

ENGINEERING



LABORATORY



GEOTECHNICAL INVESTIGATION



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1. INTRODUCTION

Fisher Engineering Ltd (Fisher) was commissioned by the Dymon Group of Companies to carry out a Geotechnical Investigation at the property municipally addressed as 3855 Dundas Street East, Mississauga, Ontario, hereinafter referred to as the 'Site'.

The purpose of the geotechnical investigation is to provide a report detailing subsurface soil and groundwater conditions and to outline geotechnical parameters and recommendations for the design of the proposed structures.

Discussion of the findings and results of the geotechnical investigation is in accordance with the general terms of reference. This report was prepared specifically and solely for the purpose of assessing geotechnical conditions as they relate to the development of the site with respect to the proposed structures as detailed to Fisher at the time of the investigation.

The report was updated to include the addition of two buildings to the site plan along with associated infrastructure.

2. SITE AND PROJECT DESCRIPTION

Site Settings

The Site is located at the north side of Dundas Street East, approximately 350m west of Highway 403, in a mix use area, and is bounded by Ninth Line to the west, baseball diamonds to the north, undeveloped land to the east, beyond which is HWY403 and Dundas Street East to the south. The property has an approximate area of 8,053m² and is rectangular in shape.

At the time of the investigation, the Site was mainly covered with grass/weeds but appeared to have been graded in the recent past. Access to the property is via an unpaved entrance off Dundas Street East.

Topography

Site grades were generally flat sloping towards drainage ditches. An average ground surface elevation of 171.15m asl was used for this report based on elevations at BH/MW locations.

Proposed Development

It was understood that the proposed development will consist of the construction of three buildings with up to 5-storeys. The buildings will have no underground or basement levels and will cover the western



portion of the Site, adjacent to Ninth Line, and the southeastern quadrant of the property. Finished Floor Elevation (FFE) are 171.40m, 171.55m and 171.55m asl for Buildings 1, 2 and 3 respectively according to the Site Servicing Plan by Crozier Consulting Engineers, dated November 20, 2020 and the updated site drawings. Building areas of 3,471m², 1,248m² and 1,248m² are shown on the architectural plans, prepared by Nicholas Caragianis Architect Inc, dated August 26, 2021, which were provided to Fisher for the updated report.

3. FIELD AND LABORATARY WORK

Subsurface exploration for the initial Geotechnical Investigation was carried out on October 26, 2018 and consisted of the drilling of five (5) boreholes (BH1 to BH5) to depths of 6.55m to 7.80m below prevailing grade. Two (2) of the boreholes were instrumented as monitoring wells (MW2 and MW4). Four (4) boreholes, BH101 to BH104, were drilled to depths of 5.03m bgs on August 19, 2020 for a preliminary hydrogeological investigation. The four (4) boreholes were instrumented as monitoring wells (MW101 to MW104). Seven (7) additional boreholes were drilled on September 13 and 14, 2021 to depths of 5.03m bgs based on the updated site plans which included two additional buildings and associated infrastructure. The seven (7) boreholes were instrumented as monitoring wells (MW201 to MW207). Six additional shallow wells (TH1 to TH6) and four test pits were excavated for infiltration tests. A clean silica sand pack was placed around the well screens and isolated with bentonite to depths below existing grade as shown in the borehole details in Appendix B.

Truck/track mounted drill rigs equipped with solid stem augers, supplied by Terra Firma Services, were used for all drilling work. Soil samples were taken at regular intervals using a split—spoon sampler advanced by means of the Standard Penetration Test (SPT) and was conducted in general accordance with ASTM specification D1586.

All recovered soil samples were placed in clear, sealed plastic bags in the field and were transported to Fisher laboratory for further examination, characterization and laboratory analyses.

Laboratory Analyses

Five (5) representative soil samples, from BH101 were selected and submitted to Fisher Environmental laboratory for grain size distribution and moisture content analyses. Two (2) soil samples from BH102 and BH103 were submitted to ALS Environmental laboratory for grain size and hydrometer analyses. Six (6) soil samples from the shallow boreholes (TH1 to TH6) were submitted for grain size and moisture content



analyses and three (3) samples for hydrometer testing. The laboratory results, which are presented in Appendix C, are consistent with the field descriptions for subsurface soils discussed in Section 4.0.

The soil samples recovered during the investigation will be stored in the Fisher Environmental laboratory for a period of 30 days after submitting this report and will be discarded thereafter unless otherwise instructed by the client.

Site Survey

Elevations at borehole/monitoring well locations were interpolated from a survey plan prepared by Speight, Van Nostrand & Gibson Limited dated September 10, 2018 which was provided to Fisher during the investigation.

4. SUBSOIL CONDITIONS

Surface and subsurface conditions encountered at borehole locations are shown in Appendix B - Log of Boreholes, and are summarized as follows:

• Fill/Disturbed Soil — A layer of fill/disturbed soil was encountered in all boreholes at ground surface and extended to depths of 0.30 to 3.00m below prevailing grade. The fill materials generally consisted of reddish brown to grey, silt/clayey silt, with trace of gravel/shale fragments, asphalt and pieces of bricks. Brown to grey silty clay with sand seams followed by black organic silty clay fill was reported in BH2 below the earth fill layer. The encountered layer of fill, which appears to be due to recent earth work, was moist to dry and was in a loose to compact state and was generally deeper in the northern section of the property covered by BH2, BH201 and BH202. A deeper layer of fill/disturbed soil was also encountered in the southeast section covered by BH207.

Depth and elevation of the fill encountered in all boreholes are presented in Table 1.

• CLAYEY SILT TILL — Reddish brown to greyish brown, moist to dry clayey silt till with trace gravel and pieces of shale were encountered below the fill and extended to termination depth in most boreholes. The encountered clayey silt till was overlain by a dark brown to grey clayey silt layer in BH102.



• Suspected Shale – Reddish brown, dry, hard shale/weathered shale was encountered at 3.2m bgs in BH204. SPT values of over 100 were observed in the shale. Refusal to power auguring occurred at approximately 4.72m bgs in the shale material.

Table 1: Fill depths and Elevations

Borehole No.	BH201	BH202	BH203	BH204	BH205	ВН206	BH207	BH101	BH102	BH103	BH104	BH2	вн4
Surface Elevation (m asl)	171.50	171.09	170.98	170.41	171.33	171.42	170.89	171.40	171.22	171.25	171.35	171.09	170.98
Depth of Borehole (m bgs)	5.03	5.03	5.03	4.72	5.03	5.03	4.99	5.03	5.03	5.03	5.03	6.71	6.55
Elevation at Bottom of Borehole (m asl)	166.47	166.06	165.95	165.69	166.30	166.39	165.90	166.37	166.19	166.22	166.32	164.38	164.43
Depth of Fill (m bgs)	3.00	1.98	0.23	1.07	1.07	1.37	2.44	0.76	1.22	0.3	0.61	1.85	0.46
Elevation at Bottom of Fill (m asl)	168.50	169.11	170.75	169.34	170.26	170.05	168.45	170.64	170.00	170.95	170.74	169.24	170.52

5. GROUNDWATER CONDITIONS

The boreholes were observed to be generally dry on completion of drilling. Small quantity of water was observed in the open borehole at the bottom of BH202. Static groundwater levels were measured between 0.49m and 5.10m below existing grade (elevations of 165.99m to 169.92m asl) but were generally at depths greater than 1.2m bgs. Higher groundwater levels were observed in MW204 located towards the eastern boundary of the property. Groundwater levels observed during late September and early October 2021 may be taken as representative of seasonal highwater levels at the site.

Measured groundwater depths and elevations are summarized in Table 2.



Table 2: Groundwater Depths and Elevations

	Elev. at	Depth of Well/BH				02-Nov-18 27-Aug-20		04-Sep-20		17-Sep-21		29-Sep-21		13-Oct-21			
Well No.	Ground (m)	m bgs	m asl	GW level, m bgs	GW Ele, m asl	GW level, m bgs	GW Ele, m asl	GW level, m bgs	GW Ele, m asl	GW level, m bgs	GW Ele, m asl	GW level, m bgs	GW Ele, m asl	GW level, m bgs	GW Ele, m asl	GW level, m bgs	GW Ele, m asl
MW201	171.50	4.57	166.93	Dry	-	n/a	-	n/a	-	n/a	-	2.89	168.61	2.81	168.69	2.59	168.91
MW202	171.09	4.57	166.52	4.55	166.54	n/a	-	n/a	-	n/a	-	1.43	169.66	1.33	169.76	1.43	169.66
MW203	170.98	4.57	166.41	Dry	-	n/a	-	n/a	-	n/a	-	1.62	169.36	1.53	169.45	1.55	169.43
MW204	170.41	4.57	165.84	Dry	-	n/a	-	n/a	-	n/a	-	1.45	168.96	0.71	169.70	0.49	169.92
MW205	171.33	4.57	166.76	Dry	-	n/a	-	n/a	-	n/a	-	3.94	167.39	3.91	167.42	3.40	167.93
MW206	171.42	4.57	166.85	Dry	-	n/a	-	n/a	-	n/a	-	4.11	167.31	4.03	167.39	3.64	167.78
MW207	170.89	4.57	166.32	Dry	-	n/a	-	n/a	-	n/a	-	3.72	167.17	3.67	167.22	2.83	168.06
MW101	171.40	4.57	166.83	Dry	-	n/a	-	Dry	-	Dry	-	1.83	169.57	1.71	169.69	1.72	169.68
MW102	171.22	4.57	166.65	Dry	-	n/a	-	Dry	-	3.77	167.45	1.46	169.76	1.28	169.94	1.41	169.81
MW103	171.25	4.57	166.68	Dry	-	n/a	-	Dry	-	Dry	-	4.12	167.13	4.10	167.15	3.96	167.29
MW104	171.35	4.57	166.78	Dry	-	n/a	-	4.32	167.03	3.89	167.47	3.38	167.97	3.39	167.96	2.95	168.40
MW2	171.09	6.10	164.99	Dry	-	5.10	165.99	4.12	166.97	3.04	168.05	1.64	169.45	1.62	169.47	1.51	169.58
MW4	170.98	6.10	164.88	Dry	-	1.67	169.31	2.09	168.89	1.40	169.58	1.56	169.42	1.37	169.61	1.26	169.72



6. FOUNDATION CONSIDERATIONS

Based on the updated Site Plan, by Nicholas Caragianis Architect, dated August 26, 2021, the proposed development will consist of: 1x 5-storey and 2 x 2 storey commercial buildings with no underground levels located at the western and southeastern portion of the site; Wilkinson heavy precast fire tank located at the northwest section and onsite sewage system tank located at the north central section along with leaching bed and infiltration facilities and associated infrastructure. FFE are 171.40m, 171.55m and 171.55m asl for Buildings 1, 2 and 3 respectively.

Subsurface soil investigations revealed that native soils at the site are dominated generally by stiff to hard clayey silt till from depths of 0.30 to 3.0m bgs to the maximum investigation depth of 7.80m. Suspected weathered shale was encountered in BH204 at depths of 3.2m bgs (elevation of 167.21m asl). The boreholes were generally dry on completion with static groundwater levels recorded in the installed wells at 0.49m to 5.10m bgs.

The following sections provide general geotechnical recommendations for design and construction of the proposed structures.

6.1 Spread/Strip Footing Found on Native Soils

The proposed structures, with no underground levels, may be supported on conventional spread/strip footings founded on the native undisturbed very stiff clayey silt till.

For footings placed over undisturbed native soils at/below the approximate minimum depths/elevations factored geotechnical resistance at ULS & geotechnical reaction at SLS are presented in in Table 3.

Footings designed to specified bearing pressure values in Table 3 are expected to settle less than 25mm total and 19mm differential.



Table 3: Foundation Design for Conventional Footings

Proposed Building/Borehole		Existing Grade/	• •	Footing levation	Recommended Soil Bearing Pressure			
		Elevation, m	Depth, m	Elev., m	SLS (kPa)	ULS (kPa)		
	BH101	171.40	2.5	168.90	300	420		
	BH102	171.22	3.0	168.22	300	420		
Building	BH103	171.25	2.4	168.85	300	420		
1	BH104	171.35	2.4	168.95	300	420		
	BH2	171.09	2.7	168.39	300	420		
	BH4	170.98	2.4	168.58	300	420		
Building	BH203	170.98	3.1	167.88	300	420		
2	BH204	170.41	2.5	167.91	300	420		
Building	BH206	171.42	3.1	168.32	300	420		
3	BH207	170.89	3.1	167.79	300	420		
Fire Tank	BH201	171.50	3.1	168.40	250	350		
Sewer Tank	BH202	171.09	2.4	168.69	250	350		

6.2 General Comments about Footing Construction

- Adjacent footings founded at different elevations should be stepped at 10 horizontals to 7 verticals.
- For frost protection requirements, all exterior footings must have a minimum soil cover of 1.22m.
- As the designed founding strata are relatively deep, consideration may be given to using trench footings for the building construction.
- The recommended bearing resistance and foundation elevations noted above were calculated from limited borehole information and are intended for design purposes only. More specific information with respect to soil conditions between and beyond the boreholes will be available when the proposed construction is underway. Therefore, the encountered soil/foundation conditions must be verified in the field, and all footings must be inspected and approved by geotechnical personnel from our office prior to placement of concrete.



If a basement/underground parking is introduced, for footings placed over the bedrock at varying depths, below existing grade, increased soil bearing pressure of 1200kPa (SLS) or more will likely be available. Rock coring is recommended to determine higher bearing capacity.

7. EARTHQUAKE CONDITIONS

The 2012 OBC Subsection 4.1.8 stipulates that a building should be designed to meet the requirements of the Earthquake Load and Effects. Site Classification for Seismic Site Response (Table 4.1.8.4.A) is determined from the average Standard Penetration Resistance (N60) and/or the undrained shear strength (Su) of the soils within the upper 30m.

Based on the results of standard penetration tests i.e., "N" values from the current geotechnical investigation, the site designation for seismic analysis applicable for the proposed buildings is "Class C". Site classification for footings placed over bedrock should be determined from shear wave velocity measurements.

Seismic parameters and requirements for analyses are detailed in Subsection 4.1.8 of the 2012 OBC.

8. EXCAVATION AND BACKFILL

No major problems should be encountered for the anticipated depths of excavation for the footings. Excavations for footings or underground services must be carried out in accordance with the latest edition of the Occupational Health and Safety Act (OHSA).

If the excavation is deeper than 1.2m, the sides should be sloped in accordance with requirements of OHSA. If this condition cannot be met, a temporary shoring system/ trench box should be introduced.

In accordance with O. Reg. 213/91, S.226 (1), the Site subsoils within anticipated excavation depths mainly consisted of earth fill, clayey silt till and can be generally classified as Type 3 soils.

Based on static groundwater measurements carried out during early fall groundwater was encountered at depths of 0.49m to 5.10m below prevailing grade. The open boreholes were however dry on completion of drilling. No defined aquifer was encountered and the groundwater may therefore be defined as trapped/perched water in silt/sand seams trapped in the predominantly clayey silt till and fill material. Some amount of seepage/trapped water will be expected for construction depending on the time of year that excavation takes place. Provisions should therefore be made to rid the site of occasional



seepage water from more permeable seams / lenses and/or surface run-off, especially following a heavy rainfall event, by pumping from sump pits.

The material to be used for backfill in service trenches should be suitable for compaction, i.e., free of organics and with moisture content within 2 percent of the optimum moisture value. The backfill material should be compacted in lifts of no more than 200mm in thickness and to at least 98 percent of Standard Proctor Maximum Dry Density (SPMDD) in the upper 1.0m from road subgrade or in settlement sensitive areas. Beyond these zones, a 95 % SPMDD compaction criterion is considered acceptable.

Additionally, onsite excavated fill materials and native soils may be used as backfill in service trenches, provided that the excavated materials are free of organic soils /construction debris and are of suitable moisture content.

For backfill against the subsurface walls and footings it is recommended that backfill materials consist of Granular Class 'B' aggregates. On-site excavated granular material may be acceptable subject to further site inspection.

9. SLAB ON GRADE AND PERMANENT DRAINAGE

For the proposed buildings, the finished floor slab can be constructed as slab on grade supported by competent native undisturbed clayey silt till or engineered fill. Engineered fill may be utilized for the replacement of existing fill (subject to further test pit tests and inspection), especially in the area around BH2/BH201 and BH204.

If engineered fill is required to raise subgrade up for slab construction, the engineered fill must be placed on a thoroughly proof-rolled exposed base and organic soil / topsoil/ fill / construction debris /underside utilities removed and the base approved by engineering staff from Fisher Engineering office before commencing of engineered fill construction.

Furthermore, any soft spots revealed during proof-rolling should be sub-excavated and backfilled with suitable granular materials, compacted to 98% SPMDD.

Engineered fill materials, compaction quality and finished subgrade proof-rolling should be supervised and inspected by engineering staff from our office. Engineered fill must be placed in layers of no more than 200mm and compacted to 98% SPMDD.



Onsite excavated native soils and selected fill materials can be used for engineered fill provided they contain suitable moisture content. Granular Class 'B' aggregates are preferred for subgrade construction for slab on grade especially during the wintertime or wet season.

For backfill against subsurface walls and footings it is recommended that backfill materials consist of Granular Class 'B' aggregates

Upon completion of foundation work, the floor slab should rest on a well compacted bed of size 19mm clear stone at least 200mm thick. The stone bed would act as a barrier and prevent capillary rise of moisture from the subgrade to the floor slab.

No perimeter drainage will be required, if the floor slab is at least 200mm above the exterior grade. The exterior grade should be sloped away from the buildings at an inclination of 1 to 2 percent to prevent ponding of water close to exterior walls. If this condition cannot be met, then a permanent perimeter drainage system as shown on Appendix D is recommended for footing/foundation walls.

10. UNDERGROUND UTILITIES

Pipe bedding and backfill materials specifications and compaction criteria for water and sewer services should be in accordance with the pipe designer's recommendations and/or local municipal requirements.

If the excavation is deeper than 1.2m, the excavation sides should be sloped in accordance with requirements of OHSA. If this condition cannot be met, a temporary shoring system or trench box should be introduced.

For the subject site, it is expected that the underground services would be founded on the clayey silt till. Granular Class 'B' aggregate is generally considered well suited to be used as bedding material. However, it should be noted, that the recommended type of bedding is to be placed on undisturbed subgrade above the groundwater level. If the construction methods will disturb the subgrade i.e., piping, existing footing, boulder removal etc. or existence of excess hydrostatic pressure, then higher-class bedding may have to be used combined with a geotextile. In some areas, localized dewatering may be required.

Selected onsite excavated fill materials / native soils are considered to be suitable for re-use in trench backfilling, provided that organics / construction debris are sorted out and materials are not allowed to be wet and moisture should be within 2% of the optimum moisture content.



In normal sewer construction practice, the problem of road settlement largely occurs adjacent to manholes, catch basins and service crossings. In these areas, granular materials are generally required for backfill and compaction.

Water lines installed outside of heated areas should be provided with a minimum of 1.5m soil cover or equivalent for frost protection.

11. PAVEMENT

The site development will be associated with asphalt paved driveways and parking areas. Pavement structures can be constructed on the native soils, engineered fill, or possibly fill materials for the site, subject to design grade and further onsite inspection.

Prior to asphalt pavement construction, topsoil/organic soil/ construction debris should be removed. The exposed base should be proof-rolled and supervised / approved by our office. Any soft/ spongy spots detected during proof-rolling should be sub-excavated and replaced with suitable materials and compact to 98% of SPMDD. Engineered fill construction, if any, should be supervised and inspected by engineering staff from our office.

Finished subgrade must be contoured/ graded and finally proof-rolled and approved by our office before placing upper granular materials.

Granular materials will be used in construction of asphalt pavement bases. Compaction for granular bases should reach to 100 % of Standard Proctor Maximum Dry Density. Perforated drains connected to sewer MHs/ CBs should be provided under the entire length of curb and constructed in accordance with required local regulations. Typical flexible pavement designs are shown in Table 4.

Table 4: Flexible pavement design.

	COMPACTED THICKNESSES				
PAVEMENT LAYER	LIGHT DUTY PARKING	DRIVEWAYS & HEAVY DUTY PARKING			
Asphalt top course, HL-3	40mm	40mm			
Asphalt base course, HL-8	40mm	60mm			
Granular 'A' or 20mm crusher run limestone base	150mm	150mm			
Granular 'B' or 50mm crusher run limestone sub-base	200mm	300mm			



The pavement thickness should also meet the minimum local region Pavement Design Standards.

The asphalt material should meet the OPSS requirements for specified grade and be compacted to at least 92% of their MRD.

12. GENERAL COMMENTS

This report is limited in scope to those items specifically referenced in the text. The discussions and recommendations presented in this report are intended only as guidance for the client named and design engineers.

The information on which these recommendations are based is subject to confirmation by engineering personnel at the time of construction.

Localized variations in subsoil conditions may be present between and beyond the boreholes and must be verified during construction. As more specific subsurface information becomes available during excavation on the subject site, this report should be updated.

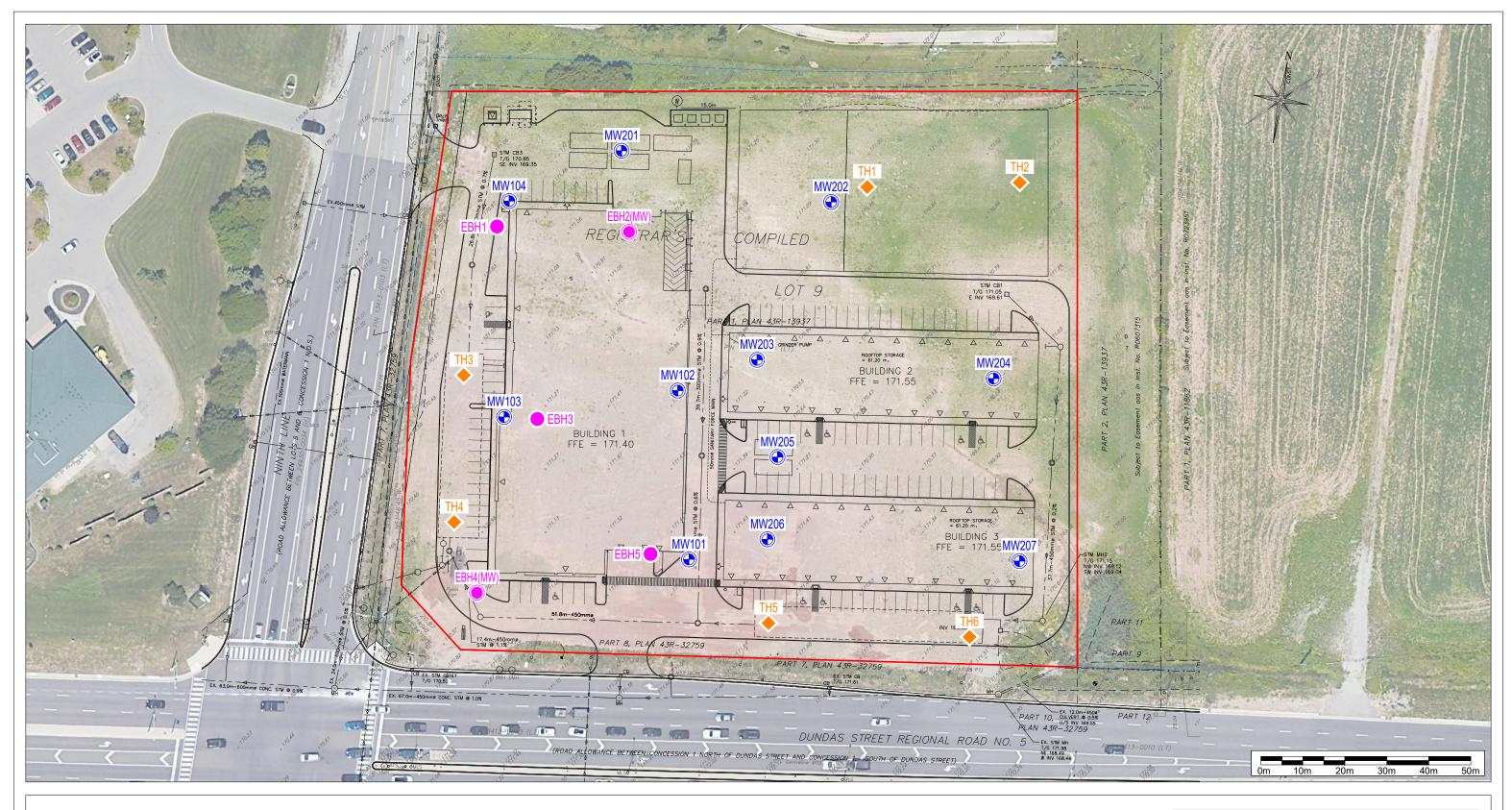
Contractors bidding on or undertaking the work should decide on their own investigations, as well as their own interpretations of the factual borehole results. This concern specifically applies to the classification of the subsurface soil and the potential reuse of these soils on/off site.

Contractors must also draw their own conclusions as to how the near surface and subsurface conditions may affect them.



APPENDIX A – SITE AND LOCATION PLANS







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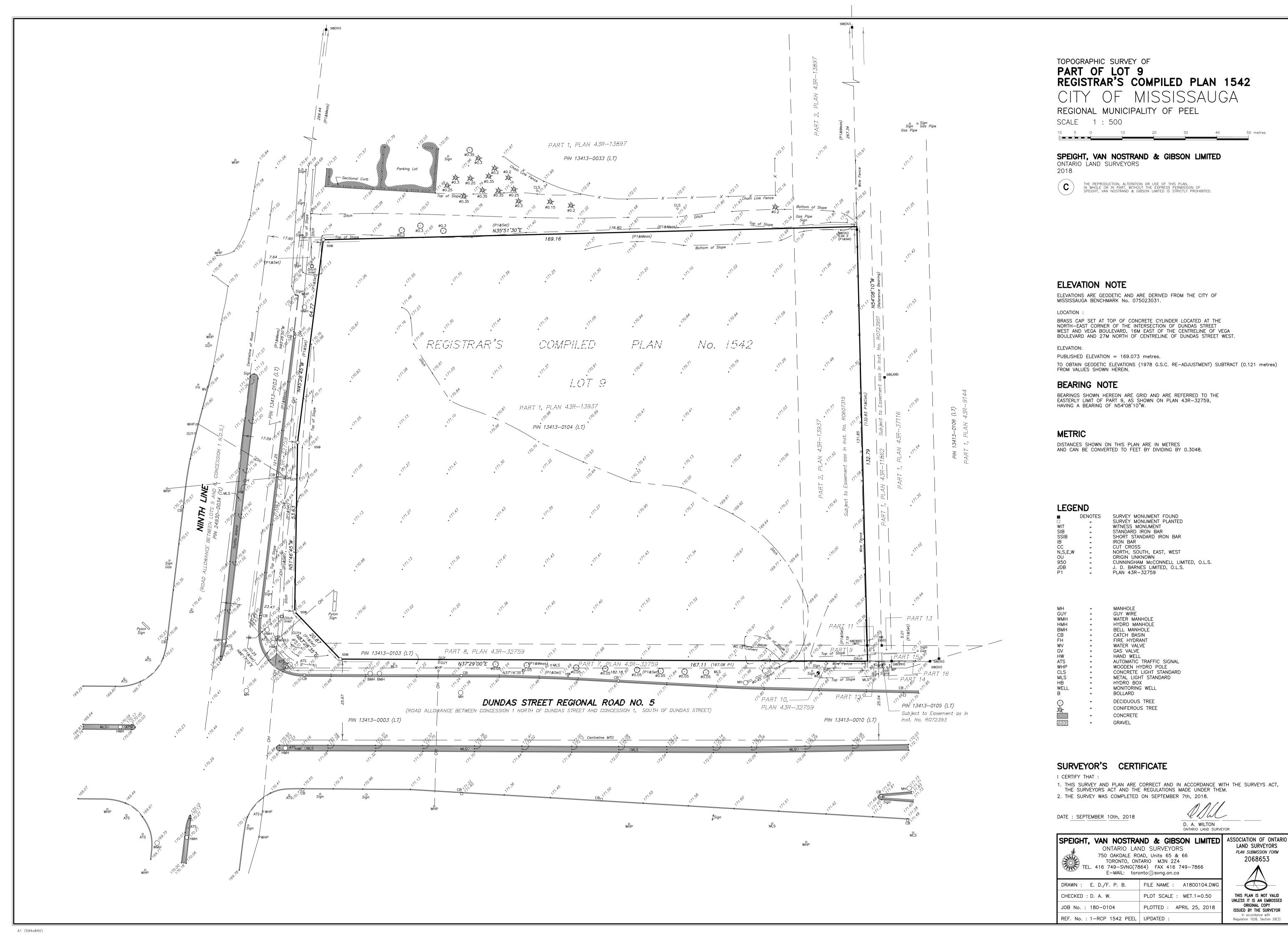


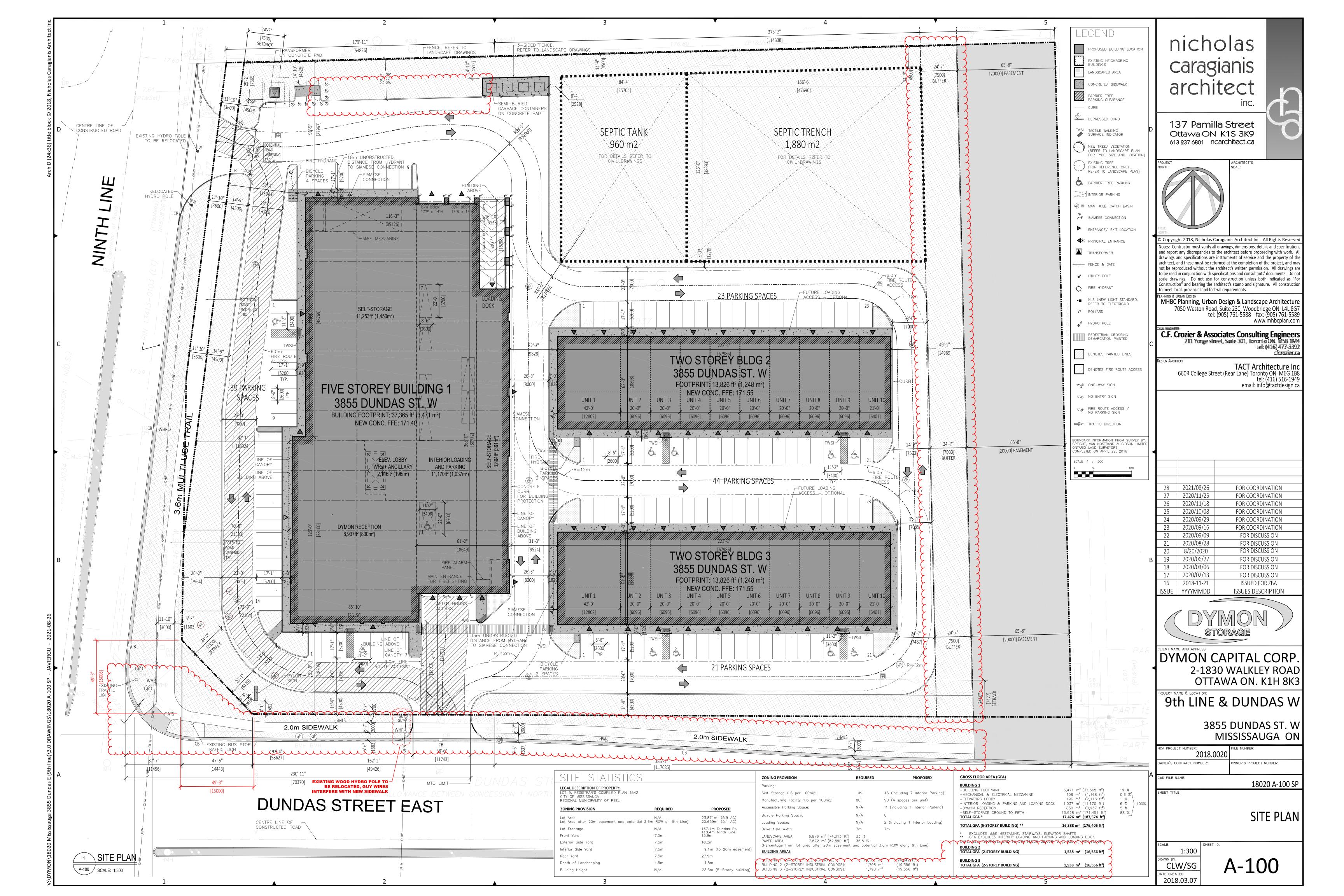
PROJECT NAME AND ADDRESS

HYDROGEOLOGICAL & **GECOTECHNICAL INVESTIGATIONS**

3855 Dundas Street East, Mississauga, ON.

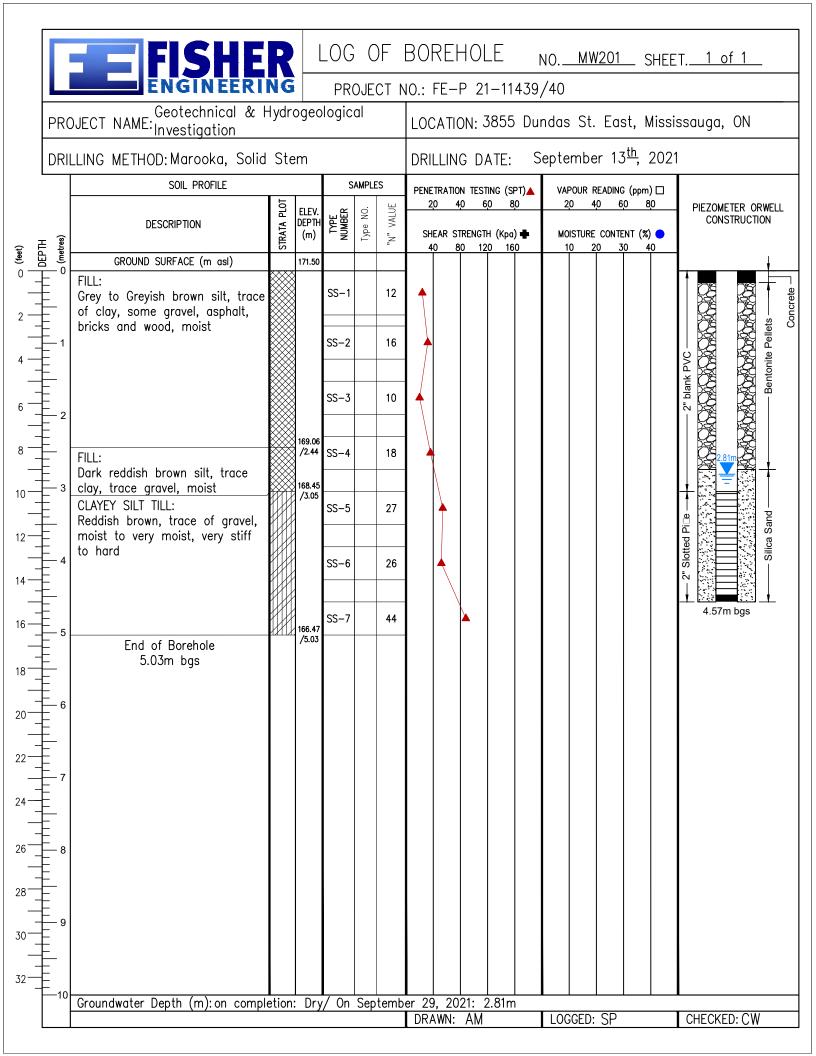
ROJECT NO.	FIGURE 1.1:	SHEET NO.
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ATE.	SITE PLAN WITH	
13 October 2021	TEST HOLE AND MONITORING WELL	
CALE.	LOCATIONS	
AS SHOWN		

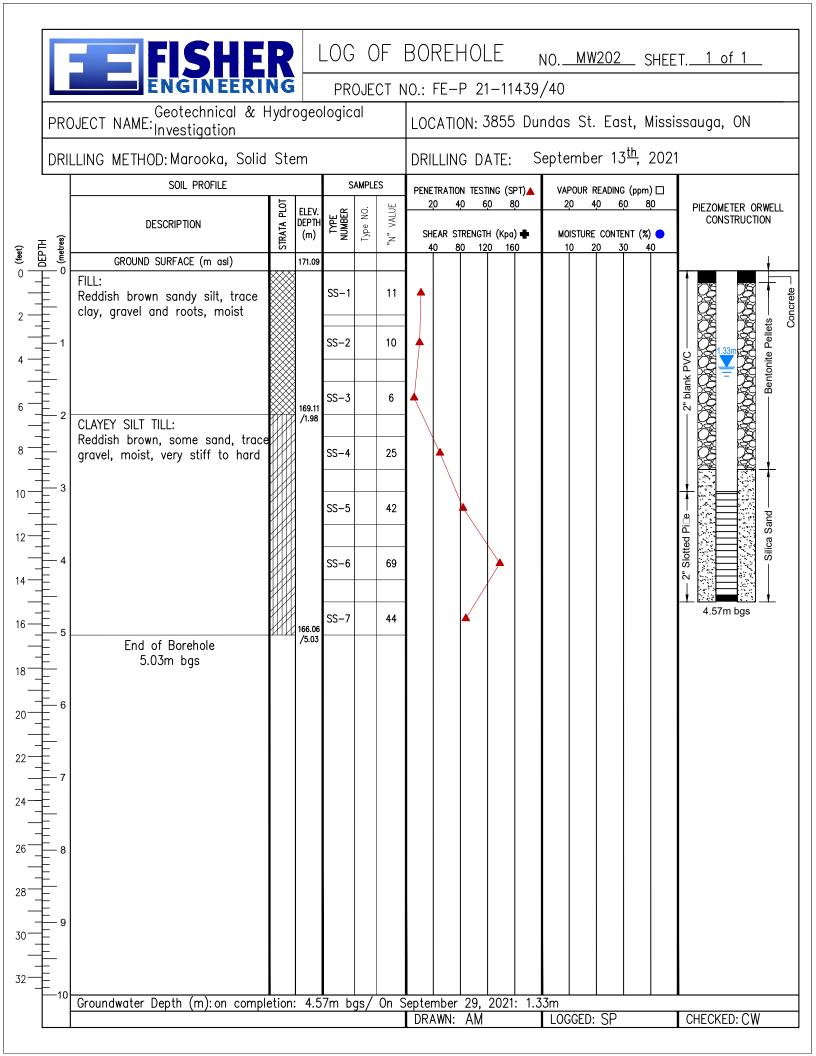


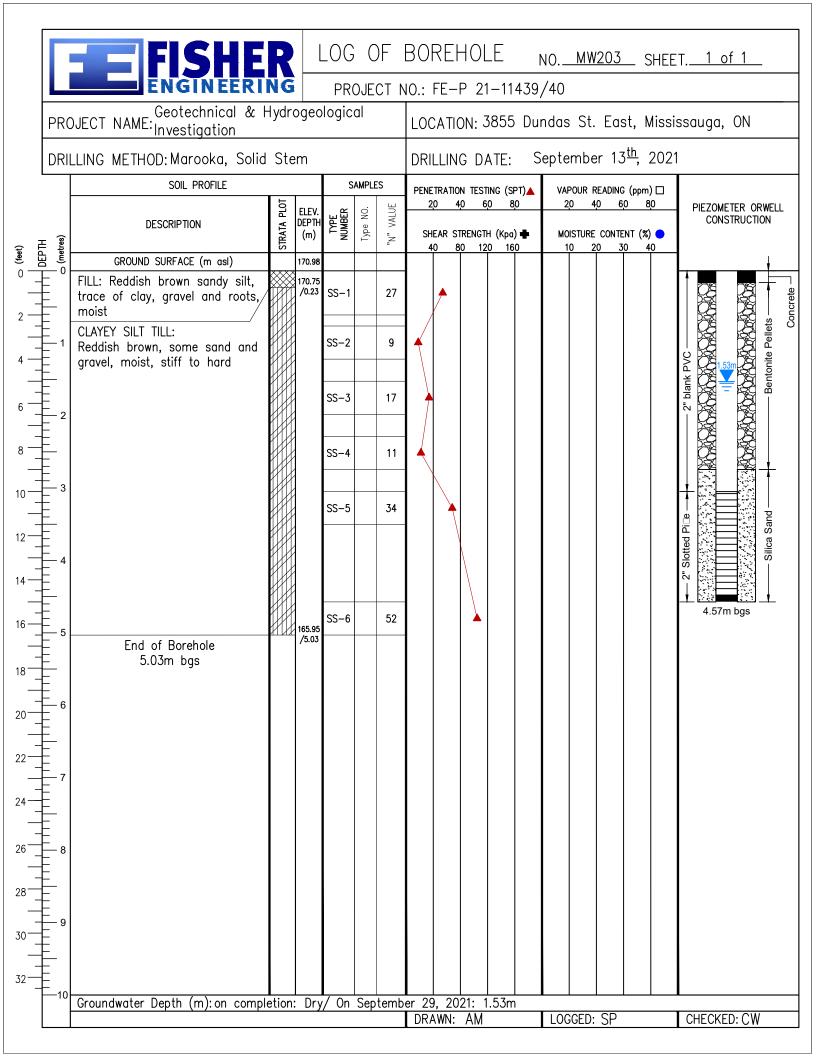


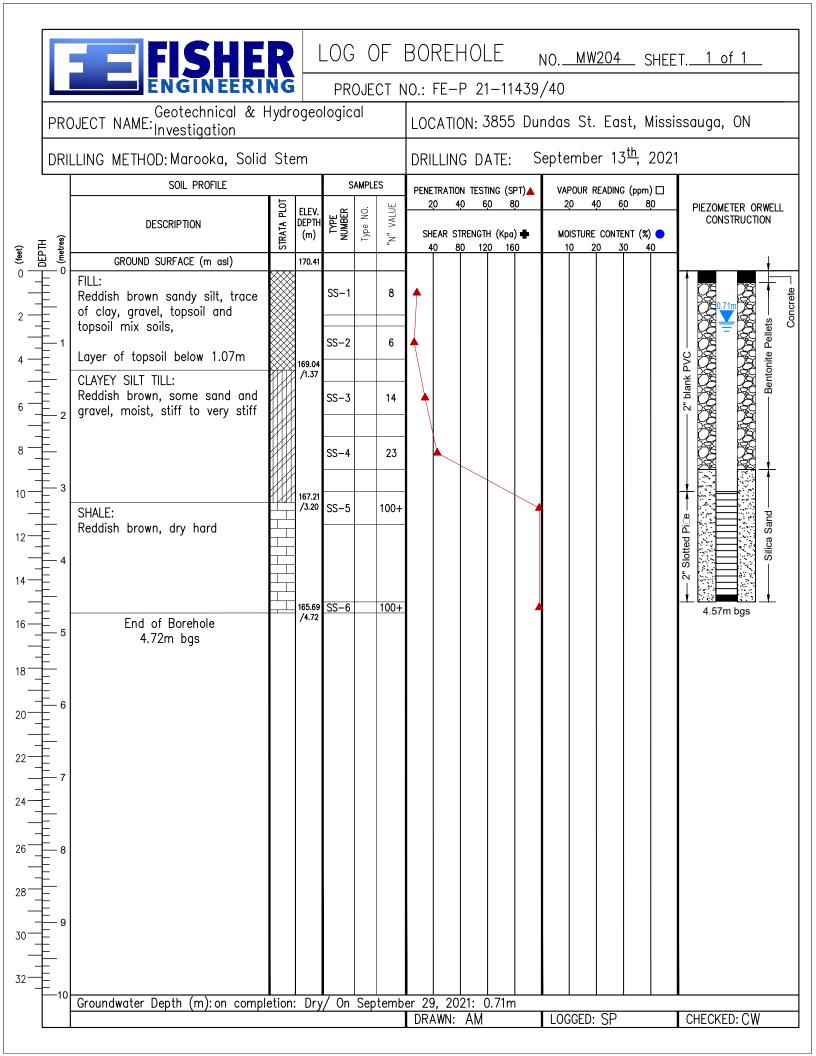
APPENDIX B – LOG OF BOREHOLES

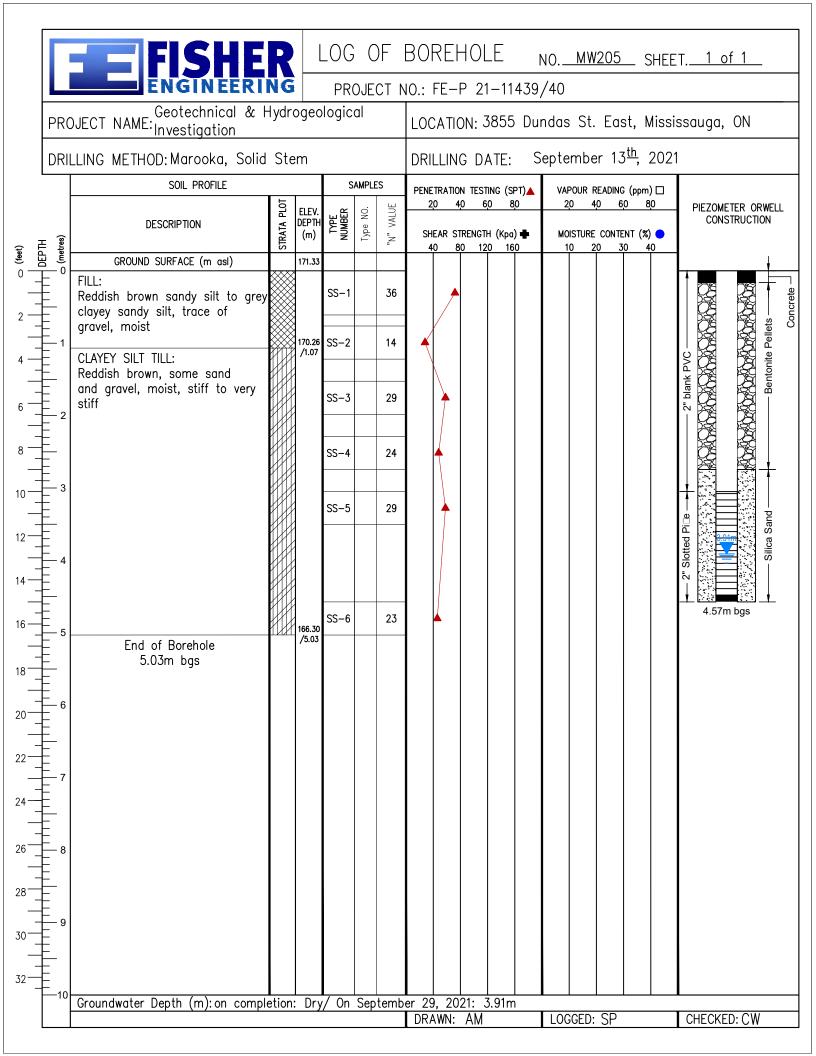


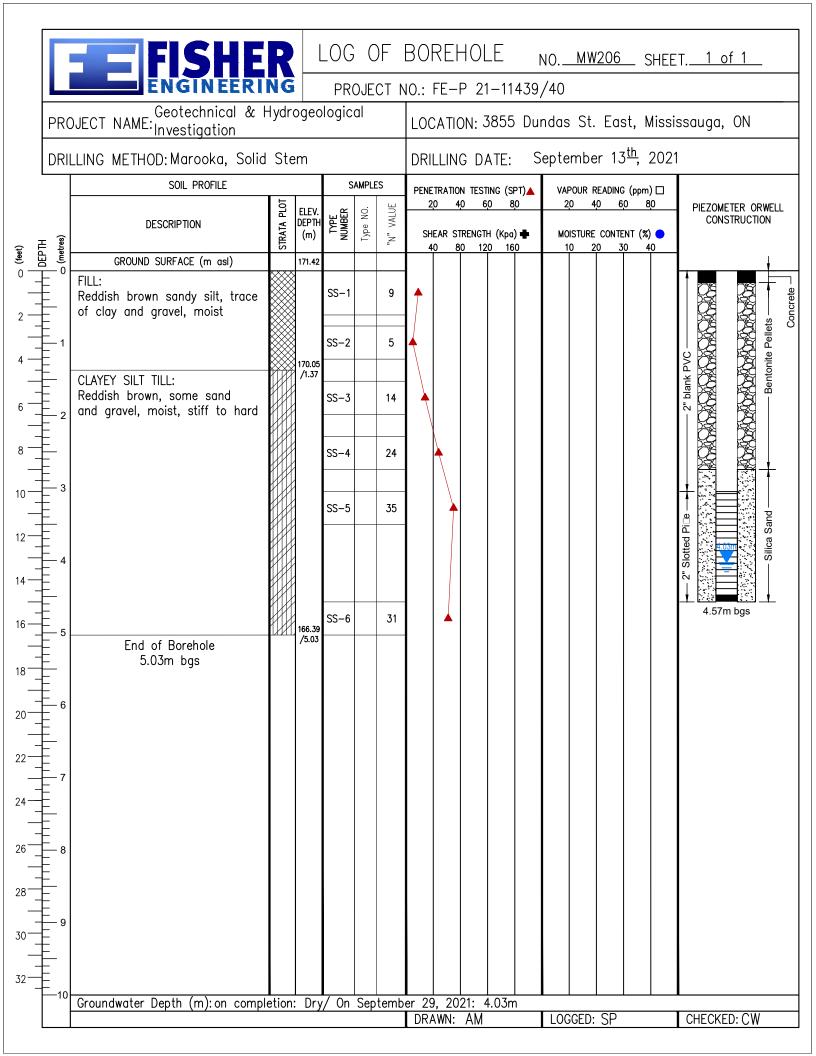


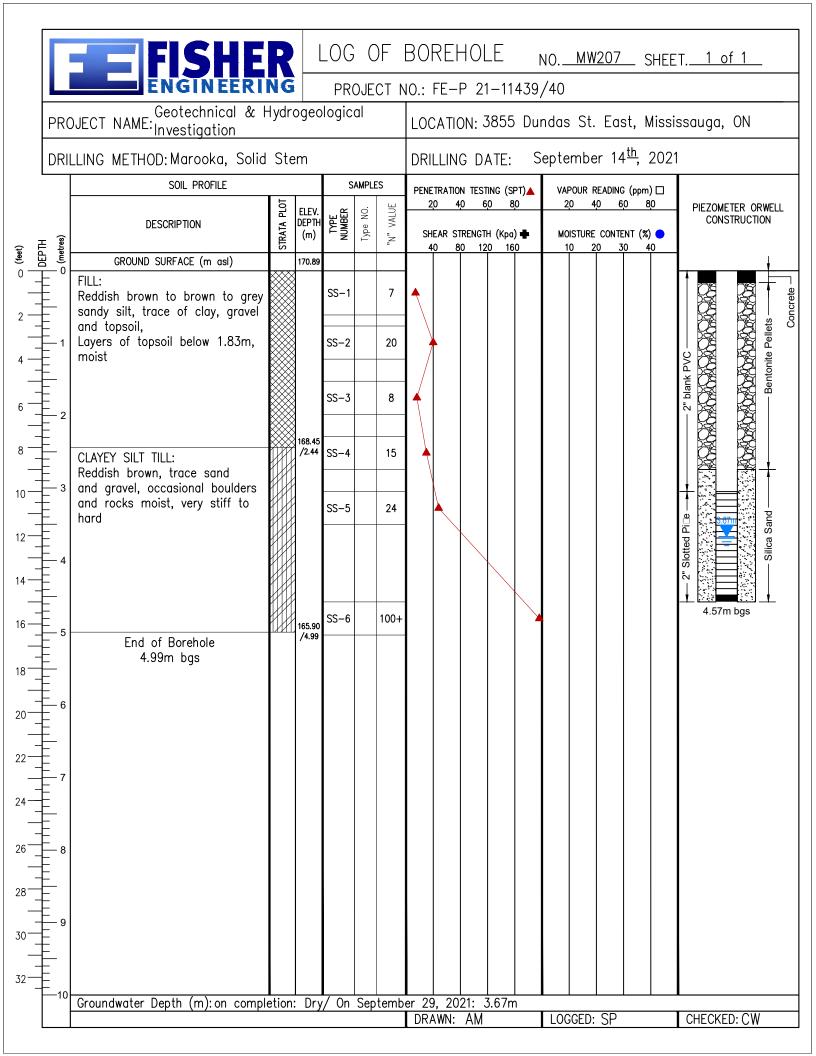


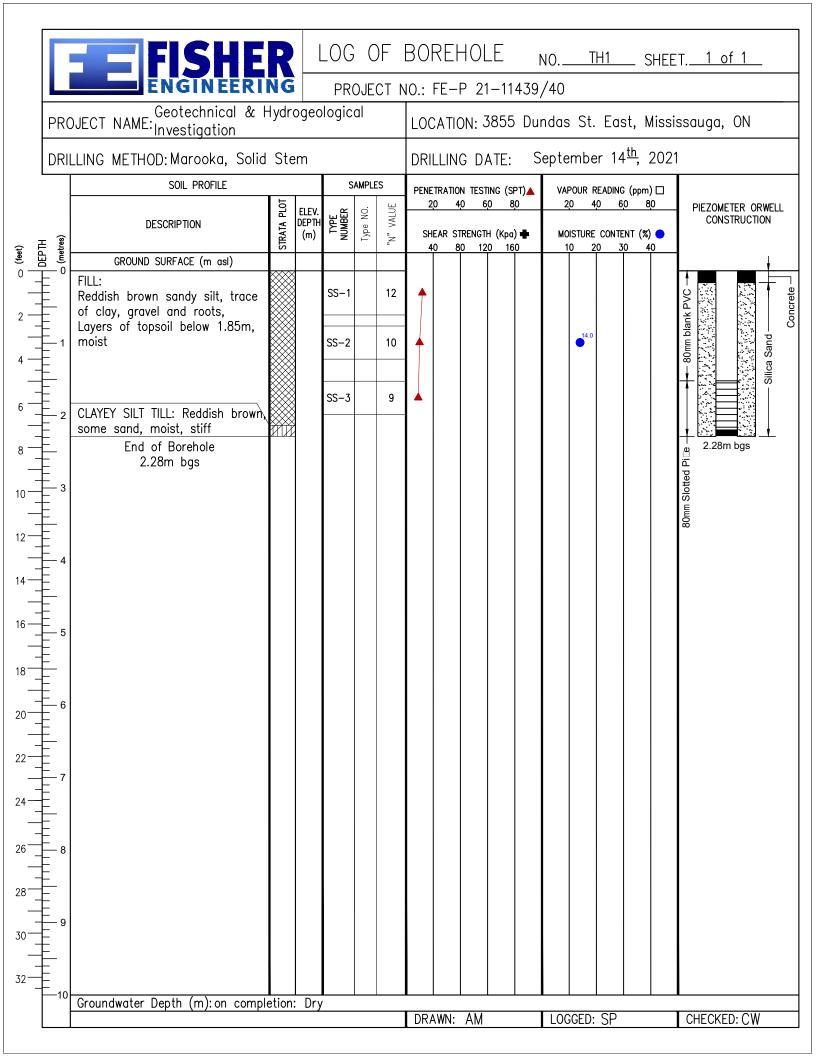


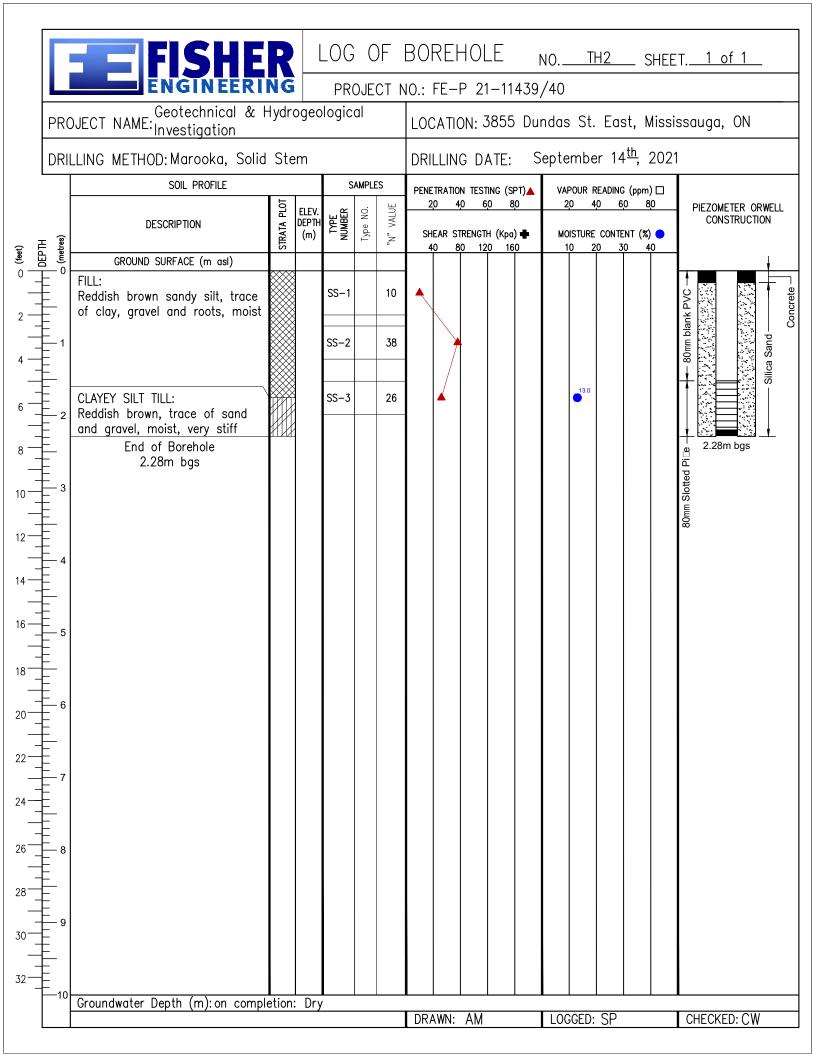


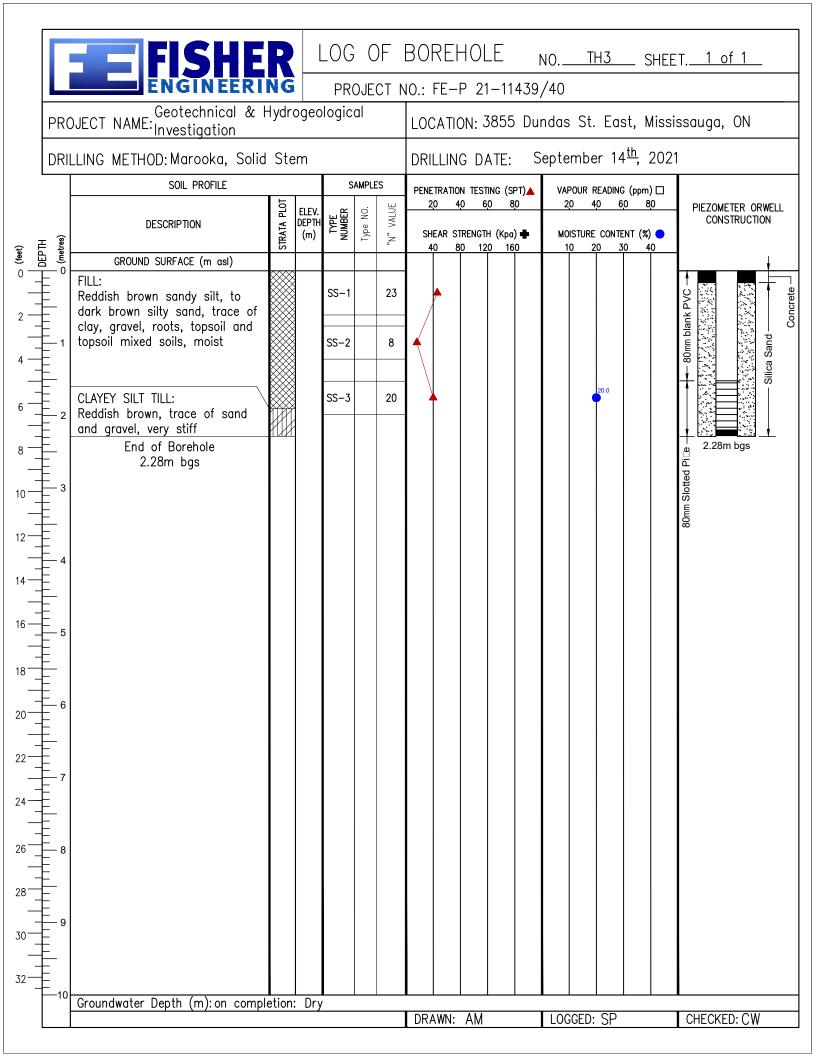


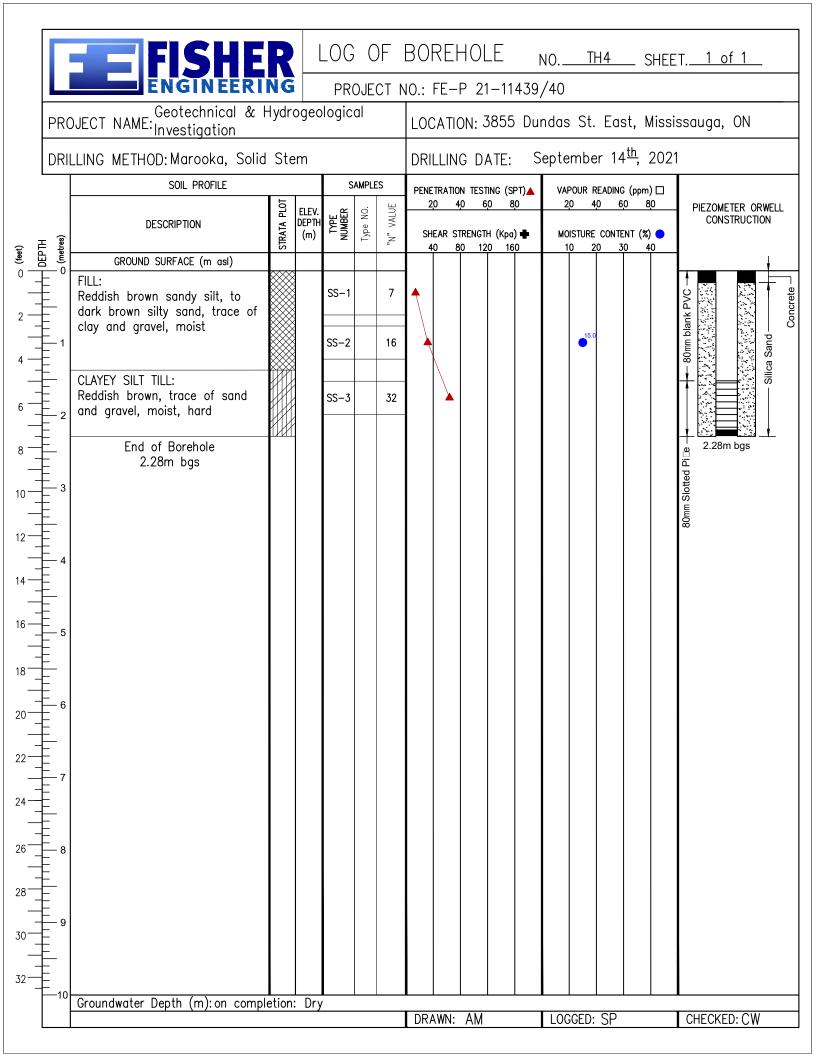


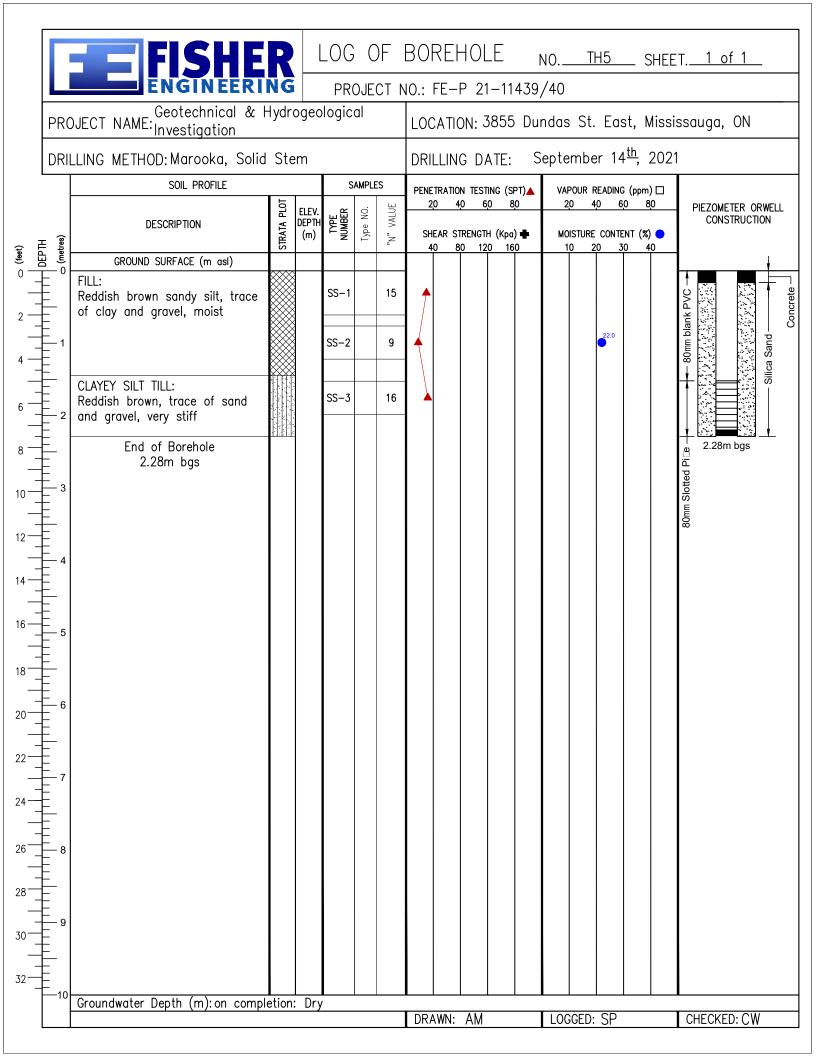


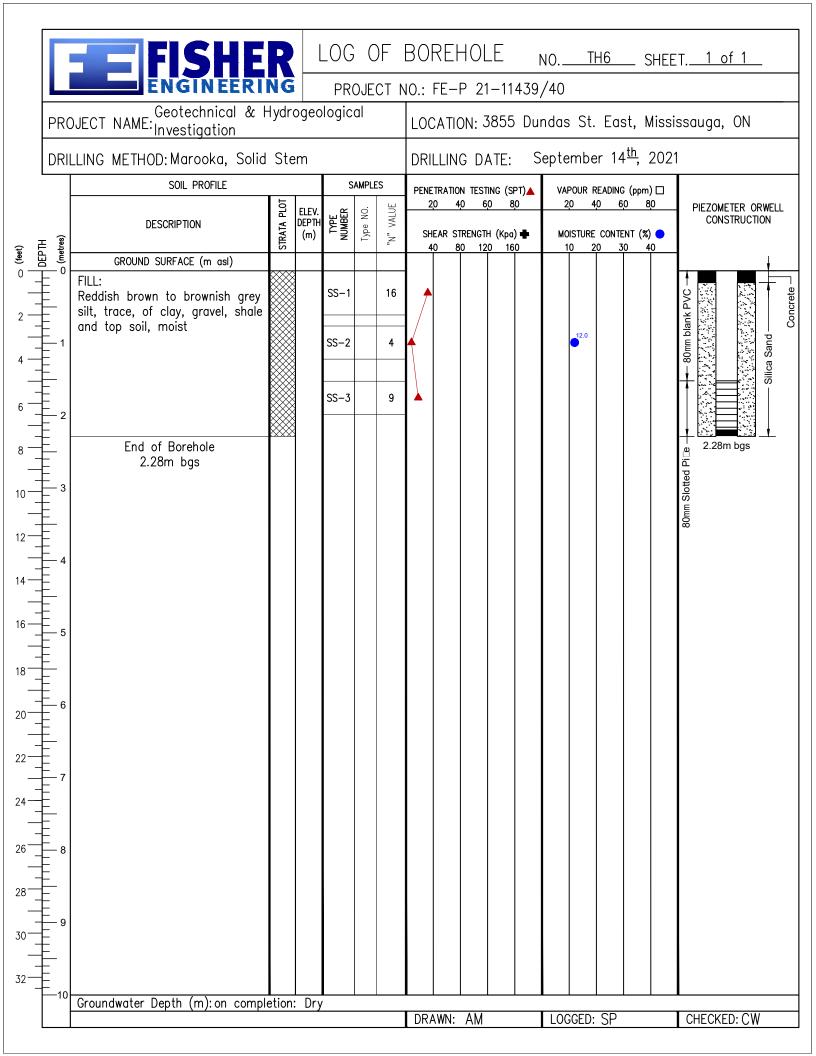


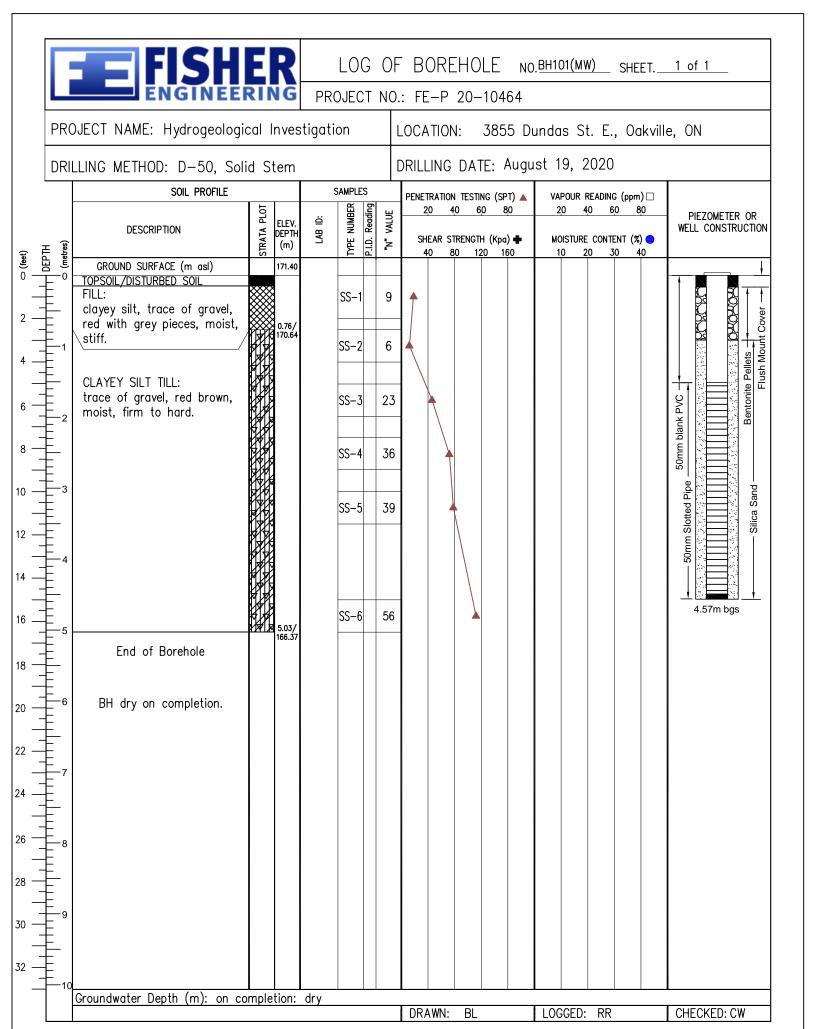


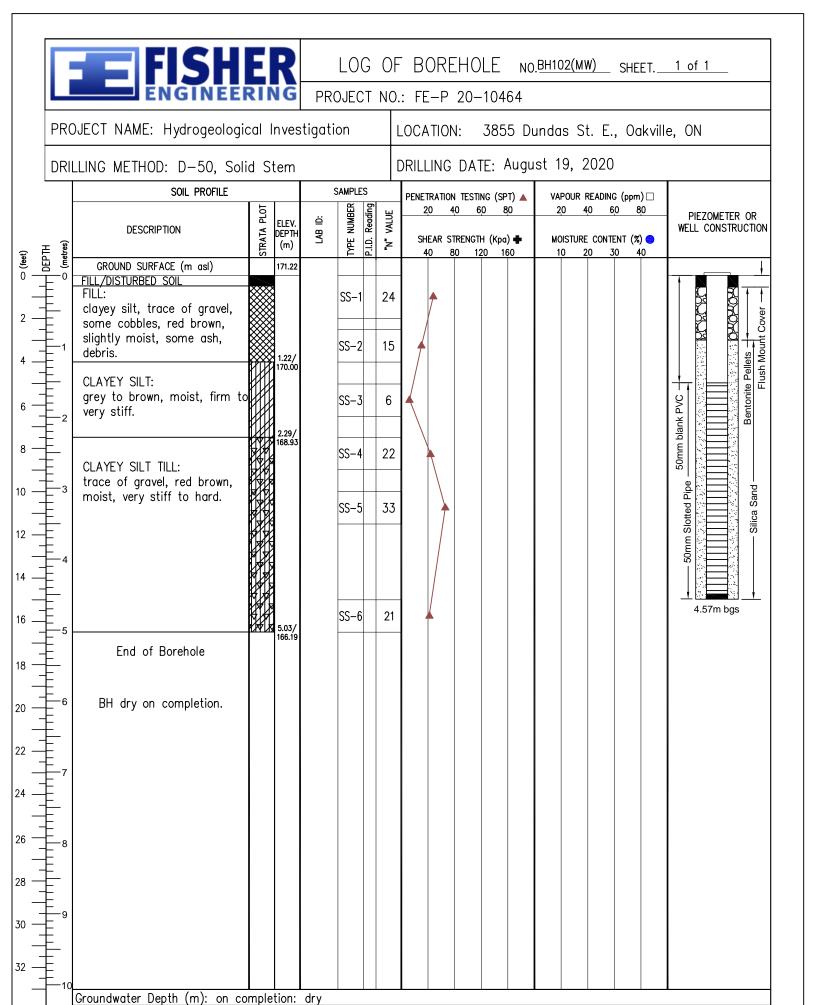










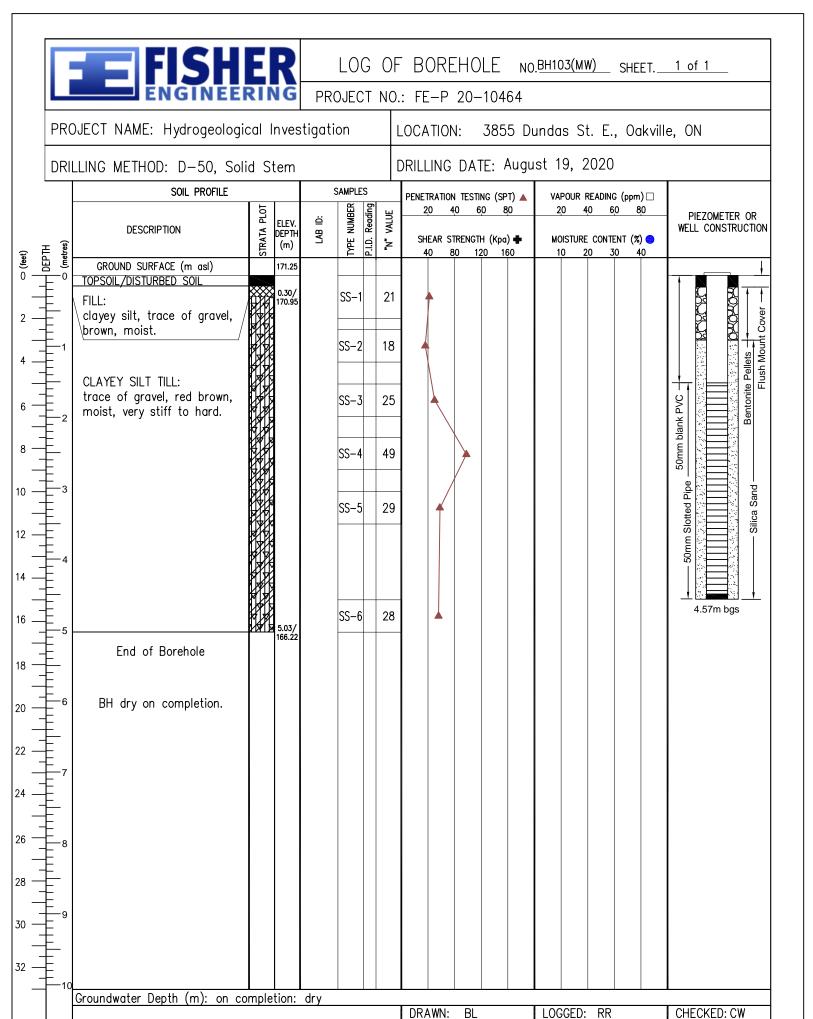


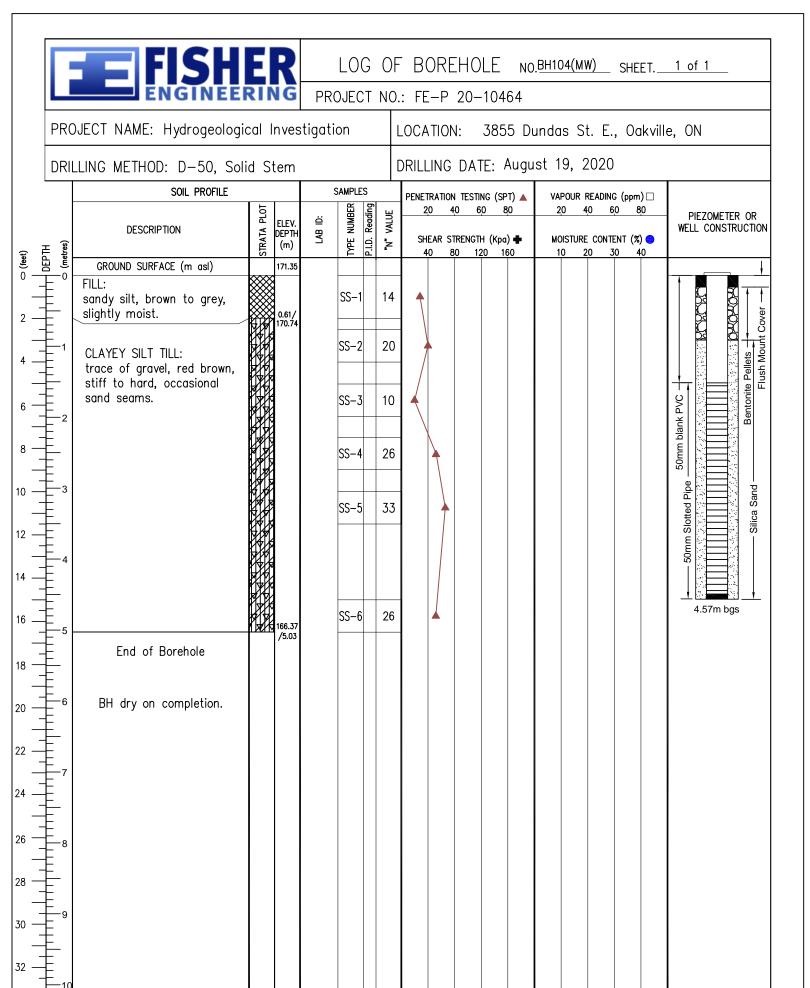
DRAWN:

BL

LOGGED: RR

CHECKED: CW





DRAWN:

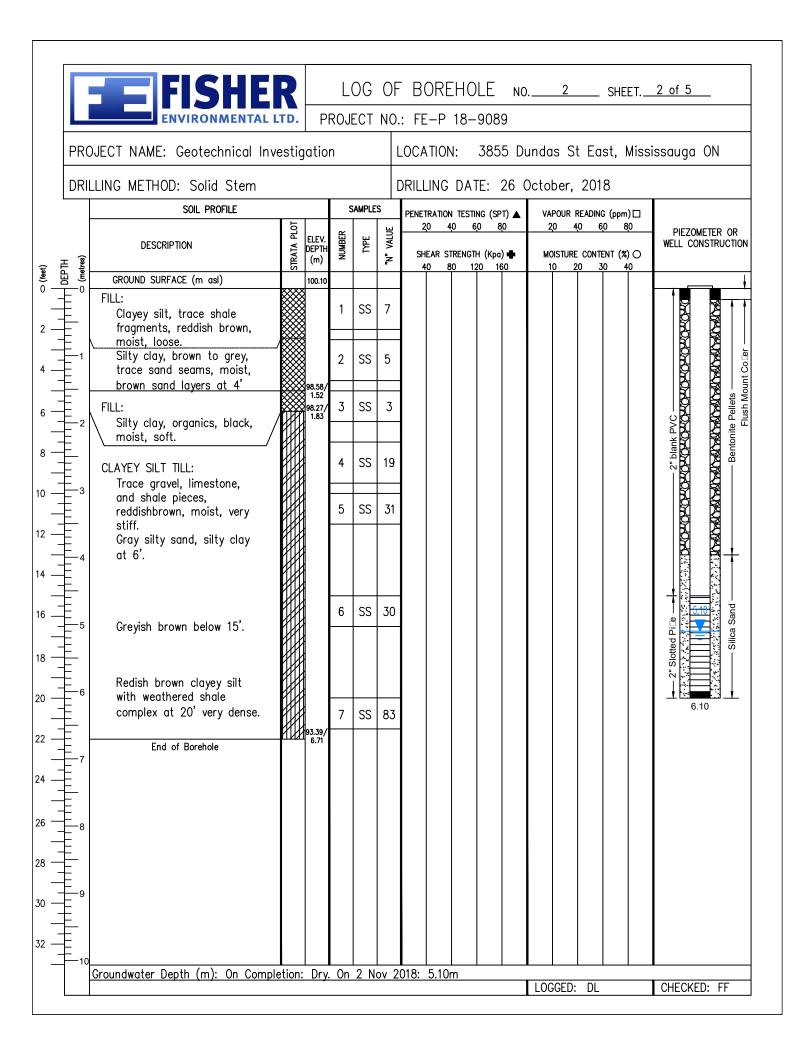
BL

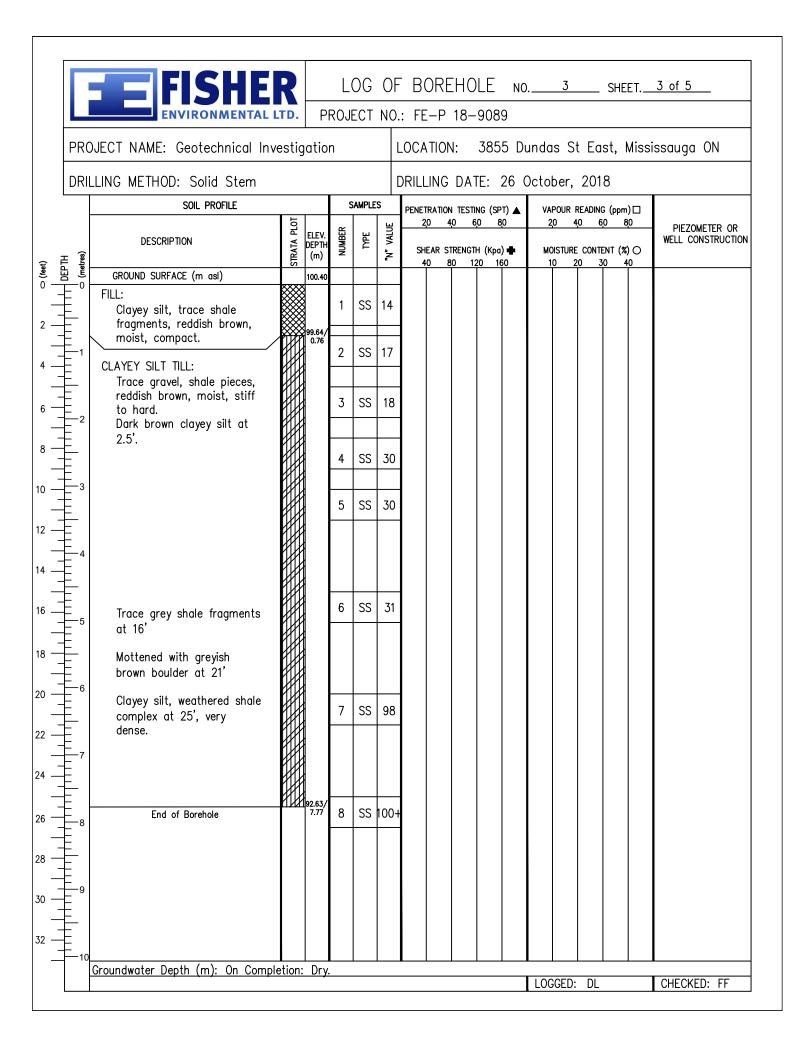
LOGGED: RR

CHECKED: CW

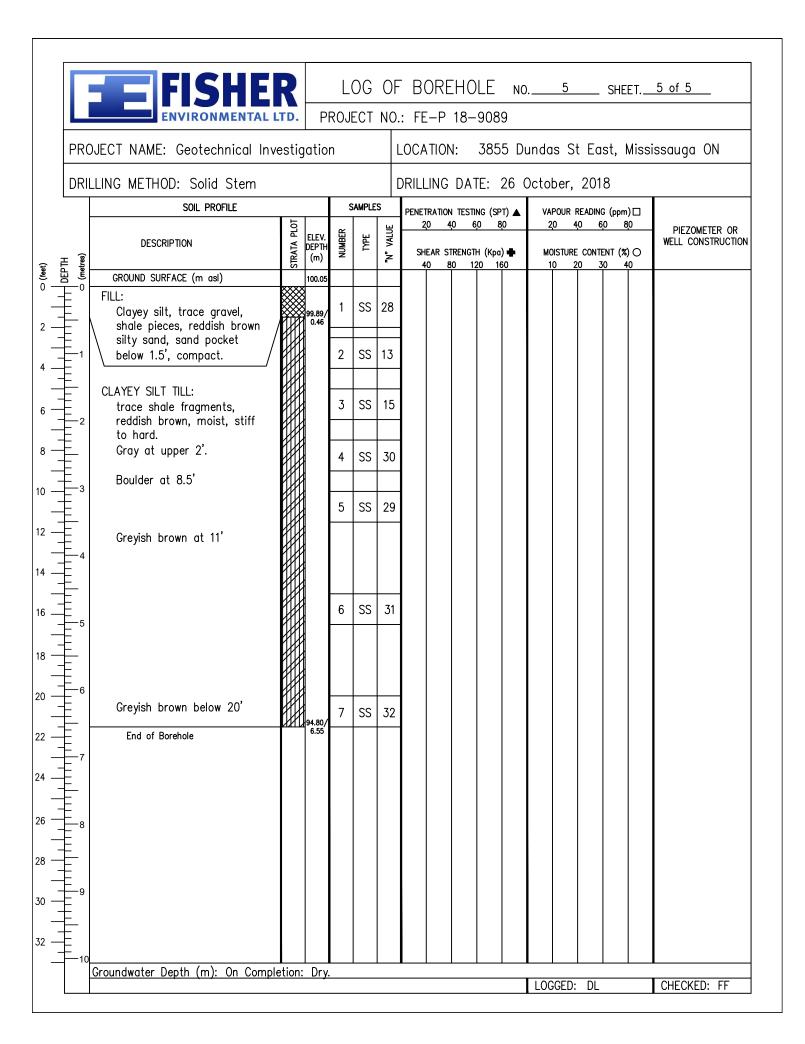
Groundwater Depth (m): on completion: dry

	FISHER ENVIRONMENTAL LTD). P				OF BOREHOLE NO. 1 SHEET. 1 of 5 O.: FE-P 18-9089
PF	ROJECT NAME: Geotechnical Invest	tigatio	n			LOCATION: 3855 Dundas St East, Mississauga ON
DF	RILLING METHOD: Solid Stem					DRILLING DATE: 26 October, 2018
•	SOIL PROFILE	=	S	AMPLES		PENETRATION TESTING (SPT) ▲ VAPOUR READING (ppm) □ 20 40 60 80 PIEZOMETER OR
(feet) DEPTH (metros)	DESCRIPTION	SKAIN FIEDED IH (m)	NUMBER	TYPE	"N" VALUE	20 40 50 50 20 40 PIEZOMETER OR WELL CONSTRUCTION SHEAR STRENGTH (Kpa)
	FILL: Clayey silt, trace shale pieces, sand pockets, coarse	100.00 98.15/ 1.52		SS	9	_
	loose. SANDY SILT TILL:		2	SS	14	<u>-</u> 4
4 —————————————————————————————————————	Trace gravel, limestone, shale pieces, redish brown, moist, stiff to hard.		3	SS	26	
6 —	2		<u> </u>	33	20	
8 —	Shale fragments at 8.5'		4	SS	31	
			5	SS	38	8
2	5		6	SS	36	<u>6</u>
	Grey below 20'					
2	End of Borehole	93.11/ 6.56	7	SS	26	
4 = = = = = = = = = = = = = = = = = = =						
6 — [3					
8 = = = = = = = = = = = = = = = = = = =						
	Groundwater Depth (m): On Completic	n: Dry				LOGGED: DL CHECKED: FF





	DJECT NAME: Geotechnical Investi		ROJ		NC	.: FE-P 18-9089	Dundas St East, Miss October, 2018	
	SOIL PROFILE			SAMPLE	 :s	PENETRATION TESTING (SPT)	1	
DEPTH (metres)	DESCRIPTION S	ELEV DEPTI (m)	NUMBER	TYPE	"N" VALUE	20 40 60 80 SHEAR STRENGTH (Kpa) 40 80 120 160	20 40 60 80	- PIEZOMETER OR WELL CONSTRUCTION
100	GROUND SURFACE (m asl) FILL: Clayey silt, trace gravel, shale pieces, reddish brown	99.89 0.46	1	SS	28	-		
	silty sand, sand pocket below 1.5', compact		2	SS	13	-		
	CLAYEY SILT TILL: trace shale fragments, reddish brown, moist, gray at uper 2', stiff to hard.		3	SS	15			blank PVC VONONONONONO II II II SETTING THE STANDARD AND THE STANDARD STAN
	Boulder at 8.5'		4	SS	30			2" blank
	Greyish brown at 11'		5	SS	29	-		2" blank PVC ———————————————————————————————————
- - - - - - - - - - - - - - - - - - -			6	SS	31	-		Slica Sand
6	Greyish brown below 20'							6.10
7	End of Borehole	94.80, 6.55	7	SS	32	-		50
8								
9								
+								



APPENDIX C- MOISTURE CONTENT ANN GRAIN SIZE ANALYSIS





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400 ESNA PARK DRIVE #15 MARKHAM, ONT. L3R 3K2 TEL: 905 475-7755 FAX: 905 475-7718 www.fisherenvironmental.com

Client: Dymon Group of Companies

Address: 2-1830 Walkley Road

Ottawa, ON

K1H 8K3 *Tel.:*

Email:

Attn.:

F.E. Job #: 21-7241A

Project Name: Infiltration Tests

Project ID: FE-P 21-11439

Date Sampled: 14-Sep-2021

Date Received: 17-Sep-2021Date Reported: 24-Sep-2021

CHEMICAL PA

Ronggen (Roger) Lin

CHEMIST

Location: 3855 Dundas Street East

Certificate of Analysis

Analyses	Matrix	Quantity	Date Extracted	Date Analyzed	Lab SOP	Method Reference
Moisture Content	Soil	6	N/A	17-Sep-21	Support Procedures F-99	Carter (1993)
Grain Size	Soil	6	N/A	21-Sep-21	Grain Size F-28	ASTM D6913-04

Fisher Environmental Laboratories is accredited by CALA (the Canadian Association for Laboratory Accreditation Inc.) for specific parameters as required by Ontario Regulation 153/04. All analytical testing has been performed in accordance with ISO 17025 and the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act published by Ontario Ministry of the Environment.

Authorized by:

Roger Lin, Ph. D., C. Chem Laboratory Manager

Page 1 of 9

Certificate of Analysis

Analysis Requested:	Moisture Content, Grain Size
Sample Description:	8 Soil Sample(s)

	21-7241-1	21-7241-3	21-7241-4	21-7241-5	21-7241-6	21-7241-8
Parameter	TH1	TH2	TH3	TH4	TH5	TH6
	0.75-1.20m	1.50-1.95m	1.50-1.95m	0.75-1.20m	0.75-1.20m	0.75-1.20m
Geo Moisture Content (%)	14	13	20	15	22	12

QA/QC Report

Parameter	Blank	RL	LCS	AR	Duplicate	AR
i arameter			Recov	ery (%)	RP	D (%)
Geo Moisture Content (%)	< 0.1	0.1	100	70-130	4.9	0-20

LEGEND:

RL - Reporting Limit

LCS - Laboratory Control Sample

AR - Acceptable Range

RPD - Relative Percent Difference

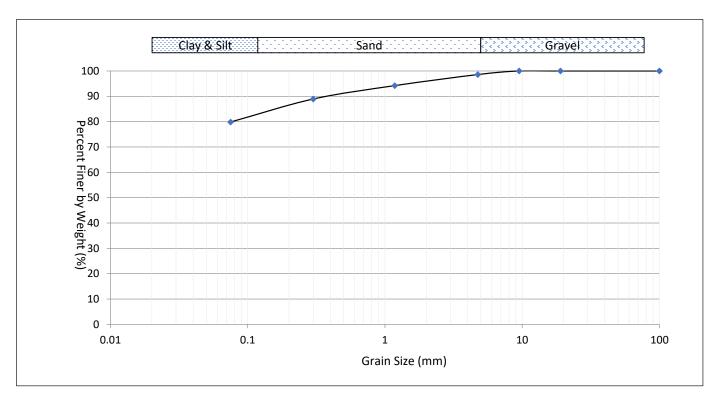
Certificate of Analysis

Analysis Requested:	Moisture Content, Grain Size
Sample Description: 8 Soil Sample(s)	

	21-7241-1	21-7241-3	21-7241-4	21-7241-5	21-7241-6	21-7241-8	
Parameter	TH1	TH2	TH3	TH4	TH5	TH6	
	0.75-1.20m	1.50-1.95m	1.50-1.95m	0.75-1.20m	0.75-1.20m	0.75-1.20m	
Grain Size (%)							
>19mm	0.0	0.0	0.0	0.0	0.0	0.0	
9.5mm-19mm	0.0	0.0	2.3	0.0	0.0	2.3	
4.75mm-9.5mm	1.4	4.2	4.2	2.2	0.7	4.2	
1.18m-4.75mmm	4.4	3.2	2.3	2.5	0.6	8.5	
300um-1.18mm	5.3	4.1	2.4	3.1	1.9	9.6	
75um-300um	9.1	7.8	5.6	6.3	4.5	12.7	
<75um	79.9	80.8	83.2	85.9	92.3	62.8	
Clay & Silt	80	81	83	86	92	63	
Sand	19	15	10	12	7	31	
Gravel	1	4	7	2	1	6	

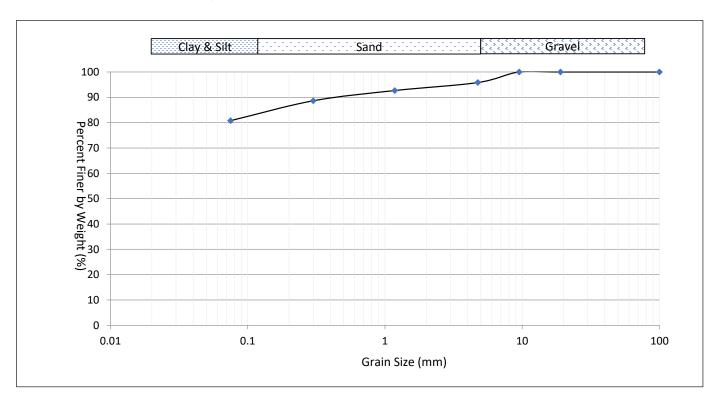
Sample ID: 21-7241-1 TH1 0.75-1.20m

Clay & Silt: 80% Sand: 19% Gravel: 1%



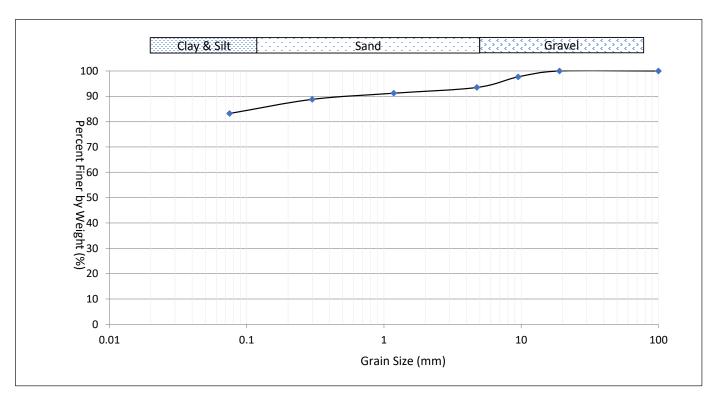
Sample ID: 21-7241-3 TH2 1.50-1.95m

Clay & Silt: 81% Sand: 15% Gravel: 4%



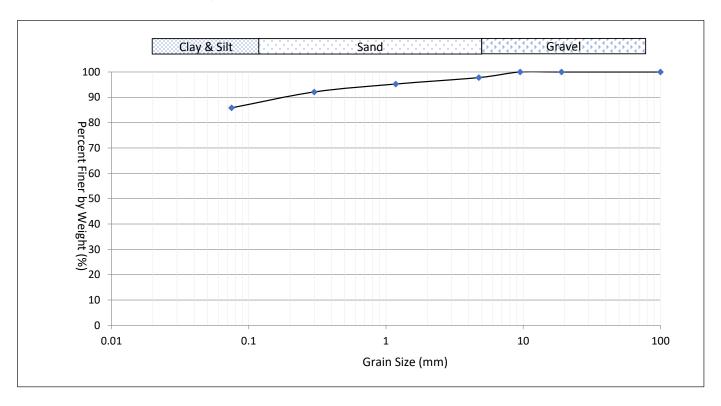
Sample ID: 21-7241-4 TH3 1.50-1.95m

Clay & Silt: 83% Sand: 10% Gravel: 7%



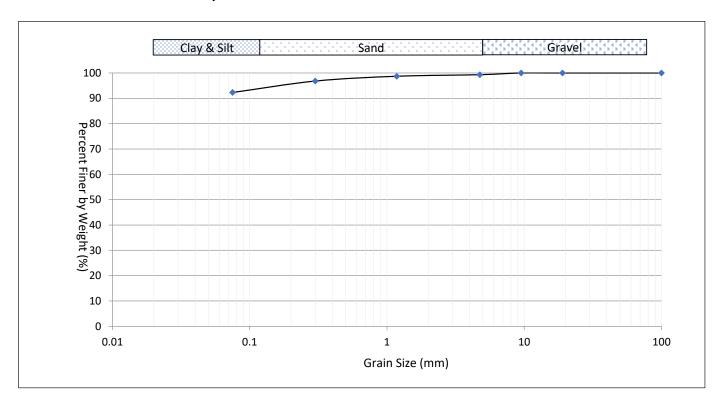
Sample ID: 21-7241-5 TH4 0.75-1.20m

Clay & Silt: 86% Sand: 12% Gravel: 2%



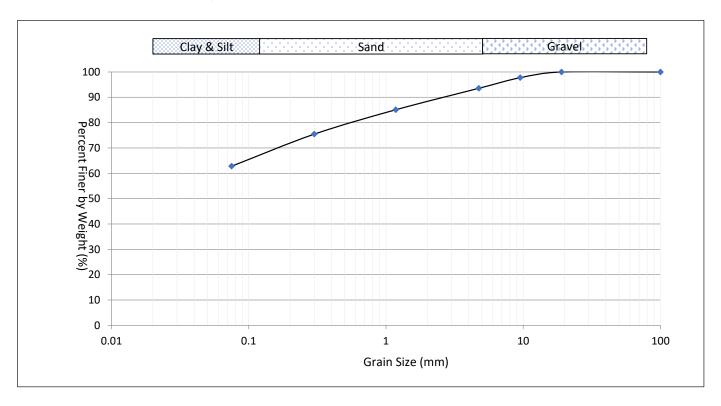
Sample ID: 21-7241-6 TH5 0.75-1.20m

Clay & Silt: 92% Sand: 7% Gravel: 1%



Sample ID: 21-7241-8 TH6 0.75-1.20m

Clay & Silt: 63% Sand: 31% Gravel: 6%





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Client: Dymon Group of Companies F.E. Job #: 21-7241B

Address: 2-1830 Walkley Road Project Name: Infiltration Tests

Ottawa, ON *Project ID:* FE-P 21-11439 K1H 8K3 *Date Sampled:* 14-Sep-2021

 Tel.:
 Date Received:
 17-Sep-2021

 Email:
 Date Reported:
 24-Sep-2021

Attn.: Location: 3855 Dundas Street East

Certificate of Analysis

Analyses	Matrix	Quantity	Date Extracted	Date Analyzed	Lab SOP	Method Reference
Hydrometer	Soil	3	N/A	22-Sep-21	Hydrometer SOP	ASTM D7928-17

Fisher Environmental Laboratories is accredited by CALA (the Canadian Association for Laboratory Accreditation Inc.) for specific parameters as required by Ontario Regulation 153/04. All analytical testing has been performed in accordance with ISO 17025 and the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act published by Ontario Ministry of the Environment.

Authorized by: Roger Lin, Ph. D., C. Chem.

ger Lin, 1 n. D., C. Cn Laboratory Manager Ronggen (Roger) Lin

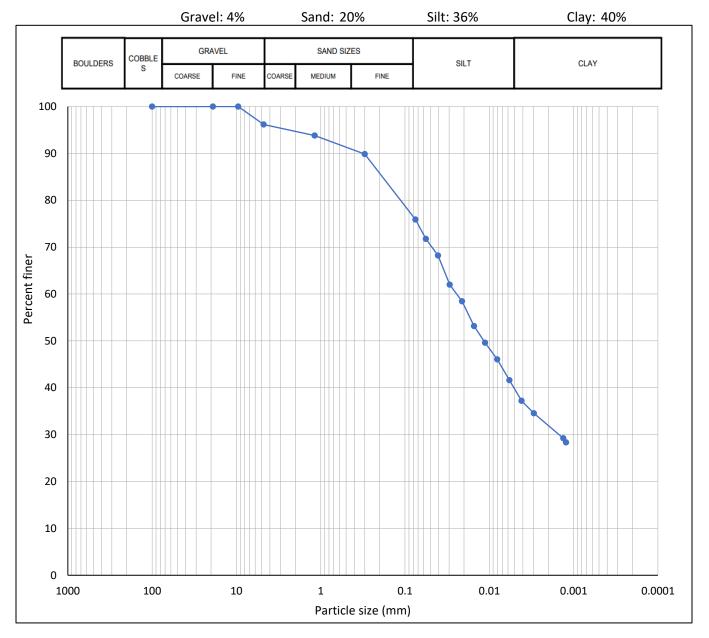
CHEMIS'

Certificate of Analysis

Analysis Requested:	Hydrometer
Sample Description:	3 Soil Sample(s)

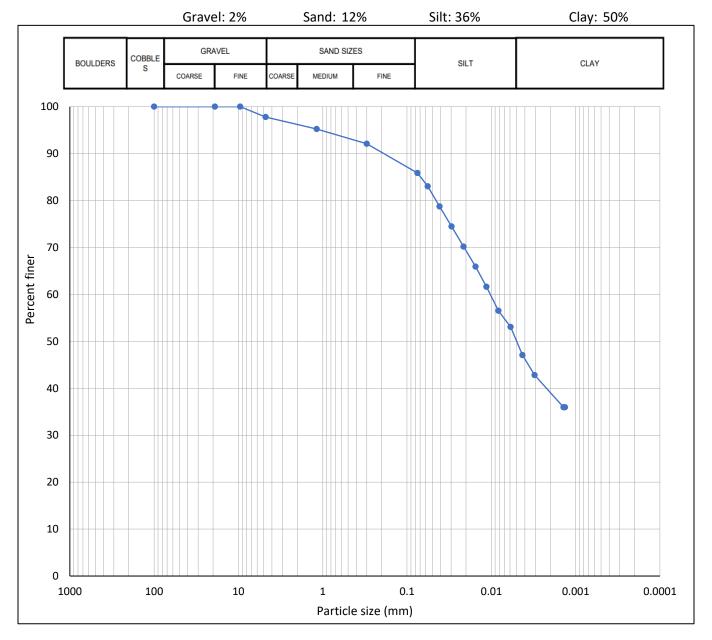
Parameter	21-7241-2	21-7241-5	21-7241-7				
	TH1	TH4	TH6				
	1.50-1.95m	0.75-1.20m	1.50-1.95m				
Grain Size (%)							
>19mm	0.0	0.0	0.0				
9.5mm-19mm	0.0	0.0	2.3				
4.75mm-9.5mm	3.8	2.2	4.2				
1.18mm-4.75mm	2.4	2.5	8.5				
300um-1.18mm	4.0	3.1	9.6				
75um-300um	14.0	6.3	12.7				
5um-75um	36	36	29				
2um-5um	8	11	10				
<2um	32	39	24				
Clay	40	50	34			_	
Silt	36	36	29				
Sand	20	12	31				
Gravel	4	2	6				

Sample ID: 21-7241-2 TH1 1.50-1.95m



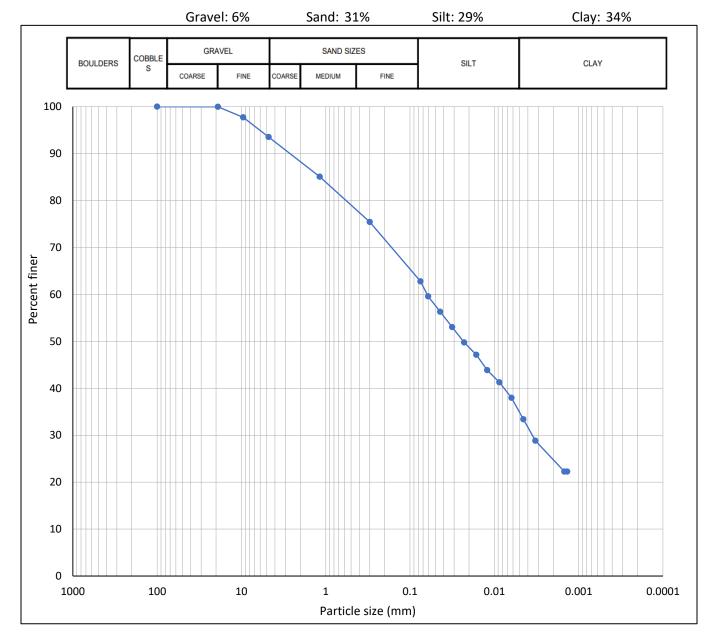
Sample	Sample ID: 21-7241-2 TH1 1.50-1.95m						
Diameter	Weight (%)	Grain Size					
>4.75mm	3.8	Gravel					
1.18mm-4.75mm	2.4	Coarse Sand					
300um-1.18mm	4.0	Medium Sand					
75um-300um	14.0	Fine Sand					
5um-75um	36	Silt					
2um-5um	8	Clay					
<2um	32	Clay					

Sample ID: 21-7241-5 TH4 0.75-1.20m

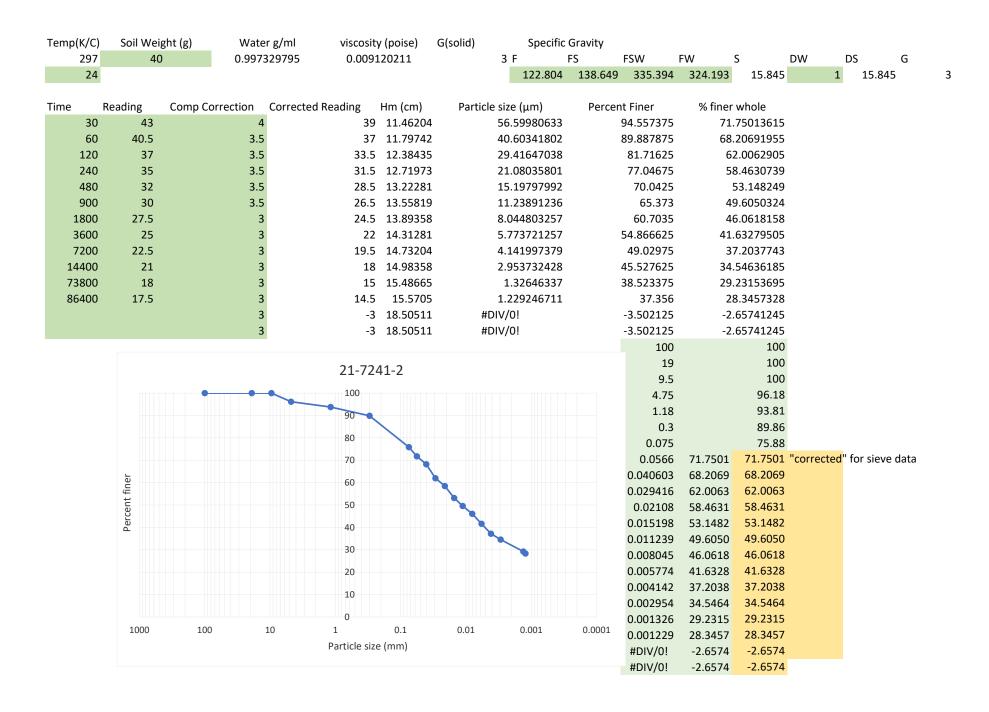


Sample ID: 21-7241-5 TH4 0.75-1.20m								
Diameter	Weight (%)	Grain Size						
>4.75mm	2.2	Gravel						
1.18mm-4.75mm	2.5	Coarse Sand						
300um-1.18mm	3.1	Medium Sand						
75um-300um	6.3	Fine Sand						
5um-75um	36	Silt						
2um-5um	11	Clay						
<2um	39	Clay						

Sample ID: 21-7241-7 TH6 1.50-1.95m



Sample	Sample ID: 21-7241-7 TH6 1.50-1.95m								
Diameter	Diameter Weight (%)								
>4.75mm	6.4	Gravel							
1.18mm-4.75mm	8.5	Coarse Sand							
300um-1.18mm	9.6	Medium Sand							
75um-300um	12.7	Fine Sand							
5um-75um	28.8	Silt							
2um-5um	10.0	Clay							
<2um	24	Clay							



Temp(K/C)	Soil Wei	ght (g)	Wate	r g/ml viscos	ity (poise)	G(solid)	Specific	Gravity						
297	49.0	06	0.9973	29795 0.00	9120211	;	2.75 F	FS	FSW	FW S		DW	DS G	
24							122.804	138.649	335.394	324.193	15.845	1	15.845	2.75
Time	Reading	Comp Corr	oction	Corrected Reading	Hm (cm)	Partic	le size (μm)	Percen	t Einor	% finer v	vholo			
30	51	Comp Com	4	_	7 10.1205		56.85661106		5.72037156)3443898			
60	48		3.5		5 10.53973		41.02794334		73478539		75431326			
120	45.5		3.5		2 10.95896		29.58248771		5.74919923		47418754			
240	43		3.5		5 11.37819		21.31432723		.76361307		19406182			
480	40.5		3.5		7 11.79742		15.34664949		.77802691		.9139361			
900	38		3.5		5 12.21665		11.40500542		.79244074		53381038			
1800	34.5		3	31	5 12.71973	3	8.228929168		.80973735		19765951			
3600	32.5		3	29	5 13.05511	1	5.894944552	61	.82126842	53.0	07355894			
7200	29		3	2	6 13.64204	4	4.261024241	54	.84144779	47.0	08138293			
14400	26.5		3	23	5 14.06127	7	3.058944762	49	.85586163	42.8	30125721			
72900	22.5		3	19	5 14.73204	4	1.391580317	41	.87892377	35.9	95305605			
79200	22.5		3		5 14.73204		1.335086642	41	.87892377	35.9	95305605			
			3		3 18.50511		DIV/0!	-2.	991351698		58075432			
			3		3 18.50511	1 #	DIV/0!	-2.	991351698	-2.56	58075432			
									100		100			
				21-7	241-5				19		100			
									9.5		100			
				100					4.75		97.79			
				90					1.18		95.25			
				80					0.3 0.075		92.11 85.85			
						X			0.075	83.0344		"corrected"	for sieve data	
				70					0.036837	78.7543	78.7543	correcteu	ioi sieve data	
	ine			60					0.029582	74.4742	74.4742			
	Percent finer			50					0.023302	70.1941	70.1941			
	erce			40					0.015347	65.9139	65.9139			
	۵			40					0.011405	61.6338	61.6338			
				30					0.008229	56.4977	56.4977			
				20					0.005895	53.0736	53.0736			
									0.004261	47.0814	47.0814			
				10					0.003059	42.8013	42.8013			
				0					0.001392	35.9531	35.9531			
	1000	100	1	1	0.1	0.01	0.001	0.0001	0.001335	35.9531	35.9531			
				Particle s	ze (mm)				#DIV/0!	-2.5681	-2.5681			
									#DIV/0!	-2.5681	-2.5681			

Temp(K/C)	Soil Wei				Specific Gravity						
297	48.	0.9973297	95 0.009120211	2.6 F			FW S	_	DW	DS G	
24					122.804 138.649	335.394	324.193	15.845	1	15.845	2.
Time F	Reading	Comp Correction Cor	rected Reading Hm (cn	n) Particle size (¡	μm) Percen	t Finer	% finer v	vhole			
30	48	4	44 10.62	358 60.92	203515 94	91440722	59.5	9675629			
60	45	3.5	41.5 11.04	281 43.92	014618 8	9.6993299	56.3	2220924			
120	42.5	3.5	39 11.46	204 31.64	025362 84	48425258	53.0	4766219			
240	40	3.5	36.5 11.88	127 22.77	'851704	26917526	49.7	7311514			
480	38	3.5	34.5 12.21	665 16.33	259395 7	5.0971134	47.1	5347751			
900	35.5	3.5	32 12.63	588 12.13	057036 69	88203608	43.8	7893046			
1800	33	3	30 12.97	127 8.690	65 697524	70997423	41.2	5929282			
3600	30.5	3	27.5 13.39	905 6.243	3768574 60	49489691	37.9	8474577			
7200	27	3	24 13.97	742 4.510	731316 53	19378866	33.	4003799			
14400	23.5	3	20.5 14.56	435 3.255	846357 45	89268041	28.8	1601403			
73800	18.5	3	15.5 15.40	281 1.47	901105 35	46252577	22.2	6691993			
86400	18.5	3	15.5 15.40	281 1.366	918837 35	46252577	22.2	6691993			
		3	-3 18.50	511 #DIV/0!	-3.1	29046392	-1.96	4728229			
		3	-3 18.50	511 #DIV/0!	-3.1	29046392	-1.96	4728229			
						100		100			
			21-7241-7			19		99.99			
			21-7241-7			9.5		97.73			
			100			4.75		93.55			
			90			1.18		85.08			
						0.3		75.44			
			80			0.075		62.79			
			70			0.060922	59.5968		corrected'	" for sieve data	l
	e		60			0.04392	56.3222	56.3222			
	ij					0.03164	53.0477	53.0477			
	Percent finer		50	The state of the s		0.022779	49.7731	49.7731			
	Perc		40	***		0.016333	47.1535	47.1535			
						0.012131	43.8789	43.8789			
			30			0.008691	41.2593	41.2593			
			20	```		0.006244	37.9847	37.9847			
			10			0.004511	33.4004	33.4004			
			10			0.003256	28.8160	28.8160			
			0			0.001479	22.2669	22.2669			
	1000	100 10	1 0.1	0.01 0	0.001 0.0001	0.001367	22.2669	22.2669			
			Particle size (mm)			#DIV/0!	-1.9647	-1.9647			
						#DIV/0!	-1.9647	-1.9647			



Revision: 2.2

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LAB JOB #	: 21-7241		(CHAI	IN OF	CU	IS1	ΓΟΙ	DY	2	258	8			Pa	geof
CLIENT INF	FORMATION			PROJEC	T INFORM	ATION							BILL	ING II	NFOR	MATION
Company Na	me: Dyner	Group		Project Name: Infultration Tests						Purchase Order #:						
COHER.			,			1 - 1110	(\uu		-212							
Address: 3	855 Du	das street a	Sort	Project ID									Verba	Author	ization	:
\ v	10.001000		•	Sampled	By: Sah	a										
	Miselseau	39		TURNAF	ROUND TIM	E (TAT)	REQ	JIRED)				Credit	Card (t	уре):	
Phone:			D	A STATE OF THE PARTY OF THE PAR	dard (5-7 working			~~~	-		Worki	ng Time:				
Fax:			sults? Y/N		Rush (48 hours)	50%		rges app		m will		ay-Friday	Credit	Card #:		
Email:		Email r	esults?(Y)N	R - Rush (24	The second secon	75%	be cons	idered re				00am- 00pm				
LAB	CUENT	S SAMPLE ID	CAMPI INC	SD - Same		100%	busines		VOIO	DEO			Expiry	CONTRACTOR AND ADDRESS OF THE PARTY OF THE P		T
					CONTAINER							ED (Che				NOTES
SAMPLE ID		SCRIPTION	DATE/TIME			(Above)	Metals	PHCs	VOCs	PAHs	PCBs	Asbestos	95	m	Hyd	ometer
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FISHER ENVIRONMENTAL

ATTN: CLIVE

15-400 ESNA PARK DRIVE

MARKHAM ON NA

Date Received: 01-SEP-20

Report Date: 14-SEP-20 12:39 (MT)

Version: FINAL

Client Phone: 905-475-7755

Certificate of Analysis

Lab Work Order #: L2497329

Project P.O. #: 3855 DUNDAS ST E

Job Reference: 20-10464

C of C Numbers:

Legal Site Desc: MISSISSAUGA

Emily Hansen Account Manager

[This report shall not be reproduced except in full without the written authority of the Laboratory.]

ADDRESS: 95 West Beaver Creek Road, Unit 1, Richmond Hill, ON L4B 1H2 Canada | Phone: +1 905 881 9887 | Fax: +1 905 881 8062

ALS CANADA LTD Part of the ALS Group An ALS Limited Company



L2497329 CONTD.... PAGE 2 of 3

Version: FINAL

ALS ENVIRONMENTAL ANALYTICAL REPORT

Sample Details/Parameters	Result	Qualifier*	D.L.	Units	Extracted	Analyzed	Batch
.2497329-1 BH102- 10-11 1/2 Sampled By: CLIENT on 28-AUG-20 Matrix: SOIL							
Physical Tests							
Grain Size Curve	SEE ATTACHED				11-SEP-20	11-SEP-20	R5222734
Particle Size							
Gravel (4.75mm - 3in.)	<1.0		1.0	%	11-SEP-20	11-SEP-20	R5222734
Medium Sand (0.425mm - 2.0mm)	9.6		1.0	%	11-SEP-20	11-SEP-20	R5222734
Coarse Sand (2.0mm - 4.75mm)	<1.0		1.0	%	11-SEP-20	11-SEP-20	R5222734
Fine Sand (0.075mm - 0.425mm)	18.0		1.0	%	11-SEP-20	11-SEP-20	R5222734
Silt (0.002mm - 0.075mm)	47.7		1.0	%	11-SEP-20	11-SEP-20	R5222734
Silt (0.005mm - 0.075mm)	37.1		1.0	%	11-SEP-20	11-SEP-20	R5222734
Clay (<0.002mm)	24.0		1.0	%	11-SEP-20	11-SEP-20	R5222734
Clay (<0.005mm)	34.6		1.0	%	11-SEP-20	11-SEP-20	R5222734
.2497329-2 BH103- 10-11 1/2 Sampled By: CLIENT on 28-AUG-20 Matrix: SOIL							
Physical Tests							
Grain Size Curve	SEE ATTACHED				11-SEP-20	11-SEP-20	R5222734
Particle Size							
Gravel (4.75mm - 3in.)	<1.0		1.0	%	11-SEP-20	11-SEP-20	R5222734
Medium Sand (0.425mm - 2.0mm)	12.9		1.0	%	11-SEP-20	11-SEP-20	R5222734
Coarse Sand (2.0mm - 4.75mm)	<1.0		1.0	%	11-SEP-20		R5222734
Fine Sand (0.075mm - 0.425mm)	21.8		1.0	%	11-SEP-20	11-SEP-20	R5222734
Silt (0.002mm - 0.075mm)	45.0		1.0	%	11-SEP-20	11-SEP-20	R5222734
Silt (0.005mm - 0.075mm)	36.1		1.0	%	11-SEP-20	11-SEP-20	
Clay (<0.002mm)	20.1		1.0	%	11-SEP-20	11-SEP-20	R5222734
Clay (<0.005mm)	28.9		1.0	%	11-SEP-20	11-SEP-20	R5222734

^{*} Refer to Referenced Information for Qualifiers (if any) and Methodology.

20-10464

L2497329 CONTD....
PAGE 3 of 3

Version: FINAL

Reference Information

Test Method References:

ALS Test Code Matrix Test Description Method Reference**

GRAIN SIZE-HYD-SK Soil Grain Size by Hydrometer ASTM D6913/D7928

Particle size curve is generated from dry sieving (particles > 2 mm), wet sieving (particles 2 mm-75 um) and hydrometer readings (particles < 75 um)

ASTM D422-63 has been withdrawn, the ASTM D6913/D7928 standard serves as the successor method.

** ALS test methods may incorporate modifications from specified reference methods to improve performance.

The last two letters of the above test code(s) indicate the laboratory that performed analytical analysis for that test. Refer to the list below:

Laboratory Definition Code	Laboratory Location
SK	ALS ENVIRONMENTAL - SASKATOON, SASKATCHEWAN, CANADA

Chain of Custody Numbers:

GLOSSARY OF REPORT TERMS

Surrogates are compounds that are similar in behaviour to target analyte(s), but that do not normally occur in environmental samples. For applicable tests, surrogates are added to samples prior to analysis as a check on recovery. In reports that display the D.L. column, laboratory objectives for surrogates are listed there.

mg/kg - milligrams per kilogram based on dry weight of sample mg/kg wwt - milligrams per kilogram based on wet weight of sample mg/kg lwt - milligrams per kilogram based on lipid weight of sample mg/L - unit of concentration based on volume, parts per million.

< - Less than.

D.L. - The reporting limit.

N/A - Result not available. Refer to qualifier code and definition for explanation.

Test results reported relate only to the samples as received by the laboratory.

UNLESS OTHERWISE STATED, ALL SAMPLES WERE RECEIVED IN ACCEPTABLE CONDITION.

Applitude results in unsigned test reports with the DRAET watermark are subject to all

Analytical results in unsigned test reports with the DRAFT watermark are subject to change, pending final QC review.



Quality Control Report

Workorder: L2497329 Report Date: 14-SEP-20 Page 1 of 2

Client: FISHER ENVIRONMENTAL

15-400 ESNA PARK DRIVE

MARKHAM ON NA

Contact: CLIVE

Test	Matrix	Reference	Result	Qualifier	Units	RPD	Limit	Analyzed
GRAIN SIZE-HYD-SK	Soil							
Batch R5222734								
WG3401674-1 DUP		L2497329-2						
Gravel (4.75mm - 3in.)		<1.0	<1.0	RPD-NA	%	N/A	5	11-SEP-20
Coarse Sand (2.0mm -	4.75mm)	<1.0	<1.0	RPD-NA	%	N/A	5	11-SEP-20
Medium Sand (0.425mr	m - 2.0mm)	12.9	12.0	J	%	1.0	5	11-SEP-20
Fine Sand (0.075mm - 0	0.425mm)	21.8	21.1	J	%	0.6	5	11-SEP-20
Silt (0.005mm - 0.075m	m)	36.1	36.4	J	%	0.4	5	11-SEP-20
Clay (<0.005mm)		28.9	30.2	J	%	1.3	5	11-SEP-20
Silt (0.002mm - 0.075m	m)	45.0	46.2	J	%	1.3	5	11-SEP-20
Clay (<0.002mm)		20.1	20.4	J	%	0.4	5	11-SEP-20
WG3401674-2 IRM		2017-PSA						
Medium Sand (0.425mr	n - 2.0mm)		8.9		%		3.9-13.9	11-SEP-20
Fine Sand (0.075mm - 0	0.425mm)		34.5		%		27.6-37.6	11-SEP-20
Silt (0.005mm - 0.075m	m)		31.1		%		25.8-35.8	11-SEP-20
Clay (<0.005mm)			25.5		%		22.7-32.7	11-SEP-20
Silt (0.002mm - 0.075m	m)		36.7		%		31.1-41.1	11-SEP-20
Clay (<0.002mm)			20.0		%		17.4-27.4	11-SEP-20

Quality Control Report

Workorder: L2497329 Report Date: 14-SEP-20 Page 2 of 2

Legend:

Limit	ALS Control Limit (Data Quality Objectives)
DUP	Duplicate
RPD	Relative Percent Difference
N/A	Not Available
LCS	Laboratory Control Sample
SRM	Standard Reference Material
MS	Matrix Spike
MSD	Matrix Spike Duplicate
ADE	Average Desorption Efficiency
MB	Method Blank
IRM	Internal Reference Material
CRM	Certified Reference Material
CCV	Continuing Calibration Verification
CVS	Calibration Verification Standard

Sample Parameter Qualifier Definitions:

LCSD Laboratory Control Sample Duplicate

Qualifier	Description
J	Duplicate results and limits are expressed in terms of absolute difference.
RPD-NA	Relative Percent Difference Not Available due to result(s) being less than detection limit.

Hold Time Exceedances:

All test results reported with this submission were conducted within ALS recommended hold times.

ALS recommended hold times may vary by province. They are assigned to meet known provincial and/or federal government requirements. In the absence of regulatory hold times, ALS establishes recommendations based on guidelines published by the US EPA, APHA Standard Methods, or Environment Canada (where available). For more information, please contact ALS.

The ALS Quality Control Report is provided to ALS clients upon request. ALS includes comprehensive QC checks with every analysis to ensure our high standards of quality are met. Each QC result has a known or expected target value, which is compared against predetermined data quality objectives to provide confidence in the accuracy of associated test results.

Please note that this report may contain QC results from anonymous Sample Duplicates and Matrix Spikes that do not originate from this Work Order.

ALS Laboratory Group

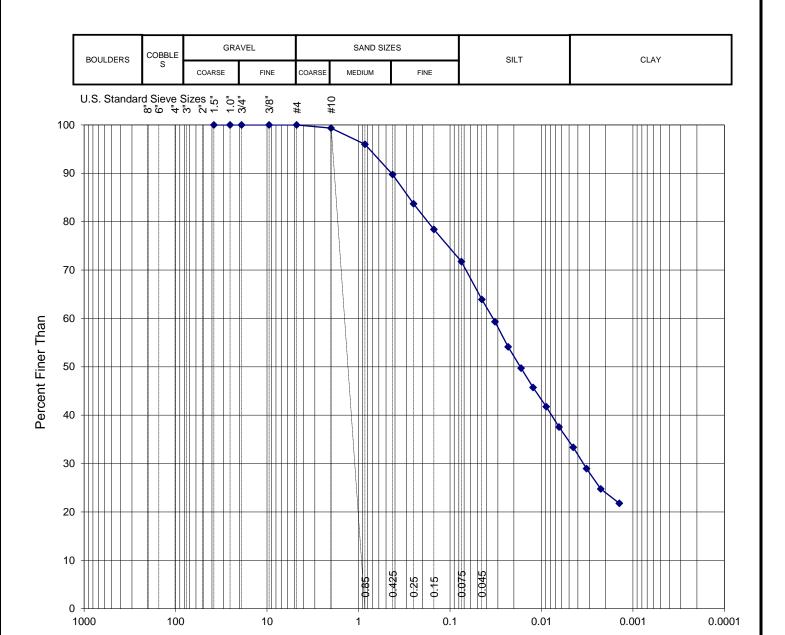
819-58th Street, Saskatoon,SK

PARTICLE SIZE DISTRIBUTION CURVE

Client Name: FISHER ENVIRONMENTAL

Project Number:

Client Sample ID BH102- 10-11 1/2
Lab Sample ID L2497329-1
Date Sample Received 01-Sep-20
Test Completion Date: 12-Sep-20
Analyst: SHCH



METHOD DESCRIPTION	SUMMARY OF RESULTS				
Method Reference: ASTM D 422 - 63 (2002)	GRAIN SIZE	WT %	DIA. RANGE (mm)		
Dispersion method: Mechanical	% GRAVEL :	<1	> 4.75		
Dispesion period: 1 minute cm/s	% COARSE SAND :	<1	2.0 - 4.75		
Soil classification system used: ASTM D422-63 Classification	% MEDIUM SAND :	9.59	0.425 - 2.0		
	% FINE SAND :	17.99	0.075 - 0.425		
DESCRIPTION OF SAND AND GRAVEL PARTICLES	% SILT :	37.14	0.075 - 0.005		
Shape: Angular	% CLAY :	34.60	< 0.005		
Hardness: Hard					

Grain Size (mm)

ALS Laboratory Group

819-58th Street, Saskatoon,SK

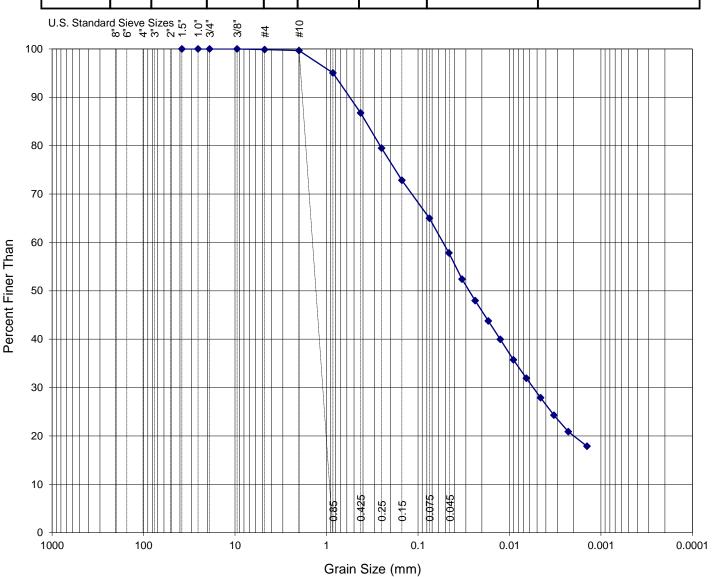
PARTICLE SIZE DISTRIBUTION CURVE

Client Name: FISHER ENVIRONMENTAL

Project Number:

Client Sample ID BH103- 10-11 1/2
Lab Sample ID L2497329-2
Date Sample Received 01-Sep-20
Test Completion Date: 12-Sep-20
Analyst: SHCH





METHOD DESCRIPTION	SUMMARY OF RESULTS				
Method Reference: ASTM D 422 - 63 (2002)	GRAIN SIZE	WT %	DIA. RANGE (mm)		
Dispersion method: Mechanical	% GRAVEL :	<1	> 4.75		
Dispesion period: 1 minute cm/s	% COARSE SAND :	<1	2.0 - 4.75		
Soil classification system used: ASTM D422-63 Classification	% MEDIUM SAND :	12.91	0.425 - 2.0		
	% FINE SAND :	21.76	0.075 - 0.425		
DESCRIPTION OF SAND AND GRAVEL PARTICLES	% SILT :	36.08	0.075 - 0.005		
Shape: Angular	% CLAY:	28.92	< 0.005		
Hardness: Hard					

Chain of Custody (COC) / Analytical Request Form

COC Number: 17 -

(ALS)	www.alsglobal.com	Canada Toll	Free: 1 800 6	68 9878	1	LZ-40.					.)		-		· ·					00	
Report To	Contact and company name below will appr			Report Format				Select Service Level Below - Contact your AM to confirm all E&P TATs (surcharges may apply)													
Company:	Fisher Enumment	\mathcal{U}	Select Report F	ormat: 🗗 🏻 [DD (DIGITAL)	Regular [R] Standard TAT if received by 3 pm - business days - no surcharges apply														
Contact:	clue		•	(QC) Report with R		□ NO	1 Business day [E - 100%]														
Phone:	2H6 605 9722		Compare Resul	ts to Criteria on Report -			Rior	3 day [P3-25%] Same Day, Weekend or Statutory holiday [E2 -200%]					2 -200%								
	Company address below will appear on the fin	al report	Select Distributi	on: E EMAIL	☐ MAIL ☐ F	FAX	_	2 day [P2-50%] (Laboratory opening fees may apply)													
Street:			Email 1 or Fax Clube					Date and Time Required for all E&P TATs: dd-mmm-yy hh:mm or tests that can not be performed according to the service level selected, you will be contacted.													
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REFER TO BACK PAGE FOR ALS LOCATIONS AND SAMPLING INFORMATION

WHITE - LABORATORY COPY YELLOW - CLIENT COPY



FISHER ENVIRONMENTAL LABORATORIES

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400 ESNA PARK DRIVE #15 MARKHAM, ONT. L3R 3K2 TEL: 905 475-7755 FAX: 905 475-7718 www.fisherenvironmental.com

Client: Dymon *F.E. Job #:* 20-5123

Address: Project Name: Geo/Hydro Investigations

Project ID: FE-P 20-10404

Ronggen (Roger) Lin

CHEMIST

Date Sampled: 19-Aug-2020 *Tel.: Date Received:* 28-Aug-2020

Email: Date Reported: 4-Sep-2020

Attn.: Location: 3855 Dundas Street, East

Mississauga, ON

Certificate of Analysis

Analyses	Matrix	Quantity	Date Extracted	Date Analyzed	Lab SOP	Method Reference
Moisture Content	Soil	5	N/A	1-Sep-20	Support Procedures F-99	Carter (1993)
Grain Size	Soil	5	N/A	3-Sep-20	Grain Size F-28	ASTM D6913-04

Fisher Environmental Laboratories is accredited by CALA (the Canadian Association for Laboratory Accreditation Inc.) for specific parameters as required by Ontario Regulation 153/04. All analytical testing has been performed in accordance with ISO 17025 and the Protocol for Analytical Methods Used in the Assessment of Properties under Part XV.1 of the Environmental Protection Act published by Ontario Ministry of the Environment.

Authorized by:

Roger Lin, Ph. D., C. Chem. Laboratory Manager

Certificate of Analysis

Analysis Requested:	Moisture Content, Grain Size
Sample Description:	5 Soil Sample(s)

	20-5123-1	20-5123-2	20-5123-3	20-5123-4	20-5123-5	
Parameter	BH101	BH101	BH101	BH101	BH101	
	1.50-1.95m	2.25-2.70m	3.00-3.45m	4.55-5.00m	0.75-1.20m	
Moisture Content (%)	12	12	9.8	10	18	

QA/QC Report

Parameter	Blank	RL	LCS	AR	Duplicate	AR
raiametei			Recovery (%)		RPD	(%)
Moisture Content (%)	< 0.1	0.1	100	70-130	4.1	0-20

<u>LEGEND:</u>

RL - Reporting Limit

LCS - Laboratory Control Sample

AR - Acceptable Range

RPD - Relative Percent Difference

Certificate of Analysis

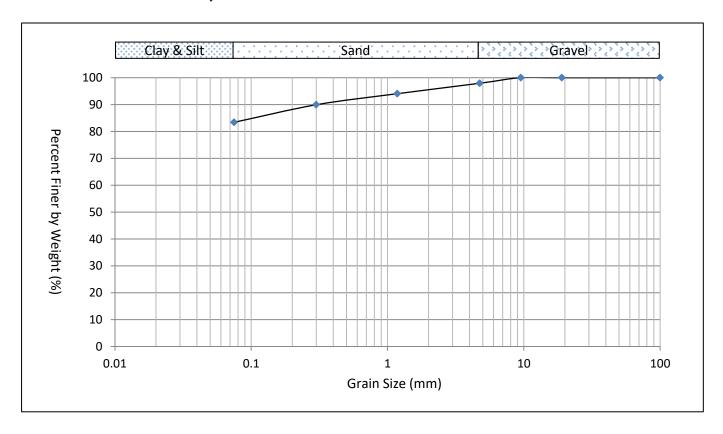
Analysis Requested:	Moisture Content, Grain Size
Sample Description:	5 Soil Sample(s)

	20-5123-1	20-5123-2	20-5123-3	20-5123-4	20-5123-5				
Parameter	BH101	BH101	BH101	BH101	BH101				
	1.50-1.95m	2.25-2.70m	3.00-3.45m	4.55-5.00m	0.75-1.20m				
Grain Size (%)									
>19mm	0.0	0.0	0.0	0.0	0.0				
9.5mm-19mm	0.0	0.0	0.0	0.0	0.0				
4.75mm-9.5mm	2.1	2.2	1.9	2.0	0.8				
1.18m-4.75mmm	3.9	5.2	7.8	9.4	1.8				
300um-1.18mm	4.1	3.3	6.1	6.6	2.1				
75um-300um	6.5	5.0	4.4	5.4	5.0				
<75um	83.4	84.3	79.7	76.6	90.3				
Clay & Silt	83	84	80	77	90				
Sand	15	14	18	21	9				
Gravel	2	2	2	2	1				

Grain Size Distribution

Sample ID: 20-5123-1 BH101 1.50-1.95m

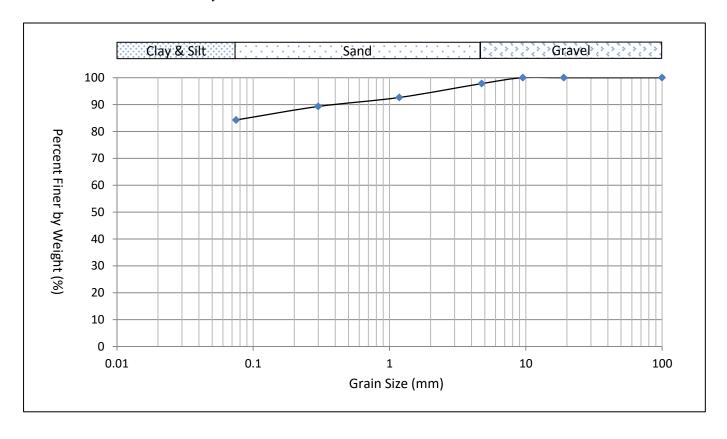
Clay & Silt: 83% Sand: 15% Gravel: 2%



Grain Size Distribution

Sample ID: 20-5123-2 BH101 2.25-2.70m

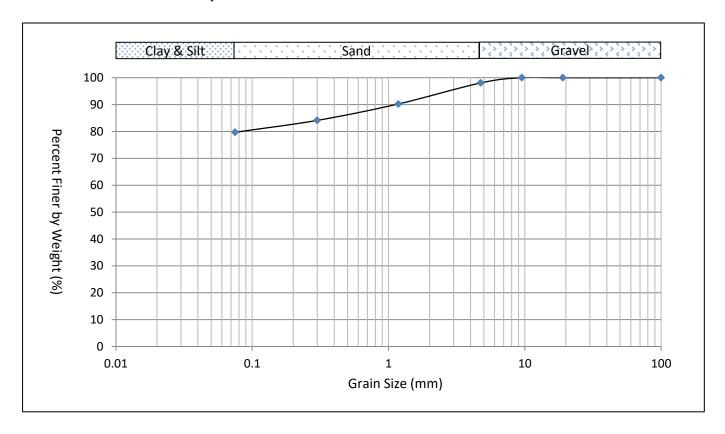
Clay & Silt: 84% Sand: 14% Gravel: 2%



Grain Size Distribution

Sample ID: 20-5123-3 BH101 3.00-3.45m

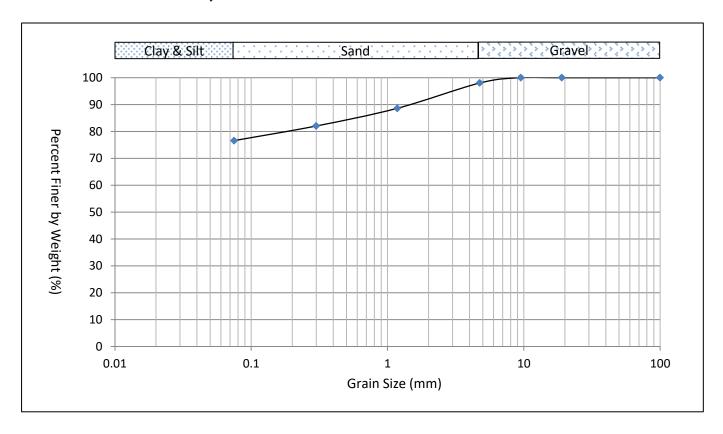
Clay & Silt: 80% Sand: 18% Gravel: 2%



Grain Size Distribution

Sample ID: 20-5123-4 BH101 4.55-5.00m

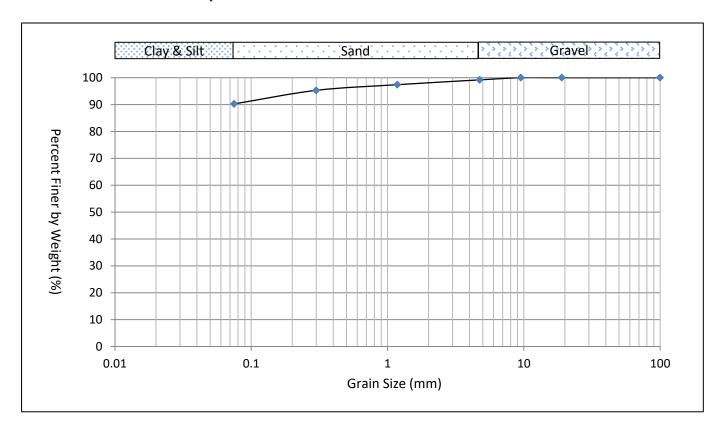
Clay & Silt: 77% Sand: 21% Gravel: 2%



Grain Size Distribution

Sample ID: 20-5123-5 BH101 0.75-1.20m

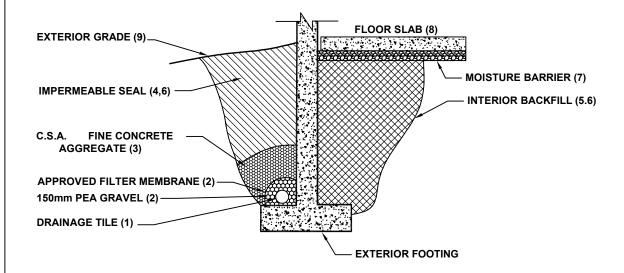
Clay & Silt: 90% Sand: 9% Gravel: 1%



APPENDIX D – DRAINAGE AND BACKFILL RECOMMENDATIONS







NOTES:

- (1) DRAINAGE TILE TO CONSIST OF 100mm (4") DIAMETER WEEPING TILE OR EQUIVALENT PERFORATED PIPE LEADING TO A POSITIVE SUMP OR OUTLET. INVERT TO BE A MINIMUM OF 150MM (6") BELOW UNDERSIDE OF FLOOR SLAB.
- (2) PEA GRAVEL-150mm (6") TOP AND SIDE OF DRAIN. IF DRAIN IS NOT ON FOOTING, PLACE 100mm (4") OF PEA GRAVEL BELOW DRAIN. 20mm (3/4") CLEAR STONE IS AN ALTERNATIVE PROVIDED IT IS SURROUNDED BY AN APPROVED FILTER FABRIC (TERRAFIX 270R OR EQUIVALENT).
- (3) C.S.A. FINE CONCRETE AGGREGATE TO ACT AS FILTER MATERIAL.
 MINIMUM 300mm (12") TOP AND SIDE OF TILE DRAIN. THIS MAY BE REPLACED
 BY AN APPROVED FILTER FABRIC AS INDICATED IN (2).
- (4) IMPERMEABLE BACKFILL SEAL COMPACTED CLAY, CLAYEY SILT OR EQUIVALENT. IF ORIGINAL SOIL IS FREE-DRAINING, SEAL MAY BE OMITTED.
- (5) THE ENTIRE FILL MAY BE ANY CLEAN NON-ORGANIC SOIL WHICH CAN BE COMPACTED TO THE SPECIFIED IN THIS CONFINED SPACE.
- (6) DO NOT USE HEAVY COMPACTION EQUIPMENT WITHIN 450mm (18") OF THE WALL. DO NOT FILL OR COMPACT WITHIN 1.8m(6') OF THE WALL UNLESS FILL IS PLACED ON BOTH SIDES SIMULTANEOUSLY.
- (7) MOISTURE BARRIER TO BE AT LEAST 200mm (8") OF COMPACTED CLEAR 20mm (3/4") STONE.
- (8) SLAB ON GRADE SHOULD NOT BE STRUCTURALLY CONNECTED TO THE WALL OR FOOTING.
- (9) EXTERIOR GRADE TO SLOPE AWAY FROM BUILDING.
- (10) THIS SYSTEM IS NOT NORMALLY REQUIRED IF THE FLOOR SLAB IS AT LEAST 300mm (1') ABOVE THE EXTERIOR GRADE.

DRAINAGE AND BACKFILL RECOMMENDATIONS

FOR SLAB ON GRADE CONSTRUCTION (NOT TO SCALE)