510 | 347 | 0 | 12 | 1136 | 138 | 1185 | 123 | 0 | 24 | 1446 | 164 | 348 | 138 | 0 | 9 | 650 | 147 | 923 | 167 | 0 | 10 | 1237 | 4469 |
| Approach\% | 24.6\% | 44.9\% | 30.5\% | 0\% |  | - | 9.5\% | 82\% | 8.5\% | 0\% |  | - | 25.2\% | 53.5\% | 21.2\% | 0\% |  | - | 11.9\% | 74.6\% | 13.5\% | 0\% |  | - | - |
| Totals \% | 6.2\% | 11.4\% | 7.8\% | 0\% |  | 25.4\% | 3.1\% | 26.5\% | 2.8\% | 0\% |  | 32.4\% | 3.7\% | 7.8\% | 3.1\% | 0\% |  | 14.5\% | 3.3\% | 20.7\% | $3.7 \%$ | 0\% |  | 27.7\% | - |
| PHF | 0.81 | 0.88 | 0.72 | 0 |  | 0.81 | 0.7 | 0.84 | 0.56 | 0 |  | 0.92 | 0.89 | 0.84 | 0.82 | 0 |  | 0.91 | 0.75 | 0.86 | 0.8 | 0 |  | 0.87 | - |
| Heavy | 2 | 2 | 3 | 0 |  | 7 | 1 | 22 | 1 | 0 |  | 24 | 0 | 4 | 1 | 0 |  | 5 | 3 | 22 | 0 | 0 |  | 25 | - |
| Heavy \% | 0.7\% | 0.4\% | 0.9\% | 0\% |  | 0.6\% | 0.7\% | 1.9\% | 0.8\% | 0\% |  | 1.7\% | 0\% | 1.1\% | 0.7\% | 0\% |  | 0.8\% | 2\% | 2.4\% | 0\% | 0\% |  | 2\% | - |
| Lights | 277 | 508 | 344 | 0 |  | 1129 | 137 | 1163 | 122 | 0 |  | 1422 | 164 | 344 | 137 | 0 |  | 645 | 144 | 901 | 167 | 0 |  | 1212 | - |
| Lights \% | 99.3\% | 99.6\% | 99.1\% | 0\% |  | 99.4\% | 99.3\% | 98.1\% | 99.2\% | 0\% |  | 98.3\% | 100\% | 98.9\% | 99.3\% | 0\% |  | 99.2\% | 98\% | 97.6\% | 100\% | 0\% |  | 98\% | - |
| Single-Unit Trucks | 0 | 0 | 1 | 0 |  | 1 | 0 | 9 | 1 | 0 |  | 10 | 0 | 0 | 1 | 0 |  | 1 | 2 | 9 | 0 | 0 |  | 11 | - |
| Single-Unit Trucks \% | 0\% | 0\% | 0.3\% | 0\% |  | 0.1\% | 0\% | 0.8\% | 0.8\% | 0\% |  | 0.7\% | 0\% | 0\% | 0.7\% | 0\% |  | 0.2\% | 1.4\% | 1\% | 0\% | 0\% |  | 0.9\% | - |
| Buses | 1 | 2 | 1 | 0 |  | 4 | 1 | 9 | 0 | 0 |  | 10 | 0 | 4 | 0 | 0 |  | 4 | 1 | 7 | 0 | 0 |  | 8 | - |
| Buses \% | 0.4\% | 0.4\% | 0.3\% | 0\% |  | 0.4\% | 0.7\% | 0.8\% | 0\% | 0\% |  | 0.7\% | 0\% | 1.1\% | 0\% | 0\% |  | 0.6\% | 0.7\% | 0.8\% | 0\% | 0\% |  | 0.6\% | - |
| Articulated Trucks | 1 | 0 | 1 | 0 |  | 2 | 0 | 4 | 0 | 0 |  | 4 | 0 | 0 | 0 | 0 |  | 0 | 0 | 6 | 0 | 0 |  | 6 | - |
| Articulated Trucks \% | 0.4\% | 0\% | 0.3\% | 0\% |  | 0.2\% | 0\% | 0.3\% | 0\% | 0\% |  | 0.3\% | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.7\% | 0\% | 0\% |  | 0.5\% | - |
| Pedestrians | - | - | - | . | 12 | - | . | - | - | - | 24 | - | . | - | . | . | 9 | - | - | - | . | - | 10 | - | - |
| Pedestrians\% | - | - | - | - | 21.8\% |  | - | - | - | - | 43.6\% |  | - | - | - | - | 16.4\% |  | - | - | - | - | 18.2\% |  | - |
| Bicycles on Road | 0 | 1 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - | - | - | - | 0\% |  | - |








| Turning Movement Count (5. QUEEN ST N \& 26 QUEEN ST N (PETRO CANADA NORTH DRIVEWAY)) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach <br> 26 QUEEN ST N (PETRO CANADA NORTH DRIVEWAY) |  |  |  |  | Int. Total <br> (15 min) | Int. Total ( 1 hr ) |
|  | $\begin{aligned} & \text { Right } \\ & \mathrm{N}: \mathrm{W} \end{aligned}$ | Thru $\mathrm{N}: \mathrm{S}$ | UTurn N:N | Peds N : | Approach Total | $\begin{aligned} & \text { Thru } \\ & \text { S:N } \end{aligned}$ | $\begin{aligned} & \text { Left } \\ & \text { S:W } \end{aligned}$ | $\begin{aligned} & \text { UTurn } \\ & \mathrm{S}: \mathrm{S} \end{aligned}$ | Peds S: | Approach Total | Right W:S | Left <br> W:N | UTurn W:W | Peds W: | Approach Total |  |  |
| 07:00:00 | 1 | 48 | 0 | 0 | 49 | 53 | 0 | 0 | 0 | 53 | 0 | 0 | 0 | 0 | 0 | 102 |  |
| 07:15:00 | 1 | 83 | 0 | 0 | 84 | 85 | 1 | 0 | 0 | 86 | 0 | 1 | 0 | 0 | 1 | 171 |  |
| 07:30:00 | 2 | 80 | 0 | 0 | 82 | 71 | 1 | 0 | 0 | 72 | 0 | 0 | 0 | 0 | 0 | 154 |  |
| 07:45:00 | 1 | 120 | 0 | 0 | 121 | 121 | 3 | 0 | 0 | 124 | 1 | 1 | 0 | 0 | 2 | 247 | 674 |
| 08:00:00 | 4 | 111 | 0 | 0 | 115 | 142 | 2 | 0 | 0 | 144 | 0 | 0 | 0 | 0 | 0 | 259 | 831 |
| 08:15:00 | 1 | 133 | 0 | 0 | 134 | 214 | 0 | 0 | 0 | 214 | 0 | 1 | 0 | 0 | 1 | 349 | 1009 |
| 08:30:00 | 1 | 146 | 0 | 1 | 147 | 165 | 2 | 0 | 0 | 167 | 0 | 0 | 0 | 2 | 0 | 314 | 1169 |
| 08:45:00 | 3 | 139 | 0 | 0 | 142 | 147 | 1 | 0 | 0 | 148 | 1 | 0 | 0 | 1 | 1 | 291 | 1213 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 3 | 143 | 0 | 0 | 146 | 125 | 4 | 0 | 0 | 129 | 0 | 1 | 0 | 0 | 1 | 276 |  |
| 16:15:00 | 5 | 154 | 0 | 0 | 159 | 103 | 1 | 0 | 0 | 104 | 2 | 2 | 0 | 0 | 4 | 267 |  |
| 16:30:00 | 5 | 143 | 0 | 0 | 148 | 132 | 3 | 0 | 0 | 135 | 0 | 1 | 0 | 0 | 1 | 284 |  |
| 16:45:00 | 2 | 143 | 0 | 0 | 145 | 138 | 3 | 0 | 0 | 141 | 0 | 0 | 0 | 1 | 0 | 286 | 1113 |
| 17:00:00 | 1 | 176 | 0 | 0 | 177 | 166 | 1 | 0 | 0 | 167 | 1 | 0 | 0 | 0 | 1 | 345 | 1182 |
| 17:15:00 | 4 | 188 | 0 | 0 | 192 | 142 | 2 | 0 | 0 | 144 | 0 | 0 | 0 | 0 | 0 | 336 | 1251 |
| 17:30:00 | 3 | 143 | 0 | 0 | 146 | 137 | 2 | 0 | 0 | 139 | 0 | 1 | 0 | 1 | 1 | 286 | 1253 |
| 17:45:00 | 3 | 132 | 0 | 0 | 135 | 115 | 0 | 0 | 0 | 115 | 0 | 1 | 0 | 4 | 1 | 251 | 1218 |
| Grand Total | 40 | 2082 | 0 | 1 | 2122 | 2056 | 26 | 0 | 0 | 2082 | 5 | 9 | 0 | 9 | 14 | 4218 | - |
| Approach\% | 1.9\% | 98.1\% | 0\% |  | - | 98.8\% | 1.2\% | 0\% |  | - | 35.7\% | 64.3\% | 0\% |  | - | - | - |
| Totals \% | 0.9\% | 49.4\% | 0\% |  | 50.3\% | 48.7\% | 0.6\% | 0\% |  | 49.4\% | 0.1\% | 0.2\% | 0\% |  | 0.3\% | - | - |
| Heavy | 4 | 68 | 0 |  | - | 55 | 0 | 0 |  | - | 0 | 1 | 0 |  | - | - | - |
| Heavy \% | 10\% | 3.3\% | 0\% |  | - | 2.7\% | 0\% | 0\% |  | - | 0\% | 11.1\% | 0\% |  | - | - | - |
| Bicycles | 0 | 2 | 0 |  | - | 1 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | - | - |
| Bicycle \% | 0\% | 0.1\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | - |

## Peak Hour: 08:00 AM-09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ )

| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach26 QUEEN ST N (PETRO CANADA NORTH DRIVEWAY) |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | UTurn | Peds | Approach Total | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total |  |
| 08:00:00 | 4 | 111 | 0 | 0 | 115 | 142 | 2 | 0 | 0 | 144 | 0 | 0 | 0 | 0 | 0 | 259 |
| 08:15:00 | 1 | 133 | 0 | 0 | 134 | 214 | 0 | 0 | 0 | 214 | 0 | 1 | 0 | 0 | 1 | 349 |
| 08:30:00 | 1 | 146 | 0 | 1 | 147 | 165 | 2 | 0 | 0 | 167 | 0 | 0 | 0 | 2 | 0 | 314 |
| 08:45:00 | 3 | 139 | 0 | 0 | 142 | 147 | 1 | 0 | 0 | 148 | 1 | 0 | 0 | 1 | 1 | 291 |
| Grand Total | 9 | 529 | 0 | 1 | 538 | 668 | 5 | 0 | 0 | 673 | 1 | 1 | 0 | 3 | 2 | 1213 |
| Approach\% | 1.7\% | 98.3\% | 0\% |  | - | 99.3\% | 0.7\% | 0\% |  | - | 50\% | 50\% | 0\% |  | - | - |
| Totals \% | 0.7\% | 43.6\% | 0\% |  | 44.4\% | 55.1\% | 0.4\% | 0\% |  | 55.5\% | 0.1\% | 0.1\% | 0\% |  | 0.2\% | - |
| PHF | 0.56 | 0.91 | 0 |  | 0.91 | 0.78 | 0.63 | 0 |  | 0.79 | 0.25 | 0.25 | 0 |  | 0.5 | - |
| Heavy | 0 | 23 | 0 |  | 23 | 18 | 0 | 0 |  | 18 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 4.3\% | 0\% |  | 4.3\% | 2.7\% | 0\% | 0\% |  | 2.7\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 9 | 506 | 0 |  | 515 | 650 | 5 | 0 |  | 655 | 1 | 1 | 0 |  | 2 | - |
| Lights \% | 100\% | 95.7\% | 0\% |  | 95.7\% | 97.3\% | 100\% | 0\% |  | 97.3\% | 100\% | 100\% | 0\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 10 | 0 |  | 10 | 6 | 0 | 0 |  | 6 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 1.9\% | 0\% |  | 1.9\% | 0.9\% | 0\% | 0\% |  | 0.9\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 11 | 0 |  | 11 | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 2.1\% | 0\% |  | 2\% | 1.5\% | 0\% | 0\% |  | 1.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Articulated Trucks | 0 | 2 | 0 |  | 2 | 2 | 0 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0.4\% | 0\% |  | 0.4\% | 0.3\% | 0\% | 0\% |  | 0.3\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 1 | - | - | - | - | 0 | - | - | - | - | 3 | - | - |
| Pedestrians\% | - | - | - | 25\% |  | - | - | - | 0\% |  | - | - | - | 75\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |


| Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds (20.46 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach <br> 26 QUEEN ST N (PETRO CANADA NORTH DRIVEWAY) |  |  |  |  | Int. Total ( 15 min ) |
|  | Right | Thru | UTurn | Peds | Approach Total | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total |  |
| 16:45:00 | 2 | 143 | 0 | 0 | 145 | 138 | 3 | 0 | 0 | 141 | 0 | 0 | 0 | 1 | 0 | 286 |
| 17:00:00 | 1 | 176 | 0 | 0 | 177 | 166 | 1 | 0 | 0 | 167 | 1 | 0 | 0 | 0 | 1 | 345 |
| 17:15:00 | 4 | 188 | 0 | 0 | 192 | 142 | 2 | 0 | 0 | 144 | 0 | 0 | 0 | 0 | 0 | 336 |
| 17:30:00 | 3 | 143 | 0 | 0 | 146 | 137 | 2 | 0 | 0 | 139 | 0 | 1 | 0 | 1 | 1 | 286 |
| Grand Total | 10 | 650 | 0 | 0 | 660 | 583 | 8 | 0 | 0 | 591 | 1 | 1 | 0 | 2 | 2 | 1253 |
| Approach\% | 1.5\% | 98.5\% | 0\% |  | - | 98.6\% | 1.4\% | 0\% |  | - | 50\% | 50\% | 0\% |  | - | - |
| Totals \% | 0.8\% | 51.9\% | 0\% |  | 52.7\% | 46.5\% | 0.6\% | 0\% |  | 47.2\% | 0.1\% | 0.1\% | 0\% |  | 0.2\% | - |
| PHF | 0.63 | 0.86 | 0 |  | 0.86 | 0.88 | 0.67 | 0 |  | 0.88 | 0.25 | 0.25 | 0 |  | 0.5 | - |
| Heavy | 1 | 10 | 0 |  | 11 | 9 | 0 | 0 |  | 9 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 10\% | 1.5\% | 0\% |  | 1.7\% | 1.5\% | 0\% | 0\% |  | 1.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 9 | 640 | 0 |  | 649 | 574 | 8 | 0 |  | 582 | 1 | 1 | 0 |  | 2 | - |
| Lights \% | 90\% | 98.5\% | 0\% |  | 98.3\% | 98.5\% | 100\% | 0\% |  | 98.5\% | 100\% | 100\% | 0\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 5 | 0 |  | 5 | 3 | 0 | 0 |  | 3 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0.8\% | 0\% |  | 0.8\% | 0.5\% | 0\% | 0\% |  | 0.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 1 | 4 | 0 |  | 5 | 6 | 0 | 0 |  | 6 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 10\% | 0.6\% | 0\% |  | 0.8\% | 1\% | 0\% | 0\% |  | 1\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Articulated Trucks | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0.2\% | 0\% |  | 0.2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 1 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 50\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 1 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 50\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 08:00 AM-09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ )



## Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds (20.46 ${ }^{\circ} \mathrm{C}$ )



| Turning Movement Count (6. QUEEN ST N \& 26 QUEEN ST N (PETRO CANADA SOUTH DRIVEWAY)) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach 26 QUEEN ST N (PETRO CANADA SOUTH DRIVEWAY) |  |  |  |  | Int. Total ( 15 min ) | Int. Total ( 1 hr ) |
|  | Right $\mathrm{N}: \mathrm{W}$ | Thru $\mathrm{N}: \mathrm{S}$ | UTurn $\mathrm{N}: \mathrm{N}$ | Peds N : | Approach Total | Thru S:N | Left <br> S:W | UTurn S:S | Peds S: | Approach Total | Right W:S | Left W:N | UTurn W:W | Peds W: | Approach Total |  |  |
| 07:00:00 | 0 | 50 | 0 | 0 | 50 | 51 | 0 | 0 | 1 | 51 | 1 | 0 | 0 | 0 | 1 | 102 |  |
| 07:15:00 | 0 | 72 | 0 | 0 | 72 | 81 | 1 | 0 | 0 | 82 | 1 | 1 | 0 | 0 | 2 | 156 |  |
| 07:30:00 | 0 | 83 | 0 | 0 | 83 | 78 | 1 | 0 | 0 | 79 | 0 | 0 | 0 | 0 | 0 | 162 |  |
| 07:45:00 | 1 | 116 | 0 | 0 | 117 | 116 | 0 | 0 | 0 | 116 | 1 | 0 | 0 | 0 | 1 | 234 | 654 |
| 08:00:00 | 0 | 117 | 0 | 0 | 117 | 135 | 1 | 0 | 0 | 136 | 2 | 3 | 0 | 0 | 5 | 258 | 810 |
| 08:15:00 | 0 | 128 | 1 | 0 | 129 | 216 | 0 | 0 | 0 | 216 | 1 | 1 | 0 | 0 | 2 | 347 | 1001 |
| 08:30:00 | 0 | 154 | 0 | 0 | 154 | 163 | 0 | 0 | 2 | 163 | 1 | 3 | 0 | 2 | 4 | 321 | 1160 |
| 08:45:00 | 0 | 131 | 0 | 0 | 131 | 155 | 1 | 0 | 0 | 156 | 1 | 1 | 0 | 1 | 2 | 289 | 1215 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 0 | 141 | 0 | 0 | 141 | 138 | 1 | 0 | 0 | 139 | 2 | 2 | 0 | 0 | 4 | 284 |  |
| 16:15:00 | 1 | 145 | 0 | 0 | 146 | 106 | 1 | 0 | 0 | 107 | 5 | 1 | 0 | 0 | 6 | 259 |  |
| 16:30:00 | 0 | 141 | 0 | 0 | 141 | 135 | 2 | 0 | 0 | 137 | 7 | 1 | 0 | 0 | 8 | 286 |  |
| 16:45:00 | 0 | 145 | 0 | 0 | 145 | 143 | 0 | 1 | 0 | 144 | 4 | 1 | 0 | 1 | 5 | 294 | 1123 |
| 17:00:00 | 0 | 179 | 0 | 0 | 179 | 170 | 0 | 0 | 1 | 170 | 2 | 2 | 0 | 0 | 4 | 353 | 1192 |
| 17:15:00 | 0 | 202 | 0 | 0 | 202 | 145 | 2 | 2 | 3 | 149 | 2 | 0 | 0 | 0 | 2 | 353 | 1286 |
| 17:30:00 | 0 | 144 | 0 | 0 | 144 | 136 | 1 | 0 | 0 | 137 | 6 | 2 | 0 | 1 | 8 | 289 | 1289 |
| 17:45:00 | 0 | 133 | 0 | 0 | 133 | 128 | 2 | 0 | 0 | 130 | 1 | 0 | 0 | 4 | 1 | 264 | 1259 |
| Grand Total | 2 | 2081 | 1 | 0 | 2084 | 2096 | 13 | 3 | 7 | 2112 | 37 | 18 | 0 | 9 | 55 | 4251 | - |
| Approach\% | 0.1\% | 99.9\% | 0\% |  | - | 99.2\% | 0.6\% | 0.1\% |  | - | 67.3\% | 32.7\% | 0\% |  | - | - | - |
| Totals \% | 0\% | 49\% | 0\% |  | 49\% | 49.3\% | 0.3\% | 0.1\% |  | 49.7\% | 0.9\% | 0.4\% | 0\% |  | 1.3\% | - | - |
| Heavy | 0 | 69 | 0 |  | - | 56 | 1 | 0 |  | - | 3 | 0 | 0 |  | - | - | - |
| Heavy \% | 0\% | 3.3\% | 0\% |  | - | 2.7\% | 7.7\% | 0\% |  | - | 8.1\% | 0\% | 0\% |  | - | - | - |
| Bicycles | 0 | 2 | 0 |  | - | 4 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | - | - |
| Bicycle \% | 0\% | 0.1\% | 0\% |  | - | 0.2\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | - |

## Peak Hour: 08:00 AM - 09:00 AM Weather: Clear Sky (13.73 $\left.{ }^{\circ} \mathrm{C}\right)$

| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach <br> 26 QUEEN ST N (PETRO CANADA SOUTH DRIVEWAY) |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | UTurn | Peds | Approach Total | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total |  |
| 08:00:00 | 0 | 117 | 0 | 0 | 117 | 135 | 1 | 0 | 0 | 136 | 2 | 3 | 0 | 0 | 5 | 258 |
| 08:15:00 | 0 | 128 | 1 | 0 | 129 | 216 | 0 | 0 | 0 | 216 | 1 | 1 | 0 | 0 | 2 | 347 |
| 08:30:00 | 0 | 154 | 0 | 0 | 154 | 163 | 0 | 0 | 2 | 163 | 1 | 3 | 0 | 2 | 4 | 321 |
| 08:45:00 | 0 | 131 | 0 | 0 | 131 | 155 | 1 | 0 | 0 | 156 | 1 | 1 | 0 | 1 | 2 | 289 |
| Grand Total | 0 | 530 | 1 | 0 | 531 | 669 | 2 | 0 | 2 | 671 | 5 | 8 | 0 | 3 | 13 | 1215 |
| Approach\% | 0\% | 99.8\% | 0.2\% |  | - | 99.7\% | 0.3\% | 0\% |  | - | 38.5\% | 61.5\% | 0\% |  | - | - |
| Totals \% | 0\% | 43.6\% | 0.1\% |  | 43.7\% | 55.1\% | 0.2\% | 0\% |  | 55.2\% | 0.4\% | 0.7\% | 0\% |  | 1.1\% | - |
| PHF | 0 | 0.86 | 0.25 |  | 0.86 | 0.77 | 0.5 | 0 |  | 0.78 | 0.63 | 0.67 | 0 |  | 0.65 | - |
| Heavy | 0 | 23 | 0 |  | 23 | 18 | 0 | 0 |  | 18 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 4.3\% | 0\% |  | 4.3\% | 2.7\% | 0\% | 0\% |  | 2.7\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 0 | 507 | 1 |  | 508 | 651 | 2 | 0 |  | 653 | 5 | 8 | 0 |  | 13 | - |
| Lights \% | 0\% | 95.7\% | 100\% |  | 95.7\% | 97.3\% | 100\% | 0\% |  | 97.3\% | 100\% | 100\% | 0\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 10 | 0 |  | 10 | 7 | 0 | 0 |  | 7 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 1.9\% | 0\% |  | 1.9\% | 1\% | 0\% | 0\% |  | 1\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 11 | 0 |  | 11 | 9 | 0 | 0 |  | 9 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 2.1\% | 0\% |  | 2.1\% | 1.3\% | 0\% | 0\% |  | 1.3\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Articulated Trucks | 0 | 2 | 0 |  | 2 | 2 | 0 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0.4\% | 0\% |  | 0.4\% | 0.3\% | 0\% | 0\% |  | 0.3\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 2 | - | - | - | - | 3 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 40\% |  | - | - | - | 60\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds ( $20.46{ }^{\circ} \mathrm{C}$ )

| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach <br> 26 QUEEN ST N (PETRO CANADA SOUTH DRIVEWAY) |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | UTurn | Peds | Approach Total | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total |  |
| 16:45:00 | 0 | 145 | 0 | 0 | 145 | 143 | 0 | 1 | 0 | 144 | 4 | 1 | 0 | 1 | 5 | 294 |
| 17:00:00 | 0 | 179 | 0 | 0 | 179 | 170 | 0 | 0 | 1 | 170 | 2 | 2 | 0 | 0 | 4 | 353 |
| 17:15:00 | 0 | 202 | 0 | 0 | 202 | 145 | 2 | 2 | 3 | 149 | 2 | 0 | 0 | 0 | 2 | 353 |
| 17:30:00 | 0 | 144 | 0 | 0 | 144 | 136 | 1 | 0 | 0 | 137 | 6 | 2 | 0 | 1 | 8 | 289 |
| Grand Total | 0 | 670 | 0 | 0 | 670 | 594 | 3 | 3 | 4 | 600 | 14 | 5 | 0 | 2 | 19 | 1289 |
| Approach\% | 0\% | 100\% | 0\% |  | - | 99\% | 0.5\% | 0.5\% |  | - | 73.7\% | 26.3\% | 0\% |  | - | - |
| Totals \% | 0\% | 52\% | 0\% |  | 52\% | 46.1\% | 0.2\% | 0.2\% |  | 46.5\% | 1.1\% | 0.4\% | 0\% |  | 1.5\% | - |
| PHF | 0 | 0.83 | 0 |  | 0.83 | 0.87 | 0.38 | 0.38 |  | 0.88 | 0.58 | 0.63 | 0 |  | 0.59 | - |
| Heavy | 0 | 11 | 0 |  | 11 | 9 | 0 | 0 |  | 9 | 1 | 0 | 0 |  | 1 | - |
| Heavy \% | 0\% | 1.6\% | 0\% |  | 1.6\% | 1.5\% | 0\% | 0\% |  | 1.5\% | 7.1\% | 0\% | 0\% |  | 5.3\% | - |
| Lights | 0 | 659 | 0 |  | 659 | 585 | 3 | 3 |  | 591 | 13 | 5 | 0 |  | 18 | - |
| Lights \% | 0\% | 98.4\% | 0\% |  | 98.4\% | 98.5\% | 100\% | 100\% |  | 98.5\% | 92.9\% | 100\% | 0\% |  | 94.7\% | - |
| Single-Unit Trucks | 0 | 6 | 0 |  | 6 | 3 | 0 | 0 |  | 3 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0.9\% | 0\% |  | 0.9\% | 0.5\% | 0\% | 0\% |  | 0.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 4 | 0 |  | 4 | 6 | 0 | 0 |  | 6 | 1 | 0 | 0 |  | 1 | - |
| Buses \% | 0\% | 0.6\% | 0\% |  | 0.6\% | 1\% | 0\% | 0\% |  | 1\% | 7.1\% | 0\% | 0\% |  | 5.3\% | - |
| Articulated Trucks | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0.1\% | 0\% |  | 0.1\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 4 | - | - | - | - | 1 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 66.7\% |  | - | - | - | 16.7\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 1 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 16.7\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 1 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 08:00 AM-09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ )



## Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds (20.46 ${ }^{\circ} \mathrm{C}$ )



| Turning Movement Count (7. QUEEN ST N \& 39 QUEEN ST N NORTH DRIVEWAY) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 39 QUEEN ST N NORTH DRIVEWAY |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) | Int. Total (1 hr) |
|  | Thru $\mathrm{N}: \mathrm{S}$ | Left $\mathrm{N}: \mathrm{E}$ | UTurn $\mathrm{N}: \mathrm{N}$ | Peds <br> N : | Approach Total | Right <br> E:N | Left E:S | UTurn E:E | Peds E: | Approach Total | $\begin{aligned} & \text { Right } \\ & \text { S:E } \end{aligned}$ | $\begin{aligned} & \text { Thru } \\ & \text { S:N } \end{aligned}$ | $\begin{aligned} & \text { UTurn } \\ & \mathrm{s}: \mathrm{S} \end{aligned}$ | Peds S: | Approach Total |  |  |
| 07:00:00 | 49 | 0 | 0 | 0 | 49 | 0 | 0 | 0 | 2 | 0 | 0 | 53 | 0 | 0 | 53 | 102 |  |
| 07:15:00 | 84 | 1 | 0 | 0 | 85 | 0 | 0 | 0 | 3 | 0 | 0 | 86 | 0 | 0 | 86 | 171 |  |
| 07:30:00 | 81 | 0 | 0 | 0 | 81 | 1 | 1 | 0 | 1 | 2 | 0 | 71 | 0 | 0 | 71 | 154 |  |
| 07:45:00 | 122 | 0 | 0 | 0 | 122 | 0 | 0 | 0 | 1 | 0 | 0 | 121 | 0 | 0 | 121 | 243 | 670 |
| 08:00:00 | 114 | 1 | 0 | 0 | 115 | 0 | 0 | 0 | 1 | 0 | 0 | 142 | 0 | 0 | 142 | 257 | 825 |
| 08:15:00 | 133 | 0 | 0 | 0 | 133 | 1 | 1 | 0 | 1 | 2 | 1 | 215 | 0 | 0 | 216 | 351 | 1005 |
| 08:30:00 | 147 | 1 | 0 | 1 | 148 | 2 | 0 | 0 | 4 | 2 | 0 | 165 | 0 | 0 | 165 | 315 | 1166 |
| 08:45:00 | 143 | 0 | 0 | 0 | 143 | 0 | 0 | 0 | 0 | 0 | 0 | 147 | 0 | 0 | 147 | 290 | 1213 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 137 | 1 | 0 | 0 | 138 | 2 | 9 | 0 | 0 | 11 | 0 | 126 | 0 | 0 | 126 | 275 |  |
| 16:15:00 | 154 | 3 | 0 | 0 | 157 | 4 | 3 | 0 | 2 | 7 | 0 | 104 | 0 | 0 | 104 | 268 |  |
| 16:30:00 | 143 | 0 | 0 | 0 | 143 | 0 | 5 | 0 | 1 | 5 | 0 | 133 | 0 | 0 | 133 | 281 |  |
| 16:45:00 | 140 | 4 | 0 | 0 | 144 | 4 | 5 | 0 | 6 | 9 | 0 | 138 | 0 | 0 | 138 | 291 | 1115 |
| 17:00:00 | 171 | 3 | 0 | 0 | 174 | 3 | 7 | 0 | 1 | 10 | 0 | 166 | 0 | 0 | 166 | 350 | 1190 |
| 17:15:00 | 186 | 3 | 0 | 0 | 189 | 8 | 6 | 0 | 3 | 14 | 0 | 141 | 0 | 0 | 141 | 344 | 1266 |
| 17:30:00 | 140 | 2 | 0 | 0 | 142 | 5 | 6 | 0 | 3 | 11 | 1 | 138 | 0 | 0 | 139 | 292 | 1277 |
| 17:45:00 | 131 | 1 | 0 | 0 | 132 | 5 | 4 | 0 | 1 | 9 | 0 | 116 | 0 | 0 | 116 | 257 | 1243 |
| Grand Total | 2075 | 20 | 0 | 1 | 2095 | 35 | 47 | 0 | 30 | 82 | 2 | 2062 | 0 | 0 | 2064 | 4241 | - |
| Approach\% | 99\% | 1\% | 0\% |  | - | 42.7\% | 57.3\% | 0\% |  | - | 0.1\% | 99.9\% | 0\% |  | - | - | - |
| Totals \% | 48.9\% | 0.5\% | 0\% |  | 49.4\% | 0.8\% | 1.1\% | 0\% |  | 1.9\% | 0\% | 48.6\% | 0\% |  | 48.7\% | - | - |
| Heavy | 71 | 0 | 0 |  | - | 0 | 1 | 0 |  | - | 0 | 55 | 0 |  | - | - | - |
| Heavy \% | 3.4\% | 0\% | 0\% |  | - | 0\% | 2.1\% | 0\% |  | - | 0\% | 2.7\% | 0\% |  | - | - | - |
| Bicycles | 2 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | 0 | 3 | 0 |  | - | - | - |
| Bicycle \% | 0.1\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0\% | 0.1\% | 0\% |  | - | - | - |

00045 BT BA Group TORONTO ONTARIO, M4V 1K CANADA

| Peak Hour: 08:00 AM- 09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 39 QUEEN ST N NORTH DRIVEWAY |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) |
|  | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total | Right | Thru | UTurn | Peds | Approach Total |  |
| 08:00:00 | 114 | 1 | 0 | 0 | 115 | 0 | 0 | 0 | 1 | 0 | 0 | 142 | 0 | 0 | 142 | 257 |
| 08:15:00 | 133 | 0 | 0 | 0 | 133 | 1 | 1 | 0 | 1 | 2 | 1 | 215 | 0 | 0 | 216 | 351 |
| 08:30:00 | 147 | 1 | 0 | 1 | 148 | 2 | 0 | 0 | 4 | 2 | 0 | 165 | 0 | 0 | 165 | 315 |
| 08:45:00 | 143 | 0 | 0 | 0 | 143 | 0 | 0 | 0 | 0 | 0 | 0 | 147 | 0 | 0 | 147 | 290 |
| Grand Total | 537 | 2 | 0 | 1 | 539 | 3 | 1 | 0 | 6 | 4 | 1 | 669 | 0 | 0 | 670 | 1213 |
| Approach\% | 99.6\% | 0.4\% | 0\% |  | - | 75\% | 25\% | 0\% |  | - | 0.1\% | 99.9\% | 0\% |  | - | - |
| Totals \% | 44.3\% | 0.2\% | 0\% |  | 44.4\% | 0.2\% | 0.1\% | 0\% |  | 0.3\% | 0.1\% | 55.2\% | 0\% |  | 55.2\% | - |
| PHF | 0.91 | 0.5 | 0 |  | 0.91 | 0.38 | 0.25 | 0 |  | 0.5 | 0.25 | 0.78 | 0 |  | 0.78 | - |
| Heavy | 23 | 0 | 0 |  | 23 | 0 | 0 | 0 |  | 0 | 0 | 17 | 0 |  | 17 | -- |
| Heavy \% | 4.3\% | 0\% | 0\% |  | 4.3\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 2.5\% | 0\% |  | 2.5\% | - |
| Lights | 514 | 2 | 0 |  | 516 | 3 | 1 | 0 |  | 4 | 1 | 652 | 0 |  | 653 | - |
| Lights \% | 95.7\% | 100\% | 0\% |  | 95.7\% | 100\% | 100\% | 0\% |  | 100\% | 100\% | 97.5\% | 0\% |  | 97.5\% | - |
| Single-Unit Trucks | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | 0 | 6 | 0 |  | 6 | - |
| Single-Unit Trucks \% | 1.9\% | 0\% | 0\% |  | 1.9\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.9\% | 0\% |  | 0.9\% | - |
| Buses | 11 | 0 | 0 |  | 11 | 0 | 0 | 0 |  | 0 | 0 | 9 | 0 |  | 9 | - |
| Buses \% | 2\% | 0\% | 0\% |  | 2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1.3\% | 0\% |  | 1.3\% | - |
| Articulated Trucks | 2 | 0 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | 0 | 2 | 0 |  | 2 | - |
| Articulated Trucks \% | 0.4\% | 0\% | 0\% |  | 0.4\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.3\% | 0\% |  | 0.3\% | - |
| Pedestrians | - | - | - | 1 | - | - | - | - | 5 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 14.3\% |  | - | - | - | 71.4\% |  | - | - | - | 0\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 14.3\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |


| Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds ( $20.46{ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 39 QUEEN ST N NORTH DRIVEWAY |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) |
|  | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total | Right | Thru | UTurn | Peds | Approach Total |  |
| 16:45:00 | 140 | 4 | 0 | 0 | 144 | 4 | 5 | 0 | 6 | 9 | 0 | 138 | 0 | 0 | 138 | 291 |
| 17:00:00 | 171 | 3 | 0 | 0 | 174 | 3 | 7 | 0 | 1 | 10 | 0 | 166 | 0 | 0 | 166 | 350 |
| 17:15:00 | 186 | 3 | 0 | 0 | 189 | 8 | 6 | 0 | 3 | 14 | 0 | 141 | 0 | 0 | 141 | 344 |
| 17:30:00 | 140 | 2 | 0 | 0 | 142 | 5 | 6 | 0 | 3 | 11 | 1 | 138 | 0 | 0 | 139 | 292 |
| Grand Total | 637 | 12 | 0 | 0 | 649 | 20 | 24 | 0 | 13 | 44 | 1 | 583 | 0 | 0 | 584 | 1277 |
| Approach\% | 98.2\% | 1.8\% | 0\% |  | - | 45.5\% | 54.5\% | 0\% |  | - | 0.2\% | 99.8\% | 0\% |  | - | - |
| Totals \% | 49.9\% | 0.9\% | 0\% |  | 50.8\% | 1.6\% | 1.9\% | 0\% |  | 3.4\% | 0.1\% | 45.7\% | 0\% |  | 45.7\% | - |
| PHF | 0.86 | 0.75 | 0 |  | 0.86 | 0.63 | 0.86 | 0 |  | 0.79 | 0.25 | 0.88 | 0 |  | 0.88 | - |
| Heavy | 11 | 0 | 0 |  | 11 | 0 | 0 | 0 |  | 0 | 0 | 9 | 0 |  | 9 | - |
| Heavy \% | 1.7\% | 0\% | 0\% |  | 1.7\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1.5\% | 0\% |  | 1.5\% | - |
| Lights | 626 | 12 | 0 |  | 638 | 20 | 24 | 0 |  | 44 | 1 | 574 | 0 |  | 575 | - |
| Lights \% | 98.3\% | 100\% | 0\% |  | 98.3\% | 100\% | 100\% | 0\% |  | 100\% | 100\% | 98.5\% | 0\% |  | 98.5\% | - |
| Single-Unit Trucks | 5 | 0 | 0 |  | 5 | 0 | 0 | 0 |  | 0 | 0 | 3 | 0 |  | 3 | - |
| Single-Unit Trucks \% | 0.8\% | 0\% | 0\% |  | 0.8\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.5\% | 0\% |  | 0.5\% | - |
| Buses | 5 | 0 | 0 |  | 5 | 0 | 0 | 0 |  | 0 | 0 | 6 | 0 |  | 6 | - |
| Buses \% | 0.8\% | 0\% | 0\% |  | 0.8\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1\% | 0\% |  | 1\% | - |
| Articulated Trucks | 1 | 0 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0.2\% | 0\% | 0\% |  | 0.2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 12 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 92.3\% |  | - | - | - | 0\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 7.7\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 1 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 08:00 AM - 09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ )


## Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds (20.46 ${ }^{\circ} \mathrm{C}$ )



Turning Movement Count (8. QUEEN ST N \& 39 QUEEN ST N SOUTH DRIVEWAY)

| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 39 QUEEN ST N SOUTH DRIVEWAY |  |  |  |  |  | S Approach QUEEN ST N |  |  |  | Int. Total (15 min) | Int. Total ( 1 hr ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thru N:S | Left <br> $\mathrm{N}: \mathrm{E}$ | UTurn $\mathrm{N}: \mathrm{N}$ | Peds <br> N : | Approach Total | Right E:N | Left E:S | UTurn E:E | Peds E: | Approach Total | $\begin{aligned} & \text { Right } \\ & \text { S:E } \end{aligned}$ | Thru S:N | $\begin{aligned} & \text { UTurn } \\ & \text { S:S } \end{aligned}$ | Peds S: | Approach Total |  |  |
| 07:00:00 | 51 | 0 | 0 | 0 | 51 | 0 | 0 | 0 | 2 | 0 | 1 | 51 | 0 | 0 | 52 | 103 |  |
| 07:15:00 | 75 | 0 | 0 | 0 | 75 | 0 | 0 | 0 | 4 | 0 | 1 | 82 | 0 | 0 | 83 | 158 |  |
| 07:30:00 | 81 | 0 | 0 | 0 | 81 | 0 | 0 | 0 | 1 | 0 | 1 | 75 | 0 | 0 | 76 | 157 |  |
| 07:45:00 | 118 | 0 | 0 | 0 | 118 | 0 | 0 | 0 | 2 | 0 | 0 | 122 | 0 | 0 | 122 | 240 | 658 |
| 08:00:00 | 116 | 0 | 0 | 0 | 116 | 0 | 0 | 0 | 2 | 0 | 0 | 137 | 0 | 0 | 137 | 253 | 808 |
| 08:15:00 | 132 | 0 | 0 | 0 | 132 | 0 | 0 | 0 | 1 | 0 | 4 | 214 | 0 | 0 | 218 | 350 | 1000 |
| 08:30:00 | 151 | 1 | 0 | 0 | 152 | 0 | 1 | 0 | 3 | 1 | 2 | 163 | 0 | 0 | 165 | 318 | 1161 |
| 08:45:00 | 133 | 0 | 0 | 0 | 133 | 0 | 0 | 0 | 0 | 0 | 1 | 156 | 0 | 0 | 157 | 290 | 1211 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 144 | 1 | 0 | 0 | 145 | 0 | 1 | 0 | 0 | 1 | 8 | 128 | 0 | 0 | 136 | 282 |  |
| 16:15:00 | 143 | 0 | 0 | 0 | 143 | 0 | 1 | 0 | 2 | 1 | 2 | 106 | 0 | 0 | 108 | 252 |  |
| 16:30:00 | 142 | 3 | 0 | 0 | 145 | 0 | 1 | 0 | 2 | 1 | 6 | 133 | 0 | 0 | 139 | 285 |  |
| 16:45:00 | 143 | 2 | 0 | 0 | 145 | 0 | 1 | 0 | 7 | 1 | 8 | 134 | 1 | 0 | 143 | 289 | 1108 |
| 17:00:00 | 179 | 0 | 0 | 0 | 179 | 0 | 2 | 0 | 2 | 2 | 3 | 179 | 0 | 0 | 182 | 363 | 1189 |
| 17:15:00 | 188 | 2 | 0 | 0 | 190 | 0 | 1 | 0 | 3 | 1 | 7 | 142 | 0 | 0 | 149 | 340 | 1277 |
| 17:30:00 | 146 | 0 | 0 | 0 | 146 | 0 | 1 | 0 | 3 | 1 | 6 | 133 | 0 | 0 | 139 | 286 | 1278 |
| 17:45:00 | 129 | 0 | 0 | 0 | 129 | 0 | 2 | 0 | 1 | 2 | 5 | 126 | 0 | 0 | 131 | 262 | 1251 |
| Grand Total | 2071 | 9 | 0 | 0 | 2080 | 0 | 11 | 0 | 35 | 11 | 55 | 2081 | 1 | 0 | 2137 | 4228 | - |
| Approach\% | 99.6\% | 0.4\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | 2.6\% | 97.4\% | 0\% |  | - | - | - |
| Totals \% | 49\% | 0.2\% | 0\% |  | 49.2\% | 0\% | 0.3\% | 0\% |  | 0.3\% | 1.3\% | 49.2\% | 0\% |  | 50.5\% | - | - |
| Heavy | 68 | 0 | 0 |  | - | 0 | 1 | 0 |  | - | 1 | 56 | 0 |  | - | - | - |
| Heavy \% | 3.3\% | 0\% | 0\% |  | - | 0\% | 9.1\% | 0\% |  | - | 1.8\% | 2.7\% | 0\% |  | - | - | - |
| Bicycles | 2 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | 0 | 2 | 0 |  | - | - | - |
| Bicycle \% | 0.1\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0\% | 0.1\% | 0\% |  | - | - | - |


| Peak Hour: 08:00 AM - 09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 39 QUEEN ST N SOUTH DRIVEWAY |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) |
|  | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total | Right | Thru | UTurn | Peds | Approach Total |  |
| 08:00:00 | 116 | 0 | 0 | 0 | 116 | 0 | 0 | 0 | 2 | 0 | 0 | 137 | 0 | 0 | 137 | 253 |
| 08:15:00 | 132 | 0 | 0 | 0 | 132 | 0 | 0 | 0 | 1 | 0 | 4 | 214 | 0 | 0 | 218 | 350 |
| 08:30:00 | 151 | 1 | 0 | 0 | 152 | 0 | 1 | 0 | 3 | 1 | 2 | 163 | 0 | 0 | 165 | 318 |
| 08:45:00 | 133 | 0 | 0 | 0 | 133 | 0 | 0 | 0 | 0 | 0 | 1 | 156 | 0 | 0 | 157 | 290 |
| Grand Total | 532 | 1 | 0 | 0 | 533 | 0 | 1 | 0 | 6 | 1 | 7 | 670 | 0 | 0 | 677 | 1211 |
| Approach\% | 99.8\% | 0.2\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | 1\% | 99\% | 0\% |  | - | - |
| Totals \% | 43.9\% | 0.1\% | 0\% |  | 44\% | 0\% | 0.1\% | 0\% |  | 0.1\% | 0.6\% | 55.3\% | 0\% |  | 55.9\% | - |
| PHF | 0.88 | 0.25 | 0 |  | 0.88 | 0 | 0.25 | 0 |  | 0.25 | 0.44 | 0.78 | 0 |  | 0.78 | - |
| Heavy | 23 | 0 | 0 |  | 23 | 0 | 0 | 0 |  | 0 | 1 | 18 | 0 |  | 19 | - |
| Heavy \% | 4.3\% | 0\% | 0\% |  | 4.3\% | 0\% | 0\% | 0\% |  | 0\% | 14.3\% | 2.7\% | 0\% |  | 2.8\% | - |
| Lights | 509 | 1 | 0 |  | 510 | 0 | 1 | 0 |  | 1 | 6 | 652 | 0 |  | 658 | - |
| Lights \% | 95.7\% | 100\% | 0\% |  | 95.7\% | 0\% | 100\% | 0\% |  | 100\% | 85.7\% | 97.3\% | 0\% |  | 97.2\% | - |
| Single-Unit Trucks | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | 1 | 6 | 0 |  | 7 | - |
| Single-Unit Trucks \% | 1.9\% | 0\% | 0\% |  | 1.9\% | 0\% | 0\% | 0\% |  | 0\% | 14.3\% | 0.9\% | 0\% |  | 1\% | - |
| Buses | 11 | 0 | 0 |  | 11 | 0 | 0 | 0 |  | 0 | 0 | 10 | 0 |  | 10 | - |
| Buses \% | 2.1\% | 0\% | 0\% |  | 2.1\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1.5\% | 0\% |  | 1.5\% | - |
| Articulated Trucks | 2 | 0 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | 0 | 2 | 0 |  | 2 | - |
| Articulated Trucks \% | 0.4\% | 0\% | 0\% |  | 0.4\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.3\% | 0\% |  | 0.3\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 5 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 83.3\% |  | - | - | - | 0\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - |  | 0\% |  | - | - | - | 16.7\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |


| Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds (20.46 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 39 QUEEN ST N SOUTH DRIVEWAY |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) |
|  | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total | Right | Thru | UTurn | Peds | Approach Total |  |
| 16:45:00 | 143 | 2 | 0 | 0 | 145 | 0 | 1 | 0 | 7 | 1 | 8 | 134 | 1 | 0 | 143 | 289 |
| 17:00:00 | 179 | 0 | 0 | 0 | 179 | 0 | 2 | 0 | 2 | 2 | 3 | 179 | 0 | 0 | 182 | 363 |
| 17:15:00 | 188 | 2 | 0 | 0 | 190 | 0 | 1 | 0 | 3 | 1 | 7 | 142 | 0 | 0 | 149 | 340 |
| 17:30:00 | 146 | 0 | 0 | 0 | 146 | 0 | 1 | 0 | 3 | 1 | 6 | 133 | 0 | 0 | 139 | 286 |
| Grand Total | 656 | 4 | 0 | 0 | 660 | 0 | 5 | 0 | 15 | 5 | 24 | 588 | 1 | 0 | 613 | 1278 |
| Approach\% | 99.4\% | 0.6\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | 3.9\% | 95.9\% | 0.2\% |  | - | - |
| Totals \% | 51.3\% | 0.3\% | 0\% |  | 51.6\% | 0\% | 0.4\% | 0\% |  | 0.4\% | 1.9\% | 46\% | 0.1\% |  | 48\% | - |
| PHF | 0.87 | 0.5 | 0 |  | 0.87 | 0 | 0.63 | 0 |  | 0.63 | 0.75 | 0.82 | 0.25 |  | 0.84 | - |
| Heavy | 11 | 0 | 0 |  | 11 | 0 | 0 | 0 |  | 0 | 0 | 9 | 0 |  | 9 | - |
| Heavy \% | 1.7\% | 0\% | 0\% |  | 1.7\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1.5\% | 0\% |  | 1.5\% | - |
| Lights | 645 | 4 | 0 |  | 649 | 0 | 5 | 0 |  | 5 | 24 | 579 | 1 |  | 604 | - |
| Lights \% | 98.3\% | 100\% | 0\% |  | 98.3\% | 0\% | 100\% | 0\% |  | 100\% | 100\% | 98.5\% | 100\% |  | 98.5\% | - |
| Single-Unit Trucks | 6 | 0 | 0 |  | 6 | 0 | 0 | 0 |  | 0 | 0 | 3 | 0 |  | 3 | - |
| Single-Unit Trucks \% | 0.9\% | 0\% | 0\% |  | 0.9\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.5\% | 0\% |  | 0.5\% | - |
| Buses | 4 | 0 | 0 |  | 4 | 0 | 0 | 0 |  | 0 | 0 | 6 | 0 |  | 6 | - |
| Buses \% | 0.6\% | 0\% | 0\% |  | 0.6\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1\% | 0\% |  | 1\% | - |
| Articulated Trucks | 1 | 0 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0.2\% | 0\% | 0\% |  | 0.2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 14 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 93.3\% |  | - | - | - | 0\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 6.7\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 1 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 08:00 AM-09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ )


## Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds (20.46 $\left.{ }^{\circ} \mathrm{C}\right)$



| Turning Movement Count (3. QUEEN ST N \& 40 QUEEN ST N NORTH DRIVEWAY) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  |  | W Approach 40 QUEEN ST N NORTH DRIVEWAY |  |  |  | Int. Total (15 min) | Int. Total (1 hr) |
|  | Right $\mathrm{N}: \mathrm{W}$ | Thru $\mathrm{N}: \mathrm{S}$ | UTurn $\mathrm{N}: \mathrm{N}$ | Peds N : | Approach Total | Thru S:N | Left S:W | UTurn S:S | Peds S: | Approach Total | Right W:S | Left W:N | UTurn W:W | Peds W: | Approach Total |  |  |
| 07:00:00 | 0 | 48 | 0 | 0 | 48 | 52 | 0 | 0 | 0 | 52 | 0 | 0 | 0 | 0 | 0 | 100 |  |
| 07:15:00 | 0 | 86 | 0 | 0 | 86 | 86 | 1 | 0 | 0 | 87 | 0 | 0 | 0 | 0 | 0 | 173 |  |
| 07:30:00 | 2 | 81 | 0 | 0 | 83 | 73 | 0 | 0 | 0 | 73 | 0 | 0 | 0 | 0 | 0 | 156 |  |
| 07:45:00 | 0 | 122 | 0 | 0 | 122 | 123 | 0 | 0 | 0 | 123 | 0 | 0 | 0 | 0 | 0 | 245 | 674 |
| 08:00:00 | 1 | 117 | 0 | 0 | 118 | 145 | 0 | 0 | 0 | 145 | 0 | 0 | 0 | 0 | 0 | 263 | 837 |
| 08:15:00 | 0 | 134 | 0 | 0 | 134 | 219 | 0 | 0 | 0 | 219 | 0 | 0 | 0 | 0 | 0 | 353 | 1017 |
| 08:30:00 | 1 | 152 | 0 | 0 | 153 | 167 | 0 | 0 | 0 | 167 | 0 | 0 | 0 | 1 | 0 | 320 | 1181 |
| 08:45:00 | 0 | 142 | 0 | 0 | 142 | 144 | 1 | 0 | 0 | 145 | 0 | 0 | 0 | 1 | 0 | 287 | 1223 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 0 | 138 | 0 | 0 | 138 | 128 | 0 | 0 | 0 | 128 | 0 | 0 | 0 | 0 | 0 | 266 |  |
| 16:15:00 | 1 | 155 | 0 | 0 | 156 | 107 | 1 | 0 | 0 | 108 | 0 | 0 | 0 | 0 | 0 | 264 |  |
| 16:30:00 | 3 | 142 | 0 | 0 | 145 | 136 | 0 | 0 | 0 | 136 | 0 | 1 | 0 | 0 | 1 | 282 |  |
| 16:45:00 | 0 | 143 | 0 | 0 | 143 | 141 | 2 | 0 | 0 | 143 | 2 | 0 | 0 | 1 | 2 | 288 | 1100 |
| 17:00:00 | 0 | 173 | 0 | 0 | 173 | 168 | 0 | 0 | 0 | 168 | 2 | 1 | 0 | 0 | 3 | 344 | 1178 |
| 17:15:00 | 0 | 186 | 0 | 0 | 186 | 148 | 1 | 0 | 0 | 149 | 1 | 0 | 0 | 0 | 1 | 336 | 1250 |
| 17:30:00 | 1 | 142 | 0 | 0 | 143 | 142 | 1 | 0 | 0 | 143 | 0 | 0 | 0 | 0 | 0 | 286 | 1254 |
| 17:45:00 | 1 | 132 | 0 | 3 | 133 | 123 | 0 | 0 | 0 | 123 | 0 | 0 | 0 | 4 | 0 | 256 | 1222 |
| Grand Total | 10 | 2093 | 0 | 3 | 2103 | 2102 | 7 | 0 | 0 | 2109 | 5 | 2 | 0 | 7 | 7 | 4219 | - |
| Approach\% | 0.5\% | 99.5\% | 0\% |  | - | 99.7\% | 0.3\% | 0\% |  | - | 71.4\% | 28.6\% | 0\% |  | - | - | - |
| Totals \% | 0.2\% | 49.6\% | 0\% |  | 49.8\% | 49.8\% | 0.2\% | 0\% |  | 50\% | 0.1\% | 0\% | 0\% |  | 0.2\% | - | - |
| Heavy | 0 | 75 | 0 |  | - | 57 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | - | - |
| Heavy \% | 0\% | 3.6\% | 0\% |  | - | 2.7\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | - |
| Bicycles | 0 | 2 | 0 |  | - | 2 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | - | - |
| Bicycle \% | 0\% | 0.1\% | 0\% |  | - | 0.1\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | - |

BA Grou TORONTO ONTARIO, M4V 1K canada

| Peak Hour: 08:00 AM - 09:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach 40 QUEEN ST N NORTH DRIVEWAY |  |  |  |  | Int. Total ( 15 min ) |
|  | Right | Thru | UTurn | Peds | Approach Total | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total |  |
| 08:00:00 | 1 | 117 | 0 | 0 | 118 | 145 | 0 | 0 | 0 | 145 | 0 | 0 | 0 | 0 | 0 | 263 |
| 08:15:00 | 0 | 134 | 0 | 0 | 134 | 219 | 0 | 0 | 0 | 219 | 0 | 0 | 0 | 0 | 0 | 353 |
| 08:30:00 | 1 | 152 | 0 | 0 | 153 | 167 | 0 | 0 | 0 | 167 | 0 | 0 | 0 | 1 | 0 | 320 |
| 08:45:00 | 0 | 142 | 0 | 0 | 142 | 144 | 1 | 0 | 0 | 145 | 0 | 0 | 0 | 1 | 0 | 287 |
| Grand Total | 2 | 545 | 0 | 0 | 547 | 675 | 1 | 0 | 0 | 676 | 0 | 0 | 0 | 2 | 0 | 1223 |
| Approach\% | 0.4\% | 99.6\% | 0\% |  | - | 99.9\% | 0.1\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - |
| Totals \% | 0.2\% | 44.6\% | 0\% |  | 44.7\% | 55.2\% | 0.1\% | 0\% |  | 55.3\% | 0\% | 0\% | 0\% |  | 0\% | - |
| PHF | 0.5 | 0.9 | 0 |  | 0.89 | 0.77 | 0.25 | 0 |  | 0.77 | 0 | 0 | 0 |  | 0 | - |
| Heavy | 0 | 27 | 0 |  | 27 | 18 | 0 | 0 |  | 18 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 5\% | 0\% |  | 4.9\% | 2.7\% | 0\% | 0\% |  | 2.7\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 2 | 518 | 0 |  | 520 | 657 | 1 | 0 |  | 658 | 0 | 0 | 0 |  | 0 | - |
| Lights \% | 100\% | 95\% | 0\% |  | 95.1\% | 97.3\% | 100\% | 0\% |  | 97.3\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Single-Unit Trucks | 0 | 10 | 0 |  | 10 | 6 | 0 | 0 |  | 6 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 1.8\% | 0\% |  | 1.8\% | 0.9\% | 0\% | 0\% |  | 0.9\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 13 | 0 |  | 13 | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 2.4\% | 0\% |  | 2.4\% | 1.5\% | 0\% | 0\% |  | 1.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Articulated Trucks | 0 | 4 | 0 |  | 4 | 2 | 0 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0.7\% | 0\% |  | 0.7\% | 0.3\% | 0\% | 0\% |  | 0.3\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 2 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 100\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

30045 ST BA Group TORONTO ONTARIO, M4V 1K9 CANADA

Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds ( $20.46{ }^{\circ} \mathrm{C}$

| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach 40 QUEEN ST N NORTH DRIVEWAY |  |  |  |  | Int. Total (15 min) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | UTurn | Peds | Approach Total | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total |  |
| 16:45:00 | 0 | 143 | 0 | 0 | 143 | 141 | 2 | 0 | 0 | 143 | 2 | 0 | 0 | 1 | 2 | 288 |
| 17:00:00 | 0 | 173 | 0 | 0 | 173 | 168 | 0 | 0 | 0 | 168 | 2 | 1 | 0 | 0 | 3 | 344 |
| 17:15:00 | 0 | 186 | 0 | 0 | 186 | 148 | 1 | 0 | 0 | 149 | 1 | 0 | 0 | 0 | 1 | 336 |
| 17:30:00 | 1 | 142 | 0 | 0 | 143 | 142 | 1 | 0 | 0 | 143 | 0 | 0 | 0 | 0 | 0 | 286 |
| Grand Total | 1 | 644 | 0 | 0 | 645 | 599 | 4 | 0 | 0 | 603 | 5 | 1 | 0 | 1 | 6 | 1254 |
| Approach\% | 0.2\% | 99.8\% | 0\% |  | - | 99.3\% | 0.7\% | 0\% |  | - | 83.3\% | 16.7\% | 0\% |  | - | - |
| Totals \% | 0.1\% | 51.4\% | 0\% |  | 51.4\% | 47.8\% | 0.3\% | 0\% |  | 48.1\% | 0.4\% | 0.1\% | 0\% |  | 0.5\% | - |
| PHF | 0.25 | 0.87 | 0 |  | 0.87 | 0.89 | 0.5 | 0 |  | 0.9 | 0.63 | 0.25 | 0 |  | 0.5 | - |
| Heavy | 0 | 11 | 0 |  | 11 | 9 | 0 | 0 |  | 9 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 1.7\% | 0\% |  | 1.7\% | 1.5\% | 0\% | 0\% |  | 1.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 1 | 633 | 0 |  | 634 | 590 | 4 | 0 |  | 594 | 5 | 1 | 0 |  | 6 | - |
| Lights \% | 100\% | 98.3\% | 0\% |  | 98.3\% | 98.5\% | 100\% | 0\% |  | 98.5\% | 100\% | 100\% | 0\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 5 | 0 |  | 5 | 3 | 0 | 0 |  | 3 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0.8\% | 0\% |  | 0.8\% | 0.5\% | 0\% | 0\% |  | 0.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 5 | 0 |  | 5 | 6 | 0 | 0 |  | 6 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 0.8\% | 0\% |  | 0.8\% | 1\% | 0\% | 0\% |  | 1\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Articulated Trucks | 0 | 1 | 0 |  | 1 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0.2\% | 0\% |  | 0.2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 1 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 100\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 08:00 AM - 09:00 AM Weather: Clear Sky ( $13.73^{\circ} \mathrm{C}$ )


## Peak Hour: 04:45 PM - 05:45 PM Weather: Scattered Clouds ( $20.46{ }^{\circ} \mathrm{C}$ )



| Turning Movement Count (4. QUEEN ST N \& 40 QUEEN ST N SOUTH DRIVEWAY) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach 40 QUEEN ST N SOUTH DRIVEWAY |  |  |  |  | Int. Total (15 min) | Int. Total ( 1 hr ) |
|  | Right $\mathrm{N}: \mathrm{W}$ | Thru $\mathrm{N}: \mathrm{S}$ | UTurn $\mathrm{N}: \mathrm{N}$ | $\begin{aligned} & \text { Peds } \\ & \mathrm{N}: \end{aligned}$ | Approach Total | Thru $\mathrm{S}: \mathrm{N}$ | $\begin{aligned} & \text { Left } \\ & \text { S:W } \end{aligned}$ | $\begin{aligned} & \text { UTurn } \\ & \text { S:S } \end{aligned}$ | Peds S: | Approach Total | Right W:S | Left <br> W:N | UTurn W:W | Peds W: | Approach Total |  |  |
| 07:00:00 | 0 | 51 | 0 | 0 | 51 | 52 | 1 | 0 | 0 | 53 | 0 | 0 | 0 | 0 | 0 | 104 |  |
| 07:15:00 | 0 | 84 | 0 | 0 | 84 | 85 | 0 | 0 | 0 | 85 | 0 | 1 | 0 | 0 | 1 | 170 |  |
| 07:30:00 | 0 | 81 | 0 | 0 | 81 | 74 | 1 | 0 | 0 | 75 | 0 | 0 | 0 | 0 | 0 | 156 |  |
| 07:45:00 | 0 | 118 | 0 | 0 | 118 | 120 | 0 | 0 | 0 | 120 | 0 | 0 | 0 | 0 | 0 | 238 | 668 |
| 08:00:00 | 1 | 118 | 0 | 0 | 119 | 139 | 0 | 0 | 0 | 139 | 0 | 1 | 0 | 0 | 1 | 259 | 823 |
| 08:15:00 | 0 | 133 | 0 | 0 | 133 | 216 | 0 | 0 | 0 | 216 | 0 | 0 | 0 | 0 | 0 | 349 | 1002 |
| 08:30:00 | 0 | 148 | 0 | 0 | 148 | 170 | 0 | 0 | 0 | 170 | 0 | 0 | 0 | 2 | 0 | 318 | 1164 |
| 08:45:00 | 0 | 142 | 0 | 0 | 142 | 147 | 0 | 0 | 0 | 147 | 0 | 0 | 0 | 1 | 0 | 289 | 1215 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 0 | 141 | 0 | 0 | 141 | 127 | 0 | 1 | 0 | 128 | 0 | 0 | 0 | 0 | 0 | 269 |  |
| 16:15:00 | 0 | 146 | 0 | 0 | 146 | 110 | 0 | 0 | 0 | 110 | 1 | 0 | 0 | 0 | 1 | 257 |  |
| 16:30:00 | 0 | 149 | 0 | 0 | 149 | 135 | 0 | 0 | 0 | 135 | 0 | 3 | 0 | 1 | 3 | 287 |  |
| 16:45:00 | 1 | 143 | 0 | 0 | 144 | 135 | 0 | 0 | 0 | 135 | 2 | 1 | 0 | 1 | 3 | 282 | 1095 |
| 17:00:00 | 1 | 174 | 0 | 0 | 175 | 173 | 2 | 0 | 0 | 175 | 1 | 0 | 0 | 0 | 1 | 351 | 1177 |
| 17:15:00 | 0 | 189 | 0 | 0 | 189 | 149 | 0 | 0 | 0 | 149 | 1 | 0 | 0 | 0 | 1 | 339 | 1259 |
| 17:30:00 | 0 | 140 | 0 | 0 | 140 | 135 | 0 | 0 | 0 | 135 | 1 | 0 | 0 | 1 | 1 | 276 | 1248 |
| 17:45:00 | 2 | 128 | 0 | 0 | 130 | 130 | 0 | 0 | 0 | 130 | 1 | 1 | 0 | 4 | 2 | 262 | 1228 |
| Grand Total | 5 | 2085 | 0 | 0 | 2090 | 2097 | 4 | 1 | 0 | 2102 | 7 | 7 | 0 | 10 | 14 | 4206 | - |
| Approach\% | 0.2\% | 99.8\% | 0\% |  | - | 99.8\% | 0.2\% | 0\% |  | - | 50\% | 50\% | 0\% |  | - | - | - |
| Totals \% | 0.1\% | 49.6\% | 0\% |  | 49.7\% | 49.9\% | 0.1\% | 0\% |  | 50\% | 0.2\% | 0.2\% | 0\% |  | 0.3\% | - | - |
| Heavy | 0 | 72 | 0 |  | - | 57 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | - | - |
| Heavy \% | 0\% | 3.5\% | 0\% |  | - | 2.7\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | - |
| Bicycles | 0 | 2 | 0 |  | - | 3 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | - | - |
| Bicycle \% | 0\% | 0.1\% | 0\% |  | - | 0.1\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | - |

BA Grou TORONTO ONTARIO, M4V 1K CANADA

| Peak Hour: 08:00 AM - 09:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach 40 QUEEN ST N SOUTH DRIVEWAY |  |  |  |  | Int. Total (15 min) |
|  | Right | Thru | UTurn | Peds | Approach Total | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total |  |
| 08:00:00 | 1 | 118 | 0 | 0 | 119 | 139 | 0 | 0 | 0 | 139 | 0 | 1 | 0 | 0 | 1 | 259 |
| 08:15:00 | 0 | 133 | 0 | 0 | 133 | 216 | 0 | 0 | 0 | 216 | 0 | 0 | 0 | 0 | 0 | 349 |
| 08:30:00 | 0 | 148 | 0 | 0 | 148 | 170 | 0 | 0 | 0 | 170 | 0 | 0 | 0 | 2 | 0 | 318 |
| 08:45:00 | 0 | 142 | 0 | 0 | 142 | 147 | 0 | 0 | 0 | 147 | 0 | 0 | 0 | 1 | 0 | 289 |
| Grand Total | 1 | 541 | 0 | 0 | 542 | 672 | 0 | 0 | 0 | 672 | 0 | 1 | 0 | 3 | 1 | 1215 |
| Approach\% | 0.2\% | 99.8\% | 0\% |  | - | 100\% | 0\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | - |
| Totals \% | 0.1\% | 44.5\% | 0\% |  | 44.6\% | 55.3\% | 0\% | 0\% |  | 55.3\% | 0\% | 0.1\% | 0\% |  | 0.1\% | - |
| PHF | 0.25 | 0.91 | 0 |  | 0.92 | 0.78 | 0 | 0 |  | 0.78 | 0 | 0.25 | 0 |  | 0.25 | - |
| Heavy | 0 | 23 | 0 |  | 23 | 18 | 0 | 0 |  | -18 | 0 | 0 | 0 |  | 0 | - |
| Heavy \% | 0\% | 4.3\% | 0\% |  | 4.2\% | 2.7\% | 0\% | 0\% |  | 2.7\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 1 | 518 | 0 |  | 519 | 654 | 0 | 0 |  | 654 | 0 | 1 | 0 |  | 1 | - |
| Lights \% | 100\% | 95.7\% | 0\% |  | 95.8\% | 97.3\% | 0\% | 0\% |  | 97.3\% | 0\% | 100\% | 0\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 10 | 0 |  | 10 | 6 | 0 | 0 |  | 6 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 1.8\% | 0\% |  | 1.8\% | 0.9\% | 0\% | 0\% |  | 0.9\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 11 | 0 |  | 11 | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 2\% | 0\% |  | 2\% | 1.5\% | 0\% | 0\% |  | 1.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Articulated Trucks | 0 | 2 | 0 |  | 2 | 2 | 0 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0.4\% | 0\% |  | 0.4\% | 0.3\% | 0\% | 0\% |  | 0.3\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 3 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 100\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

00045 ST BA Group TORONTO ONTARIO, M4V 1K CANADA

Peak Hour: 04:30 PM - 05:30 PM Weather: Scattered Clouds (20.46 $\left.{ }^{\circ} \mathrm{C}\right)$

| Start Time | N Approach QUEEN ST N |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | W Approach 40 QUEEN ST N SOUTH DRIVEWAY |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Right | Thru | UTurn | Peds | Approach Total | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total |  |
| 16:30:00 | 0 | 149 | 0 | 0 | 149 | 135 | 0 | 0 | 0 | 135 | 0 | 3 | 0 | 1 | 3 | 287 |
| 16:45:00 | 1 | 143 | 0 | 0 | 144 | 135 | 0 | 0 | 0 | 135 | 2 | 1 | 0 | 1 | 3 | 282 |
| 17:00:00 | 1 | 174 | 0 | 0 | 175 | 173 | 2 | 0 | 0 | 175 | 1 | 0 | 0 | 0 | 1 | 351 |
| 17:15:00 | 0 | 189 | 0 | 0 | 189 | 149 | 0 | 0 | 0 | 149 | 1 | 0 | 0 | 0 | 1 | 339 |
| Grand Total | 2 | 655 | 0 | 0 | 657 | 592 | 2 | 0 | 0 | 594 | 4 | 4 | 0 | 2 | 8 | 1259 |
| Approach\% | 0.3\% | 99.7\% | 0\% |  | - | 99.7\% | 0.3\% | 0\% |  | - | 50\% | 50\% | 0\% |  | - | - |
| Totals \% | 0.2\% | 52\% | 0\% |  | 52.2\% | 47\% | 0.2\% | 0\% |  | 47.2\% | 0.3\% | 0.3\% | 0\% |  | 0.6\% | - |
| PHF | 0.5 | 0.87 | 0 |  | 0.87 | 0.86 | 0.25 | 0 |  | 0.85 | 0.5 | 0.33 | 0 |  | 0.67 | - |
| Heavy | 0 | 10 | 0 |  | 10 | 7 | 0 | 0 |  | 7 | 0 | 0 | 0 |  | 0 | -- |
| Heavy \% | 0\% | 1.5\% | 0\% |  | 1.5\% | 1.2\% | 0\% | 0\% |  | 1.2\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Lights | 2 | 645 | 0 |  | 647 | 585 | 2 | 0 |  | 587 | 4 | 4 | 0 |  | 8 | - |
| Lights \% | 100\% | 98.5\% | 0\% |  | 98.5\% | 98.8\% | 100\% | 0\% |  | 98.8\% | 100\% | 100\% | 0\% |  | 100\% | - |
| Single-Unit Trucks | 0 | 4 | 0 |  | 4 | 3 | 0 | 0 |  | 3 | 0 | 0 | 0 |  | 0 | - |
| Single-Unit Trucks \% | 0\% | 0.6\% | 0\% |  | 0.6\% | 0.5\% | 0\% | 0\% |  | 0.5\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Buses | 0 | 6 | 0 |  | 6 | 4 | 0 | 0 |  | 4 | 0 | 0 | 0 |  | 0 | - |
| Buses \% | 0\% | 0.9\% | 0\% |  | 0.9\% | 0.7\% | 0\% | 0\% |  | 0.7\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Articulated Trucks | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 1 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 50\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 0 | - | - | - | - | 1 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 50\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 1 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

Peak Hour: 08:00 AM - 09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ )


## Peak Hour: 04:30 PM - 05:30 PM Weather: Scattered Clouds (20.46 ${ }^{\circ}$ C)



## Turning Movement Count (1. QUEEN ST N \& 51 QUEEN ST N (NORTH DRIVEWAY 1))

| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 51 QUEEN ST N (NORTH DRIVEWAY 1) |  |  |  |  |  | S Approach QUEEN ST N |  |  |  | Int. Total ( 15 min ) | Int. Total ( 1 hr ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thru $\mathrm{N}: \mathrm{S}$ | Left $\mathrm{N}: \mathrm{E}$ | UTurn $\mathrm{N}: \mathrm{N}$ | Peds N : | Approach Total | Right E:N | Left E:S | UTurn E:E | $\begin{aligned} & \text { Peds } \\ & \text { E: } \end{aligned}$ | Approach Total | $\begin{aligned} & \text { Right } \\ & \text { S:E } \end{aligned}$ | Thru S:N | $\begin{aligned} & \text { UTurn } \\ & \mathrm{S}: \mathrm{S} \end{aligned}$ | Peds S: | Approach Total |  |  |
| 07:00:00 | 83 | 0 | 0 | 0 | 83 | 0 | 0 | 0 | 2 | 0 | 0 | 52 | 0 | 0 | 52 | 135 |  |
| 07:15:00 | 51 | 0 | 0 | 0 | 51 | 0 | 0 | 0 | 3 | 0 | 0 | 84 | 0 | 0 | 84 | 135 |  |
| 07:30:00 | 84 | 0 | 0 | 0 | 84 | 1 | 0 | 0 | 1 | 1 | 0 | 73 | 0 | 0 | 73 | 158 |  |
| 07:45:00 | 118 | 0 | 0 | 0 | 118 | 0 | 0 | 0 | 1 | 0 | 0 | 120 | 0 | 0 | 120 | 238 | 666 |
| 08:00:00 | 121 | 0 | 0 | 0 | 121 | 0 | 0 | 0 | 1 | 0 | 0 | 140 | 0 | 0 | 140 | 261 | 792 |
| 08:15:00 | 131 | 0 | 0 | 0 | 131 | 0 | 1 | 0 | 1 | 1 | 0 | 215 | 0 | 0 | 215 | 347 | 1004 |
| 08:30:00 | 148 | 0 | 0 | 0 | 148 | 0 | 0 | 0 | 3 | 0 | 0 | 171 | 0 | 1 | 171 | 319 | 1165 |
| 08:45:00 | 144 | 0 | 0 | 0 | 144 | 0 | 0 | 0 | 0 | 0 | 0 | 144 | 0 | 0 | 144 | 288 | 1215 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 136 | 1 | 0 | 0 | 137 | 1 | 0 | 0 | 0 | 1 | 0 | 126 | 0 | 0 | 126 | 264 |  |
| 16:15:00 | 156 | 0 | 0 | 0 | 156 | 0 | 0 | 0 | 1 | 0 | 0 | 109 | 0 | 0 | 109 | 265 |  |
| 16:30:00 | 146 | 2 | 0 | 0 | 148 | 0 | 2 | 0 | 1 | 2 | 0 | 139 | 0 | 0 | 139 | 289 |  |
| 16:45:00 | 139 | 1 | 0 | 0 | 140 | 0 | 0 | 0 | 7 | 0 | 0 | 138 | 0 | 0 | 138 | 278 | 1096 |
| 17:00:00 | 173 | 0 | 0 | 0 | 173 | 0 | 1 | 0 | 2 | 1 | 0 | 170 | 0 | 0 | 170 | 344 | 1176 |
| 17:15:00 | 186 | 0 | 0 | 0 | 186 | 1 | 1 | 0 | 3 | 2 | 0 | 150 | 0 | 0 | 150 | 338 | 1249 |
| 17:30:00 | 141 | 0 | 0 | 0 | 141 | 0 | 0 | 0 | 2 | 0 | 0 | 135 | 0 | 0 | 135 | 276 | 1236 |
| 17:45:00 | 136 | 0 | 0 | 3 | 136 | 0 | 0 | 0 | 0 | 0 | 0 | 127 | 0 | 0 | 127 | 263 | 1221 |
| Grand Total | 2093 | 4 | 0 | 3 | 2097 | 3 | 5 | 0 | 28 | 8 | 0 | 2093 | 0 | 1 | 2093 | 4198 | - |
| Approach\% | 99.8\% | 0.2\% | 0\% |  | - | 37.5\% | 62.5\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | - | - |
| Totals \% | 49.9\% | 0.1\% | 0\% |  | 50\% | 0.1\% | 0.1\% | 0\% |  | 0.2\% | 0\% | 49.9\% | 0\% |  | 49.9\% | - | - |
| Heavy | 72 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | 0 | 57 | 0 |  | - | - | - |
| Heavy \% | 3.4\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0\% | 2.7\% | 0\% |  | - | - | - |
| Bicycles | 2 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | 1 | 1 | 0 |  | - | - | - |
| Bicycle \% | 0.1\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | - | - |


| Peak Hour: 08:00 AM - 09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach51 QUEEN ST N (NORTH DRIVEWAY 1) |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) |
|  | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total | Right | Thru | UTurn | Peds | Approach Total |  |
| 08:00:00 | 121 | 0 | 0 | 0 | 121 | 0 | 0 | 0 | 1 | 0 | 0 | 140 | 0 | 0 | 140 | 261 |
| 08:15:00 | 131 | 0 | 0 | 0 | 131 | 0 | 1 | 0 | 1 | 1 | 0 | 215 | 0 | 0 | 215 | 347 |
| 08:30:00 | 148 | 0 | 0 | 0 | 148 | 0 | 0 | 0 | 3 | 0 | 0 | 171 | 0 | 1 | 171 | 319 |
| 08:45:00 | 144 | 0 | 0 | 0 | 144 | 0 | 0 | 0 | 0 | 0 | 0 | 144 | 0 | 0 | 144 | 288 |
| Grand Total | 544 | 0 | 0 | 0 | 544 | 0 | 1 | 0 | 5 | 1 | 0 | 670 | 0 | 1 | 670 | 1215 |
| Approach\% | 100\% | 0\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | - |
| Totals \% | 44.8\% | 0\% | 0\% |  | 44.8\% | 0\% | 0.1\% | 0\% |  | 0.1\% | 0\% | 55.1\% | 0\% |  | 55.1\% | - |
| PHF | 0.92 | 0 | 0 |  | 0.92 | 0 | 0.25 | 0 |  | 0.25 | 0 | 0.78 | 0 |  | 0.78 | - |
| Heavy | 23 | 0 | 0 |  | 23 | 0 | 0 | 0 |  | 0 | 0 | 18 | 0 |  | 18 | - |
| Heavy \% | 4.2\% | 0\% | 0\% |  | 4.2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 2.7\% | 0\% |  | 2.7\% | - |
| Lights | 521 | 0 | 0 |  | 521 | 0 | 1 | 0 |  | 1 | 0 | 652 | 0 |  | 652 | - |
| Lights \% | 95.8\% | 0\% | 0\% |  | 95.8\% | 0\% | 100\% | 0\% |  | 100\% | 0\% | 97.3\% | 0\% |  | 97.3\% | - |
| Single-Unit Trucks | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | 0 | 6 | 0 |  | 6 | - |
| Single-Unit Trucks \% | 1.8\% | 0\% | 0\% |  | 1.8\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.9\% | 0\% |  | 0.9\% | - |
| Buses | 11 | 0 | 0 |  | 11 | 0 | 0 | 0 |  | 0 | 0 | 10 | 0 |  | 10 | - |
| Buses \% | 2\% | 0\% | 0\% |  | 2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1.5\% | 0\% |  | 1.5\% | - |
| Articulated Trucks | 2 | 0 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | 0 | 2 | 0 |  | 2 | - |
| Articulated Trucks \% | 0.4\% | 0\% | 0\% |  | 0.4\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.3\% | 0\% |  | 0.3\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 4 | - | - | - | - | 1 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 66.7\% |  | - | - | - | 16.7\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 16.7\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |


| Peak Hour: 04:30 PM - 05:30 PM Weather: Scattered Clouds (20.46 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 51 QUEEN ST N (NORTH DRIVEWAY 1) |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) |
|  | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total | Right | Thru | UTurn | Peds | Approach Total |  |
| 16:30:00 | 146 | 2 | 0 | 0 | 148 | 0 | 2 | 0 | 1 | 2 | 0 | 139 | 0 | 0 | 139 | 289 |
| 16:45:00 | 139 | 1 | 0 | 0 | 140 | 0 | 0 | 0 | 7 | 0 | 0 | 138 | 0 | 0 | 138 | 278 |
| 17:00:00 | 173 | 0 | 0 | 0 | 173 | 0 | 1 | 0 | 2 | 1 | 0 | 170 | 0 | 0 | 170 | 344 |
| 17:15:00 | 186 | 0 | 0 | 0 | 186 | 1 | 1 | 0 | 3 | 2 | 0 | 150 | 0 | 0 | 150 | 338 |
| Grand Total | 644 | 3 | 0 | 0 | 647 | 1 | 4 | 0 | 13 | 5 | 0 | 597 | 0 | 0 | 597 | 1249 |
| Approach\% | 99.5\% | 0.5\% | 0\% |  | - | 20\% | 80\% | 0\% |  | - | 0\% | 100\% | 0\% |  | - | - |
| Totals \% | 51.6\% | 0.2\% | 0\% |  | 51.8\% | 0.1\% | 0.3\% | 0\% |  | 0.4\% | 0\% | 47.8\% | 0\% |  | 47.8\% | - |
| PHF | 0.87 | 0.38 | 0 |  | 0.87 | 0.25 | 0.5 | 0 |  | 0.63 | 0 | 0.88 | 0 |  | 0.88 | - |
| Heavy | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | 0 | 7 | 0 |  | 7 | - |
| Heavy \% | 1.6\% | 0\% | 0\% |  | 1.5\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1.2\% | 0\% |  | 1.2\% | - |
| Lights | 634 | 3 | 0 |  | 637 | 1 | 4 | 0 |  | 5 | 0 | 590 | 0 |  | 590 | - |
| Lights \% | 98.4\% | 100\% | 0\% |  | 98.5\% | 100\% | 100\% | 0\% |  | 100\% | 0\% | 98.8\% | 0\% |  | 98.8\% | - |
| Single-Unit Trucks | 4 | 0 | 0 |  | 4 | 0 | 0 | 0 |  | 0 | 0 | 3 | 0 |  | 3 | - |
| Single-Unit Trucks \% | 0.6\% | 0\% | 0\% |  | 0.6\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.5\% | 0\% |  | 0.5\% | - |
| Buses | 6 | 0 | 0 |  | 6 | 0 | 0 | 0 |  | 0 | 0 | 4 | 0 |  | 4 | - |
| Buses \% | 0.9\% | 0\% | 0\% |  | 0.9\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.7\% | 0\% |  | 0.7\% | - |
| Articulated Trucks | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 10 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 76.9\% |  | - | - | - | 0\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 3 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 23.1\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 08:00 AM - 09:00 AM Weather: Clear Sky (13.73 $\left.{ }^{\circ} \mathrm{C}\right)$



## Peak Hour: 04:30 PM - 05:30 PM Weather: Scattered Clouds (20.46 ${ }^{\circ} \mathrm{C}$ )



| Turning Movement Count (2. QUEEN ST N \& 51 QUEEN ST N (SOUTH DRIVEWAY 2)) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 51 QUEEN ST N (SOUTH DRIVEWAY) |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total (15 min) | $\begin{aligned} & \text { Int. Total } \\ & (1 \mathrm{hr}) \end{aligned}$ |
|  | Thru $\mathrm{N}: \mathrm{S}$ | $\begin{aligned} & \text { Left } \\ & \mathrm{N}: \mathrm{E} \end{aligned}$ | UTurn N:N | Peds N : | Approach Total | Right E:N | Left E:S | UTurn E:E | $\begin{aligned} & \text { Peds } \\ & \text { E: } \end{aligned}$ | Approach Total | $\begin{aligned} & \text { Right } \\ & \text { S:E } \end{aligned}$ | Thru S:N | UTurn s:S | Peds S: | Approach Total |  |  |
| 07:00:00 | 51 | 0 | 0 | 0 | 51 | 0 | 0 | 0 | 2 | 0 | 1 | 53 | 0 | 0 | 54 | 105 |  |
| 07:15:00 | 84 | 0 | 0 | 0 | 84 | 0 | 0 | 0 | 3 | 0 | 0 | 85 | 0 | 0 | 85 | 169 |  |
| 07:30:00 | 83 | 0 | 0 | 0 | 83 | 0 | 0 | 0 | 1 | 0 | 0 | 72 | 0 | 0 | 72 | 155 |  |
| 07:45:00 | 118 | 0 | 0 | 0 | 118 | 0 | 0 | 0 | 1 | 0 | 0 | 120 | 0 | 0 | 120 | 238 | 667 |
| 08:00:00 | 121 | 0 | 0 | 0 | 121 | 0 | 0 | 0 | 1 | 0 | 0 | 140 | 0 | 0 | 140 | 261 | 823 |
| 08:15:00 | 134 | 0 | 0 | 0 | 134 | 0 | 0 | 0 | 1 | 0 | 1 | 216 | 0 | 0 | 217 | 351 | 1005 |
| 08:30:00 | 148 | 0 | 0 | 0 | 148 | 0 | 0 | 0 | 3 | 0 | 0 | 171 | 0 | 1 | 171 | 319 | 1169 |
| 08:45:00 | 143 | 0 | 0 | 0 | 143 | 0 | 0 | 0 | 0 | 0 | 0 | 144 | 0 | 0 | 144 | 287 | 1218 |
| ***BREAK*** |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 16:00:00 | 135 | 1 | 0 | 0 | 136 | 0 | 0 | 0 | 0 | 0 | 0 | 126 | 0 | 0 | 126 | 262 |  |
| 16:15:00 | 155 | 0 | 0 | 0 | 155 | 0 | 0 | 0 | 1 | 0 | 0 | 109 | 0 | 0 | 109 | 264 |  |
| 16:30:00 | 148 | 0 | 0 | 0 | 148 | 0 | 0 | 0 | 1 | 0 | 0 | 139 | 0 | 0 | 139 | 287 |  |
| 16:45:00 | 140 | 0 | 0 | 0 | 140 | 0 | 0 | 0 | 7 | 0 | 0 | 137 | 0 | 0 | 137 | 277 | 1090 |
| 17:00:00 | 174 | 0 | 0 | 0 | 174 | 0 | 0 | 0 | 2 | 0 | 1 | 170 | 0 | 0 | 171 | 345 | 1173 |
| 17:15:00 | 187 | 0 | 0 | 0 | 187 | 0 | 0 | 0 | 3 | 0 | 0 | 150 | 0 | 0 | 150 | 337 | 1246 |
| 17:30:00 | 140 | 1 | 0 | 0 | 141 | 0 | 0 | 0 | 2 | 0 | 0 | 135 | 0 | 0 | 135 | 276 | 1235 |
| 17:45:00 | 136 | 1 | 0 | 3 | 137 | 0 | 0 | 0 | 0 | 0 | 1 | 127 | 0 | 0 | 128 | 265 | 1223 |
| Grand Total | 2097 | 3 | 0 | 3 | 2100 | 0 | 0 | 0 | 28 | 0 | 4 | 2094 | 0 | 1 | 2098 | 4198 | - |
| Approach\% | 99.9\% | 0.1\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0.2\% | 99.8\% | 0\% |  | - | - | - |
| Totals \% | 50\% | 0.1\% | 0\% |  | 50\% | 0\% | 0\% | 0\% |  | 0\% | 0.1\% | 49.9\% | 0\% |  | 50\% | - | - |
| Heavy | 72 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | 0 | 57 | 0 |  | - | - | - |
| Heavy \% | 3.4\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0\% | 2.7\% | 0\% |  | - | - | - |
| Bicycles | 2 | 0 | 0 |  | - | 0 | 0 | 0 |  | - | 0 | 2 | 0 |  | - | - | - |
| Bicycle \% | 0.1\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0\% | 0.1\% | 0\% |  | - | - | - |


| Peak Hour: 08:00 AM - 09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 51 QUEEN ST N (SOUTH DRIVEWAY) |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) |
|  | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total | Right | Thru | UTurn | Peds | Approach Total |  |
| 08:00:00 | 121 | 0 | 0 | 0 | 121 | 0 | 0 | 0 | 1 | 0 | 0 | 140 | 0 | 0 | 140 | 261 |
| 08:15:00 | 134 | 0 | 0 | 0 | 134 | 0 | 0 | 0 | 1 | 0 | 1 | 216 | 0 | 0 | 217 | 351 |
| 08:30:00 | 148 | 0 | 0 | 0 | 148 | 0 | 0 | 0 | 3 | 0 | 0 | 171 | 0 | 1 | 171 | 319 |
| 08:45:00 | 143 | 0 | 0 | 0 | 143 | 0 | 0 | 0 | 0 | 0 | 0 | 144 | 0 | 0 | 144 | 287 |
| Grand Total | 546 | 0 | 0 | 0 | 546 | 0 | 0 | 0 | 5 | 0 | 1 | 671 | 0 | 1 | 672 | 1218 |
| Approach\% | 100\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0.1\% | 99.9\% | 0\% |  | - | - |
| Totals \% | 44.8\% | 0\% | 0\% |  | 44.8\% | 0\% | 0\% | 0\% |  | 0\% | 0.1\% | 55.1\% | 0\% |  | 55.2\% | - |
| PHF | 0.92 | 0 | 0 |  | 0.92 | 0 | 0 | 0 |  | 0 | 0.25 | 0.78 | 0 |  | 0.77 | - |
| Heavy | 23 | 0 | 0 |  | 23 | 0 | 0 | 0 |  | 0 | 0 | 18 | 0 |  | 18 | - |
| Heavy \% | 4.2\% | 0\% | 0\% |  | 4.2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 2.7\% | 0\% |  | 2.7\% | - |
| Lights | 523 | 0 | 0 |  | 523 | 0 | 0 | 0 |  | 0 | 1 | 653 | 0 |  | 654 | - |
| Lights \% | 95.8\% | 0\% | 0\% |  | 95.8\% | 0\% | 0\% | 0\% |  | 0\% | 100\% | 97.3\% | 0\% |  | 97.3\% | - |
| Single-Unit Trucks | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | 0 | 6 | 0 |  | 6 | - |
| Single-Unit Trucks \% | 1.8\% | 0\% | 0\% |  | 1.8\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.9\% | 0\% |  | 0.9\% | - |
| Buses | 11 | 0 | 0 |  | 11 | 0 | 0 | 0 |  | 0 | 0 | 10 | 0 |  | 10 | - |
| Buses \% | 2\% | 0\% | 0\% |  | 2\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1.5\% | 0\% |  | 1.5\% | - |
| Articulated Trucks | 2 | 0 | 0 |  | 2 | 0 | 0 | 0 |  | 0 | 0 | 2 | 0 |  | 2 | - |
| Articulated Trucks \% | 0.4\% | 0\% | 0\% |  | 0.4\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.3\% | 0\% |  | 0.3\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 4 | - | - | - | - | 1 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 66.7\% |  | - | - | - | 16.7\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 1 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 16.7\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 04:30 PM - 05:30 PM Weather: Scattered Clouds ( $\left.20.46{ }^{\circ} \mathrm{C}\right)$

| Start Time | N Approach QUEEN ST N |  |  |  |  | E Approach 51 QUEEN ST N (SOUTH DRIVEWAY) |  |  |  |  | S Approach QUEEN ST N |  |  |  |  | Int. Total ( 15 min ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thru | Left | UTurn | Peds | Approach Total | Right | Left | UTurn | Peds | Approach Total | Right | Thru | UTurn | Peds | Approach Total |  |
| 16:30:00 | 148 | 0 | 0 | 0 | 148 | 0 | 0 | 0 | 1 | 0 | 0 | 139 | 0 | 0 | 139 | 287 |
| 16:45:00 | 140 | 0 | 0 | 0 | 140 | 0 | 0 | 0 | 7 | 0 | 0 | 137 | 0 | 0 | 137 | 277 |
| 17:00:00 | 174 | 0 | 0 | 0 | 174 | 0 | 0 | 0 | 2 | 0 | 1 | 170 | 0 | 0 | 171 | 345 |
| 17:15:00 | 187 | 0 | 0 | 0 | 187 | 0 | 0 | 0 | 3 | 0 | 0 | 150 | 0 | 0 | 150 | 337 |
| Grand Total | 649 | 0 | 0 | 0 | 649 | 0 | 0 | 0 | 13 | 0 | 1 | 596 | 0 | 0 | 597 | 1246 |
| Approach\% | 100\% | 0\% | 0\% |  | - | 0\% | 0\% | 0\% |  | - | 0.2\% | 99.8\% | 0\% |  | - | - |
| Totals \% | 52.1\% | 0\% | 0\% |  | 52.1\% | 0\% | 0\% | 0\% |  | 0\% | 0.1\% | 47.8\% | 0\% |  | 47.9\% | - |
| PHF | 0.87 | 0 | 0 |  | 0.87 | 0 | 0 | 0 |  | 0 | 0.25 | 0.88 | 0 |  | 0.87 | - |
| Heavy | 10 | 0 | 0 |  | 10 | 0 | 0 | 0 |  | 0 | 0 | 7 | 0 |  | 7 | - |
| Heavy \% | 1.5\% | 0\% | 0\% |  | 1.5\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 1.2\% | 0\% |  | 1.2\% | - |
| Lights | 639 | 0 | 0 |  | 639 | 0 | 0 | 0 |  | 0 | 1 | 589 | 0 |  | 590 | - |
| Lights \% | 98.5\% | 0\% | 0\% |  | 98.5\% | 0\% | 0\% | 0\% |  | 0\% | 100\% | 98.8\% | 0\% |  | 98.8\% | - |
| Single-Unit Trucks | 4 | 0 | 0 |  | 4 | 0 | 0 | 0 |  | 0 | 0 | 3 | 0 |  | 3 | - |
| Single-Unit Trucks \% | 0.6\% | 0\% | 0\% |  | 0.6\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.5\% | 0\% |  | 0.5\% | - |
| Buses | 6 | 0 | 0 |  | 6 | 0 | 0 | 0 |  | 0 | 0 | 4 | 0 |  | 4 | - |
| Buses \% | 0.9\% | 0\% | 0\% |  | 0.9\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0.7\% | 0\% |  | 0.7\% | - |
| Articulated Trucks | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  | 0 | - |
| Articulated Trucks \% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | 0\% | 0\% | 0\% |  | 0\% | - |
| Pedestrians | - | - | - | 0 | - | - | - | - | 10 | - | - | - | - | 0 | - | - |
| Pedestrians\% | - | - | - | 0\% |  | - | - | - | 76.9\% |  | - | - | - | 0\% |  | - |
| Bicycles on Crosswalk | - | - | - | 0 | - | - | - | - | 3 | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk\% | - | - | - | 0\% |  | - | - | - | 23.1\% |  | - | - | - | 0\% |  | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | 0 | 0 | 0 | 0 | - | - |
| Bicycles on Road\% | - | - | - | 0\% |  | - | - | - | 0\% |  | - | - | - | 0\% |  | - |

## Peak Hour: 08:00 AM-09:00 AM Weather: Clear Sky (13.73 ${ }^{\circ} \mathrm{C}$ )



## Peak Hour: 04:30 PM - 05:30 PM Weather: Scattered Clouds (20.46 ${ }^{\circ} \mathrm{C}$ )



Appendix G:
Corridor Growth Calculations

Date: October 19, 2021
working with you
From: Chris Asmanis, BA Consulting Group Ltd.
Re: Growth Rates Data Request - Britannia Road at Queen Street
Chris,
Here are the estimated CAGR values for Britannia Road at Queen Street:

| $2016-2021$ | $2021-2031$ |
| :---: | :---: |
| $0.5 \%$ | $0.5 \%$ |

These growth rates are estimated based on multiple sources including Peel Travel Demand forecasting model, ATR and land use/forecasts data. Please note that this area may be further affected by future growth (after 2031 and beyond). Please use your professional judgement when using these values.

If you require further assistance, please contact me at robert.jay@peelregion.ca.
Regards,
Robbie Jay
Transportation Planner, Transportation System Planning
Transportation Division, Public Works Services, Region of Peel
10 Peel Centre Drive, Suite B, 4th Floor
Brampton, ON L6T 4B9
W: (905) 791-7800 x6456
E: robert.jay@peelregion.ca

## Chris Asmanis

From:
Sent:
Tyler Xuereb [Tyler.Xuereb@mississauga.ca](mailto:Tyler.Xuereb@mississauga.ca)
To:
Subject:

Monday, October 18, 2021 2:24 PM
Chris Asmanis
RE: Growth Rate Request - Queen Street / Britannia Road West

Hi Chris,

Using the City's Travel Demand Model and supporting traffic count data, the City's Transportation Planning section has determined the projected growth along Queen Street to be used as part of your study. The recommended projected growth is shown below.

Queen Street

|  | Compounded <br> Annual Growth <br> from Existing to <br> 2031 |  |
| :--- | :---: | :---: |
|  | NB | SB |
| AM Peak | $0.5 \%$ | $1.5 \%$ |
|  |  |  |
| PM Peak | $0.5 \%$ | $0.5 \%$ |

Regards,
M mississauga

## Tyler Xuereb

Transportation Planning Analyst
T 905-615-3200 ext. 4783
Tyler.xuereb@mississauga.ca
City of Mississauga | Transportation and Works Department, Infrastructure Planning and Engineering Services Division

Please consider the environment before printing.

From: Chris Asmanis [chris.asmanis@bagroup.com](mailto:chris.asmanis@bagroup.com)
Sent: Thursday, October 14, 2021 9:12 AM
To: Tyler Xuereb [Tyler.Xuereb@mississauga.ca](mailto:Tyler.Xuereb@mississauga.ca)
Subject: RE: Growth Rate Request - Queen Street / Britannia Road West

Hi Tyler,

No worries, I'll do some digging and see. Will await the rates for Queen Street!

Thanks again,
Chris

From: Tyler Xuereb [Tyler.Xuereb@mississauga.ca](mailto:Tyler.Xuereb@mississauga.ca)
Sent: Thursday, October 14, 2021 9:05 AM
To: Chris Asmanis [chris.asmanis@bagroup.com](mailto:chris.asmanis@bagroup.com)
Subject: RE: Growth Rate Request - Queen Street / Britannia Road West

Hi Chris,

Thanks for the information!

Unfortunately, I do not know the contact at the Region for growth rates.

Regards,

Tyler Xuereb
Transportation Planning Analyst
T 905-615-3200 ext. 4783
Tyler.xuereb@mississauga.ca
City of Mississauga | Transportation and Works Department,
Infrastructure Planning and Engineering Services Division
Please consider the environment before printing.

From: Chris Asmanis [chris.asmanis@bagroup.com](mailto:chris.asmanis@bagroup.com)
Sent: Thursday, October 14, 2021 8:58 AM
To: Tyler Xuereb [Tyler.Xuereb@mississauga.ca](mailto:Tyler.Xuereb@mississauga.ca)
Subject: RE: Growth Rate Request - Queen Street / Britannia Road West

Hi Tyler,

Thanks for the quick reply. Please see the attached correspondence regarding the Site and ToR. The horizon years for our study are 2026 and 2031.

Do you have a contact that I could reach out to at Peel Region for the rates along Britannia Road?

Thanks,
Chris

## Chris Asmanis

Transportation Analyst
BA Consulting Group Ltd.
300-45 St. Clair Ave. W.
Toronto, ON M4V 1K9
TEL $4169617110 \times 201$
EMAIL chris.asmanis@bagroup.com

From: Tyler Xuereb [Tyler.Xuereb@mississauga.ca](mailto:Tyler.Xuereb@mississauga.ca)
Sent: Thursday, October 14, 2021 7:49 AM
To: Chris Asmanis [chris.asmanis@bagroup.com](mailto:chris.asmanis@bagroup.com)
Subject: RE: Growth Rate Request - Queen Street / Britannia Road West

Good Morning Chris,

Thank you for your email.

I can provide you with growth rates along Queen Street but Britannia Road is a regional road and as such, you will have to contact them for the rates along Britannia.

I just have a few questions in regards to your analysis.
-What is the location of your proposed development?
-What are your horizon years?
-What background developments are you including in your analysis?
-Have you submitted a ToR to the City and have you received comments back?

Regards,

## MISSISSaUGa

## Tyler Xuereb

Transportation Planning Analyst
T 905-615-3200 ext. 4783
Tyler.xuereb@mississauga.ca
City of Mississauga | Transportation and Works Department,
Infrastructure Planning and Engineering Services Division
Please consider the environment before printing.

From: Chris Asmanis [chris.asmanis@bagroup.com](mailto:chris.asmanis@bagroup.com)
Sent: Wednesday, October 13, 2021 3:37 PM
To: Tyler Xuereb [Tyler.Xuereb@mississauga.ca](mailto:Tyler.Xuereb@mississauga.ca)
Subject: Growth Rate Request - Queen Street / Britannia Road West

Hi Tyler,

We are working on a development proposal in Streetsville and require some corridor growth rates for our analysis.

If possible, are you able to provide growth rates for Queen Street (North/South) \& Britannia Road West?

Thanks,
Chris

## Chris Asmanis <br> Transportation Analyst

BA Consulting Group Ltd.
300-45 St. Clair Ave. W.
Toronto, ON M4V 1K9
TEL $4169617110 \times 201$
EMAIL chris.asmanis@bagroup.com

Appendix H: Signal Timing Plans (STPs)

| REGIONAL MUNICIPALITY OF PEEL <br> Traffic Signal Timing Parameters |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Database Date |  | April 30, 2021 |  |  | Prepared Date |  | April 30, 2021 |  |  |
| Database Rev |  | iNET |  |  | Completed By |  | BL |  |  |
| Timing Card / Field rev |  | iNET |  |  | Checked By |  | MA |  |  |
| Location $\quad$ Britannia Road at Queen Street |  |  |  |  |  |  |  |  |  |
| Phase <br> \# | Street Name - Direction | Vehicle Minimum (s) | Pedestrian Minimum (s) |  | Amber <br> (s) | All Red (s) | TIME PERIOD (s) <br> SPLITS = Green+Amber+All Red MAX = Green only |  |  |
|  |  |  |  |  | $\begin{gathered} \hline \text { AM } \\ \text { SPLITS } \end{gathered}$ |  | $\begin{gathered} \text { OFF } \\ \text { SPLITS } \end{gathered}$ | $\begin{gathered} \hline \text { PM } \\ \text { SPLITS } \end{gathered}$ |
|  |  |  | WALK | FDWALK |  |  |  |  |
| 1 | Britannia Road - WB PP LT | 8 | 0 | 0 | 3 | 0 | 11 | 13 | 11 |
| 2 | Britannia Road - EB | 12 | 8 | 20 | 4 | 3.1 | 83 | 80 | 74 |
| 3 | Queen Street - SB PP LT | 8 | 0 | 0 | 3 | 0 | 13 | 13 | 17 |
| 4 | Queen Street - NB | 12 | 9 | 22 | 4 | 3.9 | 53 | 54 | 58 |
| 5 | Britannia Road - EB PP LT | 8 | 0 | 0 | 3 | 0 | 13 | 13 | 13 |
| 6 | Britannia Road - WB | 12 | 8 | 20 | 4 | 3.1 | 81 | 80 | 72 |
| 7 | Queen Street - NB PP LT | 8 | 0 | 0 | 3 | 0 | 0 | 19 | 14 |
| 8 | Queen Street - SB | 12 | 9 | 22 | 4 | 3.9 | 66 | 48 | 61 |
| System Control Yes |  |  |  | TIME (M-F) |  | PEAK | CYCLE LENGTH (s) |  | OFFSET (s) |
|  |  |  |  | 06:00-09:30 |  | AM | 160 |  | 155 |
|  |  |  |  | $\begin{aligned} & \text { 09:30-15:00 } \\ & \text { 19:30-00:00 } \end{aligned}$ |  | OFF | 160 |  | 69 |
| Semi-Actuated Mode Yes |  |  |  | 15:00-19:30 |  | PM | 160 |  | 114 |


| REGIONAL MUNICIPALITY OF PEEL <br> Traffic Signal Timing Parameters |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Database Date |  | January 7, 2021 |  |  | Prepared Date |  | April 30, 2021 |  |  |
| Database Rev |  | iNET |  |  | Completed By |  | BL |  |  |
| Timing Card / Field rev |  | iNET |  |  | Checked By |  | MA |  |  |
| Location $\quad$ Britannia Road @ Ellesboro Drive |  |  |  |  |  |  |  |  |  |
| Phase <br> \# | Street Name - Direction | Vehicle Minimum (s) | Pedestrian Minimum (s) |  | Amber <br> (s) | All Red (s) | TIME PERIOD (s) <br> SPLITS = Green+Amber+All Red MAX = Green only |  |  |
|  |  |  | WALK | FDWALK |  |  | AM SPLITS | OFF SPLITS | $\begin{gathered} \hline \text { PM } \\ \text { SPLITS } \end{gathered}$ |
| 1 | Not in use | - | - | - | - | - | - | - | - |
| 2 | Britannia Road - EB | 8 | 10 | 21 | 4 | 2.1 | 115 | 107 | 115 |
| 3 | Not in use | - | - | - | - | - | - | - | - |
| 4 | Ring Balance / Computer Phase | 13 | 10 | 20 | 4 | 2 | 45 | 53 | 45 |
| 5 | Not in use | - | - | - | - | - | - | - | - |
| 6 | Britannia Road - WB | 8 | 10 | 21 | 4 | 2.1 | 115 | 107 | 115 |
| 7 | Not in use | - | - | - | - | - | - | - | - |
| 8 | Ellesboro Drive - SB | 13 | 10 | 20 | 4 | 2 | 45 | 53 | 45 |
| System Control Yes |  |  |  | TIME (M-F) |  | PEAK | CYCLE LENGTH (s) |  | OFFSET (s) |
|  |  |  |  | 06:00-09:30 |  | AM | 160 |  | 139 |
|  |  |  |  | $\begin{aligned} & \text { 09:30-15:00 } \\ & \text { 19:30-00:00 } \end{aligned}$ |  | OFF | 160 |  | 59 |
| Semi-Actuated Mode Yes |  |  |  | 15:00-19:30 |  | PM | 160 |  | 96 |




Appendix I:
Synchro Analysis Worksheets

| HCM Unsignalized Intersection Capacity Analysis 1：Queen Street North \＆Matlock Ave |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  | $\dagger$ | 7 |  | $\dagger$ |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | Y |  | 个t |  | \％ | 个 $\uparrow$ |  |  |
| Traffic Volume（veh／h） | 30 | 20 | 955 | 40 | 15 | 550 |  |  |
| Future Volume（Veh／h） | 30 | 20 | 955 | 40 | 15 | 550 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |  |
| Grade | 0\％ |  | 0\％ |  |  | 0\％ |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Hourly flow rate（vph） | 33 | 22 | 1038 | 43 | 16 | 598 |  |  |
| Pedestrians | 1 |  |  |  |  |  |  |  |
| Lane Width（m） | 3.5 |  |  |  |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  | TWLTL |  |  | None |  |  |
| Median storage veh） |  |  | 2 |  |  |  |  |  |
| Upstream signal（ m ） |  |  | 313 |  |  |  |  |  |
| pX，platoon unblocked | 0.90 | 0.90 |  |  | 0.90 |  |  |  |
| vC ，conficting volume | 1392 | 542 |  |  | 1082 |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1060 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 331 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1209 | 263 |  |  | 864 |  |  |  |
| tC，single（s） | 7.3 | 7.4 |  |  | 4.9 |  |  |  |
| tC， 2 stage（s） | 6.3 |  |  |  |  |  |  |  |
| tF（s） | 3.7 | 3.5 |  |  | 2.6 |  |  |  |
| p0 queue free \％ | 88 | 96 |  |  | 97 |  |  |  |
| cM capacity（veh／h） | 280 | 602 |  |  | 511 |  |  |  |
| Direction，Lane \＃ | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | SB 3 |  |  |
| Volume Total | 55 | 692 | 389 | 16 | 299 | 299 |  |  |
| Volume Left | 33 | 0 | 0 | 16 | 0 | 0 |  |  |
| Volume Right | 22 | 0 | 43 | 0 | 0 | 0 |  |  |
| cSH | 356 | 1700 | 1700 | 511 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.15 | 0.41 | 0.23 | 0.03 | 0.18 | 0.18 |  |  |
| Queue Length 95th（m） | 4.3 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 17.0 | 0.0 | 0.0 | 12.3 | 0.0 | 0.0 |  |  |
| Lane LOS | C |  |  | B |  |  |  |  |
| Approach Delay（s） | 17.0 | 0.0 |  | 0.3 |  |  |  |  |
| Approach LOS | c |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.6 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 37．7\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

Analysis Period（min）
Existing AM 21－51 Queen Street North 10：40 am 09／24／2021 Existing AM Peak Hour

BA Group | Synchro 11 Report |
| ---: |
| Page 1 |

| HCM Unsignalized Intersection Capacity Analysis <br> 2：Queen Street North \＆ 40 Queen St $N$ Driveway／ 53 Queen St Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{*}{ }$ | $\rightarrow$ |  | 7 |  | 4 | 4 | $\dagger$ |  | ＊ | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ${ }_{\text {¢ }}$ |  |  | ${ }_{\dagger}$ |  | ${ }_{1}$ | 性 |  | ${ }^{*}$ | $\uparrow$ |  |
| Traffic Volume（veh／h） | 0 | 0 | 0 | 0 |  | 0 | 0 | 995 | 0 | 0 | 580 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 995 | 0 | 0 | 580 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1131 | 0 | 0 | 659 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.87 | 0.87 |  | 0.87 | 0.87 | 0.87 |  |  |  | 0.87 |  |  |
| vC ，conficting volume | 1224 | 1790 | 330 | 1460 | 1790 | 566 | 659 |  |  | 1131 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 659 | 659 |  | 1131 | 1131 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 566 | 1131 |  | 330 | 659 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 960 | 1610 | 330 | 1231 | 1610 | 203 | 659 |  |  | 852 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \％ | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity（veh／h） | 383 | 275 | 672 | 265 | 275 | 706 | 939 |  |  | 692 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 0 | 0 | 754 | 377 | 0 | 439 | 220 |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| cSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.00 | 0.44 | 0.22 | 0.00 | 0.26 | 0.13 |  |  |  |  |
| Queue Length 95th（ m ） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 30．8\％ |  | Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |


| HCM Unsignalized Intersection Capacity Analysis 3: Queen Street North \& 40 Queen St S Driveway |  |  |  |  |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\geqslant$ | 4 | $\dagger$ | $\downarrow$ | 4 |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | M |  | \% | 个4 | $\uparrow$ 个 |  |  |  |
| Traffic Volume (veh/h) | 0 | 0 | 0 | 995 | 580 | 0 |  |  |
| Future Volume (Veh/h) | 0 | 0 | 0 | 995 | 580 | 0 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |  |  |
| Hourly flow rate (vph) | 0 | 0 | 0 | 1144 | 667 | 0 |  |  |
| Pedestrians | 3 |  |  |  |  |  |  |  |
| Lane Width ( m ) | 3.5 |  |  |  |  |  |  |  |
| Walking Speed (m/s) | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | TWLTL |  |  |  |
| Median storage veh) |  |  |  | 2 | 2 |  |  |  |
| Upstream signal ( $m$ ) |  |  |  | 186 |  |  |  |  |
| pX, platoon unblocked | 0.86 |  |  |  |  |  |  |  |
| VC , conflicting volume | 1242 | 336 | 670 |  |  |  |  |  |
| $\mathrm{vC1}$, stage 1 conf vol | 670 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol | 572 |  |  |  |  |  |  |  |
| vCu, unblocked vol | 966 | 336 | 670 |  |  |  |  |  |
| tC, single (s) | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| $\mathrm{tc}, 2$ stage (s) | 5.8 |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \% | 100 | 100 | 100 |  |  |  |  |  |
| cM capacity (veh/h) | 426 | 664 | 927 |  |  |  |  |  |
| Direction, Lane \# | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 0 | 0 | 572 | 572 | 445 | 222 |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| cSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.34 | 0.34 | 0.26 | 0.13 |  |  |
| Queue Length 95th ( m ) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | A |  |  |  |  |  |  |  |
| Approach Delay (s) | 0.0 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 30.8\% |  | U Level of | Service | A |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

Analysis Period (min)

| HCM Unsignalized Intersection Capacity Analysis 5：Queen Street North \＆Petro Canada S Driveway |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 |  | 4 | $\dagger$ | $\downarrow$ | $\stackrel{ }{ }$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | Y |  | ${ }^{7}$ | ¢ $\uparrow$ | 个t |  |  |  |
| Traffic Volume（veh／h） | 0 | 5 | 0 | 1010 | 560 | 10 |  |  |
| Future Volume（Veh／h） | 0 | 5 | 0 | 1010 | 560 | 10 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |  |  |
| Hourly flow rate（vph） | 0 | 6 | 0 | 1148 | 636 | 11 |  |  |
| Pedestrians | 3 |  |  | 2 |  |  |  |  |
| Lane Width（m） | 3.5 |  |  | 3.6 |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | TWLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ m ） |  |  |  | 127 |  |  |  |  |
| pX，platoon unblocked | 0.85 |  |  |  |  |  |  |  |
| VC, conflicting volume | 1218 | 328 | 650 |  |  |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 644 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 574 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 914 | 328 | 650 |  |  |  |  |  |
| tC ，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 100 | 99 | 100 |  |  |  |  |  |
| cM capacity（veh／h） | 441 | 670 | 943 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 6 | 0 | 574 | 574 | 424 | 223 |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 6 | 0 | 0 | 0 | 0 | 11 |  |  |
| cSH | 670 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.01 | 0.00 | 0.34 | 0.34 | 0.25 | 0.13 |  |  |
| Queue Length 95th（ m ） | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 10.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | B |  |  |  |  |  |  |  |
| Approach Delay（s） | 10.4 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 38．6\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |


| Existing AM 21－51 Queen Street North 10：40 am 09／24／2021 Existing AM Peak Hour |  |
| :--- | ---: |
| BA Group | Synchro 11 Report <br> Page 5 |

Timings
6：Queen Street South／Queen Street North \＆Britannia Rd West 06／28／2023

|  | $\rangle$ | $\rightarrow$ | 7 |  |  |  | 4 |  | $\dagger$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations | \％ | 个分 | ＊ | 个个 | 「 | \％ | 个家 | \％ | $\uparrow$ | 「 |
| Trafic Volume（vph） | 215 | 1535 | 80 | 610 | 325 | 95 | 470 | 140 | 285 | 140 |
| Future Volume（vph） | 215 | 1535 | 80 | 610 | 325 | 95 | 470 | 140 | 285 | 140 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | Perm | NA | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm |
| Protected Phases | 5 | 2 | 1 | 6 |  |  | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 12.0 | 12.0 | 8.0 | 12.0 | 12.0 |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 38.9 | 38.9 | 11.0 | 38.9 | 38.9 |
| Total Split（s） | 13.0 | 83.0 | 11.0 | 81.0 | 81.0 | 53.0 | 53.0 | 13.0 | 66.0 | 66.0 |
| Total Split（\％） | 8．1\％ | 51．9\％ | 6．9\％ | 50．6\％ | 50．6\％ | 33．1\％ | 33．1\％ | 8．1\％ | 41．3\％ | 41．3\％ |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 3.9 | 3.9 | 0.0 | 3.9 | 3.9 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 7.9 | 7.9 | 3.0 | 7.9 | 7.9 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |
| Act Effct Green（s） | 102.5 | 86.5 | 96.7 | 83.1 | 83.1 | 33.0 | 33.0 | 50.9 | 46.0 | 46.0 |
| Actuated g／C Ratio | 0.64 | 0.54 | 0.60 | 0.52 | 0.52 | 0.21 | 0.21 | 0.32 | 0.29 | 0.29 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.42 | 0.86 | 0.54 | 0.34 | 0.36 | 0.47 | 0.82 | 0.78 | 0.54 | 0.28 |
| Control Delay | 15.0 | 37.7 | 45.3 | 21.9 | 4.1 | 62.4 | 68.2 | 68.7 | 51.3 | 6.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 15.0 | 37.7 | 45.3 | 21.9 | 4.1 | 62.4 | 68.2 | 68.7 | 51.3 | 6.8 |
| LOS | B | D | D | C | A | E | E | E | D | A |
| Approach Delay |  | 35.1 |  | 18.0 |  |  | 67.4 |  | 44.6 |  |
| Approach LOS |  | D |  | B |  |  | E |  | D |  |

## Intersection Summar

Cycle Length： 160
Actuated Cycle Length： 160
Offset： $13(8 \%)$ ，Referenced to phase 2：EBTL and $6:$ WBTL，Start of Green
Control Type：Actuated－Coordinated
Contro Type．Actuated－C

| Maximum vic Ratio：D．8a | Intersection LOS：D |
| :--- | :--- |
| Intersection Signal Delay：． | ICU Level of Service |
| Intersection Capacity Utilization 103．9\％ |  |

Intersection Capacity Utilization 103．9\％
ICU Level of Service G
Analysis Period（min） 15


[^0]Queues

| 6: Queen Street |  | S | + | th \& | ritan | a | West |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ | 7 | 4 | 4 | 4 | 4 | * | $\dagger$ | $\pm$ |  |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |  |
| Lane Group Flow (vph) | 215 | 1635 | 80 | 610 | 325 | 95 | 595 | 140 | 285 | 140 |  |
| v/c Ratio | 0.42 | 0.86 | 0.54 | 0.34 | 0.36 | 0.47 | 0.82 | 0.78 | 0.54 | 0.28 |  |
| Control Delay | 15.0 | 37.7 | 45.3 | 21.9 | 4.1 | 62.4 | 68.2 | 68.7 | 51.3 | 6.8 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 15.0 | 37.7 | 45.3 | 21.9 | 4.1 | 62.4 | 68.2 | 68.7 | 51.3 | 6.8 |  |
| Queue Length 50th (m) | 27.9 | 236.6 | 10.9 | 62.4 | 12.8 | 28.2 | 97.8 | 34.9 | 80.7 | 0.0 |  |
| Queue Length 95th (m) | 46.4 | \#334.8 | 24.2 | 86.8 | 32.3 | 46.0 | 114.3 | \#56.0 | 104.9 | 16.2 |  |
| Internal Link Dist ( $m$ ) |  | 110.7 |  | 83.1 |  |  | 135.0 |  | 103.4 |  |  |
| Turn Bay Length ( m ) | 95.0 |  | 60.0 |  | 45.0 | 40.0 |  | 35.0 |  |  |  |
| Base Capacity (vph) | 510 | 1910 | 147 | 1772 | 904 | 277 | 981 | 180 | 670 | 603 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | O | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.42 | 0.86 | 0.54 | 0.34 | 0.36 | 0.34 | 0.61 | 0.78 | 0.43 | 0.23 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maxim | fter two | cycles. |  |  |  |  |  |  |  |  |  |

Existing AM 21-51 Queen Street North 10:40 am 09/24/2021 Existing AM Peak Hour

BA Group | Synchro 11 Report |
| ---: |
| Page 7 |

HCM Signalized Intersection Capacity Analysis


## HCM Unsignalized Intersection Capacity Analysis

| 7: Arch Rd \& Britannia Rd West |  |  |  |  |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ | $\geqslant$ | 1 | $\downarrow$ | 4 | \% |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个 $\uparrow$ |  | \% | 个4 | M |  |  |  |
| Traffic Volume (veh/h) | 1795 | 5 | 10 | 1010 | 5 | 10 |  |  |
| Future Volume (Veh/h) | 1795 | 5 | 10 | 1010 | 5 | 10 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate (vph) | 1795 | 5 | 10 | 1010 | 5 | 10 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type | None |  |  | TWLTL |  |  |  |  |
| Median storage veh) |  |  |  | 2 |  |  |  |  |
| Upstream signal ( m ) | 107 |  |  | 182 |  |  |  |  |
| pX, platoon unblocked |  |  | 0.60 |  | 0.62 | 0.60 |  |  |
| vC, conficting volume |  |  | 1800 |  | 2322 | 900 |  |  |
| VC1, stage 1 conf vol |  |  |  |  | 1798 |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  | 525 |  |  |  |
| vCu , unblocked vol |  |  | 989 |  | 1515 | 0 |  |  |
| tC, single (s) |  |  | 4.1 |  | 6.8 | 7.1 |  |  |
| tC, 2 stage (s) |  |  |  |  | 5.8 |  |  |  |
| tF (s) |  |  | 2.2 |  | 3.5 | 3.4 |  |  |
| p0 queue free \% |  |  | 98 |  | 97 | 98 |  |  |
| cM capacity (veh/h) |  |  | 422 |  | 185 | 635 |  |  |
| Direction, Lane \# | EB 1 | EB2 | WB 1 | WB 2 | WB 3 | NB 1 |  |  |
| Volume Total | 1197 | 603 | 10 | 505 | 505 | 15 |  |  |
| Volume Left | 0 | 0 | 10 | 0 | 0 | 5 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 10 |  |  |
| cSH | 1700 | 1700 | 422 | 1700 | 1700 | 351 |  |  |
| Volume to Capacity | 0.70 | 0.35 | 0.02 | 0.30 | 0.30 | 0.04 |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.1 |  |  |
| Control Delay (s) | 0.0 | 0.0 | 13.7 | 0.0 | 0.0 | 15.7 |  |  |
| Lane LOS |  |  | B |  |  | C |  |  |
| Approach Delay (s) | 0.0 |  | 0.1 |  |  | 15.7 |  |  |
| Approach LOS |  |  |  |  |  | c |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 59.8\% |  | CU Level | Service | B |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
8: Earl St \& Britannia Rd West


[^1]Timings
9: Britannia Rd West \& Ellesboro Dr 06/28/2023

Intersection Summany
Cycle Length: 160
Actuated Cycle Length: 160
Offiset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBT, Start of Green
Natural Cycle: 90

Splits and Phases: 9: Britannia Rd West \& Ellesboro Dr


| Existing AM $21-51$ Queen Street North 10:40 am 09/24/2021 Existing AM Peak Hour |  |
| :--- | ---: |
| BA Group | Synchro 11 Report <br> Page 11 |

Queues
9: Britannia Rd West \& Ellesboro Dr

| Lane Group | EBL | EBT | WBT | SBL | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Lane Group Flow (vph) | 30 | 1795 | 1060 | 60 | 30 |
| V/c Ratio | 0.07 | 0.58 | 0.36 | 0.40 | 0.20 |
| Control Delay | 1.1 | 1.7 | 2.9 | 77.8 | 23.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 1.1 | 1.7 | 2.9 | 77.8 | 23.8 |
| Queue Length 50 th $(\mathrm{m})$ | 0.7 | 27.4 | 34.0 | 19.5 | 0.0 |
| Queue Length 95th $(\mathrm{m})$ | m 0.7 | 24.7 | 44.3 | 35.5 | 11.4 |
| Internal Link Dist $(\mathrm{m})$ |  | 46.6 | 115.6 | 80.1 |  |
| Turn Bay Length $(\mathrm{m})$ | 45.0 |  |  |  | 15.0 |
| Base Capacity (vph) | 416 | 3120 | 2967 | 434 | 375 |
| Starvation Cap Reductn | 0 | 152 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.60 | 0.36 | 0.14 | 0.08 |
| Intersection Summary |  |  |  |  |  |
| m Volume for 95th percentile queue is metered by upstream signal. |  |  |  |  |  |

Existing AM 21-51 Queen Street North $10: 40$ am 09/24/2021 Existing AM Peak Hour
BA Group

| HCM Signalized Intersection Capacity Analysis 9：Britannia Rd West \＆Ellesboro Dr |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{*}$ | $\rightarrow$ | $\sim$ |  |  | $\stackrel{ }{+}$ |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |  |
| Lane Configurations | ${ }^{4}$ | 个个 | $\uparrow{ }^{\text {¢ }}$ |  | ${ }^{7}$ | 「 |  |  |
| Traffic Volume（vph） | 30 | 1795 | 990 | 70 | 60 | 30 |  |  |
| Future Volume（vph） | 30 | 1795 | 990 | 70 | 60 | 30 |  |  |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Lane Width | 3.5 | 3.7 | 3.7 | 3.5 | 3.5 | 3.5 |  |  |
| Total Lost time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 0.95 |  | 1.00 | 1.00 |  |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 0.97 |  |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Frt | 1.00 | 1.00 | 0.99 |  | 1.00 | 0.85 |  |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Flow（prot） | 1729 | 3579 | 3403 |  | 1782 | 1447 |  |  |
| Fit Permitted | 0.26 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Flow（perm） | 476 | 3579 | 3403 |  | 1782 | 1447 |  |  |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj．Flow（vph） | 30 | 1795 | 990 | 70 | 60 | 30 |  |  |
| RTOR Reduction（vph） | 0 | 0 | 1 | 0 | 0 | 28 |  |  |
| Lane Group Flow（vph） | 30 | 1795 | 1059 | 0 | 60 | 2 |  |  |
| Confl．Peds．（\＃hr） | 4 |  |  | 4 | ， | 12 |  |  |
| Heavy Vehicles（\％） | 3\％ | 2\％ | 6\％ | 6\％ | 0\％ | 7\％ |  |  |
| Turn Type | Perm | NA | NA |  | Perm | Perm |  |  |
| Protected Phases |  | 2 | 6 |  |  |  |  |  |
| Permitted Phases | 2 |  |  |  | 8 | 8 |  |  |
| Actuated Green，G（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Effective Green， g （s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Actuated g／C Ratio | 0.86 | 0.86 | 0.86 |  | 0.07 | 0.07 |  |  |
| Clearance Time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |
| Lane Grp Cap（vph） | 407 | 3066 | 2915 |  | 120 | 97 |  |  |
| v／s Ratio Prot |  | c0．50 | 0.31 |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.06 |  |  |  | c0．03 | 0.00 |  |  |
| v／c Ratio | 0.07 | 0.59 | 0.36 |  | 0.50 | 0.02 |  |  |
| Uniform Delay，d1 | 1.7 | 3.3 | 2.4 |  | 72.0 | 69.7 |  |  |
| Progression Factor | 0.39 | 0.34 | 1.00 |  | 1.00 | 1.00 |  |  |
| Incremental Delay，d2 | 0.2 | 0.5 | 0.4 |  | 3.3 | 0.1 |  |  |
| Delay（s） | 0.9 | 1.6 | 2.7 |  | 75.2 | 69.7 |  |  |
| Level of Service | A | A | A |  | E | E |  |  |
| Approach Delay（s） |  | 1.6 | 2.7 |  | 73.4 |  |  |  |
| Approach LOS |  | A | A |  | E |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 4.1 |  | HCM 2000 | evel of Service | A |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.58 |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | time（s） | 12.1 |  |
| Intersection Capacity Utilization |  |  | 75．2\％ |  | CU Level | Service | D |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |


| Existing AM 21－51 Queen Street North 10：40 am 09／24／2021 Existing AM Peak Hour | Synchro11 Report <br> Page 13 |
| :--- | ---: |

HCM Unsignalized Intersection Capacity Analysis
1：Queen Street North \＆Matlock Ave
06／28／2023

Existing PM 21－51 Queen Street North $10: 40$ am 09／24／2021 Existing PM Peak Hour
BA Group

| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2: Queen Street North \& 40 Queen St N Driveway/53 Queen St Driveway |  |  |  |  |  |  |  |  |  |  | 06/28/2023 |  |
|  | $\stackrel{*}{ }$ |  |  | 1 |  |  | 4 | $\dagger$ |  |  | $\dagger$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | ${ }_{\dagger}$ |  | \% | 个t |  | ${ }^{7}$ | 个t |  |
| Traffic Volume (veh/h) | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 605 | 0 | 5 | 1100 | 0 |
| Future Volume (Veh/h) | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 605 | 0 | 5 | 1100 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate (vph) | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 665 | 0 | 5 | 1209 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh) |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX, platoon unblocked | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 |  |  |  | 0.95 |  |  |
| vC , conficting volume | 1562 | 1894 | 604 | 1294 | 1894 | 332 | 1209 |  |  | 665 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol | 1219 | 1219 |  | 675 | 675 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol | 342 | 675 |  | 620 | 1219 |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1482 | 1833 | 604 | 1201 | 1833 | 186 | 1209 |  |  | 537 |  |  |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage (s) | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \% | 100 | 100 | 99 | 99 | 100 | 100 | 99 |  |  | 99 |  |  |
| cM capacity (veh/h) | 186 | 227 | 446 | 335 | 224 | 788 | 584 |  |  | 987 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 5 | 5 | 5 | 443 | 222 | 5 | 806 | 403 |  |  |  |  |
| Volume Left | 0 | 5 | 5 | 0 | 0 | 5 | 0 | 0 |  |  |  |  |
| Volume Right | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| cSH | 446 | 335 | 584 | 1700 | 1700 | 987 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.01 | 0.01 | 0.01 | 0.26 | 0.13 | 0.01 | 0.47 | 0.24 |  |  |  |  |
| Queue Length 95th (m) | 0.3 | 0.4 | 0.2 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay (s) | 13.2 | 15.9 | 11.2 | 0.0 | 0.0 | 8.7 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | B | C | B |  |  | A |  |  |  |  |  |  |
| Approach Delay (s) | 13.2 | 15.9 | 0.1 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | B | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 41.2\% |  | Level | Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period (min)

| HCM Unsignalized Intersection Capacity Analysis <br> 4: Queen Street North \& Petro Canada N Driveway/Existing Site Driveway |  |  |  |  |  |  |  |  |  |  | 06/28/2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{*}{ }$ |  |  | 7 |  | 4 | 4 | $\uparrow$ |  |  | $\dagger$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | ${ }_{\dagger}$ |  | ${ }^{7}$ | 个t |  | ${ }^{7}$ | 个t |  |
| Traffic Volume (veh/h) | 0 | - | 0 | 30 | 0 | 20 | 10 | 585 | 25 | 15 | 1090 | 10 |
| Future Volume (Veh/h) | 0 | 0 | 0 | 30 | 0 | 20 | 10 | 585 | 25 | 15 | 1090 | 10 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate (vph) | 0 | 0 | 0 | 33 | 0 | 22 | 11 | 643 | 27 | 16 | 1198 | 11 |
| Pedestrians |  | 2 |  |  | 28 |  |  |  |  |  |  |  |
| Lane Width (m) |  | 3.7 |  |  | 3.7 |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  | 1.2 |  |  | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage |  | 0 |  |  | 2 |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh) |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal ( m ) |  |  |  |  |  |  |  | 159 |  |  |  |  |
| pX, platoon unblocked | 0.92 | 0.92 |  | 0.92 | 0.92 | 0.92 |  |  |  | 0.92 |  |  |
| vC , conficting volume | 1603 | 1958 | 606 | 1338 | 1950 | 363 | 1211 |  |  | 698 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol | 1238 | 1238 |  | 706 | 706 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol | 366 | 720 |  | 631 | 1243 |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1485 | 1869 | 606 | 1197 | 1861 | 140 | 1211 |  |  | 503 |  |  |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage (s) | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \% | 100 | 100 | 100 | 90 | 100 | 97 | 98 |  |  | 98 |  |  |
| cM capacity (veh/h) | 179 | 217 | 444 | 325 | 210 | 800 | 582 |  |  | 964 |  |  |
| Direction, Lane \# | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 55 | 11 | 429 | 241 | 16 | 799 | 410 |  |  |  |  |
| Volume Left | 0 | 33 | 11 | 0 | 0 | 16 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 22 | 0 | 0 | 27 | 0 | 0 | 11 |  |  |  |  |
| cSH | 1700 | 427 | 582 | 1700 | 1700 | 964 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.13 | 0.02 | 0.25 | 0.14 | 0.02 | 0.47 | 0.24 |  |  |  |  |
| Queue Length 95th (m) | 0.0 | 3.5 | 0.5 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |  |  |  |  |
| Control Delay (s) | 0.0 | 14.7 | 11.3 | 0.0 | 0.0 | 8.8 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | B | B |  |  | A |  |  |  |  |  |  |
| Approach Delay (s) | 0.0 | 14.7 | 0.2 |  |  | 0.1 |  |  |  |  |  |  |
| Approach LOS | A | B |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 40.5\% |  | Level | f Service |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period (min)

| Existing PM 21-51 Queen Street North 10:40 am 09/24/2021 Existing PM Peak Hour | Synchro 11 Report |
| :--- | ---: |
| BA Group | Page 4 |

Timings
6: Queen Street South/Queen Street North \& Britannia Rd West

$\frac{\text { Intersection Summan }}{\text { Cycle Length: } 160}$
Cycle Length: 160
Actuated Cycle Length: 160
Offset: $13(8 \%$ ), Referenced to phase $2:$ :EBTL and 6 WBTL, Start of Green
Noutrol Type: Actuated-Coordinated
Contro Type: Actuated--Corranaled
Maximum V Siro. 0.90
$\begin{array}{ll}\text { Intersection Signal Delay: } 44.1 & \text { Intersection LOS: D } \\ \text { Intersection Capacity Utiization } 96.3 \% & \text { ICU Level of Service F }\end{array}$

Analysis Period (min) 15
Splits and Phases: 6: Queen Street South/Queen Street North \& Britannia Rd West


Queues
6: Queen Street South/Queen Street North \& Britannia Rd West
06/28/2023

|  | $\rangle$ | $\rightarrow$ | 1 | 4 | 4 | 4 | $\dagger$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Group Flow (vph) | 145 | 1090 | 140 | 1185 | 125 | 165 | 490 | 280 | 510 | 345 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.71 | 0.70 | 0.62 | 0.76 | 0.18 | 0.88 | 0.50 | 0.80 | 0.90 | 0.63 |
| Control Delay | 40.5 | 39.1 | 32.0 | 38.8 | 9.6 | 72.0 | 45.7 | 51.3 | 73.4 | 32.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 40.5 | 39.1 | 32.0 | 38.8 | 9.6 | 72.0 | 45.7 | 51.3 | 73.4 | 32.9 |
| Queue Length 50th (m) | 23.8 | 159.1 | 15.2 | 184.5 | 7.8 | 34.9 | 66.4 | 63.9 | 162.5 | 60.1 |
| Queue Length 95th (m) | \#56.3 | 186.8 | \#26.2 | 215.7 | 14.6 | \#71.9 | 81.8 | 85.3 | 203.8 | 92.7 |
| Internal Link Dist (m) |  | 110.7 |  | 83.1 |  |  | 135.0 |  | 103.4 |  |
| Turn Bay Length ( m ) | 95.0 |  | 60.0 |  | 45.0 | 40.0 |  | 35.0 |  |  |
| Base Capacity (vph) | 205 | 1558 | 224 | 1555 | 706 | 188 | 1094 | 351 | 637 | 602 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.71 | 0.70 | 0.63 | 0.76 | 0.18 | 0.88 | 0.45 | 0.80 | 0.80 | 0.57 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |

\# 95th percentile volume exceeds capacity, queue may be longer
Queue shown is maximum after two cycles.

HCM Signalized Intersection Capacity Analysis

| 6: Queen Street South/Queen Street North \& Britannia Rd West |  |  |  |  |  |  |  |  |  |  | 06/28/2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | 4 | 7 |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 个t |  | \% | 个4 | F | \% | $\uparrow \uparrow$ |  | \% | $\uparrow$ | $\overline{7}$ |
| Traffic Volume (vph) | 145 | 925 | 165 | 140 | 1185 | 125 | 165 | 350 | 140 | 280 | 510 | 345 |
| Future Volume (vph) | 145 | 925 | 165 | 140 | 1185 | 125 | 165 | 350 | 140 | 280 | 510 | 345 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Total Lost time (s) | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Lane Util. Factor | 1.00 | 0.95 |  | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 |
| Frpb, ped/bikes | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 |
| Flpb, ped/bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.98 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1750 | 3484 |  | 1767 | 3579 | 1530 | 1785 | 3411 |  | 1760 | 1921 | 1538 |
| Flt Permitted | 0.10 | 1.00 |  | 0.14 | 1.00 | 1.00 | 0.11 | 1.00 |  | 0.33 | 1.00 | 1.00 |
| Satd. Flow (perm) | 176 | 3484 |  | 258 | 3579 | 1530 | 215 | 3411 |  | 609 | 1921 | 1538 |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj. Flow (vph) | 145 | 925 | 165 | 140 | 1185 | 125 | 165 | 350 | 140 | 280 | 510 | 345 |
| RTOR Reduction (vph) | 0 | 9 | 0 | 0 | 0 | 42 | 0 | 28 | 0 | 0 | 0 | 97 |
| Lane Group Flow (vph) | 145 | 1081 | 0 | 140 | 1185 | 83 | 165 | 462 | 0 | 280 | 510 | 248 |
| Confl. Peds. (\#hr) | 12 |  | 9 | 9 |  | 12 | 10 |  | 24 | 24 |  | 10 |
| Heavy Vehicles (\%) | 2\% | 2\% | 0\% | 1\% | 2\% | 1\% | 0\% | 1\% | 1\% | 1\% | 0\% | 1\% |
| Turn Type | pm+pt | NA |  | pm+pt | NA | Perm | pm+pt | NA |  | pm+pt | NA | Perm |
| Protected Phases | 5 | , |  | 1 | - |  | 7 | 4 |  | 3 | . |  |
| Permitted Phases | 2 |  |  | - |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green, G (s) | 82.4 | 71.2 |  | 79.0 | 69.5 | 69.5 | 55.3 | 44.3 |  | 61.3 | 47.3 | 47.3 |
| Effective Green, g(s) | 82.4 | 71.2 |  | 79.0 | 69.5 | 69.5 | 55.3 | 44.3 |  | 61.3 | 47.3 | 47.3 |
| Actuated g/C Ratio | 0.52 | 0.45 |  | 0.49 | 0.43 | 0.43 | 0.35 | 0.28 |  | 0.38 | 0.30 | 0.30 |
| Clearance Time (s) | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 200 | 1550 |  | 216 | 1554 | 664 | 182 | 944 |  | 334 | 567 | 454 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0.05 | 0.31 |  | 0.04 | c0.33 |  | c0.06 | 0.14 |  | c0.07 | c0.27 |  |
| v/s Ratio Perm | 0.32 |  |  | 0.28 |  | 0.05 | 0.25 |  |  | 0.25 |  | 0.16 |
| v/c Ratio | 0.72 | 0.70 |  | 0.65 | 0.76 | 0.13 | 0.91 | 0.49 |  | 0.84 | 0.90 | 0.55 |
| Uniform Delay, d1 | 29.0 | 35.7 |  | 27.0 | 38.3 | 27.1 | 42.1 | 48.4 |  | 41.0 | 54.1 | 47.3 |
| Progression Factor | 1.00 | 1.00 |  | 0.99 | 0.90 | 0.71 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 12.3 | 2.6 |  | 5.8 | 3.2 | 0.3 | 40.9 | 0.4 |  | 16.6 | 17.0 | 1.3 |
| Delay (s) | 41.2 | 38.4 |  | 32.4 | 37.6 | 19.5 | 83.0 | 48.8 |  | 57.5 | 71.1 | 48.7 |
| Level of Service | D | D |  | C | D | B | F | D |  | E | E | D |
| Approach Delay (s) |  | 38.7 |  |  | 35.5 |  |  | 57.4 |  |  | 60.9 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 46.0 |  | HCM 2000 | Level of S | Service |  | D |  |  |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.83 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 160.0 |  | Sum of los | time (s) |  |  | 21.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 96.3\% |  | CU Level | f Service |  |  | F |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
7: Arch Rd \& Britannia Rd West


[^2]HCM Unsignalized Intersection Capacity Analysis

| 8: Earl St \& Britannia Rd West |  |  |  |  |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ |  | 1 | $\downarrow$ | 4 | \% |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个t |  | \% | 个4 | M |  |  |  |
| Traffic Volume (veh/h) | 1340 | 5 | 5 | 1455 | 0 | 20 |  |  |
| Future Volume (Veh/h) | 1340 | 5 | 5 | 1455 | 0 | 20 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate (vph) | 1340 | 5 | 5 | 1455 | 0 | 20 |  |  |
| Pedestrians |  |  |  |  | 5 |  |  |  |
| Lane Width (m) |  |  |  |  | 3.5 |  |  |  |
| Walking Speed (m/s) |  |  |  |  | 1.2 |  |  |  |
| Percent Blockage |  |  |  |  | 0 |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type T | TWLTL |  |  | TWLTL |  |  |  |  |
| Median storage veh) | 2 |  |  | 2 |  |  |  |  |
| Upstream signal ( m ) | 219 |  |  | 71 |  |  |  |  |
| pX, platoon unblocked |  |  | 0.76 |  | 0.83 | 0.76 |  |  |
| vC , conficting volume |  |  | 1350 |  | 2085 | 678 |  |  |
| vC1, stage 1 conf vol |  |  |  |  | 1348 |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  | 738 |  |  |  |
| vCu, unblocked vol |  |  | 835 |  | 1199 | 0 |  |  |
| tC, single (s) |  |  | 4.1 |  | 6.8 | 6.9 |  |  |
| tC, 2 stage (s) |  |  |  |  | 5.8 |  |  |  |
| tF (s) |  |  | 2.2 |  | 3.5 | 3.3 |  |  |
| p0 queue free \% |  |  | 99 |  | 100 | 98 |  |  |
| cM capacity (veh/h) |  |  | 613 |  | 278 | 828 |  |  |
| Direction, Lane \# | EB 1 | EB2 | WB 1 | WB2 | WB3 | NB 1 |  |  |
| Volume Total | 893 | 452 | 5 | 728 | 728 | 20 |  |  |
| Volume Left | 0 | 0 | 5 | 0 | 0 | 0 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 20 |  |  |
| cSH | 1700 | 1700 | 613 | 1700 | 1700 | 828 |  |  |
| Volume to Capacity | 0.53 | 0.27 | 0.01 | 0.43 | 0.43 | 0.02 |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.6 |  |  |
| Control Delay (s) | 0.0 | 0.0 | 10.9 | 0.0 | 0.0 | 9.5 |  |  |
| Lane LOS |  |  | B |  |  | A |  |  |
| Approach Delay (s) | 0.0 |  | 0.0 |  |  | 9.5 |  |  |
| Approach LOS |  |  |  |  |  | A |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 50.2\% |  | CU Level | Service | A |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

Timings
9: Britannia Rd West \& Ellesboro Dr 06/28/2023


## Intersection Summar

Cycle Length: 160
Actuated Cycle Length: 160
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and $6: W B T$, Start of Green
atural Cycle: 75
Control Type: Actuated-Coordinated
Maximum Vion Rign: 0.58

| Intersection Signal Delay: 7.6 | Intersection LOS: A |
| :--- | :--- |
| Intersection Capacity Utilization $64.9 \%$ | ICU Level of Service C |

Analysis Period (min) 15
Splits and Phases: 9: Britannia Rd West \& Ellesboro Dr



HCM Signalized Intersection Capacity Analysis
9: Britannia Rd West \& Ell

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 $\uparrow$ | 性 |  | \% | 7 |  |
| Traffic Volume (vph) | 15 | 1345 | 1425 | 75 | 100 | 35 |  |
| Future Volume (vph) | 15 | 1345 | 1425 | 75 | 100 | 35 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width | 3.5 | 3.7 | 3.7 | 3.5 | 3.5 | 3.5 |  |
| Total Lost time (s) | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |  | 1.00 | 1.00 |  |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 0.98 |  |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.99 |  | 1.00 | 0.85 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1783 | 3614 | 3583 |  | 1785 | 1520 |  |
| Flt Permitted | 0.15 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (perm) | 288 | 3614 | 3583 |  | 1785 | 1520 |  |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj. Flow (vph) | 15 | 1345 | 1425 | 75 | 100 | 35 |  |
| RTOR Reduction (vph) | 0 | 0 | 1 | 0 | 0 | 27 |  |
| Lane Group Flow (vph) | 15 | 1345 | 1499 | 0 | 100 | 8 |  |
| Confl. Peds. (\#hr) | 5 |  |  | 5 |  | 5 |  |
| Heavy Vehicles (\%) | 0\% | 1\% | 1\% | 0\% | 0\% | 3\% |  |
| Turn Type | Perm | NA | NA |  | Perm | Perm |  |
| Protected Phases |  | 2 | 6 |  |  |  |  |
| Permitted Phases | 2 |  |  |  | 8 | 8 |  |
| Actuated Green, G (s) | 132.6 | 132.6 | 132.6 |  | 15.3 | 15.3 |  |
| Effective Green, g (s) | 132.6 | 132.6 | 132.6 |  | 15.3 | 15.3 |  |
| Actuated g/C Ratio | 0.83 | 0.83 | 0.83 |  | 0.10 | 0.10 |  |
| Clearance Time (s) | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 238 | 2995 | 2969 |  | 170 | 145 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | 0.37 | c0.42 |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.05 |  |  |  | c0.06 | 0.01 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.06 | 0.45 | 0.50 |  | 0.59 | 0.05 |  |
| Uniform Delay, d1 | 2.5 | 3.7 | 4.0 |  | 69.3 | 65.8 |  |
| Progression Factor | 1.03 | 1.06 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 0.4 | 0.4 | 0.6 |  | 5.1 | 0.2 |  |
| Delay (s) | 2.9 | 4.3 | 4.7 |  | 74.5 | 65.9 |  |
| Level of Service | A | A | A |  | E | E |  |
| Approach Delay (s) |  | 4.3 | 4.7 |  | 72.2 |  |  |
| Approach LOS |  | A | A |  | E |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 7.5 |  | HCM 2000 | evel of Service | A |
| HCM 2000 Volume to Capacity ratio |  |  | 0.51 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 160.0 |  | Sum of los | time (s) | 12.1 |
| Intersection Capacity Utilization |  |  | 64.9\% | Cu Level of Service |  |  | C |
| Analysis Period (min) |  |  | 15 |  |  |  |  |


| Existing PM 21-51 Queen Street North 10:40 am 09/24/2021 Existing PM Peak Hour |  |
| :--- | ---: |
| BA Group | Synchro 11 Report <br> Page 13 |


| HCM Unsignalized Intersection Capacity Analysis 1：Queen Street North \＆Matlock Ave |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  | $\dagger$ | 7 |  | $\dagger$ |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | Y |  | 个t |  | \％ | 个4 |  |  |
| Traffic Volume（veh／h） | 30 | 20 | 970 | 40 | 15 | 570 |  |  |
| Future Volume（Veh／h） | 30 | 20 | 970 | 40 | 15 | 570 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |  |
| Grade | 0\％ |  | 0\％ |  |  | 0\％ |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Hourly flow rate（vph） | 33 | 22 | 1054 | 43 | 16 | 620 |  |  |
| Pedestrians | 1 |  |  |  |  |  |  |  |
| Lane Width（m） | 3.5 |  |  |  |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  | TWLTL |  |  | None |  |  |
| Median storage veh） |  |  | 2 |  |  |  |  |  |
| Upstream signal（ m ） |  |  | 313 |  |  |  |  |  |
| pX，platoon unblocked | 0.89 | 0.89 |  |  | 0.89 |  |  |  |
| vC ，conficting volume | 1418 | 550 |  |  | 1098 |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1076 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 342 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1220 | 242 |  |  | 859 |  |  |  |
| tC，single（s） | 7.3 | 7.4 |  |  | 4.9 |  |  |  |
| tC， 2 stage（s） | 6.3 |  |  |  |  |  |  |  |
| tF（s） | 3.7 | 3.5 |  |  | 2.6 |  |  |  |
| p0 queue free \％ | 88 | 96 |  |  | 97 |  |  |  |
| cM capacity（veh／h） | 278 | 616 |  |  | 508 |  |  |  |
| Direction，Lane \＃ | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | SB 3 |  |  |
| Volume Total | 55 | 703 | 394 | 16 | 310 | 310 |  |  |
| Volume Left | 33 | 0 | 0 | 16 | 0 | 0 |  |  |
| Volume Right | 22 | 0 | 43 | 0 | 0 | 0 |  |  |
| cSH | 356 | 1700 | 1700 | 508 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.15 | 0.41 | 0.23 | 0.03 | 0.18 | 0.18 |  |  |
| Queue Length 95th（m） | 4.3 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 17.0 | 0.0 | 0.0 | 12.3 | 0.0 | 0.0 |  |  |
| Lane LOS | C |  |  | B |  |  |  |  |
| Approach Delay（s） | 17.0 | 0.0 |  | 0.3 |  |  |  |  |
| Approach LOS | c |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.6 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 38．1\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis

| 2：Queen Street North \＆ 40 Queen St N Driveway／53 Queen St Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | $\geqslant$ | 7 | － | 4 | 4 | $\uparrow$ |  | － | $\dagger$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | ${ }^{7}$ | 性 |  | \％ | 个 ${ }^{\text {a }}$ |  |
| Traffic Volume（veh／h） | 0 | 0 | 0 | 0 | ， | 0 | 0 | 1010 | 0 | 0 | 600 |  |
| Future Volume（Veh／h） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1010 | 0 | 0 | 600 |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1148 | 0 | 0 | 682 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（m／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | TWLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.86 | 0.86 |  | 0.86 | 0.86 | 0.86 |  |  |  | 0.86 |  |  |
| vC, conflicting volume | 1256 | 1830 | 341 | 1489 | 1830 | 574 | 682 |  |  | 1148 |  |  |
| vC1，stage 1 conf vol | 682 | 682 |  | 1148 | 1148 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 574 | 1148 |  | 341 | 682 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 976 | 1642 | 341 | 1246 | 1642 | 184 | 682 |  |  | 851 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF （s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity（veh／h） | 373 | 271 | 661 | 263 | 271 | 718 | 920 |  |  | 686 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 0 | 0 | 765 | 383 | 0 | 455 | 227 |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| CSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.00 | 0.45 | 0.23 | 0.00 | 0.27 | 0.13 |  |  |  |  |
| Queue Length 95th（ $m$ ） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 31．3\％ |  | CU Level | f Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^3]| HCM Unsignalized Intersection Capacity Analysis 3：Queen Street North \＆ 40 Queen St S Driveway |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ |  | 4 | $\dagger$ |  | $\pm$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | \％ |  | \％ | 个个 | 性 |  |  |  |
| Traffic Volume（veh／h） | 0 | 0 | － | 1010 | 600 | 0 |  |  |
| Future Volume（Veh／h） | 0 | 0 | 0 | 1010 | 600 | 0 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |  |  |
| Hourly flow rate（vph） | 0 | 0 | 0 | 1161 | 690 | 0 |  |  |
| Pedestrians | 3 |  |  |  |  |  |  |  |
| Lane Width（m） | 3.5 |  |  |  |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | WLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ $m$ ） |  |  |  | 186 |  |  |  |  |
| pX，platoon unblocked | 0.86 |  |  |  |  |  |  |  |
| VC ，conflicting volume | 1274 | 348 | 693 |  |  |  |  |  |
| vC1，stage 1 conf vol | 693 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 580 |  |  |  |  |  |  |  |
| vCu，unblocked vol | 983 | 348 | 693 |  |  |  |  |  |
| tC ，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 100 | 100 | 100 |  |  |  |  |  |
| cM capacity（veh／h） | 417 | 652 | 909 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 0 | 0 | 580 | 580 | 460 | 230 |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| cSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.34 | 0.34 | 0.27 | 0.14 |  |  |
| Queue Length 95th（ $m$ ） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | A |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 31．3\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |


| HCM Unsignalized Intersection Capacity Analysis <br> 4：Queen Street North \＆Petro Canada N Driveway／Existing Site Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{*}{ }$ |  |  |  |  |  |  | $\uparrow$ |  |  | $\dagger$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | \％ | 个t |  | ${ }^{*}$ | 个t |  |
| Traffic Volume（veh／h） | 0 | － | 0 | 5 | 0 | 0 | 5 | 1010 | 10 | 5 | 585 | 10 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 1010 | 10 | 5 | 585 | 10 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 1161 | 11 | 6 | 672 | 11 |
| Pedestrians |  | 3 |  |  | 6 |  |  | 1 |  |  |  |  |
| Lane Width（m） |  | 3.7 |  |  | 3.7 |  |  | 3.6 |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  | 1.2 |  |  | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage |  | 0 |  |  | 1 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 159 |  |  |  |  |
| pX，platoon unblocked | 0.85 | 0.85 |  | 0.85 | 0.85 | 0.85 |  |  |  | 0.85 |  |  |
| vC, conficting volume | 1285 | 1882 | 346 | 1534 | 1882 | 592 | 686 |  |  | 1178 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 692 | 692 |  | 1184 | 1184 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 592 | 1190 |  | 349 | 698 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 985 | 1687 | 346 | 1277 | 1687 | 170 | 686 |  |  | 859 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \％ | 100 | 100 | 100 | 98 | 100 | 100 | 99 |  |  | 99 |  |  |
| cM capacity（veh／h） | 364 | 256 | 654 | 251 | 258 | 720 | 915 |  |  | 669 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 6 | 6 | 774 | 398 | 6 | 448 | 235 |  |  |  |  |
| Volume Left | 0 | 6 | 6 | 0 | 0 | 6 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 11 |  |  |  |  |
| cSH | 1700 | 251 | 915 | 1700 | 1700 | 669 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.02 | 0.01 | 0.46 | 0.23 | 0.01 | 0.26 | 0.14 |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 0.6 | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 19.7 | 9.0 | 0.0 | 0.0 | 10.4 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | C | A |  |  | B |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 19.7 | 0.0 |  |  | 0.1 |  |  |  |  |  |  |
| Approach LOS | A | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 38．6\％ |  | Level | f Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^4]| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 5：Queen Street North \＆Petro Canada S Driveway |  |  |  |  |  |  |  | 06／28／2023 |
|  | ＊ |  |  | $\dagger$ |  | $\stackrel{ }{*}$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | \％ |  | \％ | 个4 | 性 |  |  |  |
| Traffic Volume（veh／h） | 0 | 5 | 0 | 1025 | 580 | 10 |  |  |
| Future Volume（Veh／h） | 0 | 5 | 0 | 1025 | 580 | 10 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |  |  |
| Hourly flow rate（vph） | 0 | 6 | 0 | 1165 | 659 | 11 |  |  |
| Pedestrians | 3 |  |  | 2 |  |  |  |  |
| Lane Width（m） | 3.5 |  |  | 3.6 |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | WLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ m ） |  |  |  | 127 |  |  |  |  |
| pX，platoon unblocked | 0.85 |  |  |  |  |  |  |  |
| VC, conflicting volume | 1250 | 340 | 673 |  |  |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 668 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 582 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 932 | 340 | 673 |  |  |  |  |  |
| tC，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 100 | 99 | 100 |  |  |  |  |  |
| cM capacity（veh／h） | 431 | 659 | 925 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB1 | SB 2 |  |  |
| Volume Total | 6 | 0 | 582 | 582 | 439 | 231 |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 6 | 0 | 0 | 0 | 0 | 11 |  |  |
| cSH | 659 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.01 | 0.00 | 0.34 | 0.34 | 0.26 | 0.14 |  |  |
| Queue Length 95th（m） | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 10.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | B |  |  |  |  |  |  |  |
| Approach Delay（s） | 10.5 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39．0\％ |  | Level | Service | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

Timings

| 6：Queen Str | Q |  |  |  | Brita |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | 7 |  |  | 4 | 4 |  | $\dagger$ | $\pm$ |  |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |  |
| Lane Configurations | \％ | 性 | \％ | 个个 | F | \％ | 个t | ${ }^{7}$ | $\uparrow$ | F |  |
| Traffic Volume（vph） | 215 | 1575 | 80 | 625 | 325 | 95 | 485 | 140 | 305 | 140 |  |
| Future Volume（vph） | 215 | 1575 | 80 | 625 | 325 | 95 | 485 | 140 | 305 | 140 |  |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | Perm | NA | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm |  |
| Protected Phases | 5 | 2 | 1 | 6 |  |  | 4 | 3 | 8 |  |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |  |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |  |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 12.0 | 12.0 | 8.0 | 12.0 | 12.0 |  |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 38.9 | 38.9 | 11.0 | 38.9 | 38.9 |  |
| Total Spit（s） | 19.0 | 92.0 | 11.0 | 84.0 | 84.0 | 41.0 | 41.0 | 16.0 | 57.0 | 57.0 |  |
| Total Split（\％） | 11．9\％ | 57．5\％ | 6．9\％ | 52．5\％ | 52．5\％ | 25．6\％ | 25．6\％ | 10．0\％ | 35．6\％ | 35．6\％ |  |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 |  |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 3.9 | 3.9 | 0.0 | 3.9 | 3.9 |  |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 7.9 | 7.9 | 3.0 | 7.9 | 7.9 |  |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lead |  |  |  |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |  |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |  |
| Act Effict Green（s） | 102.1 | 87.3 | 94.1 | 82.0 | 82.0 | 31.2 | 31.2 | 51.6 | 46.7 | 46.7 |  |
| Actuated g／C Ratio | 0.64 | 0.55 | 0.59 | 0.51 | 0.51 | 0.20 | 0.20 | 0.32 | 0.29 | 0.29 |  |
| $\mathrm{V} / \mathrm{c}$ Ratio | 0.43 | 0.87 | 0.61 | 0.36 | 0.36 | 0.50 | 0.89 | 0.74 | 0.57 | 0.27 |  |
| Control Delay | 15.1 | 37.9 | 52.2 | 22.4 | 4.4 | 66.6 | 77.1 | 62.6 | 52.3 | 7.1 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 15.1 | 37.9 | 52.2 | 22.4 | 4.4 | 66.6 | 77.1 | 62.6 | 52.3 | 7.1 |  |
| LOS | B | D | D | c | A | E | E | E | D | A |  |
| Approach Delay |  | 35.3 |  | 19.0 |  |  | 75.7 |  | 44.0 |  |  |
| Approach LOS |  | D |  | B |  |  | E |  | D |  |  |

## Intersection Summary

Cycle Length： 160
Actuated Cycle Length： 160
Offset： 13 （8\％），Referenced to phase 2：EBTL and $6:$ WBTL，Start of Green
Control Type：Actuated－Coordinated
Control Type：Actuated－C

| Maximum vic Ratio：D．89 | Intersection LOS：D |
| :--- | :--- |
| Intersection Signal Delay：39．3 | ICU Level of Service |
| Intersection Capacity Utilization 105．6\％ |  |

Intersection Capacity Utilization 105．6\％
ICU Level of Service G
Analysis Period（min） 15


Queues

| 6: Queen Stree |  | en St | eet N | rth \& | ritan | R | West |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ | 1 | 4 | 4 | 4 | 4 |  | $\dagger$ | $\downarrow$ |  |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |  |
| Lane Group Flow (vph) | 215 | 1675 | 80 | 625 | 325 | 95 | 610 | 140 | 305 | 140 |  |
| v/c Ratio | 0.43 | 0.87 | 0.61 | 0.36 | 0.36 | 0.50 | 0.89 | 0.74 | 0.57 | 0.27 |  |
| Control Delay | 15.1 | 37.9 | 52.2 | 22.4 | 4.4 | 66.6 | 77.1 | 62.6 | 52.3 | 7.1 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 15.1 | 37.9 | 52.2 | 22.4 | 4.4 | 66.6 | 77.1 | 62.6 | 52.3 | 7.1 |  |
| Queue Length 50th (m) | 29.5 | 256.7 | 8.2 | 67.1 | 18.6 | 28.3 | 101.6 | 34.0 | 85.2 | 0.0 |  |
| Queue Length 95th (m) | 42.8 | 294.3 | \#30.9 | 85.9 | 32.1 | 49.1 | 126.1 | \#54.2 | 117.9 | 16.9 |  |
| Internal Link Dist ( $m$ ) |  | 110.7 |  | 83.1 |  |  | 135.0 |  | 103.4 |  |  |
| Turn Bay Length ( m ) | 95.0 |  | 60.0 |  | 45.0 | 40.0 |  | 35.0 |  |  |  |
| Base Capacity (vph) | 521 | 1927 | 132 | 1747 | 897 | 203 | 724 | 194 | 566 | 531 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.41 | 0.87 | 0.61 | 0.36 | 0.36 | 0.47 | 0.84 | 0.72 | 0.54 | 0.26 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

5y Future Background AM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Background AM

BA Group | Synchro 11 Report |
| ---: |
| Page 7 |

HCM Signalized Intersection Capacity Analysis


| 5y Future Background AM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Background AM |  |
| :--- | ---: |
| BA Group | Synchro 11 Report |
| Page 8 |  |

## HCM Unsignalized Intersection Capacity Analysis

| 7: Arch Rd \& Britannia Rd West |  |  |  |  |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ | $\geqslant$ | 1 | $\Perp$ | 4 | \% |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个t |  | \% | 个4 | M |  |  |  |
| Traffic Volume (veh/h) | 1835 | 5 | 10 | 1025 | 5 | 10 |  |  |
| Future Volume (Veh/h) | 1835 | 5 | 10 | 1025 | 5 | 10 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate (vph) | 1835 | 5 | 10 | 1025 | 5 | 10 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width (m) |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type | None |  |  | WLTL |  |  |  |  |
| Median storage veh) |  |  |  | 2 |  |  |  |  |
| Upstream signal ( m ) | 107 |  |  | 182 |  |  |  |  |
| pX, platoon unblocked |  |  | 0.58 |  | 0.61 | 0.58 |  |  |
| VC, conflicting volume |  |  | 1840 |  | 2370 | 920 |  |  |
| vC1, stage 1 conf vol |  |  |  |  | 1838 |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  | 532 |  |  |  |
| vCu, unblocked vol |  |  | 1006 |  | 1545 | 0 |  |  |
| tC, single (s) |  |  | 4.1 |  | 6.8 | 7.1 |  |  |
| $\mathrm{tC}, 2$ stage (s) |  |  |  |  | 5.8 |  |  |  |
| tF (s) |  |  | 2.2 |  | 3.5 | 3.4 |  |  |
| p0 queue free \% |  |  | 98 |  | 97 | 98 |  |  |
| cM capacity (veh/h) |  |  | 405 |  | 177 | 620 |  |  |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | WB3 | NB 1 |  |  |
| Volume Total | 1223 | 617 | 10 | 512 | 512 | 15 |  |  |
| Volume Left | 0 | 0 | 10 | 0 | 0 | 5 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 10 |  |  |
| cSH | 1700 | 1700 | 405 | 1700 | 1700 | 338 |  |  |
| Volume to Capacity | 0.72 | 0.36 | 0.02 | 0.30 | 0.30 | 0.04 |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.1 |  |  |
| Control Delay (s) | 0.0 | 0.0 | 14.1 | 0.0 | 0.0 | 16.1 |  |  |
| Lane LOS |  |  | B |  |  | C |  |  |
| Approach Delay (s) | 0.0 |  | 0.1 |  |  | 16.1 |  |  |
| Approach LOS |  |  |  |  |  | C |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 60.9\% |  | CU Level | Service | B |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
8: Earl St \& Britannia Rd West


[^5]Timings
9: Britannia Rd West \& Ellesboro Dr 06/28/2023
 Lead/Lag
Recall Mode Act Efft Green (s)
C-Max C-Max C-Max None None

$\begin{array}{llllll}\text { Actuated g/C Ratio } & 0.87 & 0.87 & 0.87 & 0.08 & 0.08\end{array}$
v/c Ratio
Control Delay
Queue Delay Total Delay Approach Delay
Approach LOS

## Intersection Summary

Cycle Length: 160
Actuated Cycle Length: 160
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and $6: W B T$, Start of Green
Natural Cycle: 90
\(\begin{array}{ll}Control Type: Actuated-Coordinated \& <br>

\)|  Maximum v/c Ratio:  0.59 |  |
| :--- | :--- |
|  Intersection Signal Delay:  3.7 |  Intersection LOS: A  |
|  Intersection Capacity Utiization 76.3\%  |  ICU Level of Service D  |\end{array}

Analysis Period (min) 15


Queues
9: Britannia Rd West \& Ellesboro Dr

| Lane Group | EBL | EBT | WBT | SBL | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Lane Group Flow (vph) | 30 | 1835 | 1075 | 60 | 30 |
| v/c Ratio | 0.07 | 0.59 | 0.36 | 0.40 | 0.20 |
| Control Delay | 1.2 | 1.5 | 2.9 | 77.8 | 23.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 1.2 | 1.5 | 2.9 | 77.8 | 23.8 |
| Queue Length 50th $(\mathrm{m})$ | 0.7 | 24.1 | 34.7 | 19.5 | 0.0 |
| Queue Length 95th $(\mathrm{m})$ | m 0.9 | 30.6 | 45.3 | 35.5 | 11.4 |
| Internal Link Dist $(\mathrm{m})$ |  | 46.6 | 115.6 | 80.1 | 15 |
| Turn Bay Length $(\mathrm{m})$ | 45.0 |  |  |  | 15.0 |
| Base Capacity (vph) | 408 | 3120 | 2967 | 434 | 375 |
| Starvation Cap Reductn | 0 | 125 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.61 | 0.36 | 0.14 | 0.08 |
| Intersection Summary |  |  |  |  |  |
| Volume for 95th percentie equeue is metered by upstream signal |  |  |  |  |  |

m Volume for 95 th percentile queue is metered by upstream signal.

[^6]| HCM Signalized Intersection Capacity Analysis 9：Britannia Rd West \＆Ellesboro Dr |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | － | 4 | ＊ | 4 |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |  |
| Lane Configurations | \％ | 个4 | 性 |  | \％ | 「 |  |  |
| Traffic Volume（vph） | 30 | 1835 | 1005 | 70 | 60 | 30 |  |  |
| Future Volume（vph） | 30 | 1835 | 1005 | 70 | 60 | 30 |  |  |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Lane Width | 3.5 | 3.7 | 3.7 | 3.5 | 3.5 | 3.5 |  |  |
| Total Lost time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 0.95 |  | 1.00 | 1.00 |  |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 0.97 |  |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Frt | 1.00 | 1.00 | 0.99 |  | 1.00 | 0.85 |  |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Flow（prot） | 1729 | 3579 | 3403 |  | 1782 | 1447 |  |  |
| Fit Permitted | 0.26 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Fow（perm） | 469 | 3579 | 3403 |  | 1782 | 1447 |  |  |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj．Flow（vph） | 30 | 1835 | 1005 | 70 | 60 | 30 |  |  |
| RTOR Reduction（vph） | 0 | 0 | 1 | 0 | 0 | 28 |  |  |
| Lane Group Flow（vph） | 30 | 1835 | 1074 | 0 | 60 | 2 |  |  |
| Confl．Peds．（\＃／hr） | 4 |  |  | 4 | ， | 12 |  |  |
| Heavy Vehicles（\％） | 3\％ | 2\％ | 6\％ | 6\％ | 0\％ | 7\％ |  |  |
| Turn Type | Perm | NA | NA |  | Perm | Perm |  |  |
| Protected Phases |  | 2 | 6 |  |  |  |  |  |
| Permitted Phases | 2 |  |  |  | 8 | 8 |  |  |
| Actuated Green，G（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Effective Green，g（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Actuated g／C Ratio | 0.86 | 0.86 | 0.86 |  | 0.07 | 0.07 |  |  |
| Clearance Time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |
| Lane Grp Cap（vph） | 401 | 3066 | 2915 |  | 120 | 97 |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | c0．51 | 0.32 |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.06 |  |  |  | c0．03 | 0.00 |  |  |
| v／c Ratio | 0.07 | 0.60 | 0.37 |  | 0.50 | 0.02 |  |  |
| Uniform Delay，d1 | 1.8 | 3.4 | 2.4 |  | 72.0 | 69.7 |  |  |
| Progression Factor | 0.44 | 0.28 | 1.00 |  | 1.00 | 1.00 |  |  |
| Incremental Delay，d2 | 0.2 | 0.4 | 0.4 |  | 3.3 | 0.1 |  |  |
| Delay（s） | 1.0 | 1.4 | 2.8 |  | 75.2 | 69.7 |  |  |
| Level of Service | A | A | A |  | E | E |  |  |
| Approach Delay（s） |  | 1.4 | 2.8 |  | 73.4 |  |  |  |
| Approach LOS |  | A | A |  | E |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 4.0 |  | HCM 2000 | evel of Service | A |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.59 |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | ime（s） | 12.1 |  |
| Intersection Capacity Utilization |  |  | 76．3\％ |  | CU Level | Service | D |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |

5y Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Background AM
BA Group

HCM Unsignalized Intersection Capacity Analysis
1：Queen Street North \＆Matlock Ave
06／28／2023

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | Y |  | 个t |  | ${ }^{*}$ | 个个 |
| Traffic Volume（veh／h） | 55 | 15 | 560 | 60 | 15 | 1070 |
| Future Volume（Veh／h） | 55 | 15 | 560 | 60 | 15 | 1070 |
| Sign Control | Stop |  | Free |  |  | Free |
| Grade | 0\％ |  | 0\％ |  |  | 0\％ |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate（vph） | 60 | 16 | 609 | 65 | 16 | 1163 |
| Pedestrians | 6 |  |  |  |  | 1 |
| Lane Width（m） | 3.5 |  |  |  |  | 3.6 |
| Walking Speed（m／s） | 1.2 |  |  |  |  | 1.2 |
| Percent Blockage | 0 |  |  |  |  | 0 |
| Right turn flare（veh） |  |  |  |  |  |  |
| Median type |  |  | TWLTL |  |  | None |

None

Median storage veh）
Upstream signal（ m ）
Upstream signal（ $m$ ）


[^7]| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2：Queen Street North \＆ 40 Queen St N Driveway／53 Queen St Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
|  | $\stackrel{*}{ }$ |  |  | 1 |  |  | 4 | $\dagger$ |  |  | $\dagger$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | ${ }_{\dagger}$ |  | \％ | 个t |  | ${ }^{7}$ | 个t |  |
| Traffic Volume（veh／h） | 0 | ， | 5 | 5 | 0 | 0 | 5 | 620 | 0 | 5 | 1120 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 620 | 0 | 5 | 1120 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate（vph） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 681 | 0 | 5 | 1231 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.93 | 0.93 |  | 0.93 | 0.93 | 0.93 |  |  |  | 0.93 |  |  |
| vC ，conficting volume | 1592 | 1932 | 616 | 1322 | 1932 | 340 | 1231 |  |  | 681 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1241 | 1241 |  | 691 | 691 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 350 | 691 |  | 630 | 1241 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1489 | 1855 | 616 | 1200 | 1855 | 148 | 1231 |  |  | 513 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \％ | 100 | 100 | 99 | 99 | 100 | 100 | 99 |  |  | 99 |  |  |
| cM capacity（veh／h） | 181 | 222 | 439 | 334 | 219 | 820 | 573 |  |  | 991 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 5 | 5 | 5 | 454 | 227 | 5 | 821 | 410 |  |  |  |  |
| Volume Left | 0 | 5 | 5 | 0 | 0 | 5 | 0 | 0 |  |  |  |  |
| Volume Right | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| cSH | 439 | 334 | 573 | 1700 | 1700 | 991 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.01 | 0.01 | 0.01 | 0.27 | 0.13 | 0.01 | 0.48 | 0.24 |  |  |  |  |
| Queue Length 95th（m） | 0.3 | 0.4 | 0.2 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 13.3 | 15.9 | 11.3 | 0.0 | 0.0 | 8.7 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | B | C | B |  |  | A |  |  |  |  |  |  |
| Approach Delay（s） | 13.3 | 15.9 | 0.1 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | B | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 41．8\％ |  | Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period（min）

| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{*}{ }$ |  | 4 | $\dagger$ | $\dagger$ | $\checkmark$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | M |  | ${ }^{7}$ | 个4 | 个 ${ }_{\text {a }}$ |  |  |  |
| Traffic Volume（veh／h） | 5 | 5 | 0 | 620 | 1130 | 0 |  |  |
| Future Volume（Veh／h） | 5 | 5 | 0 | 620 | 1130 | 0 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |  |  |
| Hourly flow rate（vph） | 5 | 5 | 0 | 681 | 1242 | 0 |  |  |
| Pedestrians | 2 |  |  |  |  |  |  |  |
| Lane Width（m） | 3.5 |  |  |  |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | TWLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ m ） |  |  |  | 186 |  |  |  |  |
| pX，platoon unblocked | 0.92 |  |  |  |  |  |  |  |
| VC, conficting volume | 1584 | 623 | 1244 |  |  |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1244 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 340 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1466 | 623 | 1244 |  |  |  |  |  |
| tC，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 98 | 99 | 100 |  |  |  |  |  |
| cM capacity（veh／h） | 230 | 433 | 566 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 10 | 0 | 340 | 340 | 828 | 414 |  |  |
| Volume Left | 5 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 5 | 0 | 0 | 0 | 0 | 0 |  |  |
| cSH | 300 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.03 | 0.00 | 0.20 | 0.20 | 0.49 | 0.24 |  |  |
| Queue Length 95th（m） | 0.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 17.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | C |  |  |  |  |  |  |  |
| Approach Delay（s） | 17.4 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 41．2\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

BA Group

| HCM Unsignalized Intersection Capacity Analysis <br> 4：Queen Street North \＆Petro Canada N Driveway／Existing Site Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{*}{ }$ |  |  | 7 |  | 4 | 4 | $\uparrow$ |  |  | $\dagger$ | $\checkmark$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | $\uparrow$ |  | \％ | 个t |  | ${ }^{7}$ | 个t |  |
| Traffic Volume（veh／h） | 0 | 0 | 0 | 30 | 0 | 20 | 10 | 600 | 25 | 15 | 1110 | 10 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 30 | 0 | 20 | 10 | 600 | 25 | 15 | 1110 | 10 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 33 | 0 | 22 | 11 | 659 | 27 | 16 | 1220 | 11 |
| Pedestrians |  | 2 |  |  | 28 |  |  |  |  |  |  |  |
| Lane Width（m） |  | 3.7 |  |  | 3.7 |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  | 1.2 |  |  | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage |  | 0 |  |  | 2 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 159 |  |  |  |  |
| pX，platoon unblocked | 0.91 | 0.91 |  | 0.91 | 0.91 | 0.91 |  |  |  | 0.91 |  |  |
| vC ，conficting volume | 1633 | 1996 | 618 | 1364 | 1988 | 371 | 1233 |  |  | 714 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1260 | 1260 |  | 722 | 722 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 374 | 736 |  | 642 | 1265 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1495 | 1894 | 618 | 1200 | 1886 | 106 | 1233 |  |  | 484 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 100 | 90 | 100 | 97 | 98 |  |  | 98 |  |  |
| cM capacity（veh／h） | 174 | 212 | 437 | 324 | 205 | 828 | 571 |  |  | 966 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 55 | 11 | 439 | 247 | 16 | 813 | 418 |  |  |  |  |
| Volume Left | 0 | 33 | 11 | 0 | 0 | 16 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 22 | 0 | 0 | 27 | 0 | 0 | 11 |  |  |  |  |
| cSH | 1700 | 428 | 571 | 1700 | 1700 | 966 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.13 | 0.02 | 0.26 | 0.15 | 0.02 | 0.48 | 0.25 |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 3.5 | 0.5 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 14.7 | 11.4 | 0.0 | 0.0 | 8.8 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | B | B |  |  | A |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 14.7 | 0.2 |  |  | 0.1 |  |  |  |  |  |  |
| Approach LOS | A | B |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 41．0\％ |  | Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

5y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Background PM
BA Group

| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{*}{ }$ |  | 4 | $\dagger$ |  | $\checkmark$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | M |  | \％ | 个4 | 个1 |  |  |  |
| Traffic Volume（veh／h） | 5 | 15 | 5 | 630 | 1140 | 0 |  |  |
| Future Volume（Veh／h） | 5 | 15 | 5 | 630 | 1140 | 0 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |  |  |
| Hourly flow rate（vph） | 5 | 16 | 5 | 692 | 1253 | 0 |  |  |
| Pedestrians | 2 |  |  | 4 |  |  |  |  |
| Lane Width（m） | 3.5 |  |  | 3.6 |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | WLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ m ） |  |  |  | 127 |  |  |  |  |
| pX，platoon unblocked | 0.90 |  |  |  |  |  |  |  |
| VC, conficting volume | 1611 | 632 | 1255 |  |  |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1255 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 356 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1455 | 632 | 1255 |  |  |  |  |  |
| tC，single（s） | 6.8 | 7.0 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.4 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 98 | 96 | 99 |  |  |  |  |  |
| cM capacity（veh／h） | 227 | 409 | 560 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 21 | 5 | 346 | 346 | 835 | 418 |  |  |
| Volume Left | 5 | 5 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 16 | 0 | 0 | 0 | 0 | 0 |  |  |
| cSH | 343 | 560 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.06 | 0.01 | 0.20 | 0.20 | 0.49 | 0.25 |  |  |
| Queue Length 95th（m） | 1.6 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 16.2 | 11.5 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | C | B |  |  |  |  |  |  |
| Approach Delay（s） | 16.2 | 0.1 |  |  | 0.0 |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.2 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 42．8\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

BA Group
Page 5

Timings
6：Queen Street South／Queen Street North \＆Britannia Rd West

|  | $\stackrel{ }{ }$ |  | 7 |  |  |  | 4 |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations | \％ | 个t | \％ | 个个 | $\overline{7}$ | \％ | 中 ${ }^{\text {a }}$ | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 145 | 950 | 140 | 1215 | 125 | 165 | 365 | 280 | 530 | 345 |
| Future Volume（vph） | 145 | 950 | 140 | 1215 | 125 | 165 | 365 | 280 | 530 | 345 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 | 1 | 6 |  | 7 | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 7 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 5.0 | 12.0 | 8.0 | 12.0 | 12.0 |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 9.5 | 38.9 | 11.0 | 38.9 | 38.9 |
| Total Spit（s） | 15.0 | 71.0 | 14.0 | 70.0 | 70.0 | 15.0 | 47.0 | 28.0 | 60.0 | 60.0 |
| Total Split（\％） | 9．4\％ | 44．4\％ | 8．8\％ | 43．8\％ | 43．8\％ | 9．4\％ | 29．4\％ | 17．5\％ | 37．5\％ | 37．5\％ |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 0.0 | 3.9 | 0.0 | 3.9 | 3.9 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 | 3.0 | 7.9 | 7.9 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |
| Act Effct Green（s） | 84.1 | 68.3 | 82.0 | 67.3 | 67.3 | 54.8 | 38.0 | 67.9 | 48.1 | 48.1 |
| Actuated g／C Ratio | 0.53 | 0.43 | 0.51 | 0.42 | 0.42 | 0.34 | 0.24 | 0.42 | 0.30 | 0.30 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.75 | 0.75 | 0.65 | 0.81 | 0.18 | 0.86 | 0.60 | 0.72 | 0.92 | 0.59 |
| Control Delay | 50.8 | 42.7 | 37.8 | 42.2 | 6.6 | 73.6 | 53.8 | 41.8 | 75.5 | 26.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 50.8 | 42.7 | 37.8 | 42.2 | 6.6 | 73.6 | 53.8 | 41.8 | 75.5 | 26.9 |
| LOS | D | D | D | D | A | E | D | D | E | C |
| Approach Delay |  | 43.6 |  | 38.8 |  |  | 58.7 |  | 52.8 |  |
| Approach LOS |  | D |  | D |  |  | E |  | D |  |

$\frac{\text { Intersection Summary }}{\text { Cycle Length：} 160}$
Cycle Length： 160
Actuated Cycle Len
Actuated Cycle Length： 160
Offset： 13 （8\％），Referenced to phase 2：EBTL and 6：WBTL，Start of Green
Natural Cycle： 100
Control Type：Actuated－Coordinated
Maximum v／c Ratio：0．92
Intersection Signal Delay： $46.6 \quad$ Intersection LOS：D

| Intersection Signal Delay：46．6 | Intersection LOS：D |
| :--- | :--- |
| Intersection Capacity Utilization $97.8 \%$ | ICU Level of Service F |

Utilization $97.8 \%$
CU Level of Service F
Analysis Period（min） 15

5y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Background PM
BA Group

Queues
6：Queen Street South／Queen Street North \＆Britannia Rd West
06／28／2023

|  | $\rangle$ | $\rightarrow$ | $\dagger$ |  |  | $\checkmark$ | $\uparrow$ |  | $\downarrow$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Group Flow（vph） | 145 | 1115 | 140 | 1215 | 125 | 165 | 505 | 280 | 530 | 345 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.75 | 0.75 | 0.65 | 0.81 | 0.18 | 0.86 | 0.60 | 0.72 | 0.92 | 0.59 |
| Control Delay | 50.8 | 42.7 | 37.8 | 42.2 | 6.6 | 73.6 | 53.8 | 41.8 | 75.5 | 26.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 50.8 | 42.7 | 37.8 | 42.2 | 6.6 | 73.6 | 53.8 | 41.8 | 75.5 | 26.9 |
| Queue Length 50th（m） | 25.3 | 170.2 | 15.8 | 196.2 | 5.4 | 33.7 | 73.4 | 61.7 | 168.0 | 48.6 |
| Queue Length 95th（m） | \＃60．2 | 199.6 | 35.0 | 228.2 | 10.7 | \＃77．8 | 94.5 | 85.3 | \＃226．3 | 82.5 |
| Internal Link Dist（m） |  | 110.7 |  | 83.1 |  |  | 135.0 |  | 103.4 |  |
| Turn Bay Length（ m ） | 95.0 |  | 60.0 |  | 45.0 | 40.0 |  | 35.0 |  |  |
| Base Capacity（vph） | 200 | 1496 | 221 | 1504 | 698 | 192 | 864 | 414 | 625 | 616 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.72 | 0.75 | 0.63 | 0.81 | 0.18 | 0.86 | 0.58 | 0.68 | 0.85 | 0.56 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| \＃95th percentile volume exceeds capacity，queue may be longer． |  |  |  |  |  |  |  |  |  |  |

\＃95th percentile volume exceeds capacity，queue may be longer
Queue shown is maximum after two cycles．

HCM Signalized Intersection Capacity Analysis

| 6：Q | th／Q |  |  | rth \＆ | Brita | Rd | West |  |  |  |  | 8／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | $\uparrow$ | \％ |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 个t |  | \％ | 个个 | F | \％ | $\uparrow \uparrow$ |  | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 145 | 950 | 165 | 140 | 1215 | 125 | 165 | 365 | 140 | 280 | 530 | 345 |
| Future Volume（vph） | 145 | 950 | 165 | 140 | 1215 | 125 | 165 | 365 | 140 | 280 | 530 | 345 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Total Lost time（s） | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Lane Util．Factor | 1.00 | 0.95 |  | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.98 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1750 | 3486 |  | 1767 | 3579 | 1530 | 1784 | 3417 |  | 1761 | 1921 | 1538 |
| Flt Permitted | 0.08 | 1.00 |  | 0.12 | 1.00 | 1.00 | 0.12 | 1.00 |  | 0.28 | 1.00 | 1.00 |
| Satd．Flow（perm） | 145 | 3486 |  | 219 | 3579 | 1530 | 218 | 3417 |  | 522 | 1921 | 1538 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 145 | 950 | 165 | 140 | 1215 | 125 | 165 | 365 | 140 | 280 | 530 | 345 |
| RTOR Reduction（vph） | 0 | 9 | 0 | 0 | 0 | 55 | 0 | 25 | 0 | 0 | 0 | 119 |
| Lane Group Flow（vph） | 145 | 1106 | 0 | 140 | 1215 | 70 | 165 | 480 | ， | 280 | 530 | 226 |
| Confl．Peds．（\＃hr） | 12 |  | 9 | 9 |  | 12 | 10 |  | 24 | 24 |  | 10 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 0\％ | 1\％ | 2\％ | 1\％ | 0\％ | 1\％ | 1\％ | 1\％ | 0\％ | 1\％ |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | pm＋pt | NA |  | pm＋pt | NA | Perm |
| Protected Phases | 5 | ， |  | 1 | ， |  | 7 | 4 |  | 3 | ． |  |
| Permitted Phases | 2 |  |  | － |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green，G（s） | 79.9 | 68.2 |  | 77.9 | 67.2 | 67.2 | 49.9 | 38.0 |  | 63.1 | 48.2 | 48.2 |
| Effective Green， g （s） | 79.9 | 68.2 |  | 77.9 | 67.2 | 67.2 | 49.9 | 38.0 |  | 63.1 | 48.2 | 48.2 |
| Actuated g／C Ratio | 0.50 | 0.43 |  | 0.49 | 0.42 | 0.42 | 0.31 | 0.24 |  | 0.39 | 0.30 | 0.30 |
| Clearance Time（s） | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 189 | 1485 |  | 210 | 1503 | 642 | 184 | 811 |  | 377 | 578 | 463 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0．06 | 0.32 |  | 0.04 | c0．34 |  | c0．07 | 0.14 |  | c0．10 | c0． 28 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.33 |  |  | 0.28 |  | 0.05 | 0.21 |  |  | 0.19 |  | 0.15 |
| v／c Ratio | 0.77 | 0.75 |  | 0.67 | 0.81 | 0.11 | 0.90 | 0.59 |  | 0.74 | 0.92 | 0.49 |
| Uniform Delay，d1 | 31.6 | 38.6 |  | 28.7 | 40.7 | 28.2 | 44.9 | 54.1 |  | 36.1 | 54.0 | 45.8 |
| Progression Factor | 1.00 | 1.00 |  | 1.22 | 0.90 | 0.66 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 16.9 | 3.4 |  | 6.8 | 4.2 | 0.3 | 38.4 | 1.2 |  | 7.7 | 19.4 | 0.8 |
| Delay（s） | 48.4 | 42.0 |  | 41.9 | 41.0 | 18.9 | 83.2 | 55.3 |  | 43.8 | 73.3 | 46.6 |
| Level of Service | D | D |  | D | D | B | F | E |  | D | E | D |
| Approach Delay（s） |  | 42.8 |  |  | 39.2 |  |  | 62.2 |  |  | 58.2 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 48.4 |  | HCM 2000 | Level of S | Service |  | D |  |  |  |
| HCM 2000 Volume to Capacity | ratio |  | 0.85 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | time（s） |  |  | 21.0 |  |  |  |
| Intersection Capacity Utilizatio |  |  | 97．8\％ |  | CU Level | f Service |  |  | F |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


| 5y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Background PM |  |
| :--- | ---: |
| BA Group | Synchro 11 Report |
| Page 8 |  |

HCM Unsignalized Intersection Capacity Analysis
7：Arch Rd \＆Britannia Rd West


[^8]HCM Unsignalized Intersection Capacity Analysis

| 8: Earl St \& Britannia Rd West |  |  |  |  |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ | $\geqslant$ | 7 | $\leftarrow$ | 4 | \% |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个t |  | \% | 个4 | M |  |  |  |
| Traffic Volume (veh/h) | 1365 | 5 | 5 | 1485 | 0 | 20 |  |  |
| Future Volume (Veh/h) | 1365 | 5 | 5 | 1485 | 0 | 20 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate (vph) | 1365 | 5 | 5 | 1485 | 0 | 20 |  |  |
| Pedestrians |  |  |  |  | 5 |  |  |  |
| Lane Width (m) |  |  |  |  | 3.5 |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  | 1.2 |  |  |  |
| Percent Blockage |  |  |  |  | 0 |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type T | TWLTL |  |  | TWLTL |  |  |  |  |
| Median storage veh) | 2 |  |  | 2 |  |  |  |  |
| Upstream signal ( m ) | 219 |  |  | 71 |  |  |  |  |
| pX, platoon unblocked |  |  | 0.74 |  | 0.81 | 0.74 |  |  |
| vC , conficting volume |  |  | 1375 |  | 2125 | 690 |  |  |
| $\mathrm{vC1}$, stage 1 conf vol |  |  |  |  | 1372 |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  | 752 |  |  |  |
| vCu , unblocked vol |  |  | 817 |  | 1189 | 0 |  |  |
| tC , single (s) |  |  | 4.1 |  | 6.8 | 6.9 |  |  |
| tC, 2 stage (s) |  |  |  |  | 5.8 |  |  |  |
| tF (s) |  |  | 2.2 |  | 3.5 | 3.3 |  |  |
| p0 queue free \% |  |  | 99 |  | 100 | 98 |  |  |
| cM capacity (veh/h) |  |  | 608 |  | 277 | 809 |  |  |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | WB 3 | NB 1 |  |  |
| Volume Total | 910 | 460 | 5 | 742 | 742 | 20 |  |  |
| Volume Left | 0 | 0 | 5 | 0 | 0 | 0 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 20 |  |  |
| cSH | 1700 | 1700 | 608 | 1700 | 1700 | 809 |  |  |
| Volume to Capacity | 0.54 | 0.27 | 0.01 | 0.44 | 0.44 | 0.02 |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.6 |  |  |
| Control Delay (s) | 0.0 | 0.0 | 11.0 | 0.0 | 0.0 | 9.6 |  |  |
| Lane LOS |  |  | B |  |  | A |  |  |
| Approach Delay (s) | 0.0 |  | 0.0 |  |  | 9.6 |  |  |
| Approach LOS |  |  |  |  |  | A |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 51.0\% | ICU Level of Service |  |  | A |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

Analysis Period (min)

| 5y Future Background PM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Background PM |  |
| :--- | ---: |
| BA Group | Synchro 11 Report |
| Page 10 |  |

Timings
9: Britannia Rd West \& Ellesboro Dr 06/28/2023


## Intersection Summar

Cycle Length: 160
Actuated Cycle Length: 160
Offset: 0 ( $0 \%$ ), Referenced to phase 2:EBTL and 6:WBT, Start of Green
Natural Cycle. 80
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.58

| Intersection Signal Delay: 7.3 | Intersection LOS: A |
| :--- | :--- |
| Intersection Capacity Utilization 65.7\% | ICU Level of Service C |
| Analysis Period (min) 15 |  |

Splits and Phases: 9: Britannia Rd West \& Ellesboro Dr


[^9]9: Britannia Rd West \& Ellesboro Dr
06/28/2023

| Lane Group | EBL | EBT | WBT | SBL | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 15 | 1370 | 1530 | 100 | 35 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.07 | 0.46 | 0.51 | 0.58 | 0.20 |
| Control Delay | 3.2 | 3.8 | 5.0 | 82.8 | 26.6 |
| Queue Delay | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 |
| Total Delay | 3.2 | 3.9 | 5.0 | 82.8 | 26.6 |
| Queue Length 50th (m) | 0.6 | 42.4 | 63.4 | 32.9 | 1.6 |
| Queue Length 95th (m) | m1.1 | 55.0 | 92.3 | 52.4 | 13.2 |
| Internal Link Dist ( m ) |  | 46.6 | 115.6 | 80.1 |  |
| Turn Bay Length ( $m$ ) | 45.0 |  |  |  | 15.0 |
| Base Capacity (vph) | 230 | 2994 | 2971 | 435 | 393 |
| Starvation Cap Reductn | 0 | 448 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.54 | 0.51 | 0.23 | 0.09 |
| Intersection Summary |  |  |  |  |  |

m Volume for 95 th percentile queue is metered by upstream signal.

HCM Signalized Intersection Capacity Analysis
9: Britannia Rd West \& Ele


[^10]| HCM Unsignalized Intersection Capacity Analysis 1：Queen Street North \＆Matlock Ave |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  | $\dagger$ | 7 |  | $\dagger$ |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | Y |  | 个t |  | \％ | 个 $\uparrow$ |  |  |
| Traffic Volume（veh／h） | 30 | 20 | 1000 | 40 | 15 | 580 |  |  |
| Future Volume（Veh／h） | 30 | 20 | 1000 | 40 | 15 | 580 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |  |
| Grade | 0\％ |  | 0\％ |  |  | 0\％ |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Hourly flow rate（vph） | 33 | 22 | 1087 | 43 | 16 | 630 |  |  |
| Pedestrians | 1 |  |  |  |  |  |  |  |
| Lane Width（m） | 3.5 |  |  |  |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  | TWLTL |  |  | None |  |  |
| Median storage veh） |  |  | 2 |  |  |  |  |  |
| Upstream signal（ m ） |  |  | 313 |  |  |  |  |  |
| pX，platoon unblocked | 0.89 | 0.89 |  |  | 0.89 |  |  |  |
| vC ，conficting volume | 1456 | 566 |  |  | 1131 |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1110 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 347 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1267 | 268 |  |  | 902 |  |  |  |
| tC，single（s） | 7.3 | 7.4 |  |  | 4.9 |  |  |  |
| tC， 2 stage（s） | 6.3 |  |  |  |  |  |  |  |
| tF（s） | 3.7 | 3.5 |  |  | 2.6 |  |  |  |
| p0 queue free \％ | 88 | 96 |  |  | 97 |  |  |  |
| cM capacity（veh／h） | 264 | 592 |  |  | 488 |  |  |  |
| Direction，Lane \＃ | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | SB 3 |  |  |
| Volume Total | 55 | 725 | 405 | 16 | 315 | 315 |  |  |
| Volume Left | 33 | 0 | 0 | 16 | 0 | 0 |  |  |
| Volume Right | 22 | 0 | 43 | 0 | 0 | 0 |  |  |
| cSH | 340 | 1700 | 1700 | 488 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.16 | 0.43 | 0.24 | 0.03 | 0.19 | 0.19 |  |  |
| Queue Length 95th（m） | 4.6 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 17.6 | 0.0 | 0.0 | 12.6 | 0.0 | 0.0 |  |  |
| Lane LOS | C |  |  | B |  |  |  |  |
| Approach Delay（s） | 17.6 | 0.0 |  | 0.3 |  |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.6 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 38．9\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis

| 2：Queen Street North \＆ 40 Queen St N Driveway／53 Queen St Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | $\geqslant$ | 7 | － | 4 | 4 | $\uparrow$ |  | － | $\dagger$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | ${ }^{7}$ | 性 |  | \％ | 个家 |  |
| Traffic Volume（veh／h） | 0 | 0 | 0 | 0 | － | 0 | 0 | 1040 | 0 | 0 | 610 |  |
| Future Volume（Veh／h） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1040 | 0 | 0 | 610 |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1182 | 0 | 0 | 693 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（m／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | TWLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.86 | 0.86 |  | 0.86 | 0.86 | 0.86 |  |  |  | 0.86 |  |  |
| vC, conficting volume | 1284 | 1875 | 346 | 1528 | 1875 | 591 | 693 |  |  | 1182 |  |  |
| vC1，stage 1 conf vol | 693 | 693 |  | 1182 | 1182 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 591 | 1182 |  | 346 | 693 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1011 | 1696 | 346 | 1294 | 1696 | 207 | 693 |  |  | 892 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity（veh／h） | 365 | 261 | 655 | 249 | 261 | 694 | 912 |  |  | 663 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 0 | 0 | 788 | 394 | 0 | 462 | 231 |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| CSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.00 | 0.46 | 0.23 | 0.00 | 0.27 | 0.14 |  |  |  |  |
| Queue Length 95th（ $m$ ） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 32．1\％ |  | CU Level | f Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^11]| HCM Unsignalized In 3：Queen Street North |  | ction ) Qué | $\begin{aligned} & \text { Japac } \\ & \text { n } 5 \text { an } \end{aligned}$ |  | sis way／P | oposed |  |  |  |  |  | 2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 1 |  |  | 4 | $\dagger$ | \％ |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | \％ | 个个 |  | ＊ | 个家 |  |
| Traffic Volume（veh／h） | 0 | 0 | 0 | 60 | 0 | 30 | 0 | 1010 | 30 | 15 | 595 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 60 | 0 | 30 | 0 | 1010 | 30 | 15 | 595 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 69 | 0 | 34 | 0 | 1161 | 34 | 17 | 684 | 0 |
| Pedestrians |  | 3 |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  | 3.7 |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  | 1.2 |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  | 0 |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 186 |  |  |  |  |
| pX，platoon unblocked | 0.85 | 0.85 |  | 0.85 | 0.85 | 0.85 |  |  |  | 0.85 |  |  |
| VC, conflicting volume | 1336 | 1916 | 345 | 1554 | 1899 | 598 | 687 |  |  | 1195 |  |  |
| vC1，stage 1 conf vol | 721 | 721 |  | 1178 | 1178 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 614 | 1195 |  | 376 | 721 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1049 | 1729 | 345 | 1305 | 1709 | 184 | 687 |  |  | 884 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 100 | 73 | 100 | 95 | 100 |  |  | 97 |  |  |
| cM capacity（veh／h） | 338 | 246 | 655 | 253 | 258 | 711 | 914 |  |  | 660 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 103 | 0 | 774 | 421 | 17 | 456 | 228 |  |  |  |  |
| Volume Left | 0 | 69 | 0 | － | 0 | 17 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 34 | 0 | 0 | 34 | 0 | 0 | 0 |  |  |  |  |
| cSH | 1700 | 321 | 1700 | 1700 | 1700 | 660 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.32 | 0.00 | 0.46 | 0.25 | 0.03 | 0.27 | 0.13 |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 10.8 | 0.0 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 21.4 | 0.0 | 0.0 | 0.0 | 10.6 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | C |  |  |  | B |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 21.4 | 0.0 |  |  | 0.3 |  |  |  |  |  |  |
| Approach LOS | A | c |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.2 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 40．7\％ |  | CU Level | f Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

5y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total AM Peak Hour

BA Group | Synchro 11 Report |
| ---: |
| Page 3 |

HCM Unsignalized Intersection Capacity Analysis
4：Queen Street North \＆Petro Canada N Driveway


[^12]Synchro 11 Report

| HCM Unsignalized Intersection Capacity Analysis 5：Queen Street North \＆Petro Canada S Driveway |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 |  | 4 | $\uparrow$ |  | $\stackrel{ }{ }$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | M |  | \％ | 个 $\uparrow$ | 个t |  |  |  |
| Traffic Volume（veh／h） | 0 | 5 | 0 | 1045 | 635 | 10 |  |  |
| Future Volume（Veh／h） | 0 | 5 | 0 | 1045 | 635 | 10 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |  |  |
| Hourly flow rate（vph） | 0 | 6 | 0 | 1188 | 722 | 11 |  |  |
| Pedestrians | 3 |  |  | 2 |  |  |  |  |
| Lane Width（m） | 3.5 |  |  | 3.6 |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | WLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ $m$ ） |  |  |  | 127 |  |  |  |  |
| pX，platoon unblocked | 0.84 |  |  |  |  |  |  |  |
| VC ，conflicting volume | 1324 | 372 | 736 |  |  |  |  |  |
| vC1，stage 1 conf vol | 730 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 594 |  |  |  |  |  |  |  |
| vCu，unblocked vol | 1016 | 372 | 736 |  |  |  |  |  |
| tC ，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| $\mathrm{tF}^{\text {（ }}$ ） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 100 | 99 | 100 |  |  |  |  |  |
| cM capacity（veh／h） | 402 | 629 | 877 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 6 | 0 | 594 | 594 | 481 | 252 |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 6 | 0 | 0 | 0 | 0 | 11 |  |  |
| cSH | 629 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.01 | 0.00 | 0.35 | 0.35 | 0.28 | 0.15 |  |  |
| Queue Length 95th（m） | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 10.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | B |  |  |  |  |  |  |  |
| Approach Delay（s） | 10.8 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39．5\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

Timings
6：Queen Street South／Queen Street North \＆Britannia Rd West 06／28／2023

|  | $\rangle$ | $\rightarrow$ | 7 |  |  | 4 | $\uparrow$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations | ${ }^{4}$ | 个t | \％ | ¢个 | $\overline{7}$ | \％ | 中 ${ }^{\text {a }}$ | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 225 | 1575 | 80 | 625 | 330 | 95 | 490 | 155 | 330 | 155 |
| Future Volume（vph） | 225 | 1575 | 80 | 625 | 330 | 95 | 490 | 155 | 330 | 155 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | Perm | NA | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 | 1 | 6 |  |  | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 12.0 | 12.0 | 8.0 | 12.0 | 12.0 |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 38.9 | 38.9 | 11.0 | 38.9 | 38.9 |
| Total Split（s） | 19.0 | 92.0 | 11.0 | 84.0 | 84.0 | 41.0 | 41.0 | 16.0 | 57.0 | 57.0 |
| Total Split（\％） | 11．9\％ | 57．5\％ | 6．9\％ | 52．5\％ | 52．5\％ | 25．6\％ | 25．6\％ | 10．0\％ | 35．6\％ | 35．6\％ |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 3.9 | 3.9 | 0.0 | 3.9 | 3.9 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 7.9 | 7.9 | 3.0 | 7.9 | 7.9 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |
| Act Efft Green（s） | 101.8 | 86.9 | 93.3 | 81.2 | 81.2 | 31.3 | 31.3 | 52.0 | 47.1 | 47.1 |
| Actuated g／C Ratio | 0.64 | 0.54 | 0.58 | 0.51 | 0.51 | 0.20 | 0.20 | 0.32 | 0.29 | 0.29 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.45 | 0.87 | 0.61 | 0.36 | 0.37 | 0.53 | 0.90 | 0.81 | 0.61 | 0.30 |
| Control Delay | 15.5 | 38.3 | 56.8 | 22.7 | 3.5 | 69.2 | 77.3 | 70.3 | 53.6 | 7.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 15.5 | 38.3 | 56.8 | 22.7 | 3.5 | 69.2 | 77.3 | 70.3 | 53.6 | 7.0 |
| LOS | B | D | E | C | A | E | E | E | D | A |
| Approach Delay |  | 35.6 |  | 19.2 |  |  | 76.2 |  | 46.4 |  |
| Approach LOS |  | D |  | B |  |  | E |  | D |  |

## Intersection Summar

Cycle Length： 160
Actuated Cycle Length： 160
Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6：WBTL，Start of Green
tural Cycle： 130
Contro Type：Actuated－Coordinated

| Maximum vic Ratio： 0.90 | Intersection LOS：D |
| :--- | :--- |
| Intersection Signal Delay： 40.0 | ICU Level of Service G |
| Intersection Capacity Utilization 106．5\％ |  |

Intersection Capacity Utilization 106．5\％
ICU Level of Service G
Analysis Period（min） 15


[^13]Queues

| 6: Queen Stree |  | en St | eet N | rth \& | Britan | R | West |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ | 1 | 4 | 4 | 4 | 4 | ( | $\dagger$ | $\downarrow$ |  |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |  |
| Lane Group Flow (vph) | 225 | 1675 | 80 | 625 | 330 | 95 | 615 | 155 | 330 | 155 |  |
| v/c Ratio | 0.45 | 0.87 | 0.61 | 0.36 | 0.37 | 0.53 | 0.90 | 0.81 | 0.61 | 0.30 |  |
| Control Delay | 15.5 | 38.3 | 56.8 | 22.7 | 3.5 | 69.2 | 77.3 | 70.3 | 53.6 | 7.0 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 15.5 | 38.3 | 56.8 | 22.7 | 3.5 | 69.2 | 77.3 | 70.3 | 53.6 | 7.0 |  |
| Queue Length 50th (m) | 31.0 | 256.7 | 12.2 | 67.5 | 4.5 | 28.5 | 102.6 | 38.0 | 93.7 | 0.0 |  |
| Queue Length 95th (m) | 44.9 | 294.3 | \#34.0 | 85.9 | 14.9 | 49.8 | \#127.8 | \#67.5 | 128.7 | 17.7 |  |
| Internal Link Dist ( $m$ ) |  | 110.7 |  | 83.1 |  |  | 135.0 |  | 103.4 |  |  |
| Turn Bay Length ( m ) | 95.0 |  | 60.0 |  | 45.0 | 40.0 |  | 35.0 |  |  |  |
| Base Capacity (vph) | 516 | 1919 | 131 | 1731 | 893 | 188 | 725 | 194 | 566 | 541 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.44 | 0.87 | 0.61 | 0.36 | 0.37 | 0.51 | 0.85 | 0.80 | 0.58 | 0.29 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |

[^14]HCM Signalized Intersection Capacity Analysis


5y Future Total AM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Total AM Peak Hour BA Group

## HCM Unsignalized Intersection Capacity Analysis

| 7：Arch Rd \＆Britannia Rd West |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ | $\geqslant$ | 1 | $\Perp$ | 4 | ／ |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个施 |  | \％ | 个个 | M |  |  |  |
| Traffic Volume（veh／h） | 1850 | 5 | 10 | 1030 | 5 | 10 |  |  |
| Future Volume（Veh／h） | 1850 | 5 | 10 | 1030 | 5 | 10 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate（vph） | 1850 | 5 | 10 | 1030 | 5 | 10 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type | None |  |  | TWLTL |  |  |  |  |
| Median storage veh） |  |  |  | 2 |  |  |  |  |
| Upstream signal（ m ） | 107 |  |  | 182 |  |  |  |  |
| pX，platoon unblocked |  |  | 0.58 |  | 0.61 | 0.58 |  |  |
| vC, conficting volume |  |  | 1855 |  | 2388 | 928 |  |  |
| VC1，stage 1 conf vol |  |  |  |  | 1852 |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol |  |  |  |  | 535 |  |  |  |
| vCu ，unblocked vol |  |  | 1024 |  | 1565 | 0 |  |  |
| tC，single（s） |  |  | 4.1 |  | 6.8 | 7.1 |  |  |
| tC， 2 stage（s） |  |  |  |  | 5.8 |  |  |  |
| tF（s） |  |  | 2.2 |  | 3.5 | 3.4 |  |  |
| po queue free \％ |  |  | 97 |  | 97 | 98 |  |  |
| cM capacity（veh／h） |  |  | 397 |  | 173 | 617 |  |  |
| Direction，Lane \＃ | EB 1 | EB 2 | WB 1 | WB 2 | WB 3 | NB 1 |  |  |
| Volume Total | 1233 | 622 | 10 | 515 | 515 | 15 |  |  |
| Volume Left | 0 | 0 | 10 | 0 | 0 | 5 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 10 |  |  |
| cSH | 1700 | 1700 | 397 | 1700 | 1700 | 333 |  |  |
| Volume to Capacity | 0.73 | 0.37 | 0.03 | 0.30 | 0.30 | 0.05 |  |  |
| Queue Length 95th（m） | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.1 |  |  |
| Control Delay（s） | 0.0 | 0.0 | 14.3 | 0.0 | 0.0 | 16.3 |  |  |
| Lane LOS |  |  | B |  |  | C |  |  |
| Approach Delay（s） | 0.0 |  | 0.1 |  |  | 16.3 |  |  |
| Approach LOS |  |  |  |  |  | C |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 61．3\％ |  | CU Level | Service | B |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
8：Earl St \＆Britannia Rd West


[^15]Timings
9: Britannia Rd West \& Ellesboro Dr 06/28/2023

Intersection Summany
Cycle Length: 160
Actuated Cycle Length: 160
Offiset: 0 (0\%), Referenced to phase 2:EBTL and 6 :WBT, Start of Green
Natural Cycle: 90 Actuated-Coordinated
Control Type: Al
Control Type: Actuated-Cooranated
Maximum v/c Ratio: 0.59
Intersection Signal Delay: 3.9 Intersection LOS: A
Intersection Capacity Utilization $76.7 \%$
CU Level of Service D
Analysis Period (min) 15


Queues
9: Britannia Rd West \& Ellesboro Dr

| Lane Group | EBL | EBT | WBT | SBL | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Lane Group Flow (vph) | 30 | 1850 | 1080 | 60 | 30 |
| V/c Ratio | 0.07 | 0.59 | 0.36 | 0.40 | 0.20 |
| Control Delay | 1.4 | 1.7 | 2.9 | 77.8 | 23.8 |
| Queue Delay | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 |
| Total Delay | 1.4 | 1.8 | 2.9 | 77.8 | 23.8 |
| Queue Length 50 th $(\mathrm{m})$ | 0.7 | 28.8 | 34.8 | 19.5 | 0.0 |
| Queue Length 95th $(\mathrm{m})$ | m 0.9 | 32.6 | 45.4 | 35.5 | 11.4 |
| Internal Link Dist ( m ) |  | 46.6 | 115.6 | 80.1 |  |
| Turn Bay Length $(\mathrm{m})$ | 45.0 |  |  |  | 15.0 |
| Base Capacity (vph) | 406 | 3120 | 2967 | 434 | 375 |
| Starvation Cap Reductn | 0 | 313 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.66 | 0.36 | 0.14 | 0.08 |
| Intersection Summary |  |  |  |  |  |

m Volume for 95 th percentile queue is metered by upstream signal.

5y Future Total AM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Total AM Peak Hour
BA Group
Synchro 11 Report
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| HCM Signalized Intersection Capacity Analysis 9：Britannia Rd West \＆Ellesboro Dr |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | ఒ | 4 | ＊ | 4 |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |  |
| Lane Configurations | \％ | 个 $\uparrow$ | 个t |  | \％ | 「 |  |  |
| Traffic Volume（vph） | 30 | 1850 | 1010 | 70 | 60 | 30 |  |  |
| Future Volume（vph） | 30 | 1850 | 1010 | 70 | 60 | 30 |  |  |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Lane Width | 3.5 | 3.7 | 3.7 | 3.5 | 3.5 | 3.5 |  |  |
| Total Lost time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 0.95 |  | 1.00 | 1.00 |  |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 0.97 |  |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Frt | 1.00 | 1.00 | 0.99 |  | 1.00 | 0.85 |  |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Flow（prot） | 1729 | 3579 | 3403 |  | 1782 | 1447 |  |  |
| Fit Permitted | 0.26 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Fow（perm） | 466 | 3579 | 3403 |  | 1782 | 1447 |  |  |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj．Flow（vph） | 30 | 1850 | 1010 | 70 | 60 | 30 |  |  |
| RTOR Reduction（vph） | 0 | 0 | 1 | 0 | 0 | 28 |  |  |
| Lane Group Flow（vph） | 30 | 1850 | 1079 | 0 | 60 | 2 |  |  |
| Confl．Peds．（\＃／hr） | 4 |  |  | 4 | ， | 12 |  |  |
| Heavy Vehicles（\％） | 3\％ | 2\％ | 6\％ | 6\％ | 0\％ | 7\％ |  |  |
| Turn Type | Perm | NA | NA |  | Perm | Perm |  |  |
| Protected Phases |  | 2 | 6 |  |  |  |  |  |
| Permitted Phases | 2 |  |  |  | 8 | 8 |  |  |
| Actuated Green，G（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Effective Green，g（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Actuated g／C Ratio | 0.86 | 0.86 | 0.86 |  | 0.07 | 0.07 |  |  |
| Clearance Time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |
| Lane Grp Cap（vph） | 399 | 3066 | 2915 |  | 120 | 97 |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | c0．52 | 0.32 |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.06 |  |  |  | c0．03 | 0.00 |  |  |
| v／c Ratio | 0.08 | 0.60 | 0.37 |  | 0.50 | 0.02 |  |  |
| Uniform Delay，d1 | 1.8 | 3.4 | 2.4 |  | 72.0 | 69.7 |  |  |
| Progression Factor | 0.53 | 0.34 | 1.00 |  | 1.00 | 1.00 |  |  |
| Incremental Delay，d2 | 0.2 | 0.4 | 0.4 |  | 3.3 | 0.1 |  |  |
| Delay（s） | 1.1 | 1.6 | 2.8 |  | 75.2 | 69.7 |  |  |
| Level of Service | A | A | A |  | E | E |  |  |
| Approach Delay（s） |  | 1.6 | 2.8 |  | 73.4 |  |  |  |
| Approach LOS |  | A | A |  | E |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 4.1 |  | HCM 2000 | evel of Service | A |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.60 |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | ime（s） | 12.1 |  |
| Intersection Capacity Utilization |  |  | 76．7\％ |  | CU Level | Service | D |  |
|  |  |  | 15 |  |  |  |  |  |
| Analysis Period（min） |  |  |  |  |  |  |  |  |

5y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total AM Peak Hour

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HCM Unsignalized Intersection Capacity Analysis
1：Queen Street North \＆Matlock Ave
06／28／2023

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | Y |  |  |  | ＊ | 个4 |
| Traffic Volume（veh／h） | 55 | 15 | 575 | 60 | 15 | 1095 |
| Future Volume（Veh／h） | 55 | 15 | 575 | 60 | 15 | 1095 |
| Sign Control | Stop |  | Free |  |  | Free |
| Grade | 0\％ |  | 0\％ |  |  | 0\％ |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate（vph） | 60 | 16 | 625 | 65 | 16 | 1190 |
| Pedestrians | 6 |  |  |  |  | 1 |
| Lane Width（m） | 3.5 |  |  |  |  | 3.6 |
| Walking Speed（m／s） | 1.2 |  |  |  |  | 1.2 |
| Percent Blockage | 0 |  |  |  |  | 0 |
| Right turn flare（veh） |  |  |  |  |  |  |
| Median type |  |  | TWLTL |  |  | None |

TWLL
None
Median storage veh）

Upstream signal（ m ）

| Upstream signal（ $m$ ） | 313 |  |  |
| :---: | :---: | :---: | :---: |
| pX ，platoon unblocked | 1.00 | 1.00 | 1.00 |
| vC, conficting volume | 1290 | 352 | 696 |
| $\mathrm{vC1}$ ，stage 1 conf vol | 664 |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 627 |  |  |
| vCu ，unblocked vol | 1283 | 340 | 685 |

vC2，stage 2 conf vol
tC，single（s）
Co，single（s）
tF （s）
po queue free \％
cM capacity（veh／h）

| Direction，Lane \＃ | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | SB 3 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume Total | 76 | 417 | 273 | 16 | 595 | 595 |  |
| Volume Left | 60 | 0 | 0 | 16 | 0 | 0 |  |
| Volume Right | 16 | 0 | 65 | 0 | 0 | 0 |  |
| cSH | 387 | 1700 | 1700 | 814 | 1700 | 1700 |  |
| Volume to Capacity | 0.20 | 0.25 | 0.16 | 0.02 | 0.35 | 0.35 |  |
| Queue Length 95th（ m ） | 5.8 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |  |
| Control Delay（s） | 16.5 | 0.0 | 0.0 | 9.5 | 0.0 | 0.0 |  |
| Lane LOS | C |  |  | A |  |  |  |
| Approach Delay（s） | 16.5 | 0.0 |  | 0.1 |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.7 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 41．2\％ | ICU Level of Service |  |  | A |
| Analysis Period（min） |  |  | 15 |  |  |  |  |

5y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total PM Peak Hour
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| HCM Unsignalized In 2：Queen Street North |  | Que | apac |  | sis <br> vay／5 | Quee |  |  |  |  |  | ／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | $\geqslant$ | 1 |  |  | 4 | $\uparrow$ | \％ |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \＄ |  |  | ¢ |  | \％ | 个 ${ }^{\text {a }}$ |  | \％ | 个t |  |
| Traffic Volume（veh／h） | 0 | 0 | 5 | 5 | ， | 0 | 5 | 635 | 0 | 5 | 1145 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 635 | 0 | 5 | 1145 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate（vph） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 698 | 0 | 5 | 1258 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（m／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | ， |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 |  |  |  | 0.95 |  |  |
| VC, conflicting volume | 1627 | 1976 | 629 | 1352 | 1976 | 349 | 1258 |  |  | 698 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1268 | 1268 |  | 708 | 708 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 359 | 708 |  | 644 | 1268 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1551 | 1920 | 629 | 1261 | 1920 | 203 | 1258 |  |  | 571 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 99 | 98 | 100 | 100 | 99 |  |  | 99 |  |  |
| cM capacity（veh／h） | 174 | 214 | 430 | 319 | 211 | 768 | 560 |  |  | 959 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 5 | 5 | 5 | 465 | 233 | 5 | 839 | 419 |  |  |  |  |
| Volume Left | 0 | 5 | 5 | 0 | 0 | 5 | 0 | 0 |  |  |  |  |
| Volume Right | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| cSH | 430 | 319 | 560 | 1700 | 1700 | 959 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.01 | 0.02 | 0.01 | 0.27 | 0.14 | 0.01 | 0.49 | 0.25 |  |  |  |  |
| Queue Length 95th（m） | 0.3 | 0.4 | 0.2 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 13.5 | 16.5 | 11.5 | 0.0 | 0.0 | 8.8 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | B | C | B |  |  | A |  |  |  |  |  |  |
| Approach Delay（s） | 13.5 | 16.5 | 0.1 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | B | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 42．5\％ |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^16]| HCM Unsignalized In 3：Queen Street North |  | Que | $\begin{aligned} & \text { Japac } \\ & \text { n St } \end{aligned}$ |  | sis way／P | opose |  |  |  |  |  | 2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 |  | \％ | 1 |  |  | 4 | $\uparrow$ | 7 |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | \＄ |  | \％ | 个4 |  | ${ }^{*}$ | 个守 |  |
| Traffic Volume（veh／h） | 5 | 0 | 5 | 60 | 0 | 35 | 0 | 600 | 80 | 40 | 1115 | 0 |
| Future Volume（Veh／h） | 5 | 0 | 5 | 60 | 0 | 35 | 0 | 600 | 80 | 40 | 1115 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate（vph） | 5 | 0 | 5 | 66 | 0 | 38 | 0 | 659 | 88 | 44 | 1225 | 0 |
| Pedestrians |  | 2 |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  | 3.7 |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  | 1.2 |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  | 0 |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 186 |  |  |  |  |
| pX，platoon unblocked | 0.90 | 0.90 |  | 0.90 | 0.90 | 0.90 |  |  |  | 0.90 |  |  |
| vC, conflicting volume | 1682 | 2062 | 614 | 1408 | 2018 | 374 | 1227 |  |  | 747 |  |  |
| vC1，stage 1 conf vol | 1315 | 1315 |  | 703 | 703 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 368 | 747 |  | 706 | 1315 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1544 | 1963 | 614 | 1241 | 1914 | 96 | 1227 |  |  | 509 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 97 | 100 | 99 | 79 | 100 | 96 | 100 |  |  | 95 |  |  |
| cM capacity（veh／h） | 156 | 196 | 439 | 312 | 201 | 857 | 574 |  |  | 964 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 10 | 104 | 0 | 439 | 308 | 44 | 817 | 408 |  |  |  |  |
| Volume Left | 5 | 66 | 0 | － | 0 | 44 | 0 | 0 |  |  |  |  |
| Volume Right | 5 | 38 | 0 | 0 | 88 | 0 | 0 | 0 |  |  |  |  |
| cSH | 230 | 407 | 1700 | 1700 | 1700 | 964 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.04 | 0.26 | 0.00 | 0.26 | 0.18 | 0.05 | 0.48 | 0.24 |  |  |  |  |
| Queue Length 95th（m） | 1.1 | 8.0 | 0.0 | 0.0 | 0.0 | 1.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 21.3 | 16.9 | 0.0 | 0.0 | 0.0 | 8.9 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | C | C |  |  |  | A |  |  |  |  |  |  |
| Approach Delay（s） | 21.3 | 16.9 | 0.0 |  |  | 0.3 |  |  |  |  |  |  |
| Approach LOS | C | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 47．4\％ |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^17]

Analysis Period (min)

HCM Unsignalized Intersection Capacity Analysis
5: Queen Street North \& Petro Canada S Driveway


[^18]Timings
6：Queen Street South／Queen Street North \＆Britannia Rd West 06／28／2023

|  | 4 |  | 7 |  |  | 4 | 4 |  |  | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations | \％ | 个 ${ }^{2}$ | ${ }^{7}$ | 个¢ | 「 | ＊ | 性 | \％ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 155 | 950 | 140 | 1215 | 145 | 165 | 390 | 285 | 545 | 355 |
| Future Volume（vph） | 155 | 950 | 140 | 1215 | 145 | 165 | 390 | 285 | 545 | 355 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | $\mathrm{pm}+\mathrm{pt}$ | NA | $\mathrm{pm}+\mathrm{pt}$ | NA | Perm |
| Protected Phases | 5 | 2 | 1 | 6 |  | 7 | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 7 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 5.0 | 12.0 | 8.0 | 12.0 | 12.0 |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 9.5 | 38.9 | 11.0 | 38.9 | 38.9 |
| Total Split（s） | 15.0 | 71.0 | 14.0 | 70.0 | 70.0 | 15.0 | 47.0 | 28.0 | 60.0 | 60.0 |
| Total Split（\％） | 9．4\％ | 44．4\％ | 8．8\％ | 43．8\％ | 43．8\％ | 9．4\％ | 29．4\％ | 17．5\％ | 37．5\％ | 37．5\％ |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 0.0 | 3.9 | 0.0 | 3.9 | 3.9 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 | 3.0 | 7.9 | 7.9 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |
| Act Efft Green（s） | 83.6 | 67.5 | 80.5 | 65.9 | 65.9 | 55.9 | 39.0 | 69.0 | 49.1 | 49.1 |
| Actuated g／C Ratio | 0.52 | 0.42 | 0.50 | 0.41 | 0.41 | 0.35 | 0.24 | 0.43 | 0.31 | 0.31 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.82 | 0.75 | 0.67 | 0.82 | 0.21 | 0.88 | 0.62 | 0.74 | 0.93 | 0.60 |
| Control Delay | 62.9 | 43.4 | 39.6 | 43.5 | 8.7 | 79.1 | 54.1 | 42.4 | 76.0 | 27.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 62.9 | 43.4 | 39.6 | 43.5 | 8.7 | 79.1 | 54.1 | 42.4 | 76.0 | 27.9 |
| LOS | E | D | D | D | A | E | D | D | E | c |
| Approach Delay |  | 45.8 |  | 39.8 |  |  | 60.1 |  | 53.5 |  |
| Approach LOS |  | D |  | D |  |  | E |  | D |  |

$\frac{\text { Intersection Summary }}{\text { Cycle Length：} 160}$
Cycle Length： 160
Actuated Cycle Len
Actuated Cycle Length： 160
Offset： 13 （8\％）Ret
Offset： 13 （8\％），Referenced to phase 2：EBTL and 6：WBTL，Start of Green
Natural Cycle： 100
Control Type：Actuated－Coordinated
$\begin{array}{ll}\text { Control Type：Actuated－Coordinated } & \\ \text { Maximum v／c Ratio：0．93 } & \\ \begin{array}{ll}\text { Intersection Signal Delay：} 48.0 & \text { Intersection LOS：D } \\ \text { Intersection Capacity Utiization 99．2\％} & \text { ICU Level of Service F }\end{array}\end{array}$
ICU Level of Service F
Analysis Period（min） 15


[^19]Queues
6：Queen Street South／Queen Street North \＆Britannia Rd West
06／28／2023

|  | $\rangle$ | $\rightarrow$ | $\dagger$ | 4 | 4 | ＊ | $\dagger$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Group Flow（vph） | 155 | 1115 | 140 | 1215 | 145 | 165 | 530 | 285 | 545 | 355 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.82 | 0.75 | 0.67 | 0.82 | 0.21 | 0.88 | 0.62 | 0.74 | 0.93 | 0.60 |
| Control Delay | 62.9 | 43.4 | 39.6 | 43.5 | 8.7 | 79.1 | 54.1 | 42.4 | 76.0 | 27.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 62.9 | 43.4 | 39.6 | 43.5 | 8.7 | 79.1 | 54.1 | 42.4 | 76.0 | 27.9 |
| Queue Length 50th（m） | 31.6 | 170.2 | 15.8 | 196.4 | 7.5 | 35.0 | 77.4 | 62.0 | 172.4 | 51.8 |
| Queue Length 95th（m） | \＃72．6 | 199.6 | 35.3 | 228.2 | 14.2 | \＃82．1 | 100.3 | 86.8 | \＃236．7 | 87.6 |
| Internal Link Dist（ $m$ ） |  | 110.7 |  | 83.1 |  |  | 135.0 |  | 103.4 |  |
| Turn Bay Length（ m ） | 95.0 |  | 60.0 |  | 45.0 | 40.0 |  | 35.0 |  |  |
| Base Capacity（vph） | 193 | 1479 | 215 | 1474 | 686 | 187 | 871 | 411 | 625 | 614 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v／c Ratio | 0.80 | 0.75 | 0.65 | 0.82 | 0.21 | 0.88 | 0.61 | 0.69 | 0.87 | 0.58 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |
| \＃95th percentile volume exceeds capacity，queue may be longer． |  |  |  |  |  |  |  |  |  |  |

\＃95th percentile volume exceeds capacity，queue may be longer
Queue shown is maximum after two cycles．

HCM Signalized Intersection Capacity Analysis

| 6：Q | th／Q |  |  | rth \＆ | Brita | ia Rd | West |  |  |  |  | 8／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | 4 | \％ |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 个t |  | ＊ | 个个 | F | \％ | $\uparrow \uparrow$ |  | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 155 | 950 | 165 | 140 | 1215 | 145 | 165 | 390 | 140 | 285 | 545 | 355 |
| Future Volume（vph） | 155 | 950 | 165 | 140 | 1215 | 145 | 165 | 390 | 140 | 285 | 545 | 355 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Total Lost time（s） | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Lane Util．Factor | 1.00 | 0.95 |  | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.98 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1750 | 3486 |  | 1767 | 3579 | 1530 | 1785 | 3426 |  | 1762 | 1921 | 1538 |
| Flt Permitted | 0.07 | 1.00 |  | 0.12 | 1.00 | 1.00 | 0.10 | 1.00 |  | 0.27 | 1.00 | 1.00 |
| Satd．Flow（perm） | 133 | 3486 |  | 215 | 3579 | 1530 | 196 | 3426 |  | 497 | 1921 | 1538 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 155 | 950 | 165 | 140 | 1215 | 145 | 165 | 390 | 140 | 285 | 545 | 355 |
| RTOR Reduction（vph） | 0 | 9 | 0 | 0 | 0 | 56 | 0 | 23 | 0 | 0 | 0 | 117 |
| Lane Group Flow（vph） | 155 | 1106 | 0 | 140 | 1215 | 89 | 165 | 507 | ， | 285 | 545 | 238 |
| Confl．Peds．（\＃hr） | 12 |  | 9 | 9 |  | 12 | 10 |  | 24 | 24 |  | 10 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 0\％ | 1\％ | 2\％ | 1\％ | 0\％ | 1\％ | 1\％ | 1\％ | 0\％ | 1\％ |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | pm＋pt | NA |  | pm＋pt | NA | Perm |
| Protected Phases | 5 | ， |  | 1 | ， |  | 7 | 4 |  | 3 | ． |  |
| Permitted Phases | 2 |  |  | － |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green，G（s） | 79.5 | 67.5 |  | 76.3 | 65.9 | 65.9 | 51.0 | 39.0 |  | 64.1 | 49.1 | 49.1 |
| Effective Green， g （s） | 79.5 | 67.5 |  | 76.3 | 65.9 | 65.9 | 51.0 | 39.0 |  | 64.1 | 49.1 | 49.1 |
| Actuated g／C Ratio | 0.50 | 0.42 |  | 0.48 | 0.41 | 0.41 | 0.32 | 0.24 |  | 0.40 | 0.31 | 0.31 |
| Clearance Time（s） | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 187 | 1470 |  | 203 | 1474 | 630 | 181 | 835 |  | 373 | 589 | 471 |
| v／s Ratio Prot | c0．06 | 0.32 |  | 0.04 | 0.34 |  | c0．07 | 0.15 |  | c0．11 | c0． 28 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | c0．35 |  |  | 0.28 |  | 0.06 | 0.22 |  |  | 0.20 |  | 0.15 |
| v／c Ratio | 0.83 | 0.75 |  | 0.69 | 0.82 | 0.14 | 0.91 | 0.61 |  | 0.76 | 0.93 | 0.51 |
| Uniform Delay，d1 | 37.8 | 39.2 |  | 29.5 | 41.9 | 29.4 | 44.4 | 53.7 |  | 35.7 | 53.7 | 45.5 |
| Progression Factor | 1.00 | 1.00 |  | 1.22 | 0.90 | 0.68 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 25.0 | 3.6 |  | 8.2 | 4.7 | 0.4 | 42.5 | 1.3 |  | 9.0 | 20.5 | 0.9 |
| Delay（s） | 62.9 | 42.8 |  | 44.3 | 42.6 | 20.5 | 86.9 | 55.0 |  | 44.7 | 74.2 | 46.3 |
| Level of Service | E | D |  | D | D | C | F | D |  | D | E | D |
| Approach Delay（s） |  | 45.2 |  |  | 40.6 |  |  | 62.5 |  |  | 58.7 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | ， |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 49.8 |  | HCM 2000 | Level of S | Service |  | D |  |  |  |
| HCM 2000 Volume to Capacity | ratio |  | 0.88 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | time（s） |  |  | 21.0 |  |  |  |
| Intersection Capacity Utilizatio |  |  | 99．2\％ |  | CU Level | f Service |  |  | F |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


| 5y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total PM Peak Hour | Synchro 11 Report |
| :--- | ---: |
| BA Group | Page 8 |

HCM Unsignalized Intersection Capacity Analysis
7：Arch Rd \＆Britannia Rd West


[^20]HCM Unsignalized Intersection Capacity Analysis

| 8: Earl St \& Britannia Rd West |  |  |  |  |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ | $\geqslant$ | 7 | $\leftarrow$ | 4 | \% |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个t |  | \% | 个4 | M |  |  |  |
| Traffic Volume (veh/h) | 1370 | 5 | 5 | 1505 | 0 | 20 |  |  |
| Future Volume (Veh/h) | 1370 | 5 | 5 | 1505 | 0 | 20 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate (vph) | 1370 | 5 | 5 | 1505 | 0 | 20 |  |  |
| Pedestrians |  |  |  |  | 5 |  |  |  |
| Lane Width (m) |  |  |  |  | 3.5 |  |  |  |
| Walking Speed ( $\mathrm{m} / \mathrm{s}$ ) |  |  |  |  | 1.2 |  |  |  |
| Percent Blockage |  |  |  |  | 0 |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type T | TWLTL |  |  | TWLTL |  |  |  |  |
| Median storage veh) | 2 |  |  | 2 |  |  |  |  |
| Upstream signal ( m ) | 219 |  |  | 71 |  |  |  |  |
| pX, platoon unblocked |  |  | 0.74 |  | 0.81 | 0.74 |  |  |
| vC , conficting volume |  |  | 1380 |  | 2140 | 692 |  |  |
| vC1, stage 1 conf vol |  |  |  |  | 1378 |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  | 762 |  |  |  |
| vCu , unblocked vol |  |  | 817 |  | 1188 | 0 |  |  |
| tC , single (s) |  |  | 4.1 |  | 6.8 | 6.9 |  |  |
| tC, 2 stage (s) |  |  |  |  | 5.8 |  |  |  |
| tF (s) |  |  | 2.2 |  | 3.5 | 3.3 |  |  |
| p0 queue free \% |  |  | 99 |  | 100 | 98 |  |  |
| cM capacity (veh/h) |  |  | 606 |  | 276 | 806 |  |  |
| Direction, Lane \# | EB 1 | EB 2 | WB 1 | WB 2 | WB 3 | NB 1 |  |  |
| Volume Total | 913 | 462 | 5 | 752 | 752 | 20 |  |  |
| Volume Left | 0 | 0 | 5 | 0 | 0 | 0 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 20 |  |  |
| cSH | 1700 | 1700 | 606 | 1700 | 1700 | 806 |  |  |
| Volume to Capacity | 0.54 | 0.27 | 0.01 | 0.44 | 0.44 | 0.02 |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.6 |  |  |
| Control Delay (s) | 0.0 | 0.0 | 11.0 | 0.0 | 0.0 | 9.6 |  |  |
| Lane LOS |  |  | B |  |  | A |  |  |
| Approach Delay (s) | 0.0 |  | 0.0 |  |  | 9.6 |  |  |
| Approach LOS |  |  |  |  |  | A |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 51.6\% | ICU Level of Service |  |  | A |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

Timings
9: Britannia Rd West \& Ellesboro Dr 06/28/2023


Intersection Summar
Cycle Length: 160
Actuated Cycle Length: 160
Offset: 0 ( $0 \%$ ), Referenced to phase 2:EBTL and 6:WBT, Start of Green
Natural Cycle. 80
Contro Type: Actuated-Coordinated
Maximum v/c Ratio: 0.58

| Intersection Signal Delay : 7.3 | Intersection LOS: A |
| :--- | :--- |
| Intersection Capacity Utilization 66.3\% | ICU Level of Service C |
| Analysis Period (min) 15 |  |

Splits and Phases: 9: Britannia Rd West \& Ellesboro Dr


5y Future Total PM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Total PM Peak Hour BA Group
9: Britannia Rd West \& Ellesboro Dr
06/28/2023

| Lane Group | EBL | EBT | WBT | SBL | SBR |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Lane Group Flow (vph) | 15 | 1375 | 1550 | 100 | 35 |
| V/c Ratio | 0.07 | 0.46 | 0.52 | 0.58 | 0.20 |
| Control Delay | 3.3 | 3.8 | 5.0 | 82.8 | 26.6 |
| Queue Delay | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 |
| Total Delay | 3.3 | 3.9 | 5.0 | 82.8 | 26.6 |
| Queue Length 50th $(\mathrm{m})$ | 0.6 | 42.3 | 64.9 | 32.9 | 1.6 |
| Queue Length 95th $(\mathrm{m})$ | m 1.0 | 55.2 | 94.4 | 52.4 | 13.2 |
| Internal Link Dist $(\mathrm{m})$ | 45.0 | 46.6 | 115.6 | 80.1 | 15 |
| Turn Bay Length $(\mathrm{m})$ | 45.0 |  |  | 15.0 |  |
| Base Capacity (vph) | 224 | 2994 | 2971 | 435 | 393 |
| Starvation Cap Reductn | 0 | 448 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.54 | 0.52 | 0.23 | 0.09 |
| Intersection Summary |  |  |  |  |  |

m Volume for 95 th percentile queue is metered by upstream signal.

HCM Signalized Intersection Capacity Analysis
9: Britannia Rd West \& Elle

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 $\uparrow$ | 蚛 |  | \% | 7 |  |
| Traffic Volume (vph) | 15 | 1375 | 1475 | 75 | 100 | 35 |  |
| Future Volume (vph) | 15 | 1375 | 1475 | 75 | 100 | 35 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width | 3.5 | 3.7 | 3.7 | 3.5 | 3.5 | 3.5 |  |
| Total Lost time (s) | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |  | 1.00 | 1.00 |  |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 0.98 |  |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.99 |  | 1.00 | 0.85 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1783 | 3614 | 3584 |  | 1785 | 1520 |  |
| Flt Permitted | 0.14 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (perm) | 271 | 3614 | 3584 |  | 1785 | 1520 |  |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj. Flow (vph) | 15 | 1375 | 1475 | 75 | 100 | 35 |  |
| RTOR Reduction (vph) | 0 | 0 | 1 | 0 | 0 | 27 |  |
| Lane Group Flow (vph) | 15 | 1375 | 1549 | 0 | 100 | 8 |  |
| Confl. Peds. (\#hr) | 5 |  |  | 5 |  | 5 |  |
| Heavy Vehicles (\%) | 0\% | 1\% | 1\% | 0\% | 0\% | 3\% |  |
| Turn Type | Perm | NA | NA |  | Perm | Perm |  |
| Protected Phases |  | 2 | 6 |  |  |  |  |
| Permitted Phases | 2 |  |  |  | 8 | 8 |  |
| Actuated Green, G (s) | 132.6 | 132.6 | 132.6 |  | 15.3 | 15.3 |  |
| Effective Green, g (s) | 132.6 | 132.6 | 132.6 |  | 15.3 | 15.3 |  |
| Actuated g/C Ratio | 0.83 | 0.83 | 0.83 |  | 0.10 | 0.10 |  |
| Clearance Time (s) | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 224 | 2995 | 2970 |  | 170 | 145 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | 0.38 | c0.43 |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.06 |  |  |  | c0.06 | 0.01 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.07 | 0.46 | 0.52 |  | 0.59 | 0.05 |  |
| Uniform Delay, d1 | 2.5 | 3.8 | 4.1 |  | 69.3 | 65.8 |  |
| Progression Factor | 0.92 | 0.86 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 0.4 | 0.4 | 0.7 |  | 5.1 | 0.2 |  |
| Delay (s) | 2.7 | 3.6 | 4.8 |  | 74.5 | 65.9 |  |
| Level of Service | A | A | A |  | E | E |  |
| Approach Delay (s) |  | 3.6 | 4.8 |  | 72.2 |  |  |
| Approach LOS |  | A | A |  | E |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 7.2 |  | HCM 2000 | evel of Service | A |
| HCM 2000 Volume to Capacity ratio |  |  | 0.53 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 160.0 |  | Sum of los | time (s) | 12.1 |
| Intersection Capacity Utilization |  |  | 66.3\% | Cu Level of Service |  |  | C |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

5y Future Total PM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Total PM Peak Hour
BA Group

| HCM Unsignalized Intersection Capacity Analysis 1：Queen Street North \＆Matlock Ave |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  | $\dagger$ | 7 |  | $\dagger$ |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | Y |  | 个t |  | \％ | 个 $\uparrow$ |  |  |
| Traffic Volume（veh／h） | 30 | 20 | 985 | 40 | 15 | 595 |  |  |
| Future Volume（Veh／h） | 30 | 20 | 985 | 40 | 15 | 595 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |  |
| Grade | 0\％ |  | 0\％ |  |  | 0\％ |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Hourly flow rate（vph） | 33 | 22 | 1071 | 43 | 16 | 647 |  |  |
| Pedestrians | 1 |  |  |  |  |  |  |  |
| Lane Width（m） | 3.5 |  |  |  |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  | TWLTL |  |  | None |  |  |
| Median storage veh） |  |  | 2 |  |  |  |  |  |
| Upstream signal（ m ） |  |  | 313 |  |  |  |  |  |
| pX，platoon unblocked | 0.89 | 0.89 |  |  | 0.89 |  |  |  |
| vC ，conficting volume | 1449 | 558 |  |  | 1115 |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1094 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 356 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1249 | 243 |  |  | 872 |  |  |  |
| tC，single（s） | 7.3 | 7.4 |  |  | 4.9 |  |  |  |
| tC， 2 stage（s） | 6.3 |  |  |  |  |  |  |  |
| tF（s） | 3.7 | 3.5 |  |  | 2.6 |  |  |  |
| p0 queue free \％ | 88 | 96 |  |  | 97 |  |  |  |
| cM capacity（veh／h） | 272 | 612 |  |  | 500 |  |  |  |
| Direction，Lane \＃ | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | SB 3 |  |  |
| Volume Total | 55 | 714 | 400 | 16 | 324 | 324 |  |  |
| Volume Left | 33 | 0 | 0 | 16 | 0 | 0 |  |  |
| Volume Right | 22 | 0 | 43 | 0 | 0 | 0 |  |  |
| cSH | 350 | 1700 | 1700 | 500 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.16 | 0.42 | 0.24 | 0.03 | 0.19 | 0.19 |  |  |
| Queue Length 95th（m） | 4.4 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 17.2 | 0.0 | 0.0 | 12.4 | 0.0 | 0.0 |  |  |
| Lane LOS | C |  |  | B |  |  |  |  |
| Approach Delay（s） | 17.2 | 0.0 |  | 0.3 |  |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.6 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 38．5\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |


| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2：Queen Street North \＆ 40 Queen St N Driveway／53 Queen St Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
|  | $\stackrel{*}{ }$ |  |  | 1 |  |  | 4 | $\uparrow$ |  |  | $\dagger$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | ${ }^{7}$ | 个t |  | ${ }^{*}$ | 个t |  |
| Traffic Volume（veh／h） | 0 | ， | 0 | 0 | 0 | 0 | ， | 1025 | 0 | 0 | 625 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1025 | 0 | 0 | 625 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1165 | 0 | 0 | 710 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.86 | 0.86 |  | 0.86 | 0.86 | 0.86 |  |  |  | 0.86 |  |  |
| vC，conficting volume | 1292 | 1875 | 355 | 1520 | 1875 | 582 | 710 |  |  | 1165 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 710 | 710 |  | 1165 | 1165 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 582 | 1165 |  | 355 | 710 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1014 | 1692 | 355 | 1279 | 1692 | 189 | 710 |  |  | 866 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \％ | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity（veh／h） | 360 | 264 | 647 | 256 | 264 | 712 | 899 |  |  | 676 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 0 | 0 | 777 | 388 | 0 | 473 | 237 |  |  |  |  |
| Volume Left | 0 | 0 | 0 | － | 0 | 0 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| cSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.00 | 0.46 | 0.23 | 0.00 | 0.28 | 0.14 |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 31．7\％ |  | Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^21]| HCM Unsignalized Intersection Capacity Analysis 3：Queen Street North \＆ 40 Queen St S Driveway |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ |  | 4 | $\dagger$ |  | $\pm$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | M |  | \％ | ¢ $\uparrow$ | 中 ${ }^{\text {a }}$ |  |  |  |
| Traffic Volume（veh／h） | 0 | 0 | － | 1025 | 625 | 0 |  |  |
| Future Volume（Veh／h） | 0 | 0 | 0 | 1025 | 625 | 0 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |  |  |
| Hourly flow rate（vph） | 0 | 0 | 0 | 1178 | 718 | 0 |  |  |
| Pedestrians | 3 |  |  |  |  |  |  |  |
| Lane Width（m） | 3.5 |  |  |  |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | WLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ $m$ ） |  |  |  | 186 |  |  |  |  |
| pX，platoon unblocked | 0.85 |  |  |  |  |  |  |  |
| VC ，conflicting volume | 1310 | 362 | 721 |  |  |  |  |  |
| vC1，stage 1 conf vol | 721 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 589 |  |  |  |  |  |  |  |
| vCu，unblocked vol | 1022 | 362 | 721 |  |  |  |  |  |
| tC ，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 100 | 100 | 100 |  |  |  |  |  |
| cM capacity（veh／h） | 404 | 639 | 888 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 0 | 0 | 589 | 589 | 479 | 239 |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| cSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.35 | 0.35 | 0.28 | 0.14 |  |  |
| Queue Length 95th（ $m$ ） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | A |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | A |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 31．7\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

Analysis Period（min）

| HCM Unsignalized Intersection Capacity Analysis <br> 4：Queen Street North \＆Petro Canada N Driveway／Existing Site Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{*}{ }$ |  |  |  |  |  |  | $\dagger$ |  |  | $\dagger$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | \％ | 性 |  | ${ }^{*}$ | 个t |  |
| Traffic Volume（veh／h） | 0 | － | 0 | 5 | 0 | 0 | 5 | 1025 | 10 | 5 | 610 | 10 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 5 | 0 | 0 | 5 | 1025 | 10 | 5 | 610 | 10 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 1178 | 11 | 6 | 701 | 11 |
| Pedestrians |  | 3 |  |  | 6 |  |  | 1 |  |  |  |  |
| Lane Width（m） |  | 3.7 |  |  | 3.7 |  |  | 3.6 |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  | 1.2 |  |  | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage |  | 0 |  |  | 1 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 159 |  |  |  |  |
| pX，platoon unblocked | 0.85 | 0.85 |  | 0.85 | 0.85 | 0.85 |  |  |  | 0.85 |  |  |
| vC, conficting volume | 1322 | 1928 | 360 | 1565 | 1928 | 600 | 715 |  |  | 1195 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 722 | 722 |  | 1202 | 1202 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 601 | 1207 |  | 364 | 727 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1026 | 1739 | 360 | 1311 | 1739 | 176 | 715 |  |  | 876 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \％ | 100 | 100 | 100 | 98 | 100 | 100 | 99 |  |  | 99 |  |  |
| cM capacity（veh／h） | 350 | 249 | 640 | 244 | 251 | 713 | 892 |  |  | 659 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 6 | 6 | 785 | 404 | 6 | 467 | 245 |  |  |  |  |
| Volume Left | 0 | 6 | 6 | 0 | 0 | 6 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 11 |  |  |  |  |
| cSH | 1700 | 244 | 892 | 1700 | 1700 | 659 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.02 | 0.01 | 0.46 | 0.24 | 0.01 | 0.27 | 0.14 |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 0.6 | 0.2 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 20.1 | 9.1 | 0.0 | 0.0 | 10.5 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | C | A |  |  | B |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 20.1 | 0.0 |  |  | 0.1 |  |  |  |  |  |  |
| Approach LOS | A | c |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39．0\％ |  | Level | f Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^22]| HCM Unsignalized Intersection Capacity Analysis 5：Queen Street North \＆Petro Canada S Driveway |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 |  | 4 | $\dagger$ | $\downarrow$ | $\stackrel{ }{ }$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | Y |  | \％ | ¢ $\uparrow$ | 个t |  |  |  |
| Traffic Volume（veh／h） | 0 | 5 | 0 | 1040 | 605 | 10 |  |  |
| Future Volume（Veh／h） | 0 | 5 | 0 | 1040 | 605 | 10 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |  |  |
| Hourly flow rate（vph） | 0 | 6 | 0 | 1182 | 688 | 11 |  |  |
| Pedestrians | 3 |  |  | 2 |  |  |  |  |
| Lane Width（m） | 3.5 |  |  | 3.6 |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | TWLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ m ） |  |  |  | 127 |  |  |  |  |
| pX，platoon unblocked | 0.84 |  |  |  |  |  |  |  |
| VC, conflicting volume | 1288 | 354 | 702 |  |  |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 696 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 591 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 973 | 354 | 702 |  |  |  |  |  |
| tC ，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 100 | 99 | 100 |  |  |  |  |  |
| cM capacity（veh／h） | 417 | 645 | 902 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 6 | 0 | 591 | 591 | 459 | 240 |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 6 | 0 | 0 | 0 | 0 | 11 |  |  |
| cSH | 645 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.01 | 0.00 | 0.35 | 0.35 | 0.27 | 0.14 |  |  |
| Queue Length 95th（ m ） | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 10.6 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | B |  |  |  |  |  |  |  |
| Approach Delay（s） | 10.6 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39．4\％ |  | Level | Service | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

[^23]Timings
6：Queen Street South／Queen Street North \＆Britannia Rd West 06／18／2023

|  | $\rangle$ | $\rightarrow$ | 7 |  |  | 4 | $\uparrow$ | － | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 个t | \％ | 个4 | $\overline{7}$ | \％ | 中 | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 215 | 1615 | 80 | 640 | 325 | 95 | 500 | 140 | 330 | 140 |
| Future Volume（vph） | 215 | 1615 | 80 | 640 | 325 | 95 | 500 | 140 | 330 | 140 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | Perm | NA | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 | 1 | 6 |  |  | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 12.0 | 12.0 | 8.0 | 12.0 | 12.0 |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 38.9 | 38.9 | 11.0 | 38.9 | 38.9 |
| Total Split（s） | 13.0 | 83.0 | 11.0 | 81.0 | 81.0 | 53.0 | 53.0 | 13.0 | 66.0 | 66.0 |
| Total Split（\％） | 8．1\％ | 51．9\％ | 6．9\％ | 50．6\％ | 50．6\％ | 33．1\％ | 33．1\％ | 8．1\％ | 41．3\％ | 41．3\％ |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 3.9 | 3.9 | 0.0 | 3.9 | 3.9 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 7.9 | 7.9 | 3.0 | 7.9 | 7.9 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |
| Act Efft Green（s） | 101.2 | 85.4 | 95.2 | 81.9 | 81.9 | 34.4 | 34.4 | 52.3 | 47.4 | 47.4 |
| Actuated g／C Ratio | 0.63 | 0.53 | 0.60 | 0.51 | 0.51 | 0.22 | 0.22 | 0.33 | 0.30 | 0.30 |
| $\mathrm{V} / \mathrm{C}$ Ratio | 0.44 | 0.91 | 0.56 | 0.37 | 0.37 | 0.53 | 0.83 | 0.79 | 0.60 | 0.27 |
| Control Delay | 16.0 | 42.5 | 45.0 | 22.8 | 4.8 | 65.5 | 67.9 | 68.9 | 52.7 | 6.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 16.0 | 42.5 | 45.0 | 22.8 | 4.8 | 65.5 | 67.9 | 68.9 | 52.7 | 6.6 |
| LOS | B | D | D | C | A | E | E | E | D | A |
| Approach Delay |  | 39.5 |  | 18.9 |  |  | 67.6 |  | 45.8 |  |
| Approach LOS |  | D |  | B |  |  | E |  | D |  |

## Intersection Summary

Cycle Length： 160
Actuated Cycle Length： 160
Offset： 13 （8\％），Referenced to phase 2：EBTL and 6：WBTL，Start of Green
Control Type：Actuated－Coordinated
Maximum v／c Ratio：0．C

| Intersection Signal Delay：40．1 | Intersection LOS：D |
| :--- | :--- |
| Intersection Capacity Utilization 107．6\％ | ICU Level of Service |

Intersection Capacity Utilization 107．6\％
ICU Level of Service G
Analysis Period（min） 15


[^24]Queues

| 6: Queen Street | Qu | n Str | N | h \& | Britan | Rd | Nest |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ | 1 | $\Perp$ | 4 | 4 | 4 | * | $\downarrow$ | 4 |  |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |  |
| Lane Group Flow (vph) | 215 | 1715 | 80 | 640 | 325 | 95 | 625 | 140 | 330 | 140 |  |
| v/c Ratio | 0.44 | 0.91 | 0.56 | 0.37 | 0.37 | 0.53 | 0.83 | 0.79 | 0.60 | 0.27 |  |
| Control Delay | 16.0 | 42.5 | 45.0 | 22.8 | 4.8 | 65.5 | 67.9 | 68.9 | 52.7 | 6.6 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 16.0 | 42.5 | 45.0 | 22.8 | 4.8 | 65.5 | 67.9 | 68.9 | 52.7 | 6.6 |  |
| Queue Length 50th (m) | 28.6 | 264.6 | 10.1 | 67.4 | 16.6 | 28.4 | 103.3 | 34.5 | 95.0 | 0.0 |  |
| Queue Length 95th (m) | 47.5 | \#363.7 | 24.7 | 91.4 | 34.1 | 46.9 | 119.7 | \#56.3 | 121.3 | 16.0 |  |
| Internal Link Dist ( $m$ ) |  | 110.7 |  | 83.1 |  |  | 135.0 |  | 103.4 |  |  |
| Turn Bay Length ( m ) | 95.0 |  | 60.0 |  | 45.0 | 40.0 |  | 35.0 |  |  |  |
| Base Capacity (vph) | 485 | 1886 | 144 | 1746 | 888 | 237 | 982 | 178 | 670 | 603 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.44 | 0.91 | 0.56 | 0.37 | 0.37 | 0.40 | 0.64 | 0.79 | 0.49 | 0.23 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume | ds ca | pacity, que | may | e longer |  |  |  |  |  |  |  |

[^25]HCM Signalized Intersection Capacity Analysis


[^26]
## HCM Unsignalized Intersection Capacity Analysis

| 7：Arch Rd \＆Britannia Rd West |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ | $\geqslant$ | 1 | $\bullet$ | 4 | ／ |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个家 |  | \％ | 个4 | M |  |  |  |
| Traffic Volume（veh／h） | 1875 | 5 | 10 | 1040 | 5 | 10 |  |  |
| Future Volume（Veh／h） | 1875 | 5 | 10 | 1040 | 5 | 10 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate（vph） | 1875 | 5 | 10 | 1040 | 5 | 10 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type | None |  |  | WLTL |  |  |  |  |
| Median storage veh） |  |  |  | 2 |  |  |  |  |
| Upstream signal（ $m$ ） | 107 |  |  | 182 |  |  |  |  |
| pX，platoon unblocked |  |  | 0.55 |  | 0.58 | 0.55 |  |  |
| vC ，conficting volume |  |  | 1880 |  | 2418 | 940 |  |  |
| VC1，stage 1 conf vol |  |  |  |  | 1878 |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol |  |  |  |  | 540 |  |  |  |
| vCu ，unblocked vol |  |  | 964 |  | 1537 | 0 |  |  |
| tC，single（s） |  |  | 4.1 |  | 6.8 | 7.1 |  |  |
| tC， 2 stage（s） |  |  |  |  | 5.8 |  |  |  |
| tF（s） |  |  | 2.2 |  | 3.5 | 3.4 |  |  |
| p0 queue free \％ |  |  | 97 |  | 97 | 98 |  |  |
| cM capacity（veh／h） |  |  | 397 |  | 176 | 586 |  |  |
| Direction，Lane \＃ | EB 1 | EB 2 | WB 1 | WB 2 | WB 3 | NB 1 |  |  |
| Volume Total | 1250 | 630 | 10 | 520 | 520 | 15 |  |  |
| Volume Left | 0 | 0 | 10 | 0 | 0 | 5 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 10 |  |  |
| cSH | 1700 | 1700 | 397 | 1700 | 1700 | 330 |  |  |
| Volume to Capacity | 0.74 | 0.37 | 0.03 | 0.31 | 0.31 | 0.05 |  |  |
| Queue Length 95th（m） | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.1 |  |  |
| Control Delay（s） | 0.0 | 0.0 | 14.3 | 0.0 | 0.0 | 16.4 |  |  |
| Lane LOS |  |  | B |  |  | C |  |  |
| Approach Delay（s） | 0.0 |  | 0.1 |  |  | 16.4 |  |  |
| Approach LOS |  |  |  |  |  | C |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 62．0\％ |  | CU Level | Service | B |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
8：Earl St \＆Britannia Rd West


[^27]9: Britannia Rd West \& Ellesboro Dr 06/28/2023


## Intersection Summary

Cycle Length: 160
Actuated Cycle Length: 160
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and $6: W B T$, Start of Green
Natural Cycle: 90
\(\begin{array}{ll}Control Type: Actuated-Coordinated \& <br>

\)|  Maximum v/c Ratio:  0.60 |  |
| :--- | :--- |
|  Intersection Signal Delay:  4.2 |  Intersection LOS: A  |
|  Intersection Capacity Utiization  $77.4 \%$ |  ICU Level of Service D  |\end{array}

Analysis Period (min) 15


[^28]Queues
9: Britannia Rd West \& Ellesboro Dr

| Lane Group | EBL | EBT | WBT | SBL | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 30 | 1875 | 1090 | 60 | 30 |
| v/c Ratio | 0.07 | 0.60 | 0.37 | 0.40 | 0.20 |
| Control Delay | 1.0 | 2.3 | 2.9 | 77.8 | 23.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 1.0 | 2.3 | 2.9 | 77.8 | 23.8 |
| Queue Length 50th (m) | 0.6 | 26.8 | 35.4 | 19.5 | 0.0 |
| Queue Length 95th (m) | m0.7 | 24.4 | 46.0 | 35.5 | 11.4 |
| Internal Link Dist ( $m$ ) |  | 46.6 | 115.6 | 80.1 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  | 15.0 |
| Base Capacity (vph) | 401 | 3120 | 2967 | 434 | 375 |
| Starvation Cap Reductn | 0 | 147 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.63 | 0.37 | 0.14 | 0.08 |
| Intersection Summary |  |  |  |  |  |

[^29]| HCM Signalized Intersection Capacity Analysis 9：Britannia Rd West \＆Ellesboro Dr |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | － | 4 | ＊ | 4 |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |  |
| Lane Configurations | \％ | 个4 | 性 |  | \％ | 「 |  |  |
| Traffic Volume（vph） | 30 | 1875 | 1020 | 70 | 60 | 30 |  |  |
| Future Volume（vph） | 30 | 1875 | 1020 | 70 | 60 | 30 |  |  |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Lane Width | 3.5 | 3.7 | 3.7 | 3.5 | 3.5 | 3.5 |  |  |
| Total Lost time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 0.95 |  | 1.00 | 1.00 |  |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 0.97 |  |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Frt | 1.00 | 1.00 | 0.99 |  | 1.00 | 0.85 |  |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Flow（prot） | 1729 | 3579 | 3404 |  | 1782 | 1447 |  |  |
| Fit Permitted | 0.25 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Fow（perm） | 461 | 3579 | 3404 |  | 1782 | 1447 |  |  |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj．Flow（vph） | 30 | 1875 | 1020 | 70 | 60 | 30 |  |  |
| RTOR Reduction（vph） | 0 | 0 | 1 | 0 | 0 | 28 |  |  |
| Lane Group Flow（vph） | 30 | 1875 | 1089 | 0 | 60 | 2 |  |  |
| Confl．Peds．（\＃／hr） | 4 |  |  | 4 | ， | 12 |  |  |
| Heavy Vehicles（\％） | 3\％ | 2\％ | 6\％ | 6\％ | 0\％ | 7\％ |  |  |
| Turn Type | Perm | NA | NA |  | Perm | Perm |  |  |
| Protected Phases |  | 2 | 6 |  |  |  |  |  |
| Permitted Phases | 2 |  |  |  | 8 | 8 |  |  |
| Actuated Green，G（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Effective Green，g（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Actuated g／C Ratio | 0.86 | 0.86 | 0.86 |  | 0.07 | 0.07 |  |  |
| Clearance Time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |
| Lane Grp Cap（vph） | 395 | 3066 | 2916 |  | 120 | 97 |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | c0．52 | 0.32 |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.07 |  |  |  | c0．03 | 0.00 |  |  |
| v／c Ratio | 0.08 | 0.61 | 0.37 |  | 0.50 | 0.02 |  |  |
| Uniform Delay，d1 | 1.8 | 3.4 | 2.4 |  | 72.0 | 69.7 |  |  |
| Progression Factor | 0.37 | 0.49 | 1.00 |  | 1.00 | 1.00 |  |  |
| Incremental Delay，d2 | 0.2 | 0.4 | 0.4 |  | 3.3 | 0.1 |  |  |
| Delay（s） | 0.8 | 2.1 | 2.8 |  | 75.2 | 69.7 |  |  |
| Level of Service | A | A | A |  | E | E |  |  |
| Approach Delay（s） |  | 2.1 | 2.8 |  | 73.4 |  |  |  |
| Approach LOS |  | A | A |  | E |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 4.4 |  | HCM 2000 | evel of Service | A |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.60 |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | ime（s） | 12.1 |  |
| Intersection Capacity Utilization |  |  | 77．4\％ |  | CU Level | Service | D |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |

10y Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background AM
BA Group

HCM Unsignalized Intersection Capacity Analysis
1：Queen Street North \＆Matlock Ave
06／28／2023

| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | M |  | 个t |  | ＊ | 个 $\uparrow$ |  |
| Traffic Volume（veh／h） | 55 | 15 | 570 | 60 | 15 | 1080 |  |
| Future Volume（Veh／h） | 55 | 15 | 570 | 60 | 15 | 1080 |  |
| Sign Control | Stop |  | Free |  |  | Free |  |
| Grade | 0\％ |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |
| Hourly flow rate（vph） | 60 | 16 | 620 | 65 | 16 | 1174 |  |
| Pedestrians | 6 |  |  |  |  | 1 |  |
| Lane Width（m） | 3.5 |  |  |  |  | 3.6 |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） | 1.2 |  |  |  |  | 1.2 |  |
| Percent Blockage | 0 |  |  |  |  | 0 |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |
| Median type |  |  | TWLTL |  |  | None |  |
| Median storage veh） |  |  | 2 |  |  |  |  |
| Upstream signal（ $m$ ） |  |  | 313 |  |  |  |  |
| pX，platoon unblocked | 0.97 | 0.97 |  |  | 0.97 |  |  |
| VC ，conflicting volume | 1278 | 350 |  |  | 691 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 658 |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 619 |  |  |  |  |  |  |
| vCu ，unblocked vol | 1223 | 266 |  |  | 619 |  |  |
| tC ，single（s） | 7.0 | 6.9 |  |  | 4.4 |  |  |
| tC， 2 stage（s） | 6.0 |  |  |  |  |  |  |
| tF（s） | 3.6 | 3.3 |  |  | 2.4 |  |  |
| p0 queue free \％ | 83 | 98 |  |  | 98 |  |  |
| cM capacity（veh／h） | 363 | 711 |  |  | 844 |  |  |
| Direction，Lane \＃ | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | SB 3 |  |
| Volume Total | 76 | 413 | 272 | 16 | 587 | 587 |  |
| Volume Left | 60 | 0 | 0 | 16 | 0 | 0 |  |
| Volume Right | 16 | 0 | 65 | 0 | 0 | 0 |  |
| cSH | 404 | 1700 | 1700 | 844 | 1700 | 1700 |  |
| Volume to Capacity | 0.19 | 0.24 | 0.16 | 0.02 | 0.35 | 0.35 |  |
| Queue Length 95th（m） | 5.5 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |  |
| Control Delay（s） | 16.0 | 0.0 | 0.0 | 9.4 | 0.0 | 0.0 |  |
| Lane LOS | C |  |  | A |  |  |  |
| Approach Delay（s） | 16.0 | 0.0 |  | 0.1 |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.7 |  |  |  |  |
| Intersection Capacity UtilizationAnalysis Period（min） |  |  | 40．8\％ | ICU Level of Service |  |  | A |
|  |  |  | 15 |  |  |  |  |

[^30]| HCM Unsignalized Intersection Capacity Analysis <br> 2：Queen Street North \＆ 40 Queen St $N$ Driveway／53 Queen St Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 1 |  |  | 4 | $\dagger$ | \％ |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | \％ | 个 ${ }^{\text {a }}$ |  | ${ }^{7}$ | 个家 |  |
| Traffic Volume（veh／h） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 630 | 0 | 5 | 1130 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 630 | 0 | 5 | 1130 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate（vph） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 692 | 0 | 5 | 1242 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.94 | 0.94 |  | 0.94 | 0.94 | 0.94 |  |  |  | 0.94 |  |  |
| VC, conflicting volume | 1608 | 1954 | 621 | 1338 | 1954 | 346 | 1242 |  |  | 692 |  |  |
| vC1，stage 1 conf vol | 1252 | 1252 |  | 702 | 702 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 356 | 702 |  | 636 | 1252 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1513 | 1883 | 621 | 1224 | 1883 | 165 | 1242 |  |  | 534 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 99 | 98 | 100 | 100 | 99 |  |  | 99 |  |  |
| cM capacity（veh／h） | 178 | 219 | 435 | 328 | 216 | 802 | 568 |  |  | 977 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 5 | 5 | 5 | 461 | 231 | 5 | 828 | 414 |  |  |  |  |
| Volume Left | 0 | 5 | 5 | 0 | 0 | 5 | 0 | 0 |  |  |  |  |
| Volume Right | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| cSH | 435 | 328 | 568 | 1700 | 1700 | 977 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.01 | 0.02 | 0.01 | 0.27 | 0.14 | 0.01 | 0.49 | 0.24 |  |  |  |  |
| Queue Length 95th（m） | 0.3 | 0.4 | 0.2 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 13.4 | 16.1 | 11.4 | 0.0 | 0.0 | 8.7 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | B | c | B |  |  | A |  |  |  |  |  |  |
| Approach Delay（s） | 13.4 | 16.1 | 0.1 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | B | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 42．1\％ |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period（min）


[^31]| HCM Unsignalized In <br> 4：Queen Street North |  | $\begin{aligned} & \text { ction } \\ & \text { etro } \end{aligned}$ | paci <br> nada |  | sis way | xistin |  |  |  |  |  | 2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 1 |  |  | 4 | $\uparrow$ | 7 |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | \％ | 个t |  | ${ }^{7}$ | 个家 |  |
| Traffic Volume（veh／h） | 0 | 0 | 0 | 30 | 0 | 20 | 10 | 610 | 25 | 15 | 1120 | 10 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 30 | 0 | 20 | 10 | 610 | 25 | 15 | 1120 | 10 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 33 | 0 | 22 | 11 | 670 | 27 | 16 | 1231 | 11 |
| Pedestrians |  | 2 |  |  | 28 |  |  |  |  |  |  |  |
| Lane Width（m） |  | 3.7 |  |  | 3.7 |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  | 1.2 |  |  | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage |  | 0 |  |  | 2 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 159 |  |  |  |  |
| pX，platoon unblocked | 0.91 | 0.91 |  | 0.91 | 0.91 | 0.91 |  |  |  | 0.91 |  |  |
| VC, conflicting volume | 1650 | 2018 | 623 | 1381 | 2010 | 376 | 1244 |  |  | 725 |  |  |
| vC1，stage 1 conf vol | 1270 | 1270 |  | 734 | 734 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 379 | 747 |  | 648 | 1276 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1521 | 1924 | 623 | 1227 | 1915 | 127 | 1244 |  |  | 509 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 100 | 90 | 100 | 97 | 98 |  |  | 98 |  |  |
| cM capacity（veh／h） | 171 | 209 | 433 | 317 | 202 | 807 | 566 |  |  | 951 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 55 | 11 | 447 | 250 | 16 | 821 | 421 |  |  |  |  |
| Volume Left | 0 | 33 | 11 | － | 0 | 16 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 22 | 0 | 0 | 27 | 0 | 0 | 11 |  |  |  |  |
| cSH | 1700 | 419 | 566 | 1700 | 1700 | 951 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.13 | 0.02 | 0.26 | 0.15 | 0.02 | 0.48 | 0.25 |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 3.6 | 0.5 | 0.0 | 0.0 | 0.4 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 14.9 | 11.5 | 0.0 | 0.0 | 8.9 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | B | B |  |  | A |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 14.9 | 0.2 |  |  | 0.1 |  |  |  |  |  |  |
| Approach LOS | A | B |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 41．3\％ |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis

| 5：Queen Street North \＆Petro Canada S Driveway |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ |  | 4 | $\dagger$ | $\dagger$ | $\pm$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | Y |  | ${ }^{7}$ | 个4 | 个t |  |  |  |
| Traffic Volume（veh／h） | 5 | 15 | 5 | 640 | 1150 | 0 |  |  |
| Future Volume（Veh／h） | 5 | 15 | 5 | 640 | 1150 | 0 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |  |  |
| Hourly flow rate（vph） | 5 | 16 | 5 | 703 | 1264 | 0 |  |  |
| Pedestrians | 2 |  |  | 4 |  |  |  |  |
| Lane Width（m） | 3.5 |  |  | 3.6 |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | TWLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（m） |  |  |  | 127 |  |  |  |  |
| pX，platoon unblocked | 0.90 |  |  |  |  |  |  |  |
| vC，conficting volume | 1628 | 638 | 1266 |  |  |  |  |  |
| vC1，stage 1 conf vol | 1266 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 362 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1482 | 638 | 1266 |  |  |  |  |  |
| tC ，single（s） | 6.8 | 7.0 | 4.1 |  |  |  |  |  |
| $\mathrm{tC}, 2$ stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.4 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 98 | 96 | 99 |  |  |  |  |  |
| cM capacity（veh／h） | 224 | 405 | 555 |  |  |  |  |  |
| Direction，Lane\＃ | EB 1 | NB 1 | NB 2 | NB3 | SB 1 | SB 2 |  |  |
| Volume Total | 21 | 5 | 352 | 352 | 843 | 421 |  |  |
| Volume Left | 5 | 5 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 16 | 0 | 0 | 0 | 0 | 0 |  |  |
| cSH | 340 | 555 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.06 | 0.01 | 0.21 | 0.21 | 0.50 | 0.25 |  |  |
| Queue Length 95th（m） | 1.6 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 16.3 | 11.5 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | C | B |  |  |  |  |  |  |
| Approach Delay（s） | 16.3 | 0.1 |  |  | 0.0 |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.2 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 43．0\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

[^32]Timings
6：Queen Street South／Queen Street North \＆Britannia Rd West 06／28／2023

|  | $\stackrel{ }{ }$ |  | 1 |  |  | 4 | 4 |  | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 个t | ${ }_{1}$ | 个 $\uparrow$ | 「 | ${ }^{7}$ | 中t | ${ }^{7}$ | $\uparrow$ | F |
| Traffic Volume（vph） | 145 | 970 | 140 | 1245 | 125 | 165 | 375 | 280 | 540 | 345 |
| Future Volume（vph） | 145 | 970 | 140 | 1245 | 125 | 165 | 375 | 280 | 540 | 345 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 | 1 | 6 |  | 7 | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 7 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 5.0 | 12.0 | 8.0 | 12.0 | 12.0 |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 9.5 | 38.9 | 11.0 | 38.9 | 38.9 |
| Total Split（s） | 13.0 | 74.0 | 11.0 | 72.0 | 72.0 | 14.0 | 58.0 | 17.0 | 61.0 | 61.0 |
| Total Split（\％） | 8．1\％ | 46．3\％ | 6．9\％ | 45．0\％ | 45．0\％ | 8．8\％ | 36．3\％ | 10．6\％ | 38．1\％ | 38．1\％ |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 0.0 | 3.9 | 0.0 | 3.9 | 3.9 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 | 3.0 | 7.9 | 7.9 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |
| Act Effict Green（s） | 85.1 | 69.8 | 80.8 | 67.6 | 67.6 | 62.0 | 46.1 | 68.0 | 49.1 | 49.1 |
| Actuated g／C Ratio | 0.53 | 0.44 | 0.50 | 0.42 | 0.42 | 0.39 | 0.29 | 0.42 | 0.31 | 0.31 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.80 | 0.74 | 0.70 | 0.82 | 0.18 | 0.92 | 0.51 | 0.80 | 0.92 | 0.61 |
| Control Delay | 59.4 | 41.4 | 40.6 | 42.4 | 9.7 | 84.4 | 45.5 | 50.3 | 74.4 | 32.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 59.4 | 41.4 | 40.6 | 42.4 | 9.7 | 84.4 | 45.5 | 50.3 | 74.4 | 32.5 |
| LOS | E | D | D | D | A | F | D | D | E | C |
| Approach Delay |  | 43.4 |  | 39.5 |  |  | 54.9 |  | 56.2 |  |
| Approach LOS |  | D |  | D |  |  | D |  | E |  |

$\frac{\text { Intersection Summary }}{\text { Cycle Length：} 160}$
Cycle Length： 160
Actuated Cycle Len
Actuated Cycle Length： 160
Offset 13 （8\％）Ret
Offset： 13 （8\％），Referenced to phase 2：EBTL and 6：WBTL，Start of Green

| Natural |  |
| :--- | :--- |
| Control Type：Actuated－Coordinated |  |
| Maximum v／c Ratio： 0.92 | Intersection LOS：D |
| Intersection Signal Delay： 47.1 | ICU Level of Service F |
| Intersection Capacity Utilization $99.2 \%$ |  |

Intersection Capacity Utilization 99．2\％
ICU Level of Service F
Analysis Period（min） 15


[^33]Queues
6：Queen Street South／Queen Street North \＆Britannia Rd West
06／28／2023

\＃95th percentile volume exceeds capacity，queue may be longer
Queue shown is maximum after two cycles．

HCM Signalized Intersection Capacity Analysis

| 6：Q | th／Q |  |  | rth \＆ | Brita | Rd | West |  |  |  |  | 8／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 7 |  | 4 | 4 | 4 | \％ |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 个t |  | ＊ | 个个 | F | \％ | $\uparrow \uparrow$ |  | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 145 | 970 | 165 | 140 | 1245 | 125 | 165 | 375 | 140 | 280 | 540 | 345 |
| Future Volume（vph） | 145 | 970 | 165 | 140 | 1245 | 125 | 165 | 375 | 140 | 280 | 540 | 345 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Total Lost time（s） | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Lane Util．Factor | 1.00 | 0.95 |  | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.98 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1750 | 3487 |  | 1767 | 3579 | 1530 | 1785 | 3421 |  | 1760 | 1921 | 1538 |
| Flt Permitted | 0.07 | 1.00 |  | 0.12 | 1.00 | 1.00 | 0.10 | 1.00 |  | 0.32 | 1.00 | 1.00 |
| Satd．Flow（perm） | 129 | 3487 |  | 221 | 3579 | 1530 | 179 | 3421 |  | 589 | 1921 | 1538 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 145 | 970 | 165 | 140 | 1245 | 125 | 165 | 375 | 140 | 280 | 540 | 345 |
| RTOR Reduction（vph） | 0 | 8 | 0 | 0 | 0 | 43 | 0 | 25 | 0 | 0 | 0 | 92 |
| Lane Group Flow（vph） | 145 | 1127 | 0 | 140 | 1245 | 82 | 165 | 490 | ， | 280 | 540 | 253 |
| Confl．Peds．（\＃hr） | 12 |  | 9 | 9 |  | 12 | 10 |  | 24 | 24 |  | 10 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 0\％ | 1\％ | 2\％ | 1\％ | 0\％ | 1\％ | 1\％ | 1\％ | 0\％ | 1\％ |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | pm＋pt | NA |  | pm＋pt | NA | Perm |
| Protected Phases | 5 | ， |  | 1 | ， |  | 7 | 4 |  | 3 | ． |  |
| Permitted Phases | 2 |  |  | － |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green，G（s） | 81.1 | 69.8 |  | 76.7 | 67.6 | 67.6 | 57.1 | 46.1 |  | 63.1 | 49.1 | 49.1 |
| Effective Green，g（s） | 81.1 | 69.8 |  | 76.7 | 67.6 | 67.6 | 57.1 | 46.1 |  | 63.1 | 49.1 | 49.1 |
| Actuated g／C Ratio | 0.51 | 0.44 |  | 0.48 | 0.42 | 0.42 | 0.36 | 0.29 |  | 0.39 | 0.31 | 0.31 |
| Clearance Time（s） | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 179 | 1521 |  | 193 | 1512 | 646 | 174 | 985 |  | 334 | 589 | 471 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0．06 | 0.32 |  | 0.04 | 0.35 |  | c0．07 | 0.14 |  | c0．07 | c0． 28 |  |
| v／s Ratio Perm | c0．35 |  |  | 0.30 |  | 0.05 | 0.27 |  |  | 0.26 |  | 0.16 |
| v／c Ratio | 0.81 | 0.74 |  | 0.73 | 0.82 | 0.13 | 0.95 | 0.50 |  | 0.84 | 0.92 | 0.54 |
| Uniform Delay，d1 | 36.3 | 37.6 |  | 29.2 | 40.9 | 28.2 | 41.6 | 47.3 |  | 39.7 | 53.5 | 46.0 |
| Progression Factor | 1.00 | 1.00 |  | 1.09 | 0.90 | 0.71 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 23.4 | 3.3 |  | 11.2 | 4.6 | 0.4 | 52.6 | 0.4 |  | 16.6 | 19.1 | 1.2 |
| Delay（s） | 59.8 | 40.8 |  | 43.0 | 41.4 | 20.3 | 94.2 | 47.7 |  | 56.3 | 72.6 | 47.2 |
| Level of Service | E | D |  | D | D | C | F | D |  | E | E | D |
| Approach Delay（s） |  | 43.0 |  |  | 39.8 |  |  | 59.0 |  |  | 61.1 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | E |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 48.9 |  | HCM 2000 | Level of S | Service |  | D |  |  |  |
| HCM 2000 Volume to Capacity | ratio |  | 0.88 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | time（s） |  |  | 21.0 |  |  |  |
| Intersection Capacity Utilizatio |  |  | 99．2\％ |  | CU Level | f Service |  |  | F |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

[^34]HCM Unsignalized Intersection Capacity Analysis
7：Arch Rd \＆Britannia Rd West


[^35]HCM Unsignalized Intersection Capacity Analysis

| 8: Earl St \& Britannia Rd West |  |  |  |  |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ |  | 1 | $\downarrow$ | 4 | \% |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个t |  | \% | 个4 | M |  |  |  |
| Traffic Volume (veh/h) | 1385 | 5 | 5 | 1515 | 0 | 20 |  |  |
| Future Volume (Veh/h) | 1385 | 5 | 5 | 1515 | 0 | 20 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate (vph) | 1385 | 5 | 5 | 1515 | 0 | 20 |  |  |
| Pedestrians |  |  |  |  | 5 |  |  |  |
| Lane Width (m) |  |  |  |  | 3.5 |  |  |  |
| Walking Speed (m/s) |  |  |  |  | 1.2 |  |  |  |
| Percent Blockage |  |  |  |  | 0 |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type T | TWLTL |  |  | TWLTL |  |  |  |  |
| Median storage veh) | 2 |  |  | 2 |  |  |  |  |
| Upstream signal ( m ) | 219 |  |  | 71 |  |  |  |  |
| pX, platoon unblocked |  |  | 0.74 |  | 0.81 | 0.74 |  |  |
| vC, conficting volume |  |  | 1395 |  | 2160 | 700 |  |  |
| vC1, stage 1 conf vol |  |  |  |  | 1392 |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  | 768 |  |  |  |
| vCu, unblocked vol |  |  | 835 |  | 1203 | 0 |  |  |
| tC, single (s) |  |  | 4.1 |  | 6.8 | 6.9 |  |  |
| tC, 2 stage (s) |  |  |  |  | 5.8 |  |  |  |
| tF (s) |  |  | 2.2 |  | 3.5 | 3.3 |  |  |
| p0 queue free \% |  |  | 99 |  | 100 | 98 |  |  |
| cM capacity (veh/h) |  |  | 596 |  | 271 | 806 |  |  |
| Direction, Lane \# | EB 1 | EB2 | WB 1 | WB2 | WB3 | NB 1 |  |  |
| Volume Total | 923 | 467 | 5 | 758 | 758 | 20 |  |  |
| Volume Left | 0 | 0 | 5 | 0 | 0 | 0 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 20 |  |  |
| cSH | 1700 | 1700 | 596 | 1700 | 1700 | 806 |  |  |
| Volume to Capacity | 0.54 | 0.27 | 0.01 | 0.45 | 0.45 | 0.02 |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.6 |  |  |
| Control Delay (s) | 0.0 | 0.0 | 11.1 | 0.0 | 0.0 | 9.6 |  |  |
| Lane LOS |  |  | B |  |  | A |  |  |
| Approach Delay (s) | 0.0 |  | 0.0 |  |  | 9.6 |  |  |
| Approach LOS |  |  |  |  |  | A |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 51.9\% | ICU Level of Service |  |  | A |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

Analysis Period (min)

| 10y Future Background PM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Background PM |  |
| :--- | ---: |
| BA Group | Synchro 11 Report |
| Page 10 |  |

Timings
9: Britannia Rd West \& Ellesboro Dr 06/28/2023


Intersection Summar
Cycle Length: 160
Actuated Cycle Length: 160
Offset: 0 ( $0 \%$ ), Referenced to phase 2:EBTL and 6:WBT, Start of Green
Natural Cycle. 80
Conitro Type: Actuated-Coordinated

| Maximum v/c Ratio: 0.58 | Intersection LOS: A |
| :--- | :--- |
| Intersection Signal Delay: 7.5 | ICU Level of Service C |
| Intersection Capacity Utilization $66.6 \%$ |  |
| Analysis Period (min) 15 |  |

Analysis Period (min) 15
Splits and Phases: 9: Britannia Rd West \& Ellesboro Dr

9: Britannia Rd West \& Ellesboro Dr
06/28/2023

| Lane Group | EBL | EBT | WBT | SBL | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 15 | 1390 | 1560 | 100 | 35 |
| v/c Ratio | 0.07 | 0.46 | 0.53 | 0.58 | 0.20 |
| Control Delay | 3.4 | 4.3 | 5.0 | 82.8 | 26.6 |
| Queue Delay | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 |
| Total Delay | 3.4 | 4.4 | 5.0 | 82.8 | 26.6 |
| Queue Length 50th (m) | 0.8 | 55.6 | 65.5 | 32.9 | 1.6 |
| Queue Length 95th (m) | m1.1 | 59.4 | 95.5 | 52.4 | 13.2 |
| Internal Link Dist ( $m$ ) |  | 46.6 | 115.6 | 80.1 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  | 15.0 |
| Base Capacity (vph) | 221 | 2994 | 2971 | 435 | 393 |
| Starvation Cap Reductn | 0 | 429 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.54 | 0.53 | 0.23 | 0.09 |
| Intersection Summary |  |  |  |  |  |

m Volume for 95 th percentile queue is metered by upstream signal.

HCM Signalized Intersection Capacity Analysis
9: Britannia Rd West \& Ele

| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 个 $\uparrow$ | 性 |  | \% | 7 |  |
| Traffic Volume (vph) | 15 | 1390 | 1485 | 75 | 100 | 35 |  |
| Future Volume (vph) | 15 | 1390 | 1485 | 75 | 100 | 35 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Lane Width | 3.5 | 3.7 | 3.7 | 3.5 | 3.5 | 3.5 |  |
| Total Lost time (s) | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |
| Lane Util. Factor | 1.00 | 0.95 | 0.95 |  | 1.00 | 1.00 |  |
| Frpb, ped/bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 0.98 |  |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.99 |  | 1.00 | 0.85 |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1783 | 3614 | 3584 |  | 1785 | 1520 |  |
| Flt Permitted | 0.14 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (perm) | 267 | 3614 | 3584 |  | 1785 | 1520 |  |
| Peak-hour factor, PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Adj. Flow (vph) | 15 | 1390 | 1485 | 75 | 100 | 35 |  |
| RTOR Reduction (vph) | 0 | 0 | 1 | 0 | 0 | 27 |  |
| Lane Group Flow (vph) | 15 | 1390 | 1559 | 0 | 100 | 8 |  |
| Confl. Peds. (\#hr) | 5 |  |  | 5 |  | 5 |  |
| Heavy Vehicles (\%) | 0\% | 1\% | 1\% | 0\% | 0\% | 3\% |  |
| Turn Type | Perm | NA | NA |  | Perm | Perm |  |
| Protected Phases |  | 2 | 6 |  |  |  |  |
| Permitted Phases | 2 |  |  |  | 8 | 8 |  |
| Actuated Green, G (s) | 132.6 | 132.6 | 132.6 |  | 15.3 | 15.3 |  |
| Effective Green, g (s) | 132.6 | 132.6 | 132.6 |  | 15.3 | 15.3 |  |
| Actuated g/C Ratio | 0.83 | 0.83 | 0.83 |  | 0.10 | 0.10 |  |
| Clearance Time (s) | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 221 | 2995 | 2970 |  | 170 | 145 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | 0.38 | c0.43 |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.06 |  |  |  | c0.06 | 0.01 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.07 | 0.46 | 0.52 |  | 0.59 | 0.05 |  |
| Uniform Delay, d1 | 2.5 | 3.8 | 4.2 |  | 69.3 | 65.8 |  |
| Progression Factor | 0.97 | 0.99 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 0.4 | 0.4 | 0.7 |  | 5.1 | 0.2 |  |
| Delay (s) | 2.8 | 4.1 | 4.8 |  | 74.5 | 65.9 |  |
| Level of Service | A | A | A |  | E | E |  |
| Approach Delay (s) |  | 4.1 | 4.8 |  | 72.2 |  |  |
| Approach LOS |  | A | A |  | E |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 7.4 |  | HCM 2000 | evel of Service | A |
| HCM 2000 Volume to Capacity ratio |  |  | 0.53 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 160.0 |  | Sum of los | time (s) | 12.1 |
| Intersection Capacity Utilization |  |  | 66.6\% | Cu Level of Service |  |  | C |
| Analysis Period (min) |  |  | 15 |  |  |  |  |

[^36]| HCM Unsignalized Intersection Capacity Analysis 1：Queen Street North \＆Matlock Ave |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 7 |  | $\dagger$ | 7 |  | $\dagger$ |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |  |  |
| Lane Configurations | Y |  | 个t |  | \％ | 个 $\uparrow$ |  |  |
| Traffic Volume（veh／h） | 30 | 20 | 1015 | 40 | 15 | 605 |  |  |
| Future Volume（Veh／h） | 30 | 20 | 1015 | 40 | 15 | 605 |  |  |
| Sign Control | Stop |  | Free |  |  | Free |  |  |
| Grade | 0\％ |  | 0\％ |  |  | 0\％ |  |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |  |  |
| Hourly flow rate（vph） | 33 | 22 | 1103 | 43 | 16 | 658 |  |  |
| Pedestrians | 1 |  |  |  |  |  |  |  |
| Lane Width（m） | 3.5 |  |  |  |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  | TWLTL |  |  | None |  |  |
| Median storage veh） |  |  | 2 |  |  |  |  |  |
| Upstream signal（ m ） |  |  | 313 |  |  |  |  |  |
| pX，platoon unblocked | 0.89 | 0.89 |  |  | 0.89 |  |  |  |
| vC ，conficting volume | 1486 | 574 |  |  | 1147 |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1126 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 361 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1298 | 271 |  |  | 916 |  |  |  |
| tC，single（s） | 7.3 | 7.4 |  |  | 4.9 |  |  |  |
| tC， 2 stage（s） | 6.3 |  |  |  |  |  |  |  |
| tF（s） | 3.7 | 3.5 |  |  | 2.6 |  |  |  |
| p0 queue free \％ | 87 | 96 |  |  | 97 |  |  |  |
| cM capacity（veh／h） | 259 | 588 |  |  | 480 |  |  |  |
| Direction，Lane \＃ | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | SB 3 |  |  |
| Volume Total | 55 | 735 | 411 | 16 | 329 | 329 |  |  |
| Volume Left | 33 | 0 | 0 | 16 | 0 | 0 |  |  |
| Volume Right | 22 | 0 | 43 | 0 | 0 | 0 |  |  |
| cSH | 333 | 1700 | 1700 | 480 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.17 | 0.43 | 0.24 | 0.03 | 0.19 | 0.19 |  |  |
| Queue Length 95th（m） | 4.7 | 0.0 | 0.0 | 0.8 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 17.9 | 0.0 | 0.0 | 12.8 | 0.0 | 0.0 |  |  |
| Lane LOS | C |  |  | B |  |  |  |  |
| Approach Delay（s） | 17.9 | 0.0 |  | 0.3 |  |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.6 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39．3\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |


| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2：Queen Street North \＆ 40 Queen St N Driveway／53 Queen St Driveway |  |  |  |  |  |  |  |  |  |  | 06／28／2023 |  |
|  | $\stackrel{*}{ }$ |  |  | 1 |  |  |  | $\uparrow$ |  |  | $\dagger$ | $\downarrow$ |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | ${ }^{7}$ | 个t |  | \％ | 个t |  |
| Traffic Volume（veh／h） | 0 | ， | 0 | 0 | 0 | 0 | ， | 1055 | 0 | 0 | 635 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1055 | 0 | 0 | 635 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1199 | 0 | 0 | 722 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.86 | 0.86 |  | 0.86 | 0.86 | 0.86 |  |  |  | 0.86 |  |  |
| vC，conficting volume | 1322 | 1921 | 361 | 1560 | 1921 | 600 | 722 |  |  | 1199 |  |  |
| vC1，stage 1 conf vol | 722 | 722 |  | 1199 | 1199 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 600 | 1199 |  | 361 | 722 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1051 | 1747 | 361 | 1328 | 1747 | 213 | 722 |  |  | 909 |  |  |
| tC，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \％ | 100 | 100 | 100 | 100 | 100 | 100 | 100 |  |  | 100 |  |  |
| cM capacity（veh／h） | 352 | 254 | 641 | 242 | 254 | 688 | 889 |  |  | 652 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 0 | 0 | 799 | 400 | 0 | 481 | 241 |  |  |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 0 | 0 | 0 | － |  |  |  |  |
| cSH | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.00 | 0.00 | 0.47 | 0.24 | 0.00 | 0.28 | 0.14 |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 0.0 | 0.0 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | A | A |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 32．5\％ |  | Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^37]| HCM Unsignalized In 3：Queen Street North |  | ction ) Qué | $\begin{aligned} & \text { Japac } \\ & \text { n } 5 \text { an } \end{aligned}$ |  | sis way／P | opose |  |  |  |  |  | 2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 1 |  |  | 4 | $\dagger$ | 7 |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | \％ | 个个 |  | ＊ | 个 |  |
| Traffic Volume（veh／h） | 0 | 0 | 0 | 60 | 0 | 30 | 0 | 1025 | 30 | 15 | 620 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 0 | 60 | 0 | 30 | 0 | 1025 | 30 | 15 | 620 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Hourly flow rate（vph） | 0 | 0 | 0 | 69 | 0 | 34 | 0 | 1178 | 34 | 17 | 713 | 0 |
| Pedestrians |  | 3 |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  | 3.7 |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  | 1.2 |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  | 0 |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 186 |  |  |  |  |
| pX，platoon unblocked | 0.85 | 0.85 |  | 0.85 | 0.85 | 0.85 |  |  |  | 0.85 |  |  |
| VC, conflicting volume | 1373 | 1962 | 360 | 1586 | 1945 | 606 | 716 |  |  | 1212 |  |  |
| vC1，stage 1 conf vol | 750 | 750 |  | 1195 | 1195 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 623 | 1212 |  | 390 | 750 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1090 | 1782 | 360 | 1340 | 1762 | 190 | 716 |  |  | 901 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 100 | 72 | 100 | 95 | 100 |  |  | 97 |  |  |
| cM capacity（veh／h） | 325 | 239 | 641 | 246 | 251 | 704 | 892 |  |  | 650 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 0 | 103 | 0 | 785 | 427 | 17 | 475 | 238 |  |  |  |  |
| Volume Left | 0 | 69 | 0 | － | 0 | 17 | 0 | 0 |  |  |  |  |
| Volume Right | 0 | 34 | 0 | 0 | 34 | 0 | 0 | 0 |  |  |  |  |
| cSH | 1700 | 313 | 1700 | 1700 | 1700 | 650 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.00 | 0.33 | 0.00 | 0.46 | 0.25 | 0.03 | 0.28 | 0.14 |  |  |  |  |
| Queue Length 95th（m） | 0.0 | 11.2 | 0.0 | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 0.0 | 22.0 | 0.0 | 0.0 | 0.0 | 10.7 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | A | C |  |  |  | B |  |  |  |  |  |  |
| Approach Delay（s） | 0.0 | 22.0 | 0.0 |  |  | 0.2 |  |  |  |  |  |  |
| Approach LOS | A | c |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.2 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 41．1\％ |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

10y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total AM Peak Hour

BA Group | Synchro 11 Report |
| ---: |
| Page 3 |

HCM Unsignalized Intersection Capacity Analysis
4：Queen Street North \＆Petro Canada N Driveway

| Movement | EBL | EBR | NBL | NBT | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  |  | ${ }^{7}$ | 个 $\uparrow$ | 个 ${ }^{\text {a }}$ |  |
| Traffic Volume（veh／h） | 0 | 0 | 5 | 1055 | 670 | 10 |
| Future Volume（Veh／h） | 0 | 0 | 5 | 1055 | 670 | 10 |
| Sign Control | Stop |  |  | Free | Free |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 | 0.87 |
| Hourly flow rate（vph） | 0 | 0 | 6 | 1213 | 770 | 11 |
| Pedestrians | 3 |  |  | 1 |  |  |
| Lane Width（m） | 0.0 |  |  | 3.6 |  |  |
| Walking Speed（m／s） | 1.2 |  |  | 1.2 |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |


| Right turn flare（veh） | TWLTL TWLTL |
| :--- | :--- |
| Median type |  |

Median storage veh）$\quad 2$


[^38]| HCM Unsignalized Intersection Capacity Analysis 5：Queen Street North \＆Petro Canada S Driveway |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 |  | 4 | $\dagger$ | $\downarrow$ | $\stackrel{ }{ }$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | Y |  | \％ | ¢ $\uparrow$ | 个t |  |  |  |
| Traffic Volume（veh／h） | 0 | 5 | 0 | 1060 | 660 | 10 |  |  |
| Future Volume（Veh／h） | 0 | 5 | 0 | 1060 | 660 | 10 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 | 0.88 |  |  |
| Hourly flow rate（vph） | 0 | 6 | 0 | 1205 | 750 | 11 |  |  |
| Pedestrians | 3 |  |  | 2 |  |  |  |  |
| Lane Width（m） | 3.5 |  |  | 3.6 |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | TWLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ m ） |  |  |  | 127 |  |  |  |  |
| pX，platoon unblocked | 0.84 |  |  |  |  |  |  |  |
| VC, conflicting volume | 1361 | 386 | 764 |  |  |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 758 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 602 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1057 | 386 | 764 |  |  |  |  |  |
| tC ，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 100 | 99 | 100 |  |  |  |  |  |
| cM capacity（veh／h） | 389 | 616 | 856 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |
| Volume Total | 6 | 0 | 602 | 602 | 500 | 261 |  |  |
| Volume Left | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 6 | 0 | 0 | 0 | 0 | 11 |  |  |
| cSH | 616 | 1700 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.01 | 0.00 | 0.35 | 0.35 | 0.29 | 0.15 |  |  |
| Queue Length 95th（m） | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 10.9 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | B |  |  |  |  |  |  |  |
| Approach Delay（s） | 10.9 | 0.0 |  |  | 0.0 |  |  |  |
| Approach LOS | B |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.0 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39．9\％ |  | Level | Service | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |


| 10y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total AM Peak Hour | Synchro 11 Report |
| :--- | ---: |
| BA Group | Page 5 |

Timings
6：Queen Street South／Queen Street North \＆Britannia Rd West 06／28／2023

|  | $\rangle$ | $\rightarrow$ | 7 |  |  | 4 | 4 |  | $\dagger$ | $\stackrel{ }{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations | \％ | 个施 | \％ | 个个 | $\overline{7}$ | \％ | 中t | \％ | $\uparrow$ | 「 |
| Traffic Volume（vph） | 225 | 1615 | 80 | 640 | 330 | 95 | 505 | 155 | 355 | 155 |
| Future Volume（vph） | 225 | 1615 | 80 | 640 | 330 | 95 | 505 | 155 | 355 | 155 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | Perm | NA | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 | 1 | 6 |  |  | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 12.0 | 12.0 | 8.0 | 12.0 | 12.0 |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 38.9 | 38.9 | 11.0 | 38.9 | 38.9 |
| Total Split（s） | 13.0 | 83.0 | 11.0 | 81.0 | 81.0 | 53.0 | 53.0 | 13.0 | 66.0 | 66.0 |
| Total Split（\％） | 8．1\％ | 51．9\％ | 6．9\％ | 50．6\％ | 50．6\％ | 33．1\％ | 33．1\％ | 8．1\％ | 41．3\％ | 41．3\％ |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 4.0 | 4.0 | 3.0 | 4.0 | 4.0 |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 3.9 | 3.9 | 0.0 | 3.9 | 3.9 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 7.9 | 7.9 | 3.0 | 7.9 | 7.9 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lag | Lag | Lead |  |  |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |  |  |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |
| Act Efft Green（s） | 100.9 | 85.1 | 94.4 | 81.2 | 81.2 | 34.8 | 34.8 | 52.7 | 47.8 | 47.8 |
| Actuated g／C Ratio | 0.63 | 0.53 | 0.59 | 0.51 | 0.51 | 0.22 | 0.22 | 0.33 | 0.30 | 0.30 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.46 | 0.91 | 0.56 | 0.37 | 0.37 | 0.58 | 0.83 | 0.87 | 0.64 | 0.29 |
| Control Delay | 16.6 | 43.0 | 52.6 | 23.1 | 4.4 | 69.1 | 67.4 | 80.9 | 54.0 | 6.5 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 16.6 | 43.0 | 52.6 | 23.1 | 4.4 | 69.1 | 67.4 | 80.9 | 54.0 | 6.5 |
| LOS | B | D | D | C | A | E | E | F | D | A |
| Approach Delay |  | 39.9 |  | 19.5 |  |  | 67.7 |  | 49.2 |  |
| Approach LOS |  | D |  | B |  |  | E |  | D |  |

## Intersection Summary

Cycle Length： 160
Actuated Cycle Length： 160
Offset： $0(0 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of Green
Natural Cycle： 130
Control Type：Actuated－Coordinated

| Maximumion Sainnal Delay： 41.0 | Intersection LOS：D |
| :--- | :--- |
| Intersection |  |
| Intersection Capacity Utiization 108．4\％ | ICU Level of Service G |
| Analysis Period（min） 15 |  |

Analysis Period（min） 15


[^39]Queues

| 6: Queen Street | /Qu | S | + | th \& | ritan | a | West |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{ }{*}$ | $\rightarrow$ | 7 | 4 | 4 | 4 | 4 | * | $\dagger$ | $\pm$ |  |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |  |
| Lane Group Flow (vph) | 225 | 1715 | 80 | 640 | 330 | 95 | 630 | 155 | 355 | 155 |  |
| v/c Ratio | 0.46 | 0.91 | 0.56 | 0.37 | 0.37 | 0.58 | 0.83 | 0.87 | 0.64 | 0.29 |  |
| Control Delay | 16.6 | 43.0 | 52.6 | 23.1 | 4.4 | 69.1 | 67.4 | 80.9 | 54.0 | 6.5 |  |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total Delay | 16.6 | 43.0 | 52.6 | 23.1 | 4.4 | 69.1 | 67.4 | 80.9 | 54.0 | 6.5 |  |
| Queue Length 50th (m) | 30.3 | 265.8 | 12.0 | 62.7 | 6.8 | 28.7 | 104.1 | 38.4 | 103.6 | 0.0 |  |
| Queue Length 95th (m) | 50.1 | \#363.7 | 32.6 | 91.4 | 18.2 | 47.9 | 120.4 | \#59.6 | 131.1 | 16.6 |  |
| Internal Link Dist ( $m$ ) |  | 472.2 |  | 83.1 |  |  | 306.0 |  | 103.4 |  |  |
| Turn Bay Length ( m ) | 95.0 |  | 60.0 |  | 45.0 | 40.0 |  | 35.0 |  |  |  |
| Base Capacity (vph) | 485 | 1878 | 143 | 1731 | 885 | 215 | 982 | 179 | 670 | 612 |  |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Reduced v/c Ratio | 0.46 | 0.91 | 0.56 | 0.37 | 0.37 | 0.44 | 0.64 | 0.87 | 0.53 | 0.25 |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| \# 95th percentile volume exceeds capacity, queue may be longer. |  |  |  |  |  |  |  |  |  |  |  |
| Queue shown is maxi | after two | cycles. |  |  |  |  |  |  |  |  |  |

[^40]HCM Signalized Intersection Capacity Analysis


[^41]
## HCM Unsignalized Intersection Capacity Analysis

| 7：Arch Rd \＆Britannia Rd West |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ | $\geqslant$ | 1 | $\bullet$ | 4 | ／ |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个家 |  | \％ | 个4 | M |  |  |  |
| Traffic Volume（veh／h） | 1890 | 5 | 10 | 1045 | 5 | 10 |  |  |
| Future Volume（Veh／h） | 1890 | 5 | 10 | 1045 | 5 | 10 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate（vph） | 1890 | 5 | 10 | 1045 | 5 | 10 |  |  |
| Pedestrians |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type | None |  |  | WLTL |  |  |  |  |
| Median storage veh） |  |  |  | 2 |  |  |  |  |
| Upstream signal（ m ） | 107 |  |  | 182 |  |  |  |  |
| pX，platoon unblocked |  |  | 0.55 |  | 0.58 | 0.55 |  |  |
| vC, conficting volume |  |  | 1895 |  | 2435 | 948 |  |  |
| VC1，stage 1 conf vol |  |  |  |  | 1892 |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol |  |  |  |  | 542 |  |  |  |
| vCu ，unblocked vol |  |  | 985 |  | 1559 | 0 |  |  |
| tC，single（s） |  |  | 4.1 |  | 6.8 | 7.1 |  |  |
| tC， 2 stage（s） |  |  |  |  | 5.8 |  |  |  |
| tF（s） |  |  | 2.2 |  | 3.5 | 3.4 |  |  |
| po queue free \％ |  |  | 97 |  | 97 | 98 |  |  |
| cM capacity（veh／h） |  |  | 389 |  | 171 | 584 |  |  |
| Direction，Lane \＃ | EB 1 | EB 2 | WB 1 | WB 2 | WB 3 | NB 1 |  |  |
| Volume Total | 1260 | 635 | 10 | 522 | 522 | 15 |  |  |
| Volume Left | 0 | 0 | 10 | 0 | 0 | 5 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 10 |  |  |
| cSH | 1700 | 1700 | 389 | 1700 | 1700 | 324 |  |  |
| Volume to Capacity | 0.74 | 0.37 | 0.03 | 0.31 | 0.31 | 0.05 |  |  |
| Queue Length 95th（m） | 0.0 | 0.0 | 0.6 | 0.0 | 0.0 | 1.2 |  |  |
| Control Delay（s） | 0.0 | 0.0 | 14.5 | 0.0 | 0.0 | 16.6 |  |  |
| Lane LOS |  |  | B |  |  | C |  |  |
| Approach Delay（s） | 0.0 |  | 0.1 |  |  | 16.6 |  |  |
| Approach LOS |  |  |  |  |  | C |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 62．4\％ |  | CU Level | Service | B |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

HCM Unsignalized Intersection Capacity Analysis
8：Earl St \＆Britannia Rd West


[^42]Timings
9: Britannia Rd West \& Ellesboro Dr

Intersection Summany
Cycle Length: 160
Actuated Cycle Length: 160
Offiset: $0(0 \%)$, Referenced to phase 2:EBTL and 6 :WBT, Start of Green
Natural Cycle: 90

Splits and Phases: 9: Britannia Rd West \& Ellesboro Dr


10y Future Total AM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Total AM Peak Hour | Synchro 11 Report |
| :--- |
| BA Group | 11

Queues
9: Britannia Rd West \& Ellesboro Dr

| Lane Group | EBL | EBT | WBT | SBL | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group Flow (vph) | 30 | 1890 | 1095 | 60 | 30 |
| v/c Ratio | 0.07 | 0.61 | 0.37 | 0.40 | 0.20 |
| Control Delay | 1.2 | 2.0 | 2.9 | 77.8 | 23.8 |
| Queue Delay | 0.0 | 0.1 | 0.0 | 0.0 | 0.0 |
| Total Delay | 1.2 | 2.1 | 2.9 | 77.8 | 23.8 |
| Queue Length 50th (m) | 0.6 | 27.8 | 35.6 | 19.5 | 0.0 |
| Queue Length 95th (m) | m0.7 | 27.3 | 46.3 | 35.5 | 11.4 |
| Internal Link Dist ( $m$ ) |  | 46.6 | 115.6 | 80.1 |  |
| Turn Bay Length ( m ) | 45.0 |  |  |  | 15.0 |
| Base Capacity (vph) | 400 | 3120 | 2968 | 434 | 375 |
| Starvation Cap Reductn | 0 | 344 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.07 | 0.68 | 0.37 | 0.14 | 0.08 |
| Intersection Summary |  |  |  |  |  |

[^43]| HCM Signalized Intersection Capacity Analysis 9：Britannia Rd West \＆Ellesboro Dr |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | － | 4 | ＊ | 4 |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |  |  |
| Lane Configurations | \％ | 个4 | 性 |  | \％ | 「 |  |  |
| Traffic Volume（vph） | 30 | 1890 | 1025 | 70 | 60 | 30 |  |  |
| Future Volume（vph） | 30 | 1890 | 1025 | 70 | 60 | 30 |  |  |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |  |
| Lane Width | 3.5 | 3.7 | 3.7 | 3.5 | 3.5 | 3.5 |  |  |
| Total Lost time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Lane Util．Factor | 1.00 | 0.95 | 0.95 |  | 1.00 | 1.00 |  |  |
| Frpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 0.97 |  |  |
| Flpb，ped／bikes | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  |
| Frt | 1.00 | 1.00 | 0.99 |  | 1.00 | 0.85 |  |  |
| Flt Protected | 0.95 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Flow（prot） | 1729 | 3579 | 3404 |  | 1782 | 1447 |  |  |
| Fit Permitted | 0.25 | 1.00 | 1.00 |  | 0.95 | 1.00 |  |  |
| Satd．Fow（perm） | 458 | 3579 | 3404 |  | 1782 | 1447 |  |  |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Adj．Flow（vph） | 30 | 1890 | 1025 | 70 | 60 | 30 |  |  |
| RTOR Reduction（vph） | 0 | 0 | 1 | 0 | 0 | 28 |  |  |
| Lane Group Flow（vph） | 30 | 1890 | 1094 | 0 | 60 | 2 |  |  |
| Confl．Peds．（\＃／hr） | 4 |  |  | 4 | ， | 12 |  |  |
| Heavy Vehicles（\％） | 3\％ | 2\％ | 6\％ | 6\％ | 0\％ | 7\％ |  |  |
| Turn Type | Perm | NA | NA |  | Perm | Perm |  |  |
| Protected Phases |  | 2 | 6 |  |  |  |  |  |
| Permitted Phases | 2 |  |  |  | 8 | 8 |  |  |
| Actuated Green，G（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Effective Green，g（s） | 137.1 | 137.1 | 137.1 |  | 10.8 | 10.8 |  |  |
| Actuated g／C Ratio | 0.86 | 0.86 | 0.86 |  | 0.07 | 0.07 |  |  |
| Clearance Time（s） | 6.1 | 6.1 | 6.1 |  | 6.0 | 6.0 |  |  |
| Vehicle Extension（s） | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  |
| Lane Grp Cap（vph） | 392 | 3066 | 2916 |  | 120 | 97 |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | c0．53 | 0.32 |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.07 |  |  |  | c0．03 | 0.00 |  |  |
| v／c Ratio | 0.08 | 0.62 | 0.38 |  | 0.50 | 0.02 |  |  |
| Uniform Delay，d1 | 1.8 | 3.5 | 2.4 |  | 72.0 | 69.7 |  |  |
| Progression Factor | 0.42 | 0.42 | 1.00 |  | 1.00 | 1.00 |  |  |
| Incremental Delay，d2 | 0.2 | 0.4 | 0.4 |  | 3.3 | 0.1 |  |  |
| Delay（s） | 0.9 | 1.9 | 2.8 |  | 75.2 | 69.7 |  |  |
| Level of Service | A | A | A |  | E | E |  |  |
| Approach Delay（s） |  | 1.9 | 2.8 |  | 73.4 |  |  |  |
| Approach LOS |  | A | A |  | E |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 4.3 |  | HCM 2000 | evel of Service | A |  |
| HCM 2000 Volume to Capacity ratio |  |  | 0.61 |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | ime（s） | 12.1 |  |
| Intersection Capacity Utilization |  |  | 77．8\％ |  | CU Level | Service | D |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |

10y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total AM Peak Hour

BA Group | Synchro 11 Report |
| ---: |
| Page 13 |

HCM Unsignalized Intersection Capacity Analysis
1：Queen Street North \＆Matlock Ave
06／28／2023

[^44]| HCM Unsignalized In 2：Queen Street North |  | Que | apac |  | sis <br> vay／5 | Quee |  |  |  |  |  | ／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ | $\geqslant$ | 1 |  |  | 4 | $\uparrow$ | \％ |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \＄ |  |  | ¢ |  | \％ | 性 |  | \％ |  |  |
| Traffic Volume（veh／h） | 0 | 0 | 5 | 5 | ， | 0 | 5 | 645 | 0 | 5 | 1155 | 0 |
| Future Volume（Veh／h） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 645 | 0 | 5 | 1155 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate（vph） | 0 | 0 | 5 | 5 | 0 | 0 | 5 | 709 | 0 | 5 | 1269 | 0 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（m／s） |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | WLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | ， |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 213 |  |  |  |  |
| pX，platoon unblocked | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 |  |  |  | 0.95 |  |  |
| VC, conflicting volume | 1644 | 1998 | 634 | 1368 | 1998 | 354 | 1269 |  |  | 709 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1279 | 1279 |  | 719 | 719 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 364 | 719 |  | 650 | 1279 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1572 | 1945 | 634 | 1282 | 1945 | 215 | 1269 |  |  | 588 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tC}, 2$ stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 100 | 100 | 99 | 98 | 100 | 100 | 99 |  |  | 99 |  |  |
| cM capacity（veh／h） | 171 | 211 | 426 | 314 | 208 | 756 | 554 |  |  | 947 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 5 | 5 | 5 | 473 | 236 | 5 | 846 | 423 |  |  |  |  |
| Volume Left | 0 | 5 | 5 | 0 | 0 | 5 | 0 | 0 |  |  |  |  |
| Volume Right | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |
| cSH | 426 | 314 | 554 | 1700 | 1700 | 947 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.01 | 0.02 | 0.01 | 0.28 | 0.14 | 0.01 | 0.50 | 0.25 |  |  |  |  |
| Queue Length 95th（m） | 0.3 | 0.4 | 0.2 | 0.0 | 0.0 | 0.1 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 13.5 | 16.6 | 11.6 | 0.0 | 0.0 | 8.8 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | B | C | B |  |  | A |  |  |  |  |  |  |
| Approach Delay（s） | 13.5 | 16.6 | 0.1 |  |  | 0.0 |  |  |  |  |  |  |
| Approach LOS | B | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 42．7\％ |  | CU Level | Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

10y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total PM Peak Hour

BA Group | Synchro 11 Report |
| ---: |
| Page 2 |

| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ | $\rightarrow$ | $\geqslant$ | 7 |  | 4 | 4 | $\dagger$ |  |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | \＄ |  |  | ¢ |  | \％ | 个个 |  | \％ | 个 ${ }^{\text {a }}$ |  |
| Traffic Volume（veh／h） | 5 | ， | 5 | 60 | 0 | 35 | 0 | 610 | 80 | 40 | 1125 |  |
| Future Volume（Veh／h） | 5 | 0 | 5 | 60 | 0 | 35 | 0 | 610 | 80 | 40 | 1125 | 0 |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |  | 0\％ |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |
| Hourly flow rate（vph） | 5 | 0 | 5 | 66 | 0 | 38 | 0 | 670 | 88 | 44 | 1236 | 0 |
| Pedestrians |  | 2 |  |  |  |  |  |  |  |  |  |  |
| Lane Width（m） |  | 3.7 |  |  |  |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） |  | 1.2 |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  | 0 |  |  |  |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | TWLTL |  |  | TWLTL |  |
| Median storage veh） |  |  |  |  |  |  |  | 2 |  |  | 2 |  |
| Upstream signal（ m ） |  |  |  |  |  |  |  | 186 |  |  |  |  |
| pX ，platoon unblocked | 0.91 | 0.91 |  | 0.91 | 0.91 | 0.91 |  |  |  | 0.91 |  |  |
| vC, conficting volume | 1699 | 2084 | 620 | 1425 | 2040 | 379 | 1238 |  |  | 758 |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1326 | 1326 |  | 714 | 714 |  |  |  |  |  |  |  |
| vC2，stage 2 conf vol | 373 | 758 |  | 711 | 1326 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1570 | 1993 | 620 | 1269 | 1945 | 119 | 1238 |  |  | 536 |  |  |
| tC ，single（s） | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC， 2 stage（s） | 6.5 | 5.5 |  | 6.5 | 5.5 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \％ | 97 | 100 | 99 | 78 | 100 | 95 | 100 |  |  | 95 |  |  |
| cM capacity（veh／h） | 154 | 193 | 435 | 307 | 198 | 834 | 569 |  |  | 949 |  |  |
| Direction，Lane \＃ | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 |  |  |  |  |
| Volume Total | 10 | 104 | 0 | 447 | 311 | 44 | 824 | 412 |  |  |  |  |
| Volume Left | 5 | 66 | 0 | 0 | 0 | 44 | 0 | 0 |  |  |  |  |
| Volume Right | 5 | 38 | 0 | 0 | 88 | 0 | 0 | 0 |  |  |  |  |
| cSH | 227 | 399 | 1700 | 1700 | 1700 | 949 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.04 | 0.26 | 0.00 | 0.26 | 0.18 | 0.05 | 0.48 | 0.24 |  |  |  |  |
| Queue Length 95th（ $m$ ） | 1.1 | 8.2 | 0.0 | 0.0 | 0.0 | 1.2 | 0.0 | 0.0 |  |  |  |  |
| Control Delay（s） | 21.6 | 17.2 | 0.0 | 0.0 | 0.0 | 9.0 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | C | C |  |  |  | A |  |  |  |  |  |  |
| Approach Delay（s） | 21.6 | 17.2 | 0.0 |  |  | 0.3 |  |  |  |  |  |  |
| Approach LOS | C | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 1.1 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 47．4\％ |  | CU Level of | f Service |  |  | A |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |

[^45]| HCM Unsignalized Intersection Capacity Analysis <br> 4：Queen Street North \＆Petro Canada N Driveway |  |  |  |  |  |  |  | 06／28／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rangle$ |  | 4 | 4 |  | $\pm$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations |  |  | \％ | 个4 | 个t |  |  |  |
| Traffic Volume（veh／h） | 0 | 0 | 10 | 690 | 1180 | 10 |  |  |
| Future Volume（Veh／h） | 0 | 0 | 10 | 690 | 1180 | 10 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |  |  |
| Hourly flow rate（vph） | 0 | 0 | 11 | 758 | 1297 | 11 |  |  |
| Pedestrians | 2 |  |  |  |  |  |  |  |
| Lane Width（m） | 0.0 |  |  |  |  |  |  |  |
| Walking Speed（ $\mathrm{m} / \mathrm{s}$ ） | 1.2 |  |  |  |  |  |  |  |
| Percent Blockage | 0 |  |  |  |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | WLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ m ） |  |  |  | 159 |  |  |  |  |
| pX，platoon unblocked | 0.90 |  |  |  |  |  |  |  |
| vC ，conficting volume | 1706 | 656 | 1310 |  |  |  |  |  |
| vC1，stage 1 conf vol | 1304 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 401 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1568 | 656 | 1310 |  |  |  |  |  |
| tC，single（s） | 6.8 | 6.9 | 4.1 |  |  |  |  |  |
| $\mathrm{tC}, 2$ stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.3 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 100 | 100 | 98 |  |  |  |  |  |
| cM capacity（veh／h） | 213 | 413 | 535 |  |  |  |  |  |
| Direction，Lane\＃ | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 |  |  |  |
| Volume Total | 11 | 379 | 379 | 865 | 443 |  |  |  |
| Volume Left | 11 | 0 | 0 | ， | 0 |  |  |  |
| Volume Right | 0 | 0 | 0 | 0 | 11 |  |  |  |
| cSH | 535 | 1700 | 1700 | 1700 | 1700 |  |  |  |
| Volume to Capacity | 0.02 | 0.22 | 0.22 | 0.51 | 0.26 |  |  |  |
| Queue Length 95th（m） | 0.5 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| Control Delay（s） | 11.9 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |  |
| Lane LOS | B |  |  |  |  |  |  |  |
| Approach Delay（s） | 0.2 |  |  | 0.0 |  |  |  |  |
| Approach LOS |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 36．3\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |


| HCM Unsignalized Intersection Capacity Analysis |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\stackrel{*}{ }$ |  | 4 | $\dagger$ |  | $\checkmark$ |  |  |
| Movement | EBL | EBR | NBL | NBT | SBT | SBR |  |  |
| Lane Configurations | M |  | \％ | 个4 | 个 $\uparrow$ |  |  |  |
| Traffic Volume（veh／h） | 5 | 15 | 5 | 695 | 1180 | 0 |  |  |
| Future Volume（Veh／h） | 5 | 15 | 5 | 695 | 1180 | 0 |  |  |
| Sign Control | Stop |  |  | Free | Free |  |  |  |
| Grade | 0\％ |  |  | 0\％ | 0\％ |  |  |  |
| Peak Hour Factor | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 | 0.91 |  |  |
| Hourly flow rate（vph） | 5 | 16 | 5 | 764 | 1297 | 0 |  |  |
| Pedestrians | 2 |  |  | 4 |  |  |  |  |
| Lane Width（m） | 3.5 |  |  | 3.6 |  |  |  |  |
| Walking Speed（m／s） | 1.2 |  |  | 1.2 |  |  |  |  |
| Percent Blockage | 0 |  |  | 0 |  |  |  |  |
| Right turn flare（veh） |  |  |  |  |  |  |  |  |
| Median type |  |  |  | WLTL | WLTL |  |  |  |
| Median storage veh） |  |  |  | 2 | 2 |  |  |  |
| Upstream signal（ m ） |  |  |  | 127 |  |  |  |  |
| pX，platoon unblocked | 0.90 |  |  |  |  |  |  |  |
| VC, conficting volume | 1691 | 654 | 1299 |  |  |  |  |  |
| $\mathrm{vC1}$ ，stage 1 conf vol | 1299 |  |  |  |  |  |  |  |
| $\mathrm{vC2}$ ，stage 2 conf vol | 392 |  |  |  |  |  |  |  |
| vCu ，unblocked vol | 1539 | 654 | 1299 |  |  |  |  |  |
| tC，single（s） | 6.8 | 7.0 | 4.1 |  |  |  |  |  |
| tC， 2 stage（s） | 5.8 |  |  |  |  |  |  |  |
| tF（s） | 3.5 | 3.4 | 2.2 |  |  |  |  |  |
| p0 queue free \％ | 98 | 96 | 99 |  |  |  |  |  |
| cM capacity（veh／h） | 215 | 395 | 539 |  |  |  |  |  |
| Direction，Lane \＃ | EB 1 | NB 1 | NB 2 | NB3 | SB 1 | SB 2 |  |  |
| Volume Total | 21 | 5 | 382 | 382 | 865 | 432 |  |  |
| Volume Left | 5 | 5 | 0 | 0 | 0 | 0 |  |  |
| Volume Right | 16 | 0 | 0 | 0 | 0 | 0 |  |  |
| cSH | 329 | 539 | 1700 | 1700 | 1700 | 1700 |  |  |
| Volume to Capacity | 0.06 | 0.01 | 0.22 | 0.22 | 0.51 | 0.25 |  |  |
| Queue Length 95th（m） | 1.6 | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Control Delay（s） | 16.7 | 11.7 | 0.0 | 0.0 | 0.0 | 0.0 |  |  |
| Lane LOS | C | B |  |  |  |  |  |  |
| Approach Delay（s） | 16.7 | 0.1 |  |  | 0.0 |  |  |  |
| Approach LOS | C |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.2 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 43．9\％ | ICU Level of Service |  |  | A |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |

[^46]Timings
6：Queen Street South／Queen Street North \＆Britannia Rd West 06／28／2023

|  | $\stackrel{ }{ }$ |  | 7 |  |  |  | 4 |  |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | WBR | NBL | NBT | SBL | SBT | SBR |
| Lane Configurations | \％ | 个t | \％ | 个个 | $\overline{7}$ | \％ | 中 ${ }^{\text {a }}$ | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 155 | 970 | 140 | 1245 | 145 | 165 | 400 | 285 | 555 | 355 |
| Future Volume（vph） | 155 | 970 | 140 | 1245 | 145 | 165 | 400 | 285 | 555 | 355 |
| Turn Type | pm＋pt | NA | pm＋pt | NA | Perm | pm＋pt | NA | pm＋pt | NA | Perm |
| Protected Phases | 5 | 2 | 1 | 6 |  | 7 | 4 | 3 | 8 |  |
| Permitted Phases | 2 |  | 6 |  | 6 | 4 |  | 8 |  | 8 |
| Detector Phase | 5 | 2 | 1 | 6 | 6 | 7 | 4 | 3 | 8 | 8 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial（s） | 8.0 | 12.0 | 8.0 | 12.0 | 12.0 | 5.0 | 12.0 | 8.0 | 12.0 | 12.0 |
| Minimum Split（s） | 11.0 | 35.1 | 11.0 | 35.1 | 35.1 | 9.5 | 38.9 | 11.0 | 38.9 | 38.9 |
| Total Spit（s） | 13.0 | 74.0 | 11.0 | 72.0 | 72.0 | 14.0 | 58.0 | 17.0 | 61.0 | 61.0 |
| Total Split（\％） | 8．1\％ | 46．3\％ | 6．9\％ | 45．0\％ | 45．0\％ | 8．8\％ | 36．3\％ | 10．6\％ | 38．1\％ | 38．1\％ |
| Yellow Time（s） | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 | 3.0 | 4.0 | 3.0 | 4.0 | 4.0 |
| All－Red Time（s） | 0.0 | 3.1 | 0.0 | 3.1 | 3.1 | 0.0 | 3.9 | 0.0 | 3.9 | 3.9 |
| Lost Time Adjust（s） | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time（s） | 3.0 | 7.1 | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 | 3.0 | 7.9 | 7.9 |
| Lead／Lag | Lead | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lag | Lag |
| Lead－Lag Optimize？ | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Recall Mode | None | C－Max | None | C－Max | C－Max | None | None | None | None | None |
| Act Effct Green（s） | 84.5 | 69.1 | 79.2 | 66.2 | 66.2 | 62.9 | 47.0 | 68.9 | 50.0 | 50.0 |
| Actuated g／C Ratio | 0.53 | 0.43 | 0.50 | 0.41 | 0.41 | 0.39 | 0.29 | 0.43 | 0.31 | 0.31 |
| $\mathrm{v} / \mathrm{C}$ Ratio | 0.85 | 0.75 | 0.72 | 0.84 | 0.21 | 0.94 | 0.52 | 0.83 | 0.93 | 0.62 |
| Control Delay | 70.6 | 42.0 | 43.1 | 44.0 | 11.7 | 91.4 | 45.8 | 52.8 | 75.1 | 33.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 70.6 | 42.0 | 43.1 | 44.0 | 11.7 | 91.4 | 45.8 | 52.8 | 75.1 | 33.3 |
| LOS | E | D | D | D | B | F | D | D | E | C |
| Approach Delay |  | 45.4 |  | 40.8 |  |  | 56.5 |  | 57.4 |  |
| Approach LOS |  | D |  | D |  |  | E |  | E |  |

$\frac{\text { Intersection Summary }}{\text { Cycle Length：} 160}$
Cycle Length： 160
Actuated Cycle Len
Actuated Cycle Length： 160
Offset： $13(8 \%)$ ，Referenced to phase 2：EBTL and 6 ：WBTL，Start of Green

| Natural |  |
| :--- | :--- |
| Control Type：Actuated－Coordinated |  |
| Maximum v／c Ratio： 0.94 | Intersection LOS：D |
| Intersection Signal Delay： 48.6 | ICU Level of Service G |
| Intersection Capacity Utilization 100．5\％ |  |

Intersection Capacity Utilization 100．5\％
ICU Level of Service G
Analysis Period（min） 15


[^47]Queues
6：Queen Street South／Queen Street North \＆Britannia Rd West
06／28／2023

\＃95th percentile volume exceeds capacity，queue may be longer
Queue shown is maximum after two cycles．

HCM Signalized Intersection Capacity Analysis

| 6：Q | th／Q |  | eet | rth \＆ | Brita | a Rd | West |  |  |  |  | 8／2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 4 | $\rightarrow$ |  | 7 |  |  | 4 | $\uparrow$ | \％ |  | $\dagger$ | 4 |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 个t |  | ＊ | 个个 | F | \％ | $\uparrow \uparrow$ |  | \％ | $\uparrow$ | $\overline{7}$ |
| Traffic Volume（vph） | 155 | 970 | 165 | 140 | 1245 | 145 | 165 | 400 | 140 | 285 | 555 | 355 |
| Future Volume（vph） | 155 | 970 | 165 | 140 | 1245 | 145 | 165 | 400 | 140 | 285 | 555 | 355 |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 | 3.5 | 3.7 | 3.5 |
| Total Lost time（s） | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Lane Util．Factor | 1.00 | 0.95 |  | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 |  | 1.00 | 1.00 | 1.00 |
| Frpb，ped／bikes | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 | 1.00 | 0.99 |  | 1.00 | 1.00 | 0.97 |
| Flpb，ped／bikes | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 0.98 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.96 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） | 1750 | 3487 |  | 1767 | 3579 | 1530 | 1785 | 3430 |  | 1761 | 1921 | 1538 |
| Flt Permitted | 0.06 | 1.00 |  | 0.12 | 1.00 | 1.00 | 0.09 | 1.00 |  | 0.30 | 1.00 | 1.00 |
| Satd．Flow（perm） | 117 | 3487 |  | 219 | 3579 | 1530 | 162 | 3430 |  | 563 | 1921 | 1538 |
| Peak－hour factor，PHF | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj．Flow（vph） | 155 | 970 | 165 | 140 | 1245 | 145 | 165 | 400 | 140 | 285 | 555 | 355 |
| RTOR Reduction（vph） | 0 | 9 | 0 | 0 | 0 | 43 | 0 | 23 | 0 | 0 | 0 | 91 |
| Lane Group Flow（vph） | 155 | 1126 | 0 | 140 | 1245 | 102 | 165 | 517 | 0 | 285 | 555 | 264 |
| Confl．Peds．（\＃hr） | 12 |  | 9 | 9 |  | 12 | 10 |  | 24 | 24 |  | 10 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 0\％ | 1\％ | 2\％ | 1\％ | 0\％ | 1\％ | 1\％ | 1\％ | 0\％ | 1\％ |
| Turn Type | pm＋pt | NA |  | pm＋pt | NA | Perm | pm＋pt | NA |  | pm＋pt | NA | Perm |
| Protected Phases | 5 | ， |  | 1 | ， |  | 7 | 4 |  | 3 | ． |  |
| Permitted Phases | 2 |  |  | － |  | 6 | 4 |  |  | 8 |  | 8 |
| Actuated Green，G（s） | 80.9 | 69.1 |  | 75.1 | 66.2 | 66.2 | 58.0 | 47.0 |  | 64.0 | 50.0 | 50.0 |
| Effective Green， g （s） | 80.9 | 69.1 |  | 75.1 | 66.2 | 66.2 | 58.0 | 47.0 |  | 64.0 | 50.0 | 50.0 |
| Actuated g／C Ratio | 0.51 | 0.43 |  | 0.47 | 0.41 | 0.41 | 0.36 | 0.29 |  | 0.40 | 0.31 | 0.31 |
| Clearance Time（s） | 3.0 | 7.1 |  | 3.0 | 7.1 | 7.1 | 3.0 | 7.9 |  | 3.0 | 7.9 | 7.9 |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） | 179 | 1505 |  | 188 | 1480 | 633 | 170 | 1007 |  | 330 | 600 | 480 |
| v／s Ratio Prot | c0．06 | 0.32 |  | 0.04 | 0.35 |  | c0．07 | 0.15 |  | c0．08 | c0． 29 |  |
| v／s Ratio Perm | c0．37 |  |  | 0.31 |  | 0.07 | 0.29 |  |  | 0.27 |  | 0.17 |
| v／c Ratio | 0.87 | 0.75 |  | 0.74 | 0.84 | 0.16 | 0.97 | 0.51 |  | 0.86 | 0.93 | 0.55 |
| Uniform Delay，d1 | 42.4 | 38.2 |  | 30.0 | 42.2 | 29.5 | 42.1 | 47.0 |  | 39.8 | 53.2 | 45.7 |
| Progression Factor | 1.00 | 1.00 |  | 1.11 | 0.90 | 0.74 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 | 32.7 | 3.5 |  | 12.9 | 5.2 | 0.5 | 60.1 | 0.4 |  | 20.2 | 20.2 | 1.4 |
| Delay（s） | 75.1 | 41.6 |  | 46.2 | 43.2 | 22.2 | 102.2 | 47.4 |  | 60.0 | 73.4 | 47.0 |
| Level of Service | E | D |  | D | D | C | F | D |  | E | E | D |
| Approach Delay（s） |  | 45.6 |  |  | 41.5 |  |  | 60.3 |  |  | 62.4 |  |
| Approach LOS |  | D |  |  | D |  |  | E |  |  | ， |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2000 Control Delay |  |  | 50.7 |  | HCM 2000 | Level of S | Service |  | D |  |  |  |
| HCM 2000 Volume to Capacity | ratio |  | 0.92 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length（s） |  |  | 160.0 |  | Sum of los | time（s） |  |  | 21.0 |  |  |  |
| Intersection Capacity Utilizatio |  |  | 100．5\％ |  | CU Level | f Service |  |  | G |  |  |  |
| Analysis Period（min） |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

10y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total PM Peak Hour
BA Group

HCM Unsignalized Intersection Capacity Analysis
7：Arch Rd \＆Britannia Rd West


| Direction，Lane \＃ | EB 1 | EB 2 | WB 1 | WB2 | WB 3 | NB 1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volume Total | 923 | 472 | 5 | 765 | 765 | 10 |  |
| Volume Left | 0 | 0 | 5 | 0 | 0 | 0 |  |
| Volume Right | 0 | 10 | 0 | 0 | 0 | 10 |  |
| cSH | 1700 | 1700 | 605 | 1700 | 1700 | 799 |  |
| Volume to Capacity | 0.54 | 0.28 | 0.01 | 0.45 | 0.45 | 0.01 |  |
| Queue Length 95th（ m ） | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.3 |  |
| Control Delay（s） | 0.0 | 0.0 | 11.0 | 0.0 | 0.0 | 9.6 |  |
| Lane LOS |  |  | B |  |  | A |  |
| Approach Delay（s） | 0.0 |  | 0.0 |  |  | 9.6 |  |
| Approach LOS |  |  |  |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |
| Intersection Capacity Utilization |  |  | 52．3\％ | ICU Level of Service |  |  | A |
| Analysis Period（min） |  |  | 15 |  |  |  |  |

[^48]HCM Unsignalized Intersection Capacity Analysis

| 8: Earl St \& Britannia Rd West |  |  |  |  |  |  |  | 06/28/2023 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\rightarrow$ |  | 1 | $\downarrow$ | 4 | \% |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |  |
| Lane Configurations | 个t |  | \% | 个4 | M |  |  |  |
| Traffic Volume (veh/h) | 1390 | 5 | 5 | 1535 | 0 | 20 |  |  |
| Future Volume (Veh/h) | 1390 | 5 | 5 | 1535 | 0 | 20 |  |  |
| Sign Control | Free |  |  | Free | Stop |  |  |  |
| Grade | 0\% |  |  | 0\% | 0\% |  |  |  |
| Peak Hour Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |  |
| Hourly flow rate (vph) | 1390 | 5 | 5 | 1535 | 0 | 20 |  |  |
| Pedestrians |  |  |  |  | 5 |  |  |  |
| Lane Width (m) |  |  |  |  | 3.5 |  |  |  |
| Walking Speed (m/s) |  |  |  |  | 1.2 |  |  |  |
| Percent Blockage |  |  |  |  | 0 |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |
| Median type T | TWLTL |  |  | TWLTL |  |  |  |  |
| Median storage veh) | 2 |  |  | 2 |  |  |  |  |
| Upstream signal ( m ) | 219 |  |  | 71 |  |  |  |  |
| pX, platoon unblocked |  |  | 0.74 |  | 0.81 | 0.74 |  |  |
| vC, conficting volume |  |  | 1400 |  | 2175 | 702 |  |  |
| vC1, stage 1 conf vol |  |  |  |  | 1398 |  |  |  |
| $\mathrm{vC2}$, stage 2 conf vol |  |  |  |  | 778 |  |  |  |
| vCu, unblocked vol |  |  | 836 |  | 1202 | 0 |  |  |
| tC, single (s) |  |  | 4.1 |  | 6.8 | 6.9 |  |  |
| tC, 2 stage (s) |  |  |  |  | 5.8 |  |  |  |
| tF (s) |  |  | 2.2 |  | 3.5 | 3.3 |  |  |
| p0 queue free \% |  |  | 99 |  | 100 | 98 |  |  |
| cM capacity (veh/h) |  |  | 594 |  | 270 | 803 |  |  |
| Direction, Lane \# | EB 1 | EB2 | WB 1 | WB2 | WB3 | NB 1 |  |  |
| Volume Total | 927 | 468 | 5 | 768 | 768 | 20 |  |  |
| Volume Left | 0 | 0 | 5 | 0 | 0 | 0 |  |  |
| Volume Right | 0 | 5 | 0 | 0 | 0 | 20 |  |  |
| cSH | 1700 | 1700 | 594 | 1700 | 1700 | 803 |  |  |
| Volume to Capacity | 0.55 | 0.28 | 0.01 | 0.45 | 0.45 | 0.02 |  |  |
| Queue Length 95th (m) | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | 0.6 |  |  |
| Control Delay (s) | 0.0 | 0.0 | 11.1 | 0.0 | 0.0 | 9.6 |  |  |
| Lane LOS |  |  | B |  |  | A |  |  |
| Approach Delay (s) | 0.0 |  | 0.0 |  |  | 9.6 |  |  |
| Approach LOS |  |  |  |  |  | A |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 0.1 |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 52.4\% |  | CU Level | Service | A |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |

Analysis Period (min)

| 10y Future Total PM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Total PM Peak Hour | Synchro 11 Report |
| :--- | ---: |
| BA Group | Page 10 |

Timings
9: Britannia Rd West \& Ellesboro Dr 06/28/2023


Intersection Summar
Cycle Length: 160
Actuated Cycle Length: 160
Offset: $0(0 \%)$, Referenced to phase 2:EBTL and $6: W B T$, Start of Green
atural Cycle: 80
Contro Type: Actuated-Coordinated
Maximum Vigna. 0.58

| Intersection Signal Delay: 7.5 | Intersection LOS: A |
| :--- | :--- |
| Intersection Capacity Utilization $67.1 \%$ | ICU Level of Service C |

Analysis Period (min) 15
Splits and Phases: 9: Britannia Rd West \& Ellesboro Dr


10y Future Total PM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Total PM Peak Hour BA Group


HCM Signalized Intersection Capacity Analysis
9: Britannia Rd West \& Elles


[^49]Appendix J:
Signal Warrant - Justification 7 (OTM Book 12)

## OTM BOOK 12, JUSTIFICATION 7 - SUMMARY

EXISTING CONDITIONS

| Justification | Description | Minimum Requirement 2 or more lanes |  | Compliance |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Sectional |  | Entire \% |
|  |  | Free Flow | Restr. Flow | Numerical | \% |  |
| 1. Minimum Vehicular Volume | A. Vehicle volume, all approaches (average hour) | 900 | 1350 | 837.5 | 62\% | 12\% |
|  | B. Vehicle volume, along minor streets (average hour) | 180 | 255 | 30 | 12\% |  |
| 2. Delay to cross traffic | A. Vehicle volume, major street (average hour) | 900 | 1350 | 807.5 | 60\% | 12\% |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 180 | 255 | 30.5 | 12\% |  |

*Note: Thresholds increased by 50\% due to "T intersection".

## 2031 FUTURE BACKGROUND CONDITIONS

| Justification | Description | Minimum Requirement 2 or more lanes |  | Compliance |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Sectional |  | Entire \% |
|  |  | Free Flow | Restr. Flow | Numerical | \% |  |
| 1. Minimum Vehicular Volume | A. Vehicle volume, all approaches (average hour) | 900 | 1350 | 870 | 64\% | 12\% |
|  | B. Vehicle volume, along minor streets (average hour) | 180 | 255 | 30 | 12\% |  |
| 2. Delay to cross traffic | A. Vehicle volume, major street (average hour) | 900 | 1350 | 840 | 62\% | 12\% |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 180 | 255 | 30.5 | 12\% |  |

*Note: Thresholds increased by 50\% due to "T intersection".

## 2031 FUTURE TOTAL CONDITIONS

| Justification | Description | Minimum Requirement 2 or more lanes |  | Compliance |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Sectional |  | Entire \% |
|  |  | Free Flow | Restr. Flow | Numerical | \% |  |
| 1. Minimum Vehicular Volume | A. Vehicle volume, all approaches (average hour) | 900 | 1350 | 890 | 66\% | 12\% |
|  | B. Vehicle volume, along minor streets (average hour) | 180 | 255 | 30 | 12\% |  |
| 2. Delay to cross traffic | A. Vehicle volume, major street (average hour) | 900 | 1350 | 860 | 64\% | 12\% |
|  | B. Combined vehicle and pedestrian volume crossing artery from minor streets (average hour) | 180 | 255 | 30.5 | 12\% |  |

[^50]
[^0]:    Existing AM 21－51 Queen Street North 10：40 am 09／24／2021 Existing AM Peak Hour
    BA Group
    BA Group

[^1]:    Existing AM 21-51 Queen Street North 10:40 am 09/24/2021 Existing AM Peak Hour
    BA Group
    Synchro 11 Report
    Page 10

[^2]:    Existing PM 21-51 Queen Street North 10:40 am 09/24/2021 Existing PM Peak Hour
    BA Group

[^3]:    5y Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Background AM
    BA Group

[^4]:    5y Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Background AM
    BA Group
    BA Group

[^5]:    5y Future Background AM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Background AM
    BA Group
    Synchro 11 Report

[^6]:    5y Future Background AM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Background AM
    Synchro 11 Report

[^7]:    5y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Background PM

[^8]:    5y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Background PM
    BA Group
    BA Group
    Synchro 11 Report

[^9]:    5y Future Background PM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Background PM

[^10]:    5y Future Background PM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Background PM
    BA Group

[^11]:    5y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total AM Peak Hour
    BA Group
    BA Group

[^12]:    BA Group

[^13]:    5y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total AM Peak Hour
    BA Group

[^14]:    5y Future Total AM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Total AM Peak Hour
    BA Group

[^15]:    5y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total AM Peak Hour
    BA Group

[^16]:    5y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total PM Peak Hour
    BA Group

[^17]:    5y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total PM Peak Hour
    BA Group

[^18]:    5y Future Total PM 21-51 Queen Street North 10:40 am 09/24/2021 5y Future Total PM Peak Hour
    BA Group

[^19]:    5y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total PM Peak Hour BA Group

[^20]:    5y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 5y Future Total PM Peak Hour
    BA Group
    Synchro 11 Report

[^21]:    10y Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background AM
    Synchro 11 Report

[^22]:    10y Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background AM
    Synchro 11 Report
    Page 4

[^23]:    $10 y$ Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background AM
    BA Group
    Synchro 11 Report

[^24]:    10y Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background AM

[^25]:    10y Future Background AM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Background AM
    Synchro 11 Report
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[^26]:    BA Frour Background AM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Background AM
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[^27]:    10y Future Background AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background AM
    Synchro 11 Report

[^28]:    BA Future Background AM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Background AM
    BA
    Synchro 11 Report

[^29]:    10y Future Background AM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Background AM
    Synchro 11 Report

[^30]:    10y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background PM
    Synchro 11 Report

[^31]:    10y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background PM
    Synchro 11 Report

[^32]:    10y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background PM
    Synchro 11 Report

[^33]:    10y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background PM
    Synchro 11 Report
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[^34]:    $10 y$ Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background PM
    BA Group
    Synchro 11 Report
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[^35]:    10y Future Background PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Background PM
    Synchro 11 Report

[^36]:    10y Future Background PM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Background PM
    Synchro 11 Report
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[^37]:    10y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total AM Peak Hour
    BA Group

[^38]:    10y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total AM Peak Hour
    BA Group
    Synchro 11 Report

[^39]:    10y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total AM Peak Hour BA Group

[^40]:    10y Future Total AM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Total AM Peak Hour
    BA Group

[^41]:    10y Future Total AM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Total AM Peak Hour
    BA Group

[^42]:    10y Future Total AM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total AM Peak Hour
    BA Group
    Synchro 11 Report

[^43]:    10y Future Total AM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Total AM Peak Hour
    BA Group
    Synchro 11 Report

[^44]:    10y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total PM Peak Hour
    BA Group

[^45]:    10y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total PM Peak Hour
    BA Group
    Synchro 11 Report

[^46]:    10y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total PM Peak Hour
    BA Group
    Synchro 11 Report

[^47]:    10y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total PM Peak Hour
    BA Group
    BA Group

[^48]:    10y Future Total PM 21－51 Queen Street North 10：40 am 09／24／2021 10y Future Total PM Peak Hour
    BA Group
    BA Group
    Synchro 11 Report

[^49]:    10y Future Total PM 21-51 Queen Street North 10:40 am 09/24/2021 10y Future Total PM Peak Hour
    BA Group

[^50]:    *Note: Thresholds increased by 50\% due to "T intersection".

