Dymon Group of Companies

3855 Dundas Street West

Transportation Impact Study



Dymon 3855 Dundas Street West

Transportation Impact Study

Prepared for:

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Executive Summary

CGH Transportation Inc. has been retained by Dymon Group of Companies to undertake a Transportation Impact Study, and an Access Review to support the development application for a proposed mixed-use development at 3855 Dundas Street West in the City of Mississauga.

A Transportation Impact Study (TIS) was previously prepared by others in 2018 for the proposed development at 3855 Dundas Street West. An updated TIS was submitted by Crozier in November 2020. The site design and building Gross Floor Areas (GFAs) have changed since the previous submission. This report provides an updated study with the new site stats and addresses the comments received from the City of Mississauga, Halton Region, and MTO in July 2022.

The enclosed Transportation Impact Study evaluates the impacts of the proposed development on the surrounding transportation network, recommends potential mitigation measures for the anticipated operational concerns, and provides a Transportation Demand Management Plan. The Access Review examines the compliance of the proposed access design with Halton Region's and TAC requirements.

Proposed Development:

The proposed development of 3855 Dundas Street West is located west of the Highway 403 interchange at Dundas Street East. A four-storey mixed-use building is proposed, consisting of 168,091 square feet of self-storage space, 1,048 square feet of wine cellar, 61,941 square feet of Dymon Work Refined office space, 13,255 square feet of industrial condo units, and 15,065 square feet of reception / retail area as ancillary use. A total of 190 vehicle parking spaces will be provided, including 97 at-grade and 93 underground. A total of 12 barrier-free parking spaces will be provided among them. A total of 28 bicycle parking spaces will be provided on site, including 16 short-term and 12 long-term spaces. The development will also include a 1,464 square metre (15,760 square feet) interior drive-through area which serves the self-storage customers by providing loading and overflow parking spaces.

A full-movement access on Ninth Line approximately 110 metres north of Dundas Street East (from curb return to curb return) is proposed for this site. The access will align with the existing Glen Oaks Funeral Home & Cemetery Access (herein referred to as the Glen Oaks Access) on the west side of Ninth Line. The vehicles will circulate the site via a two-way driveway surrounding the building providing access to the surface parking spaces, the drive-through / interior loading area, the exterior loading area, and the ramp to underground parking.

Analysis Process & Key Findings:

Full build-out is estimated to occur in 2026. Traffic analysis for the existing (2023), full build-out (2026), and full build-out plus five years horizons (2031) for weekday AM and PM peak periods was conducted based on City of Mississauga's Transportation Impact Study Guidelines.

Pedestrian, cycling, and transit volumes generated by the proposed development are expected to have a minimal impact on the surrounding active transportation modes and transit facilities due to the low site trip volumes and the significant available capacity in the future with the planned bicycle lanes, sidewalks, and Dundas Street BRT within the Study Area road network. This study has focused on Level of Service (LOS) analysis for auto mode.

The Existing Conditions of the Study Area road network indicates that the Ninth Line at Dundas Street East intersection is operating at capacity during the PM peak hour with several movements having v/c ratios around 1.0. This is consistent with the existing high through volumes along Dundas Street East and considered acceptable



at the intersection of two Regional roads. Signal timing optimization, involving implementing a permissive-overlap phase for northbound right-turn movement, has been proposed to mitigate the operational concern.

Growth rates for Dundas Street and Ninth Line were obtained from the City of Mississauga. The widening of Ninth Line from two lanes to four lanes north of the Ninth Line at Dundas Street East intersection, is anticipated to be completed before the 2031 horizon and will be incorporated into the 2031 Future Background analysis. The vehicle traffic analysis of the Study Area intersections of the Future Background horizons indicates multiple critical movements at the Ninth Line at Dundas Street East intersection triggered by the high through-movement volumes along Dundas Street East added by the background developments to the intersection that is already at-capacity under existing conditions. Signal optimization has been proposed as a mitigation measure for the Ninth Line at Dundas Street East intersection for 2026 and 2031 Future Background conditions. No geometric reconfigurations have been proposed due to the limits on the rights-of-way of the roads and the existing properties within the Study Area.

The proposed development is projected to generate 110 AM and 94 PM two-way vehicle trips in both 2026 and 2031 horizons, based on proxy site rates. Synchro analysis results for the 2026 and 2031 Future Total conditions show that the site-generated traffic will have a negligible impact on the operational conditions at the Ninth Line at Dundas Street East intersection as the v/c ratios and delays are projected to increase slightly from the values in Future Background conditions. Signal optimization has been proposed as a mitigation measure similar to existing and Future Background scenarios. The outbound traffic at the Site Access at Ninth Line intersection is projected to perform within permissible operational thresholds for both 2026 and 2031 Future Total scenarios. The high through volumes projected along Ninth Line have the potential to generate queuing for the site access but it is anticipated that the queue can be accommodated by the driveway on site.

The access onto Ninth Line will operate as a full movement unsignalized access. The access has been reviewed per Mississauga's TIS Guidelines and TAC Geometric Design Guide with no issues identified aside from the access throat length. The deficiency in clear throat length can be accepted for the specific use on this site as Synchro analysis result shows that there would be at most 1 to 2 vehicles queuing in the two driveways approaching the access at 95th percentile. Therefore, blockages to inbound vehicles and impacts to the adjacent street are unlikely.

No conflicts within the site have been noted as a result of the site circulation analysis for garbage and loading trucks. The driveways, curbs, and the loading bays can all accommodate the design vehicles (WB-20 and HSU).

A total of 190 parking spaces are proposed for all uses. The details of the parking and loading evaluations are provided in a separate document, the Parking Justification Letter. The recommended parking space provisions will be based on the proxy site parking demand rates.

As required in Mississauga's Transportation Impact Study Guidelines, a Transportation Demand Management (TDM) statement has been prepared. This statement documents the various TDM measures, including: transit facilities improvement, pedestrian and cycling facilities improvement, and parking reduction.

Given the minor impact of the proposed development on the surrounding Study Area road network, the proposed development application is recommended to proceed from a transportation perspective.



1 Introduction

CGH Transportation has been retained by Dymon Group of Companies to undertake the transportation impact study to support the Zoning By-law Amendment and Site Plan Application of 3855 Dundas Street West in the City of Mississauga. As such, a Transportation Impact Study, On-site Circulation Study, Access Study, and a Transportation Demand Management Plan have been developed.

1.1 Summary of Consultation with Agencies

Prior to completion of this study, the pre-study consultation checklist outlining the scope, horizons, assumptions, and Synchro parameters was submitted to the City of Mississauga. The submitted and approved checklist for this development, as well as various email correspondences, can be found in Appendix A.

1.2 Proposed Development

The proposed development is located on the northeast corner of the intersection of Ninth Line and Dundas Street East. The subject land is currently zoned as an Employment Schedule E2-93 zone, with a multitude of permitted land uses related to employment activities, including office and self-storage. The subject site is currently vacant, with a sports park to the north, a funeral home and cemetery to the west, opposite of Ninth Line, and a garden centre to the south, opposite of Dundas Street East. Figure 1 illustrates the Study Area Context.



Figure 1: Area Context Plan



The proposed development consists of a four-storey building containing a mix of Dymon self-storage and office land uses. The four-storey building will include approximately 15,616 m² (168,091 ft²) of self-storage, 97 m² (1,048 ft²) of wine cellar, 5,755 m² (61,941 ft²) of office space, 1,231 m² (13,255 ft²) of industrial condo units, and 1,400 m² (15,065 ft²) of reception and retail area. There is also a 1,464 m² (15,760 ft²) interior loading / parking area that serves the industrial condos and self-storage customers.

One full-movement vehicular site access is proposed on Ninth Line to serve the proposed Dymon development. The proposed site access is located approximately 150 metres north of the intersection of Ninth Line and Dundas Street East and will align with the Glen Oaks Access. Figure 2 illustrates the proposed site plan.

For the purposes of this report, it has been assumed that the proposed development will be built and operational by 2026. Therefore, the analysis horizons will include 2023 existing conditions, a full build-out horizon year of 2026, and a full build-out plus five years horizon year of 2031.

1.3 Study Area

The Study Area will consist of the following intersections:

- Dundas Street East at Ninth Line (Existing)
- Glen Oaks Funeral Homes & Cemetery Access at Ninth Line (Existing)
- Glen Oaks Funeral Homes & Cemetery Access / Dymon Site Access at Ninth Line (Future)







Figure 2: Site Plan

| 6 Leswyn Road Toronto Ontario Mé | a 54 1K2 | rchitect inc tel (416)256- fax (416)256- | 4440 | |
|---|--|--|-----------------------------|--|
| Design Architect | T 60R C | ACT Architecture college Street (Rear I | Inc _ane) | |
| | | Toronto ON. M60 tel: (416) 516- | 5 1B8 1949 | |
| Planning, Urban Desig MHBC 1 | n & La ^D lann Lar 7050 | ndscape Architect ing, Urban Desig ndscape Architec Weston Road, Suite Woodbridge ON. L4L | n & ture 230, 8G7 | |
| Civil Engineer C. | F. | Crozier & Associ | ates | |
| | 211 | Consulting Engin Yonge street, Suite Toronto ON. M5B tel: (416) 477- | eers 301, 1M4 3392 | |
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2 Existing Transportation Systems

2.1 Existing Study Area Road Network

Dundas Street East

Dundas Street East is a Region of Halton N2 urban arterial road with a six-lane cross-section. No cycling facilities are provided along Dundas Street East within the Study Area. A multi-use path is only provided on the south side, west of Ninth Line. The Halton Region Official Plan (2018) maintains a 50-metre right-of-way for Dundas Street East within the Study Area. A 60 km/h posted speed limit applies east of Ninth Line and a 70 km/h posted speed limit applies west of Ninth Line.

Ninth Line

Ninth Line is a Region of Halton C2 arterial road with a two-lane cross-section north of the Glen Oaks Access, and a four-lane rural cross-section south of the site access. No sidewalks are provided along Ninth Line within the Study Area. Bicycle lanes are provided along Ninth Line near the intersection of Ninth Line and Dundas Street East north of Dundas Street East, and south of Dundas Street East. The Region of Halton Region Official Plan (2018) maintains a 35-metre right-of-way for Ninth Line within the Study Area. A 60 km/h posted speed limit applies.

2.2 Existing Intersections

Dundas Street East at Ninth Line

The intersection of Dundas Street East at Ninth Line is a four-legged signalized intersection. The northbound and southbound approaches each consist of one auxiliary left-turn lane, two through lanes, and one auxiliary right-turn lane. A bicycle lane is also present between the eastern-most through lane and the right-turn lane in the northbound approach, and between the western-most through lane and the right-turn lane in the southbound approach. The eastbound and westbound approaches each consist of an auxiliary left-turn lane, three through lanes, and an auxiliary right-turn lane. Pedestrian cross walks, signal heads, and call buttons are located on all four legs of the intersection. No turn restrictions are noted at the intersection. A weight limit of 5 tonnes per axle applies to Ninth Line north of the intersection. Figure 3 illustrates the configuration of this intersection.







Glen Oaks Funeral Home & Cemetery Access at Ninth Line

The intersection of Glen Oaks Access at Ninth Line is a three-legged unsignalized intersection. South of the intersection, the northbound approach consists of two through lanes and one bicycle lane. The eastmost through lane and the bicycle lane starts tapering off north of the intersection and there is only one northbound through lane. The southbound approach consists of one through lane and the left turn storage lane extending from the Dundas Street East at Ninth Line intersection. The eastbound approach consists of one shared left turn / right turn lane. No turn restrictions are noted at the intersection. No pedestrian cross walks are provided. Figure 4 illustrates the configuration of this intersection.





2.3 Existing Accesses

There is an existing full-movement Glen Oaks Access on the west side of Ninth Line approximately 145 metres north of Dundas Street East. Multiple additional existing accesses are present along Ninth Line between the Glen Oaks access and Burnhamthorpe Road, but no access exists along Ninth Line between the Glen Oaks access and the Ninth Line at Dundas Street East intersection. As such, the traffic volumes are balanced between Study Area intersections.

2.4 Existing Pedestrian Facilities

The subjected site is connected to limited existing pedestrian facilities in its immediate surroundings as described in Section 2.1 above. No sidewalks are provided along Ninth Line north of Dundas Street East. Sidewalk is present on the east side of Ninth Line south of Dundas Street East. Multi-use trails are provided on the west side of Ninth Line south of Dundas Street East as well as the south side of Dundas Street East west of Ninth Line. No other pedestrian facilities are available along Dundas Street East within the Study Area.

Additionally, pedestrian signal heads and crosswalks are present at all approaches at the intersection of Ninth Line and Dundas Street East. Figure 5 and Figure 6 are the excerpts from maps showing the existing facilities in the surrounding area, taken from City of Mississauga Pedestrian Master Plan and Town of Oakville Active Transportation Master Plan.





Figure 5: Mississauga Pedestrian Facilities within Proximity to Study Area

Source: Excerpt from City of Mississauga Pedestrian Master Plan (2021)



Figure 6: Oakville Pedestrian Facilities within Proximity to Study Area

Source: Town of Oakville Active Transportation Master Plan (2017)



2.5 Existing Cycling Facilities

As described in Section 2.1 above, cycling facilities within the Study Area are provided as dedicated bike lanes on both sides of Ninth Line south of the Glen Oaks Access and multi-use paths on the south side of Dundas Street East west of Ninth Line. No other cycling facilities are provided within the Study Area. Figure 7 and Figure 8 illustrate the excerpts from the 2018 City of Mississauga Cycling Master Plan and Town of Oakville's online interactive map showing the existing cycling network within and surrounding the Study Area.



Source: Excerpt from City of Mississauga Cycling Master Plan (2018)





2.6 Existing Transit

The subject site has access to Oakville public transit routes nearby as shown in Figure 9. Currently, no Mississauga miWay Transit routes are operated within the Study Area.



Figure 9: Existing Study Area Oakville Transit Service

Source: Excerpt from Oakville Transit System Map (September 2021)

The existing Oakville Transit network within the Study Area is described below.



2.6.1 Route 24 – South Common

Oakville Transit Route 24 operates along Dundas Street East within the Study Area. Route 24 operates between Oakville GO Station in the west, and a loop formed by Winston Churchill Boulevard, The Collegeway, Glen Erin Drive, and Burnhamthorpe Road. Within the Study Area, Route 24 has stops located at the intersection of Ninth Line and Dundas Street East in both the eastbound and westbound directions.

Service on Route 24 is provided between 6:10 AM and 12:20 AM on the next day on weekdays, with a headway of 15 minutes. On Saturdays, Route 24 operates between 7:10 AM and 12:20 AM on the next day, with a headway of 30 minutes. Sunday and holiday service along Route 24 is provided between 8:10 AM and 8:00 PM, with a headway of 30 minutes.

2.7 Existing Operational Analysis

2.7.1 Existing Traffic Volumes

The proposed development consists of self-storage, office, and retail land uses. Among these land uses, the trip generation for the office component follows a typical AM and PM peak period pattern, while the self-storage and retail components tend to attract customers during the weekday PM peak period as well as weekend midday peak period. Although Mississauga's TIS Guidelines recommends weekday AM peak, weekday PM peak, and Weekend as typical peak periods for analysis, only the AM and PM peak periods have been selected as the analysis periods in this study given that trip generation of the office land use dominates that of the other uses at this specific site. Section 4.1.2.2 presents the Dymon proxy site trip generation data and validates this assumption as fewer trips are generated during Saturday midday peak hour than during weekday AM and PM peak hours.

Turning movement count data was collected in May 2023 at the two intersections within the Study Area: Dundas Street East at Ninth Line, and Glen Oaks Access at Ninth Line. The data was collected on the same date and there were only minimal volume imbalances (<1%). The counts were collected in the same horizon year as the 2023 existing conditions and reflect the existing traffic volumes; therefore, no modifications were applied to the counts.

Cyclist and pedestrian volumes are very low at the Study Area intersections (less than 4 pedestrians or 1 cyclist during any peak hour) and they were not included in the operational analysis as they would exert minimal impact on the transportation network.

Table 1 summarizes the intersection count dates and data sources. Appendix B includes the detailed traffic count data.

| Table 1: Traffic Count Date | | | | |
|----------------------------------|-----------|------------------------|----------------------|--|
| Intersection/Location | Data Type | Count Date | Data Source | |
| Dundas Street East at Ninth Line | TMC | Thursday, May 11, 2023 | Ontario Traffic Inc. | |
| Glen Oaks Access at Ninth Line | TMC | Thursday, May 11, 2023 | Ontario Traffic Inc. | |

Figure 10 illustrates the 2023 existing horizon traffic volumes at the Study Area intersections. A low volume of Uturns were observed at both intersections, a maximum of 3 in any direction) which would have a negligible impact on the operational analysis. U-turn volumes have been added to the left turn volumes for analysis purpose.





Before proceeding the transportation study with the 2023 turning movement counts, a comparison has been made between them and the pre-Covid19 counts from 2018 and 2019 as requested by City staff to confirm the validity of the new counts collected. Table 2 summarizes the intersection count dates and data sources. Appendix C includes the historical turning movement counts and the growth rate calculations.

| Table 2: Historical Traffic Count Date | | | | |
|--|-----------|----------------------------|----------------------|--|
| Intersection/Location | Data Type | Count Date | Data Source | |
| Dundas Street East at Ninth Line | TMC | Tuesday, February 19, 2019 | Ontario Traffic Inc. | |
| Dundas Street East at Ninth Line | TMC | Thursday, October 25, 2018 | Spectrum | |
| Glen Oaks Access at Ninth Line | TMC | Thursday, October 25, 2018 | Spectrum | |

The annual growth rate between the historical traffic volumes and the most recent 2023 counts has been calculated for the Dundas Street East at Ninth Line intersection and the Glen Oaks Access at Ninth Line intersection. The overall growth rate shows that the difference between the total volumes pass through each intersection in 2023 is within 1% of the volume passing through each intersection in the previous counts. Therefore, it is assumed that the Study Area intersection volumes have generally returned to pre-Covid19 travel patterns and the 2023 turning movement counts can be used for this study without further adjustments.

2.7.2 Existing Transportation Network and Modeling Parameters

To understand the automobile operational characteristics of the Study Area intersections, a Synchro model has been created using Trafficware's Synchro (Version 11). Analysis results from Synchro for signalized intersections are based on Highway Capacity Manual 6th v/c calculations for individual lane movements and Highway Capacity Manual 2000 v/c calculations for the overall intersection. Analysis results from Synchro for unsignalized intersections are based on Highway Capacity Manual 2000 and the average delay is used for calculations.



The configurations of Study Area intersections have been coded based on aerial and ground-level imagery as described in Section 2.2. The Glen Oaks Access is assumed to consist of a shared left-turn / right-turn lane and is stop-controlled on the driveway. Lane widths have been coded as measured from the aerial imagery. Turning-lane storage lengths have been rounded to the closest five metres. The Synchro model has been coded using the existing traffic signal timing plans provided by Halton Region which can be found in Appendix D.

The AM and PM peak hour factors (PHF) for each intersection from the 2023 turning movement counts have been used for the corresponding intersections. The values can be found in the turning movement count summary sheets in Appendix B. A summary of the peak hour factors applied at each intersection can be seen in Table 3. In all future scenarios, a default peak hour factor of 0.92 have been applied to all movements at Study Area intersections.

| Intersection | Peak Hour Factor | | |
|--|------------------|------|--|
| Intersection | AM | PM | |
| Dundas Street East at Ninth Line | 0.89 | 0.97 | |
| Glen Oaks Funeral Home & Cemetery Access at Ninth Line | 0.94 | 0.97 | |

Table 3: Peak Hour Factors Applied at Study Area Intersections

Heavy vehicle percentages (HV%) for the intersections within the Study Area have been calculated based on the 2023 turning movement counts. Appendix E contains the calculations. Pedestrian and cyclist volumes have also been taken from these counts and included in the Synchro model. The bus blockage numbers have been determined based on the existing routes, the location of the bus stops, the intersection configurations (i.e. whether the approach contains a dedicated right turn lane or a shared right / through lane), and the frequencies calculated using the current schedules provided by the transit agencies.

An ideal saturation flow of 1,900 vehicles/hour/lane has been used for all movements at each Study Area intersection in accordance with Mississauga's TIS Guidelines. The Guidelines have also prescribed the Lost Time for signalized intersections as shown in Table 4. Lost time adjustments were calculated so that the total lost times for the respective phases are equal to the values set out in the City's guidelines.

| Movement | Total Lost Time (s) | Lost time adjustments (s) | | | |
|--------------------|---------------------|---------------------------|--|--|--|
| Advanced Green | 1.0 | NA | | | |
| Back-to-back Lefts | 1.0 | EBL, WBL, NBL, SBL: -3.0 | | | |
| Main Phase | E Q | EBTR, WBTR: -1.9 | | | |
| Ividiii Filase | 5.0 | NBTR, SBTR: -2.0 | | | |

Table 4: Lost Time Adjustments

All other parameters have been coded using Mississauga's TIS Guidelines and Synchro default parameters where applicable.

2.7.3 Threshold Criteria

The performance of signalized and un-signalized intersections within the study area will follow the performance evaluation requirements included in Appendix C of Mississauga's TIS Guidelines and be assessed based on the following three criteria:

- Volume-to-capacity (V/C) ratio for signalized intersections;
- Level of Service (LOS) for un-signalized intersections; and
- 95th percentile queues, as derived from Highway Capacity Manual (HCM) outputs from Synchro.

The threshold criteria for signalized intersections are:



- V/C ratios for overall intersection operations to reach or exceed 0.85;
- V/C ratios for individual through or turning movements to reach or exceed 1.0;
- Estimated 95th percentile queue lengths for an individual movement to exceed available turning lane storage;
- Estimated 95th percentile queue lengths for through lanes to block vehicles from entering turning lanes.

Table 5 summarizes the level of service criteria for signalized intersections.

| Level of Service | Delay (Seconds/Vehicle) | V/C |
|------------------|-------------------------|--------------|
| Α | ≤10 | 0 to 0.60 |
| В | >10-20 | 0.61 to 0.70 |
| С | >20 - 35 | 0.71 to 0.80 |
| D | >35 – 55 | 0.81 to 0.90 |
| E | >55 – 80 | 0.91 to 1.00 |
| F | >80 | > 1.00 |

Table 5: Level of Service Criteria for Signalized Intersections

The threshold criteria for unsignalized intersections are:

- Level of service, based on average delay per vehicle, on individual movements to exceed LOS E;
- Estimated 95th percentile queue lengths for an individual movement to exceed available storage.

Table 6 summarizes the level of service criteria for unsignalized intersections.

| Level of Service | Average Control Delay (Second/Vehicle) |
|------------------|---|
| А | ≤10 |
| В | >10-15 |
| С | >15 – 25 |
| D | >25 – 35 |
| E | >35 – 50 |
| F | >50 |

 Table 6: Level of Service Criteria for Unsignalized Intersections

2.7.4 2023 Existing Operational Analysis

Table 7 summarizes the resulting operational analysis of the 2023 existing conditions. The critical movements as defined by the Mississauga Transportation Impact Study Guidelines are identified in red. Synchro worksheets for the 2023 existing horizon can be found in Appendix F.



| | Lana | | AM Pea | ak Hour | | PM Peak Hour | | | | | |
|-------------------------------|---|-----|--------|---------|--------|--------------|------|-------|--------|--|--|
| Intersection | Lane | LOS | V/C | Delay | Queues | LOS | V/C | Delay | Queues | | |
| | EBL | В | 0.53 | 19 | 35 | D | 0.72 | 42 | 45 | | |
| | EBT | D | 0.99 | 55 | #274 | С | 0.58 | 27 | 123 | | |
| | EBR | С | 0.41 | 27 | 39 | С | 0.20 | 22 | 12 | | |
| | WBL | D | 0.77 | 54 | #61 | С | 0.43 | 21 | 22 | | |
| | WBT | С | 0.47 | 25 | 91 | D | 0.92 | 42 | #249 | | |
| | WBR | С | 0.20 | 22 | 12 | С | 0.33 | 25 | 31 | | |
| | NBL | D | 0.61 | 41 | 42 | D | 0.63 | 35 | 66 | | |
| | NBT | D | 0.49 | 50 | 53 | E | 0.95 | 71 | #151 | | |
| | NBR | D | 0.61 | 53 | 17 | F | 1.43 | 259 | #149 | | |
| | SBL | D | 0.71 | 41 | 68 | D | 0.72 | 45 | 55 | | |
| | SBT | E | 0.80 | 56 | 99 | D | 0.43 | 46 | 52 | | |
| Nimth Line O | SBR | D | 0.48 | 48 | 16 | D | 0.46 | 48 | 16 | | |
| Ninth Line & Dundas Street | Overall | D | 0.89 | 45 | - | E | 0.90 | 60 | - | | |
| | Mitigation Measure: Signal Optimization (incl. changing the turn type of NBR to pm+over) | | | | | | | | | | |
| EdSL (Signalized) | EBL | - | - | - | - | E | 0.83 | 68 | #66 | | |
| (Signalized) | EBT | - | - | - | - | С | 0.62 | 33 | 120 | | |
| | EBR | - | - | - | - | С | 0.22 | 26 | 12 | | |
| | WBL | - | - | - | - | С | 0.47 | 25 | 24 | | |
| | WBT | - | - | - | - | D | 0.97 | 53 | #235 | | |
| | WBR | - | - | - | - | С | 0.35 | 29 | 28 | | |
| | NBL | - | - | - | - | D | 0.65 | 39 | 66 | | |
| | NBT | - | - | - | - | D | 0.77 | 49 | 130 | | |
| | NBR | - | - | - | - | E | 0.96 | 72 | #166 | | |
| | SBL | - | - | - | - | D | 0.74 | 45 | #69 | | |
| | SBT | - | - | - | - | D | 0.29 | 35 | 47 | | |
| | SBR | - | - | - | - | D | 0.31 | 36 | 18 | | |
| | Overall | - | - | - | - | D | 0.92 | 46 | - | | |
| Ninth Lina 8 | EBL/R | С | 0.04 | 24 | <1 | С | 0.16 | 19 | <1 | | |
| Glop Oaks | NBL/T | В | 0.03 | 11 | <1 | А | 0.03 | 9 | <1 | | |
| | NBT | А | - | 0.2 | - | А | - | 0.3 | - | | |
| (Unsignalized) | SBT/R | - | - | - | - | - | - | - | - | | |
| (Unsignalized) | Overall | С | - | 0.3 | - | C | - | 0.8 | - | | |
| Notes: | m indicates that the volume for the 95 th percentile queue is metred by an upstream signal # indicates the volume for the 95 th percentile cycle exceeds capacity | | | | | | | | | | |

Table 7: 2023 Existing Conditions Operational Analysis

As shown above, the unsignalized intersection of Glen Oaks Access at Ninth Line experiences no operational constraints in the existing conditions. All movements operate with good overall LOS, low delays, and acceptable queues.

In contrast, the signalized intersection of Ninth Line & Dundas Street East currently operates near capacity with overall v/c ratios above 0.85 for both the AM and PM peak hours. Long delays and queues are present on movements where over the delay exceeds the capacity. The traffic volumes show significantly different directional distributions between AM and PM peak hours. During the AM peak hour, the traffic is primarily eastbound along Dundas Street East and southbound along Ninth Line. During the PM hour the traffic is primarily westbound along Dundas Street East and northbound along Ninth Line. This is reflected in the LOS and v/c ratios. While not exceeding the critical threshold, the eastbound through movement during the AM peak have v/c ratios close to 1.00. The critical



movement during the AM peak is the westbound left movement which has insufficient lane storage for the queue. The critical movement during the PM peak is the northbound right movement with a v/c ratio of 1.43, caused by the high right turn volumes on the northbound approach. Signal optimization has been employed to reduce the v/c ratios for the PM peak hour. The green time assigned to each movement has been adjusted and the turn type of northbound right has been changed from permitted only to permitted and overlapping with the westbound left movement. This adjustment could reduce all v/c ratios below 1.00 for the intersection, although the overall v/c ratios are critical by the City Guidelines.

Given the fact that both Dundas Street East and Ninth Line are regional roads facilitating local and regional northsouth and east-west traffic, high delays for certain movements during the peak hours are expected.

3 Future Background

3.1 Future Analysis Horizons

The subject development is anticipated to be fully built-out and occupied in three years (2026). The proposed development will be constructed in a single phase; thus, the full build-out future horizon of 2026 will be studies with no interim horizons. The full build-out horizon plus five years horizon of 2031 will be evaluated to determine the long-term impact of the development on the Study Area.

3.2 Background Developments in the Area

Due to the location of the subject development being next to the border of Mississauga and Oakville, a review of both the City of Mississauga's City Planning Data Hub and the Town of Oakville's Active Development Applications website has found that the following developments proposed within proximity to 3855 Dundas Street West will contribute to the Future Background volumes in this Study:

- Ninth Line Coptic Church (Mississauga)
- Ivan Franko Homes (Mississauga)
- Mattamy Joshua Creek Phase 3 (Oakville)
- Mattamy Joshua Creek Phase 4 (Oakville)
- Dunoak and Bressa Joshua Creek Development (Oakville)
- ARGO Joshua Creek Development (Oakville)
- Redoak / Capoak Residential Development (Oakville)

These developments are expected to impact the Study Area intersections and road network and the site traffic generated by these developments will be included in the Future Background and Future Total scenarios.

3.2.1 Ninth Line Coptic Church

The Coptic Church development is located on the east side of Ninth Line, south of Burnhamthorpe Road in the City of Mississauga, north of the subject site. The site is currently bound by an existing self-storage development to the north, Highway 403 to the east, vacant land to the south, and Ninth Line to the west. The development is to be constructed in two phases, with a full build-out of Phase 1 anticipated for 2028, and a full build-out of Phase 2 anticipated for 2030. Phase 1 of the development will consist of the Coptic Church and Banquet Hall. One full-movement access will be provided on Ninth Line in Phase 1. Phase 2 of the development will consist of a community service building. Internal connections will be provided in Phase 2 to provide site access. The total site trips generated by this development were added to the 2031 Future Background volumes.

Due to the land use of the development being a church, the peak hours that were analyzed were the weekday PM, the Saturday PM, and Sunday AM, among which only the weekday PM coincides with the peak hours for the



proposed Dymon development in this study. The site is expected to generate 314 two-way trips during the weekday PM peak hour. Figure 11 illustrates the total site generated trips of Ninth Line Coptic Church.



Figure 11: Ninth Line Coptic Church Total Site Generated Trips

Source: Ninth Line Coptic Church Traffic Impact Study, RVA, 2022

3.2.2 Mattamy Joshua Creek Phase 3

The proposed residential and institutional development is located north of the Dunoak and ARGO developments, consisting of 306 townhouse units, 709 single-detached homes, and an elementary school that will accommodate approximately 700 students. Under the interim traffic scenario, before the full build-out of the Joshua Creek lands and construction of the ultimate planned road network, per the Secondary Plan, access to the proposed residential development from the surrounding road network is provided via Wheat Boom Drive, John McKay Boulevard, Meadowridge Drive and William Cutmore Boulevard. The proposed subdivision is expected to generate a total of 1,050 new two-way trips including 532 for the residential units and 518 for the elementary school during weekday AM peak hour and 806 new two-way trips including 694 for the residential units and 112 for the elementary school during the weekday PM peak hour. Figure 12 illustrates the total site generated trips of Mattamy Joshua Creek Development Phase 3.





Figure 12: Mattamy Joshua Creek Phase 3 Total Site Generated Trips



3.2.3 Mattamy Joshua Creek Phase 4 at 1429 Dundas Street East

The subject site is located north of Dundas Street and east of Meadowridge Drive and forms Phase 4 of the Joshua Creek Composite Plan. It is estimated that the proposed development will generate approximately 96 new two-way vehicle trips consisting of 24 inbound and 72 outbound trips during the AM peak hour and 129 new two-way vehicle trips consisting of 81 inbound and 48 outbound trips during the PM peak hour. Figure 13 illustrates the total site generated trips of Mattamy Joshua Creek Development Phase 4.



Figure 13: Mattamy Joshua Creek Phase 4 Site Generated Trips

Source: Mattamy (Joshua Creek) Limited Traffic Impact Study Joshua Creek Phase 4; GHD; April 2020



3.2.4 Dunoak and Bressa Development Ltd.

The Dunoak and Bressa residential subdivisions are located north of Dundas Street between Eighth Line and Ninth Line abutting the ARGO Joshua Creek development to the west and east, respectively. This study included an analysis of the 2020 and 2025 planning horizon years. The Bressa Development completed in 2021, so it has been assumed that the site trips from the Bressa Development have been captured in the 2023 turning movement counts, undertaken as part of this study. The Dunoak Residential Development will generate 568 AM and 682 PM two-way peak hour trips. Only the trips generated by the Dunoak portion were added to the 2026 and 2031 Future Background volumes. Figure 14 illustrates the total site generated trips of the Dunoak and Bressa Development. Figure 15 illustrates the total site generated trips of the Dunoak Development.





Source: Dunoak and Bressa Draft Plans Proposed Residential Developments Traffic Impact Study; GHD; July 2020



Figure 15: Dunoak Site Generated Trips

Source: Dunoak and Bressa Draft Plans Proposed Residential Developments Traffic Impact Study; GHD



3.2.5 ARGO Joshua Creek

ARGO's Joshua Creek Subdivision is located on Dundas Street west of the Bressa Development and east of the Dunoak Development. The proposed development will include 656 residential units and a Dundas Urban Core (DUC) parcel that will include a further 977 units. Phase 1 of the development includes 160 detached houses, 401 townhouses, and a small condo block with a total of 95 apartment units. Future phases will include 50 detached houses, 22 townhouses, and a small condo block with a total of 905 apartment units.

The proposed development will have a primary access that forms the fourth leg of the intersection of Meadowridge Drive at Dundas Street. Additionally, a right in / right out access is proposed into the Dundas Urban Core portion of the development. This development will also have connections to both adjacent proposed developments (Dunoak to the west and Bressa to the east).

Phase 1 is projected to generate 272 AM and 336 PM peak hour two-way auto trips during the 2024 horizon. As a result of projected changes in mode share, Phase 1 is anticipated to generate 251 AM and 311 PM peak hour vehicle trips in 2029. Future phases, with anticipated build out in 2029, are expected to generate an additional 290 AM and 363 PM peak hour vehicle trips. Figure 16 and Figure 17 illustrate the site generated trips of ARGO Joshua Creek development in 2024 and 2029, respectively.



Source: ARGO Joshua Creek TIS; CGH Transportation; 2021







Source: ARGO Joshua Creek TIS; CGH Transportation; 2021

3.2.6 Redoak / Capoak Residential Development

The subject development is located in the northeast quadrant of the intersection of Dundas Street East and Eighth Line Road and west of the Dunoak Development, in the Town of Oakville. Outside the Dundas Street Urban Core blocks, the proposed development consists of 116 single family detached units, and 489 multifamily units which can be broken down to 457 townhouse units, 8 live-work units, and an additional 24 residential units. Within the Dundas Street Urban Core blocks, the proposed development consists of 542 condominium apartment units and 36 back-to-back townhouse units.

Access is proposed to Dundas Street via a right-in/out driveway, and through adjacent draft plans via the future extension of Prince Michael Drive north of Dundas Street to the east and a connection to Eighth Line to the west. The proposed Development Plan is estimated to generate approximately 471 new two-way vehicle trips during the AM peak hour consisting of 356 inbound and 115 outbound trips. During the PM peak hour, it is expected to generate 584 new two-way vehicle trips consisting of 363 inbound and 221 outbound trips. Figure 18 illustrates the total site generated trips of Redoak / Capoak Residential Development.





Source: Proposed Redoak/Capoak Residential Development Traffic Impact Study; GHD; April 2021

3.2.7 Ivan Franko Homes – 3058 Winston Churchill Boulevard

There is an assisted living / retirement home "Ivan Franko Homes" located at 3058 Winston Churchill Boulevard. A long-term care facility with 160 beds will be added to the site. The proposed development is expected to generate a total of 34 two-way trips consisting of 22 inbound and 12 outbound during weekday AM peak hour and 67 two-way trips consisting of 26 inbound and 41 outbound during weekday PM peak hour. Figure 19 illustrates the site trip generated by 3058 Winston Churchill Boulevard.





Figure 19: Ivan Franko Homes Site Generated Trips



3.2.8 Background Development Trips Summary

The total AM and PM peak hour trips generated by the background developments by the 2026 and 2031 horizons are summarized in Table 8 and Table 9.



| Land Lisa | A | M Peak Ho | ur | PM Peak Hour | | | |
|-------------------------------|-----|-----------|-------|--------------|-----|-------|--|
| Land Ose | In | Out | Total | In | Out | Total | |
| Mattamy Joshua Creek Phase 3 | 423 | 627 | 1,050 | 481 | 325 | 806 | |
| Mattamy Joshua Creek Phase 4 | 24 | 72 | 96 | 81 | 48 | 129 | |
| Dunoak and Bressa Development | 137 | 431 | 568 | 418 | 264 | 682 | |
| ARGO Joshua Creek | 66 | 206 | 272 | 211 | 126 | 336 | |
| Redoak / Capoak Residential | 115 | 356 | 471 | 363 | 221 | 584 | |
| 2026 Total Trips | 765 | 1,692 | 2,457 | 1,554 | 984 | 2,537 | |

Table 8: Background Developments Site Trips By 2026 Summary

A total of 2,457 AM and 2,537 PM peak hour two-way vehicle trips will be generated by the ten background developments included in this Study by the 2026 horizon.

| Land Has | Α | M Peak Hou | Jr | PM Peak Hour | | | |
|--------------------------------------|-----|------------|-------|--------------|-------|-------|--|
| Land Use | In | Out | Total | In | Out | Total | |
| Mattamy Joshua Creek Phase 3 | 423 | 627 | 1,050 | 481 | 325 | 806 | |
| Mattamy Joshua Creek Phase 4 | 24 | 72 | 96 | 81 | 48 | 129 | |
| Dunoak and Bressa Development | 137 | 431 | 568 | 418 | 264 | 682 | |
| ARGO Joshua Creek | 136 | 406 | 541 | 416 | 256 | 674 | |
| Redoak / Capoak Residential | 115 | 356 | 471 | 363 | 221 | 584 | |
| Ninth Line Coptic Church | - | - | - | 144 | 170 | 314 | |
| Ivan Franko Homes | 22 | 12 | 34 | 26 | 41 | 67 | |
| 2031 Total Trips | 857 | 1,904 | 2,760 | 1,929 | 1,325 | 3,256 | |

Table 9: Background Developments Site Trips By 2031 Summary Page 2031 Summary

With the completion of later phases of ARGO Joshua Creek and the two Mississauga sites, a total of 2,760 AM and 3,256 PM peak hour two-way vehicle trips will be generated by all the background developments combined by the 2031 horizon.

3.3 Planned Study Area Improvements

The official plans and transportation master plans from the City of Mississauga, the Town of Oakville, and the Halton Region have been reviewed for planned transportation infrastructure improvements within the Study Area.

The major road network improvement that is anticipated to be complete within the study horizons is the Ninth Line widening north of Dundas Street East. Pedestrian and cycling facilities will be constructed on each side of the regional roads within the Study Area which will strength the connectivity of the site to active transportation modes.

3.3.1 Dundas Bus Rapid Transit

Metrolinx's 2041 Regional Transportation Plan identifies rapid transit along Dundas Street through Mississauga as a key link in an integrated, multi-modal, and regional transit system. Metrolinx and the City of Mississauga are currently undertaking a Transit Project Assessment Process (TPAP) and the Preliminary Design and Preliminary Design Business Case for the proposed Dundas Bus Rapid Transit Project. If approved, the proposed BRT route would be implemented along Dundas Street from Kipling TTC Station and Transit Hub in the City of Toronto, to Highway 6 in the City of Hamilton, passing through the City of Mississauga, the Town of Oakville, and the City of Burlington. Within the Study Area, the proposed BRT route would be located along Dundas Street East. Along



Dundas Street corridor, the curb lanes include provisions to accommodate potential HOV or bus-only lanes in Halton Region.

Details such as the cross-section design and its impact on the right-of-way of Dundas Street, and proposed transit stop locations for the section of the BRT within the Study Area have not been determined. No anticipated completion date is available. Therefore, the direct impact from the Dundas BRT has not been considered for this study.

3.3.2 City of Mississauga Official Plan (2010)

Schedule 6 of the City of Mississauga Official Plan (2010) outlines Dundas Street, within the Study Area, as an intensification corridor. A copy of Schedule 6 can be found in Appendix G.

3.3.3 City of Mississauga Transportation Master Plan (2019)

The City of Mississauga Transportation Master Plan (2019) has been reviewed, and it has been determined that no improvements or significant changes are planned or proposed for the transportation network surrounding the proposed development.

3.3.4 City of Mississauga Pedestrian Master Plan (2021)

Figure 7 of the City of Mississauga Pedestrian Master Plan (2021) outlines the existing gaps within the Mississauga pedestrian network, in which no sidewalk is present on one or both sides of a street. The gaps within the pedestrian network are proposed to be filled through private development and capital projects. As discussed above in Section 2.4, within the Study Area road network, sidewalks or multi-use paths are missing along both sides of Ninth Line north of Dundas Street East, along both sides of Dundas Street East, east of Ninth Line, and along the north side of Dundas Street East west of Ninth Line.

Figure 7 of the City of Mississauga Pedestrian Master Plan (2021) illustrates a boulevard multi-use path along Ninth Line and Dundas Street within the Study Area A copy of the figure can be found in Appendix H. Figure 10 of the City of Mississauga Pedestrian Master Plan (2021) outlines the pedestrian network priority level for implementation of pedestrian facilities on City of Mississauga roads. Within the Study Area, Dundas Street has been designated a low prioritization score. The priority level of pedestrian facility implementation is not discussed for Ninth Line south of Dundas Street which is under the jurisdiction of the Region of Halton. A copy of Figure 10 of the City of Mississauga Pedestrian Master Plan (2021) can also be found in Appendix H. No timeline for the implementation of the proposed pedestrian facilities is noted within the plan.

3.3.5 City of Mississauga Cycling Master Plan (2018)

Figure 15 of the City of Mississauga Cycling Master Plan (2018) outlines the proposed cycling facilities for the City of Mississauga. Within the Study Area, cycling facilities are proposed as multi-use paths along Ninth Line and Dundas Street. This remains consistent with the proposed multi-use paths within the Study Area road network discussed above in Section 3.3.4. A copy of Figure 15 of the City of Mississauga Cycling Master Plan (2018) can be found in Appendix I. The City of Mississauga Cycling Master Plan (2018) identifies the proposed cycling facilities within the Study Area road network as part of the "Primary On-Road Network". No timeline for the proposed cycling facilities within the Study Area is noted within the plan.

3.3.6 Town of Oakville Active Transportation Master Plan (2017)

The Town of Oakville Active Transportation Master Plan (2017) has been reviewed, and it has been determined that no improvements or significant changes are planned or proposed for the active transportation network within the Study Area.



3.3.7 Halton Region Transportation Master Plan 2031 (2011)

Figure 7.2 of the Halton Region Transportation Master Plan 2031 (2011) outlines the 2031 transportation system within the Region of Halton. Within the Study Area, the Halton Region Transportation Master Plan 2031 (2011) proposes widening Ninth Line from the existing two-lane rural cross-section to a four-lane C2 Urban cross-section. The implementation of this widening is expected to begin in 2024 and is anticipated to be complete by 2031. As Ninth Line already has a four-lane cross-section south of Dundas Street East and a localized widening is already in place at the Dundas Street East at Ninth Line intersection, the widening will be applied to the segment of Ninth Line north of the Dundas Street East at Ninth Line intersection in this study. Appendix J includes the preliminary design drawings showing the cross sections of Ninth Line after widening and configurations of intersections along Ninth Line.

Dundas Street is currently a three-lane road in each direction, with all lanes operating as general-purpose traffic lanes with no vehicle restrictions. It has been indicated by Halton Region Staff that it is anticipated that the outer traffic lane on the curbside would be converted to a high occupancy vehicle (HOV) lane, restricting single occupant vehicles from using this lane. There is a potential for the HOV lanes to become transit lanes when the Dundas BRT is constructed. However, the HOV lanes have not been modelled in the Synchro models for this study, as the initial reduction of capacity due to the HOV lanes would not adequately serve projected traffic volumes. Although in the long run the modal split for single-occupant private vehicles will decrease, the current level of traffic, which is already at capacity in the existing conditions, does not support the HOV implementation as examined in the Synchro analysis.

Bike lanes and boulevard multi-use trails are planned to be added along Ninth Line while boulevard multi-use trails are planned to be added along Dundas Street. Halton Region has not provided a detailed timeline for these active transportation improvement projects.

3.4 Background Growth Rate

The background growth rate considers the growth in traffic volumes on streets within the Study Area due to a multitude of factors affected by land use planning and large-scale transportation projects (i.e., the overall population change in the Region and the improvement of the public transit and active transportation systems).

A Transportation Impact Study for 3855 Dundas Street West dated November 2018 was previously completed by others with growth rates on Dundas Street West and Ninth Line derived from City's forecasting models for the weekday AM and PM peak periods provided by the City staff. Appendix K includes the related section from the previous report dated 2018. The City of Mississauga transportation model has been updated since 2018. City staff have provided updated values along Dundas Street and Ninth Line north of Dundas Street for the time horizons of this study.

Table 10 below outlines the compound annual growth rates provided by City staff. The growth rates on Ninth Line are higher than the typical 2%, reflecting the future widening of Ninth Line north of Dundas Street West. Growth on Dundas Street East is lower as some trips will shift to other corridors such as the newly constructed William Halton Parkway and the future widening of Upper Middle Road. Compared to the 2018 report, the growth rates on Dundas Street have increased slightly and the growth rates on Ninth Line have decreased.



| Peak Hour | | From Existi | ing to 2026 | | From 2026 to 2031 | | | | |
|-----------|---------------------------|-------------|-------------|------|---------------------------|------|------------|------|--|
| | Dundas Street East | | Ninth Line | | Dundas Street East | | Ninth Line | | |
| | EB | WB | NB | SB | EB | WB | NB | SB | |
| AM | 0.5% | 1.5% | 4.5% | 3.5% | 0.5% | 1.5% | 4.5% | 3.5% | |
| PM | 1.5% | 1.5% | 3.0% | 4.5% | 1.5% | 1.5% | 3.0% | 4.5% | |

Table 10: Compounded Annual Growth Rates

The growth rates outlined above were applied to all movements on the respective roadways, with the exception of the turning movements on Ninth Line. The compounded growth rates between 3-4.5% were applied to through movements only on Ninth Line for the corresponding directions. An industry standard compounded annual growth rate of 2% was applied to the turning movements on Ninth Line.

3.5 Future Background Traffic Volumes

Using the background growth rate established above, the 2023 turning movement volumes were grown to reflect the 2026 and 2031 Future Background traffic volumes. Additionally, the six background developments discussed in Section 3.2, have been directly considered in the background conditions. The 2026 Future Background traffic is illustrated in Figure 20 and the 2031 Future Background traffic is illustrated in Figure 21.









3.6 Future Background Operational Analysis

3.6.1 Future Conditions Modeling Parameters

Parameters applied in the Synchro model have followed the suggestions in Appendix D of the Mississauga's TIS Guidelines. At the signalized intersection of Dundas Street East at Ninth Line, the minimum green time has been set to 10 seconds for through movements and 5 seconds for left-turn phases. The cycle lengths have been determined for each scenario based on the volumes, with the intent to optimize the overall LOS and delay for the intersection, while adhering to the maximum of 160 seconds. The amber and all-red clearance times have been included for every phase and generally kept the values from the existing signal timing plan. The parameters for the pedestrian phases are consistent with the existing signal timing plan. The same saturation flow rates and lost times as those in existing models are also carried forward. A default peak hour factor of 0.92 have been applied to all movements at Study Area intersections.

3.6.2 2026 Future Background Conditions

3.6.2.1 2026 Future Background Intersection Design

As discussed in Section 3.3.7, no changes will be made to the intersections in the 2026 horizon. The transportation network from the 2023 existing conditions has been used for 2026 Future Background conditions.



3.6.2.2 2026 Future Background Operational Analysis

The 2026 Future Background intersection volumes have been analysed to allow for a comparison between the future volumes with and without the proposed development. Table 11 summarizes the operational analysis for the 2026 Future Background conditions.

The parameters used to assess the existing conditions operational analysis discussed in Section 2.7.1 have been applied to future conditions as well. The intersections have been analyzed based on the identified signal control and intersection configurations in Section 3.6.2.1. 2026 Future Background Synchro worksheets are included in Appendix L.

| | Lana | | AM Pea | ak Hour | | PM Peak Hour | | | | | | |
|----------------------|---|-----------------------------|--|---|-----------------------------|----------------------------|--------------|------------|--------|--|--|--|
| Intersection | Lane | LOS | V/C | Delay | Queues | LOS | V/C | Delay | Queues | | | |
| | EBL | С | 0.61 | 24 | 45 | D | 0.74 | 49 | 51 | | | |
| | EBT | F | 1.34 | 194 | #399 | D | 0.84 | 37 | #216 | | | |
| | EBR | С | 0.60 | 35 | 71 | С | 0.33 | 25 | 28 | | | |
| | WBL | D | 0.78 | 54 | #65 | С | 0.62 | 33 | 35 | | | |
| | WBT | С | 0.61 | 30 | 119 | F | 1.38 | 212 | #423 | | | |
| | WBR | С | 0.21 | 24 | 12 | С | 0.39 | 28 | 46 | | | |
| | NBL | D | 0.71 | 44 | #67 | F | 1.04 | 95 | #121 | | | |
| | NBT | D | 0.49 | 47 | 59 | F | 1.10 | 113 | #188 | | | |
| | NBR | D | 0.57 | 50 | 18 | F | 1.60 | 334 | #192 | | | |
| | SBL | D | 0.70 | 39 | 71 | D | 0.78 | 49 | #69 | | | |
| | SBT | E | 0.84 | 58 | 109 | D | 0.50 | 47 | 63 | | | |
| | SBR | D | 0.48 | 48 | 17 | D | 0.50 | 47 | 17 | | | |
| Ninth Line & | Overall | F | 1.06 | 104 | - | F | 1.20 | 132 | - | | | |
| East | Signal Optimization (incl. pm+over NBR in the PM) | | | | | | | | | | | |
| EdSL (Signalized) | EBL | С | 0.62 | 24 | 45 | F | 1.29 | 225 | #98 | | | |
| (Signalized) | EBT | F | 1.15 | 109 | #403 | D | 0.84 | 42 | #223 | | | |
| | EBR | С | 0.52 | 28 | 67 | С | 0.33 | 29 | 34 | | | |
| | WBL | F | 1.17 | 173 | #105 | D | 0.69 | 40 | 42 | | | |
| | WBT | С | 0.56 | 29 | 129 | F | 1.25 | 158 | #429 | | | |
| | WBR | С | 0.20 | 23 | 13 | С | 0.35 | 27 | 42 | | | |
| | NBL | E | 0.83 | 61 | #78 | Е | 0.95 | 71 | #135 | | | |
| | NBT | D | 0.39 | 45 | 58 | E | 0.95 | 74 | #190 | | | |
| | NBR | D | 0.46 | 47 | 32 | F | 1.41 | 137 | #224 | | | |
| | SBL | E | 0.88 | 75 | 76 | E | 0.89 | 76 | #94 | | | |
| | SBT | E | 0.80 | 59 | 112 | E | 0.53 | 55 | 73 | | | |
| | SBR | D | 0.46 | 51 | 17 | E | 0.53 | 56 | 32 | | | |
| | Overall | E | 1.06 | 73 | - | F | 1.18 | 99 | - | | | |
| Ninth Lina 8 | EBL/R | D | 0.05 | 31 | 1 | С | 0.20 | 22 | 5 | | | |
| Glan Oaks | NBL | А | 0.04 | 2 | <1 | А | 0.03 | 1 | <1 | | | |
| | NBT | - | 0.29 | 0 | 0 | - | 0.55 | 0 | 0 | | | |
| (Unsignalized) | SBT/R | - | 0.68 | 0 | 0 | - | 0.47 | 0 | 0 | | | |
| (Shisighalized) | Overall | С | - | 0.3 | - | В | - | 0.7 | - | | | |
| Notes: | m indicates # indicates | s that the vo the volume | olume for th for the 95 th | e 95 th perce ¹ percentile | entile queue cycle excee | is metred l ds capacity | oy an upstre | eam signal | | | | |

Table 11: 2026 Future Background Conditions Operational Analysis



As shown above, with the addition of background growth to reflect the 2026 horizon as well as traffic generated from surrounding developments, the Study Area intersections operate worse than existing conditions during both AM peak hour and PM peak hour. Critical movements are identified in red.

The Glen Oaks at Ninth Line intersection is projected to operate within possible operational thresholds despite the growth along Ninth Line. However, the Dundas Street East at Ninth Line will likely experience operational constraints with long delays and queues especially in the PM peak hour 2026 Future Background horizon.

At the Dundas Street East at Ninth Line intersection, operational constraints are projected on the eastbound through movement during the AM peak with a v/c ratio of 1.34 and a 400-metre queue, reflecting the high projected volumes on this movement. Optimizing the signal timing plan is projected to reduce the overall delay, but not the v/c ratios. To reduce the v/c ratios and delays on the eastbound through movement, the conflicting movement of westbound left was assigned a shorter green time which caused operational constraints at that movement as a result.

During the PM peak, the volumes are similar to the AM peak pattern with the heaviest direction of flow reversed. The critical movements are westbound through, northbound left, northbound through, and northbound right. The queues on the northbound left and northbound right movements have exceeded the available storage lengths. Signal optimizations have been applied to the PM peak hour signal timings to optimize the overall delays, yet similar to the situation encountered in the AM conditions, the improvements are limited at this intersection. The operational constraints on the northbound left and northbound through movements have been mitigated, but the eastbound left movement opposite to the critical movement of westbound through does not have enough residual capacity to release some of its green time to accommodate the volumes at the critical movements and would become congested. While the delay on the westbound through movement is reduced, the delay on the eastbound left significantly increases. The northbound right movement has been modelled with permissive and overlap phases. As it overlaps with the westbound left movement, the green time assigned to this movement is restricted by that of the westbound left movement, which cannot be further increased without affecting the operational conditions at the eastbound through movement.

Unlike the eastbound through movement during the AM peak hour which has sufficient spacing between the Ninth Line intersection and the next intersection to the west, William Cutmore Boulevard, the 95th percentile queue at westbound through movement is about 423 metres long during the PM peak hour while the Highway 403 southbound off ramp is located approximately 320 metres east of the Dundas Street East at Ninth Line intersection. The queues from the Ninth Line intersection could potentially spill back to the highway off ramp and block vehicles exiting the highway, causing queues on the off ramp.

Given the high projected Future Background volumes along Dundas Street, it is expected that the current configuration of the road cannot efficiently accommodate the traffic at the Dundas Street at Ninth Line intersection. It is unlikely that the projected level of growth will occur along this corridor as the planned completion of the parallel William Halton Parkway is expected to be completed by 2027 and some of this east-west traffic will divert away from Dundas Street which should improve intersection operations.

Additionally, the potential conversion of the curbside lane to an HOV/BRT lane would reduce the capacity along Dundas Street. The HOV lane has not been modelled in this study as the reduction in capacity would further exacerbate existing operational issues. It is recommended that the Region monitor changes in traffic volumes along the corridor and determine the appropriate timing of implementation of the HOV lane. The introduction of the HOV and future BRT service will help increase the modal share for non-auto modes from existing levels and decrease the vehicle volumes along the corridor, which will offset the impact of reduced capacity due to the


HOV/BRT lane and improve the operation of intersections along Dundas Street. No geometric improvements are recommended at this intersection as part of this study, due to property constraints.

3.6.3 2031 Future Background Conditions

3.6.3.1 2031 Future Background Intersection Design

For 2031 Future Background conditions, Ninth Line will be widened to a four-lane road north of the intersection with Dundas Street East. The 2031 Future Background Synchro model is based on the preliminary design, included in Appendix J. The Ninth Line at Glen Oaks Access intersection is assumed to have the following configuration:

- northbound approach consists of an auxiliary left turn lane with a storage length of approximately 15 metres and two through lanes;
- southbound approach consists of a through lane and a shared through / right-turn lane;
- and eastbound approach stays the same as the existing conditions with a shared left turn / right turn lane.

3.6.3.2 2031 Future Background Operational Analysis

The 2031 Future Background intersection volumes have been analysed to allow for a comparison between the future volumes with and without the proposed development. Table 12 summarizes the operational analysis results for the 2031 Future Background conditions.

The parameters used to assess the existing conditions operational analysis are the same as the 2026 Future Background conditions. The signal timing optimization measures have been incorporated into the 2031 Future Background network. 2031 Future Background Synchro worksheets are included in Appendix M.

| Interestion | Lana | | AM Pea | ak Hour | | | PM Pea | ak Hour | |
|----------------------|--|-----------------------------|--|-------------------------------|-----------------------------|-------------------------|--|------------|--------|
| Intersection | Lane | LOS | V/C | Delay | Queues | LOS | V/C | Delay | Queues |
| | EBL | С | 0.71 | 33 | 58 | F | 1.39 | 264 | #107 |
| | IntersectionLaneAM Peak HourPM PeakLOSV/CDelayQueuesLOSV/CEBLC0.713358F1.39EBTF1.29175#445D0.94EBRC0.583475C0.36WBLF1.30223#118D0.72WBTD0.6636153F1.37WBRC0.232718C0.38Nundas StreetNBLE0.8460#99F1.07NBTD0.494879E0.98NBRD0.514944F1.11SBLE0.9073#108F1.38SBTE0.9375#162E0.74SBRD0.505331E0.65OverallF1.14104-F1.38Glen Oaks Access (Unsignalized)B0.05131B0.04Nate:m indicates that the volume for the 95 th percetile queue is metred by an upstrear | 51 | #263 | | | | | | |
| | EBR | С | 0.58 | 34 | 75 | С | 0.36 | 30 | 36 |
| | WBL | F | 1.30 | 223 | #118 | D | 0.72 | 52 | 47 |
| | WBT | D | 0.66 | 36 | 153 | F | 1.37 0.38 | 212 | #493 |
| Ninth Line & | WBR | С | 0.23 | 27 | 18 | С | 0.38 | 28 | 48 |
| East (Signalized) | NBL | E | 0.84 | 60 | #99 | F | 1.07 | 102 | #190 |
| | NBT | D | 0.49 | 48 | 79 | E | 0.98 | 75 | #219 |
| (Signalized) | NBR | D | 0.51 | 49 | 44 | F | 1.11 | 119 | #258 |
| | SBL | E | 0.90 | 73 | #108 | F | 1.38 | 257 | #128 |
| | SBT | E | 0.93 | 75 | #162 | E | DS V/C Delay F 1.39 264 D 0.94 51 C 0.36 30 D 0.72 52 F 1.37 212 C 0.38 28 F 1.07 102 E 0.98 75 F 1.11 119 F 1.38 257 E 0.65 64 F 1.38 126 C 0.20 22 B 0.04 10 - 0.48 0 - 0.39 0 A - 0.5 | 64 | 95 |
| | SBR | D | 0.50 | 53 | 31 | E | 0.65 | 64 | 40 |
| | Overall | F | 1.14 | 104 | - | F | 1.38 | 126 | - |
| | EBL/R | Е | 0.06 | 36 | 1 | С | 0.20 | 22 | 5 |
| Ninth Line & | NBL | В | 0.05 | 13 | 1 | В | 0.04 | 10 | <1 |
| | NBT | - | 0.27 | 0 | 0 | - | 0.48 | 0 | 0 |
| (Unsignalized) | SBT/R | - | 0.54 | 0 | 0 | - | 0.39 | 0 | 0 |
| (Onsignalized) | Overall | Α | - | 0.3 | - | Α | - | 0.5 | - |
| Notes: | m indicates # indicates | s that the vo the volume | olume for th for the 95 th | e 95 th percentile | entile queue cycle excee | e is metred de capacity | oy an upstre | eam signal | |

Table 12: 2031 Future Background Conditions Operational Analysis

As shown above, with the addition of background growth to reflect the 2031 horizon as well as traffic generated from surrounding developments, the Study Area intersections operate with higher v/c ratios, longer delays, and



longer queues than the 2026 Future Background conditions. Critical movements as defined by Mississauga's TIS Guidelines are identified in red.

The Glen Oaks Access at Ninth Line intersection is anticipated to operate with acceptable LOS in the 2031 Future Background conditions. The shared eastbound left / right movement during the AM peak hour is the only movement that has a relatively long delay of 36 seconds for an unsignalized intersection due to the high volumes projected along Ninth Line, leaving short gaps for vehicles at the access to complete the turn. As the queue lengths at the Glen Oaks Access are much shorter for both the AM and PM peak hours than the driveway length, the delay at the Glen Oaks Access will not impact the operation of the intersection.

The Dundas Street East at Ninth Line is anticipated to experience operational constraints in the same pattern as in the 2026 Future Background horizon, except that the v/c ratios and delays are generally worse. The eastbound through and westbound left movements are constrained with long delays and queues in the AM peak hour. As they are conflicting movements and the v/c ratios at the northbound left and southbound through movements are also approaching 1.0, signal timing optimization cannot be implemented to improve the conditions. During the PM peak hour, the eastbound left, westbound through, northbound left, northbound right, and southbound left movements would have exceeded the critical threshold with v/c ratios above 1.0 and queues exceeding storage lane lengths. Similarly, improvements through signal optimization are not feasible as conflicting movements are either over capacity or at capacity.

Similar to the 2026 Future Background conditions, the major concern at this intersection is the long queues projected for the westbound movements during the PM peak hour which have the potential to spillback to the Highway 403 off ramp approximately 320 metres east of the Dundas Street East at Ninth Line intersection. The queues on these movements are caused by the high projected volumes along Dundas Street which cannot be accommodated by the current configuration of three through lanes per direction. The 1.5% annual growth rate on the corridor worsens the traffic operational conditions that are already at capacity in the existing conditions. The volumes along the corridor will not continue to increase at this growth rate in the future conditions with the alternative E-W corridors to be completed and the reduction in auto volumes due to the projected increase in transit and active modes.

The HOV/BRT curbside lanes have not been included in the analysis as the capacity of the road will not be able to accommodate the projected traffic volumes. The HOV lanes should be implemented when the transit and active mode transportation facilities support the modal shift.

4 Forecasting

4.1 Trip Generation and Mode Shares

This proposed development is mixed-use, containing 15,616 m² (168,091ft²) of self-storage, 97 m² (1,048 ft²) of wine cellar, 5,755 m² (61,941 ft²) of office space, 1,231 m² (13,255 ft²) of industrial condo units, and 1,400 m² (15,065 ft²) of reception and retail spaces that support the self-storage customers. The wine cellar is a specific type of self-storage service that the proposed Dymon facility provides where restaurants or private collectors can rent high-standard wine cellar units to store their wine collections. The GFA of the wine cellar is less than 1% of the entire self-storage component, thus it is appropriate to aggregate it with the self-storage land use for trip generation calculation. Therefore, four land uses are involved in the trip generation of this site: office, self-storage, retail, and industrial condo. The development will be built in a single phase, and the site generated trips will be the same for 2026 and 2031 horizons.



Due to the unique business model, the land use cases identified and surveyed by the ITE to obtain trip generation rates are not always representative of the land uses in the proposed development. The site trip generation of the proposed development will be projected using two different methods – ITE rates and proxy site data rates – which will be compared to determine the most appropriate site-generated trip volumes.

4.1.1 Trip Generation by ITE Rates

The ITE Trip Generation Manual 11th Edition has been reviewed to determine the appropriate rate equations for each land use. Industrial condos can be used for a wide range of industrial activities such as small-scale manufacturing, processing, and warehousing. The General Light Industrial land use was considered to be the most appropriate land use for this type of Table 13 summarizes the vehicle trip rates for the proposed land uses.

| | Land Use | CEA (1000 ft ²) | Peak | Mathad | Vehicle | Distri | bution |
|----------------------|----------|-----------------------------|------|----------|-----------|--------|--------|
| Lanu Ose | Code | GFA (1000 IL) | Hour | Method | Trip Rate | In | Out |
| Strip Retail | 077 | 1 5 1 | AM | Weighted | 2.36 | 62% | 38% |
| Plaza (<40k) | 022 | 15.1 | PM | Average | 6.59 | 49% | 51% |
| Office | 710 | AM Fitted Curve 1. | | 1.79 | 88% | 12% | |
| Onice | /10 | 01.9 | PM | Equation | 1.80 | 17% | 83% |
| Mini- | 151 | 160 1 | AM | Weighted | 0.09 | 59% | 41% |
| Warehouse | 151 | 109.1 | PM | Average | 0.15 | 47% | 53% |
| General Light | 110 | 12.2 | AM | Weighted | 0.74 | 88% | 12% |
| Industrial | 110 | 13.5 | PM | Average | 0.65 | 14% | 86% |

Table 13: Trip Generation Vehicle Trip Rates

The weighted average rates were applied when there were no fitted curve equations given, a small sample size, or when the curve did not fit the data well. The fitted curve equations were used when the regressions were calculated based on more than 20 studies and the criteria of R^2 values being greater than 0.75 were met.

Internal capture rates from the ITE Trip Generation Handbook 3rd Edition have not been assigned to any components of the development. Although it is a mixed-use development, there are no strong correlations between each use. A pass-by trip to the retail component on the way to an ultimate destination (i.e., work) is also unlikely due to the type of items sold. The proxy site data in Section 4.1.2 accounted for the on-site interactions as the total external inbound and outbound trips are counted for sites containing similar components.

Using the above person trip rates, the total person trip generation has been estimated. Table 14 below illustrates the total person trip generation by land use category.

| Proposed Land | | $C \Gamma A (1000 ft^2)$ | AN | 1 Peak H | our | ٩N | PM Peak Hour | | | |
|-----------------------|------------------------------|--------------------------|-----|----------|-------|-----|--------------|-------|--|--|
| Use | Lanu Use | GFA (1000 IL) | In | Out | Total | In | Out | Total | | |
| Retail / Reception | Strip Retail Plaza (<40k) | 15.1 | 22 | 14 | 36 | 49 | 50 | 99 | | |
| Co-working Office | Office | 61.9 | 98 | 13 | 111 | 19 | 92 | 111 | | |
| Self-Storage | Mini-Warehouse | 169.1 | 9 | 6 | 15 | 12 | 13 | 25 | | |
| Industrial Condo | General Light Industrial | 13.3 | 9 | 1 | 10 | 1 | 8 | 9 | | |
| | 138 | 34 | 172 | 81 | 163 | 244 | | | | |

Table 14: Total Vehicle Trip Generation



As shown above, 172 AM and 244 PM new peak hour two-way vehicle trips are projected as a result of the proposed development. The largest trip generator among all uses is the office component which is anticipated to generate 98 and 99 two-way vehicle trips during the AM and PM peak hours, respectively.

4.1.2 Trip Generation by Proxy Site Rates

4.1.2.1 Dymon Business Model and Site Context

Dymon offers a unique customer-centric storage solution unlike anything else in the marketplace. Unlike traditional self-storage operations, Dymon facilities are located along arterial corridors, in very prominent locations within close proximity to its residential and business customers. With its high level of security, total humidity and climate control environment, and relentless focus on customer service, Dymon offers a reliable extension to people's homes and businesses. The primary access to Dymon's facilities is via an interior loading area (with secure access 24 hours a day) that protects customers from the weather while loading/unloading their possessions. By providing this interior area the reliance on surface parking is significantly reduced, as up to 75% of visitors to the site during any period use the interior loading bay, rather than the provided parking lot. In fact, any visit after the initial visit uses the interior loading area as this is the direct access to the storage lockers. Dymon sites include a reception and a retail area that is not used directly for self-storage. This space has several functions, including allowing space for new customers to come in and rent a storage locker or purchase storage supplies (boxes, tape, bubble wrap, etc.). In Spring 2019, Dymon expanded the services available in this space to include home storage solutions including closet organizers, under counter shelving, and storage bins. The subject development also will include a Work Refined co-working space which provides members with 24/7 secure access to fully equipped office facilities and dedicated high speed wi-fi, on flexible terms with no long-term commitments.

Industrial condos proposed on this site are a new addition to Dymon facilities. The industrial condo is a condominium development like residential and office condominiums but dedicated to industrial land uses. Dymon's industrial condos aim at providing quality spaces for small to mid-bay industrial activities. The industrial condos are located in a multi-unit structure and share common driveways, loading areas, parking areas, garbage collection, and sidewalks.

4.1.2.2 Proxy Site Data

To better understand the trip generation of the proposed development, a proxy site trip generation survey has been undertaken at five established, comparable Dymon sites in both Ottawa and GTA. These sites have been selected as they are similar in size to the proposed development and have similar features (GFA, land uses, urban environment, arterial road access). The selected sites include the new Dymon retail functions and sell the home storage solutions discussed previously. The most recent survey site of 1460 The Queensway in Etobicoke also includes the co-working office area that will be available at the proposed site at 3855 Dundas Street West. These will operate in the same manner as the proposed site and are appropriate proxy sites for comparison. The Ottawa sites have been selected for review to supplement the lack of data due to the limited number of Dymon sites that have been completed and/or opened in the GTA. This data has been used to support the trip generation projection for a Dymon development located at 3855 Dundas Street West. Table 15 summarizes the site statistics for the surveyed and proposed sites. The number of parking stalls per the approved Site Plan for each proxy site have been documented in Table 15, however the parking provisions will be discussed in a separate document, *3855 Dundas Street Parking and Loading Study*, included in Appendix N.



| Site | Reception / Retail GFA (m²) | Self-Storage GFA (m ²) | Office GFA (m²) | Total GFA (m²) | Parking Stalls (SPA) |
|-------------------|-----------------------------------|---------------------------------------|--------------------|---------------------|--------------------------|
| 1554 Carling | 2.714 | 18.204 | _ | 21.685 | 59 Exterior |
| Avenue | _, | | | , | 4 in Loading Area |
| 323 Coventry Road | 867 | 11,484 | - | 12,351 | 44 Exterior ¹ |
| 300 Greenbank | ~700 | 9 40E | | 0 105 | 9 Exterior |
| Road | 700 | 0,495 | - | 9,195 | 4 in Loading Area |
| 1460 The | 1 7 7 1 | 27 5 6 9 2 | 2 102 | 20.001 | 266 Exterior |
| Queensway | 1,251 | 27,508 | 2,192 | 50,991 | 59 Interior |
| 5 Nevets Road | 563 | 12,448 | - | 13,012 | 41 Exterior |
| 3855 Dundas | 1,400 | 15,714 ² | 5,755 | 22,869 ³ | 97 Exterior |
| Street West | , | , | , | , | 93 Underground |

Table 15: Site Statistics Comparison

Note 1: some of these parking stalls are restricted due to truck movements. This will be discussed further below.

Note 2: These self-storage GFAs include a Dymon Wine component. The wine cellar at 1460 The Queensway is 854 square metres. The wine cellar at 3855 Dundas Street West is 223 square metres.

Note 3: 3855 Dundas Street West also includes industrial condo land use which is not present in the surveyed proxy sites.

As shown in Table 15, the proposed development at 3855 Dundas Street West contains the same reception/retail and self-storage components as all of the proxy sites, and the same office component with 1460 The Queensway site, therefore, the trip generation for these components on site can be projected using proxy site data. Mode choice of the customers has been implicitly reflected in the proxy site survey data; therefore, no additional mode splits are applied to the trip generation results.

The industrial condos will support various types of activities which may generate trips at different rates. Survey data is unavailable for the industrial condos. Without specific information ITE trip generation rates for the general light industrial land use were applied. An auto driver mode share of 100% has been assumed for this type of use as industrial properties typically have higher auto mode shares.

Table 16 summarizes the surveyed trip generation for the same sites. In the case of 1460 The Queensway, since the parking area is not divided into parts and each designated for a specific land use, there are not well-defined self-storage parking spaces or office parking spaces. Therefore, trip generation data specific to each use is not available from the data collection process. The division between the self-storage and office uses was undertaken using the following methodology:

- The vehicles heading to the office component were assumed to have taken the accesses closest to the location of the office: the southmost access on Vansco Road, and the access on Wickman Road. The vehicles using the other accesses were all assumed to be self-storage users.
- The percentage of inbound and outbound trips at an access for the office use are assumed to be related to the percentage of the parking spaces that are frequently used by the office users (information supplied by Dymon) out of all the parking spaces in the proximity of this access. Although the parking and trip generation are not directly related, considering that the average time length of parking of office users is much longer than that of self-storage users, this is a reasonable approximation as the number of parking spaces provided is related to the maximum demand of incoming vehicles.



Two counts have been collected at 1460 The Queensway specifically for the trip generation for the Work Refined office area to provide a larger data set to help determine the trip generation rates at the co-working office. The weekday AM, weekday PM, and Saturday midday peak hour trip generation for self-storage and office uses have been individually tabulated in

Table 16 and Table 17, respectively. Appendix O includes the trip generation proxy counts and site plans for each surveyed site.

| Site | GFA (m²) | AM F (/) | Peak Hour 1000 m ² Gl | Rate FA) | PM Peak Hour Rate (/1000 m ² GFA) | | | Sa (/1 | Sat Peak Hour (/1000 m ² GFA) | | |
|--|----------|-------------|-------------------------------------|-------------|---|-----|-------|-----------|---|-------|--|
| | | In | Out | Total | In | Out | Total | In | Out | Total | |
| 1554 Carling | 21,685 | 6 | 2 | 8 | 13 | 9 | 22 | - | - | - | |
| 323 Coventry (May) | 12,351 | 14 | 9 | 23 | 17 | 19 | 36 | - | - | - | |
| 323 Coventry (June) | 12,351 | 7 | 5 | 12 | 11 | 15 | 26 | 11 | 15 | 26 | |
| 300 Greenbank | 9,195 | 7 | 4 | 11 | 10 | 10 | 20 | 14 | 18 | 32 | |
| 1460 The Queensway (February 2022) | 28,799 | 26 | 18 | 44 | 13 | 23 | 36 | 20 | 20 | 40 | |
| 1460 The Queensway (October 2022) | 28,799 | 45 | 9 | 54 | 24 | 16 | 40 | - | - | - | |
| 5 Nevets Road | 13,012 | 5 | 3 | 8 | 9 | 8 | 17 | 18 | 13 | 31 | |

| Table AC Das | | C | Call stands |
|----------------|---------------|------------|----------------|
| Table 16: Prox | ky site i rip | Generation | – Self-storage |

Table 17: Proxy Site Trip Generation – Office

| Sito | GEA (m ²) | AN | /I Peak Ho | our | PN | /I Peak Ho | our | Sa | it Peak Hour | |
|--|-----------------------|----|------------|-----------------------|-------|------------|-----|-------|--------------|---|
| Site | GFA (m.) | In | Out | Out Total In Out Tota | Total | In | Out | Total | | |
| 1460 The Queensway (February 2022) | 2,192 | 16 | 2 | 17 | 1 | 5 | 6 | 4 | 2 | 6 |
| 1460 The Queensway (October 2022) | 2,192 | 16 | 3 | 19 | 10 | 9 | 19 | - | - | _ |

The selected sites have a wide range of gross floor areas. To accurately compare these sites to the proposed site, the trip generation rate has been determined for each survey in terms of vehicle trips generated per 1000 square metres. Table 18 and Table 19 summarize the trip generation rates for each site for self-storage and office, respectively.



| Site | GFA (m²) | AM F (/1 | AM Peak Hour Rate (/1000 m ² GFA) | | PM F (/1 | Peak Hour 1000 m ² Gl | Rate FA) | Sa (/1 | Sat Peak Hour /1000 m ² GFA) | |
|--|----------|-------------|---|-------|-------------|-------------------------------------|-------------|-----------|--|-------|
| | | In | Out | Total | In | Out | Total | In | Out | Total |
| 1554 Carling | 21,685 | 0.28 | 0.09 | 0.37 | 0.60 | 0.42 | 1.01 | - | - | - |
| 323 Coventry (May) | 12,351 | 1.13 | 0.73 | 1.86 | 1.38 | 1.54 | 2.91 | - | - | - |
| 323 Coventry (June) | 12,351 | 0.57 | 0.40 | 0.97 | 0.89 | 1.21 | 2.11 | 0.89 | 1.21 | 2.11 |
| 300 Greenbank | 9,195 | 0.76 | 0.44 | 1.20 | 1.09 | 1.09 | 2.18 | 1.52 | 1.96 | 3.48 |
| 1460 The Queensway (February 2022) | 28,799 | 0.90 | 0.63 | 1.53 | 0.45 | 0.80 | 1.25 | 0.69 | 0.69 | 1.39 |
| 1460 The Queensway (October 2022) | 28,799 | 1.56 | 0.31 | 1.88 | 0.83 | 0.56 | 1.39 | - | - | - |
| 5 Nevets Road | 13,012 | 0.38 | 0.23 | 0.61 | 0.69 | 0.61 | 1.31 | 1.38 | 1.00 | 2.38 |
| Average Rate | - | 0.80 | 0.40 | 1.20 | 0.85 | 0.89 | 1.74 | 1.12 | 1.22 | 2.34 |

Table 18: Proxy Site Trip Generation Rates – Self-storage and Retail

| Table 19 | : Proxv | Site | Trip | Generation | Rates – | Office |
|----------|---------|------|------|-------------|---------|---|
| | | 0.00 | | 00110101011 | | 0,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |

| Site | GFA (m²) | AM Peak Hour Rate (/1000 m ² GFA) | | | PM Peak Hour Rate (/1000 m ² GFA) | | | Sat Peak Hour (/1000 m2 GFA) | | |
|-----------------|----------|---|------|-------|---|------|-------|---------------------------------|------|-------|
| | | In | Out | Total | In | Out | Total | In | Out | Total |
| 1460 The | | | | | | | | | | |
| Queensway | 2,192 | 7.30 | 0.91 | 7.76 | 0.46 | 2.28 | 2.74 | 1.82 | 0.91 | 2.74 |
| (February 2022) | | | | | | | | | | |
| 1460 The | | | | | | | | | | |
| Queensway | 2,192 | 7.30 | 1.37 | 8.67 | 4.56 | 4.11 | 8.67 | - | - | - |
| (October 2022) | | | | | | | | | | |
| Average Rate | | 7.30 | 1.14 | 8.21 | 2.51 | 3.19 | 5.70 | 1.82 | 0.91 | 2.74 |

Since the 1460 Queensway is a relatively recent establishment, the site is not expected to have been operating at full capacity during the time the traffic data was obtained. At the 1460 Queensway location as of the February 2022, 59.5% of the lockers were rented (1548 Units) while 40.5% were available or vacant (1055 Units) for the self-storage, and 64.5% of the co-working spaces were rented (129 workstations) while 35.5% (71 workstations) were available. The same occupancy rates have been assumed for the October 2022 count dates as well, to be conservative. The office PM peak trip generation rates in the February count are much lower than those in the October count due to that the actual number of trips is as low as 1 inbound and 5 outbound as shown in Table 17 which caused the rates to be sensitive to small changes in the survey results. Considering the potential growth from more customers, the trip generation at maximum capacity, assuming that the increase in the number of trips generated will be linear to the number of rented units, is calculated for self-storage and office as show in Table 20 and Table 21.



| Site | GFA (m²) | AM I (/ | AM Peak Hour Rate (/1000 m ² gfa) | | | Peak Hour 1000 m ² g | Rate fa) | Sa (/1 | at Peak Hour 1000 m2 GFA) | |
|--|----------|------------|---|-------|------|------------------------------------|-------------|-----------|------------------------------|-------|
| | | In | Out | Total | In | Out | Total | In | Out | Total |
| 1554 Carling | 21,685 | 0.28 | 0.09 | 0.37 | 0.60 | 0.42 | 1.01 | - | - | - |
| 323 Coventry (May) | 12,351 | 1.13 | 0.73 | 1.86 | 1.38 | 1.54 | 2.91 | - | - | - |
| 323 Coventry (June) | 12,351 | 0.57 | 0.40 | 0.97 | 0.89 | 1.21 | 2.11 | 0.89 | 1.21 | 2.11 |
| 300 Greenbank | 9,195 | 0.76 | 0.44 | 1.20 | 1.09 | 1.09 | 2.18 | 1.52 | 1.96 | 3.48 |
| 1460 The Queensway (February 2022) | 28,799 | 1.52 | 1.05 | 2.57 | 0.76 | 1.34 | 2.10 | 1.17 | 1.17 | 2.34 |
| 1460 The Queensway (October 2022) | 28,799 | 2.63 | 0.53 | 3.15 | 1.40 | 0.93 | 2.34 | - | - | - |
| 5 Nevets Road | 13,012 | 0.38 | 0.23 | 0.61 | 0.69 | 0.61 | 1.31 | 1.38 | 1.00 | 2.38 |
| Average Rate | - | 1.04 | 0.50 | 1.53 | 0.97 | 1.02 | 1.99 | 1.24 | 1.33 | 2.58 |

Table 20: Proxy Site Trip Generation Rates – Self-storage and Retail

| Table 21 · Drov | v Sito | Trin | Congration | Patos | - Office |
|-----------------|--------|------|------------|-------|--------------|
| Table 21: Prox | y site | irip | Generation | Rates | $-O_{IIICE}$ |

| Site | GFA (m²) | AM Peak Hour Rate (/1000 m ² gfa) | | | PM Peak Hour Rate (/1000 m ² gfa) | | | Sat Peak Hour (/1000 m2 GFA) | | |
|--|----------|---|------|-------|---|------|-------|---------------------------------|------|-------|
| | | In | Out | Total | In | Out | Total | In | Out | Total |
| 1460 The Queensway (February 2022) | 2,192 | 11.32 | 1.41 | 12.02 | 0.71 | 3.54 | 4.24 | 2.83 | 1.41 | 4.24 |
| 1460 The Queensway (October 2022) | 2,192 | 11.32 | 2.12 | 13.44 | 7.07 | 6.37 | 13.44 | - | - | - |
| Average Rate | - | 11.32 | 1.77 | 12.73 | 3.89 | 4.95 | 8.84 | 2.83 | 1.41 | 4.24 |

The trip generation rates above have been examined and these sites do not have a strong correlation between gross floor area and trip generation. Although there is only one survey site for Dymon Work Refined Office, the October 2022 trip generation is likely overestimated as occupancy rates have been applied to scale the trip generation, however, there is not enough data to conclude that the relationship between occupancy and trip generation is linear. Additionally, due to the low magnitude of trips in the survey a small change in the number of trips has a large impact on the trip generation rate. Therefore, the average trip generation rate has been applied to the proposed site to project the anticipated trip generation of the subject development on a typical day.

Table 22 summarizes the projected trip generation for the proposed Dymon development at 3855 Dundas Street West. As discussed previously in Section 2.7.1, the weekday AM and PM peak periods are the critical periods for this site due to the Saturday midday peak period having a lower trip generation from the co-working office use.



| Land Llas | | AM Peak Hour | | | PM Peak Hour | | | Sat Peak Hour | | |
|---|-----------------------|--------------|-----|-------|--------------|-----|-------|---------------|-----|-------|
| Land Use | GFA (m ⁻) | In | Out | Total | In | Out | Total | In | Out | Total |
| Dymon Self-Storage, Wine Cellar, & Reception/Retail | 17,113 | 18 | 8 | 26 | 17 | 17 | 34 | 21 | 23 | 44 |
| Office | 5,755 | 65 | 10 | 73 | 22 | 28 | 51 | 16 | 8 | 24 |
| | Subtotal | 83 | 19 | 100 | 39 | 46 | 85 | 38 | 31 | 69 |
| Industrial Condo | 1,231 | 9 | 1 | 10 | 1 | 8 | 9 | 4 | 5 | 9 |
| | Total | 92 | 20 | 110 | 40 | 54 | 94 | 42 | 36 | 78 |

Table 22: Projected 3855 Dundas Street West Site Trip Generation by Proxy Site Data

Table 23 summarizes the ITE trip generation results for vehicle trips for comparison.

| | | AM Peak Hour | | | | PM Peak Hour | | |
|---|------------------|--------------|-----|-------|----|--------------|-------|--|
| Land Use | Units / GFA (m²) | In | Out | Total | In | Out | Total | |
| Dymon Self-Storage Wine Cellar, & Reception/Retail | 17,113 | 31 | 20 | 51 | 61 | 63 | 124 | |
| Office | 5,755 | 98 | 13 | 111 | 19 | 92 | 111 | |
| Industrial Condo | 1,231 | 9 | 1 | 10 | 1 | 8 | 9 | |
| Total | | | 34 | 172 | 81 | 163 | 244 | |

Table 22: Drojected 2055 Dundas Street West Site Trip Congration by ITE Pat

The total ITE trip generation results are higher than the proxy site trip generation results during both the weekday AM and PM peak hours.

The General Office Building Land Use in the ITE Manual represents a typical office building with regular working hours. It does not represent the 24/7 co-working space Dymon provides which serves different enterprises at the same time and allows the flexibility of arrival and departure times.

The trips generated by the self-storage portion using proxy data are also lower than those calculated using ITE rates. A typical industrial warehouse has heavy trucks loading and unloading during certain periods of the day (i.e., early morning) while visits to self-storage sites predominantly use passenger vehicles and are more frequent and scattered throughout the day.

Therefore, the proxy site trip generation results are more representative of the specific land uses in this exercise. The proposed development will generate 110 AM and 94 PM new two-way vehicle trips in both 2026 and 2031.

As the proposed development at 3855 Dundas Street West will be built on vacant spaces, the new site generated volumes will be the net site generated volumes and it will be added to the Future Background volumes.

The site traffic generated is much lower than the total site traffic from background developments in the surrounding area considered in the study, which will generate 2,760 AM and 3,256 PM trips. The site traffic is anticipated to have a relatively minor impact on the transportation network, compared to the background traffic.

4.2 Auto Site Trip Distribution

The proposed development primarily consists of self-storage and co-working office land uses; hence the targeted customers are primarily residents or businesses from nearby neighbourhoods. As a result, the trips generated will be primarily local. The trips generated by the proposed development were distributed to the boundary road network based on the locations of estimated residential, industrial, and commercial catchment areas. The potential catchment areas were determined based on the locations of existing self-storage facilities and coworking spaces in Oakville and Mississauga.



A review of existing self-storage facilities shows that there are several east of Highway 403 in Mississauga and south of Highway 403 in Oakville, which are expected to capture the surrounding areas in Mississauga and Oakville. A similar pattern is observed for the co-working spaces in the surrounding areas, except that the proposed Dymon Work Refined will likely have another catchment area located east of the site in the lands south of Highway 407 and east of Highway 403. Therefore, trips are primarily expected to be local, arriving from and departing to the west within Oakville, with a smaller percentage from the other directions. Figure 22 and Figure 23 illustrate existing self-storage facilities and co-working spaces in Mississauga and Oakville and the potential catchment areas of the subject site at 3855 Dundas Street West.



Figure 22: Existing Self-storage Facilities in Mississauga and Oakville







To determine the travel patterns of the subject development, the 2016 Transportation Tomorrow Survey (TTS) has also been taken into consideration. The OD matrix of the traffic zone containing the proposed development and the surrounding zones that currently have similar land uses (traffic zones 3634, 4024, 4180) have been extracted. Due to the specific land uses of the proposed development, only the local trips, which have origins or destinations in nearby zones in Oakville or Mississauga, have been analyzed. TTS data for these zones can be found in Appendix P. The resulting trip distribution for the three zones aggregated is illustrated in Table 24.



Table 24: Trip Distribution – Traffic Zones

| To/From | Percent of Trips |
|---------|------------------|
| North | 25% |
| South | 35% |
| East | 30% |
| West | 10% |
| Total | 100% |

The directions in Table 24 are cardinal directions and many trips travelling from the north and south will access the site via Dundas Street East instead of Ninth Line depending on their locations (i.e., northwest of the site) and the connectivity of the road network within Oakville. The shortest routes from major residential and commercial zones to the site have been identified and the trip distribution along the Study Area roads are summarized in Table 25.

Table 25: 2016 TTS Trip Distribution

| Arriving From / Departing To | Percentage of Trips |
|-------------------------------|---------------------|
| West (via Dundas Street West) | 40% |
| East (via Dundas Street West) | 30% |
| South (via Ninth Line) | 20% |
| North (via Ninth Line) | 10% |
| Total | 100% |

Compared to the 2016 TTS trip distribution, the percentage of the trips arriving from the west will be higher as substantial residential developments are being proposed and constructed on the north side along Dundas Street west of Ninth Line as noted in Section 3.2. These developments will be within the catchment areas of the proposed self-storage and co-working office. These are not captured in 2016 TTS data but will contribute to the site traffic in 2026 and 2031 future horizons. The TTS trip distribution has been adjusted to the percentages in Table 26 based on future developments in the catchment areas. The trips arriving from the west will increase by 15% while the trips arriving from the east and south will decrease by 10% and 5%, respectively, as competing establishments with similar or the same uses located at the east and south will make it unlikely for a steady increase in customers attracted from these directions. The following trip distribution rates have been applied to the site trips generated by 3855 Dundas Street West.

Table 26: Future Trip Distribution

| Arriving From / Departing To | Percentage of Trips |
|-------------------------------|---------------------|
| West (via Dundas Street West) | 55% |
| East (via Dundas Street West) | 20% |
| South (via Ninth Line) | 15% |
| North (via Ninth Line) | 10% |
| Total | 100% |

4.3 Auto Site Trip Assignment

Using the distribution outlined above, turning movement splits, intersection and access turning restrictions, and access to major transportation infrastructure, the trips generated by the site have been assigned to the Study Area road network. The trip assignment exercise was generally based on the principle that the most direct route with the shortest travel distance would be chosen. As the site only has one vehicular access, all inbound trips and



outbound trips will use the access. With full movements allowed at the access, no U-turns are expected from the site trips as they can travel directly towards their destinations. With no access provided on Dundas Street East, trips travelling from the west and east along Dundas Street East will access the site by making westbound right and eastbound left turns onto Ninth Line first, 90% of the total inbound trips take a northbound right turn at the future site access at Ninth Line intersection and the rest 10%, which are trips coming from the North, will take a southbound left turn. The opposite applies to the outbound trips, hence 10% of the trips will leave the site with a westbound right movement and 90% will make a westbound left turn and divert to south, east, and west at the Dundas Street East at Ninth Line intersection. Figure 24, Figure 25, and Figure 26 illustrate the 2026 and 2031 new site traffic generated volumes for the self-storage and retail, the co-working office, and the industrial condos, respectively. Figure 27 illustrates the 2026 and 2031 new site traffic generated volumes for all land uses combined.









Figure 25: 2026 and 2031 New Site Generation Auto Volumes – Office

Figure 26: 2026 and 2031 New Site Generation Auto Volumes – Industrial Condos







Figure 27: 2026 and 2031 New Site Generation Auto Volumes – Total

5 Future Total

5.1 Future Total Traffic Volumes

The site generated traffic has been combined with the 2026 and 2031 Future Background traffic volumes to estimate the Future Total traffic volumes. The 2026 Future Total traffic volumes are illustrated in Figure 28 and the 2031 Future Total traffic volumes are illustrated in Figure 29.





Figure 28: 2026 Future Total Traffic Volumes

Figure 29: 2031 Future Total Traffic Volumes





5.2 Future Total Operational Analysis

5.2.1 Future Total Intersection Design

The Ninth Line at Dundas Street East intersection has been designed with the same geometry as was considered in the Future Background analysis.

The Glen Oaks Access at Ninth Line intersection has been modified into a four-legged intersection, with the addition of the site access of the proposed Dymon development as the westbound approach of the intersection. The intersection is assumed to be stop-controlled on the minor streets, in this case the accesses. Both the Glen Oaks Access and proposed Dymon site access are assumed to be full movement.

Left turn lane warrants have been assessed for the Glen Oaks Access / Future Dymon Access at Ninth Line based on the projected volumes for 2026 Future Total and 2031 Future Total scenarios. Both the northbound left turn and southbound left turn lanes are warranted due to the high advancing and opposing volumes with a storage length of 25 metres. Appendix Q includes the left turn warrant graphs.

For the 2026 horizon, the Glen Oaks Access / Future Dymon Access at Ninth Line will have a shared left turn / through / right turn lane at the eastbound and westbound approaches, a shared left turn / through lane and a shared through / right turn lane on the northbound approach, and a dedicated left turn and a shared through / right turn lane on the southbound approach. A dedicated northbound left turn is warranted but has not been modelled for the 2026 horizon as it is not certain whether the reconstruction of Ninth Line will be completed by then. The median along Ninth Line in front of the accesses has been coded as a TWLTL (two-way left turn lane) in Synchro.

For the 2031 horizon, the eastbound approach (the Glen Oaks Access) and westbound approach (Dymon access) both consist of a shared left-turn / through / right-turn lane. The northbound approach has been modelled with a dedicated left-turn lane, a through lane, and a shared through / right-turn lane. Along the side there is also a 1.8-metre bike lane and a 3.0-metre multi-use path. The southbound approach is assumed to consist of a dedicated left-turn lane, a through lane, and a shared through / right-turn lane. The bike lane and the multi-use path are planned to be constructed to mirror the existing east side of Ninth Line. The median along Ninth Line is coded as a TWLTL (two-way left turn lane) in Synchro. The left-turn lane of the southbound left movement at the Ninth Line at Dundas Street East intersection currently extends all the way up to the Glen Oaks Access, therefore sufficient space is available to construct a southbound left turn lane for the inbound vehicles to Dymon. This configuration is based on the preliminary design of Ninth Line from the EA completed by Halton Region.

5.2.2 2026 Future Total Operational Analysis

The proposed development's trip generation has been added to the 2026 Future Background traffic volumes to project the impact of the site traffic on the Study Area road network. Table 27 summarizes the operational analysis for the 2026 Future Total conditions. The parameters used to assess the Future Background conditions operational analysis, discussed in Section 3.6.1, have been applied to Future Total conditions as well. The intersections have been analyzed based on the identified signal control and intersection configurations in Section 6.2.1. 2026 Future Total Synchro worksheets are included in Appendix R.



| Interrection | lana | | AM Pea | ak Hour | | PM Peak Hour | | | | |
|----------------|--------------|-------------------------------------|--------------------------|---------------------------|--------------|--------------|--------------|-----------|--------|--|
| | | LOS | V/C | Delay | Queues | LOS | V/C | Delay | Queues | |
| | EBL | С | 0.75 | 30 | 68 | F | 1.36 | 250 | #112 | |
| | EBT | F | 1.16 | 116 | #402 | D | 0.85 | 43 | #235 | |
| | EBR | С | 0.52 | 30 | 65 | С | 0.34 | 29 | 35 | |
| | WBL | F | 1.13 | 161 | #107 | D | 0.69 | 40 | 41 | |
| Niinth Line Q | WBT | С | 0.59 | 32 | 141 | F | 1.28 | 174 | #436 | |
| Ninth Line & | WBR | С | 0.23 | 26 | 17 | С | 0.37 | 29 | 45 | |
| East | NBL | E | 0.79 | 56 | #86 | E | 0.92 | 64 | #135 | |
| (Signalized) | NBT | D | 0.46 | 51 | 67 | E | 0.96 | 76 | #192 | |
| (Signalized) | NBR | D | 0.52 | 53 | 34 | F | 1.14 | 136 | #224 | |
| | SBL | E | 0.82 | 62 | #89 | E | 0.91 | 78 | #99 | |
| | SBT | E | 0.85 | 66 | 124 | E | 0.55 | 57 | 75 | |
| | SBR | D | 0.52 | 55 | 23 | E | 0.63 | 61 | 43 | |
| | Overall | E | 1.04 | 77 | - | F | 1.21 | 106 | - | |
| | EBL/T/R | С | 0.04 | 25 | <1 | С | 0.16 | 18 | 4 | |
| Ninth Line & | WBL/T/R | D | 0.12 | 29 | 3 | E | 0.33 | 35 | 10 | |
| Glen Oaks | NBL/T | А | 0.04 | 1 | <1 | А | 0.03 | 1 | <1 | |
| Access / Site | NBT/R | - | 0.27 | 0 | 0 | - | 0.43 | 0 | 0 | |
| Access | SBL | А | 0.01 | 9 | <1 | В | 0.01 | 11 | <1 | |
| (Unsignalized) | SBT/R | - | 0.68 | 0 | 0 | - | 0.47 | 0 | 0 | |
| | Overall | С | - | 0.7 | - | С | - | 1.5 | - | |
| | m indicates | s that the vo | olume for th | ie 95 th perce | entile queue | is metred l | oy an upstre | am signal | | |
| Notes: | # indicates | the volume | for the 95 ^{tl} | ^h percentile | cycle excee | ds capacity | | | | |
| | \$ indicates | \$ indicates the delay exceeds 300s | | | | | | | | |

Table 27: 2026 Future Total Conditions Operational Analysis

With the addition of the site-generated traffic to the 2026 Future Background traffic, the Study Area intersections operate in similar manner to the Study Area intersections for Ninth Line but slightly worse than the 2026 Future Background conditions. Critical movements have been highlighted in red.

The operational conditions at the Dundas Street at Ninth Line intersection indicate that the site traffic has little impact on the traffic conditions. Compared to the 2026 Future Background conditions, the v/c ratios for the 2026 Future Total conditions are similar and the delays increased slightly. The overall delay has increase from 73 seconds to 77 seconds during the AM peak hour and from 99 seconds to 106 seconds during the PM peak hour, which are minimal and do not change the nature of the operational conditions.

The four-legged unsignalized intersection formed with the site access operates well. The two-way left turn lane, included in the preliminary design for Ninth line, in front of the two accesses provides sufficient capacity for left turning vehicles exiting the accesses. The LOS and delays are acceptable at all movements, and the queues can be accommodated by the driveways on both sites.

The operational characteristics of this study area intersections are not significantly impacted by the addition of the site traffic to the road network. The increase in v/c ratios and delays are minor. Alternative routes and modal shifts are expected to decrease the Future Background volumes to improve the Future Background conditions. As the site trips do not impact the traffic conditions at nearby intersections, no geometric improvements are recommended.



5.2.3 2031 Future Total Operational Analysis

The proposed development's trip generation has been added to the 2031 Future Background traffic volumes to project the impact of the new traffic on the Study Area road network five years beyond the anticipated full buildout date.

The parameters used to assess the existing conditions operational analysis discussed in Section 2.7.3, have been applied to future conditions as well. The intersections have been analyzed based on the identified signal control and intersection configurations in Section 5.2.1.

Table 28 summarizes the operational analysis for the 2031 Future Total conditions. 2031 Future Total Synchro worksheets are included in Appendix S.

| Interestica | 1 | | AM Pea | ak Hour | | PM Peak Hour | | | | |
|----------------------|---|-----|--------|---------|--------|--------------|------|-------|--------|--|
| intersection | Lane | LOS | V/C | Delay | Queues | LOS | V/C | Delay | Queues | |
| | EBL | D | 0.82 | 43 | 83 | F | 1.57 | 338 | #123 | |
| | EBT | F | 1.28 | 173 | #445 | E | 0.98 | 60 | #271 | |
| | EBR | С | 0.58 | 34 | 75 | С | 0.36 | 32 | 38 | |
| | WBL | F | 1.39 | 259 | #122 | Е | 0.86 | 74 | #55 | |
| | WBT | D | 0.71 | 40 | 162 | F | 1.49 | 266 | #514 | |
| Ninth Line & | WBR | С | 0.28 | 31 | 23 | С | 0.41 | 32 | 55 | |
| Dundas Street | NBL | E | 0.85 | 62 | #105 | F | 1.19 | 150 | #203 | |
| EdSL (Signalized) | NBT | D | 0.52 | 50 | 83 | F | 1.09 | 112 | #238 | |
| (Signalized) | NBR | D | 0.53 | 51 | 47 | F | 1.23 | 172 | #271 | |
| | SBL | E | 0.89 | 67 | #86 | F | 1.40 | 262 | #133 | |
| | SBT | E | 0.89 | 67 | #153 | Е | 0.76 | 66 | 97 | |
| | SBR | D | 0.51 | 51 | 31 | Е | 0.78 | 74 | 51 | |
| | Overall | F | 1.16 | 104 | - | F | 1.48 | 160 | - | |
| | EBL/T/R | С | 0.03 | 22 | <1 | С | 0.13 | 15 | 3 | |
| Ninth Line & | WBL/T/R | С | 0.08 | 21 | 2 | Е | 0.40 | 46 | 12 | |
| Glen Oaks | NBL | В | 0.05 | 13 | 1 | В | 0.04 | 10 | <1 | |
| Access / Site | NBT/R | - | 0.36 | 0 | 0 | - | 0.64 | 0 | 0 | |
| Access | SBL | А | 0.01 | 10 | <1 | В | 0.01 | 13 | <1 | |
| (Unsignalized) | SBT/R | - | 0.54 | 0 | 0 | - | 0.39 | 0 | 0 | |
| | Overall | Α | - | 0.4 | - | В | - | 1.4 | - | |
| Notes: | m indicates that the volume for the 95 th percentile queue is metred by an upstream signal # indicates the volume for the 95 th percentile cycle exceeds capacity \$ indicates the delay exceeds 300s | | | | | | | | | |

Table 28: 2031 Future Total Conditions Operational Analysis

With the addition of the site-generated traffic to the 2031 Future Background traffic, the Study Area intersections operate in similar manner to the 2031 Future Background conditions. Critical movements as defined by City of Mississauga TIS Guidelines are identified in red.

The site-generated trips remained the same from 2026 to 2031, but the background trips for 2031 increases significantly from the 2026 conditions with an annual growth rate up to 1.5% along Dundas Stret and an annual growth rate up to 4.5% along Ninth Line. Overall, the higher volumes in the transportation system in the 2031 Future Total scenarios increase the v/c ratios and delays significantly from the 2026 Future Total scenarios, especially during the PM peak hour.



Comparing the 2031 Future Background operational analysis to the 2031 Future Total analysis illustrates that the site-generated traffic is projected to have a minimal impact on the Study Area road network. The v/c ratios and delays on individual movements are similar to the 2031 Future Background results, with only small increases that do not change the level of service on individual movements or the overall intersections. The eastbound left, westbound through, and southbound left movements have larger increases in v/c ratios. It is understood that the intersection of Dundas Street at Ninth Line is already over capacity in the 2031 Future Background scenarios, therefore, small volume increases result in disproportionately higher delays.

The Site Access / Glen Oaks Access on Ninth Line operates well. The only movement with relatively long delay is the outbound movement at the Site Access during the PM peak hour which exhibits an LOS of E, but the 95th percentile queue of 12 metres can be accommodated by the site driveways without impacting the traffic along Ninth Line. The site access will be further examined in the Section 6.2.

As the operational constraints at the study area intersections are projected to be caused by the Future Background volumes and the site trips have a minimal impact, no geometric improvements are recommended at this intersection.

5.2.4 Mitigation Measures for Auto Mode

Signal optimization has been proposed for both 2026 and 2031 Future Background and Future Total scenarios, including assigning a permissive and overlap phase to the northbound right movement during the PM peak hour. It is suggested that the City should monitor the Dundas Street East at Ninth Line intersection and optimize the signal timing plan as the volume pattern changes. No intersection reconfiguration has been proposed due to property constraints. East-west volumes along the Dundas Street corridor are projected to exceed the theoretical capacity. Volume reductions, through rerouting to other intersection and transportation demand management strategies including providing more transit and active transportation facilities, are anticipated to be the most effective strategies for addressing the projected deficiencies. The timing of implementing the HOV / transit lane for each direction along Dundas Street planned should be reconsidered by Halton Region regarding the balance between reduced capacity due to the converted lane and the reduced demand in the future.

6 Concept Plan Review

6.1 Site Circulation

A site circulation assessment was completed using AutoTURN 11.0 to develop turning templates for garbage trucks and loading trucks. WB-20 and HSU design vehicles were used to simulate the movements of vehicles as they manoeuvre throughout the site. Key areas of assessment include the Ninth Line full-moves site access, the garbage loading space, the drive-in loading area, and site circulation.

WB-20 tractor trailers are shown to be able to access the site via the full-movement access on Ninth Line and exit via the same access. On site, WB-20s will use the driveway in the northern half of the site which are wider. They will exit by taking a left turn at the northeast corner of the site after using the loading docks. They are able to access the interior loading dock in the interior loading / drive-through as well as the loading dock on the exterior south of the drive-through. Both the north and south loading bays can accommodate the WB-20s turning in from the access north of the interior loading area. All turning paths to and from the site are accommodated by the proposed curbs.

HSUs are demonstrated to be able to perform the same maneuvers as the WB-20s. Additionally, HSUs can access the entire driveway. HSUs are used for testing the garbage collection located in the northeast corner of the site.



An HSU is shown to take a right turn upon entering the site and take two left turns at the southwest and southeast corners and arrive in front of the garbage bins. After picking up the garbage, the vehicle is shown to be able to reverse onto the driveway and make a left turn to exit via the site access on Ninth Line. All turning paths to and from the site are accommodated by the proposed curbs.

The provided fire route has been reviewed with a fire truck. The fire truck can enter the site via the access on Ninth Line, make a right turn to go around the driveway in a counterclockwise direction, and exit the site via the same access without obstructions. All turning paths to and from the site are accommodated by the proposed curbs.

Other design vehicles such as MSUs and passenger vehicles are not deemed to cause critical conditions compared to larger vehicles tested. The turning templates showing these movements can be found in Appendix T.

6.2 Access Review

One vehicular access point has been proposed on Ninth Line. Access onto Dundas Street from the previous design (as shown in the previous 2018 TIS) has been removed in response to MTO's comments to reduce the potential impact on the Highway 403 off-ramps east of the site. Removal of this access would also reduce the impact on traffic flow on Dundas Street which is projected to carry high volumes of traffic.

The proposed site access is a full-movement access providing a direct connection to Ninth Line aligning with the existing Glen Oaks Access. The segment of Ninth Line north of Dundas Street belongs to the City of Mississauga; therefore, it is reviewed using the relevant sections in Mississauga's TIS Guidelines and TAC'S Geometric Design Guide for Canadian Roads.

6.2.1 Access Control and Spacing

The Transportation Association of Canada Geometric Design Guide for Canadian Roads (TAC GDG) Section 8.3.3 notes that accesses to major commercial, industrial or residential properties, where volumes can be relatively high, should be treated as intersections. However, the proposed access to the subject site would only serve the proposed building and would not provide future connections to additional properties. As shown in Section 4.1.2.2 the proposed development is anticipated to generate a relatively low volume of traffic. Therefore, this access, aligning with the existing access to Glen Oaks, should be treated as driveways, not as an intersection. Sections 8.8 of the TAC GDG discusses the geometric and spacing requirements for driveways.

Section 8.8 illustrates the suggested minimum corner clearance dimensions. Figure 8.8.2. item A (included in Appendix U) suggests that the minimum corner clearance along an arterial road, with a traffic control signal at the crossroad, is 70 metres. The proposed access has been located 120 metres north of the intersection of Ninth Line and Dundas Street, such that it aligns with the existing Glen Oaks Access, and maximizes the distance from the access to the signalized intersection. Therefore, the spacing between the proposed access and the intersection of Ninth Line at Dundas Street exceeds the minimum recommended spacing in TAC GDG Section 8.8, and the proposed driveway is acceptable.

The subject site has limited access options. It has been previously indicated that MTO will not allow an access to this site via an access on Dundas Street. As a result, access to the site is only possible on the Ninth Line frontage. The proposed access has been aligned with the Glen Oaks access (the site directly to the west of the subject site) and has been positioned at the northern end of the property, maximizing the distance between the signalized intersection of Ninth Line at Dundas Street and the proposed driveway.



6.2.2 Medians

There is currently a concrete median extending 92 metres north of the Dundas Street at Ninth Line intersection. This concrete median will be kept for the future horizons. North of the concrete median, where the Glen Oaks Access and proposed site access are located, will be a two-way left turn lane that will facilitate left-turn inbound vehicles to the two sites.

6.2.3 Intersection Alignment

The City of Mississauga's TIS Guidelines have stated that the locations of access points must align with existing intersections and/or opposing access points wherever possible. The site access location satisfies this by aligning with the existing Glen Oaks Access. Glen Oaks Access is also a full-movement access. Since the existing Glen Oaks Access is full-moves, and with the two-way left turn to provided, the site access is also proposed to be a full-movement. Having a right-in / right-out at this location may encourage U-turns. It will also be difficult to enforce the turning restrictions considering the opposite access to which the site access is aligned allows full movements and such restrictions are not compatible with the two-way left turn lane included on the preliminary drawings.

6.2.4 Sightline Requirements

In addition to providing adequate spacing between intersections and driveways, it is necessary to ensure that proper sight distances are achieved utilizing the TAC GDG and confirmed by field measurements. However, as the segment of Ninth Line near the access is a flat and straight road without horizontal or vertical curves. A sightline analysis is not necessary as the geometry of the road does not create impediments to obstruct visibility from the access point to cars approaching on Ninth Line in either the northbound or the southbound direction.

6.2.5 Access Design

The Dymon access forms a westbound approach at the existing Glen Oaks Access at Ninth Line intersection, consisting of a shared left-turn / through / right-turn lane. The eastbound approach Glen Oaks Access has the same configuration. The northbound and southbound approaches are not controlled, and no turn restrictions are present, each of which will consist of a dedicated left-turn, a through lane, and a shared through / right-turn lane by 2031. The operational analysis in Synchro has demonstrated that the longest 95th percentile queue on site is 12 metres.

The TAC Geometric Guide for Canadian Roads indicates that a minimum of 30 metres of clear throat length is required for a light industrial development with a size between 10,000 and 45,000 square metres accessing an arterial road. The measured clear throat distance at the proposed site access on Ninth Line is the distance measured from the edge of asphalt to the first point of on-site vehicular conflict. As the segment of the driveway running in the N-S direction south of the access provides the first point of on-site conflict, the throat length provided will not satisfy the minimum value of 30 metres indicated in the TAC Guidelines.

As the TAC Guidelines requirement will not be met, this driveway has been examined using a first principles approach. As demonstrated in the turning templates, the heavy vehicles will exit the site using the aisle on the north side in the westbound through direction while the N-S driveway will mostly be used by passenger vehicles. The separation of types of vehicles helps improve the site safety as well as the efficiency at the access. The queue lengths imply that there would rarely be more than three passenger vehicles waiting in the queue. As the access and the site driveway are designed to accommodate two-way traffic, the only condition when there is the potential for outbound vehicles to block the access is when vehicles are approaching from both internal driveways and the northbound left-turn vehicles need to wait for westbound through vehicles to clear. As the queue result from Synchro analysis shows that there are only 1 to 2 vehicles on each side, given the frequency of the inbound vehicles, this condition is unlikely to occur.



The access is adequate to accommodate HSUs and passenger vehicles as design vehicles within the site without blocking an adjacent lane of traffic. The HSU will be the most frequent truck type. While the site is designed to accommodate WB-20 trucks, the frequency of these trucks is low. As a result, these trucks are unlikely to encounter other vehicles and are not anticipated to stack in the throat of the access.

The access locations and designs have been evaluated against several criteria. The access has been placed at the only possible location for an access for this site as it fronts two arterial roads. MTO will not permit access from Dundas Street within their permit control area, so the access can only be provided on Ninth Line. As Mississauga specifically requests the newly proposed accesses to align with the existing ones, the only feasible access location on Ninth Line is aligning with the Glen Oaks Access.

7 Transportation Demand Management Plan

Transportation Demand Management (TDM) is a set of measures and procedures implemented to make more efficient use of the transportation system. TDM manages the demands placed on transportation infrastructure using policies, programs, infrastructure improvements, and/or services to influence travel behaviour by modes, time of day, frequency, trip length, cost, etc. Aiming at reducing the reliance on single-occupant vehicle trips, TDM encourages sustainable travel choices by supporting alternatives to driving alone.

This development is forecasted to generate 110 new peak hour person trips or less during the worst peak hour. As the size of the development is small, a TDM Statement with a reduced scope has been prepared below. The TDM statement outlines the TDM measures that will be incorporated into the proposed development.

The proposed development includes a self-storage facility, a co-working office, and industrial condos. Different TDM measures are applicable to different land uses. For the co-working office component, one of the most effective Transportation Demand Management (TDM) measures are access and usability of transit, cycling, and pedestrian facilities.

7.1 Transit Measures

The proposed development is serviced by Oakville Transit along Dundas Street with frequent services on weekdays and during the weekend. The closest stop is within 120 metres' and 200 metres' walking distance for the westbound and eastbound buses, respectively. Currently the service is limited to one local bus route which connects to Oakville GO for access to regional transit. In the future the transit services will be improved as the Dundas BRT will pass through the Study Area. At that time, one of the through lanes in each direction along Dundas Street will be converted to a transit lane. The closest BRT stops are assumed to be located at the Dundas Street at Ninth Line intersection, where the current local bus stops are. With the addition of rapid transit, the site will be provided with a more direct access to long-range regional transit service, enhancing mobility and transit experience along Dundas Street corridor. The combination of regional and local transit will be able to satisfy the transit needs of travelers with different destinations and purposes. The improved transit experience could encourage modal split for transit to increase and modal split for auto drivers decrease.

7.2 Active Mode Measures

The site is currently situated in an area with limited pedestrian and cycling facilities. However, the gaps that are present in sidewalks and cycle lanes are planned to be filled in future horizons as discussed in Section 3.3. Active mode facilities are proposed within the site and connect to existing pedestrian and cycling facilities on Ninth Line. In order to further encourage cycling trips to and from the site, surface and underground bicycle parking has been provided, regardless of land use. As discussed in the parking justification letter, 28 bicycle parking spaces including 16 short-term and 12 long-term spaces will be provided which is more than the minimum required number of



spaces. By providing more bicycle spaces than is required, a reduction in auto dependence will be further encouraged. Bicycle repair stations are also recommended to support the high number of provided bicycle parking spaces and to encourage residents to use a bicycle.

7.3 Parking Measures

As discussed in the parking justification letter, fewer vehicle parking spaces will be provided at the proposed development than what is required by Mississauga's Zoning By-law 0225-2007. The By-law has accounted for some of the site context and existing transit infrastructure, but the rates are too general for the co-working office land uses. The parking provision rates are calculated based on multiple surveys on parking demand and supply at Dymon-operated sites consisting of identical land uses, similar GFAs, and situated within comparable urban environments. Therefore, although the on-site vehicular parking provisions will be less than the zoning by-law requirement, they will be sufficient to meet the projected demand. Lower parking requirements can lower development costs and yield significant cost savings that can be used to implement TDM programs and install TDM supportive infrastructure. Meanwhile, reduced on-site parking will work to reduce auto dependence.

7.4 Mixed-Use and Increased Density

The proposed development is mixed-use, containing self-storage, office, and industrial condos that will be used for various small-scale industrial activities. Compared to the sites with single land uses, the traffic patterns at a mixed-used site are more scattered as different uses have different peak hours. Compared to the single-storey self-storage facilities, Dymon's self-storage allows density intensification on site which increases the leasable and saleable space to serve more customers while keeping the trip generation rate per unit lower than the ITE rates. Mississauga's TIS Guidelines recognize that density intensification is encouraged as revenue generated by the increase in leasable or saleable space can be used to implement TDM programs and install TDM supportive infrastructure.

7.5 Short Trips

Dymon self-storage and co-working office business model requires for them to be located in close proximity to its target market. This means that although the low number of self-storage customer trips are mostly constrained to the auto mode because of the need to transport personal or business belongings, these trips will be made by local residents and business owners, producing minimal vehicle kilometers traveled. This is important to note, as short-distance trips should be treated differently in context of TDM when compared to longer trips, which result in more vehicle kilometers traveled, and oftentimes utilize already constrained inter-city roadways or highways, contributing to congestion, and impacting a larger number of road users. The proximity of Dymon self-storage facilities to the user's homes and businesses also allows for pass-by trips during the peak hours, which has an even lower impact on the overall transportation network efficiency.

8 Conclusions and Recommendations

Introduction and Proposed Site:

- The proposed development of 3855 Dundas Street West is a mixed-use development that consists of a 15,616 m² (168,091 ft²) of self-storage, 97 m² (1,048 ft²) of wine cellar, 5,755 m² (61,941 ft²) of office space, 1,231 m² (13,255 ft²) of industrial condo units, and 1,400 m² (15,065 ft²) of reception and retail spaces that support the self-storage customers. In addition, a 1,464 m² (15,760 ft²) interior parking and loading area provided for industrial condos and self-storage customers.
- A total of 190 vehicle parking spaces will be provided, including 12 barrier-free parking spaces.



- A total of 28 bicycle parking spaces will be provided on site for all uses combined, including 16 short-term and 12 long-term parking spaces.
- The development will also include one loading space in the interior parking / loading area and another on the exterior south of the interior loading area.
- Garbage collection areas are located at the northeast corner of the site and by the curbside across from the exit bay doors of the interior loading area.
- The proposed development will be built and operational by 2026.
- One vehicular access point has been proposed on Ninth Line allowing full movements approximately 145 metres north of Dundas Street East.
- The application for the proposed site is for a Zoning By-Law Amendment.

Existing Conditions:

- Sidewalks or multi-paths are noted on both sides of Ninth Line south of Dundas Street East as well as the south side of Dundas Street East west of Ninth Line within the Study Area.
- Dedicated bike lanes with pavement markings are noted on both sides of Ninth Line south of the Glen Oaks Access and multi-use paths on the south side of Dundas Street East west of Ninth Line.
- Existing Oakville Transit route #24 has service within the Study Area and the closest stops are located at the Dundas Street at Ninth Line intersection.
- Operational analysis on the existing 2023 horizon is based on the 2023 turning movement counts at the Study Area intersections. Model parameters are based on Mississauga's TIS Guidelines and Synchro defaults.
- The existing automobile operational analysis indicates that the Glen Oaks Access at Ninth Line intersection operates with good LOS and short delays while the Dundas Street at Ninth Line intersection is at capacity. The northbound right movement at the Dundas Street at Ninth Line intersection experiences operational constraints during the PM peak hour, reflecting the high volume. Signal optimization, including changing the northbound right movement to a permissive and overlap type, is proposed to improve the LOS and delays at this movement and the intersection overall.

Future Background Conditions:

- Both the full build-out future horizon of 2026 and the full build-out horizon plus 5 years horizon of 2031 were evaluated.
- The trips generated by the background developments of Ninth Line Coptic Church and Ivan Franko Homes in Mississauga, and the residential developments in Joshua Creek Subdivisions in Oakville including Mattamy Joshua Creek Phase 3 and Phase 4, Dunoak Residential Development, ARGO Joshua Creek Development, and Redoak / Capoak Residential Development have been included within the 2026 and 2031 Future Background volumes. The background development traffic volumes are high and contribute to a significant portion of the Future Background traffic volumes.
- New rates were provided by staff from the City of Mississauga as the City's transportation model has been updated since 2018. Compound annual growth rates between 0.5% and 1.5% were applied to all movements along and compounded annual growth rates between 3.0% and 4.5% were applied to Ninth Line through movements. An industry standard 2% growth rate has been applied to Ninth Line turning movements.



- The road network in the 2026 Future Background scenarios will be the same as the Existing. In 2031 Future Background scenarios, Ninth Line north of the Dundas Street East at Ninth Line intersection will be widened from a two-lane road to a four-lane road.
- The automobile operational analysis for both Future Background horizons indicate that the traffic operational performance is much worse than that of the existing horizon during the PM peak hour with the increase in westbound through volumes resulting primarily from the proposed residential developments located along the north side of Dundas Street between Eighth Line and Ninth Line. Multiple overcapacity and critical movements are present at the Dundas Street East at Ninth Line intersection.
- Signal optimization is proposed as a mitigation strategy to be carried out by the Region when reviewing the signals to settle for the best configuration and coordination. However, it will not be efficient enough to improve the LOS for all movements.
- After the planned extension of William Halton Parkway is completed, some of the through traffic along Dundas Street will be diverted and the decrease in travel demand will improve the operational conditions of the Study Area road network.

Site Trip Forecasting:

- Proxy Site Data have been used to determine the trip generation rates at the subject site. These rates are applied to the self-storage, office, and retail components of the proposed development. ITE trip generation rates of general industrial land use have been applied to the industrial condos.
- The proposed development is forecast to generate 110 AM and 94 PM net new two-way vehicle trips in 2026 and 2031. The self-storage and retail / reception component is projected to generate 26 AM and 34 PM net new two-way vehicle trips, and the office component 73 AM and 51 PM trips. The industrial condo is projected to generate 10 AM and 9 PM trips using ITE trip generation rates.
- Existing self-storage facilities and co-working office spaces have been reviewed to determine that the catchment area of the proposed Dymon 3855 Dundas Street development will primarily be the residents and businesses from Oakville north of Highway 403, which means the trips will primarily be local trips from the west. Combined with the existing distribution of local trips from the nearby zones with similar land uses in 2016 TTS, the site trip distribution is estimated to be 10% to the north, 15% to the south, 20% to the east, and 55% to the west.

Future Total Conditions:

- Both accesses were modelled as stop-controlled and consisting of one shared left / through / right lane, although no through traffic were projected for the developments.
- The automobile operational analysis of 2026 and 2031 Future Total horizons indicates the presence of multiple over capacity and critical movements within the Study Area which is consistent with anticipated Future Background conditions.
- Site-generated trips only cause minor increase in the v/c ratios and delays, but they do not change the conditions. Addition of the site generated traffic was observed to have a negligible impact on the operation of the surrounding road network.
- Signal optimization that has been proposed at the Dundas Street at Ninth Line intersection is incorporated. No mitigation measures are proposed to alleviate the traffic conditions except for optimizing the signals. Most of the potential improvements are already planned by the governing authorities.
- The operational conditions at the Site Access / Glen Oaks Access at Ninth Line are projected to have good LOS and delays at individual movements and all queues can be accommodated by the storage lengths.



Site Circulation:

- The site includes a two-way driveway that surrounds the building along the property boundary. The driveway provides access to the interior loading area, the exterior loading dock, the garbage pick-up area, the access ramp to underground parking level, and surface parking spaces.
- AutoTURN 11.0 was used to develop turning templates for garbage trucks and loading trucks. WB-20s and HSUs were tested as design vehicles.
- The accesses, driveways, garbage loading area and drive-in loading area can accommodate the WB-20s and HSUs. All turning paths to and from the site are accommodated by the proposed curbs.

Access Study:

- Only one access is proposed for Dymon 3855 Dundas Street West and is located on Ninth Line and aligned with the existing Glen Oaks Access. It is assumed to operate as an unsignalized full-movement intersection.
- This access is subject to Mississauga's TIS Guidelines and TAC's Geometric Design Guide for Canadian Road.
- This access is approximately 110 metres north of the curb return at the Dundas Street at Ninth Line intersection, shorter than the typical distance required for a full-moves access.
- The originally proposed Dundas Street Access has been removed to minimize the impact on the Highway 403 off ramp.
- The current location is the only possible location for the site access. It is aligned with the Glen Oaks Access on the opposite side of Ninth Line in accordance with Mississauga's Guidelines.
- The measured clear throat distance falls short of the minimum value of 30 metres indicated in the TAC Guidelines, but it will be adequate to accommodate the outbound queue of the vehicles without blocking the inbound vehicles on an adjacent lane of traffic on Ninth Line. The frequency of WB-20s will be low, thus they are unlikely to encounter other vehicles and stack in the throat of the access.

Transportation Demand Management Plan:

• Transit, active mode, and parking transportation demand management plan measures were recommended in order to reduce reliance on single occupant vehicle trips.

The proposed development will have a minor impact on the Study Area road network. Given its location, design, and recommended TDM measures, the proposed development will encourage a movement away from single-occupant vehicles and will therefore seamlessly integrate with the future vision for the surrounding area. It is recommended that, from a transportation perspective, the proposed development application proceeds.



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Terms of Reference



Appendix B

Pre-Study Consultation Checklist

| Description | Information | Section Reference | | |
|--|---|----------------------|--|--|
| Development Information | | | | |
| Development Description (land use, size, and number of phases of development) | Phase 1: a four-storey building including approximately 175,250 square feet of self-storage, 68,600 square feet of office space, and 10,800 square feet of reception / retail space. The development will be completed in a single phase. | 2.3.6 | | |
| Transportation Impact Assess | sment | | | |
| Step 1 – Screening | | | | |
| Type of Application (attach a drawing) | Official Plan Amendment Zoning Amendment Site Plan Control Application Plan of Subdivision Other | 2.3.5 | | |
| Screening Criteria | Trip Generation Trigger Satisfied Location Trigger Satisfied Operational/Safety Trigger Satisfied | | | |
| Type of Study | ✓ Transportation Impact Study ✓ Access Review □ No Additional Study Required | 2.2.1 | | |
| Step 2 – Scoping | | | | |
| Study Area (intersections to be analyzed) Note: The Transportation Consultant is responsible to identify any further intersections impacted as the study progresses. | Ninth Line at Dundas Street East (Existing) Glen Oaks Funeral Homes Access at Ninth Line (Existing) Site Access at Ninth Line (Future, may align with the existing Glen Oaks Funeral Homes Access at Ninth Line) | 2.3.8 | | |
| Horizon Years | □ 5 years from date of TIS □ Interim years ☑ Other: Build-out year 2026 and Build-out plus 5 years 2031 | 2.3.9 | | |
| Analysis Periods | AM weekday peak hour of adjacent roadway PM weekday peak hour of adjacent roadway Saturday peak hour of adjacent roadway AM weekday peak hour of development | 2.3.10 | | |

| Description | Information | Section Reference |
|---|--|----------------------|
| | PM weekday peak hour of development Saturday peak hour of development Other | |
| Input Parameters and Assumptions (potential deviations) | Saturation flow, Peak Hour Factors, Lost Time, Lane Utilization Factor, Analysis Period, Cycle Length, Minimum Green Time, etc. will follow Appendix D of the Mississauga Transportation Impact Study Guidelines Parameters not mentioned in the Guidelines will use the Synchro defaults | 2.3.13 |
| Existing Transportation Conditions | City data sources New data collection: <u>TMCs at Ninth Line at Dundas</u> <u>Street East and Glen Oaks Funeral Homes Access at</u> <u>Ninth Line</u> Other | 2.3.14 |
| Planned Network Improvements (with timing) | Ninth Line to be widened from the existing two-lane cross-section to a four-lane C2 Urban cross-section according to Halton Region TMP (expect to begin in 2025 and be complete by 2031) Dundas Bus Rapid Transit along Dundas Street (construction of Mississauga East expected to begin in 2025, timing of the segment within the Study Area TBD) Bike lanes and boulevard multi-use trails to be added along Ninth Line; boulevard multi-use trails to be added, presumably will be done by 2031) | 2.3.16 |
| Other Planned Developments (per <u>City's Website</u>) | 3033 Dundas Street West Ninth Line Coptic Church 1429 Dundas St E (Oakville) Bressa Residential Development (Oakville) ARGO Joshua Creek (Oakville) Redoak/Capoak Residential Development (Oakville) | 2.3.17 |
| Identification of Mitigation Improvement Measures | Neighbourhood Traffic Management Plan Other: <u>Signal Optimization and Intersection</u> <u>Reconfiguration (if applicable)</u> | 2.3.23 |
| Safety Analysis (any special issues) | No special issues | 2.3.25 |
| Site Access and Circulation (design vehicles) | Passenger Car (P) Light Single Unit Truck (LSU) Medium Single Unit Truck (MSU) Heavy Single Unit Truck (HSU) Pumper Fire Truck WB-20 Tractor Semi-Trailer Truck | 2.3.26 |

| Description | Information | Section Reference |
|--|--|----------------------|
| | Other | |
| Impacts During Construction (any special issues) | No special issues | 2.3.27 |
| Step 3 – Forecasting | | |
| Growth Rate | □ Obtained from City ☑ Historical traffic counts ☑ Travel demand forecasts □ Proposed Growth Rate: | 2.3.15 |
| Site Trip Generation | ITE Trip Generation Manual "First Principles" Observed rates for similar developments in area Other: Observed rates for similar developments also operated by Dymon | 2.3.19 |
| Trip Reductions | Internal capture reductions for mixed-use developments Pass-by reductions Other: reductions for mixed-use developments already captured by the proxy site trip generation rates, no additional trip reduction applied. | 2.3.19 |
| Trip Distribution | Local traffic patterns TTS Travel demand model Population and employment distribution Market analysis of catchment area Other | 2.3.20 |
| Trip Assignment | Local traffic patterns Shortest distance Site layout, access design and logical routing Existing turning movements Other | 2.3.21 |
| Transportation Demand Man | agement Plan | |
| Format | ✓ Within a TIA Report□ Standalone | 3.2.1 |
| Type of Transportation Demand Management Plan | ☑ TDM Statement□ TDM Scheme | 3.2.2 |
| Pedestrian Circulation Plan | | |
| Format | ✓ Within a TIA Report□ Standalone | 4.2.1 |
| Additional Comments | | |

| Description | Information | Section Reference |
|-------------|-------------|----------------------|
| | | |
| | | |
| | | |



2023 Turning Movement Counts





| Intersection: | Ninth Line & Dundas St E |
|---------------|--------------------------|
| Site Code: | 2314400001 |
| Count Date: | May 11, 2023 |

Peak Hour Diagram

| Specified Pe | riod | One Hour Peak | | | | | | | | |
|---------------------|----------|---------------|----------|--|--|--|--|--|--|--|
| From: | 07:00:00 | From: | 08:00:00 | | | | | | | |
| To: | 10:00:00 | To: | 09:00:00 | | | | | | | |

Weather conditions:

Clear

** Signalized Intersection **





🚘 - Cars

起 - Trucks

🖽 - Buses

💑 - Bicycles

Comments



Peak Hour Summary

| Intersection: | Ninth Line & Dundas St E |
|---------------|--------------------------|
| Site Code: | 2314400001 |
| Count Date: | May 11, 2023 |
| Period: | 07:00 - 10:00 |

Peak Hour Data (08:00 - 09:00)

| | North Approach Ninth Line | | | | | | | South Approach Ninth Line | | | | | | | East Approach Dundas St E | | | | | | | West Approach Dundas St E | | | | | |
|----------------|------------------------------|------|------|---|------|-------|------|------------------------------|------|---|------|-------|------|------|------------------------------|------|------|-------|------|------|------|------------------------------|------|-------|------|--|--|
| Start Time | 4 | t | • | ŋ | Peds | Total | • | t | P | ŋ | Peds | Total | • | t | P | ŋ | Peds | Total | 4 | 1 | P | ŋ | Peds | Total | es | | |
| 08:00 | 73 | 131 | 36 | 0 | 0 | 240 | 27 | 81 | 33 | 0 | 0 | 141 | 42 | 211 | 40 | 1 | 0 | 294 | 60 | 458 | 63 | 0 | 0 | 581 | 1256 | | |
| 08:15 | 60 | 167 | 50 | 0 | 0 | 277 | 32 | 66 | 42 | 0 | 0 | 140 | 39 | 270 | 34 | 0 | 0 | 343 | 32 | 639 | 71 | 0 | 0 | 742 | 1502 | | |
| 08:30 | 53 | 131 | 29 | 0 | 0 | 213 | 41 | 85 | 44 | 0 | 0 | 170 | 45 | 225 | 24 | 0 | 0 | 294 | 37 | 454 | 56 | 0 | 0 | 547 | 1224 | | |
| 08:45 | 53 | 145 | 34 | 0 | 0 | 232 | 47 | 83 | 48 | 0 | 0 | 178 | 46 | 255 | 31 | 0 | 0 | 332 | 42 | 504 | 68 | 0 | 0 | 614 | 1356 | | |
| Grand Total | 239 | 574 | 149 | 0 | 0 | 962 | 147 | 315 | 167 | 0 | 0 | 629 | 172 | 961 | 129 | 1 | 0 | 1263 | 171 | 2055 | 258 | 0 | 0 | 2484 | 5338 | | |
| Approach % | 24.8 | 59.7 | 15.5 | 0 | | - | 23.4 | 50.1 | 26.6 | 0 | | - | 13.6 | 76.1 | 10.2 | 0.1 | | - | 6.9 | 82.7 | 10.4 | 0 | | - | | | |
| Totals % | 4.5 | 10.8 | 2.8 | 0 | | 18 | 2.8 | 5.9 | 3.1 | 0 | | 11.8 | 3.2 | 18 | 2.4 | 0 | | 23.7 | 3.2 | 38.5 | 4.8 | 0 | | 46.5 | | | |
| PHF | 0.82 | 0.86 | 0.75 | 0 | | 0.87 | 0.78 | 0.93 | 0.87 | 0 | | 0.88 | 0.93 | 0.89 | 0.81 | 0.25 | | 0.92 | 0.71 | 0.8 | 0.91 | 0 | | 0.84 | 0.89 | | |
| Cars | 233 | 554 | 149 | 0 | | 936 | 132 | 301 | 157 | 0 | | 590 | 161 | 869 | 121 | 1 | | 1152 | 167 | 2023 | 251 | 0 | | 2441 | 5119 | | |
| % Cars | 97.5 | 96.5 | 100 | 0 | | 97.3 | 89.8 | 95.6 | 94 | 0 | | 93.8 | 93.6 | 90.4 | 93.8 | 100 | | 91.2 | 97.7 | 98.4 | 97.3 | 0 | | 98.3 | 95.9 | | |
| Trucks | 5 | 17 | 0 | 0 | | 22 | 13 | 9 | 9 | 0 | | 31 | 10 | 88 | 7 | 0 | | 105 | 3 | 24 | 7 | 0 | | 34 | 192 | | |
| % Trucks | 2.1 | 3 | 0 | 0 | | 2.3 | 8.8 | 2.9 | 5.4 | 0 | | 4.9 | 5.8 | 9.2 | 5.4 | 0 | | 8.3 | 1.8 | 1.2 | 2.7 | 0 | | 1.4 | 3.6 | | |
| Buses | 1 | 3 | 0 | 0 | | 4 | 2 | 5 | 1 | 0 | | 8 | 1 | 4 | 1 | 0 | | 6 | 1 | 8 | 0 | 0 | | 9 | 27 | | |
| % Buses | 0.4 | 0.5 | 0 | 0 | | 0.4 | 1.4 | 1.6 | 0.6 | 0 | | 1.3 | 0.6 | 0.4 | 0.8 | 0 | | 0.5 | 0.6 | 0.4 | 0 | 0 | | 0.4 | 0.5 | | |
| Bicycles | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | | |
| % Bicycles | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | | |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 | | |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | |


| Intersection: | Ninth Line & Dundas St E |
|---------------|--------------------------|
| Site Code: | 2314400001 |
| Count Date: | May 11, 2023 |

Peak Hour Diagram

| Specified Pe | riod | One Hour Peak | | | | | | |
|---------------------|----------|---------------|----------|--|--|--|--|--|
| From: | 16:00:00 | From: | 16:45:00 | | | | | |
| To: | 19:00:00 | To: | 17:45:00 | | | | | |

Weather conditions:

Clear

** Signalized Intersection **





🚘 - Cars

🗔 - Trucks

🖽 - Buses

💑 - Bicycles

Comments



Peak Hour Summary

| Intersection: | Ninth Line & Dundas St E |
|---------------|--------------------------|
| Site Code: | 2314400001 |
| Count Date: | May 11, 2023 |
| Period: | 16:00 - 19:00 |

Peak Hour Data (16:45 - 17:45)

| | North Approach Ninth Line | | | | | | South Approach Ninth Line | | | | | | | East Approach Dundas St E | | | | | | West Approach Dundas St E | | | | | |
|----------------|------------------------------|------|------|---|------|-------|------------------------------|------|------|---|------|-------|------|------------------------------|------|------|------|-------|------|------------------------------|------|-----|------|-------|------|
| Start Time | • | 1 | • | J | Peds | Total | 1 | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | 1 | 1 | • | J | Peds | Total | es |
| 16:45 | 33 | 101 | 35 | 0 | 0 | 169 | 53 | 192 | 136 | 0 | 0 | 381 | 29 | 505 | 55 | 0 | 0 | 589 | 38 | 410 | 54 | 0 | 0 | 502 | 1641 |
| 17:00 | 49 | 82 | 40 | 0 | 0 | 171 | 65 | 214 | 146 | 0 | 2 | 425 | 23 | 490 | 55 | 1 | 0 | 569 | 43 | 355 | 35 | 1 | 0 | 434 | 1599 |
| 17:15 | 52 | 65 | 39 | 0 | 0 | 156 | 67 | 218 | 115 | 0 | 0 | 400 | 29 | 545 | 55 | 2 | 0 | 631 | 36 | 322 | 34 | 1 | 1 | 393 | 1580 |
| 17:30 | 47 | 86 | 42 | 0 | 0 | 175 | 67 | 197 | 129 | 0 | 1 | 393 | 29 | 545 | 67 | 0 | 0 | 641 | 34 | 263 | 19 | 0 | 0 | 316 | 1525 |
| Grand Total | 181 | 334 | 156 | 0 | 0 | 671 | 252 | 821 | 526 | 0 | 3 | 1599 | 110 | 2085 | 232 | 3 | 0 | 2430 | 151 | 1350 | 142 | 2 | 1 | 1645 | 6345 |
| Approach % | 27 | 49.8 | 23.2 | 0 | | - | 15.8 | 51.3 | 32.9 | 0 | | - | 4.5 | 85.8 | 9.5 | 0.1 | | - | 9.2 | 82.1 | 8.6 | 0.1 | | - | |
| Totals % | 2.9 | 5.3 | 2.5 | 0 | | 10.6 | 4 | 12.9 | 8.3 | 0 | | 25.2 | 1.7 | 32.9 | 3.7 | 0 | | 38.3 | 2.4 | 21.3 | 2.2 | 0 | | 25.9 | |
| PHF | 0.87 | 0.83 | 0.93 | 0 | | 0.96 | 0.94 | 0.94 | 0.9 | 0 | | 0.94 | 0.95 | 0.96 | 0.87 | 0.38 | | 0.95 | 0.88 | 0.82 | 0.66 | 0.5 | | 0.82 | 0.97 |
| Cars | 179 | 319 | 156 | 0 | | 654 | 246 | 808 | 513 | 0 | | 1567 | 107 | 2066 | 228 | 3 | | 2404 | 150 | 1310 | 137 | 2 | | 1599 | 6224 |
| % Cars | 98.9 | 95.5 | 100 | 0 | | 97.5 | 97.6 | 98.4 | 97.5 | 0 | | 98 | 97.3 | 99.1 | 98.3 | 100 | | 98.9 | 99.3 | 97 | 96.5 | 100 | | 97.2 | 98.1 |
| Trucks | 2 | 15 | 0 | 0 | | 17 | 6 | 13 | 13 | 0 | | 32 | 3 | 12 | 4 | 0 | | 19 | 1 | 34 | 4 | 0 | | 39 | 107 |
| % Trucks | 1.1 | 4.5 | 0 | 0 | | 2.5 | 2.4 | 1.6 | 2.5 | 0 | | 2 | 2.7 | 0.6 | 1.7 | 0 | | 0.8 | 0.7 | 2.5 | 2.8 | 0 | | 2.4 | 1.7 |
| Buses | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 7 | 0 | 0 | | 7 | 0 | 6 | 1 | 0 | | 7 | 14 |
| % Buses | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0.3 | 0 | 0 | | 0.3 | 0 | 0.4 | 0.7 | 0 | | 0.4 | 0.2 |
| Bicycles | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Bicycles | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 3 | - | | | | | 0 | - | | | | | 1 | - | 4 |
| % Peds | | | | | 0 | - | | | | | 75 | - | | | | | 0 | - | | | | | 25 | - | |



| Intersection: | Ninth Line & Glen Oaks Funeral Home Access |
|---------------|--|
| Site Code: | 2314400002 |
| Count Date: | May 11, 2023 |

Peak Hour Diagram

| Specified Pe | riod | One Hour Peak | | | | | | |
|---------------------|----------|---------------|----------|--|--|--|--|--|
| From: | 07:00:00 | From: | 07:45:00 | | | | | |
| To: | 10:00:00 | To: | 08:45:00 | | | | | |

Weather conditions:

1

5

24

930

960

Ļ

Peds: 0

Clear

0

0

0

0

0

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Peds: 0

** Unsignalized Intersection **









| | Wes | West Approach | | | | | | | | | |
|---|-----|---------------|-------|--|--|--|--|--|--|--|--|
| | Out | In | Total | | | | | | | | |
| ₽ | 7 | 25 | 32 | | | | | | | | |
| G | 0 | 0 | 0 | | | | | | | | |
| | 0 | 0 | 0 | | | | | | | | |
| æ | 0 | 0 | 0 | | | | | | | | |
| | 7 | 25 | 32 | | | | | | | | |

| Peds: 0 | | | | | | | |
|----------|----|-----|----------|--|--|--|--|
| | 4 | t | n | | | | |
| Totals | 20 | 598 | 1 | | | | |
| ⊟ | 20 | 572 | 1 | | | | |
| D | 0 | 20 | 0 | | | | |
| | 0 | 6 | 0 | | | | |
| æ | 0 | 0 | 0 | | | | |
| | | | | | | | |

Ninth Line

| | South Approach | | | | | | | |
|----------|----------------|-----|-------|--|--|--|--|--|
| | Out | In | Total | | | | | |
| <u>⊟</u> | 593 | 935 | 1528 | | | | | |
| D | 20 | 24 | 44 | | | | | |
| | 6 | 5 | 11 | | | | | |
| æ | 0 | 1 | 1 | | | | | |
| | 619 | 965 | 1584 | | | | | |

🔁 - Cars

🖵 - Trucks

🖽 - Buses

💑 - Bicycles

Comments



Peak Hour Summary

| Intersection: | Ninth Line & Glen Oaks Funeral Home Access |
|---------------|--|
| Site Code: | 2314400002 |
| Count Date: | May 11, 2023 |
| Period: | 07:00 - 10:00 |

Peak Hour Data (07:45 - 08:45)

| | | ľ | North A Nint | Approa h Line | ch | | | South Approach Ninth Line | | | | | | East Approach | | | | | | West Approach Glen Oaks Funeral Home Access | | | | | |
|----------------|---|------|-----------------|------------------|------|-------|------|------------------------------|--|------|------|-------|---|---------------|--|---|------|-------|------|--|------|---|------|-------|------|
| Start Time | • | 1 | | J | Peds | Total | 1 | 1 | | J | Peds | Total | • | 1 | | J | Peds | Total | • | 1 | • | J | Peds | Total | es |
| 07:45 | | 230 | 1 | 0 | 0 | 231 | 3 | 157 | | 1 | 0 | 161 | | | | | 0 | | 1 | | 0 | 0 | 0 | 1 | 393 |
| 08:00 | | 241 | 0 | 0 | 0 | 241 | 5 | 176 | | 0 | 0 | 181 | | | | | 0 | | 0 | | 0 | 0 | 0 | 0 | 422 |
| 08:15 | | 283 | 2 | 0 | 0 | 285 | 6 | 124 | | 0 | 0 | 130 | | | | | 0 | | 0 | | 1 | 0 | 0 | 1 | 416 |
| 08:30 | | 206 | 2 | 0 | 0 | 208 | 6 | 141 | | 0 | 0 | 147 | | | | | 0 | | 2 | | 3 | 0 | 0 | 5 | 360 |
| Grand Total | | 960 | 5 | 0 | 0 | 965 | 20 | 598 | | 1 | 0 | 619 | | | | | 0 | 0 | 3 | | 4 | 0 | 0 | 7 | 1591 |
| Approach % | | 99.5 | 0.5 | 0 | | - | 3.2 | 96.6 | | 0.2 | | - | | | | | | - | 42.9 | | 57.1 | 0 | | - | |
| Totals % | | 60.3 | 0.3 | 0 | | 60.7 | 1.3 | 37.6 | | 0.1 | | 38.9 | | | | | | 0 | 0.2 | | 0.3 | 0 | | 0.4 | |
| PHF | | 0.85 | 0.63 | 0 | | 0.85 | 0.83 | 0.85 | | 0.25 | | 0.85 | | | | | | 0 | 0.38 | | 0.33 | 0 | | 0.35 | 0.94 |
| Cars | | 930 | 5 | 0 | | 935 | 20 | 572 | | 1 | | 593 | | | | | | 0 | 3 | | 4 | 0 | | 7 | 1535 |
| % Cars | | 96.9 | 100 | 0 | | 96.9 | 100 | 95.7 | | 100 | | 95.8 | | | | | | 0 | 100 | | 100 | 0 | | 100 | 96.5 |
| Trucks | | 24 | 0 | 0 | | 24 | 0 | 20 | | 0 | | 20 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 44 |
| % Trucks | | 2.5 | 0 | 0 | | 2.5 | 0 | 3.3 | | 0 | | 3.2 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 2.8 |
| Buses | | 5 | 0 | 0 | | 5 | 0 | 6 | | 0 | | 6 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 11 |
| % Buses | | 0.5 | 0 | 0 | | 0.5 | 0 | 1 | | 0 | | 1 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 0.7 |
| Bicycles | | 1 | 0 | 0 | | 1 | 0 | 0 | | 0 | | 0 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 1 |
| % Bicycles | | 0.1 | 0 | 0 | | 0.1 | 0 | 0 | | 0 | | 0 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 0.1 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Ninth Line & Glen Oaks Funeral Home Access |
|---------------|--|
| Site Code: | 2314400002 |
| Count Date: | May 11, 2023 |

Peak Hour Diagram

| Specified Pe | riod | One Hour Pe | eak |
|--------------|----------|-------------|----------|
| From: | 16:00:00 | From: | 16:45:00 |
| To: | 19:00:00 | To: | 17:45:00 |

Weather conditions:

Clear

0

0

0

0

0

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Peds: 0

** Unsignalized Intersection **

Major Road: Ninth Line runs N/S





| | Wes | t Appr | oach |
|---|-----|--------|-------|
| | Out | In | Total |
| | 49 | 23 | 72 |
| G | 0 | 0 | 0 |
| | 0 | 0 | 0 |
| æ | 0 | 0 | 0 |
| | 49 | 23 | 72 |

| | 4 | + | ŋ |
|----------|----|------|---|
| Totals | 18 | 1177 | 4 |
| Ē | 18 | 1159 | 4 |
| P | 0 | 18 | 0 |
| | 0 | 0 | 0 |
| ණි | 0 | 0 | 0 |
| | | | |

Peds: 2

Ninth Line

| | Sout | h Appı | roach |
|----|------|--------|-------|
| | Out | In | Total |
| | 1181 | 664 | 1845 |
| 5 | 18 | 15 | 33 |
| | 0 | 0 | 0 |
| ණ් | 0 | 0 | 0 |
| | 1199 | 679 | 1878 |

🔁 - Cars

🖵 - Trucks

🖽 - Buses

💑 - Bicycles

Comments



Peak Hour Summary

| Intersection: | Ninth Line & Glen Oaks Funeral Home Access |
|---------------|--|
| Site Code: | 2314400002 |
| Count Date: | May 11, 2023 |
| Period: | 16:00 - 19:00 |

Peak Hour Data (16:45 - 17:45)

| | | Ν | North A Nint | Approach Line | ch | | | 9 | South A Nint | Approac h Line | h | | | | East A | pproach | Ì | | G | len Oal | West Aj ks Fune | pproac ral Hon | h ne Acce | SS | Total Vehicl |
|----------------|---|------|-----------------|------------------|------|-------|-----|------|-----------------|-------------------|------|-------|---|---|--------|---------|------|-------|------|---------|--------------------|-------------------|--------------|-------|-----------------|
| Start Time | • | 1 | • | 1 | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | | J | Peds | Total | • | 1 | • | J | Peds | Total | es |
| 16:45 | | 152 | 2 | 0 | 0 | 154 | 3 | 280 | | 1 | 0 | 284 | | | | | 0 | | 3 | | 11 | 0 | 0 | 14 | 452 |
| 17:00 | | 162 | 1 | 0 | 0 | 163 | 2 | 309 | | 3 | 0 | 314 | | | | | 0 | | 2 | | 6 | 0 | 0 | 8 | 485 |
| 17:15 | | 146 | 1 | 0 | 0 | 147 | 4 | 303 | | 0 | 0 | 307 | | | | | 0 | | 3 | | 15 | 0 | 0 | 18 | 472 |
| 17:30 | | 177 | 1 | 0 | 0 | 178 | 9 | 285 | | 0 | 2 | 294 | | | | | 0 | | 3 | | 6 | 0 | 0 | 9 | 481 |
| Grand Total | | 637 | 5 | 0 | 0 | 642 | 18 | 1177 | | 4 | 2 | 1199 | | | | | 0 | 0 | 11 | | 38 | 0 | 0 | 49 | 1890 |
| Approach % | | 99.2 | 0.8 | 0 | | - | 1.5 | 98.2 | | 0.3 | | - | | | | | | - | 22.4 | | 77.6 | 0 | | - | |
| Totals % | | 33.7 | 0.3 | 0 | | 34 | 1 | 62.3 | | 0.2 | | 63.4 | | | | | | 0 | 0.6 | | 2 | 0 | | 2.6 | |
| PHF | | 0.9 | 0.63 | 0 | | 0.9 | 0.5 | 0.95 | | 0.33 | | 0.95 | | | | | | 0 | 0.92 | | 0.63 | 0 | | 0.68 | 0.97 |
| Cars | | 622 | 5 | 0 | | 627 | 18 | 1159 | | 4 | | 1181 | | | | | | 0 | 11 | | 38 | 0 | | 49 | 1857 |
| % Cars | | 97.6 | 100 | 0 | | 97.7 | 100 | 98.5 | | 100 | | 98.5 | | | | | | 0 | 100 | | 100 | 0 | | 100 | 98.3 |
| Trucks | | 15 | 0 | 0 | | 15 | 0 | 18 | | 0 | | 18 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 33 |
| % Trucks | | 2.4 | 0 | 0 | | 2.3 | 0 | 1.5 | | 0 | | 1.5 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 1.7 |
| Buses | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| % Buses | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Bicycles | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| % Bicycles | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | | | | | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 2 | - | | | | | 0 | - | | | | | 0 | - | 2 |
| % Peds | | | | | 0 | - | | | | | 100 | - | | | | | 0 | - | | | | | 0 | - | |



Historical Turning Movement Counts





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Turning Movement Count (1 . DUNDAS ST E & NINTH LINE)

| Chart Time | | | N M | Approad | ch NE | | | | D | E Approa | i ch ∃⊤W | | | | S | Approac | ≿h NE | | | | V D | V Approa | ach ⊺W | | Int. Total (15 min) | Int. Total (1 hr) |
|-------------|--------------|-------------|-------------|---------------|------------|----------------|--------------|-------------|-------------|---------------|--------------------|----------------|--------------|-------------|-------------|---------------|-----------------|----------------|--------------|-------------|-------------|---------------|------------|----------------|------------------------|----------------------|
| Start Time | Right N:W | Thru N:S | Left N:E | U-Turn N:N | Peds N: | Approach Total | Right E:N | Thru E:W | Left E:S | U-Turn E:E | Peds E: | Approach Total | Right S:E | Thru S:N | Left S:W | U-Turn S:S | Peds S: | Approach Total | Right W:S | Thru W:E | Left W:N | U-Turn W:W | Peds W: | Approach Total | | |
| 06:00:00 | 4 | 27 | 21 | 0 | 0 | 52 | 4 | 62 | 5 | 0 | 0 | 71 | 2 | 7 | 6 | 0 | 0 | 15 | 41 | 238 | 6 | 0 | 0 | 285 | 423 | |
| 06:15:00 | 4 | 50 | 28 | 0 | 0 | 82 | 8 | 101 | 7 | 1 | 0 | 117 | 11 | 15 | 19 | 0 | 0 | 45 | 43 | 300 | 12 | 0 | 0 | 355 | 599 | |
| 06:30:00 | 9 | 50 | 45 | 0 | 0 | 104 | 5 | 136 | 9 | 1 | 0 | 151 | 11 | 27 | 13 | 0 | 0 | 51 | 59 | 371 | 13 | 0 | 0 | 443 | 749 | |
| 06:45:00 | 8 | 78 | 41 | 0 | 0 | 127 | 13 | 180 | 10 | 0 | 0 | 203 | 17 | 15 | 23 | 0 | 0 | 55 | 59 | 449 | 23 | 0 | 0 | 531 | 916 | 2687 |
| 07:00:00 | 9 | 70 | 35 | 0 | 0 | 114 | 11 | 163 | 7 | 1 | 0 | 182 | 17 | 48 | 28 | 0 | 1 | 93 | 50 | 405 | 29 | 0 | 0 | 484 | 873 | 3137 |
| 07:15:00 | 8 | 89 | 47 | 0 | 0 | 144 | 13 | 177 | 11 | 0 | 0 | 201 | 25 | 66 | 22 | 0 | 0 | 113 | 71 | 615 | 44 | 0 | 0 | 730 | 1188 | 3726 |
| 07:30:00 | 13 | 131 | 54 | 0 | 0 | 198 | 32 | 210 | 24 | 0 | 0 | 266 | 43 | 68 | 30 | 0 | 0 | 141 | 59 | 562 | 67 | 0 | 0 | 688 | 1293 | 4270 |
| 07:45:00 | 19 | 159 | 71 | 0 | 0 | 249 | 13 | 227 | 42 | 0 | 0 | 282 | 43 | 99 | 31 | 0 | 0 | 173 | 86 | 584 | 51 | 0 | 0 | 721 | 1425 | 4779 |
| 08:00:00 | 21 | 132 | 55 | 0 | 0 | 208 | 41 | 218 | 47 | 0 | 0 | 306 | 30 | 66 | 37 | 0 | 0 | 133 | 74 | 601 | 59 | 0 | 0 | 734 | 1381 | 5287 |
| 08:15:00 | 36 | 140 | 56 | 0 | 0 | 232 | 48 | 230 | 37 | 0 | 0 | 315 | 36 | 82 | 43 | 0 | 0 | 161 | 92 | 523 | 65 | 0 | 0 | 680 | 1388 | 5487 |
| 08:30:00 | 40 | 117 | 61 | 0 | 0 | 218 | 26 | 173 | 28 | 0 | 0 | 227 | 39 | 64 | 53 | 0 | 0 | 156 | 95 | 561 | 57 | 1 | 0 | 714 | 1315 | 5509 |
| 08:45:00 | 32 | 112 | 49 | 0 | 0 | 193 | 20 | 221 | 17 | 1 | 0 | 259 | 30 | 57 | 40 | 0 | 0 | 127 | 84 | 507 | 47 | 0 | 0 | 638 | 1217 | 5301 |
| ***BREAK | *** | | | | | | | | | | | - | | | | | | | | | | | | | | |
| 15:00:00 | 31 | 47 | 26 | 0 | 0 | 104 | 49 | 474 | 36 | 4 | 0 | 563 | 44 | 95 | 75 | 0 | 0 | 214 | 33 | 266 | 27 | 0 | 0 | 326 | 1207 | |
| 15:15:00 | 40 | 60 | 30 | 0 | 0 | 130 | 34 | 414 | 33 | 2 | 0 | 483 | 63 | 113 | 80 | 0 | 0 | 256 | 44 | 306 | 33 | 0 | 0 | 383 | 1252 | |
| 15:30:00 | 47 | 79 | 30 | 0 | 1 | 156 | 46 | 477 | 26 | 1 | 0 | 550 | 76 | 111 | 71 | 0 | 0 | 258 | 44 | 314 | 34 | 0 | 0 | 392 | 1356 | |
| 15:45:00 | 51 | 66 | 23 | 0 | 0 | 140 | 44 | 468 | 31 | 2 | 0 | 545 | 115 | 149 | 79 | 0 | 0 | 343 | 35 | 275 | 42 | 0 | 0 | 352 | 1380 | 5195 |
| 16:00:00 | 63 | 67 | 37 | 0 | 0 | 167 | 43 | 548 | 33 | 2 | 1 | 626 | 156 | 147 | 68 | 0 | 2 | 371 | 38 | 310 | 26 | 0 | 0 | 374 | 1538 | 5526 |
| 16:15:00 | 54 | 65 | 27 | 0 | 0 | 146 | 29 | 558 | 24 | 1 | 1 | 612 | 164 | 140 | 100 | 0 | 1 | 404 | 38 | 301 | 28 | 0 | 0 | 367 | 1529 | 5803 |
| 16:30:00 | 52 | 74 | 35 | 0 | 0 | 161 | 28 | 450 | 36 | 0 | 0 | 514 | 178 | 177 | 87 | 0 | 0 | 442 | 35 | 284 | 24 | 0 | 0 | 343 | 1460 | 5907 |
| 16:45:00 | 57 | 78 | 30 | 0 | 0 | 165 | 31 | 574 | 28 | 0 | 0 | 633 | 194 | 157 | 61 | 0 | 1 | 412 | 47 | 374 | 31 | 0 | 0 | 452 | 1662 | 6189 |
| 17:00:00 | 62 | 76 | 33 | 0 | 0 | 171 | 38 | 689 | 30 | 0 | 1 | 757 | 170 | 171 | 88 | 0 | 0 | 429 | 29 | 346 | 32 | 1 | 0 | 408 | 1765 | 6416 |
| 17:15:00 | 70 | 68 | 36 | 0 | 0 | 174 | 33 | 613 | 29 | 1 | 0 | 676 | 174 | 199 | 66 | 0 | 1 | 439 | 45 | 378 | 39 | 0 | 0 | 462 | 1751 | 6638 |
| 17:30:00 | 44 | 78 | 39 | 0 | 0 | 161 | 40 | 697 | 27 | 1 | 0 | 765 | 153 | 156 | 84 | 0 | 0 | 393 | 38 | 392 | 35 | 0 | 0 | 465 | 1784 | 6962 |
| 17:45:00 | 54 | 74 | 22 | 0 | 0 | 150 | 33 | 601 | 35 | 0 | 0 | 669 | 174 | 190 | 92 | 0 | 0 | 456 | 40 | 323 | 42 | 0 | 0 | 405 | 1680 | 6980 |
| 18:00:00 | 57 | 62 | 45 | 0 | 0 | 164 | 36 | 539 | 28 | 2 | 0 | 605 | 110 | 123 | 69 | 0 | 0 | 302 | 43 | 304 | 31 | 0 | 0 | 378 | 1449 | 6664 |
| 18:15:00 | 41 | 61 | 21 | 0 | 0 | 123 | 38 | 578 | 35 | 4 | 1 | 655 | 102 | 86 | 64 | 0 | 0 | 252 | 47 | 345 | 22 | 1 | 0 | 415 | 1445 | 6358 |
| 18:30:00 | 38 | 53 | 30 | 0 | 0 | 121 | 34 | 485 | 28 | 1 | 0 | 548 | 78 | 98 | 70 | 0 | 1 | 246 | 39 | 310 | 18 | 1 | 0 | 368 | 1283 | 5857 |
| 18:45:00 | 14 | 44 | 25 | 0 | 0 | 83 | 42 | 442 | 37 | 1 | 0 | 522 | 50 | 86 | 62 | 0 | 0 | 198 | 32 | 323 | 30 | 0 | 0 | 385 | 1188 | 5365 |
| Grand Total | 978 | 2207 | 1052 | 0 | 1 | 4237 | 832 | 10705 | 740 | 26 | 4 | 12303 | 2305 | 2812 | 1561 | 0 | 7 | 6678 | 1440 | 10867 | 967 | 4 | 0 | 13278 | 36496 | - |
| Approach% | 23.1% | 52.1% | 24.8% | 0% | | - | 6.8% | 87% | 6% | 0.2% | | - | 34.5% | 42.1% | 23.4% | 0% | | - | 10.8% | 81.8% | 7.3% | 0% | | - | - | - |

Turning Movement Count

Page 1 of 6

| | nor | -tru | m | | | | | | Lo | Turning I cation Name: DU | Movem NDAS \$ | ent Cou ST E & | nt NINTH | LINE | | | | | | | Crozier & As | ssociates |
|-----------|------|------|------|----|-------|------|-------|------|---------|------------------------------|------------------|-------------------|-------------|-------------|-------|------|-------|------|----|-------|--------------|-----------|
| | per | uu | | | | | | | Date: T | hu, Oct 25, 2018 | Deplo | yment l | _ead: W | alter Fugaj | | | | | | | | , , |
| Totals % | 2.7% | 6% | 2.9% | 0% | 11.6% | 2.3% | 29.3% | 2% | 0.1% | 33.7% | 6.3% | 7.7% | 4.3% | 0% | 18.3% | 3.9% | 29.8% | 2.6% | 0% | 36.4% | - | - |
| Heavy | 20 | 54 | 18 | 0 | - | 27 | 333 | 25 | 0 | - | 124 | 73 | 63 | 0 | - | 58 | 273 | 13 | 0 | - | - | - |
| Heavy % | 2% | 2.4% | 1.7% | 0% | - | 3.2% | 3.1% | 3.4% | 0% | - | 5.4% | 2.6% | 4% | 0% | - | 4% | 2.5% | 1.3% | 0% | - | - | - |
| Bicycles | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |
| Bicycle % | - | - | - | - | | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - |



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Peak Hour: 07:45 AM - 08:45 AM Weather: Mostly Cloudy (2.8 °C)

| Start Time | | | N N | Approad | ≿h NE | | | | E DL | Approa | ch ⊺W | | | | S N | Approac | :h IE | | | | W DL | Approac | h W | | Int. Total (15 min) |
|------------------------|-------|-------|--------|---------|-----------------|----------------|-------|-------|---------|--------|----------|----------------|-------|-------|--------|---------|----------|----------------|-------|-------|----------------|---------|--------|----------------|------------------------|
| | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | |
| 07:45:00 | 19 | 159 | 71 | 0 | 0 | 249 | 13 | 227 | 42 | 0 | 0 | 282 | 43 | 99 | 31 | 0 | 0 | 173 | 86 | 584 | 51 | 0 | 0 | 721 | 1425 |
| 08:00:00 | 21 | 132 | 55 | 0 | 0 | 208 | 41 | 218 | 47 | 0 | 0 | 306 | 30 | 66 | 37 | 0 | 0 | 133 | 74 | 601 | 59 | 0 | 0 | 734 | 1381 |
| 08:15:00 | 36 | 140 | 56 | 0 | 0 | 232 | 48 | 230 | 37 | 0 | 0 | 315 | 36 | 82 | 43 | 0 | 0 | 161 | 92 | 523 | 65 | 0 | 0 | 680 | 1388 |
| 08:30:00 | 40 | 117 | 61 | 0 | 0 | 218 | 26 | 173 | 28 | 0 | 0 | 227 | 39 | 64 | 53 | 0 | 0 | 156 | 95 | 561 | 57 | 1 | 0 | 714 | 1315 |
| Grand Total | 116 | 548 | 243 | 0 | 0 | 907 | 128 | 848 | 154 | 0 | 0 | 1130 | 148 | 311 | 164 | 0 | 0 | 623 | 347 | 2269 | 232 | 1 | 0 | 2849 | 5509 |
| Approach% | 12.8% | 60.4% | 26.8% | 0% | | - | 11.3% | 75% | 13.6% | 0% | | - | 23.8% | 49.9% | 26.3% | 0% | | - | 12.2% | 79.6% | 8.1% | 0% | | - | - |
| Totals % | 2.1% | 9.9% | 4.4% | 0% | | 16.5% | 2.3% | 15.4% | 2.8% | 0% | | 20.5% | 2.7% | 5.6% | 3% | 0% | | 11.3% | 6.3% | 41.2% | 4.2% | 0% | | 51.7% | - |
| PHF | 0.73 | 0.86 | 0.86 | 0 | | 0.91 | 0.67 | 0.92 | 0.82 | 0 | | 0.9 | 0.86 | 0.79 | 0.77 | 0 | | 0.9 | 0.91 | 0.94 | 0.89 | 0.25 | | 0.97 | |
| Heavy | 4 | 12 | 2 | 0 | | 18 | 3 | 97 | 7 | 0 | | 107 | 9 | 14 | 11 | 0 | | 34 | 17 | 27 | 3 | 0 | | 47 | - |
| Heavy % | 3.4% | 2.2% | 0.8% | 0% | | 2% | 2.3% | 11.4% | 4.5% | 0% | | 9.5% | 6.1% | 4.5% | 6.7% | 0% | | 5.5% | 4.9% | 1.2% | 1.3% | 0% | | 1.6% | - |
| Lights | 112 | 535 | 241 | 0 | | 888 | 125 | 751 | 147 | 0 | | 1023 | 139 | 297 | 153 | 0 | | 589 | 330 | 2242 | 229 | 1 | | 2802 | - |
| Lights % | 96.6% | 97.6% | 99.2% | 0% | | 97.9% | 97.7% | 88.6% | 95.5% | 0% | | 90.5% | 93.9% | 95.5% | 93.3% | 0% | | 94.5% | 95.1% | 98.8% | 98.7% | 100% | | 98.4% | - |
| Single-Unit Trucks | 1 | 8 | 1 | 0 | | 10 | 3 | 52 | 6 | 0 | | 61 | 3 | 6 | 7 | 0 | | 16 | 4 | 14 | 0 | 0 | | 18 | - |
| Single-Unit Trucks % | 0.9% | 1.5% | 0.4% | 0% | | 1.1% | 2.3% | 6.1% | 3.9% | 0% | | 5.4% | 2% | 1.9% | 4.3% | 0% | | 2.6% | 1.2% | 0.6% | 0% | 0% | | 0.6% | - |
| Buses | 3 | 3 | 0 | 0 | | 6 | 0 | 5 | 0 | 0 | | 5 | 2 | 3 | 1 | 0 | | 6 | 3 | 5 | 2 | 0 | | 10 | - |
| Buses % | 2.6% | 0.5% | 0% | 0% | | 0.7% | 0% | 0.6% | 0% | 0% | | 0.4% | 1.4% | 1% | 0.6% | 0% | | 1% | 0.9% | 0.2% | 0.9% | 0% | | 0.4% | - |
| Articulated Trucks | 0 | 1 | 1 | 0 | | 2 | 0 | 40 | 1 | 0 | | 41 | 4 | 5 | 3 | 0 | | 12 | 10 | 8 | 1 | 0 | | 19 | - |
| Articulated Trucks % | 0% | 0.2% | 0.4% | 0% | | 0.2% | 0% | 4.7% | 0.6% | 0% | | 3.6% | 2.7% | 1.6% | 1.8% | 0% | | 1.9% | 2.9% | 0.4% | 0.4% | 0% | | 0.7% | - |
| Bicycles on Road | 0 | 1 | 0 | 0 | | 1 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | - |
| Bicycles on Road % | 0% | 0.2% | 0% | 0% | | 0.1% | 0% | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | 0% | | 0% | - |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| Pedestrians% | - | - | - | - | 0% | | - | - | - | - | 0% | | - | - | - | - | 0% | | - | - | - | - | 0% | | - |
| Bicycles on Crosswalk | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk% | - | - | - | - | 0% | | - | - | - | - | 0% | | - | - | - | - | 0% | | - | - | - | - | 0% | | - |



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Peak Hour: 05:00 PM - 06:00 PM Weather: Overcast (7.4 °C)

| Start Time | | | и 1 | I Approad | sh NE | | | | E DL | Approa | ch ⊺W | | | | S N | Approac | h E | | | | W Dl | / Approa JNDAS S⊺ | ch ⊺W | | Int. Total (15 min) |
|------------------------|-------|-------|--------|-----------|----------|----------------|-------|-------|---------|--------|----------|----------------|-------|-------|--------|----------------|--------|----------------|-------|-------|----------------|-----------------------------|----------|----------------|------------------------|
| | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | |
| 17:00:00 | 62 | 76 | 33 | 0 | 0 | 171 | 38 | 689 | 30 | 0 | 1 | 757 | 170 | 171 | 88 | 0 | 0 | 429 | 29 | 346 | 32 | 1 | 0 | 408 | 1765 |
| 17:15:00 | 70 | 68 | 36 | 0 | 0 | 174 | 33 | 613 | 29 | 1 | 0 | 676 | 174 | 199 | 66 | 0 | 1 | 439 | 45 | 378 | 39 | 0 | 0 | 462 | 1751 |
| 17:30:00 | 44 | 78 | 39 | 0 | 0 | 161 | 40 | 697 | 27 | 1 | 0 | 765 | 153 | 156 | 84 | 0 | 0 | 393 | 38 | 392 | 35 | 0 | 0 | 465 | 1784 |
| 17:45:00 | 54 | 74 | 22 | 0 | 0 | 150 | 33 | 601 | 35 | 0 | 0 | 669 | 174 | 190 | 92 | 0 | 0 | 456 | 40 | 323 | 42 | 0 | 0 | 405 | 1680 |
| Grand Total | 230 | 296 | 130 | 0 | 0 | 656 | 144 | 2600 | 121 | 2 | 1 | 2867 | 671 | 716 | 330 | 0 | 1 | 1717 | 152 | 1439 | 148 | 1 | 0 | 1740 | 6980 |
| Approach% | 35.1% | 45.1% | 19.8% | 0% | | - | 5% | 90.7% | 4.2% | 0.1% | | - | 39.1% | 41.7% | 19.2% | 0% | | - | 8.7% | 82.7% | 8.5% | 0.1% | | - | - |
| Totals % | 3.3% | 4.2% | 1.9% | 0% | | 9.4% | 2.1% | 37.2% | 1.7% | 0% | | 41.1% | 9.6% | 10.3% | 4.7% | 0% | | 24.6% | 2.2% | 20.6% | 2.1% | 0% | | 24.9% | - |
| PHF | 0.82 | 0.95 | 0.83 | 0 | | 0.94 | 0.9 | 0.93 | 0.86 | 0.5 | | 0.94 | 0.96 | 0.9 | 0.9 | 0 | | 0.94 | 0.84 | 0.92 | 0.88 | 0.25 | | 0.94 | - |
| Heavy | 0 | 4 | 1 | 0 | | 5 | 2 | 24 | 3 | 0 | | 29 | 37 | 9 | 6 | 0 | | 52 | 3 | 50 | 1 | 0 | | 54 | - |
| Heavy % | 0% | 1.4% | 0.8% | 0% | | 0.8% | 1.4% | 0.9% | 2.5% | 0% | | 1% | 5.5% | 1.3% | 1.8% | 0% | | 3% | 2% | 3.5% | 0.7% | 0% | | 3.1% | - |
| Lights | 230 | 292 | 129 | 0 | | 651 | 142 | 2576 | 118 | 2 | | 2838 | 634 | 707 | 324 | 0 | | 1665 | 149 | 1389 | 147 | 1 | | 1686 | - |
| Lights % | 100% | 98.6% | 99.2% | 0% | | 99.2% | 98.6% | 99.1% | 97.5% | 100% | | 99% | 94.5% | 98.7% | 98.2% | 0% | | 97% | 98% | 96.5% | 99.3% | 100% | | 96.9% | - |
| Single-Unit Trucks | 0 | 4 | 0 | 0 | | 4 | 1 | 9 | 0 | 0 | | 10 | 17 | 6 | 4 | 0 | | 27 | 1 | 26 | 1 | 0 | | 28 | - |
| Single-Unit Trucks % | 0% | 1.4% | 0% | 0% | | 0.6% | 0.7% | 0.3% | 0% | 0% | | 0.3% | 2.5% | 0.8% | 1.2% | 0% | | 1.6% | 0.7% | 1.8% | 0.7% | 0% | | 1.6% | - |
| Buses | 0 | 0 | 0 | 0 | | 0 | 0 | 6 | 0 | 0 | | 6 | 1 | 1 | 0 | 0 | | 2 | 0 | 5 | 0 | 0 | | 5 | - |
| Buses % | 0% | 0% | 0% | 0% | | 0% | 0% | 0.2% | 0% | 0% | | 0.2% | 0.1% | 0.1% | 0% | 0% | | 0.1% | 0% | 0.3% | 0% | 0% | | 0.3% | - |
| Articulated Trucks | 0 | 0 | 1 | 0 | | 1 | 1 | 9 | 3 | 0 | | 13 | 19 | 2 | 2 | 0 | | 23 | 2 | 19 | 0 | 0 | | 21 | - |
| Articulated Trucks % | 0% | 0% | 0.8% | 0% | | 0.2% | 0.7% | 0.3% | 2.5% | 0% | | 0.5% | 2.8% | 0.3% | 0.6% | 0% | | 1.3% | 1.3% | 1.3% | 0% | 0% | | 1.2% | - |
| Bicycles on Road | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | - |
| Bicycles on Road % | 0% | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | 0% | | 0% | - |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 1 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| Pedestrians% | - | - | - | - | 0% | | - | - | - | - | 50% | | - | - | - | - | 0% | | - | - | - | - | 0% | | - |
| Bicycles on Crosswalk | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 1 | - | - | - | - | - | 0 | - | - |
| Bicycles on Crosswalk% | - | - | - | - | 0% | | - | - | - | - | 0% | | - | - | - | - | 50% | | - | - | - | - | 0% | | - |











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Turning Movement Count (1 . DUNDAS ST E & NINTH LINE)

| | | | N N | Approad | sh NE | | | | C | E Approa | a ch STE | | | | S I | S Approad NINTH LIN | ch NE | | | | I | W Appro DUNDAS : | ach ST E | | Int. Total (15 min) | Int. Total (1 hr) |
|-------------|--------------|-------------|-------------|---------------|------------|----------------|--------------|-------------|-------------|---------------|--------------------|----------------|--------------|-------------|-------------|------------------------|------------|----------------|--------------|-------------|-------------|---------------------|--------------------|----------------|------------------------|----------------------|
| Start Time | Right N:W | Thru N:S | Left N:E | U-Turn N:N | Peds N: | Approach Total | Right E:N | Thru E:W | Left E:S | U-Turn E:E | Peds E: | Approach Total | Right S:E | Thru S:N | Left S:W | U-Turn S:S | Peds S: | Approach Total | Right W:S | Thru W:E | Left W:N | U-Turn W:W | Peds W: | Approach Total | | |
| 10:00:00 | 32 | 44 | 43 | 1 | 0 | 120 | 33 | 227 | 10 | 1 | 1 | 271 | 27 | 36 | 30 | 0 | 1 | 93 | 45 | 350 | 20 | 0 | 0 | 415 | 899 | |
| 10:15:00 | 24 | 37 | 29 | 0 | 0 | 90 | 19 | 244 | 15 | 0 | 0 | 278 | 18 | 29 | 25 | 0 | 0 | 72 | 34 | 402 | 22 | 0 | 0 | 458 | 898 | |
| 10:30:00 | 16 | 36 | 32 | 0 | 0 | 84 | 33 | 275 | 17 | 0 | 0 | 325 | 37 | 41 | 25 | 0 | 0 | 103 | 46 | 362 | 25 | 0 | 0 | 433 | 945 | |
| 10:45:00 | 16 | 45 | 46 | 0 | 0 | 107 | 23 | 272 | 26 | 1 | 0 | 322 | 26 | 55 | 37 | 0 | 0 | 118 | 36 | 397 | 32 | 0 | 0 | 465 | 1012 | 3754 |
| 11:00:00 | 23 | 35 | 40 | 0 | 0 | 98 | 31 | 310 | 25 | 0 | 0 | 366 | 32 | 34 | 36 | 0 | 0 | 102 | 62 | 418 | 28 | 0 | 0 | 508 | 1074 | 3929 |
| 11:15:00 | 19 | 30 | 27 | 0 | 0 | 76 | 26 | 394 | 21 | 1 | 0 | 442 | 30 | 43 | 31 | 0 | 0 | 104 | 44 | 397 | 26 | 1 | 0 | 468 | 1090 | 4121 |
| 11:30:00 | 25 | 41 | 45 | 0 | 0 | 111 | 31 | 341 | 20 | 5 | 0 | 397 | 34 | 63 | 25 | 0 | 0 | 122 | 34 | 408 | 25 | 0 | 0 | 467 | 1097 | 4273 |
| 11:45:00 | 26 | 41 | 27 | 0 | 0 | 94 | 55 | 379 | 28 | 1 | 0 | 463 | 26 | 48 | 36 | 0 | 0 | 110 | 42 | 428 | 34 | 0 | 0 | 504 | 1171 | 4432 |
| 12:00:00 | 39 | 53 | 42 | 0 | 0 | 134 | 58 | 338 | 36 | 1 | 0 | 433 | 33 | 57 | 33 | 1 | 0 | 124 | 47 | 370 | 32 | 0 | 0 | 449 | 1140 | 4498 |
| 12:15:00 | 25 | 47 | 48 | 0 | 0 | 120 | 60 | 350 | 26 | 2 | 0 | 438 | 30 | 71 | 26 | 0 | 0 | 127 | 48 | 460 | 28 | 0 | 0 | 536 | 1221 | 4629 |
| 12:30:00 | 40 | 46 | 33 | 0 | 0 | 119 | 63 | 436 | 34 | 0 | 0 | 533 | 31 | 67 | 30 | 0 | 0 | 128 | 57 | 427 | 40 | 0 | 0 | 524 | 1304 | 4836 |
| 12:45:00 | 44 | 50 | 45 | 0 | 0 | 139 | 66 | 352 | 43 | 2 | 0 | 463 | 34 | 73 | 40 | 0 | 0 | 147 | 48 | 418 | 43 | 0 | 0 | 509 | 1258 | 4923 |
| 13:00:00 | 52 | 45 | 45 | 0 | 0 | 142 | 58 | 413 | 29 | 5 | 0 | 505 | 30 | 53 | 50 | 0 | 0 | 133 | 56 | 407 | 31 | 0 | 0 | 494 | 1274 | 5057 |
| 13:15:00 | 30 | 52 | 39 | 0 | 0 | 121 | 25 | 424 | 24 | 3 | 0 | 476 | 20 | 38 | 35 | 0 | 0 | 93 | 51 | 386 | 37 | 1 | 0 | 475 | 1165 | 5001 |
| 13:30:00 | 20 | 42 | 45 | 0 | 0 | 107 | 36 | 353 | 25 | 4 | 0 | 418 | 32 | 58 | 22 | 0 | 0 | 112 | 48 | 404 | 26 | 1 | 0 | 479 | 1116 | 4813 |
| 13:45:00 | 23 | 37 | 39 | 0 | 0 | 99 | 39 | 427 | 34 | 1 | 0 | 501 | 40 | 40 | 33 | 1 | 0 | 114 | 55 | 410 | 23 | 0 | 0 | 488 | 1202 | 4757 |
| 14:00:00 | 39 | 52 | 56 | 0 | 0 | 147 | 56 | 368 | 36 | 3 | 0 | 463 | 37 | 83 | 32 | 0 | 0 | 152 | 33 | 345 | 23 | 0 | 0 | 401 | 1163 | 4646 |
| 14:15:00 | 61 | 50 | 46 | 0 | 0 | 157 | 57 | 385 | 35 | 3 | 0 | 480 | 32 | 46 | 36 | 0 | 0 | 114 | 46 | 442 | 35 | 0 | 0 | 523 | 1274 | 4755 |
| 14:30:00 | 40 | 64 | 53 | 0 | 0 | 157 | 34 | 470 | 29 | 1 | 0 | 534 | 30 | 47 | 39 | 0 | 0 | 116 | 45 | 386 | 26 | 0 | 0 | 457 | 1264 | 4903 |
| 14:45:00 | 41 | 39 | 62 | 0 | 0 | 142 | 41 | 406 | 24 | 1 | 0 | 472 | 35 | 60 | 45 | 0 | 0 | 140 | 56 | 391 | 35 | 0 | 0 | 482 | 1236 | 4937 |
| 15:00:00 | 26 | 50 | 45 | 0 | 0 | 121 | 45 | 455 | 35 | 1 | 0 | 536 | 45 | 59 | 39 | 0 | 0 | 143 | 50 | 398 | 30 | 0 | 0 | 478 | 1278 | 5052 |
| 15:15:00 | 39 | 49 | 41 | 0 | 0 | 129 | 42 | 490 | 20 | 1 | 0 | 553 | 29 | 62 | 30 | 0 | 0 | 121 | 49 | 379 | 26 | 0 | 0 | 454 | 1257 | 5035 |
| 15:30:00 | 28 | 31 | 33 | 0 | 0 | 92 | 34 | 430 | 26 | 2 | 0 | 492 | 32 | 65 | 30 | 0 | 0 | 127 | 48 | 378 | 33 | 0 | 0 | 459 | 1170 | 4941 |
| 15:45:00 | 20 | 43 | 42 | 0 | 0 | 105 | 33 | 505 | 31 | 2 | 0 | 571 | 27 | 58 | 35 | 0 | 0 | 120 | 40 | 350 | 27 | 0 | 0 | 417 | 1213 | 4918 |
| 16:00:00 | 27 | 36 | 24 | 0 | 0 | 87 | 43 | 454 | 20 | 1 | 0 | 518 | 29 | 58 | 35 | 0 | 0 | 122 | 37 | 368 | 29 | 0 | 0 | 434 | 1161 | 4801 |
| 16:15:00 | 30 | 51 | 41 | 0 | 0 | 122 | 33 | 406 | 29 | 3 | 0 | 471 | 31 | 87 | 31 | 0 | 0 | 149 | 40 | 422 | 30 | 0 | 0 | 492 | 1234 | 4778 |
| 16:30:00 | 29 | 50 | 30 | 0 | 0 | 109 | 51 | 505 | 23 | 1 | 0 | 580 | 23 | 59 | 37 | 0 | 0 | 119 | 37 | 368 | 31 | 0 | 0 | 436 | 1244 | 4852 |
| 16:45:00 | 19 | 64 | 31 | 0 | 0 | 114 | 39 | 413 | 31 | 1 | 0 | 484 | 24 | 61 | 40 | 0 | 0 | 125 | 47 | 310 | 45 | 0 | 0 | 402 | 1125 | 4764 |
| Grand Total | 853 | 1260 | 1129 | 1 | 0 | 3243 | 1164 | 10822 | 752 | 47 | 1 | 12785 | 854 | 1551 | 943 | 2 | 1 | 3350 | 1281 | 10981 | 842 | 3 | 0 | 13107 | 32485 | - |
| Approach% | 26.3% | 38.9% | 34.8% | 0% | | - | 9.1% | 84.6% | 5.9% | 0.4% | | | 25.5% | 46.3% | 28.1% | 0.1% | | - | 9.8% | 83.8% | 6.4% | 0% | | - | - | - |
| Totals % | 2.6% | 3.9% | 3.5% | 0% | | 10% | 3.6% | 33.3% | 2.3% | 0.1% | | 39.4% | 2.6% | 4.8% | 2.9% | 0% | | 10.3% | 3.9% | 33.8% | 2.6% | 0% | | 40.3% | - | - |

| G : | Spectrum |
|------------|----------|
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| Heavy | 6 | 11 | 11 | 0 | - | 15 | 74 | 7 | 0 | - | 6 | 16 | 15 | 0 | - | | 14 | 99 | 6 | 0 | - | - | - |
|-----------|------|------|----|----|---|------|------|------|----|---|------|----|------|----|---|---|-----|------|------|----|---|---|---|
| Heavy % | 0.7% | 0.9% | 1% | 0% | - | 1.3% | 0.7% | 0.9% | 0% | - | 0.7% | 1% | 1.6% | 0% | - | 1 | .1% | 0.9% | 0.7% | 0% | - | - | - |
| Bicycles | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | | - | - | - | - | - | - | - |
| Bicycle % | - | - | - | - | - | - | - | - | - | - | - | - | - | - | - | | - | - | - | - | - | - | - |

Crozier & Associates

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Peak Hour: 12:15 PM - 01:15 PM Weather: Rain (3.2 °C)

| Start Time | | | N M | I Approac NINTH LIN | :h IE | | | | E DL | Approact | h ⁻E | | | | S N | Approad | sh NE | | | | v D | V Approa | ch ⊤ E | | Int. Total (15 min) |
|----------------------|-------|-------|--------|-------------------------------|----------|----------------|-------|-------|---------|----------|---------|----------------|-------|-------|--------|---------|----------|----------------|-------|-------|---------------|----------|------------------|----------------|------------------------|
| | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | Right | Thru | Left | U-Turn | Peds | Approach Total | |
| 12:15:00 | 25 | 47 | 48 | 0 | 0 | 120 | 60 | 350 | 26 | 2 | 0 | 438 | 30 | 71 | 26 | 0 | 0 | 127 | 48 | 460 | 28 | 0 | 0 | 536 | 1221 |
| 12:30:00 | 40 | 46 | 33 | 0 | 0 | 119 | 63 | 436 | 34 | 0 | 0 | 533 | 31 | 67 | 30 | 0 | 0 | 128 | 57 | 427 | 40 | 0 | 0 | 524 | 1304 |
| 12:45:00 | 44 | 50 | 45 | 0 | 0 | 139 | 66 | 352 | 43 | 2 | 0 | 463 | 34 | 73 | 40 | 0 | 0 | 147 | 48 | 418 | 43 | 0 | 0 | 509 | 1258 |
| 13:00:00 | 52 | 45 | 45 | 0 | 0 | 142 | 58 | 413 | 29 | 5 | 0 | 505 | 30 | 53 | 50 | 0 | 0 | 133 | 56 | 407 | 31 | 0 | 0 | 494 | 1274 |
| Grand Total | 161 | 188 | 171 | 0 | 0 | 520 | 247 | 1551 | 132 | 9 | 0 | 1939 | 125 | 264 | 146 | 0 | 0 | 535 | 209 | 1712 | 142 | 0 | 0 | 2063 | 5057 |
| Approach% | 31% | 36.2% | 32.9% | 0% | | | 12.7% | 80% | 6.8% | 0.5% | | | 23.4% | 49.3% | 27.3% | 0% | | - | 10.1% | 83% | 6.9% | 0% | | - | |
| Totals % | 3.2% | 3.7% | 3.4% | 0% | | 10.3% | 4.9% | 30.7% | 2.6% | 0.2% | | 38.3% | 2.5% | 5.2% | 2.9% | 0% | | 10.6% | 4.1% | 33.9% | 2.8% | 0% | | 40.8% | - |
| PHF | 0.77 | 0.94 | 0.89 | 0 | | 0.92 | 0.94 | 0.89 | 0.77 | 0.45 | | 0.91 | 0.92 | 0.9 | 0.73 | 0 | | 0.91 | 0.92 | 0.93 | 0.83 | 0 | | 0.96 | |
| Heavy | 0 | 3 | 3 | 0 | | 6 | 4 | 12 | 2 | 0 | | 18 | 0 | 3 | 2 | 0 | | 5 | 2 | 15 | 0 | 0 | | 17 | - |
| Heavy % | 0% | 1.6% | 1.8% | 0% | | 1.2% | 1.6% | 0.8% | 1.5% | 0% | | 0.9% | 0% | 1.1% | 1.4% | 0% | | 0.9% | 1% | 0.9% | 0% | 0% | | 0.8% | |
| Lights | 161 | 185 | 168 | 0 | | 514 | 243 | 1539 | 130 | 9 | | 1921 | 125 | 261 | 144 | 0 | | 530 | 207 | 1697 | 142 | 0 | | 2046 | - |
| Lights % | 100% | 98.4% | 98.2% | 0% | | 98.8% | 98.4% | 99.2% | 98.5% | 100% | | 99.1% | 100% | 98.9% | 98.6% | 0% | | 99.1% | 99% | 99.1% | 100% | 0% | | 99.2% | - |
| Single-Unit Trucks | 0 | 3 | 3 | 0 | | 6 | 3 | 7 | 1 | 0 | | 11 | 0 | 3 | 1 | 0 | | 4 | 1 | 8 | 0 | 0 | | 9 | - |
| Single-Unit Trucks % | 0% | 1.6% | 1.8% | 0% | | 1.2% | 1.2% | 0.5% | 0.8% | 0% | | 0.6% | 0% | 1.1% | 0.7% | 0% | | 0.7% | 0.5% | 0.5% | 0% | 0% | | 0.4% | - |
| Buses | 0 | 0 | 0 | 0 | | 0 | 0 | 3 | 0 | 0 | | 3 | 0 | 0 | 0 | 0 | | 0 | 0 | 2 | 0 | 0 | | 2 | - |
| Buses % | 0% | 0% | 0% | 0% | | 0% | 0% | 0.2% | 0% | 0% | | 0.2% | 0% | 0% | 0% | 0% | | 0% | 0% | 0.1% | 0% | 0% | | 0.1% | - |
| Articulated Trucks | 0 | 0 | 0 | 0 | | 0 | 1 | 2 | 1 | 0 | | 4 | 0 | 0 | 1 | 0 | | 1 | 1 | 5 | 0 | 0 | | 6 | - |
| Articulated Trucks % | 0% | 0% | 0% | 0% | | 0% | 0.4% | 0.1% | 0.8% | 0% | | 0.2% | 0% | 0% | 0.7% | 0% | | 0.2% | 0.5% | 0.3% | 0% | 0% | | 0.3% | - |
| Pedestrians | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - | - | - | - | 0 | - | - |
| Pedestrians% | - | - | - | - | 0% | | - | - | - | - | 0% | | - | - | - | - | 0% | | - | - | - | - | 0% | | - |







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Turning Movement Count (4 . NINTH LINE & GLEN OAKS FUNERAL HOME ACCESS)

| Start Time | | | n Api Nint | proach H LINE | - | | | S Apj NINT | oroach H LINE | = | GL | EN OA | W Ap KS FUNE | proac ERAL H | h IOME ACCESS | Int. Total (15 min) | Int. Total (1 hr) |
|------------|--------------|-------------|----------------------|------------------|----------------|-------------|-------------|----------------------|------------------|----------------|--------------|-------------|-----------------|-----------------|------------------|------------------------|----------------------|
| | Right N:W | Thru N:S | U-Turn N:N | Peds N: | Approach Total | Thru S:N | Left S:W | U-Turn S:S | Peds S: | Approach Total | Right W:S | Left W:N | U-Turn W:W | Peds W: | Approach Total | | |
| 06:00:00 | 0 | 57 | 0 | 0 | 57 | 21 | 0 | 0 | 0 | 21 | 0 | 0 | 0 | 0 | 0 | 78 | |
| 06:15:00 | 0 | 80 | 0 | 0 | 80 | 33 | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 113 | |
| 06:30:00 | 0 | 114 | 0 | 0 | 114 | 41 | 0 | 0 | 0 | 41 | 1 | 0 | 0 | 0 | 1 | 156 | |
| 06:45:00 | 0 | 111 | 0 | 0 | 111 | 54 | 1 | 0 | 0 | 55 | 0 | 0 | 0 | 0 | 0 | 166 | 513 |
| 07:00:00 | 0 | 123 | 0 | 0 | 123 | 77 | 0 | 0 | 0 | 77 | 0 | 0 | 0 | 0 | 0 | 200 | 635 |
| 07:15:00 | 1 | 150 | 0 | 0 | 151 | 114 | 4 | 0 | 0 | 118 | 0 | 0 | 0 | 0 | 0 | 269 | 791 |
| 07:30:00 | 0 | 209 | 0 | 0 | 209 | 162 | 6 | 0 | 0 | 168 | 1 | 0 | 0 | 0 | 1 | 378 | 1013 |
| 07:45:00 | 1 | 233 | 0 | 0 | 234 | 157 | 6 | 0 | 0 | 163 | 0 | 0 | 0 | 0 | 0 | 397 | 1244 |
| 08:00:00 | 0 | 215 | 0 | 0 | 215 | 153 | 2 | 1 | 0 | 156 | 1 | 0 | 0 | 0 | 1 | 372 | 1416 |
| 08:15:00 | 0 | 225 | 0 | 0 | 225 | 208 | 1 | 0 | 0 | 209 | 1 | 0 | 0 | 0 | 1 | 435 | 1582 |
| 08:30:00 | 0 | 225 | 0 | 0 | 225 | 134 | 8 | 1 | 0 | 143 | 1 | 0 | 0 | 0 | 1 | 369 | 1573 |
| 08:45:00 | 3 | 189 | 0 | 0 | 192 | 124 | 9 | 0 | 0 | 133 | 5 | 1 | 0 | 0 | 6 | 331 | 1507 |
| ***BREAK | *** | »····· | | | - | _ | - | | | | - | | | | | - | |
| 15:00:00 | 2 | 100 | 0 | 0 | 102 | 184 | 8 | 0 | 0 | 192 | 8 | 3 | 0 | 0 | 11 | 305 | |
| 15:15:00 | 2 | 134 | 0 | 0 | 136 | 162 | 4 | 1 | 0 | 167 | 11 | 1 | 0 | 0 | 12 | 315 | |
| 15:30:00 | 0 | 139 | 0 | 0 | 139 | 199 | 5 | 0 | 0 | 204 | 6 | 1 | 0 | 0 | 7 | 350 | |
| 15:45:00 | 1 | 128 | 0 | 0 | 129 | 219 | 4 | 1 | 0 | 224 | 3 | 1 | 0 | 0 | 4 | 357 | 1327 |
| 16:00:00 | 0 | 169 | 0 | 0 | 169 | 202 | 6 | 0 | 0 | 208 | 7 | 3 | 0 | 0 | 10 | 387 | 1409 |
| 16:15:00 | 2 | 136 | 0 | 0 | 138 | 224 | 3 | 0 | 0 | 227 | 7 | 3 | 0 | 0 | 10 | 375 | 1469 |
| 16:30:00 | 2 | 145 | 0 | 0 | 147 | 192 | 2 | 1 | 0 | 195 | 16 | 0 | 0 | 0 | 16 | 358 | 1477 |
| 16:45:00 | 1 | 168 | 0 | 0 | 169 | 236 | 1 | 0 | 0 | 237 | 5 | 1 | 0 | 0 | 6 | 412 | 1532 |
| 17:00:00 | 1 | 160 | 0 | 0 | 161 | 228 | 5 | 1 | 0 | 234 | 2 | 0 | 0 | 0 | 2 | 397 | 1542 |
| 17:15:00 | 0 | 186 | 0 | 0 | 186 | 255 | 2 | 1 | 0 | 258 | 0 | 0 | 0 | 0 | 0 | 444 | 1611 |
| 17:30:00 | 0 | 143 | 0 | 0 | 143 | 246 | 7 | 1 | 0 | 254 | 5 | 0 | 0 | 0 | 5 | 402 | 1655 |



| 17:45:00 | 5 | 149 | 0 | 0 | 154 | 226 | 4 | 0 | 0 | 230 | 2 | 0 | 0 | 0 | 2 | 386 | 1629 |
|-------------|------|-------|----|---|------|-------|------|------|---|-------|------|------|----|---|------|------|------|
| 18:00:00 | 0 | 155 | 0 | 0 | 155 | 202 | 6 | 0 | 0 | 208 | 10 | 2 | 0 | 0 | 12 | 375 | 1607 |
| 18:15:00 | 4 | 121 | 0 | 0 | 125 | 151 | 6 | 0 | 0 | 157 | 2 | 0 | 0 | 0 | 2 | 284 | 1447 |
| 18:30:00 | 3 | 112 | 0 | 0 | 115 | 140 | 4 | 0 | 0 | 144 | 5 | 0 | 0 | 0 | 5 | 264 | 1309 |
| 18:45:00 | 6 | 88 | 0 | 0 | 94 | 144 | 10 | 1 | 0 | 155 | 5 | 1 | 0 | 0 | 6 | 255 | 1178 |
| Grand Total | 34 | 4164 | 0 | 0 | 4198 | 4488 | 114 | 9 | 0 | 4611 | 104 | 17 | 0 | 0 | 121 | 8930 | - |
| Approach% | 0.8% | 99.2% | 0% | | - | 97.3% | 2.5% | 0.2% | | - | 86% | 14% | 0% | | - | - | - |
| Totals % | 0.4% | 46.6% | 0% | | 47% | 50.3% | 1.3% | 0.1% | | 51.6% | 1.2% | 0.2% | 0% | | 1.4% | - | - |
| Heavy | 0 | 95 | 0 | | - | 111 | 2 | 0 | | - | 3 | 0 | 0 | | - | - | - |
| Heavy % | 0% | 2.3% | 0% | | - | 2.5% | 1.8% | 0% | | - | 2.9% | 0% | 0% | | - | - | - |
| Bicycles | - | - | - | | - | - | - | - | | - | - | - | - | | - | - | - |
| Bicycle % | - | - | - | | - | - | - | - | | - | - | - | - | | - | - | - |

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| | | | | Peak | Hour: 07:30 A | M - 08: | 30 AM | Weat | her: N | lostly Cloudy (| (2.8 °C | ;) | | | | |
|-------------|-------|-------|---------------------|------------------|----------------|---------|-------|-----------------------|------------------------|-----------------|---------|-------|--------|------------------|------------------|------------------------|
| Start Time | | | n Ap Nint | broach H LINE | | | | S App NINTH | roach H LINE | | GLE | en oa | W AI | oproac ERAL H | h IOME ACCESS | Int. Total (15 min) |
| | Right | Thru | U-Turn | Peds | Approach Total | Thru | Left | U-Turn | Peds | Approach Total | Right | Left | U-Turn | Peds | Approach Total | |
| 07:30:00 | 0 | 209 | 0 | 0 | 209 | 162 | 6 | 0 | 0 | 168 | 1 | 0 | 0 | 0 | 1 | 378 |
| 07:45:00 | 1 | 233 | 0 | 0 | 234 | 157 | 6 | 0 | 0 | 163 | 0 | 0 | 0 | 0 | 0 | 397 |
| 08:00:00 | 0 | 215 | 0 | 0 | 215 | 153 | 2 | 1 | 0 | 156 | 1 | 0 | 0 | 0 | 1 | 372 |
| 08:15:00 | 0 | 225 | 0 | 0 | 225 | 208 | 1 | 0 | 0 | 209 | 1 | 0 | 0 | 0 | 1 | 435 |
| Grand Total | 1 | 882 | 0 | 0 | 883 | 680 | 15 | 1 | 0 | 696 | 3 | 0 | 0 | 0 | 3 | 1582 |
| Approach% | 0.1% | 99.9% | 0% | | - | 97.7% | 2.2% | 0.1% | | - | 100% | 0% | 0% | | - | - |
| Totals % | 0.1% | 55.8% | 0% | | 55.8% | 43% | 0.9% | 0.1% | | 44% | 0.2% | 0% | 0% | | 0.2% | - |
| PHF | 0.25 | 0.95 | 0 | | 0.94 | 0.82 | 0.63 | 0.25 | | 0.83 | 0.75 | 0 | 0 | | 0.75 | - |
| μοοια | | 01 | | | 01 | 01 | | 0 | | າງ | 0 | | | | <u>^</u> | |

| Totals % | 0.1% | 55.8% | 0% | 55.8% 43 | % | 0.9% | 0.1% | 44% | 0.2% | 0% | 0% | 0.2% | - |
|----------------------|------|-------|----|------------|----|-------|------|-------|------|----|----|------|---|
| PHF | 0.25 | 0.95 | 0 | 0.94 0.8 | 82 | 0.63 | 0.25 | 0.83 | 0.75 | 0 | 0 | 0.75 | - |
| Heavy | 0 | 21 | 0 | 21 2 | 1 | 1 | 0 | 22 | 0 | 0 | 0 | 0 | - |
| Heavy % | 0% | 2.4% | 0% | 2.4% 3.1 | ۱% | 6.7% | 0% | 3.2% | 0% | 0% | 0% | 0% | - |
| Lights | 1 | 860 | 0 | 861 65 | 59 | 14 | 1 | 674 | 3 | 0 | 0 | 3 | - |
| Lights % | 100% | 97.5% | 0% | 97.5% 96.9 | 9% | 93.3% | 100% | 96.8% | 100% | 0% | 0% | 100% | - |
| Single-Unit Trucks | 0 | 10 | 0 | 10 10 | 0 | 1 | 0 | 11 | 0 | 0 | 0 | 0 | - |
| Single-Unit Trucks % | 0% | 1.1% | 0% | 1.1% 1.5 | 5% | 6.7% | 0% | 1.6% | 0% | 0% | 0% | 0% | - |
| Buses | 0 | 7 | 0 | 7 5 | 5 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | - |
| Buses % | 0% | 0.8% | 0% | 0.8% 0.7 | 7% | 0% | 0% | 0.7% | 0% | 0% | 0% | 0% | - |
| Articulated Trucks | 0 | 4 | 0 | 4 6 | 6 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | - |
| Articulated Trucks % | 0% | 0.5% | 0% | 0.5% 0.9 | 9% | 0% | 0% | 0.9% | 0% | 0% | 0% | 0% | - |
| Bicycles on Road | 0 | 1 | 0 | 1 0 |) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | - |
| Bicycles on Road % | 0% | 0.1% | 0% | 0.1% 09 | % | 0% | 0% | 0% | 0% | 0% | 0% | 0% | - |



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Peak Hour: 04:45 PM - 05:45 PM Weather: Overcast (7.4 °C)

| Start Time | | | n App Ninti | broach H LINE | | | | S App Ninti | roach H LINE | | GL | EN OAK | W Apj S FUNE | oroach RAL HO | OME ACCESS | Int. Total (15 min) |
|----------------------|-------|-------|-----------------------|-------------------------|----------------|-------|------|-----------------------|-----------------|----------------|-------|--------|-----------------|------------------|----------------|------------------------|
| | Right | Thru | U-Turn | Peds | Approach Total | Thru | Left | U-Turn | Peds | Approach Total | Right | Left | U-Turn | Peds | Approach Total | |
| 16:45:00 | 1 | 168 | 0 | 0 | 169 | 236 | 1 | 0 | 0 | 237 | 5 | 1 | 0 | 0 | 6 | 412 |
| 17:00:00 | 1 | 160 | 0 | 0 | 161 | 228 | 5 | 1 | 0 | 234 | 2 | 0 | 0 | 0 | 2 | 397 |
| 17:15:00 | 0 | 186 | 0 | 0 | 186 | 255 | 2 | 1 | 0 | 258 | 0 | 0 | 0 | 0 | 0 | 444 |
| 17:30:00 | 0 | 143 | 0 | 0 | 143 | 246 | 7 | 1 | 0 | 254 | 5 | 0 | 0 | 0 | 5 | 402 |
| Grand Total | 2 | 657 | 0 | 0 | 659 | 965 | 15 | 3 | 0 | 983 | 12 | 1 | 0 | 0 | 13 | 1655 |
| Approach% | 0.3% | 99.7% | 0% | | - | 98.2% | 1.5% | 0.3% | | - | 92.3% | 7.7% | 0% | | - | - |
| Totals % | 0.1% | 39.7% | 0% | | 39.8% | 58.3% | 0.9% | 0.2% | | 59.4% | 0.7% | 0.1% | 0% | | 0.8% | - |
| PHF | 0.5 | 0.88 | 0 | | 0.89 | 0.95 | 0.54 | 0.75 | | 0.95 | 0.6 | 0.25 | 0 | | 0.54 | - |
| Heavy | 0 | 10 | 0 | | 10 | 15 | 0 | 0 | | 15 | 0 | 0 | 0 | | 0 | - |
| Heavy % | 0% | 1.5% | 0% | | 1.5% | 1.6% | 0% | 0% | | 1.5% | 0% | 0% | 0% | | 0% | - |
| Lights | 2 | 647 | 0 | | 649 | 950 | 15 | 3 | | 968 | 12 | 1 | 0 | | 13 | - |
| Lights % | 100% | 98.5% | 0% | | 98.5% | 98.4% | 100% | 100% | | 98.5% | 100% | 100% | 0% | | 100% | - |
| Single-Unit Trucks | 0 | 7 | 0 | | 7 | 10 | 0 | 0 | | 10 | 0 | 0 | 0 | | 0 | - |
| Single-Unit Trucks % | 0% | 1.1% | 0% | | 1.1% | 1% | 0% | 0% | | 1% | 0% | 0% | 0% | | 0% | - |
| Buses | 0 | 1 | 0 | | 1 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | - |
| Buses % | 0% | 0.2% | 0% | | 0.2% | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | | 0% | - |
| Articulated Trucks | 0 | 2 | 0 | | 2 | 5 | 0 | 0 | | 5 | 0 | 0 | 0 | | 0 | - |
| Articulated Trucks % | 0% | 0.3% | 0% | | 0.3% | 0.5% | 0% | 0% | | 0.5% | 0% | 0% | 0% | | 0% | - |
| Bicycles on Road | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | - |
| Bicycles on Road % | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | | 0% | - |











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Turning Movement Count (4 . NINTH LINE & GLEN OAKS FUNERAL HOME ACCESS)

| Chaut Time | | | n Ap Nint | oroach H LINE | 1 E | | | S App NINT | oroach H LINE | 1 | GLI | EN OAK | W App S FUNE | roach RAL HO | OME ACCESS | Int. Total (15 min) | Int. Total (1 hr) |
|------------|--------------|-------------|---------------------|------------------|----------------|-------------|-------------|----------------------|------------------|----------------|--------------|-------------|-----------------|-----------------|----------------|------------------------|----------------------|
| Start 11me | Right N:W | Thru N:S | U-Turn N:N | Peds N: | Approach Total | Thru S:N | Left S:W | U-Turn S:S | Peds S: | Approach Total | Right W:S | Left W:N | U-Turn W:W | Peds W: | Approach Total | | |
| 10:00:00 | 0 | 117 | 0 | 0 | 117 | 83 | 5 | 1 | 0 | 89 | 2 | 1 | 0 | 0 | 3 | 209 | |
| 10:15:00 | 1 | 85 | 0 | 0 | 86 | 64 | 6 | 0 | 0 | 70 | 4 | 1 | 0 | 0 | 5 | 161 | |
| 10:30:00 | 1 | 88 | 0 | 0 | 89 | 92 | 4 | 0 | 0 | 96 | 0 | 1 | 0 | 0 | 1 | 186 | |
| 10:45:00 | 3 | 94 | 0 | 0 | 97 | 101 | 7 | 0 | 0 | 108 | 7 | 1 | 0 | 0 | 8 | 213 | 769 |
| 11:00:00 | 0 | 102 | 0 | 0 | 102 | 90 | 2 | 0 | 0 | 92 | 0 | 1 | 0 | 0 | 1 | 195 | 755 |
| 11:15:00 | 1 | 77 | 0 | 0 | 78 | 99 | 1 | 0 | 0 | 100 | 3 | 0 | 0 | 0 | 3 | 181 | 775 |
| 11:30:00 | 1 | 106 | 0 | 0 | 107 | 97 | 4 | 2 | 0 | 103 | 4 | 0 | 0 | 0 | 4 | 214 | 803 |
| 11:45:00 | 2 | 99 | 0 | 0 | 101 | 134 | 9 | 0 | 0 | 143 | 2 | 0 | 0 | 0 | 2 | 246 | 836 |
| 12:00:00 | 4 | 124 | 0 | 0 | 128 | 116 | 36 | 1 | 0 | 153 | 3 | 0 | 0 | 0 | 3 | 284 | 925 |
| 12:15:00 | 2 | 110 | 0 | 0 | 112 | 121 | 31 | 0 | 0 | 152 | 5 | 0 | 0 | 0 | 5 | 269 | 1013 |
| 12:30:00 | 8 | 114 | 0 | 0 | 122 | 132 | 47 | 1 | 0 | 180 | 7 | 1 | 0 | 0 | 8 | 310 | 1109 |
| 12:45:00 | 5 | 112 | 0 | 0 | 117 | 138 | 40 | 0 | 0 | 178 | 15 | 0 | 0 | 0 | 15 | 310 | 1173 |
| 13:00:00 | 4 | 124 | 0 | 0 | 128 | 117 | 13 | 0 | 0 | 130 | 37 | 6 | 0 | 0 | 43 | 301 | 1190 |
| 13:15:00 | 1 | 99 | 0 | 0 | 100 | 110 | 7 | 0 | 0 | 117 | 3 | 1 | 0 | 0 | 4 | 221 | 1142 |
| 13:30:00 | 2 | 106 | 0 | 0 | 108 | 102 | 2 | 0 | 0 | 104 | 5 | 1 | 0 | 0 | 6 | 218 | 1050 |
| 13:45:00 | 3 | 94 | 0 | 0 | 97 | 110 | 6 | 0 | 0 | 116 | 7 | 3 | 0 | 0 | 10 | 223 | 963 |
| 14:00:00 | 9 | 129 | 0 | 0 | 138 | 139 | 9 | 0 | 0 | 148 | 13 | 3 | 0 | 0 | 16 | 302 | 964 |
| 14:15:00 | 2 | 100 | 0 | 0 | 102 | 134 | 9 | 0 | 0 | 143 | 71 | 0 | 0 | 0 | 71 | 316 | 1059 |
| 14:30:00 | 1 | 103 | 0 | 0 | 104 | 111 | 5 | 1 | 0 | 117 | 42 | 4 | 0 | 0 | 46 | 267 | 1108 |
| 14:45:00 | 1 | 103 | 0 | 0 | 104 | 114 | 9 | 0 | 0 | 123 | 31 | 4 | 0 | 0 | 35 | 262 | 1147 |
| 15:00:00 | 1 | 106 | 0 | 0 | 107 | 130 | 9 | 0 | 0 | 139 | 25 | 5 | 0 | 0 | 30 | 276 | 1121 |
| 15:15:00 | 0 | 101 | 0 | 0 | 101 | 135 | 2 | 0 | 0 | 137 | 21 | 2 | 0 | 0 | 23 | 261 | 1066 |
| 15:30:00 | 0 | 83 | 0 | 0 | 83 | 114 | 4 | 0 | 0 | 118 | 12 | 1 | 0 | 0 | 13 | 214 | 1013 |
| | | | | | | | | | | | | | | | | | |



Crozier & Associates

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| 15:45:00 | 1 | 104 | 0 | 0 | 105 | 124 | 6 | 0 | 0 | 130 | 4 | 0 | 0 | 0 | 4 | 239 | 990 |
|-------------|------|-------|----|---|-------|-------|------|------|---|-------|-------|-------|----|---|------|------|-----|
| 16:00:00 | 0 | 76 | 0 | 0 | 76 | 124 | 5 | 0 | 0 | 129 | 4 | 0 | 0 | 0 | 4 | 209 | 923 |
| 16:15:00 | 0 | 112 | 0 | 0 | 112 | 134 | 2 | 0 | 0 | 136 | 10 | 0 | 0 | 0 | 10 | 258 | 920 |
| 16:30:00 | 0 | 108 | 0 | 0 | 108 | 151 | 1 | 0 | 0 | 152 | 11 | 1 | 0 | 0 | 12 | 272 | 978 |
| 16:45:00 | 2 | 99 | 0 | 0 | 101 | 129 | 4 | 0 | 0 | 133 | 5 | 3 | 0 | 0 | 8 | 242 | 981 |
| Grand Total | 55 | 2875 | 0 | 0 | 2930 | 3245 | 285 | 6 | 0 | 3536 | 353 | 40 | 0 | 0 | 393 | 6859 | - |
| Approach% | 1.9% | 98.1% | 0% | | - | 91.8% | 8.1% | 0.2% | | - | 89.8% | 10.2% | 0% | | - | - | - |
| Totals % | 0.8% | 41.9% | 0% | | 42.7% | 47.3% | 4.2% | 0.1% | | 51.6% | 5.1% | 0.6% | 0% | | 5.7% | - | - |
| Heavy | 1 | 25 | 0 | | - | 32 | 5 | 0 | | - | 5 | 0 | 0 | | - | - | - |
| Heavy % | 1.8% | 0.9% | 0% | | - | 1% | 1.8% | 0% | | - | 1.4% | 0% | 0% | | - | - | - |
| Bicycles | - | - | - | | - | - | - | - | | - | - | - | - | | - | - | - |
| Bicycle % | - | - | - | | - | - | - | - | | - | - | - | - | | - | - | - |



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Peak Hour: 12:15 PM - 01:15 PM Weather: Rain (3.2 °C)

| Start Time | | | n App Ninti | roach H LINE | | | | S App NINTH | roach I LINE | | GLE | EN OAK | W App S FUNE | roach RAL HC | OME ACCESS | Int. Total (15 min) |
|----------------------|-------|-------|-----------------------|------------------------|----------------|-------|-------|-----------------------|-----------------|----------------|-------|--------|-----------------|------------------------|----------------|------------------------|
| | Right | Thru | U-Turn | Peds | Approach Total | Thru | Left | U-Turn | Peds | Approach Total | Right | Left | U-Turn | Peds | Approach Total | |
| 12:15:00 | 2 | 110 | 0 | 0 | 112 | 121 | 31 | 0 | 0 | 152 | 5 | 0 | 0 | 0 | 5 | 269 |
| 12:30:00 | 8 | 114 | 0 | 0 | 122 | 132 | 47 | 1 | 0 | 180 | 7 | 1 | 0 | 0 | 8 | 310 |
| 12:45:00 | 5 | 112 | 0 | 0 | 117 | 138 | 40 | 0 | 0 | 178 | 15 | 0 | 0 | 0 | 15 | 310 |
| 13:00:00 | 4 | 124 | 0 | 0 | 128 | 117 | 13 | 0 | 0 | 130 | 37 | 6 | 0 | 0 | 43 | 301 |
| Grand Total | 19 | 460 | 0 | 0 | 479 | 508 | 131 | 1 | 0 | 640 | 64 | 7 | 0 | 0 | 71 | 1190 |
| Approach% | 4% | 96% | 0% | | - | 79.4% | 20.5% | 0.2% | | - | 90.1% | 9.9% | 0% | | - | - |
| Totals % | 1.6% | 38.7% | 0% | | 40.3% | 42.7% | 11% | 0.1% | | 53.8% | 5.4% | 0.6% | 0% | | 6% | - |
| PHF | 0.59 | 0.93 | 0 | | 0.94 | 0.92 | 0.7 | 0.25 | | 0.89 | 0.43 | 0.29 | 0 | | 0.41 | - |
| Heavy | 0 | 8 | 0 | | 8 | 7 | 0 | 0 | | 7 | 0 | 0 | 0 | | 0 | - |
| Heavy % | 0% | 1.7% | 0% | | 1.7% | 1.4% | 0% | 0% | | 1.1% | 0% | 0% | 0% | | 0% | - |
| Lights | 19 | 452 | 0 | | 471 | 501 | 131 | 1 | | 633 | 64 | 7 | 0 | | 71 | - |
| Lights % | 100% | 98.3% | 0% | | 98.3% | 98.6% | 100% | 100% | | 98.9% | 100% | 100% | 0% | | 100% | - |
| Single-Unit Trucks | 0 | 8 | 0 | | 8 | 6 | 0 | 0 | | 6 | 0 | 0 | 0 | | 0 | - |
| Single-Unit Trucks % | 0% | 1.7% | 0% | | 1.7% | 1.2% | 0% | 0% | | 0.9% | 0% | 0% | 0% | | 0% | - |
| Buses | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 0 | - |
| Buses % | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | | 0% | 0% | 0% | 0% | | 0% | - |
| Articulated Trucks | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | | 1 | 0 | 0 | 0 | | 0 | - |
| Articulated Trucks % | 0% | 0% | 0% | | 0% | 0.2% | 0% | 0% | | 0.2% | 0% | 0% | 0% | | 0% | - |







| Ontario T | raffic Inc. |
|---|---|
| Morning Peak Diagram | Specified Period One Hour Peak From: 7:00:00 From: 7:45:00 To: 9:00:00 To: 8:45:00 |
| Municipality:OakvilleSite #:1902900001Intersection:Dundas St E & Ninth LineTFR File #:1Count date:19-Feb-19 | Weather conditions: Person(s) who counted: |
| ** Signalized Intersection ** | Major Road: Dundas St E runs W/E |
| North Leg Total: 1452 Heavys 0 0 0 0 North Entering: 800 Trucks 0 2 0 2 North Peds: 0 Cars 98 518 182 79 Peds Cross: Image: March 100 Totals 98 520 182 | Heavys0East Leg Total:3571Trucks5East Entering:1102Cars647East Peds:0Totals652Peds Cross:X |
| Heavys Trucks Cars Totals | Cars Trucks Heavys Totals 122 0 0 122 786 74 0 860 |
| Dundas St E | $\frac{118 \ 2 \ 0}{1026 \ 76 \ 0} \ 120$ |
| Heavys Trucks Cars Totals 0 0 217 217 5 0 25 2109 2134 | Dundas St E |
| 0 1 312 313 0 26 2638 Ninth Line | Cars Trucks Heavys Totals 2439 30 0 2469 |
| Peds Cross:Image: Carse of the sector of the se | rs 152 308 148 608 Peds Cross: ▷ rs 21 5 5 31 South Peds: 0 rs 0 0 0 South Entering: 639 rs 173 313 153 South Leg Total: 1592 |
| Comn | nents |
| West Leg Total: 3795 Totals 953 Tota | Is 173 313 153 South Leg Total: 1592 |





| | | | | <i>On</i> Traff | <i>itari</i> fic C | o <i>Traf</i> i count S | fic In umm | C. arv | | | | |
|---|---|--|--|--|--|--|---|--|--|---|--|--|
| Intersection: | Dundas | St E & | Ninth Lir | e | Count D | ^{late:} 19-Feb-1 |) Muni | cipality: Oa | kville | | | |
| | Nort | h Appro | ach Tot | als | | | | Sout | h Appro | ach To | als | |
| | Includ | es Cars, T | rucks, & H | eavys | | North/South | | Include | es Cars, T | rucks, & H | eavys | |
| Hour Ending 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 | Left 0 194 177 0 82 115 | Thru 0 414 510 0 283 307 | Right 0 43 107 0 207 192 | Grand Total 0 651 794 0 572 614 | Total Peds 0 1 0 0 0 | 0 1193 1413 0 1982 2129 | Hour Ending 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 | Left 0 136 188 0 305 335 | Thru 0 268 289 0 654 676 | Right 0 138 142 0 451 504 | Grand Total 0 542 619 0 1410 1515 | Total Peds 0 0 0 1 0 |
| Totals: | 568 East | 1514 t Approa es Cars, T | 549 ach Tota rucks, & H | 2631 als eavys | 1 | 6717 East/West | | 964 Wes | 1887 t Appro es Cars, T | 1235 ach Tot rucks, & H | 4086 als eavys | 1 |
| Hour Ending | Left | Thru | Right | Grand Total | Total Peds | Total Approaches | Hour Ending | Left | Thru | Right | Grand Total | Total Peds |
| 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 | 0 94 103 0 134 142 | 0 718 817 0 2350 2340 | 0 86 106 0 111 139 | 0 898 1026 0 2595 2621 | | 0 3452 3527 0 3998 4045 | 7:00:00 8:00:00 9:00:00 16:00:00 17:00:00 18:00:00 | 0 181 204 0 99 127 | 0 2131 2007 0 1147 1136 | 0 242 290 0 157 161 | 0 2554 2501 0 1403 1424 | |
| Totals: | 473 | 6225 | 442 | 7140 | 0 | 15022 | | 611 | 6421 | 850 | 7882 | 0 |
| Hours En Crossing | ding: Values: | 7:00 0 | Calc 8:00 744 | ulated V 9:00 875 | alues f 16:00 0 | or Traffic Cr | ossing M 17:00 1041 | ajor Stre 18:00 2609 | eet 18:00 1126 | 18:00 2609 | | |

Count Date: 19-Feb-19 Site #: 1902900001

| | Passenger Cars - North Approach | | | | | | | Tru | icks - Nori | th Appro | ach | | Heavys - North Approach | | | | | | | Pedestrians | | |
|----------|---------------------------------|------|------|----------|-----|----------|-----|------|-------------|----------|-----|------|-------------------------|------|-----|------|-----|------|-------|-------------|--|--|
| Interval | Le | ft | Th | Thru | | jht | Le | ft | Th | ru | Riç | ght | Le | ft | Th | ru | Rig | jht | North | Cross | | |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | | |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | |
| 7:15:00 | 39 | 39 | 77 | 77 | 5 | 5 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | | |
| 7:30:00 | 85 | 46 | 162 | 85 | 18 | 13 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 7:45:00 | 146 | 61 | 279 | 117 | 25 | 7 | 0 | 0 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 8:00:00 | 194 | 48 | 412 | 133 | 42 | 17 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 8:15:00 | 240 | 46 | 544 | 132 | 64 | 22 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 8:30:00 | 277 | 37 | 672 | 128 | 95 | 31 | 0 | 0 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 8:45:00 | 328 | 51 | 797 | 125 | 123 | 28 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 9:00:00 | 370 | 42 | 918 | 121 | 149 | 26 | 1 | 1 | 6 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 9:02:05 | 370 | 0 | 918 | 0 | 149 | 0 | 1 | 0 | 6 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 16:00:00 | 370 | 0 | 918 | 0 | 149 | 0 | 1 | 0 | 6 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 16:15:00 | 396 | 26 | 988 | 70 | 204 | 55 | 1 | 0 | / | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 16:30:00 | 414 | 18 | 1051 | 63 | 264 | 60 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 16:45:00 | 437 | 23 | 1200 | 79 | 310 | 52 | 2 | 1 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 17:00.00 | 401 | 14 | 1200 | 70 | 402 | 40 | 2 | 0 | / 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 17:30:00 | 511 | 25 | 1290 | 90 62 | 402 | 40 54 | 2 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 17:45:00 | 530 | 23 | 1427 | 75 | 511 | 55 | 4 | 1 | 9 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 18:00:00 | 563 | 20 | 1505 | 78 | 548 | 37 | | 1 | 9 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 18:15:00 | 563 | 0 | 1505 | 0 | 548 | 0 | 5 | 0 | 9 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 18:16:59 | 563 | 0 | 1505 | 0 | 548 | 0 | 5 | 0 | 9 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| | | Ŭ | | Ŭ | 0.0 | | | | Ū | | | | Ŭ | Ū | Ŭ | | Ū | | - | | | |
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Count Date: 19-Feb-19 Site #: 1902900001

| | Passenger Cars - East Approach | | | | | | | Tre | ucks - Eas | st Approa | ach | | Heavys - East Approach | | | | | | | Pedestrians | | |
|----------|--------------------------------|------|------|------|-----|-------|-----|------|------------|-----------|-----|------|------------------------|------|-----|------|-----|------|------|-------------|--|--|
| Interval | Le | ft | Th | Thru | | Right | | eft | Th | ru | Rig | ght | Le | ft | Th | ru | Rig | ht | East | Cross | | |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | | |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C |) 0 | | |
| 7:15:00 | 11 | 11 | 122 | 122 | 8 | 8 | 0 | 0 | 15 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C |) (| | |
| 7:30:00 | 20 | 9 | 284 | 162 | 27 | 19 | 0 | 0 | 36 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C |) (| | |
| 7:45:00 | 52 | 32 | 422 | 138 | 49 | 22 | 0 | 0 | 55 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) C | | |
| 8:00:00 | 94 | 42 | 642 | 220 | 86 | 37 | 0 | 0 | 76 | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 8:15:00 | 123 | 29 | 782 | 140 | 113 | 27 | 2 | 2 | 93 | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 8:30:00 | 150 | 27 | 985 | 203 | 152 | 39 | 2 | 0 | 118 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 8:45:00 | 170 | 20 | 1208 | 223 | 171 | 19 | 2 | 0 | 129 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 9:00:00 | 193 | 23 | 1388 | 180 | 191 | 20 | 4 | 2 | 147 | 18 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 9:02:05 | 193 | 0 | 1388 | 0 | 191 | 0 | 4 | 0 | 147 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 16:00:00 | 193 | 0 | 1388 | 0 | 191 | 0 | 4 | 0 | 147 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 16:15:00 | 219 | 26 | 1937 | 549 | 224 | 33 | 5 | 1 | 166 | 19 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |) (| | |
| 16:30:00 | 247 | 28 | 2544 | 607 | 250 | 26 | 7 | 2 | 179 | 13 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |) (| | |
| 16:45:00 | 284 | 37 | 3056 | 512 | 274 | 24 | 7 | 0 | 184 | 5 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 17:00:00 | 323 | 39 | 3699 | 643 | 301 | 27 | 8 | 1 | 186 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 17:15:00 | 355 | 32 | 4273 | 574 | 331 | 30 | 9 | 1 | 189 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 17:30:00 | 391 | 36 | 4860 | 587 | 366 | 35 | 9 | 0 | 197 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |) (| | |
| 17:45:00 | 422 | 31 | 5449 | 589 | 407 | 41 | 10 | 1 | 204 | 7 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |) (| | |
| 18:00:00 | 463 | 41 | 6020 | 571 | 440 | 33 | 10 | 0 | 205 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |) (| | |
| 18:15:00 | 463 | 0 | 6020 | 0 | 440 | 0 | 10 | 0 | 205 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |) (| | |
| 18:16:59 | 463 | 0 | 6020 | 0 | 440 | 0 | 10 | 0 | 205 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |) (| | |
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Count Date: 19-Feb-19 Site #: 1902900001

3-1 eb-13 Site #. 1902900001

| | | Passeng | er Cars - | South A | pproach | | | Tru | cks - Sou | th Appro | ach | | Heavys - South Approach | | | | | | | Pedestrians | | |
|----------|-----|---------|-----------|----------------------------|---------|------|-----|------|-----------|----------|-------|------|-------------------------|-------|-----|------|-----|------|-----|-------------|--|--|
| Interval | Le | eft | Thr | Thru Right Left Thru Right | | ht | Le | eft | Th | iru | Right | | South | Cross | | | | | | | | |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | | |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C |) 0 | | |
| 7:15:00 | 26 | 26 | 50 | 50 | 18 | 18 | 2 | 2 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | C |) 0 | | |
| 7:30:00 | 55 | 29 | 104 | 54 | 55 | 37 | 11 | 9 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 0 | | C |) 0 | | |
| 7:45:00 | 89 | 34 | 187 | 83 | 96 | 41 | 17 | 6 | 1 | 0 | 5 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | C | <i>i</i> 0 | | |
| 8:00:00 | 113 | 24 | 266 | 79 | 132 | 36 | 23 | 6 | 2 | 1 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | C | <i>i</i> 0 | | |
| 8:15:00 | 148 | 35 | 349 | 83 | 159 | 27 | 30 | 7 | 2 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 0 | | C | 0 | | |
| 8:30:00 | 193 | 45 | 444 | 95 | 199 | 40 | 34 | 4 | 4 | 2 | 6 | 0 | 0 | 0 | 0 | 0 | 0 0 | | C | <i>i</i> 0 | | |
| 8:45:00 | 241 | 48 | 495 | 51 | 244 | 45 | 38 | 4 | 6 | 2 | 10 | 4 | 0 | 0 | 0 | 0 | 0 0 | | C |) 0 | | |
| 9:00:00 | 282 | 41 | 547 | 52 | 267 | 23 | 42 | 4 | 10 | 4 | 13 | 3 | 0 | 0 | 0 | 0 | 0 0 | | C | 0 0 | | |
| 9:02:05 | 282 | 0 | 547 | 0 | 267 | 0 | 42 | 0 | 10 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 0 | | C | 0 0 | | |
| 16:00:00 | 282 | 0 | 547 | 0 | 267 | 0 | 42 | 0 | 10 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 0 | | C | 0 0 | | |
| 16:15:00 | 369 | 87 | 696 | 149 | 356 | 89 | 43 | 1 | 12 | 2 | 17 | 4 | 0 | 0 | 0 | 0 | 0 | 0 0 | | 1 1 | | |
| 16:30:00 | 442 | 73 | 852 | 156 | 458 | 102 | 45 | 2 | 14 | 2 | 22 | 5 | 0 | 0 | 0 | 0 | 0 0 | | 1 | 1 0 | | |
| 16:45:00 | 516 | 74 | 1036 | 184 | 563 | 105 | 49 | 4 | 14 | 0 | 26 | 4 | 0 | 0 | 0 | 0 | 0 0 | | 1 | 0 | | |
| 17:00:00 | 580 | 64 | 1196 | 160 | 699 | 136 | 49 | 0 | 15 | 1 | 32 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 17:15:00 | 661 | 81 | 1373 | 177 | 803 | 104 | 52 | 3 | 15 | 0 | 39 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 17:30:00 | 743 | 82 | 1563 | 190 | 923 | 120 | 53 | 1 | 17 | 2 | 42 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 17:45:00 | 824 | 81 | 1728 | 165 | 1067 | 144 | 54 | 1 | 20 | 3 | 52 | 10 | 0 | 0 | 0 | 0 | 0 0 | | 1 | 0 | | |
| 18:00:00 | 908 | 84 | 1866 | 138 | 1177 | 110 | 56 | 2 | 21 | 1 | 58 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 18:15:00 | 908 | 0 | 1866 | 0 | 1177 | 0 | 56 | 0 | 21 | 0 | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
| 18:16:59 | 908 | 0 | 1866 | 0 | 1177 | 0 | 56 | 0 | 21 | 0 | 58 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | | |
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Count Date: 19-Feb-19 Site #: 1902900001

| | | Passen | ger Cars - | West Ap | oproach | | | Tru | ıcks - We | st Approa | ach | | | Pedestrians | | | | | | |
|----------|------------|--------|------------|---------|---------|-------|-----|------|-----------|-----------|-----|------|-----|-------------|-----|------|-----|------|------|-------|
| Interval | Le | ft | Th | Thru | | Right | | Left | | ru | Rig | ght | Le | ft | Th | ru | Rig | jht | West | Cross |
| Time | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr | Cum | Incr |
| 7:00:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:15:00 | 22 | 22 | 439 | 439 | 42 | 42 | 0 | 0 | 6 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7:30:00 | 59 | 37 | 1026 | 587 | 96 | 54 | 1 | 1 | 13 | 7 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | C |
| 7:45:00 | 126 | 67 | 1526 | 500 | 157 | 61 | 1 | 0 | 19 | 6 | 5 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:00:00 | 180 | 54 | 2108 | 582 | 237 | 80 | 1 | 0 | 23 | 4 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:15:00 | 235 | 55 | 2588 | 480 | 312 | 75 | 1 | 0 | 31 | 8 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:30:00 | 299 | 64 | 3127 | 539 | 393 | 81 | 1 | 0 | 34 | 3 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8:45:00 | 343 | 44 | 3635 | 508 | 469 | 76 | 1 | 0 | 44 | 10 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:00:00 | 384 | 41 | 4084 | 449 | 524 | 55 | 1 | 0 | 54 | 10 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9:02:05 | 384 | 0 | 4084 | 0 | 524 | 0 | 1 | 0 | 54 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:00:00 | 384 | 0 | 4084 | 0 | 524 | 0 | 1 | 0 | 54 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:15:00 | 407 | 23 | 4342 | 258 | 552 | 28 | 1 | 0 | 11 | 23 | 11 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30:00 | 433 | 26 | 4605 | 263 | 590 | 38 | 1 | 0 | 93 | 16 | 12 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45:00 | 459 | 26 | 4877 | 272 | 631 | 41 | 1 | 0 | 105 | 12 | 14 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:00:00 | 483 | 24 | 5171 | 294 | 0/5 | 44 | 1 | 0 | 114 | 9 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:15:00 | 510 | 30 | 5403 | 292 | 714 | 39 | 1 | 0 | 120 | | 10 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17:30.00 | 599 | 40 | 5007 | 274 | 700 | 39 | 1 | 0 | 1.34 | 9 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17.45.00 | 500 610 | 30 | 6276 | 200 | 820 | 37 | 1 | 0 | 140 | 5 | 20 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:15:00 | 610 | 22 | 6276 | 2/9 | 830 | 40 | 1 | 0 | 145 | 0 | 20 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18:16:59 | 610 | 0 | 6276 | 0 | 830 | 0 | 1 | 0 | 145 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10.10.00 | 010 | | 0210 | | 000 | | | 0 | | 0 | 20 | 0 | | 0 | 0 | 0 | Ŭ | 0 | | |
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Signal Timing Plan



18. APPENDIX D: PROGRAM REFERENCE CARD



CONFIGURATION SUBMENU

1-1-1. PHASE RING ASSIGNMENT

| RING | |
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1-1-2. PHASE COMPATIBILITY

| PH AS E | 1 | 2 | З | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
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| 15 | | | | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | | | | |

1-2. PHASES IN USE / EXCLUSIVE PED

| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|---------------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|
| PHASES IN USE | | | | | | | | | | | | | | | | |
| EXCLUSIVE PED | | | | | | | | | | | | | | | | |

1-1-4. BACKUP PREVENT PHASES

| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
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| 13 | | | | | | | | | | | | | | | | |
| 14 | | | | | | | | | | | | | | | | |
| 15 | | | | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | | | | |

1-1-5 SIMULTANEOUS GAP

| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
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1-1-3. PHASE RING SEQUENCE

| CONTROLLER 1 | SEQUENCE 1 | | | | |
|--------------|------------|---|------|----------|--------------|
| RING 1 | | | | | |
| RING 2 | | | | | |
| RING 3 | | | | | |
| RING 4 | | | | | |
| CONTROLLER 1 | SEQUENCE 2 | | | <u> </u> | |
| RING 1 | | | | | |
| RING 2 | | | | | |
| RING 3 | | | | | |
| RING 4 | | | | | |
| CONTROLLER 1 | SEQUENCE 3 | • | | • | : |
| RING 1 | | | | | |
| RING 2 | | | | | |
| RING 3 | | | | | |
| RING 4 | | | | | |
| CONTROLLER 1 | SEQUENCE 4 | | | | |
| RING 1 | | | | | |
| RING 2 | | | | | |
| RING 3 | | | | | |
| RING 4 | | | | | |
| CONTROLLER 1 | SEQUENCE 5 | | | | |
| RING 1 | | | | | |
| RING 2 | | | | | |
| RING 3 | | | | | |
| RING 4 | | | | | |
| CONTROLLER 1 | SEQUENCE 6 | | | | |
| RING 1 | | | | | |
| RING 2 | | | | | |
| RING 3 | | | | | |
| RING 4 | | | | | |
| CONTROLLER 1 | SEQUENCE 7 | | | | |
| RING 1 | | | | | |
| RING 2 | | | | | |
| RING 3 | | | | | |
| RING 4 | | | | | |
| CONTROLLER 1 | SEQUENCE 8 | | | | |
| RING 1 | | | | | |
| RING 2 | | | | | |
| RING 3 | | | | | |
| RING 4 | | | | | |

1-1-3. PHASE RING SEQUENCE (CONT)

| CONTROLLER 1 | SEQUENCE 9 | <u> </u> | | | | | | | |
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| RING 1 | | | | | | | | | |
| RING 2 | | | | | | | | | |
| RING 3 | | | | | | | | | |
| RING 4 | | | | | | | | | |
| CONTROLLER 1 | SEQUENCE 10 | | | | | | | | |
| RING 1 | | | | | | | | | |
| RING 2 | | | | | | | | | |
| RING 3 | | | | | | | | | |
| RING 4 | | | | | | | | | |
| CONTROLLER 1 | SEQUENCE 11 | | | | | | | | |
| RING 1 | | | | | | | | | |
| RING 2 | | | | | | | | | |
| RING 3 | | | | | | | | | |
| RING 4 | | | | | | | | | |
| CONTROLLER 1 | SEQUENCE 12 | | | | | | | | |
| RING 1 | | | | | | | | | |
| RING 2 | | | | | | | | | |
| RING 3 | | | | | | | | | |
| RING 4 | | | | | | | | | |
| CONTROLLER 1 | SEQUENCE 13 | | | | | | | | |
| RING 1 | | | | | | | | | |
| RING 2 | | | | | | | | | |
| RING 3 | | | | | | | | | |
| RING 4 | | | | | | | | | |
| CONTROLLER 1 | SEQUENCE 14 | | | | | | | | |
| RING 1 | | | | | | | | | |
| RING 2 | | | | | | | | | |
| RING 3 | | | | | | | | | |
| RING 4 | | | | | | | | | |
| CONTROLLER 1 | SEQUENCE 15 | | | | | | | | |
| RING 1 | | | | | | | | | |
| RING 2 | | | | | | | | | |
| RING 3 | | | | | | | | | |
| RING 4 | | | | | | | | | |
| CONTROLLER 1 | SEQUENCE 16 | | | | | | | | |
| RING 1 | | | | | | | | | |
| RING 2 | | | | | | | | | |
| RING 3 | | | | | | | | | |
| RING 4 | | | | | | | | | |

1-3. PHASE TO LOAD SWITCH (MMU) ASSIGNMENT

| TOND | PHASE | | DIMM | ING | | AUTO FLASH | | | | |
|-------|-------------|----------|---------|------------|-----------|------------|-----------|-----------|--|--|
| SWITC | / OVERLA | TYP E | RE D | YELLO W | GREE N | PHAS E | COLO R | TOGE - | | |
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1-4-1. SDLC OPTIONS

| | BIU NUMBER | | | | | | | | | | |
|----------------------------------|------------|---|---|---|---|---|---|---|--|--|--|
| TERM & FACIL | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| ENABLE | | | | | | | | | | | |
| PEER-PEER EN | | | | | | | | | | | |
| DETECTOR RACK | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | |
| ENABLE | | | | | | | | | | | |
| PEER-PEER EN | | | | | | | | | | | |
| MMU ENABLE | | | | | | | | | | | |
| MMU STOP TIME | | | | | | | | | | | |
| DIAGNOSTIC ENABLE (TEST FIXTURE) | | | | | | | | | | | |
| CONTROLLER PEER TO PEER ENABLE | | | | | | | | | | | |
| DISABLE 3 CRITICAL RFES LOCKUP | | | | | | | | | | | |

1-4-2. MMU PROGRAM



1-4-3. COLOR CHECK DISABLE

| DISABLE ALL CO CHECKS | LOR | | | | | | | |
|--------------------------|-----|----|----|----|----|----|----|----|
| MMU CHANNEL | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| GREEN / WALK | | | | | | | | |
| YELLOW / PC | | | | | | | | |
| RED / DW | | | | | | | | |
| MMU CHANNEL | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| GREEN / WALK | | | | | | | | |
| YELLOW / PC | | | | | | | | |
| RED / DW | | | | | | | | |

1-5-1 GLOBAL PORT PARAMETERS

| NTCIP BACKUP TIME (SECONDS) | |
|-----------------------------|--|
| PORT 2 PRIORITY | |
| PORT 3A PRIORITY | |
| PORT 3B PRIORITY | |
| ETHERNET PRIORITY | |

1-5-1 PORT 2 (TERMINAL)

| PROTOCOL | |
|-----------------------------------|--|
| ENABLE | |
| DATA RATE (BPS) | |
| DATA, PARITY, STOP | |
| MODEM SETUP STRING | |
| USER STRING | |
| OMM. PORT ADDRESS | |
| SYSTEM DETECTOR 9 - 16 ADDRESS | |
| TELEMETRY RESPONSE DELAY | |
| DUPLEX HALF - FULL | |
| AB3418 / NTCIP GROUP ADDRESS | |
| AB3418 / NTCIP SINGLE FLAG ENABLE | |
| NTCIP PROTOCOL | |
| RTS TO CTS DELAY | |
| RTS TURN OFF DELAY | |
| DROP OUT TIME (in seconds) | |
| EARLY RTS | |

1-5-3 PORT 3A (TELEMETRY)

| PROTOCOL | |
|-----------------------------------|--|
| ENABLE | |
| DATA RATE (BPS) | |
| DATA, PARITY, STOP | |
| MODEM SETUP STRING | |
| USER STRING | |
| COMM. PORT ADDRESS | |
| SYSTEM DETECTOR 9 - 16 ADDRESS | |
| ELEMETRY RESPONSE DELAY | |
| DUPLEX HALF - FULL | |
| AB3418 / NTCIP GROUP ADDRESS | |
| AB3418 / NTCIP SINGLE FLAG ENABLE | |
| NTCIP PROTOCOL | |
| RTS TO CTS DELAY | |
| RTS TURN OFF DELAY | |
| DROP OUT TIME (in seconds) | |
| EARLY RTS | |

1-7-1 ADMINISTRATION

| SUPERVISOR ACCESS CODE | |
|--|--|
| ENABLE CRC CHECK OF DATA BASE | |
| CRC OF PROGRAM DATA BASE | |
| REQUEST DOWNLOAD OF PROGRAMMED DATA | |

1-7-2 DISPLAY OPTIONS

| KEY | CLICK | ENABLE |
|------|-------|--------|
| BACK | TTGHT | ENABLE |

1-5-4. PORT 3B (TELEMETRY)

| PROTOCOL | | | | |
|--------------------------------------|--|--|--|--|
| ENABLE | | | | |
| DATA RATE (BPS) | | | | |
| DATA, PARITY, STOP | | | | |
| MODEM SETUP STRING | | | | |
| USER STRING | | | | |
| COMM. PORT ADDRESS | | | | |
| SYSTEM DETECTOR 9 - 16 ADDRESS | | | | |
| TELEMETRY RESPONSE DELAY | | | | |
| DUPLEX HALF - FULL | | | | |
| AB3418 / NTCIP GROUP ADDRESS | | | | |
| AB3418 / NTCIP SINGLE FLAG ENABLE | | | | |
| NTCIP PROTOCOL | | | | |
| RTS TO CTS DELAY | | | | |
| RTS TURN OFF DELAY | | | | |
| DROP OUT TIME (in seconds) | | | | |
| EARLY RTS | | | | |

1-5-5 ETHERNET PORT CONFIGURATION

| IP ADDRESS | | | |
|----------------------------|--|--|--|
| ADDRESS MASK | | | |
| FTP SERVER ADDRESS | | | |
| DEFAULT GATEWAY ADDRESS | | | |

1-6-1 ENABLE EVENT LOGS

| CRITICAL RFE'S (MMU/TE) | |
|-----------------------------------|--|
| 3 CRITICAL RFE ERRORS IN 24 HOURS | |
| NON-CRITICAL RFE'S (DET/TEST) | |
| DETECTOR ERRORS | |
| COORDINATION ERRORS | |
| MMU FLASH FAULTS | |
| LOCAL FLASH FAULTS | |
| PREEMPT | |
| POWER ON/OFF | |
| LOW BATTERY | |
| ACCESS | |
| DATA CHANGE | |
| CONTROLLER DOWNLOAD | |
| ALARM 1 | |
| ALARM 2 | |
| ALARM 3 | |
| ALARM 4 | |
| ALARM 5 | |
| ALARM 6 | |
| ALARM 7 | |
| ALARM 8 | |
| ALARM 9 | |
| ALARM 10 | |
| ALARM 11 | |
| ALARM 12 | |
| ALARM 13 | |
| ALARM 14 | |
| ALARM 15 | |
| ALARM 16 | |

1-8-1 LOGIC STATEMENT CONTROL

| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 |
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| LP 1- | | | | | | | | | | |
| 10 | | | | | | | | | | |
| LP 11-20 | | | | | | | | | | |
| LP 21-30 | | | | | | | | | | |
| LP 31-40 | | | | | | | | | | |
| LP 41-50 | | | | | | | | | | |
| LP 51-60 | | | | | | | | | | |
| LP 61-70 | | | | | | | | | | |
| LP 71-80 | | | | | | | | | | |
| LP 81-90 | | | | | | | | | | |
| LP 91-10 | | | | | | | | | | |

1-8-1 LOGIC STATEMENT CONTROL

| LOGIC GATE NUMBER | | | | |
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1-8-2 LOGIC PROCESSOR STATEMENTS

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ASC/3 Programming Manual

1-8-2 LOGIC PROCESSOR (CONTINUED)

| LOGIC | GATE NUMBER | | |
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| 1-8-2 LOGIC PROCESSOR (CONTINUED) | | | | |
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1-8-2 LOGIC PROCESSOR (CONTINUED)

| LOGIC GATE NUMBER | | | | | | | | | | |
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CONTROLLER SUBMENU

2-1. CONTROLLER TIMING DATA

| PHASE 1 0 1 0 0 1 0 0 1 1 0 1 1 0 1 | DUAGE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|--|---|-----|-----|----------|-----|----------|-----|-----|-----|---|----|----|----|----|----|----------|----|
| MINIMUM GREEN 7 20 7 10 </td <td>PHASE</td> <td>- 7</td> <td>20</td> <td>7</td> <td>10</td> <td>7</td> <td>20</td> <td>7</td> <td>10</td> <td>Ŭ</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>10</td> | PHASE | - 7 | 20 | 7 | 10 | 7 | 20 | 7 | 10 | Ŭ | | | | | | | 10 |
| BICYCLE MINIMUM GREEN I | | ' | 20 | <i>'</i> | 10 | <i>'</i> | 20 | ' | 10 | | | | | | | <u> </u> | |
| CONDITIONAL SERVICE MINIMUM GREEN I | | | | | | | | | | | | | | | | ┣── | |
| DELAYED GREEN Image: Control of the | CONDITIONAL SERVICE MINIMUM GREEN | | | | | | | | | | | | | | | ┣── | |
| WALKMALKMMM <td>DELAYED GREEN</td> <td></td> | DELAYED GREEN | | | | | | | | | | | | | | | | |
| WALK I | | - | 7 | | 7 | | 7 | | 7 | | | | | | | | |
| WALK 2 I <td>WALK</td> <td></td> <td>1</td> <td></td> <td>1</td> <td></td> <td>1</td> <td></td> <td>1</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td><u> </u></td> <td></td> | WALK | | 1 | | 1 | | 1 | | 1 | | | | | | | <u> </u> | |
| WALK MAX Image: Constraint of the cons | WALK 2 | | | | | | | | | | | | | | | <u> </u> | |
| PEDESTRIAN CLEARANCE 32 34 32 34 32 34 32 34 34 32 34 35 35 35 <td< td=""><td>WALK MAX</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>\vdash</td><td></td></td<> | WALK MAX | | | | | | | | | | | | | | | \vdash | |
| PEDESTRIAN CLEARANCE 2 I <td>PEDESTRIAN CLEARANCE</td> <td></td> <td>32</td> <td></td> <td>34</td> <td></td> <td>32</td> <td></td> <td>34</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> | PEDESTRIAN CLEARANCE | | 32 | | 34 | | 32 | | 34 | | | | | | | | |
| PEDESTRIAN CLEARANCE MAXIII <thi< th="">II<t< td=""><td>PEDESTRIAN CLEARANCE 2</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<></thi<> | PEDESTRIAN CLEARANCE 2 | | | | | | | | | | | | | | | | |
| PEDESTRIAN CARRY OVER Image: style sty | PEDESTRIAN CLEARANCE MAX | | | | | | | | | | | | | | | | |
| VEHICLE EXTENSION3.55.53.53.53.55.53.53.55.53.5 | PEDESTRIAN CARRY OVER | | | | | | | | | | | | | | | | |
| VEHICLE EXTENSION 3.5 5.5 3.5 <td></td> | | | | | | | | | | | | | | | | | |
| VEHICLE EXTENSION 2 I | VEHICLE EXTENSION | 3.5 | 5.5 | 3.5 | 3.5 | 3.5 | 5.5 | 3.5 | 3.5 | | | | | | | | |
| MAX1 20 55 20 35 20 55 20 36 20 40 20 < | VEHICLE EXTENSION 2 | | | | | | | | | | | | | | | | |
| MAX1 20 55 20 36 20 40 20 < | | | | | | | | | | | | | | | | | |
| MAX2 20 60 20 40 20 < | MAX1 | 20 | 55 | 20 | 35 | 20 | 55 | 20 | 35 | | | | | | | | |
| MAX3 Image: Constraint of the second sec | MAX2 | 20 | 60 | 20 | 40 | 20 | 60 | 20 | 40 | | | | | | | | |
| DYNAMIC MAXImage: Second systemImage: Se | MAX3 | | | | | | | | | | | | | | | | |
| DYNAMIC MAX STEPIII <td>DYNAMIC MAX</td> <td></td> | DYNAMIC MAX | | | | | | | | | | | | | | | | |
| YELLOW CHANGE3.03.7< | DYNAMIC MAX STEP | | 1 | | | | | | | | | | | | | | |
| YELLOW CHANGE 3.0 3.7 3.0 | | | | | | | | | | | | | | | | | |
| RED CLRANCE 1.0 2.6 1.0 2.8 2.0 2.6 1.0 2.8 | YELLOW CHANGE | 3.0 | 3.7 | 3.0 | 3.7 | 3.0 | 3.7 | 3.0 | 3.7 | | | | | | | | |
| RED MAX Image: Constraint of the second | RED CLRANCE | 1.0 | 2.6 | 1.0 | 2.8 | 2.0 | 2.6 | 1.0 | 2.8 | | | | | | | | |
| RED REVERT Image: Constraint of the second seco | RED MAX | | | | | | | | | | | | | | | | |
| ACTUATIONS BEFORE GAP REDUCTION Image: Constraint of the second seco | RED REVERT | | | | | | | | | | | | | | | | |
| ACTUATIONS BEFORE GAP REDUCTION Image: Constraint of the second seco | | | | | | | | | | | | | | | | | |
| SECONDS PER ACTIONS ADDED TO INITIAL Image: Constraint of the second | ACTUATIONS BEFORE GAP REDUCTION | | | | | | | | | | | | | | | | |
| MAXIMUM ADDED INITIAL GREEN Image: Constraint of the second s | SECONDS PER ACTIONS ADDED TO INITIAL | | | | | | | | | | | | | | | | |
| TIME BEFORE GAP REDUCTION Image: Constraint of the second sec | MAXIMUM ADDED INITIAL GREEN | | | | | | | | | | | | | | | | |
| CARS WAITING BEFORE GAP REDUCTION Image: Constraint of the second seco | TIME BEFORE GAP REDUCTION | İ | 1 | 1 | | | 1 | 1 | 1 | 1 | | 1 | 1 | | | | 1 |
| STEP TO REDUCE Image: Constraint of the second se | CARS WAITING BEFORE GAP REDUCTION | | 1 | | | | | | | | | | | | | | |
| TIME TO REDUCE TO MINIMUM Image: Constraint of the second secon | STEP TO REDUCE | | 1 | | | | | | | | | | | | | | |
| MININIMUM GAP | TIME TO REDUCE TO MINIMUM | | | | | | | | | | | | | | | <u> </u> | |
| | MININIMUM GAP | | | | | | | | | | | | | | | <u> </u> | |

2-2 VEHICLE OVERLAP

| OVERLAP PHASES 1 | | | | | | | | | | | | | | | | | | _ | | | | | | | | | | | | | | | | | |
|--|----------------|---|---|---|----|-------|----------|---|---|---|--------|--------|--------|--------|--------|--------|--------|------------|-------------------|---|---|---|----------|------|---------|---|---|---|---|----------|------|----|---|---|----------|
| PHASES 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 1 <td>OVERLAP A</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td></td> <td>OVERLAP C</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> | OVERLAP A | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | OVERLAP C | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| INCLUDED Image: State of the state of | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| PROTECT I </td <td>INCLUDED</td> <td></td> <td>INCLUDED</td> <td></td> | INCLUDED | | | | | | | | | | | | | | | | | | INCLUDED | | | | | | | | | | | | | | | | |
| MODIFIER I< | PROTECT ED | | | | | | | | | | | | | | | | | | PROTECT ED | | | | | | | | | | | | | | | | |
| PEDESTRI AN PROTECT NOT | MODIFIER | | | | | | | | | | | | | | | | | | MODIFIER | | | | | | | | | | | | | | | | |
| AN OVERLAP AN OVERLAP <td>PEDESTRI</td> <td></td> <td>PEDESTRI</td> <td></td> | PEDESTRI | | | | | | | | | | | | | | | | | | PEDESTRI | | | | | | | | | | | | | | | | |
| NOT N | AN PROTECT | | | | | | | | | | | | | | | | | | AN PROTECT | | | | | | | | | | | | | | | | |
| TRALING GREEN TRALING YELOW TRALING TRALING TRALING TRALING TRALING TRALING TRALING RED TRALING TRALING TRALING RED TRALING RED TRALING TRALING TRALING RED TRALING TRALING TRALING RED TRALING TRALING TRALING TRALING TRALING RED TRALING TRALING TRALING RED TRALING TRALING T | NOT OVERLAP | | | | | | | | | | | | | | | | | | NOT OVERLAP | | | | | | | | | | | | | | | | |
| GHEEN VELLOW PHab Image: state of the state of | TRAILING | | | | TR | AILI | NG | | | | | TF | AILI | NG | | | | | TRAILING | | | | TF | AILI | NG | | | | | TR | AILI | NG | | | |
| PHASES 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 <th1< th=""> 1 <th1< th=""> <th1< th=""></th1<></th1<></th1<> | GREEN | | | 1 | YE | :LLO | W | r | 1 | | - | RE | :D | 4 | 4 | 4 | 4 | | GREEN | | | | YE | LLO | vv | | 1 | | 1 | RE 1 | :D | 4 | 1 | 4 | 1 |
| TRALING I </td <td>PHASES</td> <td>1</td> <td>2</td> <td>3</td> <td>4</td> <td>5</td> <td>6</td> <td>7</td> <td>8</td> <td>9</td> <td>0</td> <td>1</td> <td>2</td> <td>3</td> <td>4</td> <td>1 5</td> <td>6</td> <td></td> <td>PHASES</td> <td>1</td> <td>2</td> <td>3</td> <td>4</td> <td>5</td> <td>6</td> <td>7</td> <td>8</td> <td>9</td> <td>0</td> <td>1</td> <td>2</td> <td>3</td> <td>4</td> <td>5</td> <td>6</td> | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 1 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| LEbuling Log Log <thlog< th=""> Log <thlog< th=""> <t< td=""><td>TRAILING</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td></t<></thlog<></thlog<> | TRAILING | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | - |
| OVERLAP B OVERLAP B OVERLAP B OVERLAP B OVERLAP B OVERLAP B OVERLAP B OVERLAP B OVERLAP CREEN OVERLAP CREEN <td></td> <td><u>u</u> </td> <td></td> | | | | | | | | | | | | | | | | | | <u>u</u> | | | | | | | | | | | | | | | | | |
| PHASES 1 2 3 4 5 6 7 8 9 0 1 <td>GREEN</td> <td></td> <td>ļ</td> <td>GREEN</td> <td></td> | GREEN | | | | | | | | | | | | | | | | | ļ | GREEN | | | | | | | | | | | | | | | | |
| PHASES 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 <td></td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>DUADED</td> <td></td> <td>•</td> <td>•</td> <td></td> <td>-</td> <td>•</td> <td>7</td> <td></td> <td>•</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> | | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | DUADED | | • | • | | - | • | 7 | | • | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| PLASH GREEN GREEN | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | FLASH | 1 | 2 | 3 | 4 | 5 | 6 | 1 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| OVERLAP | GREEN | | | | | | | | | | | | | | | | | | GREEN | | | | | | | | | | | | | | | | |
| OVERLAP B PHASES 1 2 3 4 5 6 7 8 9 0 1 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| DB D <thd< th=""> <thd< th=""> <thd< th=""></thd<></thd<></thd<> | | | | | | | | | | | | | | | | | | i 1 | OVERLAP | | | | | | | | | | | | | | | | |
| PHASES 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 <td>B</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td></td> <td>D</td> <td></td> <td>~</td> <td>~</td> <td></td> <td>-</td> <td>~</td> <td>-</td> <td></td> <td>~</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> | B | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | D | | ~ | ~ | | - | ~ | - | | ~ | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| INCLUDED Image: state stat | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 1 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| PROTECT | INCLUDED | | | | | | | | | | | | | | | | | | INCLUDED | | | | | | | | | | | | | | | | |
| MODIFIER I <thi< th=""> I<!--</td--><td>PROTECT ED</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>ED</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></thi<> | PROTECT ED | | | | | | | | | | | | | | | | | | ED | | | | | | | | | | | | | | | | |
| PEDESTRI AN PROTECT PEDESTRI AN PROTECT< | MODIFIER | | | | | | | | | | | | | | | | | | MODIFIER | | | | | | | | | | | | | | | | |
| AN PROTECT AN PROTECT <td>PEDESTRI</td> <td></td> <td>PEDESTRI</td> <td></td> | PEDESTRI | | | | | | | | | | | | | | | | | | PEDESTRI | | | | | | | | | | | | | | | | |
| NOT OVERLAP NOT ITRAILING GREEN TRAILING YELLOW TRAILING RED TRAILING TRAILING <t< td=""><td>AN PROTECT</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>AN PROTECT</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<> | AN PROTECT | | | | | | | | | | | | | | | | | | AN PROTECT | | | | | | | | | | | | | | | | |
| TRAILING GREEN TRAILING YELLOW TRAILING RED TRAILING RED TRAILING YELLOW TRAILING RED TRAILING TRAILING RED | NOT OVERLAP | | | | | | | | | | | | | | | | | | NOT OVERLAP | | | | | | | | | | | | | | | | |
| PHASES 1 2 3 4 5 6 7 8 9 0 1 <th1< th=""> 1 <th1< th=""> <th1< th=""></th1<></th1<></th1<> | | | | | TR | RAILI | NG | • | • | | | TF | | NG | | | | i | TRAILING GREEN | | | | TF YE | | NG W | | | | | TR RE | AILI | NG | | | |
| PHASES 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 <th1< th=""> 1 <th1< th=""> <th1< th=""></th1<></th1<></th1<> | | | | | | | <u> </u> | [| | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | i li | | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| TRAILING Indicator | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| LEADING Image: Construction of the c | TRAILING | | | | | | | | | | | | | | | | | | LEADING | | | | | | | | | | | | | | | | \vdash |
| ADVANCE GREEN GREEN PHASES 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 FLASH GREEN GREEN I I I I 1 <td< td=""><td></td><td></td><td></td><td> </td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td><u>∥</u> ∥</td><td>ADVANCE</td><td>L</td><td></td><td>L</td><td> </td><td>L</td><td>L</td><td>L</td><td>I</td><td></td><td></td><td><u> </u></td><td>L</td><td></td><td>1</td><td></td><td></td></td<> | | | | | | | | | | | | | | | | | | <u>∥</u> ∥ | ADVANCE | L | | L | | L | L | L | I | | | <u> </u> | L | | 1 | | |
| PHASES 1 2 3 4 5 6 7 8 9 0 1 <td>GREEN</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>-</td> <td>-</td> <td></td> <td>GREEN</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td> </td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> <td>1</td> | GREEN | | | | | | - | - | | | | | | | | | | | GREEN | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| GREEN | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| | FLASH | | | | | | | | | | | | | | | | | | GREEN | | | | | | | | | | | | | | | | |

2-2 VEHICLE OVERLAP (CONTINUED)

| OVERLAP E | | | 0 | | - | | | | • | 1 | 1 | 1 | 1 | 1 | 1 | 1 | OVERLAP G | | • | 0 | | - | | - | 0 | 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
|--|---|---|---|---------------|-------------------|--------------|--------------------|---|---|------------------|--------------------|--------------------------------|------------------------|--------|------------------|------------------|---|---|---|---|---------------|--------------------|-------------------|---|---|---|--------|--------------------|--------------------------------|----------|--------|---------|--------|
| | 1 | 2 | 3 | 4 | 5 | 6 | - / | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | 1 | 2 | 3 | 4 | 5 | 6 | / | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| PROTECT | | | | | | | \vdash | | | | | | | | | | PROTECT | | | | | | | | | | | | | ⊢┤ | | | |
| ED | | | | | | | | | | | | | | | | | ED | | | | | | | | | | | | | | | | |
| MODIFIER | | | | | | | | | | | | | | | | | MODIFIER | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PROTECT | | | | | | | | | | | | | | | | | PROTECT | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| TRAILING | | | | TR | AILI | NG | | | | | TR | AILII | NG | | | | TRAILING | | | | TR | AILIN | ١G | | | | | TR | AILI | NG | | | |
| GREEN | 1 | | | YE | LLO | W | — | - | | | RE | D | | | . 1 | | GREEN | - | | | YE | LLO\ | N | | | | | RE | D | | | | |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| TRAILING | | | | | | | | | | | | | | | | | TRAILING | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| GREEN | | | | | | | | | | | | | | | | | GREEN | | | | | | | | | | | | | | | | |
| DUADED | | • | • | | - | | _ | | • | 1 | 1 | 1 | 1 | 1 | 1 | 1 | BUAGEO | | • | ~ | | - | • | - | • | • | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| FLASH | 1 | 2 | 3 | 4 | 5 | 6 | - / | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | FLASH | 1 | 2 | 3 | 4 | 5 | 6 | 1 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| GREEN | | | | | | | | | | | | | | | | | GREEN | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| OVERLAP | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | | | | | | | | | | 1 | 1 | 1 | | 1 | 1 | 1 |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| INCLUDED | | | | | | | | | | | | | | | | | INCLUDED | | | | | | | | | | | | | | | | |
| PROTECT | | | | | | | | | | | | | | | | | DROTECT | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | PROTECT | | | | | | | | | | | | | | | | |
| | | | | | | | $\left - \right $ | | | | | | | | | | | | | | | | | | | | | | | \vdash | 1 | | |
| PEDESTRI | | | | | | | | | | | | | | | | | MODIFIER PEDESTRI | | | | | | | | | | | | | | | | |
| AN | | | | | | | | | | | | | | | | | MODIFIER PEDESTRI AN | | | | | | | | | | | | | | | | |
| AN PROTECT NOT | | | | | | | | | | | | | | | | | PROTECT ED MODIFIER PEDESTRI AN PROTECT NOT | | | | | | | | | | | | | | | | |
| PEDESTRI AN PROTECT NOT OVERLAP | | | | | | | | | | | | | | | | | PROTECT ED MODIFIER PEDESTRI AN PROTECT NOT OVERLAP | | | | | | | | | | | | | | | | |
| PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN | | | | TR YE | AILI | NG | | | | | TR | AILII D | NG | | | | MODIFIER PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN | | | | TR | AILIN | NG N | | | | | TR | AILI | NG | | | |
| PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES | 1 | 2 | 3 | TR YE | AILI | NG W | 7 | 8 | 9 | 1 | TR RE 1 | AILII D 1 2 | NG 1 | 1 | 1 | 1 | PHOTECT ED MODIFIER PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES | 1 | 2 | 3 | TR YE | AILIN | NG NG | 7 | 8 | 9 | 1 | TR RE 1 | AILII D 1 | NG 1 | 1 4 | 1 | 1 |
| PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING | 1 | 2 | 3 | TR YE 4 | AILI LLO 5 | NG W 6 | 7 | 8 | 9 | 1 0 | TR RE 1 | AILII D 1 2 | NG 1 3 | 1 4 | 1 5 | 1 6 | MODIFIER PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING | 1 | 2 | 3 | TR YE 4 | AILIN LLO\ 5 | NG N 6 | 7 | 8 | 9 | 1 0 | TR RE 1 | AILII D 1 2 | NG | 1 4 | 1 5 | 1 6 |
| PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING LEADING | 1 | 2 | 3 | TR YE 4 | AILI LLO 5 | NG W 6 | 7 | 8 | 9 | 1 0 | TR RE 1 1 | AILII D 1 2 | NG 1 3 | 1 4 | 1 5 | 1 6 | MODIFIER PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING LEADING | 1 | 2 | 3 | TR YE 4 | AILIN LLOV | NG W 6 | 7 | 8 | 9 | 1 0 | TR RE 1 | AILII D 1 2 | NG 1 3 | | 1 5 | 1 6 |
| PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING LEADING ADVANCE GREEN | 1 | 2 | 3 | TR YE 4 | AILI LLO 5 | NG W 6 | 7 | 8 | 9 | 1 0 | TR RE 1 | AILII D 1 2 | NG 1 3 | 1 4 | 1 5 | 1 6 | PHOTECT ED MODIFIER PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING LEADING ADVANCE GREEN | 1 | 2 | 3 | TR YE 4 | AILIN LLOV 5 | NG W 6 | 7 | 8 | 9 | 10 | TR RE 1 | AILI D 1 2 | NG | 1 4 | 1 5 | 1 6 |
| PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES PHASES | 1 | 2 | 3 | TR YE 4 | AILII LLO 5 | NG W 6 | 7 | 8 | 9 | 1 0 | TR RE 1 1 | AILII D 1 2 | NG 1 3 | | 1 5 | 1 6 | PHOTECT ED MODIFIER PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING LEADING ADVANCE GREEN PHASES | 1 | 2 | 3 | TR YE 4 | AILIN LLOV | NG W 6 | 7 | 8 | 9 | 1 0 | TR RE 1 1 | AILII D 1 2 | NG | | 1 5 1 5 | 1 6 |
| PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING LEADING ADVANCE GREEN PHASES FLASH | 1 | 2 | 3 | TR YE 4 | AILI LLO 5 | NG W 6 | 7 | 8 | 9 | 1 0 1 0 | TR RE 1 1 | AILII D 1 2 1 2 | NG 1 3 1 3 | | 1 5 1 5 | 1 6 1 6 | PHOTECT ED MODIFIER PEDESTRI AN PROTECT NOT OVERLAP TRAILING GREEN PHASES TRAILING LEADING ADVANCE GREEN PHASES FLASH | 1 | 2 | 3 | TR YE 4 | AILIN LLOV 5 | √G ₩ 6 6 | 7 | 8 | 9 | 1 0 | TR RE 1 1 | AILII D 1 2 1 2 | NG | | 1 5 1 5 | |

2-2 VEHICLE OVERLAP (CONTINUED)

| OVERLAP | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | OVERLAP | | | | | | | | | | 1 | 1 | 1 | 1 | 4 | 1 | 1 |
|-----------------|----------|---|---|----|-------|----|---|---|---|--------|---------|--------|--------|--------|--------|--------|------|----------------|---|---|---|----|------|----------|---|---|---|----------|---------|--------|--------|----------|--------|--------|
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| INCLUDED | | | | | | | | | | | | | | | | | | INCLUDED | | | | | | | | | | | | | | | | |
| PROTECT ED | | | | | | | | | | | | | | | | | | PROTECT ED | | | | | | | | | | | | | | | | |
| MODIFIER | | | | | | | | | | | | | | | | | | MODIFIER | | | | | | | | | | | | | | | | |
| PEDESTRI | | | | | | | | | | | | | | | | | | PEDESTRI | | | | | | | | | | | | | | | | |
| PROTECT | | | | | | | | | | | | | | | | | | PROTECT | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | | | TB | All I | NG | | | | | TB | All II | NG | | | | ╎┢ | | | | | TB | | NG | | | | TR | | JG B | FD | _ | | _ |
| GREEN | | | | YE | LLO | W | | | | | RE | D | | | | | | GREEN | | | | YE | LLO | N | | | | | | | | | | |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| | | | | | | | | | | | | | | | | | ╎┝ | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | ! F | | | | | | | | | | | | | | | | | |
| GREEN | | | | | | | | | | | | | | | | | . | GREEN | | | | | | | | | | | | | | _ | | |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| FLASH | | | | | | | | | | | | | | | | | | FLASH | | | | | | | | | | | | | | | | |
| GREEN | | | | | | | | | | | | | | | | | 1 6 | GREEN | | | | | | | | | | <u> </u> | | | | | | |
| OVERLAP | 1 | 1 | | | | 1 | | | | | | | | | | |] [| OVERLAP | | | | | | | | | 1 | | | | | | | |
| J | 1 | _ | _ | 4 | F | ~ | - | | _ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | | 1 | 0 | 0 | 4 | F | <u> </u> | - | | _ | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| | | 2 | 3 | 4 | э | 0 | | 8 | 9 | 0 | 1 | 2 | 3 | 4 | э | Ø | | | - | 2 | 3 | 4 | э | 0 | / | 0 | 9 | 0 | 1 | 2 | 3 | 4 | э | 0 |
| PROTECT | | | | | | | | | | | | | | | | | ╎┠ | PROTECT | | | | | | | | | | | | | | | | |
| ED | | | | | | | | | | | | | | | | | | ED | | | | | | | | | | | | | | | | |
| MODIFIER | | | | | | | | | | | | | | | | | | MODIFIER | | | | | | | | | | | | | | | | |
| PEDESTRI ANI | | | | | | | | | | | | | | | | | | PEDESTRI AN | | | | | | | | | | | | | | | | |
| PROTECT | | | | | | | | | | | | | | | | | | PROTECT | | | | | | | | | | | | | | | | |
| NOT OVERLAP | | | | | | | | | | | | | | | | | | NOT OVERLAP | | | | | | | | | | | | | | | | |
| TRAILING | | ĺ | | TR | AILI | NG | | | | | TR | AILI | NG | | | | ľ | TRAILING | | | | TR | AILI | ١G | | | [| | TR | AILI | NG | | | |
| GREEN | 1 | | | YE | LLO | W | 1 | | | 1 | RE 1 | D 1 | 1 | 1 | 1 | 1 | ╎┟ | GREEN | | | | YE | LLO | N | | | | 1 | RE 1 | :D | 1 | 1 | 1 | 1 |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| | | | | | | | | | | | | | | | | | ╎╟ | TRAILING | | | | | | | | | | | | | | \dashv | - | |
| ADVANCE | <u> </u> | | | | I | | | I | I | l | | | 1 | | | | ! - | ADVANCE | | | | | | | I | I | | I | I | I | | | | |
| GREEN | 1 | | 1 | | | 1 | 1 | 1 | 1 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | ┇╟ | GREEN | | | | | | | 1 | 1 | 1 | 4 | 4 | 4 | 4 | | + 1 | 4 |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | י 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | י 5 | 6 |
| FLASH GREEN | | | | | | | | | | | | | | | | | | FLASH GREEN | | | | | | | | | | | | | | | | |

2-2 VEHICLE OVERLAP (CONTINUED)

| | | | | | | | | | | | | | | | | | 1 6 | | | | | | | | | | | | | | | | | |
|------------------|---|---|---|----|------|----|---|---|---|--------|----|--------|--------|--------|--------|--------|-----|------------------|---|---|---|----|-------|----|---|---|---|--------|----------|--------|--------|--------|--------|--------|
| OVERLAP | | | | | | | | | | 1 | 4 | 4 | 4 | 1 | 4 | 4 | | OVERLAP | | | | | | | | | | 1 | 4 | 4 | 4 | 4 | 4 | 1 |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| INCLUDED | | | - | | - | - | - | - | | | | | - | | - | - | | INCLUDED | | | - | - | Ţ | | - | - | - | | | | - | | - | - |
| PROTECT | | | | | | | | | | | | | | | | | | PROTECT | | | | | | | | | | | | | | | | |
| ED | | | | | | | | | | | | | | | | | | ED | | | | | | | | | | | | | | | | |
| MODIFIER | | | | | | | | | | | | | | | | | | MODIFIER | | | | | | | | | | | | | | | | |
| PEDESTRI | | | | | | | | | | | | | | | | | | PEDESTRI | | | | | | | | | | | | | | | | |
| AN | | | | | | | | | | | | | | | | | | AN | | | | | | | | | | | | | | | | |
| NOT | | | | | | | | | | | | | | | | | | NOT | | | | | | | | | | | | | | | | |
| OVERLAP | | | | | | | | | | | | | | | | | | OVERLAP | | | | | | | | | | | | | | | | |
| TRAILING | | | | TR | AILI | NG | | | | | TR | AILII | NG | | | | | TRAILING | | | | TR | AILI | ١G | | | | | TR | AILI | NG | | | |
| GREEN | - | | | YE | LLO | W | | - | | | RE | D | | | | | | GREEN | | | | YE | LLO | N | - | | | | RE | D | | | | |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| TRAILING | | | | | | | | | | | | | | | | | | TRAILING | | | | | | | | | | | | | | | | |
| LEADING | | | | | | | | | | | | | | | | | ļļ | LEADING | | | | | | | | | | | | | | | | |
| ADVANCE | | | | | | | | | | | | | | | | | | ADVANCE | | | | | | | | | | | | | | | | |
| GREEN | 1 | | | | | 1 | | 1 | | 4 | 4 | 4 | 4 | 4 | 4 | 4 | n k | GREEN | | | | | | | 1 | 1 | 1 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 1 | 1 3 | 4 | ו 5 | 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 1 3 | 4 | ו 5 | 6 |
| FLASH | | | | | | | | | | | | | | | | | | FLASH | | | | | | | | | | | | | | | | |
| GREEN | | | | | | | | | | | | | | | | | | GREEN | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| OVERLAP | | | | | | | | | | | | | | | | | | OVERLAP | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| | 1 | 2 | 2 | 4 | Б | 6 | 7 | 0 | ٥ | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | P | | | | | | | | | | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| | | 2 | 3 | 4 | 5 | 0 | / | 0 | 9 | 0 | - | 2 | 3 | 4 | 5 | 0 | | INCLUDED | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | PROTECT | | | | | | | | | | | | | | | | |
| ED | | | | | | | | | | | | | | | | | | ED | | | | | | | | | | | | | | | | |
| MODIFIER | | | | | | | | | | | | | | | | | | MODIFIER | | | | | | | | | | | | | | | | |
| PEDESTRI | | | | | | | | | | | | | | | | | | PEDESTRI | | | | | | | | | | | | | | | | |
| AN | | | | | | | | | | | | | | | | | | AN | | | | | | | | | | | | | | | | |
| PROTECT | | | | | | | | | | | | | | | | | | PROTECT | | | | | | | | | | | | | | | | |
| OVERLAP | | | | | | | | | | | | | | | | | | OVERLAP | | | | | | | | | | | | | | | | |
| TRAILING | | | | TR | AILI | NG | | | | | TR | AILII | NG | | | | Í | TRAILING | | | | TR | AILII | ١G | | | | | TR | AILI | NG | | | |
| GREEN | | | | YE | LLO | W | | | | | RE | D | | | | | | GREEN | | | | YE | LLO | N | | | | | RE | D | | | | |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 1 | 1 2 | 1 3 | 1 | 1 5 | 1 6 | | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 1 1 | 1 | 1 3 | 1 4 | 1 5 | 1 6 |
| TRAILING | Ŀ | | | Ė | | Ľ | | | Ĺ | | _ | _ | | Ė | - | _ | | TRAILING | | | | | | | | | | | <u> </u> | Ē | - | | | - |
| LEADING | | | | | | | | | | | | | | | | | | LEADING | | | | | | | | | | | | | | | | |
| ADVANCE GREEN | | | | | | | | | | | | | | | | | - | ADVANCE GREEN | | | | | | | | | | | | | | | | |
| | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | Ī | PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| PHASES | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | ╽╟ | | | | | | | | | | | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| GREEN | | | | | | | | | | | | | | | | | | GREEN | | | | | | | | | | | | | | | | |

2-3 PEDESTRIAN OVERLAP

| PEDESTRIAN | 1 O V | ERL | AP | CON | ISIS | rs o | F PH | IASE | S | | | | | | | |
|---------------------------|-------|-----|----|-----|------|------|------|------|---|--------|--------|--------|--------|--------|--------|--------|
| PEDESTRI AN OVERLAP | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| 1 | | | | | | | | | | | | | | | | |
| 2 | | | | | | | | | | | | | | | | |
| 3 | | | | | | | | | | | | | | | | |
| 4 | | | | | | | | | | | | | | | | |
| 5 | | | | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | | | | |
| 7 | | | | | | | | | | | | | | | | |
| 8 | | | | | | | | | | | | | | | | |
| 9 | | | | | | | | | | | | | | | | |
| 10 | | | | | | | | | | | | | | | | |
| 11 | | | | | | | | | | | | | | | | |
| 12 | | | | | | | | | | | | | | | | |
| 13 | | | | | | | | | | | | | | | | |
| 14 | | | | | | | | | | | | | | | | |
| 15 | | | | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | | | | |

2-4 GUARANTEED MINIMUM TIMES

| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|----------------------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|
| MINIMUM GREEN | | | | | | | | | | | | | | | | |
| WALK | | | | | | | | | | | | | | | | |
| PEDESTRIAN CLEARANCE | | | | | | | | | | | | | | | | |
| YELLOW CHANGE | | | | | | | | | | | | | | | | |
| RED CLEARANCE | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| OVERLAP | A | В | С | D | E | F | G | Н | I | J | К | L | М | N | 0 | Ρ |
| MINIMUM GREEN | | | | | | | | | | | | | | | | |
| | Ī | Ī | l | | Ī | | | | | | | | | | | |

2-5 START / FLASH DATA

| POWER S | STAF | T | | | | | | | | | | | | | | |
|-------------|------|------|------|-------|-----|---|---|---|----------|-------------|--------|--------|--------|--------|--------|--------|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| PHASE | | | | | | | | | | | | | | | | |
| OVERL AP | | | | | | | | | | | | | | | | |
| POWER S | STAF | T RE | Ð | | | | | | FL | ASH | TIM | E | | | | |
| REMOTE | (AUT | ГОМ | ATIC |) FLA | ASH | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| ENTRY | | | | | | | | | | | | | | | | |
| EXIT | | | | | | | | | | | | | | | | |
| OVERL AP | A | В | С | D | Е | F | G | Н | I | J | К | L | М | N | 0 | Ρ |
| EXIT | | | | | | | | | | | | | | | | |
| EXIT REM | IOTE | FL | ASH | | | | | | MI FL | NIMI ASH | JM A | UTC | DMAT | IC | | |
| MINIMUM | REC | CALL | | | | | | | СУ | CLE | THF | ROU | GH F | PHAS | ES | |

2-6-1 CONTROLLER OPTIONS

| PEDESTRIAN C | LEA | RAN | CEI | PRO | TEC | , 1 | | | | | | | | | | |
|---------------------------------|-----|-----|-----|-----|-----|-----|---|---|---|--------|--------|--------|--------|--------|--------|--------|
| UNIT RED REVE | ERT | | | | | | | | | | | | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| GUARANTEE D PASSAGE | | | | | | | | | | | | | | | | |
| NON-ACT I | | | | | | | | | | | | | | | | |
| NON ACT II | | | | | | | | | | | | | | | | |
| DUAL ENTRY | | | | | | | | | | | | | | | | |
| PED RESERVICE | | | | | | | | | | | | | | | | |
| REST IN WALK | | | | | | | | | | | | | | | | |
| FLASHING WALK | | | | | | | | | | | | | | | | |
| PED CLEAR > YELLOW | | | | | | | | | | | | | | | | |
| PED CLEAR > ALL RED | | | | | | | | | | | | | | | | |
| INIT GREEN + VEHICLE EXIT | | | | | | | | | | | | | | | | |

2-7 ACTUATED / PRE-TIMED MODE PHASES

| ENABLE I | PRE- | TIME | ED O | PER | ATIC | N | | | | | | | | | | |
|----------------|-------|------|------|------|------|-----|---|---|---|--------|--------|--------|--------|--------|--------|--------|
| FREE INF | ם דטי | DISA | BLE | D PR | E-TI | MED | | | | | | | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| PRE - TIMED | | | | | | | | | | | | | | | | |

COORDINATOR SUBMENU

3-1 COORDINATOR OPTIONS

| MANUAL PATTERN | Auto | | |
|-----------------------------------|--------|---------------------------------------|--------|
| INTERCONNECT SOURCE | TBC | INTERCONNECT FORMAT | |
| TRANSITION | Smooth | ECPI COORDINATION | Yes |
| OFFSET REFERENCE | Lead | DWELL / ADD TIME | |
| DELAY COORD WALK TO LOCAL ZERO | No | FORCE OFF | Float |
| FORCE OFF ADDED INITIAL GREEN | No | USE PED TIME FOR SMOOTH TRANSITION | No |
| PEDESTRIAN RECALL | No | PEDESTRIAN RESERVICE | Yes |
| ENABLE MANUAL SYNC | | LOCAL ZERO OVERRIDE | Yes |
| RE-SYNC COUNT | No | MAX SELECT | MaxInh |
| MULTISYNC | No | | |

3-2 COORDINATOR PATTERN

| COORDINA | 10 | R P/ | 4 I I | FKI | N | 1 | | | | | | | | | | | | | | | |
|-----------------------|-----------|----------|-------|-----|-----|----|----|----|------|------|------|-----|------|------|----|-----|-----|---|---|----|----|
| CYCLE LEI (SECONDS | NGT 3) | Ή | | | | 13 | 30 | S | PLI | ΓPΑ | TT | ERI | N | | | | | | | | |
| OFFSET V | ÁLU | E | | | | 12 | | S | EQI | JEN | CE | | | | | | | | | | |
| SPLITS IN | | | | | | Pe | er | 0 | FFS | SET | s in | ۱ | | | | | | | | Pe | er |
| CROSSING | à AR | TEF | ٦Υ | | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P | PERI | MISS | SIVE | E 1 | | | | V | EHI | CLE | PE | ERN | liss | SIVE | Ξ2 | LEN | IGT | Н | | | |
| LENGTH | | | | | | | | | | | | | | | | | | | | | |
| VEHICLE F | PERI | MISS | SIVE | Ξ2 | | | | A | CTI | ON | PLA | ١N | | | | | | | | 1 | |
| DISPLACE | MEN | JT | | | | | | | | | | | | | | | | | | | |
| ACTUATE |) | | | | | Υe | es | Т | IMIN | NG F | ۷LA | N | | | | | | | | | |
| COORDINA | ATIC | <u>N</u> | | | | | | | | | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | .K | | | P | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| RING SPLI | T E> | (TEI | VSI | NC | (SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEM | 1ANI | D PA | ١T | ERN | ١ | | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EМ | ENT | Γ | | | | | | | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | | | | 8 | 9 | 1 | | 1 | | | 1 | | | 1 | | |
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| PREFER | | | | | | | | | | | | | | | | | | | | | |
| ENCE 1 | | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER | | | | | | | | | | | | | | | | | | | | | |
| ENCE 2 | | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | _ | | | | | | | | | | | | | | | | |
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| SPECIAL | | | | | | | | | | | | | | | | | | | | | |
| FUNCT | | | | | | | | | | | | | | | | | | | | | |
| UN | | | | | | | | | | | | | | | | | | | | | |

| COORDINA | TO | R P/ | ٩TT | ERN | J | 2 | | | | | | | | | | | | | | | |
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| CYCLE LEN (SECONDS | NGT | Ή | | | | 120 |) | S | PLI | ΓPA | λTΤ | ERI | N | | | | | | | | |
| OFFSET VA | ٩LU | E | | | | 49 | | S | EQI | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | Per | | 0 | FFS | SET | s in | J | | | | | | | | Pe | er |
| CROSSING | i AR | TEF | ٦Υ | | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P | ERM | VIS | SIVE | E 1 | | | | V | EHI | CLE | E PE | ERN | liss | SIVE | Ξ2 | LEN | 1G1 | Н | | | |
| LENGTH | | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P | ERM | MISS | SIVE | 2 | | | | A | CTI | ON | PL | ٩N | | | | | | | | 2 | |
| DISPLACE | MEN | 1T | | | | | | | | | | | | | | | | | | 2 | |
| ACTUATED |) | | | | | Yes | s | TI | MIN | NG F | PLA | N | | | | | | | | | |
| COORDINA | | N N | | | | | _ | _ | | | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | K | | | P | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| | | | | | | | | | | | | 1 | | 2 | | | 3 | | | 4 | |
| RING SPLI | ΓЕХ | (TEI | VSIC | DN (| SEC | ON | ID: | S) | | | | | | | | | | | | | |
| SPLIT DEM | AN |) PA | ۱TT | ERN | | | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EМ | ENT | • | | | | | | | | | | | | | | | | | |
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| PREFER | | | | | | | | | | | | | | | | | | | | | |
| ENCE 1 | | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER | | | | | | | | | | | | | | | | | | | | | |
| ENCE 2 | | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | | |

| COORDINA | ٩ΤΟ | RΡ | ATT | ERN | ١ | 3 | | | | | | | | | | | | | | | |
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| CYCLE LEI (SECONDS | NGT 3) | Ή | | | | 13 | 30 | S | PLI | ΤP | ١T | ER | N | | | | | | | | |
| OFFSET V | ALU | E | | | | 1: | 2 | S | EQI | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | P | Per | 0 | FFS | SET | s II | ٧ | | | | | | | | Pe | er |
| CROSSING PATTERN | à AR | TEF | ٦Y | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | PERI | MIS | SIVE | Ξ1 | | | | V | EHI | CLE | P | ERN | liss | SIVE | Ξ2 | LEN | 1G1 | ГН | | | |
| VEHICLE P DISPLACE | PERI | NISS IT | SIVE | E 2 | | | | A | CTI | ON | PL/ | ٩N | | | | | | | | 3 | |
| ACTUATED COORDINA |) ATIC | N | | | | Y | es | T | IMIN | NG F | PLA | ١N | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | Κ | | | Ρ | HAS | SE F | RES | SER | VIC | E | | | | | | | |
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| RING SPLI | T E> | (TEI | NSI | ON (| SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEM | IAN | | ATT | ERN | Ì | | | / | | | | | | | | | | | | | |
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| RING DISP | LAC | EM | ENT | - | | | | | | | | I | | | | | | | | | |
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| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

3-2 COORDINATOR PATTERN (CONTINUED)

| COORDINA | NTΟ | R P/ | ATT | ERM | ۱. | 4 | | | | | | | | | | | | | | | |
|----------------------------|------|------------|------|------|-----|----|----|----|------|------|--------|-----|--------|------|---|--------|-----|---|--------|----|----|
| CYCLE LEN (SECONDS | NGT | Ή | | | | 10 | 0 | S | PLI | ΓPΑ | ١T | ERI | N | | | | | | | | |
| OFFSET V | ÁLU | E | | | | 59 | 9 | | | | | | | | | | | | | | |
| SPLITS IN | | | | | | Pe | er | 0 | FFS | SET | S IN | 1 | | | | | | | | Pe | er |
| CROSSING PATTERN | i AR | TEF | ۲Y | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MISS | SIVE | E 1 | | | | V | EHI | CLE | PE | R№ | liss | SIVE | 2 | LEN | IGT | Ή | | | |
| VEHICLE P DISPLACE | | MISS JT | SIVE | 2 | | | | A | СТІ | ON | PLA | ١N | | | | | | | | 4 | |
| | |)N | | | | Ye | es | Т | IMIN | NG F | ۶LA | N | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | K | | | Р | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| RING SPLI | ΓE> | (TEI | VSI |) NC | (SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEM | IANI | D PA | ١TT | ERN | 1 | | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EМ | ENT | - | | | | | | | | | | | | | | | | | |
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| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

| COORDINA | TΟ | R P/ | ATT | ERN | 1 | 5 | | | | | | | | | | | | | | |
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| CYCLE LEN | IGT | Ή | | | | | S | PLI | T PA | ١ΤΤ | ERI | N | | | | | | | | |
| (SECONDS |) | | | | | | | | | | | | | | | | | | | |
| OFFSET VA | ٩LU | E | | | | | S | EQI | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | C |)FFS | SET | s in | | | | | | | | | | |
| CROSSING | i AR | TEF | RY | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MISS | SIVE | 1 | | | V | EHI | CLE | E PE | RM | liss | SIVE | 2 | LEN | IGT | Н | | | |
| VEHICLE P DISPLACEI | | NISS IT | SIVE | 2 | | | A | CTI | ON | PLA | N | | | | | | | | 5 | |
| ACTUATED |) | | | | | | Т | IMIN | NG F | PLA | N | | | | | | | | | _ |
| COORDINA | TIC | N | | | | | | | - | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | K | | Р | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| RING SPLI | ΓE> | (TEI | NSIC | DN (| SEC | ONC | S) | | | | | | | | | | | | | |
| SPLIT DEM | AN |) PA | ATTI | ERN | l | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EМ | ENT | • | | | | | | | | | | | | | | | | |
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| PREFER | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | 1 |
| PREFER | | | | | | | | | | | | | | | | | | | | |
| ENCE 2 | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | |

| COORDINA | TO | R P/ | ATT | ERN | ١ | | 1 | | | | | | | | | | | | | |
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| CYCLE LEN (SECONDS | NGT 5) | Ή | | | | | S | PLI | ΤP | ΛTT | ERI | N | | | | | | | | Î |
| OFFSET V | ٩LU | E | | | | | S | EQ | UEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | С |)FFS | SET | s in | I | | | | | | | | | |
| CROSSING PATTERN | à AR | TEF | ۲Y | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ER | MISS | SIVE | 1 | | | V | ΈHI | CLE | PE | RM | liss | SIVE | 2 | LEN | IGT | ΓH | | | |
| VEHICLE P DISPLACE | | NISS NT | SIVE | 2 | | | A | CTI | ON | PLA | ٨N | | | | | | | | | |
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| ACTUATED |) RE | ST | IN V | VAL | К | | Ρ | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| RING SPLI | T E> | (TEI | VSI | DN (| SECO | DND | S) | | | | | | | | | | | | | |
| SPLIT DEN | IAN | D PA | ١TT | ERN | 1 | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EM | ENT | - | | | | | | | | | | | | | | | | |
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| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | |

| COORDINA | ΔTO | R P/ | ATT | ERN | 7 | | | | | | | | | | | | | | | | |
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| CYCLE LEN (SECONDS | NGT | Ή | | | | | | S | PLI | ΤP | λTT | ERI | N | | | | | | | | |
| OFFSET VA | ٩LU | E | | | | | | S | EQI | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | | 0 | FFS | SET | S IN | 1 | | | | | | | | | |
| CROSSING | AR | TEF | ۲Y | | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MIS | SIVE | E 1 | | | | V | EHI | CLE | E PE | RN | liss | SIVE | 2 | LEN | IGT | Н | | | |
| VEHICLE P DISPLACE | | | SIVE | 2 | | | | A | CTI | ON | PLA | ٨N | | | | | | | | | |
| ACTUATED |) | | | | | | | Т | IMIN | NG F | ۶LA | N | | | | | | | | | |
| COORDINA | TIC | N | | | | | | | | | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | Κ | | | Ρ | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| RING SPLIT | ΓE> | (TEI | NSIC |) NC | SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEM | ANI |) P/ | ٩TTI | ERN | 1 | | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EМ | ENT | - | | | | | | | | | | | | | | | | | |
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| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

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3-2 COORDINATOR PATTERN (CONTINUED)

| COORDINA | ٩ΤΟ | R P/ | ATT | ERN | ٧ | | | | | | | | | | | | | | | | |
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| CYCLE LEN (SECONDS | NGT 5) | Ή | | | | | | S | PLI | T P/ | ٩ΤΤ | ERI | N | | | | | | | | |
| OFFSET V | ٩LU | E | | | | | | S | EQ | UEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | | С | FFS | Set | S IN | 1 | | | | | | | | | |
| CROSSING | à AF | TEF | ٦Y | | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MISS | SIVE | Ξ1 | | | | V | EHI | CLE | E PE | RN | liss | SIVE | Ξ2 | LEN | IGT | Н | | | |
| VEHICLE P DISPLACE | 'ERI MEN | MISS NT | SIVE | 2 | | | | A | CTI | ON | PL | ٨N | | | | | | | | | |
| ACTUATED |) | | | | | | | Т | IMI | NG I | PLA | N | | | | | | | | | |
| COORDINA | ATIC | N | | | | | | | | | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | K | | | P | HA | SE F | RES | ER | VIC | Е | | | | | | | |
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| RING SPLI | T E) | KTEI | NSI | ON (| (SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEM | IAN | D PA | ٩TT | ERN | 1 | | | | | | | | | | | | | | | | |
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| RING DISP | LAC | ЕМ | ENT | - | | | | | | | | | | | | | | | | | |
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| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

| COORDINA | ΔTO | R P/ | ATT | ERN | J | | | | | | | | | | | | | | | |
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| CYCLE LEN | IGT | Ή | | | | | S | PLI | ΓP | ١TT | ERI | N | | | | | | | | |
| (SECONDS | 5) | | | | | | | | | | | | | | | | | | | |
| OFFSET VA | 4LU | E | | | | | S | EQ | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | 0 | FFS | SET | S IN | | | | | | | | | | |
| CROSSING | i AR | TEF | ٦Y | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MISS | SIVE | 1 | | | V | EHI | CLE | E PE | RM | liss | SIVE | 2 | LEN | JGT | Η | | | |
| VEHICLE P | ER | MISS | SIVE | 2 | | | A | CTI | ON | PLA | ٨N | | | | | | | | | |
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| ACTOATEL | | .01 | | | N | | Г | TIA. | | 1LO | LN | VIC | <u> </u> | | | | | | | |
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| SPLIT DEM | IANI | JPA | 111 | ERN | | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EM | ENT | | | | | | | | | | | | | | - | | | |
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| PREFER | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | |
| PREFER | | | | | | 1 | | | | | | | | | | | | | | |
| ENCE 2 | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | |

| COORDIN | ٩TO | RΡ | ATT | ERN | ٧ | | | | | | | | | | | | | | | | |
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| CYCLE LE | NGT | Ή | | | | | | S | PLľ | T PA | ١Τ٢ | ERI | Ν | | | | | | | | |
| (SECONDS | S) | | | | | | | | | | | | | | | | | | | | |
| OFFSET V | ALU | E | | | | | | S | EQI | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | | 0 | FFS | SET | S IN | | | | | | | | | | |
| CROSSING | 3 AF | TEF | ٦Y | | | | | | | | | | | | | | | | | | |
| VEHICLE F | PERI | MIS | SIVE | Ξ1 | | | | V | EHI | CLE | E PE | RM | liss | SIVE | Ξ2 | LEN | IGT | ΓH | | | |
| VEHICLE F | PERI | VIS: VT | SIVE | 2 | | | | A | СТІ | ON | PLA | N | | | | | | | | | |
| ACTUATE | C | | | | | | | Т | IMIN | NG F | ۶LA | Ν | | | | | | | | | _ |
| COORDIN | ATIC | N | | | | | | | | | | | | | | | | | | | |
| ACTUATE |) RE | ST | IN V | VAL | K | | | Ρ | HAS | SE F | RES | ER | VIC | Е | | | | | | | |
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| | | | | | | | | | | | | 1 | | 2 | | | 3 | | | 4 | |
| RING SPLI | T E) | (TE | NSI | ON (| (SE | COI | ND | S) | | | | | | | | | | | | | |
| SPLIT DEN | 1AN | D P/ | ٩TT | ERN | 1 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| RING DISP | LAC | ЕM | EN٦ | Γ | | | | | | | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | | | | 8 | 9 | 1 | | 1 | | | 1 | | | 1 | | |
| | L | | | | | | | | | | 0 | | 1 | | | 3 | | | 5 | | |
| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

| COORDINA | TΟ | RΡ | ATT | ERN | ١ | | | | | | | | | | | | | | | | |
|----------------------------|------------|------|------|------|----|----|----|----|------|------|--------|-----|--------|------|----|--------|-----|---|--------|---|--|
| CYCLE LEN (SECONDS | NGT | Ή | | | | | | S | PLI | ΓPΑ | ٩ΤΤ | ERI | N | | | | | | | | |
| OFFSET VA | ٩LU | E | | | | | | S | EQI | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | | 0 | FFS | SET | S IN | I | | | | | | | | | |
| CROSSING PATTERN | i AR | TEF | ٦Y | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | VIS | SIVE | 1 | | | | V | EHI | CLE | E PE | RM | liss | SIVE | Ξ2 | LEN | IGT | Ή | | | |
| VEHICLE P SPLACEME | ERI ENT | MIS | SIVE | 2 | | | | A | CTI | ON | PLA | ٨N | | | | | | | | | |
| ACTUATED |) | | | | | | | T | IMIN | NG F | PLA | Ν | | | | | | | | | |
| COORDINA | TIC | N | | | | | | | | | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | K | | | Ρ | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| | | | | | | | | | | | | 1 | | 2 | | | 3 | | | 4 | |
| RING SPLI | ΓE> | (TEI | NSI | DN (| SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEM | ANI |) P/ | ATT | ERN | 1 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| RING DISP | LAC | EМ | ENT | • | | | | | | | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | | | | 8 | 9 | 1 0 | | 1 1 | | | 1 3 | | | 1 5 | | |
| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

3-2 COORDINATOR PATTERN (CONTINUED)

| COORDINA | ٩ΤΟ | R P/ | ATT | ERN | ٧ | | | | | | | | | | | | | | | | |
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| CYCLE LEN (SECONDS | NGT 5) | Ή | | | | | | S | PLI | T P/ | ٩ΤΤ | ERI | N | | | | | | | | |
| OFFSET V | ٩LU | E | | | | | | S | EQ | UEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | | С | FFS | Set | S IN | 1 | | | | | | | | | |
| CROSSING | à AF | TEF | ٦Y | | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MISS | SIVE | Ξ1 | | | | V | EHI | CLE | E PE | RN | liss | SIVE | Ξ2 | LEN | IGT | Н | | | |
| VEHICLE P DISPLACE | 'ERI MEN | MISS NT | SIVE | 2 | | | | A | CTI | ON | PL | ٨N | | | | | | | | | |
| ACTUATED |) | | | | | | | Т | IMI | NG I | PLA | N | | | | | | | | | |
| COORDINA | ATIC | N | | | | | | | | | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | K | | | P | HA | SE F | RES | ER | VIC | Е | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | 1 | | 2 | | | 3 | | | 4 | |
| RING SPLI | T E) | KTEI | NSI | ON (| (SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEM | IAN | D PA | ٩TT | ERN | 1 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| RING DISP | LAC | ЕМ | ENT | - | | | | | | | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | | | | 8 | 9 | 1 0 | | 1 1 | | | 1 3 | | | 1 5 | | |
| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

| COORDINA | ΔTO | R P/ | ATT | ERN | J | | | | | | | | | | | | | | | |
|---------------------|------|-----------|------|-------|------|-----|----|--------|------|--------|-----|--------|----------|---|--------|-----|---|--------|---|---|
| CYCLE LEN | IGT | Ή | | | | | S | PLI | ΓP | ١TT | ERI | N | | | | | | | | |
| (SECONDS | 5) | | | | | | | | | | | | | | | | | | | |
| OFFSET VA | 4LU | E | | | | | S | EQ | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | 0 | FFS | SET | S IN | | | | | | | | | | |
| CROSSING | i AR | TEF | ٦Y | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MISS | SIVE | 1 | | | V | EHI | CLE | E PE | RM | liss | SIVE | 2 | LEN | JGT | Η | | | |
| VEHICLE P | ER | MISS | SIVE | 2 | | | A | CTI | ON | PLA | ٨N | | | | | | | | | |
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| ACTOATEL | | .01 | | | N | | Г | TIA. | | 1LO | LN | VIC | <u> </u> | | | | | | | |
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| | | | 1510 | | SEUC | עמו | 5) | | | | | | | | | | | | | |
| SPLIT DEM | IANI | JPA | 111 | ERN | | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EM | ENT | | | | | | | | | | | | | | - | | | |
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| PREFER | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | |
| PREFER | | | | | | 1 | | | | | | | | | | | | | | |
| ENCE 2 | | | | | | | | | | | | | | | | | | | | |
| PHASES | | | | | | | | | | | | | | | | | | | | |

| COORDIN | ATO | R P | ATT | ERI | ٧ | | | | | | | | | | | | | | | | |
|----------------------------|------|------------|------|-----|-----|-----|----|----|------|------|------|-----|------|------|---|-----|-----|----|---|---|--|
| CYCLE LE | NGT | Ή | | | | | | S | PLI | T PA | ١Τ | ERI | N | | | | | | | | |
| (SECONDS | S) | | | | | | | | | | | | | | | | | | | | |
| OFFSET V | ALU | E | | | | | | S | EQI | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | | 0 | FFS | SET | S IN | | | | | | | | | | |
| CROSSING | g af | RTEF | ٦Y | | | | | | | | | | | | | | | | | | |
| VEHICLE F | PERI | MIS | SIVE | Ξ1 | | | | V | EHI | CLE | E PE | RM | liss | SIVE | 2 | LEN | IGT | ГН | | | |
| VEHICLE F | PERI | MIS: VT | SIVE | 2 | | | | A | CTI | ON | PLA | N | | | | | | | | | |
| ACTUATE | D | | | | | | | Т | IMIN | NG F | ۶LA | N | | | | | | | | | |
| COORDIN | ATIC | DΝ | | | | | | | | | | | | | | | | | | | |
| ACTUATE | D RE | EST | IN V | VAL | K | | | Ρ | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| | | | | | | | | | | | | 1 | | 2 | | | 3 | | | 4 | |
| RING SPLI | T E) | KTE | NSI | NC | (SE | COI | ND | S) | | | | | | | | | | | | | |
| SPLIT DEN | /AN | D P/ | ATT | ERN | 1 | | | | | | | | | | | | | | | | |
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| RING DISF | LAC | СЕМ | EN٦ | Γ | | | | | | | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | | | | 8 | 9 | 1 | | 1 | | | 1 | | | 1 | | |
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| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

| COORDINA | ΔTO | RΡ | ATT | ERN | 1 | | | | | | | | | | | | | | | | |
|----------------------------|------------|------|------|------|----|----|----|----|-----|------|--------|-----|--------|------|---|--------|-----|---|--------|---|--|
| CYCLE LEN (SECONDS | NGT | Ή | | | | | | S | PLI | ΤP | ATT | ERI | N | | | | | | | | |
| OFFSET VA | ٩LU | E | | | | | | S | EQI | JEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | | 0 | FFS | SET | S IN | 1 | | | | | | | | | |
| CROSSING PATTERN | i AR | TEF | ٦Y | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MIS | SIVE | 1 | | | | V | EHI | CLE | E PE | RM | liss | SIVE | 2 | LEN | NGT | Ή | | | |
| VEHICLE P DISPLACEI | ERI MEN | NIS: | SIVE | 2 | | | | A | CTI | ON | PLA | ٨N | | | | | | | | | |
| ACTUATED |) | | | | | | | T | IMI | NG F | PLA | Ν | | | | | | | | | |
| COORDINA | TIC | N | | | | | | | | | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | Κ | | | Ρ | HAS | SE F | RES | ER | VIC | Е | | | | | | | |
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| | | | | | | | | | | | | 1 | | 2 | | | 3 | | | 4 | |
| RING SPLI | ΓE> | (TEI | NSI | DN (| SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEM | ANI | D P/ | ATT | ERN | J | | | | | | | | | | | | | | | | |
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| RING DISP | LAC | EМ | ENT | - | | | | | | | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | | | | 8 | 9 | 1 0 | | 1 1 | | | 1 3 | | | 1 5 | | |
| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

| COORDINA | ٩ΤΟ | R P/ | ATT | ERN | ١ | | | | | | | | | | | | | | | | |
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| CYCLE LEN (SECONDS | NGT S) | Ή | | | | | | S | PLI | T P/ | ΥT | ERI | N | | | | | | | | |
| OFFSET V | ٩LU | E | | | | | | S | EQI | UEN | ICE | | | | | | | | | | |
| SPLITS IN | | | | | | | | 0 | FFS | SET | s in | l | | | | | | | | | |
| CROSSING PATTERN | i AR | TEF | ۲Y | | | | | | | | | | | | | | | | | | |
| VEHICLE P LENGTH | ERI | MISS | SIVE | Ξ1 | | | | V | EHI | CLE | PE | RN | liss | SIVE | Ξ2 | LEN | IGT | Ή | | | |
| VEHICLE P DISPLACE | ERI MEN | NISS NT | SIVE | E 2 | | | | A | СТІ | ON | PLA | ٨N | | | | | | | | | |
| ACTUATED |) | | | | | | | Т | IMIN | NG F | ۲LA | Ν | | | | | | | | | |
| COORDINA | ATIC | N | | | | | | | | | | | | | | | | | | | |
| ACTUATED |) RE | ST | IN V | VAL | Κ | | | Ρ | HAS | SE F | RES | ER | VIC | E | | | | | | | |
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| | | | | | | | | | | | | 1 | | 2 | | | 3 | | | 4 | |
| RING SPLI | TΕ> | KTEI | NSI | ON (| SE | CO | ND | S) | | | | | | | | | | | | | |
| SPLIT DEN | IANI | D PA | ٩TT | ERN | 1 | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | | |
| RING DISP | LAC | ЕМ | ENT | - | | | | | | | | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | | | | 8 | 9 | 1 0 | | 1 1 | | | 1 3 | | | 1 5 | | |
| PREFER ENCE 1 PHASES | | | | | | | | | | | | | | | | | | | | | |
| PREFER ENCE 2 PHASES | | | | | | | | | | | | | | | | | | | | | |

| COORDINAT | OR | PAT | TER | Ν | | | | | | | | | | | | |
|--|-------------|------|------|-----|------|-----|----------|------|------------|--------|--------|--------|--------|--------|--------|--------|
| CYCLE LENG | ЭТН | (SEC | CON | DS) | | | SF | LIT | PAT | TER | N | | | | | |
| OFFSET VAL | UE. | | | | | | SE | QUE | ENC | Ε | | | | | | |
| SPLITS IN | | | | | | | OF | FSE | TS I | Ν | | | | | | |
| CROSSING A | ARTE | ERY | PAT | TER | IN | | | | | | | | | | | |
| VEHICLE PE LENGTH | RMI | SSIV | 'E 1 | | | | VE LE | HIC | LE P TH | ERN | AISS | IVE | 2 | | | |
| VEHICLE PE DISPLACEM | RMIS ENT | SSIV | 'E 2 | | | | AC | CIT | N PL | AN. | | | | | | |
| ACTUATED (| 200 | RDI | NATI | ION | | | TI | MINC |) PL | AN | | | | | | |
| ACTUATED F | RES | T IN | WAL | K | | | PF | IASE | E RE | SER | VICE | = | | | | |
| | | | | | | | | | | | | | | | | |
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| RING SPLIT | EXT | ENS | ION | (SE | CONE | DS) | | | | | | | | | | |
| SPLIT DEMA | ND I | PAT | ΓERI | N | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| RING DISPL | ACEI | MEN | Т | | | | | | | | | | | | | |
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3-3 SPLIT PATTERN

| SPLIT PATTER | RN N | IUME | BER | | 1 | | | | | | | | | | | | SPLIT PATTER | RN N | IUME | BER | | 2 | | | | | | | | | | | |
|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | x | | | | x | | | | | | | | | | | COORDINA TED PHASE(S) | | x | | | | x | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | | PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | 9 | | 53 | 3 | 1 | 1 | 2 | 7 | 1 | 5 | 4 | 7 | 1 | 1 | 2 | ?7 | SPLIT VALUE | 1 | 2 | 5 | 1 | 1 | 2 | 2 | 5 | 1 | 2 | 51 | I | 1 | 2 | 25 | 5 |
| MODE | | | | | | | | | | | | | | | | | MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | 6 | PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | | MODE | | | | | | | | | | | | | | | | |

| SPLIT PATTER | ERN NUMBER | | | | 3 | | | | | | | | | | | | Γ | SPLI |
|-----------------------------|------------|---|----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|---|--------------------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | | PHAS |
| COORDINA TED PHASE(S) | | x | | | | x | | | | | | | | | | | | COO TED PHAS |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | | [| PHAS |
| SPLIT VALUE | 1 | 0 | 5 | 3 | 17 | | 20 | | 10 |) | 5 | 3 | 10 |) | 27 | | | SPLI VALU |
| MODE | | | | | | | | | | | | | | | | | | MOD |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | | | PHAS |
| SPLIT VALUE | | | | | | | | | | | | | | | | | | SPLI VALU |
| MODE | | | | | | | | | | | | | | | | | | MOD |

| SPLIT PATTER | TTERN NUMBER | | | | 4 | | | | | | | | | | | |
|-----------------------------|--------------|---|----|--|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 2 3 4 | | | | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | x | | | | х | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | 12 | 2 | 48 | | 12 | 2 | 2 | 8 | 12 | 2 | 48 | В | 12 | 2 | 28 | 3 |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

| SPLIT PATTER | RN N | UME | BER | | | | | | | | | | | | | |
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| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

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| SPLIT PATTER | RN N | UME | BER | | | | | | | | | | | | | |
|-----------------------------|------|-----|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

| SPLIT PATTER | RN N | UME | BER | | | | | | | | | | | | | |
|-----------------------------|------|-----|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

| SPLIT PATTER | RN N | IUME | BER | | | | | | | | | | | | | |
|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

3-3 SPLIT PATTERN (CONTINUED)

| SPLIT PATTER | RN N | UME | BER | | | | | | | | | | | | | | | SPLIT PATTER | RN N | IUME | BER | | | | | | | | | | | | | |
|-----------------------------|------|-----|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|---|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | Ĩ | PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | | | COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | | | PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | | | MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | | | PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | | 1 | MODE | | | | | | | | | | | | | | | | |

| SPLIT PATTER | RN N | IUME | BER | | | | | | | | | | | | | | SPLIT PATTER | RN N | UME | BER | | | | | | | | | | | | | |
|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|-----------------------------|------|-----|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | | COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | | PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | | MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | | PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | | MODE | | | | | | | | | | | | | | | | |

| SPLIT PATTER | PATTERN NUMBER | | | | | | | | | | | | | | | |
|-----------------------------|----------------|--|----|--|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 2 3 4 | | | | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

| SPLIT PATTER | RN N | IUME | BER | | | | | | | | | | | | | |
|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

| | | | | | | | 7 | | | | | | | | | |
|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| SPLIT PATTER | RN N | IUME | BER | | | | | | | | | | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

| SPLIT PATTER | RN N | IUME | BER | | | | | | | | | | | | | |
|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | |

3-3 SPLIT PATTERN (CONTINUED

| SPLIT PATTERN NUMBER | | | | | | | | | ſ | SPLIT PATTER | RN N | UMB | ER | | | | | | | | | | | | | |
|-----------------------------|----|-----|-----|--------|-----|------------|----|--------|---|-----------------------------|------|-----|----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE 1 2 3 4 | 56 | 7 8 | 9 0 | 1 1 | 1 2 | 1 1 3 4 | 1 | 1 6 | | PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE 1 2 | 3 | 4 | 5 | 6 | | 7 | 8 | | | PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | MODE | | | | | | | | | | | | | | | | |
| PHASE 9 10 | 11 | 12 | 13 | 14 | | 15 | 16 | 5 | | PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | MODE | | | | | - | | | | | | | | | | | |

| SPLIT PATTER | RN N | IUME | BER | | | | | | | | | | | | | | | SPLIT PATTER | RN N | IUME | BER | | | | | | | | | | | | | |
|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|---|-----------------------------|------|------|-----|---|----|---|----|---|----|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 | Ī | PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | | | COORDINA TED PHASE(S) | | | | | | | | | | | | | | | | |
| PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | | | PHASE | 1 | | 2 | | 3 | | 4 | | 5 | | 6 | | 7 | | 8 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | | | MODE | | | | | | | | | | | | | | | | |
| PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | | | PHASE | 9 | | 10 | | 11 | | 12 | | 13 | | 14 | | 15 | | 16 | |
| SPLIT VALUE | | | | | | | | | | | | | | | | | | SPLIT VALUE | | | | | | | | | | | | | | | | |
| MODE | | | | | | | | | | | | | | | | | | MODE | | | | | | | | | | | | | | | | |

3-4 AUTO PERMISSIVE MINIMUM GREEN TIME

| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
|------------------|---|----|----|----|----|----|----|----|
| MINIMUM GREEN | | | | | | | | |
| PHASE | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| MINIMUM GREEN | | | | | | | | |

3-5 SPLIT DEMAND

| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
|--------------|-----|---|---|---|---|---|---|---|---|--------|--------|--------|--------|--------|--------|--------|
| DEMAN D 1 | | | | | | | | | | | | | | | | |
| DEMAN D 2 | | | | | | | | | | | | | | | | |
| DEMAND | | | 1 | | 2 | | | | | | | | | | | |
| DETECTO | R | | | | | | | | | | | | | | | |
| CALL TIME | | | | | | | | | | | | | | | | |
| (SECONDS | S) | | | | | | | | | | | | | | | |
| CYCLE CO | UNT | | | | | | | | | | | | | | | |

PREEMPTOR SUBMENU 4-1 PREEMPTOR

| PREEMPTOR N | IUMI | BER | | | | 1 | | 1 | | | | | | | | | | |
|---------------|---------|------|------|------|-------|------|-------|-----|----------|-------|-------|------|----------|------|-----|-----|----------|---|
| ACTIVE | | | | | | | | NO | N-LO | CK IN | PUT | | | | | | | |
| PREEMPTION (| DVE | RRI | DE | | | | | INT | ERLO | CK E | NABL | E | | | | | | |
| DELAY TIME (S | ECC |)ND | S) | | | | | INH | IBIT 1 | IME | (SEC | OND | S) | | | | | |
| EXTEND INPUT | (SE | CO | NDS | 5) | | | | MA | X PRE | SEN | CE TI | ME (| SECC | NDS |) | | | |
| DURATION TIM | È (S | ECC | OND | Ś) | | | | TRA | ACK C | LEA | RANC | ERE | SER\ | /ICE | / | | | |
| PED DARK | | | | / | | | | RES | SERV | ICE T | IME | | | | | | | |
| AUTOMATIC FL | .ASH | H HA | SP | RIOF | RITY | | | RE | D CLE | ARG | OES | GRE | EN | | | | | |
| TERMINATE O | /ERI | LAPS | S AS | SAP | | | | PE |) CLE | AR T | HRO | JGH | YELL | OW | | | | |
| BING | _ | | | | | | | 1 | | 2 | | | 3 | | 1 | 4 | | |
| FREE DURING | PRF | FM | PTIC |)N | | | | · · | | - | | | • | | _ | · · | | |
| THEE BOILING | | | The | | 1 | | | DEI | ` | | | | | | _ | | | |
| | | | | | \M | | | | | G | | | VEI | IOW | , | R | ED | |
| | 1. 41 1 | | | | •• | | | ULL | | u | NEEP | • | 166 | LOW | _ | 11 | | |
| | | | | | L | | | | | - | | | | | | | | |
| TRACK CLEAR | ANC | ETI | ME | | | | | | | _ | | | | | | | | |
| MIN DWELL – C | YCL | .E G | IREE | EN/E | XIT ' | YELL | ow /I | RED | | | | | | | | | | |
| DWELL FLASH | | | | | | | | FLA | SH E | XIT C | OLO | R | | | | | | |
| PHASE | | | Τ | | | | | | | | 1 | 1 | 1 | 1 | 1 | T | 1 | 1 |
| | 1 | 2 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | | 5 | 6 |
| TRACK | | | | | | | | | | | | | | | | | | |
| CLEAR | | | | | | | | | | | | | | | | | | |
| PHASE | | | | | | | | | | | | | | | | | | |
| DWELL | | | | | | | | | | | | | | | | | | |
| PHASE | | | | | | | | | | | | | | | | | | |
| DWELL | | | | | | | | | | | | | | | | | | |
| PEDESTRIAN | | | | | | | | | | | | | | | | | | |
| CYCLING | | | | | | | | | | | | | | | | | | |
| PHASE | | | | | | | | | | | | | | | | | | |
| CYCLING | | | | | | | | | | | | | | | | | | |
| PEDESTRIAN | | | | | | | | | | | | | | | | | | |
| EXIT | | | | | | | | | | | | | | | | | | |
| PHASE | | _ | _ | | | | | | | | | | | | | | | |
| EXIT | | | | | | | | | | | | | | | | | | |
| CALLS | | _ | | | | | | | | | | | <u> </u> | | | _ | | |
| SPECIAL | | | | | | | | | | | | | 1 | | 1 | | | |
| FUNCTION | | | | | | L | | | | | | | | | I | Ц, | | |
| PREEMPTION | 100 | :00 | KDII | NATI | UN | _ | | EXI | I TIM | ING | 'LAN | | | | | | | |
| LINKED PREEM | IPT(| JR | | | | | | | | | | | | | | | I | |
| PREEMPTOR A | CTI | VE C | DUTI | PUTS | 3 | | | - | | | | | | | | | n | |
| PREEMPTOR A | CTI | VE C | DUT | | | | | PRI | EEMP | TOR | ACTI | VE O | UT IN | DWE | ELL | | <u> </u> | |
| OTHER PRIORI | TY F | PRE | EMF | PTOR | | | | NO | - | | l | | | | | | | |
| OUT | | | | 1 | 1 | | | | | - | | | - | | - | | | |
| OVERLAP | A | | В | с | D | Е | F | G | н | | J | к | L | м | Ν | С |) | Р |
| TRACK CLEAR | | | | 1 | Ť | Ē | | | <u> </u> | | | Ė | 1 | 1 | Ť | ſ | | |
| OVERLAP | | | | | | | | | | | | 1 | | | | | | |
| DWELL | t | | | 1 | 1 | | | | | 1 | 1 | 1 | | 1 | 1 | | | |
| OVERLAP | | | | | 1 | | | | | | | 1 | | 1 | | | | |
| CYCLING | | | | 1 | | | | | | 1 | 1 | 1 | | | 1 | | | |
| OVERLAP | | | | | | | | | | | 1 | 1 | 1 | 1 | | | | |

| PREEMPTOR N | UMBI | ER | | | 2 | | | | | | | | | | | |
|---------------|-------|--------|--------------|------|-----|-------|-----|---------|-------|-------|-------|-------|------|----------|-----|---|
| ACTIVE | | | | | | | NO | N-LOC | CK IN | PUT | | | | | | |
| PREEMPTION C | VER | RIDE | | | | | INT | ERLO | CK E | NABL | .E | | | | | |
| DELAY TIME (S | ECON | VDS) | | | | | INH | IIBIT T | IME | (SEC | OND | S) | | | | |
| EXTEND INPUT | (SEC | OND | IS) | | | | MA | X PRE | SEN | CE TI | IME (| SECC | NDS |) | | |
| DURATION TIM | E (SE | CON | DS) | | | | TR/ | ACK C | LEAF | RANC | E RE | SER\ | /ICE | | | |
| PED DARK | | | | | | | RE | SERVI | CE T | IME | | | | | | |
| AUTOMATIC FL | ASH | HAS | PRIOF | RITY | | | REI | D CLE | AR G | iOES | GRE | EN | | | | |
| TERMINATE OV | 'ERL/ | APS A | ASAP | | | | PE | D CLE | AR T | HRO | JGH | YELL | OW | | | |
| RING | | | | | | | 1 | | 2 | | | 3 | | | 4 | |
| FREE DURING | PREE | MPT | ION | | | | | | | | | | | | | |
| | | | | | | | PE |) | | | | | | | | |
| | | | | W | ALK | | CLE | EAR | G | REEN | 1 | YEL | LOW | | RED | |
| ENTERING MIN | IMUN | I TIMI | F | | | | - | | | | | | | - | | |
| | | TIME | - | I | | | | | 1 | | | | | + | | |
| | | | | | | ם/ואר | ED | | 1 | | | | | -+ | | |
| | ULLE | GRE | LCIN/E | | | 744/H | | | | | | | | | _ | |
| DWELL FLASH | | | | | | - | FLA | SH E | XII C | OLO | ĸ | | | <u> </u> | | |
| PHASE | | ~ | ~ | | - | ~ | - | | • | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| | 1 | 2 | 3 | 4 | 5 | 6 | / | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| TRACK | | | | | | | | | | | | | | | | |
| CLEAR | | | | | | | | | | | | | | | | |
| PHASE | | | | | | | | | | | | | | | + | - |
| DWELL | | | | | | | | | | | | | | | | |
| DWELL | | | | | | | | | | | | | | | | |
| PEDESTRIAN | | | | | | | | | | | | | | | | |
| CYCLING | | | | | | | | | | | | | | | | |
| PHASE | | | | | | | | | | | | | | | | |
| CYCLING | | | | | | | | | | | | | | | + | |
| PEDESTRIAN | | | | | | | | | | | | | | | | |
| EXIT | | | | | | | | | | | | | | | - | 1 |
| PHASE | | | | | | | | | | | | | | | | |
| EXIT | | | | | | | | | | | | | | | | |
| CALLS | | | | | | | | | | | | | | | | |
| SPECIAL | | | | | | | | | | | | | | | | |
| FUNCTION | | | | | | | | | | | | | | | | |
| PREEMPTION T | 0 00 | ORD | INATI | ON | | | EXI | T TIM | ING F | PLAN | | | | | | |
| LINKED PREEM | PTO | 7 | | | | | | | | | | | | | | |
| PREEMPTOR A | CTIVI | EOU | TPUTS | 3 | | | | | | | | | | | | |
| PREEMPTOR A | CTIVI | E OU | Т | | | | PRI | EEMP | TOR | ACTI | VE O | UT IN | DWE | LL | | |
| OTHER PRIORI | ty pf | REEN | IPTOF | } | 1 | | NO | N-PRI | ORIT | Y PR | EEM | PTOR | OUT | | | |
| OUT | | | | | | | | | | | | | | | | |
| OVERLAP | А | В | С | D | Е | F | G | н | I | J | К | L | М | N | 0 | Р |
| TRACK CLEAR | | | | | | | | | 1 | 1 | 1 | | | 1 | T | 1 |
| OVERLAP | | | | | | | | | | 1 | | | | 1 | | 1 |
| DWELL | Ť | | | | 1 | | | | 1 | 1 | 1 | | 1 | 1 | 1 | 1 |
| OVERLAP | | | | | | | | | | 1 | | | | 1 | | 1 |
| CYCLING | | | | | | | | | 1 | 1 | 1 | | | 1 | 1 | |
| OVERLAP | | | | | | | | | | | | | | | | |

4-2 LOW PRIORITY PREEMPTOR SELECTION

| FILTERED INPUT | SOLID | PULSING |
|-------------------|-------|---------|
| 1 | | |
| 2 | | |
| 3 | | |
| 4 | | |
| 5 | | |
| 6 | | |
| 7 | | |
| 8 | | |
| 9 | | |
| 10 | | |

| PREEMPTOR N | UMBE | R | | | 3 | 3 | | | | | | | | | | | PREEMPTOR N | UMB | ER | | | 4 | | | | | | | | | | | |
|----------------|-------|-------|------|------|------|------|----------------------------|----------------------------|---------------------|-------|-------|------|------|---|----------|---------|---------------|-------|-------|---------|-------|------|-------|------|--------|-------|-------|-------|-------------|--------------|--------------|----------|----------|
| ACTIVE | | | | | | | NC | N-LO | CK IN | IPUT | | | | | | | ACTIVE | | | | | | | NO | N-LO | CK IN | IPUT | | | | | | |
| PREEMPTION C | VER | RIDE | | | | | INT | ERLO | DCK E | ENAB | E | | | | | | PREEMPTION C | VER | RIDE | | | | | INT | ERLC | CK E | ENABI | LE | | | | | |
| DELAY TIME (SE | ECON | IDS) | | | | | INH | HIBIT | TIME | (SEC | ONDS | S) | | | | | DELAY TIME (S | ECON | VDS) | | | | | INH | IBIT 1 | IME | (SEC | ONDS | 3) | | | | |
| EXTEND INPUT | (SEC | OND | S) | | | | MA | X PR | ESEN | ICF T | IMF (| SECC | NDS |) | | | EXTEND INPUT | (SEC | COND | S) | | | | MA | | SEN | ICF T | IMF (| SECC | NDS | 1 | | |
| DUBATION TIME | = (SF | CON | 25) | | | | TR | ACK (| | RANC | FRF | SFR | /ICF | | | | DUBATION TIM | F (SF | CON | DS) | | | | TRA | ACK (| | RANC | FRF | SFR\ | /ICF | | + | |
| PED DARK | - (02 | | | | | | RF | SEB\ | | TIME | | | | | | | PED DABK | - (02 | | | | | | BE | SERV | ICF T | | | | | | - | |
| AUTOMATIC FL | | | | RITY | | | RE | | | SOES | GRE | FN | | | - | | AUTOMATIC FL | ΔSH | HAS | PRI∩I | | | | BEI | | ARO | OES | GRE | FN | | | + | |
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5-1 CLOCK/CALENDAR DATA

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| LP 71-80 | | | | | | | | | | | | | | | | |
| LP 81-90 | | | | | | | | | | | | | | | | |
| LP 91-100 | | | | | | | | | | | | | | | | |

| ACTION PLAN | | 2 | | | | | | | | | | | | | |
|----------------|-------|------|---|---|-----|-----|-----|------|-------|--------|------|------|-----|---|---|
| PATTERN | | | | | 2 | | SY | STEN | / OVE | ERRID | E | | | | |
| VEHICLE DETECT | 'OR F | PLAN | | | | | DE | TECT | for L | .OG | | | | | |
| FLASH | | | | | | | | | | | | | | | |
| RED REST | | | | | | | VE | HICL | e de. | T DIAC | SNO | STIC | PLA | N | |
| CONTROLLER SE | QUE | NCE | | | | | PE | D DE | t dia | GNOS | STIC | PLA | Ν | | |
| TIMING PLAN | | | | | | | DIN | MMIN | G EN | ABLE | | | | | |
| PHASE | 4 | 0 | 0 | | - | | 7 | | 0 | 1 | 1 | 1 | 1 | 1 | 1 |
| | | 2 | 3 | 4 | . 5 | 0 | 1 | 0 | 9 | U | 1 | 2 | 3 | 4 | Э |
| PED RECALL | | | | - | _ | _ | _ | | | | | | | | |
| WALK 2 | | | | - | _ | _ | _ | | | | | | | | |
| | | | | - | - | - | - | | | | | | | 1 | |
| | | | | - | - | - | - | | | | | | | 1 | |
| MAX RECALL | | | | | _ | _ | _ | | | | - | | | - | |
| MAX 3 | | | | - | | - | 1 | | | | | | | | |
| CS INHIBIT | | | | | | | | | | | - | | | | |
| PHASE OMIT | | | | t | | | | | | | | | | | |
| SPEC | | | | T | | | | | (1- | 8) | L | | | | |
| FUNCTION | | | | | | | | | (. | •) | | | | | |
| AUX FUNCTION | | | | | (1 | -3) | | | - | | | | | | |
| | 1 | 2 | 3 | 4 | - 5 | 6 | 7 | 8 | 9 | 10 | 1 | | | | |
| LP 1-10 | | | | | | | | | | | | | | | |
| LP 11-20 | | | | | | | | | | | | | | | |
| LP 21-30 | | | | | | | | | | | | | | | |
| LP 31-40 | | | | | | | | | | | | | | | |
| LP 41-50 | | | | | | | | | | | | | | | |
| LP 51-60 | | | | | | | | | | | | | | | |
| LP 61-70 | | | | | | | | | | | | | | | |
| LP 71-80 | | | | | | | | | | | | | | | |
| LP 81-90 | | | | | | | | | | | | | | | |
| LP 91-100 | | | | | | | | | | | | | | | |

1 6

| ACTION PLAN | | 3 | | | | | | | | | | | | | | |
|--|-------|------|---|---|------|--------------|-----|-------|-------|--------------|--------|--------|------------|--------|--------|--------|
| PATTERN | | | | | 3 | | SY | STEN | 1 OVE | RRID | E | | | | | |
| VEHICLE DETECT | 'OR F | PLAN | | | | | DE | TECT | 'OR L | .0G | | | | | | |
| FLASH | | | | | | | | | | | | | | | | |
| RED REST | | | | | | | VE | HICLI | E DE | r diag | iNO | STIC | PLAN | ۱. | | |
| CONTROLLER SE | QUE | NCE | | _ | | | PE | D DE | T DIA | GNOS | TIC | PLA | N | | | |
| | 1 | r | r | ᆜ | 1 | 1 | DIN | 1MIN | G EN | ABLE | | | 1 . | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| PED RECALL | | | | | | | | | | | | | | | | |
| WALK 2 | | | | | | | | | | | | | | | | |
| VEH EXT 2 | | | | | | | | | | | | | | | | |
| VEH RECALL | | | | | | | | | | | | | | | | |
| MAX RECALL | | | | | | | | | | | | | | | | |
| MAX 2 | | | | | | | | | | | | | | | | |
| MAX 3 | | | | | _ | | | | | | | | | | | |
| CS INHIBIT | | | | | | | | | | | | | | | | |
| PHASE OMIT | | | | - | | | | | | | | | | | | |
| SPEC | | | | | | | | | (1- | 8) | | | | | | |
| | | | | _ | (1) | 2) | | | IJ | | | | | | | |
| AUX FUNCTION | 4 | 0 | 0 | 4 | (1-, | 3) | 7 | 0 | 0 | 10 | i | | | | | |
| 10110 | | 2 | 3 | 4 | 5 | 6 | / | 8 | 9 | 10 | | | | | | |
| LF 1-10 | | | | | - | | | | | | | | | | | |
| LF 11-20 | | | | | | | | | | | | | | | | |
| LP 21-30 | | | | - | - | | | | | | | | | | | |
| LP 41-50 | | | | - | | | | | | | | | | | | |
| LP 51-60 | | | | | | | | | | | | | | | | |
| LP 61-70 | | | | | | | | | | | | | | | | |
| LP 71-80 | | | | - | | | | | | | | | | | | |
| LP 81-90 | | | | | | | | | | | | | | | | |
| LP 91-100 | | | | 1 | | | | | | | | | | | | |
| VEHICLE DETECT | OR F | PLAN | | | 4 | | DE | TECT | ORL | .0G | E | | | | | |
| FLASH | | | | | | | | | | | | | | | | |
| RED REST | | | | | | | VE | HICLI | E DE | r diag | iNO | STIC | PLAN | ١ | | |
| CONTROLLER SE | QUE | NCE | | _ | | | PE | D DE | | GNOS | TIC | PLA | N | | | |
| | 1 | | r | ᆛ | | 1 | DIN | IMIN | G EN | ABLE | | | - | | | 4 |
| PIROL | | | | | | | | | | 4 | + | - | - | 4 | - | |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 6 |
| PED RECALL | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 6 |
| PED RECALL WALK 2 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 6 |
| PED RECALL WALK 2 VEH EXT 2 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 6 |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 6 |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 6 |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 2 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | 1 5 | 6 |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIPT | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | 1 3 | 1 4 | | 6 |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE CMIT | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 | 1 2 | | | | 6 |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 8) | 1 | 1 2 | 1 3 | | 1 5 | 6 |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | | 1 2 | | | 1 5 | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 8) | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION | | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 8) | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 1-10 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 8) | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 1-10 LP 1-10 LP 11-20 | | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 1-10 LP 1-10 LP 1-20 LP 21-30 | | 2 | 3 | 4 | 5 | 6 3) 6 | 7 | 8 | 9 | 1 0 | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 11-10 LP 11-20 LP 21-30 LP 21-30 LP 31-40 | | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 11-20 LP 11-20 LP 21-30 LP 21-30 LP 31-40 LP 41-50 | | 2 | 3 | 4 | 5 | 6 3) 6 | 7 | 8 | 9 | 1 0 | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 11-20 LP 11-20 LP 21-30 LP 21-30 LP 31-40 LP 41-50 LP 51-60 | | 2 | 3 | 4 | 5 | 6 3) 6 | 7 | 8 | 9 | 1 0 | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 11-20 LP 11-20 LP 21-30 LP 31-40 LP 31-40 LP 51-60 LP 51-60 LP 61-70 | | 2 | 3 | 4 | 5 | 6 3) 6 | 7 | 8 | 9 | 1 0 | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 11-20 LP 11-20 LP 21-30 LP 21-30 LP 31-40 LP 31-40 LP 51-60 LP 51-60 LP 51-80 | | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 1-10 LP 11-20 LP 21-30 LP 31-40 LP 31-40 LP 31-40 LP 41-50 LP 51-60 LP 51-60 LP 51-80 LP 51-90 | | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | | | | | | |
| PED RECALL WALK 2 VEH EXT 2 VEH RECALL MAX RECALL MAX 2 MAX 3 CS INHIBIT PHASE OMIT SPEC FUNCTION AUX FUNCTION LP 11-20 LP 11-20 LP 21-30 LP 21-30 LP 31-40 LP 51-60 LP 51-60 LP 51-60 LP 51-70 LP 11-20 LP 11-20 LP 51-90 LP 51-90 LP 91-100 | | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | | | | | | |

| | | | | _ | | | | | | | | | | | | | |
|----------------|------|------|---|---|---|------|----|-----|-------|-------|--------|------|------|------|---|---|---|
| ACTION PLAN | | 5 | | | | | | | | | | | | | | | |
| PATTERN | | | | Ĩ | 5 | | | SY | STEN | 1 OVE | RRID | E | | | | | |
| VEHICLE DETECT | OR F | 'LAN | | | | | | DE | TECT | OR L | .0G | | | | | | |
| FLASH | | | | | | | | | | | | | | | | | |
| RED REST | | | | | | | | VE | HICLI | E DE | T DIAG | SNO | STIC | PLA | ١ | | |
| CONTROLLER SE | QUEI | NCE | | | | | | PE | D DE | t dia | GNOS | STIC | PLA | Ν | | | |
| TIMING PLAN | | | | | | | | DIN | 1MIN | G EN | ABLE | | | | | | |
| PHASE | | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| | 1 | 2 | 3 | 4 | 1 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| PED RECALL | | | | | | | | | | | | | | | | | |
| WALK 2 | | | | | | | | | | | | | | | | | |
| VEH EXT 2 | | | | | | | | | | | | | | | | | |
| VEH RECALL | | | | | | | | | | | | | | | | | |
| MAX RECALL | | | | | | | | | | | | | | | | | |
| MAX 2 | | | | | | | | | | | | | | | | | |
| MAX 3 | | | | | | | | | | | | | | | | | |
| CS INHIBIT | | | | | | | | | | | | | | | | | |
| PHASE OMIT | | | | | | | | | | | | | | | | | |
| SPEC | | | | | | | | | | (1- | 8) | | | | | | |
| FUNCTION | | | | | | | | | | | | | | | | | |
| AUX FUNCTION | | | | | 1 | (1-3 | 3) | | | - | | | | | | | |
| | 1 | 2 | 3 | 4 | ł | 5 | 6 | 7 | 8 | 9 | 10 | 1 | | | | | |
| LP 1-10 | | | | | | | | | | | | | | | | | |
| LP 11-20 | | | | | | | | | | | | | | | | | |
| LP 21-30 | | | | | | | | | | | | | | | | | |
| LP 31-40 | | | | | | | | | | | | | | | | | |
| LP 41-50 | | | | | | | | | | | | | | | | | |
| LP 51-60 | | | | | | | | | | | | | | | | | |
| LP 61-70 | | | | | | | | | | | | | | | | | |
| LP 71-80 | | | | | | | | | | | | | | | | | |
| LP 81-90 | | | | | | | | | | | | | | | | | |
| LP 91-100 | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |
| ACTION PLAN | | | | | | | | | | | | | | | | | |
| PATTERN | | | | | | | | SY | STEN | 1 OVE | RRID | E | | | | | |
| VEHICLE DETECT | OR F | PLAN | | | | | | DE | TECT | 'OR L | .OG | | | | | | |
| FLASH | | | | | | | | | | | | | | | | | |
| RED REST | | | | | | | | VE | HICLI | E DE | T DIAG | SNO | STIC | PLAN | ٧ | | |
| CONTROLLER SE | QUEI | NCE | | | | | | PE | D DE | t dia | GNOS | STIC | PLA | N | | | |
| TIMING PLAN | | | | | | | | DIN | 1MIN | G EN | ABLE | | | | | | |
| PHASE | | | | | | | | ľ | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| | 1 | 2 | 3 | 4 | 1 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| PED RECALL | | | | | | | | | | | | | | | | | |
| WALK 2 | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | |

| | | | | | | | | | | | | | | | | | | LI 21-00 | |
|----------------|------|------|---|---|-----|----|-----|-------|-------|--------|------|------|-----|---|---|---|---|--------------|-------|
| LP 31-40 | | | | | | | | | | | | | | | | | | LP 31-40 | |
| LP 41-50 | | | | | | | | | | | | | | | | | | LP 41-50 | |
| LP 51-60 | | | | | | | | | | | | | | | | | | LP 51-60 | |
| LP 61-70 | | | | | | | | | | | | | | | | | | LP 61-70 | |
| LP 71-80 | | | | | | | | | | | | | | | | | | LP 71-80 | |
| LP 81-90 | | | | | | | | | | | | | | | | | | LP 81-90 | |
| LP 91-100 | | | | | | | | | | | | | | | | | | LP 91-100 | |
| | | | | | - | | | | | | | | | | | | | | |
| ACTION PLAN | | | | | | | | | | | | | | | | | | ACTION PLAN | |
| PATTERN | | | | | | | SY | STEN | / OVE | RRID | E | | | | | | [| PATTERN | |
| VEHICLE DETECT | OR F | 'LAN | | | | | DE | TECT | FOR L | .OG | | | | | | | | VEHICLE DETE | CTOR |
| FLASH | | | | | | | | | | | | | | | | | | FLASH | |
| RED REST | | | | | | | VE | HICLI | E DET | r diag | SNO | STIC | PLA | ٧ | | | | RED REST | |
| CONTROLLER SE | QUEI | NCE | | | | | PE | d de | t dia | GNOS | STIC | PLA | Ν | | | | | CONTROLLER S | SEQUE |
| TIMING PLAN | | | | | | | DIN | /MIN | G EN | ABLE | | | | | | | | TIMING PLAN | |
| PHASE | | | | | | | | | | 1 | 1 | 1 | 1 | 1 | 1 | 1 | | PHASE | |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | | | _ 1 |
| PED RECALL | | | | | | | | | | | | | | | | | | PED RECALL | |
| WALK 2 | | | | | | | | | | | | | | | | | | WALK 2 | |
| VEH EXT 2 | | | | | | | | | | | | | | | | | | VEH EXT 2 | |
| VEH RECALL | | | | | | | | | | | | | | | | | | VEH RECALL | |
| MAX RECALL | | | | | | | | | | | | | | | | | | MAX RECALL | |
| MAX 2 | | | | | | | | | | | | | | | | | | MAX 2 | |
| MAX 3 | | | | | | | | | | | | | | | | | | MAX 3 | |
| CS INHIBIT | | | | | | | | | | | | | | | | | | CS INHIBIT | |
| PHASE OMIT | | | | | | | | | | | | | | | | | | PHASE OMIT | |
| SPEC | | | | | | | | | (1- | 8) | | | | | | | - | SPEC | |
| FUNCTION | | | | | | | | | | | | | | | | | | FUNCTION | |
| AUX FUNCTION | | | | | (1- | 3) | | | | | _ | | | | | | | AUX FUNCTION | 1 |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | | | | | | | | 1 |
| LP 1-10 | | | | | | | | | | | | | | | | | | LP 1-10 | |
| LP 11-20 | | | | | | | | | | | | | | | | | | LP 11-20 | |
| LP 21-30 | | | | | | | | | | | | | | | | | | LP 21-30 | |
| LP 31-40 | | | | | | | | | | | | | | | | | | LP 31-40 | |
| LP 41-50 | | | | | | | | | | | | | | | | | | LP 41-50 | |
| LP 51-60 | | | | | | | | | | | | | | | | | | LP 51-60 | |
| LP 61-70 | | | | | | | | | | | | | | | | | | LP 61-70 | |
| LP 71-80 | | | | | | | | | | | | | | | | | | LP 71-80 | |
| LP 81-90 | | | | | | | | | | | | | | | | | | LP 81-90 | |
| LP 91-100 | | | | | | | | | | | | | | | | | | LP 91-100 | |

| ACTION PLAN | | 1 | | Π | | | | | | | | | | | | |
|----------------|----------|-------|---|----------|------|----|----------|----------|----------|------------|------|------|-----|---|---|---|
| PATTERN | | | | | | | SY | STEN | 1 OVE | ERRID | E | | | | | |
| VEHICLE DETECT | OR P | PI AN | | | | | DF | TFCT | ORI | OG | _ | | | | | |
| FLASH | • | | | | | | | | 0 | | | | | | | |
| RED REST | | | | | | | VF | HICL | E DE. | | NO | STIC | | N | | |
| CONTROLLER SE | OUE | NCE | | - | | | PF | | | GNOS | TIC | | N | · | | |
| TIMING PLAN | | | | | | | | | G FN | ABIF | | , . | | | | |
| PHASE | | 1 | 1 | | | 1 | | 1 | | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 |
| PED RECALL | | _ | - | | - | - | - | - | - | - | | _ | - | | - | - |
| WALK 2 | | | | | | | | | | | | | | | | |
| VEH EXT 2 | | | | | - | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| MAX NEOALL | | | | | _ | | | | | | | | | | | |
| MAX 2 | | | | | | | | | | | | | | | | |
| | | | | | _ | | | | | | | | | | | |
| | | | | | _ | | | | | | | | | | | |
| PHASE UMIT | | | | | _ | | | | | a) | | | | | | |
| SPEC | | | | | | | | | (1- | 8) | | | | | | |
| FUNCTION | | | | - | | | | | IJ | | | | | | | |
| AUX FUNCTION | | | | | (1- | 3) | | | | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | | | | | |
| LP 1-10 | | | | | | | | | | | | | | | | |
| LP 11-20 | | | | | | | | | | | | | | | | |
| LP 21-30 | | | | | | | | | | | | | | | | |
| LP 31-40 | | | | | | | | | | | | | | | | |
| LP 41-50 | | | | | | | | | | | | | | | | |
| LP 51-60 | | | | | | | | | | | | | | | | |
| LP 61-70 | | | | | | | | | | | | | | | | |
| LP 71-80 | | | | | | | | | | | | | | | | |
| LP 81-90 | | | | | | | | | | | | | | | | |
| LP 91-100 | | | | | | | | | | | | | | | | |
| VEHICLE DETECT | 'OR P | PLAN | | | | | DE | TECT | 'OR L | .0G | | | | | | |
| FLASH | | | | | | | | | | | | | | | | |
| RED REST | | | | | | | VE | HICLI | E DE | T DIAG | ino | STIC | PLA | N | | |
| CONTROLLER SE | QUEI | NCE | | | | | PE | D DE | T DIA | GNOS | STIC | PLA | N | | | |
| | 1 | T | T | | - | r | DIN | /MIN | G EN | ABLE | | | | | | |
| PHASE | | 0 | 2 | | F | ~ | 7 | | _ | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| | | 2 | 3 | 4 | 5 | 0 | 1 | 0 | 9 | U | - | 2 | 3 | 4 | 5 | 0 |
| | | | | | _ | | | | | | | | | | | |
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| | | | | | _ | | | | | | | | | | | |
| | | | | | _ | | | | | | | | | | | |
| | | | | | _ | | | | | | | | | | | |
| MAX 2 | | | | | _ | | | | | | | | | | | |
| MAX 3 | | | | | | | | | | | | | | | | |
| | | | | | _ | | | | | | | | | | | |
| PHASE OMIT | | | | | _ | | | | | | | | | | | |
| SPEC | | | | | | | | | (1- | 8) | | | | | | |
| FUNCTION | | | | - | | | | | IJ | | | | | | | |
| AUX FUNCTION | | _ | _ | <u> </u> | (1-; | 3) | I - | - | - | | | | | | | |
| 1.5.4.40 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | | | | | | |
| LP 1-10 | | | | _ | + | | | <u> </u> | <u> </u> | | | | | | | |
| LP 11-20 | | | | _ | + | | | <u> </u> | <u> </u> | | | | | | | |
| LP 21-30 | | | | L | | | | L | L | | | | | | | |
| LP 31-40 | | | | | | | | | | <u> </u> | | | | | | |
| LP 41-50 | | | | | | | <u> </u> | | | | | | | | | |
| LP 51-60 | | | | _ | | | | ļ | ļ | | | | | | | |
| LP 61-70 | | | | <u> </u> | | | | | | ļ | | | | | | |
| LP 71-80 | | | | | | | | | | I | | | | | | |
| LP 81-90 | | | | <u> </u> | | | | | | ļ | | | | | | |
| LP 91-100 | <u> </u> | | | L | | | L | | | I | | | | | | |
| | | | | | | | | | | | | | | | | |

LP 1-10 LP 11-20 LP 21-30 LP 31-40 LP 41-50 LP 51-60 LP 61-70 LP 71-80 LP 81-90 LP 91-100

5-5 EXCEPTION DAY PROGRAM

| EXECEPTION DAY | FLOAT / FIXED | MON / MON | DOW / DOM | WOM / YEAR | DAY PLAN |
|-------------------|------------------|-----------|-----------|---------------|----------|
| 1 | | | | | |
| 2 | | | | | |
| 3 | | | | | |
| 4 | | | | | |
| 5 | | | | | |
| 6 | | | | | |
| 7 | | | | | |
| 8 | | | | | |
| 9 | | | | | |
| 10 | | | | | |
| 11 | | | | | |
| 12 | | | | | |
| 13 | | | | | |
| 14 | | | | | |
| 15 | | | | | |
| 16 | | | | | |
| 17 | | | | | |
| 18 | | | | | |
| 19 | | | | | |
| 20 | | | | | |
| 21 | | | | | |
| 22 | | | | | |
| 23 | | | | | |
| 24 | | | | | |
| 25 | | | | | |
| 26 | | | | | |
| 27 | | | | | |
| 28 | | | | | |
| 29 | | | | | |
| 30 | | | | | |
| 31 | | | | | |
| 32 | | | | | |
| 33 | | | | | |
| 34 | | | | | |
| 35 | | | | | |
| 36 | | | | | |

DETECTORS

6-1. DETECTOR TYPE AND TS SELECT

| DET | TYPE | TS1 DETECTOR | D | ET | TYPE | TS1 DETECTOR |
|-----|------|--------------|----|----|------|--------------|
| 1 | | | 33 | 3 | | |
| 2 | | | 34 | 1 | | |
| 3 | | | 35 | 5 | | |
| 4 | | | 36 | 6 | | |
| 5 | | | 3 | 7 | | |
| 6 | | | 38 | 3 | | |
| 7 | | | 39 | 9 | | |
| 8 | | | 40 |) | | |
| 9 | | | 4 | | | |
| 10 | | | 42 | 2 | | |
| 11 | | | 43 | 3 | | |
| 12 | | | 44 | 1 | | |
| 13 | | | 4 | 5 | | |
| 14 | | | 46 | 6 | | |
| 15 | | | 4 | 7 | | |
| 16 | | | 48 | 3 | | |
| 17 | | | 49 |) | | |
| 18 | | | 50 |) | | |
| 19 | | | 5 | | | |
| 20 | | | 52 | 2 | | |
| 21 | | | 53 | 3 | | |
| 22 | | | 54 | 1 | | |
| 23 | | | 55 | 5 | | |
| 24 | | | 56 | 6 | | |
| 25 | | | 5 | 7 | | |
| 26 | | | 58 | 3 | | |
| 27 | | | 59 | 9 | | |
| 28 | | | 60 |) | | |
| 29 | | | 6 | | | |
| 30 | | | 62 | 2 | | |
| 31 | | | 63 | 3 | | |
| 32 | | | 64 | 1 | | |

| VEHICLE F | PLAN | NUM | BER | | | | | | | | | | | | | |
|-----------|--------|------|-----|---|---|---|---|----|-------|--------|--------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | } | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | ll de | TECT | OR O | PTION | ١ | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECTO | DR OF | TION | | | |
| DELAY TIM | ЛE | | | | | | | QU | EUE [| DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | MIT | | | | | | | NT | CIP O | CCUF | ANC | LOG | | | | |
| FAIL TIME | | | | | | | | NT | CIP V | OLUM | IE LOO | 3 | | | | |
| FAIL CALL | . DEL/ | AY | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOC | CK | | | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE I | PLAN | NUM | BER | | | | |] | | | | | | | | |
|-----------|--------|------|-----|---|---|---|---|----|-------|--------|-------------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | } | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | ll de | TECT | OR O | PTIOI | N | | | |
| EXTEND 1 | IME | | | | | | | PA | SSAG | E DE | TECT | or of | PTION | | | |
| DELAY TI | ЛE | | | | | | | QU | EUE I | DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | MIT | | | | | | | NT | CIP O | CCUF | ANC | / LOG | l | | | |
| FAIL TIME | | | | | | | | NT | CIP V | OLUM | IE LO | G | | | | |
| FAIL CALL | . DEL/ | AY | | | | | | EC | PI LO | G | | | | | | |
| YELLOW I | .OCK | | | | | | | RE | D LOO | CK | | | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE F | PLAN | NUM | BER | | | | | | | | | | | | | |
|-----------|--------|------|-----|---|---|---|---|----|-------|--------|--------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | } | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | ll de | TECT | OR O | PTIOI | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECTO | or of | PTION | | | |
| DELAY TIM | | | | | | | | QU | EUE [| DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | | | | | | | | NT | CIP O | CCUF | ANC | / LOG | i | | | |
| FAIL TIME | | | | | | | | NT | CIP V | OLUM | IE LO | G | | | | |
| FAIL CALL | . DEL/ | ٩Y | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | OCK | | | | | | | RE | D LOC | CK | | | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

6-2 VEHICLE DETECTOR SETUP

| VEHICLE I | PLAN | NUM | BER | | | | | | | | | | | | | |
|-----------|------------|------|-----|---|---|---|---|----|-------|--------|--------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | 1 | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | LL DE | TECT | OR O | PTIO | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECT | or of | PTION | | | |
| DELAY TI | | | | | | | | QU | EUE [| DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | JEUE LIMIT | | | | | | | NT | CIP O | CCUF | ANC | / LOG | i | | | |
| FAIL TIME | | | | | | | | NT | CIP V | OLUM | IE LO | G | | | | |
| FAIL CALL | . DEL/ | ٩Y | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOC | CK | | | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE | PLAN OR NU | I NUN JMBE | iber R | | | | | | | | | | | | | |
|----------|-----------------|---------------|-----------|--|--|--|---|----|-------|--------|--------|--------|--------|--------|--------|--------|
| ASSIGNE | DPH | ASE | | | | | | AD | DED I | NITIA | L OPT | ION | | | I | |
| SWITCH | PHAS | E | | | | | | CA | LL DE | TECT | OR O | PTION | I | | | |
| EXTEND | TIME | | | | | | | PA | SSAG | E DET | TECTO |)r of | TION | | | |
| DELAY T | | | | | | | | QU | EUE [| DETE | CTOR | OPTI | NC | | | |
| QUEUE L | QUEUE LIMIT | | | | | | | NT | CIP O | CCUF | ANCY | ' LOG | | | | |
| FAIL TIM | FAIL TIME | | | | | | | NT | CIP V | OLUM | E LOC | à | | | | |
| FAIL CAL | L DEL | AY. | | | | | | EC | PI LO | G | | | | | | |
| YELLOW | LOCK | (| | | | | | RE | D LOC | Ж | | | | | | |
| PHASE | PHASE 1 2 3 4 5 | | | | | | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE I | PLAN | NUM | BER | | | | | 1 | | | | | | |
|-----------|--------|------|-----|---|---|---|---|----|-------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | { | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | |
| SWITCH P | HASE | | | | | | | CA | ll de | TECT | OR O | PTIOI | N | |
| EXTEND 1 | IME | | | | | | | PA | SSAG | E DE1 | TECT(| or of | PTION | |
| DELAY TI | ΛE | | | | | | | QU | EUE [| DETEC | CTOR | OPTI | ON | |
| QUEUE LI | MIT | | | | | | | NT | CIP O | CCUP | ANC | / LOG | i | |
| FAIL TIME | | | | | | | | NT | CIP V | OLUM | E LO | G | | |
| FAIL CALL | . DEL/ | AY | | | | | | EC | PI LO | G | | | | |
| YELLOW L | OCK | | | | | | | RE | D LOC | CK | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 |
| CALLED | | | | | | | | | | | | | | |

1 1 5 6

| VEHICLE I | PLAN | NUM | BER | | | | |] | | | | | | | | |
|-----------|-----------------|------|-----|--|--|--|---|----|-------|--------|-------------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | 1 | | | | | | | | | | | | | |
| ASSIGNED | PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | LL DE | TECT | OR O | PTIOI | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DET | TECT | or of | PTION | | | |
| DELAY TIM | | | | | | | | QU | EUE I | DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | QUEUE LIMIT | | | | | | | NT | CIP O | CCUP | ANC | / LOG | i | | | |
| FAIL TIME | FAIL TIME | | | | | | | NT | CIP V | OLUM | E LO | G | | | | |
| FAIL CALL | DEL/ | ٩Y | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOO | CK | | | | | | |
| PHASE | PHASE 1 2 3 4 5 | | | | | | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE F | PLAN | NUM | BER | | | | | 1 | | | | | | | | |
|-----------|--------|------|-----|---|---|---|---|----|-------|--------|--------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | } | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | ll de | TECT | OR 0 | PTIOI | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECTO | or of | PTION | | | |
| DELAY TIM | ЛE | | | | | | | QU | EUE [| DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | | | | | | | | NT | CIP O | CCUF | ANC | / LOG | i | | | |
| FAIL TIME | | | | | | | | NT | CIP V | OLUM | E LO | G | | | | |
| FAIL CALL | . DEL/ | AY | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOO | CK | | | | | | |
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE I | PLAN | NUM | BER | | | | | 1 | | | | | | | | |
|-----------|--------------------------|------|-----|--|--|--|---|----|--------|--------|-------------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | 1 | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | LL DE | TECT | OR O | PTIO | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DET | TECT | or of | PTION | | | |
| DELAY TIM | | | | | | | | QU | IEUE I | DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | | | | | | | | NT | CIP O | CCUP | ANC | LOG | | | | |
| FAIL TIME | GUEUE LIMIT FAIL TIME | | | | | | | NT | CIP V | OLUM | E LO | 3 | | | | |
| FAIL CALL | . DEL/ | ٩Y | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOO | Ж | | | | | | |
| PHASE | HASE 1 2 3 4 5 | | | | | | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE I | PLAN | NUM | BER | | | | | | | | | | | | | |
|-----------|---------------|------|-----|--|--|--|--|----|-------|--------|--------|--------|--------|--------|--------|--------|
| DETECTO | K NU | MBFH | | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | LL DE | TECT | OR O | PTIO | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECTO | or of | PTION | | | |
| DELAY TIN | DELAY TIME | | | | | | | QU | EUE [| DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | | | | | | | | NT | CIP O | CCUF | ANC | / LOG | | | | |
| FAIL TIME | FAIL TIME | | | | | | | NT | CIP V | OLUM | IE LO | G | | | | |
| FAIL CALL | DEL | ٩Y | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOC | CK | | | | | | |
| PHASE | PHASE 1 2 3 4 | | | | | | | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE I | | | BER | | | | | 1 | | | | | | | | |
|-----------|--------------------------|------|-----|--|--|--|---|----|-------|--------|--------|--------|--------|--------|--------|--------|
| DETECTO | RINU | NBEF | { | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | LL DE | TECT | OR O | PTIO | ٧ | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECT | DR OF | PTION | | | |
| DELAY TIM | | | | | | | | QU | EUE [| DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | | | | | | | | NT | CIP O | CCUF | ANC | LOG | | | | |
| FAIL TIME | QUEUE LIMIT FAIL TIME | | | | | | | NT | CIP V | OLUM | E LO | 3 | | | | |
| FAIL CALL | . DEL/ | ٩Y | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOC | Ж | | | | | | |
| PHASE | 2HASE 1 2 3 4 5 | | | | | | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE I | PLAN | NUM | BER | | | | |] | | | | | | | | |
|-----------|--------------------------|------|-----|--|--|--|--|----|-------|--------|--------|--------|--------|--------|--------|--------|
| DETECTO | r nu | MBEF | } | | | | | | | | | | | | | |
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | ll de | TECT | OR O | PTIOI | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECTO | or of | PTION | | | |
| DELAY TIM | DELAY TIME | | | | | | | QU | EUE [| DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | | | | | | | | NT | CIP O | CCUF | ANC | / LOG | i | | | |
| FAIL TIME | QUEUE LIMIT FAIL TIME | | | | | | | NT | CIP V | OLUM | IE LO | G | | | | |
| FAIL CALL | DEL/ | ٩Y | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOC | CK | | | | | | |
| PHASE | PHASE 1 2 3 4 | | | | | | | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE I | PLAN R NU | NUM MBEF | BER } | | | | | | | | | | | | | |
|-----------|---------------|-------------|----------|--|--|--|--|----|-------|--------|--------|--------|--------|--------|--------|--------|
| ASSIGNED |) PHA | SE | <u> </u> | | | | | AD | DED I | NITIA | L OPT | ION | | | T | |
| SWITCH P | HASE | | | | | | | CA | LL DE | TECT | OR O | PTIOI | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECT | or of | PTION | | | |
| DELAY TIM | | | | | | | | QU | EUE I | DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | QUEUE LIMIT | | | | | | | NT | CIP O | CCUF | ANC | LOG | i | | | |
| FAIL TIME | FAIL TIME | | | | | | | NT | CIP V | OLUM | IE LO | 3 | | | | |
| FAIL CALL | . DEL/ | AY | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | .OCK | | | | | | | RE | D LOO | CK | | | | | | |
| PHASE | PHASE 1 2 3 4 | | | | | | | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

| VEHICLE F | ²LAN R NU | NUME MBEF | 3ER { | | | | | | | | | | | | | |
|-----------|---------------|--------------|----------|--|--|--|--|----|-------|--------|--------|--------|--------|--------|--------|--------|
| ASSIGNED |) PHA | SE | | | | | | AD | DED I | NITIA | L OPT | ION | | | | |
| SWITCH P | HASE | | | | | | | CA | LL DE | TECT | OR O | PTIOI | N | | | |
| EXTEND T | IME | | | | | | | PA | SSAG | E DE | TECTO | OR OF | PTION | | | |
| DELAY TIN | DELAY TIME | | | | | | | QU | EUE [| DETE | CTOR | OPTI | ON | | | |
| QUEUE LI | QUEUE LIMIT | | | | | | | NT | CIP O | CCUF | ANC | / LOG | i | | | |
| FAIL TIME | FAIL TIME | | | | | | | NT | CIP V | OLUM | E LO | G | | | | |
| FAIL CALL | DEL/ | AY | | | | | | EC | PI LO | G | | | | | | |
| YELLOW L | OCK | | | | | | | RE | D LOO | CK | | | | | | |
| PHASE | PHASE 1 2 3 4 | | | | | | | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| CALLED | | | | | | | | | | | | | | | | |

6-3 PHASE DETECTOR OPTIONS

| PHASE DETECTO | r op | TION | PLA | N NU | MBE | 2 | 1 | | | | | | | | | |
|------------------|------|------|-----|------|-----|---|---|---|---|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| DETECTOR LOCK | | | | | | | | | | | | | | | | |
| VEH RECALL | | | | | | | | | | | | | | | | |
| PED RECALL | | | | | | | | | | | | | | | | |
| MAX RECALL | | | | | | | | | | | | | | | | |
| SOFT RECALL | | | | | | | | | | | | | | | | |
| NO REST | | | | | | | | | | | | | | | | |
| ADD INIT CALC | | | | | | | | | | | | | | | | |

| PHASE DETECTO | r op | TION | PLA | N NU | MBEF | r | 2 | | | | | | | | | |
|------------------|------|------|-----|------|------|---|---|---|---|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| DETECTOR LOCK | | | | | | | | | | | | | | | | |
| VEH RECALL | | | | | | | | | | | | | | | | |
| PED RECALL | | | | | | | | | | | | | | | | |
| MAX RECALL | | | | | | | | | | | | | | | | |
| SOFT RECALL | | | | | | | | | | | | | | | | |
| NO REST | | | | | | | | | | | | | | | | |
| ADD INIT CALC | | | | | | | | | | | | | | | | |

| PHASE DETECTO | r op | TION | PLA | N NU | MBE | 3 | 3 | | | | | | | | | |
|------------------|------|------|-----|------|-----|---|---|---|---|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| DETECTOR LOCK | | | | | | | | | | | | | | | | |
| VEH RECALL | | | | | | | | | | | | | | | | |
| PED RECALL | | | | | | | | | | | | | | | | |
| MAX RECALL | | | | | | | | | | | | | | | | |
| SOFT RECALL | | | | | | | | | | | | | | | | |
| NO REST | | | | | | | | | | | | | | | | |
| ADD INIT CALC | | | | | | | | | | | | | | | | |

| PHASE DETECTOR | R OP | TION | PLA | N NU | MBE | 7 | 4 | | | | | | | | | |
|------------------|------|------|-----|------|-----|---|---|---|---|--------|--------|--------|--------|--------|--------|--------|
| PHASE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 1 0 | 1 1 | 1 2 | 1 3 | 1 4 | 1 5 | 1 6 |
| DETECTOR LOCK | | | | | | | | | | | | | | | | |
| VEH RECALL | | | | | | | | | | | | | | | | |
| PED RECALL | | | | | | | | | | | | | | | | |
| MAX RECALL | | | | | | | | | | | | | | | | |
| SOFT RECALL | | | | | | | | | | | | | | | | |
| NO REST | | | | | | | | | | | | | | | | |
| ADD INIT CALC | | | | | | | | | | | | | | | | |

6-4 PEDESTRIAN AND SYSTEM DETECTOR OPTIONS

| | PHASE I | PEDESTRI | AN DETEC | CTOR | | | | |
|---------------|----------|----------|----------|------|---------|---------|---------|----|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| PED DET INPUT | | | | | | | | |
| | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| PED DET INPUT | | | | | | | | |
| | LOCALS | SVSTEM D | ETECTOR |) | | | | |
| | 200/12 0 | | | | | | | |
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| VEH DET INPUT | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| VEH DET INPUT | 9 | 2 10 | 3 | 4 | 5 13 | 6 14 | 7 15 | 8 |

6-5 LOG – SPEED DETECTOR SET UP

| NTCIP LOG PERIOD | | | | | | | | | |
|-------------------|---|----|----|----|----|----|----|----|--|
| ECPI LOG PERIOD |) | | | | | | | | |
| LENGTH UNIT | | | | | | | | | |
| SPEED DETECTOR | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | |
| LOCAL DETECTOR | | | | | | | | | |
| ONE / TWO DET | | | | | | | | | |
| VEH LENGTH | | | | | | | | | |
| TRAP LENGTH | | | | | | | | | |
| ENABLE LOG | | | | | | | | | |
| SPEED DETECTOR | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | |
| LOCAL DETECTOR | | | | | | | | | |
| ONE / TWO DET | | | | | | | | | |
| VEH LENGTH | | | | | | | | | |
| TRAP LENGTH | | | | | | | | | |
| ENABLE LOG | | | | | | | | | |

6-6 VEHICLE DETECTOR DIAGNOSTICS

| VEHICL | VEHICLE DIAGNOSTIC PLAN NUMBER | | | BER | 1 | | | | | |
|--------|--------------------------------|------------|----------|------------|---|----------|--------|------------|----------|------------|
| DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER | | DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER |
| 1 | | | | | | 33 | | | | |
| 2 | | | | | | 34 | | | | |
| 3 | | | | | | 35 | | | | |
| 4 | | | | | | 36 | | | | |
| 5 | | | | | | 37 | | | | |
| 6 | | | | | | 38 | | | | |
| 7 | | | | | | 39 | | | | |
| 8 | | | | | | 40 | | | | |
| 9 | | | | | | 41 | | | | |
| 10 | | | | | | 42 | | | | |
| 11 | | | | | | 43 | | | | |
| 12 | | | | | | 44 | | | | |
| 13 | | | | | | 45 | | | | |
| 14 | | | | | | 46 | | | | |
| 15 | | | | | | 47 | | | | |
| 10 | | | | | | 48 | | | | |
| 10 | | | | | | 49 50 | | | | |
| 10 | | | | | | 50 | | | | |
| 20 | | | | | | 52 | | | | |
| 21 | | | | | | 53 | | | | |
| 22 | | | | | | 54 | | | | |
| 23 | | | | | | 55 | | | | |
| 24 | | | | | | 56 | | | | |
| 25 | | | | | | 57 | 1 | | | |
| 26 | | | | | | 58 | 1 | | | |
| 27 | | | | | | 59 | 1 | | | |
| 28 | | | 1 | | | 60 | Î | | | |
| 29 | | | | | | 61 | 1 | | | |
| 30 | | | | | | 62 | 1 | | | |
| 31 | | | | | | 63 | 1 | | | |
| 32 | | | | | | 64 | 1 | | | |

| VEHICL | E DIAGN | OSTIC PI | AN NUM | BER | 2 | | | | | |
|--------|---------|------------|----------|------------|---|-----|--------|------------|----------|------------|
| DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER | | DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER |
| 1 | | | | | | 33 | _ | | | _ |
| 2 | | | | | | 34 | | | | |
| 3 | | | | | | 35 | | | | |
| 4 | | | | | | 36 | | | | |
| 5 | | | | | | 37 | | | | |
| 6 | | | | | | 38 | | | | |
| / | | | | | | 39 | | | | |
| 0 | | | | | | 40 | | | | |
| 9 | | | | | | 41 | | | | |
| 10 | | | | | | 42 | | | | |
| 12 | | | | | | 44 | | | | |
| 13 | | | | | | 45 | | | | |
| 14 | | | | | | 46 | | | | |
| 15 | | | | | | 47 | | | | |
| 16 | | | | | | 48 | | | | |
| 17 | | | | | | 49 | | | | |
| 18 | | | | | | 50 | | | | |
| 19 | | | | | | 51 | | | | |
| 20 | | | | | | 52 | | | | |
| 21 | | | | | | 53 | | | | |
| 22 | | | | | | 54 | | | | |
| 23 | | | | | | 55 | | | | |
| 24 | | | | | | 56 | | | | |
| 25 | | | | | | 5/ | | | | |
| 26 | | | | | | 58 | | | | |
| 2/ | | | | | | 59 | | | | |
| 28 | | | | | | 61 | | | | |
| 29 | | | | | | 62 | | | | |
| 30 | | | | | | 63 | | | | |
| 32 | | | | | | 64 | | | | |
| 52 | | | | | | 04 | | | | |

6-6 VEHICLE DETECTOR DIAGNOSTICS (CONTINUED)

| VEHICL | .E DIAGN | OSTIC PI | LAN NUM | BER | 3 | | | | | |
|--------|----------|------------|----------|------------|---|----------|--------|------------|----------|------------|
| | | | | | | | | | | |
| DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER | | DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER |
| 1 | | | | | | 33 | | | | |
| 2 | | | | | | 34 | | | | |
| 3 | | | | | | 35 | | | | |
| 4 | | | | | | 36 | | | | |
| 5 | | | | | | 37 | | | | |
| 6 | | | | | | 38 | | | | |
| 7 | | | | | | 39 | | | | |
| 8 | | | | | | 40 | | | | |
| 9 | | | | | | 41 | | | | |
| 10 | | | | | | 42 | | | | |
| 11 | | | | | | 43 | | | | |
| 12 | | | | | | 44 | | | | |
| 13 | | | | | | 45 | | | | |
| 14 | | | | | | 46 | | | | |
| 15 | | | | | | 4/ | | | | |
| 16 | | | | | | 48 | | | | |
| 1/ | | | | | | 49 | | | | |
| 18 | | | | | | 50 | | | | |
| 19 | | | | | | 51 | | | | |
| 20 | | | | | | 52 | | | | |
| 21 | | | | | | 53 | | | | |
| 22 | | | | | | 54 | | | | |
| 23 | | | | | | 55 | | | | |
| 24 | | | | | | 00 57 | | | | |
| 20 | | | <u> </u> | | | 5/ | I | | <u> </u> | |
| 20 | | | | | | 50 50 | | | | |
| 2/ | | | | | | 09 60 | | | | |
| 20 | | | | | | 61 | | | | |
| 29 | | | | | | 62 | | | | |
| 30 | | | | | | 62 | ł | <u> </u> | | |
| 31 | | | | | | 03 64 | | | | |
| 32 | | | | | 1 | 04 | 1 | | | |

| VEHICL | VEHICLE DIAGNOSTIC PLAN NUMBE | | | | | | | | | |
|--------|-------------------------------|------------|----------|------------|---|-----|--------|------------|----------|------------|
| | | | | | | | | | | |
| DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER | | DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER |
| 1 | | | | | | 33 | | | | |
| 2 | | | | | | 34 | | | | |
| 3 | | | | | | 35 | | | | |
| 4 | | | | | | 36 | | | | |
| 5 | | | | | | 3/ | | | | |
| 7 | | | | | | 30 | | | | |
| 8 | | | | | | 40 | | | | |
| 9 | | | | | | 41 | | | | |
| 10 | | | | | | 42 | | | | |
| 11 | | | | | | 43 | | | | |
| 12 | | | | | | 44 | | | | |
| 13 | | | | | | 45 | | | | |
| 14 | | | | | | 46 | | | | |
| 15 | | | | | | 47 | | | | |
| 16 | | | | | | 48 | | | | |
| 17 | | | | | | 49 | | | | |
| 18 | | | | | | 50 | | | | |
| 19 | | | | | | 51 | | | | |
| 20 | | | | | | 53 | | | | |
| 22 | | | | | | 54 | | | | |
| 23 | | | | | | 55 | | | | |
| 24 | | | | | | 56 | | | | |
| 25 | | | | | | 57 | | | | |
| 26 | | | | | | 58 | | | | |
| 27 | | | | | | 59 | | | | |
| 28 | | | | | | 60 | | | | |
| 29 | | | | | | 61 | | | | |
| 30 | | | | | | 62 | | | | |
| 31 | | | | | | 63 | | | | |
| 32 | | | | | 1 | 64 | | | | |

6-7 PEDESTRIAN DETECTOR DIAGNOSTICS

| PED DIA | AGNOSTIC |) PLAN NU | IMBER | 1 | PED D NUMB | IAGNOST ER | IC PLAN | | 2 |
|---------|----------|------------|----------|------------|---------------|---------------|------------|----------|------------|
| DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER | DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER |
| 1 | | | | | 1 | | | | |
| 2 | | | | | 2 | | | | |
| 3 | | | | | 3 | | | | |
| 4 | | | | | 4 | | | | |
| 5 | | | | | 5 | | | | |
| 6 | | | | | 6 | | | | |
| / | | | | | / | | | | |
| 0 | | | | | 0 | | | | |
| 10 | | | | | 10 | | | | |
| 11 | | | | | 11 | | | | |
| 12 | | | | | 12 | | | | |
| 13 | | | | | 13 | | | | |
| 14 | | | | | 14 | | | | |
| 15 | | | | | 15 | | | | |
| 16 | | | | | 16 | | | | |

| PED DIA | AGNOSTIC |) PLAN NU | JMBER | 3 | PED D NUMB |)IAGNOST ER | TIC PLAN | | 4 |
|---------|----------|------------|----------|------------|---------------|----------------|------------|----------|------------|
| DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER | DET | COUNTS | ACTUATIONS | PRESENCE | MULTIPLIER |
| 1 | | | | | 1 | | | | |
| 2 | | | | | 2 | | | | |
| 3 | | | | | 3 | | | | |
| 4 | | | | | 4 | | | | |
| 6 | | | | | 6 | | | | |
| 7 | | | | | 7 | | | | |
| 8 | | | | | 8 | | | | |
| 9 | | | | | 9 | | | | |
| 10 | | | | | 10 | | | | |
| 11 | | | | | 11 | | | | |
| 12 | | | | | 12 | | | | |
| 13 | | | | | 13 | | | | |
| 14 | | | | | 14 | | | | |
| 16 | | | | | 16 | | | | |

(This page left intentionally blank.)



HV% Calculations





2%(2%) 2%(2%) 2%(2%) 2%(2%)

2%(2%)

3%(2%)

2%(2%)

2%(2%) 2%(2%)

2%(2%)

2%(2%)

4%(2%)

Appendix F

2022 Existing Synchro Intersection Worksheets



Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٠ | - | 7 | 1 | + | • | 1 | Ť | 1 | 4 | ţ | ~ |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | *** | 1 | 5 | *** | 1 | 5 | 44 | 1 | 5 | ** | 1 |
| Traffic Volume (vph) | 171 | 2055 | 258 | 173 | 961 | 129 | 147 | 315 | 167 | 239 | 574 | 149 |
| Future Volume (vph) | 171 | 2055 | 258 | 173 | 961 | 129 | 147 | 315 | 167 | 239 | 574 | 149 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd, Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.188 | | | 0.065 | | | 0.171 | | | 0.402 | | |
| Satd. Flow (perm) | 339 | 5085 | 1491 | 113 | 4715 | 1449 | 276 | 3433 | 1422 | 692 | 3466 | 1478 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd, Flow (RTOR) | | | 180 | | | 145 | | | 188 | | | 167 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 329.1 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 19.7 | | | 11.3 | | | 5.7 | |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 192 | 2309 | 290 | 194 | 1080 | 145 | 165 | 354 | 188 | 269 | 645 | 167 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 192 | 2309 | 290 | 194 | 1080 | 145 | 165 | 354 | 188 | 269 | 645 | 167 |
| Enter Blocked Intersection | No |
| Lane Alignment | Left | Left | Right |
| Median Width(m) | | 3.3 | Ŭ | | 3.3 | Ŭ | | 3.0 | Ŭ | | 3.0 | Ŭ |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | CI+Ex | Cl+Ex | Cl+Ex | CI+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | Cl+Ex | | | CI+Ex | | | CI+Ex | | | Cl+Ex | |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |

07-24-2023

Lanes, Volumes, Timings 1: Ninth Line & Dundas Street East

| | ٦ | → | 7 | 4 | + | * | 1 | t | 1 | 1 | ŧ | ~ |
|------------------------------|-------------|-----------|---------|---------------|------------|-------|-------|-------|-------|--------------------|-----------|-----------------------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 | 7.0 | 10.0 | 10.0 | 7.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 52.9 | 52.9 | 11.0 | 52.9 | 52.9 | 11.0 | 56.0 | 56.0 | 11.0 | 56.0 | 56.0 |
| Total Split (s) | 20.0 | 60.0 | 60.0 | 20.0 | 60.0 | 60.0 | 20.0 | 40.0 | 40.0 | 20.0 | 40.0 | 40.0 |
| Total Split (%) | 14.3% | 42.9% | 42.9% | 14.3% | 42.9% | 42.9% | 14.3% | 28.6% | 28.6% | 14.3% | 28.6% | 28.6% |
| Maximum Green (s) | 16.0 | 53.1 | 53.1 | 16.0 | 53.1 | 53.1 | 16.0 | 33.0 | 33.0 | 16.0 | 33.0 | 33.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.7 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 3.3 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | 15.0 | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | 34.0 | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Act Effct Green (s) | 79.8 | 59.7 | 59.7 | 82.2 | 61.4 | 61.4 | 53.4 | 31.5 | 31.5 | 54.9 | 32.6 | 32.6 |
| Actuated g/C Ratio | 0.57 | 0 43 | 0 43 | 0.59 | 0 44 | 0 44 | 0.38 | 0.22 | 0.22 | 0.39 | 0.23 | 0.23 |
| v/c Ratio | 0.55 | 1.06 | 0.39 | 0.74 | 0.52 | 0.20 | 0.62 | 0.46 | 0.40 | 0.67 | 0.80 | 0.35 |
| Control Delay | 20.3 | 78.0 | 12.6 | 50.9 | 30.8 | 4 7 | 38.6 | 48.3 | 8.2 | 39.3 | 58.7 | 8.0 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 20.3 | 78.0 | 12.6 | 50.9 | 30.8 | 4 7 | 38.6 | 48.3 | 8.2 | 39.3 | 58.7 | 8.0 |
| | C | F | B | D | C | Δ | D | D | Δ | D | F | 0.0 A |
| Approach Delay | Ű | 67 2 | U | Ľ | 30.9 | 7. | 5 | 35.4 | 71 | U | 46 0 | 71 |
| Approach LOS | | F | | | C.00 | | | D | | | 10.0 D | |
| Oueue Length 50th (m) | 22.8 | ~253 9 | 18.4 | 33.9 | 75.6 | 0.0 | 27.3 | 40.3 | 0.0 | <u>47</u> <u>4</u> | 80.8 | 0.0 |
| Queue Length 95th (m) | 34.9 | #273.8 | 39.4 | #61.4 | 91.0 | 11.8 | 41.0 | 53.1 | 16.5 | 67.6 | 99.1 | 15.0 |
| Internal Link Dist (m) | 04.0 | 269.2 | 55.4 | <i>m</i> 01.4 | 305.1 | 11.0 | +1.5 | 164.2 | 10.0 | 07.0 | 71.5 | 10.0 |
| Turn Bay Length (m) | 220.0 | 205.2 | 80.0 | 230.0 | 000.1 | 80.0 | 130.0 | 104.2 | 130.0 | 130.0 | 71.5 | 70.0 |
| Rase Canacity (vnh) | 220.0 | 2160 | 730 | 230.0 | 2067 | 716 | 277 | 858 | /06 | 300 | 866 | 10.0 |
| Starvation Can Reductn | -00 0 | 2103 | 100 | 270 | 2007 | 0 1 | 211 | 0.00 | 430 | 000 | 000 | + 5 + 0 |
| Stallback Can Reductin | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductin | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| | 0 50 | 1.06 | 0.30 | 0 70 | 0.52 | 0 20 | 0 60 | 0 / 1 | 0.38 | 0.67 | 0.74 | 0.34 |
| | 0.50 | 1.00 | 0.59 | 0.70 | 0.52 | 0.20 | 0.00 | 0.41 | 0.50 | 0.07 | 0.74 | 0.34 |
| Intersection Summary | <u></u> | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 140 | | | | | | | | | | | | |
| Actuated Cycle Length: 140 |) | _ | | | | | | | | | | |
| Otfset: 100 (71%), Reference | ced to phas | se 2:EBTL | and 6:W | 'BTL, Sta | rt of Gree | n | | | | | | |
| Natural Cycle: 155 | | | | | | | | | | | | |
| Control Type: Actuated-Coc | ordinated | | | | | | | | | | | |

Maximum v/c Ratio: 1.06 Intersection Signal Delay: 51.1

Intersection LOS: D

Intersection Capacity Utilization 88.3%

ICU Level of Service E

Analysis Period (min) 15

- Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

| Splits and Phases: | 1: Ninth Line & Dundas Street East |
|--------------------|------------------------------------|
|--------------------|------------------------------------|

| Ø1 | ■ → Ø2 (R) | Ø3 | 1 Ø4 |
|---------|------------|-------------|-------------|
| 20 s | 60 s | 20 s | 40 s |
| ▶ Ø5 | ● | 1 Ø7 | Ø8 |
| 20 s | 60 s | 20 s | 40 s |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | 4 | • | • | 1 | Ť | 1 | 6 | ţ | ~ |
|--|-------|-----------|-------|-------|-----------|------------|---------|-----------|------|-------|-----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | *** | 1 | 5 | *** | 1 | 5 | ^ | 1 | 5 | ** | 1 |
| Traffic Volume (vph) | 171 | 2055 | 258 | 173 | 961 | 129 | 147 | 315 | 167 | 239 | 574 | 149 |
| Future Volume (vph) | 171 | 2055 | 258 | 173 | 961 | 129 | 147 | 315 | 167 | 239 | 574 | 149 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.19 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.17 | 1.00 | 1.00 | 0.40 | 1.00 | 1.00 |
| Satd. Flow (perm) | 339 | 5085 | 1491 | 112 | 4715 | 1449 | 275 | 3433 | 1422 | 693 | 3466 | 1478 |
| Peak-hour factor, PHF | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Adj. Flow (vph) | 192 | 2309 | 290 | 194 | 1080 | 145 | 165 | 354 | 188 | 269 | 645 | 167 |
| RTOR Reduction (vph) | 0 | 0 | 103 | 0 | 0 | 81 | 0 | 0 | 146 | 0 | 0 | 128 |
| Lane Group Flow (vph) | 192 | 2309 | 187 | 194 | 1080 | 64 | 165 | 354 | 42 | 269 | 645 | 39 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 70.9 | 57.8 | 57.8 | 74.3 | 59.5 | 59.5 | 44.4 | 29.5 | 29.5 | 46.6 | 30.6 | 30.6 |
| Effective Green, g (s) | 76.9 | 59.7 | 59.7 | 79.6 | 61.4 | 61.4 | 50.4 | 31.5 | 31.5 | 52.5 | 32.6 | 32.6 |
| Actuated g/C Ratio | 0.55 | 0.43 | 0.43 | 0.57 | 0.44 | 0.44 | 0.36 | 0.22 | 0.22 | 0.38 | 0.23 | 0.23 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 343 | 2168 | 635 | 258 | 2067 | 635 | 259 | 772 | 319 | 387 | 807 | 344 |
| v/s Ratio Prot | 0.06 | c0.45 | | c0.10 | 0.23 | | 0.08 | 0.10 | | c0.09 | c0.19 | |
| v/s Ratio Perm | 0.24 | | 0.13 | 0.33 | | 0.04 | 0.15 | | 0.03 | 0.17 | | 0.03 |
| v/c Ratio | 0.56 | 1.07 | 0.29 | 0.75 | 0.52 | 0.10 | 0.64 | 0.46 | 0.13 | 0.70 | 0.80 | 0.11 |
| Uniform Delay, d1 | 17.5 | 40.1 | 26.3 | 41.0 | 28.6 | 23.1 | 33.8 | 46.9 | 43.3 | 33.1 | 50.6 | 42.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 2.2 | 39.4 | 1.2 | 12.0 | 0.9 | 0.3 | 5.3 | 0.5 | 0.2 | 5.5 | 5.7 | 0.2 |
| Delay (s) | 19.7 | 79.5 | 27.5 | 53.0 | 29.6 | 23.4 | 39.1 | 47.4 | 43.6 | 38.6 | 56.3 | 42.5 |
| Level of Service | В | E | С | D | C | С | D | D | D | D | E | D |
| Approach Delay (s) Approach LOS | | 70.0 E | | | 32.1 C | | | 44.4 D | | | 49.8 D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 54.4 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capacity ratio 0.89 | | | 0.89 | | | | | | | | | |
| Actuated Cycle Length (s) 140.0 | | | | S | um of los | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utiliza | tion | | 88.3% | IC | CU Level | of Service | Э | | E | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM 6th Signalized Intersection Summary 1: Ninth Line & Dundas Street East

| | ٠ | → | 7 | 4 | + | • | 1 | Ť | 1 | 1 | ŧ | ~ |
|------------------------------|------|----------|------|------|------|-------|------|------|------|------|------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 3 | *** | 1 | 5 | *** | 1 | 5 | ** | 1 | 5 | ** | 1 |
| Traffic Volume (veh/h) | 171 | 2055 | 258 | 173 | 961 | 129 | 147 | 315 | 167 | 239 | 574 | 149 |
| Future Volume (veh/h) | 171 | 2055 | 258 | 173 | 961 | 129 | 147 | 315 | 167 | 239 | 574 | 149 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1856 | 1811 | 1752 | 1811 | 1682 | 1841 | 1739 | 1781 | 1856 | 1796 |
| Adj Flow Rate, veh/h | 192 | 2309 | 290 | 194 | 1080 | 145 | 165 | 354 | 188 | 269 | 645 | 167 |
| Peak Hour Factor | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 | 0.89 |
| Percent Heavy Veh, % | 2 | 2 | 3 | 6 | 10 | 6 | 10 | 4 | 6 | 3 | 3 | 2 |
| Cap, veh/h | 365 | 2326 | 705 | 251 | 2288 | 723 | 268 | 726 | 306 | 379 | 808 | 349 |
| Arrive On Green | 0.09 | 0.46 | 0.46 | 0.12 | 0.48 | 0.48 | 0.11 | 0.21 | 0.21 | 0.14 | 0.23 | 0.23 |
| Sat Flow, veh/h | 1781 | 5106 | 1547 | 1725 | 4782 | 1510 | 1602 | 3497 | 1473 | 1696 | 3526 | 1522 |
| Grp Volume(v), veh/h | 192 | 2309 | 290 | 194 | 1080 | 145 | 165 | 354 | 188 | 269 | 645 | 167 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1702 | 1547 | 1725 | 1594 | 1510 | 1602 | 1749 | 1473 | 1696 | 1763 | 1522 |
| Q Serve(g_s), s | 7.5 | 62.9 | 17.6 | 10.9 | 21.3 | 7.8 | 10.8 | 12.5 | 16.2 | 16.8 | 24.2 | 13.3 |
| Cycle Q Clear(g_c), s | 7.5 | 62.9 | 17.6 | 10.9 | 21.3 | 7.8 | 10.8 | 12.5 | 16.2 | 16.8 | 24.2 | 13.3 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 365 | 2326 | 705 | 251 | 2288 | 723 | 268 | 726 | 306 | 379 | 808 | 349 |
| V/C Ratio(X) | 0.53 | 0.99 | 0.41 | 0.77 | 0.47 | 0.20 | 0.61 | 0.49 | 0.61 | 0.71 | 0.80 | 0.48 |
| Avail Cap(c_a), veh/h | 442 | 2326 | 705 | 286 | 2288 | 723 | 303 | 874 | 368 | 379 | 881 | 380 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 17.7 | 37.9 | 25.5 | 42.8 | 24.6 | 21.1 | 37.6 | 48.9 | 50.4 | 34.8 | 50.9 | 46.7 |
| Incr Delay (d2), s/veh | 1.4 | 17.0 | 1.8 | 11.4 | 0.7 | 0.6 | 3.4 | 0.6 | 2.6 | 6.3 | 5.0 | 1.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 3.5 | 31.2 | 7.3 | 7.7 | 8.9 | 3.1 | 4.8 | 5.8 | 6.5 | 8.0 | 11.8 | 5.4 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 19.1 | 54.9 | 27.3 | 54.2 | 25.3 | 21.7 | 41.0 | 49.5 | 52.9 | 41.2 | 55.9 | 47.9 |
| LnGrp LOS | В | D | С | D | С | С | D | D | D | D | E | <u> </u> |
| Approach Vol, veh/h | | 2791 | | | 1419 | | | 707 | | | 1081 | |
| Approach Delay, s/veh | | 49.6 | | | 28.9 | | | 48.4 | | | 51.0 | |
| Approach LOS | | D | | | С | | | D | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 17.2 | 68.8 | 20.0 | 34.1 | 13.9 | 72.0 | 17.0 | 37.1 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 16.0 | * 53 | 16.0 | 33.0 | 16.0 | * 53 | 16.0 | 33.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 12.9 | 65.9 | 18.8 | 18.2 | 9.5 | 24.3 | 12.8 | 27.2 | | | | |
| Green Ext Time (p_c), s | 0.2 | 0.0 | 0.0 | 3.5 | 0.4 | 19.3 | 0.2 | 2.9 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 44.8 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green. * HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| | ٠ | 7 | 1 | Ť | ŧ | 4 |
|-------------------------------|------------|-------|------|-------|----------|--------------|
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y | | | 41 | ¢Î, | |
| Traffic Volume (vph) | 3 | 4 | 21 | 598 | 960 | 5 |
| Future Volume (vph) | 3 | 4 | 21 | 598 | 960 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.2 | 3.3 | 3.5 | 3.5 | 3.5 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 |
| Ped Bike Factor | | | | | | |
| Frt | 0.923 | | | | 0.999 | |
| Flt Protected | 0.979 | | | 0.998 | | |
| Satd. Flow (prot) | 1608 | 0 | 0 | 3428 | 1822 | 0 |
| Flt Permitted | 0.979 | | | 0.998 | | |
| Satd. Flow (perm) | 1608 | 0 | 0 | 3428 | 1822 | 0 |
| Link Speed (k/h) | 60 | | | 60 | 60 | |
| Link Distance (m) | 47.4 | | | 51.2 | 157.3 | |
| Travel Time (s) | 2.8 | | | 3.1 | 9.4 | |
| Confl. Bikes (#/hr) | | | | | | 1 |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 |
| Heavy Vehicles (%) | 2% | 2% | 2% | 4% | 3% | 2% |
| Adj. Flow (vph) | 3 | 4 | 22 | 636 | 1021 | 5 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 7 | 0 | 0 | 658 | 1026 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.2 | | | 0.0 | 0.0 | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 3.0 | | | 3.0 | 3.0 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.06 | 1.06 | 1.04 | 1.01 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | 15 | 25 | | | 15 |
| Sign Control | Stop | | | Free | Free | |
| Intersection Summary | | | | | | |
| Area Type: | Other | | | | | |
| Control Type: Unsignalized | | | | | | |
| Intersection Capacity Utiliza | tion 60.8% | | | IC | CU Level | of Service B |

Analysis Period (min) 15

| | ٠ | 7 | 1 | t | Ļ | ∢ | |
|-----------------------------------|------|------|-------|------|------------|------------|---|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | M | | | -۠ | ţ, | | |
| Traffic Volume (veh/h) | 3 | 4 | 21 | 598 | 960 | 5 | |
| Future Volume (Veh/h) | 3 | 4 | 21 | 598 | 960 | 5 | |
| Sign Control | Stop | | | Free | Free | | |
| Grade | 0% | | | 0% | 0% | | |
| Peak Hour Factor | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | 0.94 | |
| Hourly flow rate (vph) | 3 | 4 | 22 | 636 | 1021 | 5 | |
| Pedestrians | | | | | | | |
| Lane Width (m) | | | | | | | |
| Walking Speed (m/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | | |
| Median type | | | | None | None | | |
| Median storage veh) | | | | | | | |
| Upstream signal (m) | | | | 147 | | | |
| pX, platoon unblocked | 0.92 | | | | | | |
| vC, conflicting volume | 1386 | 1024 | 1026 | | | | |
| vC1, stage 1 conf vol | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | 1242 | 1024 | 1026 | | | | |
| tC, single (s) | 6.8 | 6.9 | 4.1 | | | | |
| tC, 2 stage (s) | | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | | |
| p0 queue free % | 98 | 98 | 97 | | | | |
| cM capacity (veh/h) | 148 | 233 | 673 | | | | |
| Direction, Lane # | EB 1 | NB 1 | NB 2 | SB 1 | | | |
| Volume Total | 7 | 234 | 424 | 1026 | | | |
| Volume Left | 3 | 22 | 0 | 0 | | | |
| Volume Right | 4 | 0 | 0 | 5 | | | |
| cSH | 187 | 673 | 1700 | 1700 | | | |
| Volume to Capacity | 0.04 | 0.03 | 0.25 | 0.60 | | | |
| Queue Length 95th (m) | 0.8 | 0.7 | 0.0 | 0.0 | | | |
| Control Delay (s) | 25.0 | 1.3 | 0.0 | 0.0 | | | |
| Lane LOS | С | А | | | | | |
| Approach Delay (s) | 25.0 | 0.5 | | 0.0 | | | |
| Approach LOS | С | | | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 0.3 | | | | |
| Intersection Capacity Utilization | on | | 60.8% | IC | CU Level c | of Service | В |
| Analysis Period (min) | | | 15 | | | | |

Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٠ | - | 7 | 4 | + | • | 1 | Ť | 1 | 1 | ţ | ~ |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | *** | 1 | 5 | *** | 1 | 7 | 44 | 1 | ۲ | ^ | 1 |
| Traffic Volume (vph) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Future Volume (vph) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | | | 0.99 | 1.00 | | | 1.00 | | | | | 0.99 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5036 | 1477 | 1694 | 5085 | 1506 | 1652 | 3500 | 1478 | 1652 | 3433 | 1478 |
| Flt Permitted | 0.067 | | | 0.107 | | | 0.432 | | | 0.110 | | |
| Satd. Flow (perm) | 121 | 5036 | 1455 | 191 | 5085 | 1506 | 751 | 3500 | 1478 | 191 | 3433 | 1459 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 146 | | | 160 | | | 258 | | | 161 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 329.1 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 19.7 | | | 11.3 | | | 5.7 | |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | Ŭ | | 3.3 | Ŭ | | 3.0 | Ŭ | | 3.0 | Ŭ |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | Cl+Ex | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | Cl+Ex | Cl+Ex | CI+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | CI+Ex | | | CI+Ex | | | CI+Ex | | | CI+Ex | |

07-24-2023

Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٠ | - | 7 | 1 | + | * | 1 | 1 | 1 | 1 | ŧ | ~ |
|------------------------------|---------------------|----------|---------|-----------|------------|-------|-------|--------|--------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | - | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 | 7.0 | 10.0 | 10.0 | 7.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 52.9 | 52.9 | 11.0 | 52.9 | 52.9 | 11.0 | 56.0 | 56.0 | 11.0 | 56.0 | 56.0 |
| Total Split (s) | 20.0 | 60.0 | 60.0 | 20.0 | 60.0 | 60.0 | 20.0 | 40.0 | 40.0 | 20.0 | 40.0 | 40.0 |
| Total Split (%) | 14.3% | 42.9% | 42.9% | 14.3% | 42.9% | 42.9% | 14.3% | 28.6% | 28.6% | 14.3% | 28.6% | 28.6% |
| Maximum Green (s) | 16.0 | 53.1 | 53.1 | 16.0 | 53.1 | 53.1 | 16.0 | 33.0 | 33.0 | 16.0 | 33.0 | 33.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.7 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 3.3 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | 15.0 | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | 34.0 | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Act Effct Green (s) | 79.0 | 60.1 | 60.1 | 75.9 | 58.0 | 58.0 | 58.3 | 36.3 | 36.3 | 56.9 | 35.2 | 35.2 |
| Actuated g/C Ratio | 0.56 | 0.43 | 0.43 | 0.54 | 0.41 | 0.41 | 0.42 | 0.26 | 0.26 | 0.41 | 0.25 | 0.25 |
| v/c Ratio | 0.63 | 0.64 | 0.21 | 0.46 | 1.02 | 0.33 | 0.60 | 0.93 | 0.94 | 0.72 | 0.40 | 0.33 |
| Control Delay | 39.1 | 33.6 | 4.6 | 20.5 | 65.4 | 11.0 | 34.6 | 68.3 | 52.8 | 47.0 | 45.3 | 7.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 39.1 | 33.6 | 4.6 | 20.5 | 65.4 | 11.0 | 34.6 | 68.3 | 52.8 | 47.0 | 45.3 | 7.8 |
| LOS | D | С | А | С | E | В | С | E | D | D | D | А |
| Approach Delay | | 31.6 | | | 58.1 | | | 57.9 | | | 37.0 | |
| Approach LOS | | С | | | E | | | E | | | D | |
| Queue Length 50th (m) | 23.6 | 100.5 | 0.0 | 13.3 | ~214.7 | 12.4 | 45.0 | 113.0 | 81.7 | 30.8 | 38.7 | 0.0 |
| Queue Length 95th (m) | 45.3 | 123.1 | 12.2 | 22.2 | #248.6 | 31.3 | 66.2 | #151.0 | #149.4 | 55.2 | 52.3 | 16.1 |
| Internal Link Dist (m) | | 269.2 | | | 305.1 | | | 164.2 | | | 71.5 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 284 | 2162 | 707 | 311 | 2105 | 717 | 435 | 907 | 574 | 277 | 864 | 487 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.56 | 0.64 | 0.21 | 0.37 | 1.02 | 0.33 | 0.60 | 0.93 | 0.94 | 0.68 | 0.40 | 0.33 |
| Intersection Summary | ntersection Summary | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 140 | | | | | | | | | | | | |
| Actuated Cycle Length: 140 |) | | | | | | | | | | | |
| Offset: 100 (71%), Reference | ced to phas | e 2:EBTL | and 6:W | 'BTL, Sta | rt of Gree | n | | | | | | |
| Natural Cycle: 145 | | | | | | | | | | | | |

Control Type: Actuated-Coordinated

| Ма | aximum v/c Ratio: 1.02 | |
|-----|--|------------------------|
| Int | ersection Signal Delay: 48.9 | Intersection LOS: D |
| Int | ersection Capacity Utilization 96.5% | ICU Level of Service F |
| An | alysis Period (min) 15 | |
| ~ | Volume exceeds capacity, queue is theoretically infinite. | |
| | Queue shown is maximum after two cycles. | |
| # | 95th percentile volume exceeds capacity, queue may be long | ger. |
| | Queue shown is maximum after two cycles. | |
| | | |
| | | |

Splits and Phases: 1: Ninth Line & Dundas Street East

| √ Ø1 | 🗘 🖉 Ø2 (R) | Ø3 | ™ ø4 |
|-------------|------------|------|-------------|
| 20 s | 60 s | 20 s | 40 s |
| ▶ Ø5 | ● Ø6 (R) | 107 | Ø8 |
| 20 s | 60 s | 20 s | 40 s |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | 1 | + | • | 1 | Ť | 1 | 4 | Ŧ | ~ |
|---|---------|------|------|-------|------------|------------|---------|-------|------|-------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 5 | *** | 1 | 5 | ** | 1 | 5 | ** | 1 |
| Traffic Volume (vph) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Future Volume (vph) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5036 | 1455 | 1694 | 5085 | 1506 | 1651 | 3500 | 1478 | 1652 | 3433 | 1459 |
| Flt Permitted | 0.07 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 | 0.43 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 |
| Satd. Flow (perm) | 120 | 5036 | 1455 | 190 | 5085 | 1506 | 751 | 3500 | 1478 | 192 | 3433 | 1459 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| RTOR Reduction (vph) | 0 | 0 | 83 | 0 | 0 | 94 | 0 | 0 | 191 | 0 | 0 | 121 |
| Lane Group Flow (vph) | 158 | 1392 | 63 | 116 | 2149 | 145 | 260 | 846 | 351 | 187 | 344 | 40 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 71.3 | 58.2 | 58.2 | 67.1 | 56.1 | 56.1 | 50.0 | 34.3 | 34.3 | 47.8 | 33.2 | 33.2 |
| Effective Green, g (s) | 76.2 | 60.1 | 60.1 | 73.1 | 58.0 | 58.0 | 55.9 | 36.3 | 36.3 | 53.8 | 35.2 | 35.2 |
| Actuated g/C Ratio | 0.54 | 0.43 | 0.43 | 0.52 | 0.41 | 0.41 | 0.40 | 0.26 | 0.26 | 0.38 | 0.25 | 0.25 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 248 | 2161 | 624 | 249 | 2106 | 623 | 420 | 907 | 383 | 257 | 863 | 366 |
| v/s Ratio Prot | c0.07 | 0.28 | | 0.05 | c0.42 | | c0.08 | c0.24 | | c0.09 | 0.10 | |
| v/s Ratio Perm | 0.27 | | 0.04 | 0.20 | | 0.10 | 0.16 | | 0.24 | 0.19 | | 0.03 |
| v/c Ratio | 0.64 | 0.64 | 0.10 | 0.47 | 1.02 | 0.23 | 0.62 | 0.93 | 0.92 | 0.73 | 0.40 | 0.11 |
| Uniform Delay, d1 | 35.6 | 31.5 | 23.8 | 20.5 | 41.0 | 26.6 | 30.3 | 50.7 | 50.4 | 33.5 | 43.6 | 40.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 5.5 | 1.5 | 0.3 | 1.6 | 24.9 | 0.9 | 2.8 | 16.2 | 26.4 | 10.2 | 0.4 | 0.2 |
| Delay (s) | 41.2 | 33.0 | 24.1 | 22.1 | 65.9 | 27.5 | 33.1 | 66.8 | 76.8 | 43.7 | 44.0 | 40.5 |
| Level of Service | D | С | С | С | E | С | С | E | E | D | D | D |
| Approach Delay (s) | | 33.0 | | | 60.2 | | | 64.8 | | | 43.1 | |
| Approach LOS | | С | | | E | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 52.5 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capacit | v ratio | | 0.90 | | | | | | _ | | | |
| Actuated Cycle Length (s) 140.0 | | | | S | um of lost | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization 96.5% | | | | IC | U Level o | of Service |) | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM 6th Signalized Intersection Summary 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | 1 | ← | • | 1 | t | 1 | 4 | ŧ | ~ |
|------------------------------|------|-------|------|------|------|-------|------|----------|----------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 2 | *** | 1 | 7 | *** | * | 7 | ^ | 7 | 7 | ^ | 1 |
| Traffic Volume (veh/h) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Future Volume (veh/h) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1841 | 1856 | 1870 | 1870 | 1796 | 1870 | 1796 | 1796 | 1841 | 1796 |
| Adj Flow Rate, veh/h | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 2 | 3 | 4 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 2 |
| Cap, veh/h | 220 | 2416 | 731 | 270 | 2346 | 715 | 416 | 888 | 380 | 259 | 807 | 351 |
| Arrive On Green | 0.09 | 0.48 | 0.48 | 0.07 | 0.46 | 0.46 | 0.14 | 0.25 | 0.25 | 0.12 | 0.23 | 0.23 |
| Sat Flow, veh/h | 1781 | 5066 | 1532 | 1767 | 5106 | 1557 | 1710 | 3554 | 1520 | 1710 | 3497 | 1520 |
| Grp Volume(v), veh/h | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1689 | 1532 | 1767 | 1702 | 1557 | 1710 | 1777 | 1520 | 1710 | 1749 | 1520 |
| Q Serve(g_s), s | 7.0 | 27.7 | 7.7 | 4.5 | 55.0 | 13.7 | 15.4 | 32.8 | 35.0 | 11.1 | 11.7 | 12.8 |
| Cycle Q Clear(g_c), s | 7.0 | 27.7 | 7.7 | 4.5 | 55.0 | 13.7 | 15.4 | 32.8 | 35.0 | 11.1 | 11.7 | 12.8 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 220 | 2416 | 731 | 270 | 2346 | 715 | 416 | 888 | 380 | 259 | 807 | 351 |
| V/C Ratio(X) | 0.72 | 0.58 | 0.20 | 0.43 | 0.92 | 0.33 | 0.63 | 0.95 | 1.43 | 0.72 | 0.43 | 0.46 |
| Avail Cap(c_a), veh/h | 304 | 2416 | 731 | 385 | 2346 | 715 | 416 | 888 | 380 | 292 | 874 | 380 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 35.9 | 26.4 | 21.2 | 19.8 | 35.3 | 24.2 | 31.9 | 51.7 | 52.5 | 36.7 | 45.9 | 46.3 |
| Incr Delay (d2), s/veh | 5.8 | 1.0 | 0.6 | 1.3 | 7.1 | 1.3 | 3.2 | 19.6 | 206.6 | 7.9 | 0.4 | 1.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 6.0 | 12.3 | 3.2 | 2.1 | 25.6 | 5.7 | 7.2 | 17.7 | 35.8 | 5.5 | 5.5 | 5.2 |
| Unsig. Movement Delay, s/veh | | 07.4 | 04.0 | 04.4 | 10.1 | 05.4 | 05.4 | 74.0 | 050 (| | 10.1 | 17 - |
| LnGrp Delay(d),s/veh | 41./ | 27.4 | 21.8 | 21.1 | 42.4 | 25.4 | 35.1 | /1.3 | 259.1 | 44.6 | 46.4 | 47.5 |
| LnGrp LOS | D | C | C | C | D | C | D | E | <u> </u> | D | <u>D</u> | D |
| Approach Vol, veh/h | | 1696 | | | 2504 | | | 1648 | | | 692 | |
| Approach Delay, s/veh | | 28.3 | | | 39.8 | | | 127.4 | | | 46.1 | |
| Approach LOS | | С | | | D | | | F | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 10.9 | 71.8 | 17.3 | 40.0 | 13.4 | 69.3 | 20.0 | 37.3 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 16.0 | * 53 | 16.0 | 33.0 | 16.0 | * 53 | 16.0 | 33.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 6.5 | 30.7 | 13.1 | 37.0 | 9.0 | 57.0 | 17.4 | 14.8 | | | | |
| Green Ext Time (p_c), s | 0.3 | 18.5 | 0.2 | 0.0 | 0.4 | 0.0 | 0.0 | 3.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 59.5 | | | | | | | | | |
| HCM 6th LOS | | | Е | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| | ٠ | 7 | 1 | † | Ŧ | ~ |
|-----------------------------------|------------|-------|------|------------|----------|--------------|
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y | | | ₫ ħ | Þ | |
| Traffic Volume (vph) | 11 | 38 | 22 | 1177 | 637 | 5 |
| Future Volume (vph) | 11 | 38 | 22 | 1177 | 637 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.2 | 3.3 | 3.5 | 3.5 | 3.5 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 |
| Ped Bike Factor | | | | | | |
| Frt | 0.895 | | | | 0.999 | |
| Flt Protected | 0.989 | | | 0.999 | | |
| Satd. Flow (prot) | 1576 | 0 | 0 | 3496 | 1840 | 0 |
| Flt Permitted | 0.989 | | | 0.999 | | |
| Satd. Flow (perm) | 1576 | 0 | 0 | 3496 | 1840 | 0 |
| Link Speed (k/h) | 60 | | | 60 | 60 | |
| Link Distance (m) | 47.4 | | | 51.2 | 158.7 | |
| Travel Time (s) | 2.8 | | | 3.1 | 9.5 | |
| Confl. Peds. (#/hr) | | 2 | | | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 11 | 39 | 23 | 1213 | 657 | 5 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 50 | 0 | 0 | 1236 | 662 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.2 | | | 0.0 | 0.0 | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 3.0 | | | 3.0 | 3.0 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.06 | 1.06 | 1.04 | 1.01 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | 15 | 25 | | | 15 |
| Sign Control | Stop | | | Free | Free | |
| Intersection Summary | | | | | | |
| Area Type: | Other | | | | | |
| Control Type: Unsignalized | | | | | | |
| Intersection Capacity Utilization | tion 58.8% | | | IC | CU Level | of Service E |
| Analysis Period (min) 15 | | | | | | |

| | ٠ | 7 | 1 | Ť | ŧ | 1 | |
|-----------------------------------|------|------|-------|------|------------|------------|------|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | Y | | | -fî† | f, | | |
| Traffic Volume (veh/h) | 11 | 38 | 22 | 1177 | 637 | 5 | |
| Future Volume (Veh/h) | 11 | 38 | 22 | 1177 | 637 | 5 | |
| Sign Control | Stop | | | Free | Free | | |
| Grade | 0% | | | 0% | 0% | | |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | |
| Hourly flow rate (vph) | 11 | 39 | 23 | 1213 | 657 | 5 | |
| Pedestrians | | | | 2 | | | |
| Lane Width (m) | | | | 3.5 | | | |
| Walking Speed (m/s) | | | | 1.1 | | | |
| Percent Blockage | | | | 0 | | | |
| Right turn flare (veh) | | | | | | | |
| Median type | | | | None | None | | |
| Median storage veh) | | | | | | | |
| Upstream signal (m) | | | | 147 | | | |
| pX, platoon unblocked | 0.76 | | | | | | |
| vC, conflicting volume | 1312 | 662 | 662 | | | | |
| vC1, stage 1 conf vol | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | 792 | 662 | 662 | | | | |
| tC, single (s) | 6.8 | 6.9 | 4.1 | | | | |
| tC, 2 stage (s) | | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | | |
| p0 queue free % | 95 | 90 | 98 | | | | |
| cM capacity (veh/h) | 243 | 404 | 922 | | | | |
| Direction, Lane # | EB 1 | NB 1 | NB 2 | SB 1 | | | |
| Volume Total | 50 | 427 | 809 | 662 | | | |
| Volume Left | 11 | 23 | 0 | 0 | | | |
| Volume Right | 39 | 0 | 0 | 5 | | | |
| cSH | 353 | 922 | 1700 | 1700 | | | |
| Volume to Capacity | 0.14 | 0.02 | 0.48 | 0.39 | | | |
| Queue Length 95th (m) | 3.4 | 0.5 | 0.0 | 0.0 | | | |
| Control Delay (s) | 16.9 | 0.8 | 0.0 | 0.0 | | | |
| Lane LOS | С | А | | | | | |
| Approach Delay (s) | 16.9 | 0.3 | | 0.0 | | | |
| Approach LOS | С | | | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 0.6 | | | | |
| Intersection Capacity Utilization | on | | 58.8% | IC | CU Level c | of Service | В |
| Analysis Period (min) | | | 15 | | | | |

Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٦ | - | $\mathbf{\hat{z}}$ | 4 | + | * | 1 | 1 | ۲ | 1 | ŧ | ~ |
|----------------------------|-------|-------|--------------------|-------|-------|-------|-------|-------|-------|-------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 5 | *** | 1 | 5 | 44 | 1 | 5 | * | 1 |
| Traffic Volume (vph) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Future Volume (vph) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | | | 0.99 | 1.00 | | | 1.00 | | | | | 0.99 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5036 | 1477 | 1694 | 5085 | 1506 | 1652 | 3500 | 1478 | 1652 | 3433 | 1478 |
| Flt Permitted | 0.061 | | | 0.109 | | | 0.519 | | | 0.107 | | |
| Satd. Flow (perm) | 110 | 5036 | 1455 | 194 | 5085 | 1506 | 902 | 3500 | 1478 | 186 | 3433 | 1459 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 146 | | | 166 | | | 59 | | | 144 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 329.1 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 19.7 | | | 11.3 | | | 5.7 | |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | | | 3.3 | | | 3.0 | | | 3.0 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | |

07-24-2023 ZL

Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

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|----------------------------|------------|----------|--------------------|-------------|----------|-------|-------|-------|--------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | . 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 1 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 | 7.0 | 10.0 | 7.0 | 7.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 52.9 | 52.9 | 11.0 | 52.9 | 52.9 | 11.0 | 56.0 | 11.0 | 11.0 | 56.0 | 56.0 |
| Total Split (s) | 12.0 | 67.0 | 67.0 | 13.0 | 68.0 | 68.0 | 11.0 | 50.0 | 13.0 | 15.0 | 54.0 | 54.0 |
| Total Split (%) | 8.3% | 46.2% | 46.2% | 9.0% | 46.9% | 46.9% | 7.6% | 34.5% | 9.0% | 10.3% | 37.2% | 37.2% |
| Maximum Green (s) | 8.0 | 60.1 | 60.1 | 9.0 | 61.1 | 61.1 | 7.0 | 43.0 | 9.0 | 11.0 | 47.0 | 47.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.0 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 1.0 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 2.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | | | 0 | 0 |
| Act Effct Green (s) | 80.8 | 64.9 | 64.9 | 80.3 | 64.3 | 64.3 | 56.0 | 42.0 | 58.1 | 61.0 | 46.0 | 46.0 |
| Actuated g/C Ratio | 0.56 | 0.45 | 0.45 | 0.55 | 0.44 | 0.44 | 0.39 | 0.29 | 0.40 | 0.42 | 0.32 | 0.32 |
| v/c Ratio | 0.79 | 0.62 | 0.20 | 0.50 | 0.95 | 0.31 | 0.65 | 0.83 | 0.86 | 0.85 | 0.32 | 0.29 |
| Control Delay | 59.1 | 32.5 | 4.3 | 23.1 | 50.0 | 9.5 | 39.6 | 56.2 | 50.2 | 63.9 | 38.0 | 8.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 59.1 | 32.5 | 4.3 | 23.1 | 50.0 | 9.5 | 39.6 | 56.2 | 50.2 | 63.9 | 38.0 | 8.2 |
| LOS | E | С | A | С | D | A | D | E | D | E | D | A |
| Approach Delay | | 32.6 | | | 44.9 | | | 51.6 | | | 38.1 | |
| Approach LOS | | С | | | D | | | D | | | D | |
| Queue Length 50th (m) | 27.4 | 105.5 | 0.0 | 14.3 | 201.5 | 11.4 | 45.7 | 108.6 | 114.7 | 31.3 | 35.6 | 3.1 |
| Queue Length 95th (m) | #65.9 | 120.3 | 11.9 | 24.1 | #235.3 | 28.3 | 65.5 | 130.2 | #165.6 | #68.5 | 47.2 | 17.9 |
| Internal Link Dist (m) | | 269.2 | | | 305.1 | | | 164.2 | | | 71.5 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 201 | 2254 | 731 | 234 | 2253 | 760 | 400 | 1086 | 629 | 219 | 1160 | 588 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.79 | 0.62 | 0.20 | 0.50 | 0.95 | 0.31 | 0.65 | 0.78 | 0.86 | 0.85 | 0.30 | 0.27 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 145 | | | | | | | | | | | | |
| Actuated Cycle Length: 145 | a | | | Otert | Creation | | | | | | | |
| Natural Cycle: 145 | o priase 2 | .EBIL an | n o:MRT | ., Start of | Green | | | | | | | |
| | | | | | | | | | | | | |

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.95

Intersection Signal Delay: 42.7 Intersection Capacity Utilization 96.5% Intersection LOS: D ICU Level of Service F

Analysis Period (min) 15

95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Ninth Line & Dundas Street East

| 1 Ø1 | 🖉 🖉 🖉 🖉 🖉 | Ø3 | ₩ Ø4 |
|-------------|-----------|-------------|-------------|
| 13 s | 67 s | 15 s | 50 s |
| | ∮ Ø6 (R) | 1 Ø7 | Ø8 |
| 12 s | 68 s | 11s 54 | łs |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ≯ | - | $\mathbf{\hat{z}}$ | ∢ | + | * | 1 | 1 | ۲ | 1 | Ŧ | ~ |
|---------------------------------|-----------|---------|--------------------|-------|-----------|------------|---------|---------|-------|-------|---------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 1 | <u></u> | 1 | ľ | ^ | 1 | ľ | <u></u> | 1 | ľ | <u></u> | 1 |
| Traffic Volume (vph) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Future Volume (vph) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 2.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5036 | 1455 | 1694 | 5085 | 1506 | 1651 | 3500 | 1478 | 1652 | 3433 | 1459 |
| Flt Permitted | 0.06 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 | 0.52 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 |
| Satd. Flow (perm) | 109 | 5036 | 1455 | 195 | 5085 | 1506 | 902 | 3500 | 1478 | 187 | 3433 | 1459 |
| Peak-hour factor, PHF | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Adj. Flow (vph) | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| RTOR Reduction (vph) | 0 | 0 | 81 | 0 | 0 | 92 | 0 | 0 | 37 | 0 | 0 | 98 |
| Lane Group Flow (vph) | 158 | 1392 | 65 | 116 | 2149 | 147 | 260 | 846 | 505 | 187 | 344 | 63 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 72.7 | 63.0 | 63.0 | 71.5 | 62.4 | 62.4 | 47.0 | 40.0 | 49.1 | 55.0 | 44.0 | 44.0 |
| Effective Green, g (s) | 78.7 | 64.9 | 64.9 | 77.5 | 64.3 | 64.3 | 53.0 | 42.0 | 53.1 | 58.0 | 46.0 | 46.0 |
| Actuated g/C Ratio | 0.54 | 0.45 | 0.45 | 0.53 | 0.44 | 0.44 | 0.37 | 0.29 | 0.37 | 0.40 | 0.32 | 0.32 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 4.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 199 | 2254 | 651 | 229 | 2254 | 667 | 381 | 1013 | 541 | 216 | 1089 | 462 |
| v/s Ratio Prot | c0.07 | 0.28 | | 0.04 | c0.42 | | 0.05 | 0.24 | c0.07 | c0.08 | 0.10 | |
| v/s Ratio Perm | 0.36 | | 0.04 | 0.23 | | 0.10 | 0.20 | | 0.27 | 0.26 | | 0.04 |
| v/c Ratio | 0.79 | 0.62 | 0.10 | 0.51 | 0.95 | 0.22 | 0.68 | 0.84 | 0.93 | 0.87 | 0.32 | 0.14 |
| Uniform Delay, d1 | 40.9 | 30.6 | 23.2 | 20.5 | 38.9 | 24.9 | 36.4 | 48.3 | 44.2 | 34.0 | 37.6 | 35.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 19.7 | 1.3 | 0.3 | 2.1 | 10.8 | 0.8 | 5.2 | 6.2 | 23.4 | 28.9 | 0.2 | 0.2 |
| Delay (s) | 60.7 | 31.9 | 23.5 | 22.6 | 49.7 | 25.6 | 41.6 | 54.5 | 67.7 | 63.0 | 37.8 | 35.5 |
| Level of Service | E | С | С | С | D | С | D | D | E | E | D | D |
| Approach Delay (s) | | 33.8 | | | 46.1 | | | 56.8 | | | 44.0 | |
| Approach LOS | | С | | | D | | | E | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 45.4 | Н | CM 2000 | Level of | Service | | D | | | |
| HCM 2000 Volume to Capaci | ity ratio | | 0.92 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 145.0 | S | um of los | t time (s) | | | 13.0 | | | |
| Intersection Capacity Utilizati | on | | 96.5% | IC | U Level | of Service |) | | F | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

| | ≯ | - | \mathbf{r} | • | - | * | 1 | 1 | 1 | 1 | ŧ | ~ |
|------------------------------|------|----------|--------------|----------|----------|-------|------|----------|------|------|---------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | ^ | 1 | <u> </u> | ^ | 1 | ٦ | <u>^</u> | 1 | ۲ | <u></u> | 1 |
| Traffic Volume (veh/h) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Future Volume (veh/h) | 153 | 1350 | 142 | 113 | 2085 | 232 | 252 | 821 | 526 | 181 | 334 | 156 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1841 | 1856 | 1870 | 1870 | 1796 | 1870 | 1796 | 1796 | 1841 | 1796 |
| Adj Flow Rate, veh/h | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| Peak Hour Factor | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 | 0.97 |
| Percent Heavy Veh, % | 2 | 3 | 4 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 2 |
| Cap, veh/h | 189 | 2236 | 676 | 249 | 2219 | 676 | 401 | 1103 | 566 | 253 | 1182 | 514 |
| Arrive On Green | 0.08 | 0.44 | 0.44 | 0.07 | 0.43 | 0.43 | 0.07 | 0.31 | 0.31 | 0.10 | 0.34 | 0.34 |
| Sat Flow, veh/h | 1781 | 5066 | 1532 | 1767 | 5106 | 1556 | 1710 | 3554 | 1520 | 1710 | 3497 | 1520 |
| Grp Volume(v), veh/h | 158 | 1392 | 146 | 116 | 2149 | 239 | 260 | 846 | 542 | 187 | 344 | 161 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1689 | 1532 | 1767 | 1702 | 1556 | 1710 | 1777 | 1520 | 1710 | 1749 | 1520 |
| Q Serve(g_s), s | 8.2 | 30.7 | 8.5 | 5.0 | 59.6 | 14.9 | 10.0 | 31.2 | 45.0 | 10.2 | 10.5 | 11.4 |
| Cycle Q Clear(g_c), s | 8.2 | 30.7 | 8.5 | 5.0 | 59.6 | 14.9 | 10.0 | 31.2 | 45.0 | 10.2 | 10.5 | 11.4 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 189 | 2236 | 676 | 249 | 2219 | 676 | 401 | 1103 | 566 | 253 | 1182 | 514 |
| V/C Ratio(X) | 0.83 | 0.62 | 0.22 | 0.47 | 0.97 | 0.35 | 0.65 | 0.77 | 0.96 | 0.74 | 0.29 | 0.31 |
| Avail Cap(c_a), veh/h | 189 | 2236 | 676 | 273 | 2219 | 676 | 401 | 1103 | 566 | 253 | 1182 | 514 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 40.9 | 31.2 | 25.0 | 23.5 | 40.0 | 27.4 | 35.5 | 45.3 | 44.4 | 33.1 | 35.2 | 35.5 |
| Incr Delay (d2), s/veh | 26.6 | 1.3 | 0.7 | 1.6 | 13.0 | 1.4 | 3.9 | 3.4 | 27.5 | 11.3 | 0.2 | 0.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 4.4 | 13.7 | 3.5 | 2.4 | 28.9 | 6.3 | 4.0 | 15.1 | 24.3 | 5.3 | 4.8 | 4.6 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 67.6 | 32.5 | 25.7 | 25.2 | 53.1 | 28.8 | 39.4 | 48.7 | 71.9 | 44.5 | 35.4 | 36.0 |
| LnGrp LOS | E | С | С | С | D | С | D | D | E | D | D | <u> </u> |
| Approach Vol, veh/h | | 1696 | | | 2504 | | | 1648 | | | 692 | |
| Approach Delay, s/veh | | 35.2 | | | 49.5 | | | 54.8 | | | 38.0 | |
| Approach LOS | | D | | | D | | | D | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 11.0 | 69.0 | 15.0 | 50.0 | 12.0 | 68.0 | 11.0 | 54.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 9.0 | * 60 | 11.0 | 43.0 | 8.0 | * 61 | 7.0 | 47.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 7.0 | 33.7 | 12.2 | 47.0 | 10.2 | 61.6 | 12.0 | 13.4 | | | | |
| Green Ext Time (p_c), s | 0.1 | 21.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 45.9 | | | | | | | | | |
| HCM 6th LOS | | | D | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Appendix G

Schedule 6 of the City of Mississauga Official Plan





or bodies of water outside the city boundaries, is shown for information purposes only.

Appendix H

Figures from City of Mississauga Pedestrian Master Plan





Proposed Routes ---- Boulevard Multi-Use Trail --- Off Road Trail City of Mississauga Pedestrian Network Gap Region of Peel Pedestrian Network Gap **Existing Routes** Existing Multi-use Trails Existing Pedestrian Trails Sidewalks Engineered Walkways Railway Parks Cemetery Schools Places of Religious Assembly Mixed Use and Commercial Office Land Use



Figure 7. Gaps in the Pedestrian Network

Gaps are locations where there is no sidewalk or multiuse trail on one or both sides of the street. The map does not speak to the quality of the existing infrastructure.

The gaps have been identified based on a GIS analysis of existing infrastructure and does not distinguish whether infrastructure will be implemented through development or other capital projects.

Additional public engagement will be required prior to implementation.


Figure 10. Pedestrian Network Map Priorities

Appendix I

Figures from City of Mississauga Cycling Master Plan



Figure 15: Proposed cycling network



Appendix J

Ninth Line Widening Preliminary Design







| FROM STA. 3+740 TO STA. 3+995 | | | | | | | | |
|---|--|--|--|--|--|--|--|--|
| HALTON REGION | | | | | | | | |
| NINTH LINE – HYDRO RELOCATION ON EAST | | | | | | | | |
| OPTION 1- HYDRO 0.8m TO MUT 2.3m TO R-WALL | | | | | | | | |
| CLASS ENVIRONMENTAL ASSESSMENT STUDY | | | | | | | | |
| SECTION 2 – WILLIAM HALTON PARKWAY TO DUNDAS ST | | | | | | | | |







GRADING LIMIT TEMPORARY EASEMENT

> PROPOSED HYDRO EXISTING HYDRO

PLATE

21

Appendix K

Background Compounded Annual Growth Rates



| From: | Tyler Xuereb <tyler.xuereb@mississauga.ca></tyler.xuereb@mississauga.ca> |
|----------|--|
| Sent: | June 19, 2023 9:31 AM |
| То: | May Lai |
| Cc: | Mark Crockford |
| Subject: | RE: 3855 Dundas Street East Transportation Pre-Study Checklist |

Good Morning May,

Ninth Line south of Dundas Street is under the jurisdiction of Halton Region. Below are the growth rates for Ninth Line north of Dundas Street. While the rates may seem high, this is due to the widening of Ninth Line from 1 through lanes per direction to 2 through lanes per direction.

Dundas Street

| | Compo Annual from Ex 20 | ounded Growth isting to 26 |
|---------|----------------------------------|-------------------------------------|
| | NB | SB |
| AM Peak | 4.5% | 3.5% |
| | | |
| PM Peak | 3.0% | 4.5% |

| | Compo Annual from 202 | ounded Growth 6 to 2031 |
|---------|-----------------------------|-------------------------------|
| | NB | SB |
| AM Peak | 4.5% | 3.5% |
| | | |
| PM Peak | 3.0% | 4.5% |

r

Regards,

Mississauga

Tyler Xuereb Transportation Planning Analyst T 905-615-3200 ext.4783 Tyler.xuereb@mississauga.ca

<u>City of Mississauga</u> | Transportation and Works Department, Infrastructure Planning and Engineering Services Division

Please consider the environment before printing.

From: May Lai <<u>may.lai@cghtransportation.com</u>> Sent: Thursday, June 15, 2023 4:00 PM To: Tyler Xuereb <<u>Tyler.Xuereb@mississauga.ca</u>> Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>> Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi Tyler,

Thank you for the rates along Dundas Street. Is Ninth Line under the jurisdiction of Halton Region? Does Mississauga have the section of Ninth Line south of Dundas Street in the City's model?

Best regards,



May Lai, E.I.T. CGH Transportation Inc. P:289-834-0646 E:May.Lai@CGHTransportation.com

From: Tyler Xuereb <<u>Tyler.Xuereb@mississauga.ca</u>>
Sent: Thursday, June 15, 2023 3:15 PM
To: May Lai <<u>may.lai@cghtransportation.com</u>>
Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>>
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi May,

Below are the recommended growth rates to be used along Dundas Street from existing to 2026 and 2026 to 2031. These rates are compounded annually.

Dundas Street

| | Compo Annual from Ex 20 | ounded Growth isting to 26 | | |
|---------|----------------------------------|-------------------------------------|--|--|
| | EB | WB | | |
| AM Peak | 0.5% | 1.5% | | |
| | | | | |
| PM Peak | 1.5% | 1.5% | | |



| | EB | WB |
|---------|------|------|
| AM Peak | 0.5% | 1.5% |
| | | |
| PM Peak | 1.5% | 1.5% |

Best,



Tyler Xuereb

Transportation Planning Analyst T 905-615-3200 ext.4783 Tyler.xuereb@mississauga.ca

<u>City of Mississauga</u> | Transportation and Works Department, Infrastructure Planning and Engineering Services Division

Please consider the environment before printing.

From: May Lai <<u>may.lai@cghtransportation.com</u>>
Sent: Thursday, June 15, 2023 9:15 AM
To: Tyler Xuereb <<u>Tyler.Xuereb@mississauga.ca</u>>
Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>>
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi Tyler,

Just following up on the email below. I would like to confirm that we will be able to get the growth rates later today for our traffic study. Really appreciate your help!

Best regard,



May Lai, E.I.T. CGH Transportation Inc. P:289-834-0646 E:<u>May.Lai@CGHTransportation.com</u>

From: May Lai
Sent: Tuesday, June 13, 2023 8:03 AM
To: Tyler Xuereb Tyler Xuereb@mississauga.ca
Cc: Mark Crockford mark.crockford@cghtransportation.com
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi Tyler,

Great, thank you so much!

Best regards,



From: Tyler Xuereb Tyler Xuereb@mississauga.ca
Sent: Tuesday, June 13, 2023 8:01 AM
To: May Lai <<u>may.lai@cghtransportation.com</u>
Co: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Good Morning May,

I should be able to get them to you by end of day Thursday.

Regards,



Tyler Xuereb Transportation Planning Analyst T 905-615-3200 ext.4783 Tyler.xuereb@mississauga.ca

<u>City of Mississauga</u> | Transportation and Works Department, Infrastructure Planning and Engineering Services Division

Please consider the environment before printing.

From: May Lai <<u>may.lai@cghtransportation.com</u>>
Sent: Tuesday, June 13, 2023 7:58 AM
To: Tyler Xuereb <<u>Tyler.Xuereb@mississauga.ca</u>>
Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>>
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi Tyler,

Thank you for checking up the growth rates. Do you have an estimate on how long this would take?

Best regards,



May Lai, E.I.T. CGH Transportation Inc. P:289-834-0646 E:May.Lai@CGHTransportation.com From: Tyler Xuereb <<u>Tyler.Xuereb@mississauga.ca</u>>
Sent: Monday, June 12, 2023 11:20 AM
To: May Lai <<u>may.lai@cghtransportation.com</u>>
Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>>
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Thanks May.

I will send the rates to you as soon as I have them.

Regards,



Tyler Xuereb Transportation Planning Analyst T 905-615-3200 ext.4783 Tyler.xuereb@mississauga.ca

<u>City of Mississauga</u> | Transportation and Works Department, Infrastructure Planning and Engineering Services Division

Please consider the environment before printing.

From: May Lai <<u>may.lai@cghtransportation.com</u>>
Sent: Monday, June 12, 2023 11:08 AM
To: Tyler Xuereb <<u>Tyler.Xuereb@mississauga.ca</u>>
Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>>
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi Tyler,

Our future horizons are 2026 and 2031.

Best regards,



May Lai, E.I.T. CGH Transportation Inc. P:289-834-0646 E:<u>May.Lai@CGHTransportation.com</u>

From: Tyler Xuereb Tyler Xuereb@mississauga.ca
Sent: Monday, June 12, 2023 7:47 AM
To: May Lai may.lai@cghtransportation.com
Cc: Mark Crockford mark.crockford@cghtransportation.com
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Good Morning May,

Hope you had a great weekend!

I will provide you with updated rates as or travel demand model has been updated since 2018.

Can you please provide me with your horizon years.

Regards,



Tyler Xuereb Transportation Planning Analyst T 905-615-3200 ext.4783 Tyler.xuereb@mississauga.ca

<u>City of Mississauga</u> | Transportation and Works Department, Infrastructure Planning and Engineering Services Division

Please consider the environment before printing.

From: May Lai <<u>may.lai@cghtransportation.com</u>>
Sent: Friday, June 9, 2023 4:51 PM
To: Tyler Xuereb <<u>Tyler.Xuereb@mississauga.ca</u>>
Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>>
Subject: FW: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi Tyler,

We are currently working on the transportation study for 3855 Dundas Street. Bo has provided his comments on our Terms of Reference. Regarding the compounded annual growth rates to be applied to calculate the future background volumes along Dundas Street East and Ninth Line, we decided to use the rates the City staff informed Crozier to use in their 2018 TIS on the proposed development. Please confirm whether these rates still apply.

Best regards,



May Lai, E.I.T. CGH Transportation Inc. P:289-834-0646 E:May.Lai@CGHTransportation.com

From: Bo Yu <<u>BoYang.Yu@mississauga.ca</u>> Sent: Friday, June 9, 2023 4:18 PM To: May Lai <<u>may.lai@cghtransportation.com</u>> Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>>; Michael Franzolini <<u>Michael.Franzolini@mississauga.ca</u>>; Trans Projects <<u>Trans.Projects@mississauga.ca</u>> Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi May,

Please find attached stamped and approved ToR for the proposed development, which encompasses City comments. Other items to note:

- Certification Form The Transportation Consultant must complete, sign, and seal (if appropriate) the attached Certification Form from the City's TIS Guidelines (2022) and submit the document with the application/report to ensure compliance with qualification requirements. The TIS Guidelines can be found at https://www.mississauga.ca/wp-content/uploads/2023/03/CMississauga-TIS-Guidelines-Version-5.1-Dec-2022.pdf. It must be ensured that the report conforms to the City's TIS Guidelines.
- For City of Mississauga roadways, please contact Tyler Xuereb from the City's Transportation Planning Section (<u>tyler.xuereb@mississauga.ca</u>, Ext. 4783) to confirm growth rates and historical AADT data and Turning Movements Count for the study area roadways. Otherwise, please contact the Halton Region. New traffic counts are to be compared to pre-pandemic counts to ensure that there are no major discrepancies.
- Signal timing plans for signalized intersections under the City's jurisdiction can be obtained from Jim Kartsomanis (Jim.Kartsomanis@mississauga.ca, Ext. 3964).

Should you have any questions, please feel free to contact me.

Regards,

Mississauga

Bo Yang Yu, C.Tech Traffic Planning Technologist T 905-615-3200 ext. 4784 boyang.yu@mississauga.ca

<u>City of Mississauga</u> | Transportation & Works Department Infrastructure Planning & Engineering Services Division

Please consider the environment before printing

From: Ryan Au <<u>Ryan.Au@mississauga.ca</u>> On Behalf Of Trans Projects
Sent: Wednesday, May 31, 2023 8:57 AM
To: May Lai <<u>may.lai@cghtransportation.com</u>>
Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>>; Michael Franzolini
<<u>Michael.Franzolini@mississauga.ca</u>>; Bo Yu <<u>BoYang.Yu@mississauga.ca</u>>
Subject: RE: 3855 Dundas Street East Transportation Pre-Study Checklist

Hi May,

This is to acknowledge receipt of your email. Bo (copied) will provide a response on the TOR.

Thanks,

MISSISSauga

Ryan Au, P.Eng.

Manager, Traffic Planning T 905-615-3200 ext. 3713 ryan.au@mississauga.ca

<u>City of Mississauga</u> | Transportation & Works Department 300 City Centre Drive | Mississauga ON | L5B 3C1

Please consider the environment before printing.

From: May Lai <<u>may.lai@cghtransportation.com</u>> Sent: Tuesday, May 30, 2023 5:01 PM To: Trans Projects <<u>Trans.Projects@mississauga.ca</u>> Cc: Mark Crockford <<u>mark.crockford@cghtransportation.com</u>> Subject: 3855 Dundas Street East Transportation Pre-Study Checklist

Greetings,

CGH Transportation has been retained by Dymon Group of Companies to undertake a traffic impact study to support a mixed-use development at 3855 Dundas Street East in the City of Mississauga, near the Mississauga / Oakville boundary. The proposed development will include a self-storage facility, a coworking office and a retail / reception space. We have filled out the attached checklist with the scope, parameters and assumptions intended to be used in our proposed traffic impact study. Please let us know if City staff have any comments or questions.

Best regards,



May Lai, E.I.T. CGH Transportation Inc. P:289-834-0646 E:<u>May.Lai@CGHTransportation.com</u>

Appendix L

2026 Future Background Synchro Intersection Worksheets



| | ٠ | - | 7 | 4 | + | * | 1 | t | 1 | 1 | ŧ | ~ |
|----------------------------|-------|-------|-------|-------|-------|-------|-------|----------|-------|-------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 111 | 1 | 7 | *** | 1 | ۲ | ^ | 1 | 7 | ^ | 1 |
| Traffic Volume (vph) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Future Volume (vph) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.115 | | | 0.067 | | | 0.144 | | | 0.385 | | |
| Satd. Flow (perm) | 207 | 5085 | 1491 | 116 | 4715 | 1449 | 232 | 3433 | 1422 | 663 | 3466 | 1478 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 197 | | | 147 | | | 192 | | | 172 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 329.1 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 19.7 | | | 11.3 | | | 5.7 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| Enter Blocked Intersection | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | | | 3.3 | | | 3.0 | | | 3.0 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | | | Cl+Ex | |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |

ZL

| | ٨ | + | * | 4 | ł | * | 1 | 1 | 1 | 1 | ţ | ~ |
|----------------------------|-------------|-----------|-----------|----------|------------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 | 7.0 | 10.0 | 10.0 | 7.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 52.9 | 52.9 | 11.0 | 52.9 | 52.9 | 11.0 | 56.0 | 56.0 | 11.0 | 56.0 | 56.0 |
| Total Split (s) | 20.0 | 60.0 | 60.0 | 20.0 | 60.0 | 60.0 | 20.0 | 40.0 | 40.0 | 20.0 | 40.0 | 40.0 |
| Total Split (%) | 14.3% | 42.9% | 42.9% | 14.3% | 42.9% | 42.9% | 14.3% | 28.6% | 28.6% | 14.3% | 28.6% | 28.6% |
| Maximum Green (s) | 16.0 | 53.1 | 53.1 | 16.0 | 53.1 | 53.1 | 16.0 | 33.0 | 33.0 | 16.0 | 33.0 | 33.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.7 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 3.3 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | 15.0 | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | 34.0 | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Act Effct Green (s) | 79.2 | 58.0 | 58.0 | 80.1 | 58.6 | 58.6 | 56.0 | 33.3 | 33.3 | 56.5 | 33.6 | 33.6 |
| Actuated g/C Ratio | 0.57 | 0.41 | 0.41 | 0.57 | 0.42 | 0.42 | 0.40 | 0.24 | 0.24 | 0.40 | 0.24 | 0.24 |
| v/c Ratio | 0.63 | 1.40 | 0.55 | 0.76 | 0.67 | 0.21 | 0.78 | 0.48 | 0.40 | 0.69 | 0.83 | 0.35 |
| Control Delay | 28.9 | 215.4 | 19.0 | 52.5 | 35.7 | 4.8 | 51.4 | 47.8 | 8.0 | 39.4 | 60.2 | 7.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 28.9 | 215.4 | 19.0 | 52.5 | 35.7 | 4.8 | 51.4 | 47.8 | 8.0 | 39.4 | 60.2 | 7.8 |
| LOS | С | H 100 f | В | D | D | A | D | D | A | D | E | A |
| Approach Delay | | 183.1 | | | 34.9 | | | 39.0 | | | 47.2 | |
| Approach LOS | | H | 10 - | 07.0 | C | | 05.4 | D | | 10.1 | D | |
| Queue Length 50th (m) | 22.7 | ~377.3 | 40.5 | 35.0 | 103.1 | 0.0 | 35.1 | 44.5 | 0.0 | 48.4 | 87.4 | 0.0 |
| Queue Length 95th (m) | 44.7 | #399.2 | 71.1 | #64.5 | 119.0 | 12.3 | #66.6 | 59.2 | 17.6 | 70.7 | 108.6 | 16.5 |
| Internal Link Dist (m) | 000.0 | 269.2 | 00.0 | 000.0 | 305.1 | 00.0 | 400.0 | 164.2 | 100.0 | 400.0 | /1.5 | 70.0 |
| Turn Bay Length (m) | 220.0 | 0400 | 80.0 | 230.0 | 4070 | 80.0 | 130.0 | 050 | 130.0 | 130.0 | 000 | 70.0 |
| Base Capacity (vph) | 322 | 2106 | 733 | 274 | 1972 | 691 | 269 | 858 | 499 | 399 | 866 | 498 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.59 | 1.40 | 0.55 | 0.72 | 0.67 | 0.21 | 0.77 | 0.45 | 0.38 | 0.69 | 0.80 | 0.35 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 140 | | | | | | | | | | | | |
| Actuated Cycle Length: 140 |) | | | | | | | | | | | |
| Ottset: 100 (71%), Referen | ced to phas | se 2:EBTL | . and 6:W | BIL, Sta | rt of Gree | n | | | | | | |

Natural Cycle: 155 Control Type: Actuated-Coordinated

Maximum v/c Ratio: 1.40 Intersection Signal Delay: 110.9

Intersection LOS: F

Intersection Capacity Utilization 105.6%

ICU Level of Service G

Analysis Period (min) 15

- Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

| Splits and Phases: | 1: Ninth Line & Dundas Street East |
|--------------------|------------------------------------|
|--------------------|------------------------------------|

| Ø1 | ■ → Ø2 (R) | Ø3 | 1 ₀₄ |
|---------|------------|-------------|-----------------|
| 20 s | 60 s | 20 s | 40 s |
| ▶ Ø5 | ● | 1 Ø7 | Ø8 |
| 20 s | 60 s | 20 s | 40 s |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | * | + | * | 1 | Ť | 1 | 1 | ţ | ~ |
|--------------------------------|------------|-------|--------|-------|------------|------------|---------|----------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | *** | 1 | ۲ | *** | 1 | 3 | ^ | 1 | ٦ | 44 | 1 |
| Traffic Volume (vph) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Future Volume (vph) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.12 | 1.00 | 1.00 | 0.07 | 1.00 | 1.00 | 0.14 | 1.00 | 1.00 | 0.39 | 1.00 | 1.00 |
| Satd. Flow (perm) | 207 | 5085 | 1491 | 116 | 4715 | 1449 | 231 | 3433 | 1422 | 663 | 3466 | 1478 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| RTOR Reduction (vph) | 0 | 0 | 115 | 0 | 0 | 86 | 0 | 0 | 146 | 0 | 0 | 131 |
| Lane Group Flow (vph) | 189 | 2946 | 289 | 197 | 1320 | 61 | 208 | 390 | 46 | 276 | 691 | 41 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 70.3 | 56.1 | 56.1 | 71.3 | 56.6 | 56.6 | 47.0 | 31.3 | 31.3 | 47.6 | 31.6 | 31.6 |
| Effective Green, g (s) | 76.3 | 58.0 | 58.0 | 77.3 | 58.5 | 58.5 | 53.0 | 33.3 | 33.3 | 53.6 | 33.6 | 33.6 |
| Actuated g/C Ratio | 0.54 | 0.41 | 0.41 | 0.55 | 0.42 | 0.42 | 0.38 | 0.24 | 0.24 | 0.38 | 0.24 | 0.24 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 297 | 2106 | 617 | 257 | 1970 | 605 | 261 | 816 | 338 | 385 | 831 | 354 |
| v/s Ratio Prot | 0.08 | c0.58 | | c0.10 | 0.28 | | c0.11 | 0.11 | | c0.10 | c0.20 | |
| v/s Ratio Perm | 0.27 | | 0.19 | 0.32 | | 0.04 | 0.19 | | 0.03 | 0.18 | | 0.03 |
| v/c Ratio | 0.64 | 1.40 | 0.47 | 0.77 | 0.67 | 0.10 | 0.80 | 0.48 | 0.14 | 0.72 | 0.83 | 0.12 |
| Uniform Delay, d1 | 20.9 | 41.0 | 29.8 | 40.8 | 32.9 | 24.8 | 33.8 | 45.9 | 42.0 | 32.5 | 50.5 | 41.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 4.6 | 182.4 | 2.5 | 13.2 | 1.8 | 0.3 | 15.8 | 0.5 | 0.2 | 6.5 | 7.3 | 0.2 |
| Delay (s) | 25.5 | 223.4 | 32.3 | 54.0 | 34.8 | 25.1 | 49.6 | 46.4 | 42.2 | 39.0 | 57.8 | 41.8 |
| Level of Service | С | F | С | D | С | С | D | D | D | D | Е | D |
| Approach Delay (s) | | 191.0 | | | 36.2 | | | 46.2 | | | 50.8 | |
| Approach LOS | | F | | | D | | | D | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 116.5 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capac | city ratio | | 1.06 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 140.0 | S | um of losi | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utilizat | tion | | 105.6% | IC | U Level | of Service |) | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

| | ≯ | - | 7 | 4 | + | • | 1 | Ť | 1 | 1 | ŧ | ~ |
|------------------------------|------|----------|-------|------|------|-------|------|----------|------|------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 1 | ^ | 1 | 7 | *** | 1 | ٦ | ^ | 1 | 7 | ^ | 1 |
| Traffic Volume (veh/h) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Future Volume (veh/h) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1856 | 1811 | 1752 | 1811 | 1682 | 1841 | 1739 | 1781 | 1856 | 1796 |
| Adj Flow Rate, veh/h | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 3 | 6 | 10 | 6 | 10 | 4 | 6 | 3 | 3 | 2 |
| Cap, veh/h | 311 | 2206 | 669 | 254 | 2179 | 688 | 292 | 801 | 338 | 392 | 826 | 357 |
| Arrive On Green | 0.09 | 0.43 | 0.43 | 0.12 | 0.46 | 0.46 | 0.13 | 0.23 | 0.23 | 0.14 | 0.23 | 0.23 |
| Sat Flow, veh/h | 1781 | 5106 | 1547 | 1725 | 4782 | 1510 | 1602 | 3497 | 1473 | 1696 | 3526 | 1522 |
| Grp Volume(v), veh/h | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1702 | 1547 | 1725 | 1594 | 1510 | 1602 | 1749 | 1473 | 1696 | 1763 | 1522 |
| Q Serve(g_s), s | 7.7 | 60.5 | 28.1 | 11.2 | 29.1 | 8.2 | 13.2 | 13.5 | 16.2 | 16.7 | 26.1 | 13.7 |
| Cycle Q Clear(g_c), s | 7.7 | 60.5 | 28.1 | 11.2 | 29.1 | 8.2 | 13.2 | 13.5 | 16.2 | 16.7 | 26.1 | 13.7 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 311 | 2206 | 669 | 254 | 2179 | 688 | 292 | 801 | 338 | 392 | 826 | 357 |
| V/C Ratio(X) | 0.61 | 1.34 | 0.60 | 0.78 | 0.61 | 0.21 | 0.71 | 0.49 | 0.57 | 0.70 | 0.84 | 0.48 |
| Avail Cap(c_a), veh/h | 386 | 2206 | 669 | 286 | 2179 | 688 | 300 | 874 | 368 | 392 | 881 | 380 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 22.0 | 39.8 | 30.6 | 42.3 | 28.7 | 23.0 | 35.5 | 46.8 | 47.8 | 33.0 | 51.0 | 46.3 |
| Incr Delay (d2), s/veh | 2.3 | 154.1 | 4.0 | 11.9 | 1.3 | 0.7 | 7.9 | 0.6 | 2.0 | 5.9 | 6.9 | 1.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 3.7 | 58.1 | 12.0 | 7.9 | 12.2 | 3.3 | 6.1 | 6.3 | 6.5 | 8.0 | 12.9 | 5.6 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 24.3 | 193.8 | 34.6 | 54.2 | 29.9 | 23.7 | 43.3 | 47.4 | 49.9 | 38.8 | 58.0 | 47.5 |
| LnGrp LOS | С | F | С | D | С | С | D | D | D | D | E | <u>D</u> |
| Approach Vol, veh/h | | 3539 | | | 1664 | | | 790 | | | 1139 | |
| Approach Delay, s/veh | | 166.6 | | | 32.2 | | | 46.9 | | | 51.8 | |
| Approach LOS | | F | | | С | | | D | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 17.4 | 65.5 | 20.0 | 37.1 | 14.2 | 68.8 | 19.3 | 37.8 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 16.0 | * 53 | 16.0 | 33.0 | 16.0 | * 53 | 16.0 | 33.0 | | | | |
| Max Q Clear Time (q c+l1), s | 13.2 | 63.5 | 18.7 | 18.2 | 9.7 | 31.1 | 15.2 | 28.1 | | | | |
| Green Ext Time (p_c), s | 0.2 | 0.0 | 0.0 | 3.8 | 0.4 | 17.9 | 0.1 | 2.7 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 103.6 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| | ٠ | 7 | 1 | Ť | ŧ | 1 |
|-------------------------------|------------|-------|------|-------|----------|--------------|
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y | | | -۠ | ħ | |
| Traffic Volume (vph) | 3 | 4 | 22 | 682 | 1064 | 5 |
| Future Volume (vph) | 3 | 4 | 22 | 682 | 1064 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.2 | 3.3 | 3.5 | 3.5 | 3.5 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 |
| Ped Bike Factor | | | | | | |
| Frt | 0.923 | | | | 0.999 | |
| Flt Protected | 0.979 | | | 0.998 | | |
| Satd. Flow (prot) | 1608 | 0 | 0 | 3428 | 1822 | 0 |
| Flt Permitted | 0.979 | | | 0.998 | | |
| Satd. Flow (perm) | 1608 | 0 | 0 | 3428 | 1822 | 0 |
| Link Speed (k/h) | 60 | | | 60 | 60 | |
| Link Distance (m) | 47.4 | | | 51.2 | 157.3 | |
| Travel Time (s) | 2.8 | | | 3.1 | 9.4 | |
| Confl. Bikes (#/hr) | | | | | | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 2% | 4% | 3% | 2% |
| Adj. Flow (vph) | 3 | 4 | 24 | 741 | 1157 | 5 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 7 | 0 | 0 | 765 | 1162 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.2 | | | 0.0 | 0.0 | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 3.0 | | | 3.0 | 3.0 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.06 | 1.06 | 1.04 | 1.01 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | 15 | 25 | | | 15 |
| Sign Control | Stop | | | Free | Free | |
| Intersection Summary | | | | | | |
| Area Type: | Other | | | | | |
| Control Type: Unsignalized | | | | | | |
| Intersection Capacity Utiliza | tion 66.3% | | | IC | CU Level | of Service C |

Analysis Period (min) 15

| | ۶ | 7 | 1 | Ť | Ļ | 4 | |
|-----------------------------------|------|------|-------|------|------------|-----------|---|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | Y | | | -۠ | ţ, | | |
| Traffic Volume (veh/h) | 3 | 4 | 22 | 682 | 1064 | 5 | |
| Future Volume (Veh/h) | 3 | 4 | 22 | 682 | 1064 | 5 | |
| Sign Control | Stop | | | Free | Free | | |
| Grade | 0% | | | 0% | 0% | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Hourly flow rate (vph) | 3 | 4 | 24 | 741 | 1157 | 5 | |
| Pedestrians | | | | | | | |
| Lane Width (m) | | | | | | | |
| Walking Speed (m/s) | | | | | | | |
| Percent Blockage | | | | | | | |
| Right turn flare (veh) | | | | | | | |
| Median type | | | | None | None | | |
| Median storage veh) | | | | | | | |
| Upstream signal (m) | | | | 147 | | | |
| pX, platoon unblocked | 0.91 | | | | | | |
| vC, conflicting volume | 1578 | 1160 | 1162 | | | | |
| vC1, stage 1 conf vol | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | 1432 | 1160 | 1162 | | | | |
| tC, single (s) | 6.8 | 6.9 | 4.1 | | | | |
| tC, 2 stage (s) | | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | | |
| p0 queue free % | 97 | 98 | 96 | | | | |
| cM capacity (veh/h) | 109 | 189 | 597 | | | | |
| Direction, Lane # | EB 1 | NB 1 | NB 2 | SB 1 | | | |
| Volume Total | 7 | 271 | 494 | 1162 | | | |
| Volume Left | 3 | 24 | 0 | 0 | | | |
| Volume Right | 4 | 0 | 0 | 5 | | | |
| cSH | 144 | 597 | 1700 | 1700 | | | |
| Volume to Capacity | 0.05 | 0.04 | 0.29 | 0.68 | | | |
| Queue Length 95th (m) | 1.1 | 0.9 | 0.0 | 0.0 | | | |
| Control Delay (s) | 31.3 | 1.5 | 0.0 | 0.0 | | | |
| Lane LOS | D | А | | | | | |
| Approach Delay (s) | 31.3 | 0.5 | | 0.0 | | | |
| Approach LOS | D | | | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 0.3 | | | | |
| Intersection Capacity Utilization | n | | 66.3% | IC | CU Level c | f Service | С |
| Analysis Period (min) | | | 15 | | | | |

| | ٠ | → | 7 | 1 | + | * | 1 | Ť | 1 | 1 | ţ | ~ |
|----------------------------|-------------|------------|-------|-------|------------|-------|-------|------------|-------|-------|------------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | *** | 1 | 7 | ^ | 1 | ۲ | ^ | 1 | 7 | ^ | 1 |
| Traffic Volume (vph) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Future Volume (vph) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.124 | | | 0.056 | | | 0.151 | | | 0.481 | | |
| Satd. Flow (perm) | 223 | 5085 | 1491 | 97 | 4715 | 1449 | 243 | 3433 | 1422 | 828 | 3466 | 1478 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 199 | | | 146 | | | 128 | | | 170 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 329.1 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 19.7 | | | 11.3 | | | 5.7 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| Shared Lane Traffic (%) | | | | | (| | | | 100 | | | |
| Lane Group Flow (vph) | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | | | 3.3 | | | 3.0 | | | 3.0 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| I wo way Lent Turn Lane | 1 0 1 | 1 00 | 1 07 | 1 0 4 | 1 00 | 1.07 | 1 00 | 1 01 | 1 00 | 1 00 | 1 01 | 1 00 |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (K/n) | 25 | C | 15 | 25 | 0 | 10 | 25 | 0 | 15 | 25 | 0 | 15 |
| Number of Detectors | 0# | Z | Diaht | l off | Z | Diaht | l off | Z | Diaht | l off | Z | Diaht |
| Leading Detector (m) | Leit 2.0 | 10.0 | Right | Leit | 10.0 | Right | Leit | 10.0 | Right | Leit | 10.0 | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Detector 1 Desition(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(III) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(iii) | | | | | | | | | | | | |
| Detector 1 Channel | | | | CI+EX | OI+EX | CI+EX | | UI+EX | CI+EX | | CI+EX | |
| Detector 1 Extend (c) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Size(m) | | 9.4 0.6 | | | 9.4 0.6 | | | 9.4 0.6 | | | 9.4 0.6 | |
| Detector 2 Type | | CI+Ev | | | CI±Ev | | | CI+Ev | | | | |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Deletion 2 Externa (3) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |

ZL

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|----------------------------|--------------|----------|----------|-------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 | 7.0 | 10.0 | 10.0 | 7.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 52.9 | 52.9 | 11.0 | 52.9 | 52.9 | 11.0 | 56.0 | 56.0 | 11.0 | 56.0 | 56.0 |
| Total Split (s) | 21.0 | 76.0 | 76.0 | 12.0 | 67.0 | 67.0 | 17.0 | 56.0 | 56.0 | 11.0 | 50.0 | 50.0 |
| Total Split (%) | 13.5% | 49.0% | 49.0% | 7.7% | 43.2% | 43.2% | 11.0% | 36.1% | 36.1% | 7.1% | 32.3% | 32.3% |
| Maximum Green (s) | 17.0 | 69.1 | 69.1 | 8.0 | 60.1 | 60.1 | 13.0 | 49.0 | 49.0 | 7.0 | 43.0 | 43.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.7 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 3.3 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | 15.0 | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | 34.0 | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Act Effct Green (s) | 89.1 | 71.0 | 71.0 | 88.4 | 70.6 | 70.6 | 60.3 | 45.3 | 45.3 | 53.3 | 39.3 | 39.3 |
| Actuated g/C Ratio | 0.57 | 0.46 | 0.46 | 0.57 | 0.46 | 0.46 | 0.39 | 0.29 | 0.29 | 0.34 | 0.25 | 0.25 |
| v/c Ratio | 0.65 | 1.26 | 0.51 | 0.89 | 0.62 | 0.20 | 0.92 | 0.39 | 0.38 | 0.82 | 0.79 | 0.34 |
| Control Delay | 28.5 | 159.0 | 16.6 | 79.8 | 34.6 | 4.9 | 75.8 | 44.4 | 16.3 | 60.1 | 60.6 | 7.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 28.5 | 159.0 | 16.6 | 79.8 | 34.6 | 4.9 | 75.8 | 44.4 | 16.3 | 60.1 | 60.6 | 7.7 |
| LOS | С | F | В | E | С | А | Е | D | В | E | E | А |
| Approach Delay | | 135.7 | | | 37.4 | | | 45.8 | | | 52.5 | |
| Approach LOS | | F | | | D | | | D | | | D | |
| Queue Length 50th (m) | 23.6 | ~383.2 | 39.5 | 42.2 | 103.9 | 0.2 | 41.2 | 46.3 | 13.4 | 56.8 | 96.2 | 0.4 |
| Queue Length 95th (m) | 45.3 | #403.1 | 67.3 | #104.7 | 129.4 | 13.0 | #77.7 | 57.5 | 32.1 | 76.4 | 112.3 | 16.6 |
| Internal Link Dist (m) | | 269.2 | | | 305.1 | | | 164.2 | | | 71.5 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 325 | 2329 | 790 | 221 | 2146 | 739 | 227 | 1129 | 553 | 337 | 1006 | 549 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.58 | 1.26 | 0.51 | 0.89 | 0.62 | 0.20 | 0.92 | 0.35 | 0.35 | 0.82 | 0.69 | 0.31 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 155 | | | | | | | | | | | | |
| Actuated Cycle Length: 15 | 5 | | | | | | | | | | | |
| Offset: 0 (0%), Referenced | I to phase 2 | :EBTL an | d 6:WBTI | L, Start of | Green | | | | | | | |
| Natural Cycle: 155 | | | | | | | | | | | | |
| Control Type: Actuated-Co | ordinated | | | | | | | | | | | |

Maximum v/c Ratio: 1.26 Intersection Signal Delay: 89.5

Intersection LOS: F

Intersection Capacity Utilization 105.6%

ICU Level of Service G

Analysis Period (min) 15

- Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Ninth Line & Dundas Street East

| 🖌 Ø1 🔶 ØŢ (R) | ▶ø3 1 ø4 |
|---------------|-------------------------|
| 12 s 76 s | 11 s 56 s |
| ▲ Ø5 Ø6 (R) | ↑ Ø7 ↓ Ø8 |
| 21 s 67 s | 17 s 50 s |

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|-----------------------------------|------------------------------|-------|--------|-------|------------------------|------------|---------|------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | *** | 1 | 5 | *** | 1 | 5 | ** | 1 | 5 | ^ | 1 |
| Traffic Volume (vph) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Future Volume (vph) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.12 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.15 | 1.00 | 1.00 | 0.48 | 1.00 | 1.00 |
| Satd. Flow (perm) | 224 | 5085 | 1491 | 97 | 4715 | 1449 | 243 | 3433 | 1422 | 828 | 3466 | 1478 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| RTOR Reduction (vph) | 0 | 0 | 108 | 0 | 0 | 79 | 0 | 0 | 91 | 0 | 0 | 127 |
| Lane Group Flow (vph) | 189 | 2946 | 296 | 197 | 1320 | 68 | 208 | 390 | 101 | 276 | 691 | 45 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 83.2 | 69.1 | 69.1 | 82.4 | 68.7 | 68.7 | 54.3 | 43.3 | 43.3 | 44.3 | 37.3 | 37.3 |
| Effective Green, g (s) | 89.2 | 71.0 | 71.0 | 88.4 | 70.6 | 70.6 | 57.3 | 45.3 | 45.3 | 50.3 | 39.3 | 39.3 |
| Actuated g/C Ratio | 0.58 | 0.46 | 0.46 | 0.57 | 0.46 | 0.46 | 0.37 | 0.29 | 0.29 | 0.32 | 0.25 | 0.25 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 292 | 2329 | 682 | 222 | 2147 | 659 | 222 | 1003 | 415 | 320 | 878 | 374 |
| v/s Ratio Prot | c0.07 | c0.58 | | c0.10 | 0.28 | | c0.10 | 0.11 | | 0.06 | 0.20 | |
| v/s Ratio Perm | 0.30 | | 0.20 | 0.41 | | 0.05 | 0.25 | | 0.07 | c0.22 | | 0.03 |
| v/c Ratio | 0.65 | 1.26 | 0.43 | 0.89 | 0.61 | 0.10 | 0.94 | 0.39 | 0.24 | 0.86 | 0.79 | 0.12 |
| Uniform Delay, d1 | 20.5 | 42.0 | 28.4 | 50.8 | 31.9 | 24.1 | 38.7 | 43.8 | 41.8 | 46.6 | 53.9 | 44.5 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 5.1 | 122.8 | 2.0 | 32.3 | 1.3 | 0.3 | 43.1 | 0.3 | 0.4 | 21.0 | 4.8 | 0.2 |
| Delay (s) | 25.6 | 164.8 | 30.4 | 83.1 | 33.2 | 24.4 | 81.8 | 44.1 | 42.2 | 67.6 | 58.8 | 44.7 |
| Level of Service | С | F | С | F | С | С | F | D | D | E | E | D |
| Approach Delay (s) | | 142.0 | | | 38.4 | | | 53.6 | | | 58.8 | |
| Approach LOS | | F | | | D | | | D | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 94.7 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capacit | ty ratio | | 1.06 | | | | | | | | | |
| Actuated Cycle Length (s) | uated Cycle Length (s) 155.0 | | | |) Sum of lost time (s) | | | | 12.0 | | | |
| Intersection Capacity Utilization | on | | 105.6% | IC | CU Level | of Service | 9 | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

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|------------------------------|------|-------|------|-------|------|-------|------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | *** | 1 | ٦ | *** | 1 | ٦ | ^ | 1 | 5 | ^ | 1 |
| Traffic Volume (veh/h) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Future Volume (veh/h) | 174 | 2710 | 372 | 181 | 1214 | 135 | 191 | 359 | 177 | 254 | 636 | 158 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1856 | 1811 | 1752 | 1811 | 1682 | 1841 | 1739 | 1781 | 1856 | 1796 |
| Adj Flow Rate, veh/h | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 3 | 6 | 10 | 6 | 10 | 4 | 6 | 3 | 3 | 2 |
| Cap, veh/h | 305 | 2572 | 779 | 169 | 2349 | 742 | 250 | 991 | 418 | 314 | 863 | 372 |
| Arrive On Green | 0.08 | 0.50 | 0.50 | 0.07 | 0.49 | 0.49 | 0.10 | 0.28 | 0.28 | 0.06 | 0.24 | 0.24 |
| Sat Flow, veh/h | 1781 | 5106 | 1547 | 1725 | 4782 | 1510 | 1602 | 3497 | 1473 | 1696 | 3526 | 1522 |
| Grp Volume(v), veh/h | 189 | 2946 | 404 | 197 | 1320 | 147 | 208 | 390 | 192 | 276 | 691 | 172 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1702 | 1547 | 1725 | 1594 | 1510 | 1602 | 1749 | 1473 | 1696 | 1763 | 1522 |
| Q Serve(g_s), s | 7.5 | 78.1 | 27.2 | 11.0 | 30.1 | 8.5 | 14.6 | 13.9 | 16.6 | 10.0 | 28.5 | 14.9 |
| Cycle Q Clear(g_c), s | 7.5 | 78.1 | 27.2 | 11.0 | 30.1 | 8.5 | 14.6 | 13.9 | 16.6 | 10.0 | 28.5 | 14.9 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 305 | 2572 | 779 | 169 | 2349 | 742 | 250 | 991 | 418 | 314 | 863 | 372 |
| V/C Ratio(X) | 0.62 | 1.15 | 0.52 | 1.17 | 0.56 | 0.20 | 0.83 | 0.39 | 0.46 | 0.88 | 0.80 | 0.46 |
| Avail Cap(c_a), veh/h | 386 | 2572 | 779 | 169 | 2349 | 742 | 250 | 1151 | 485 | 314 | 1024 | 442 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 21.2 | 38.5 | 25.8 | 52.1 | 27.7 | 22.2 | 40.1 | 44.8 | 45.8 | 51.2 | 55.0 | 49.8 |
| Incr Delay (d2), s/veh | 2.5 | 70.6 | 2.5 | 121.1 | 1.0 | 0.6 | 20.8 | 0.3 | 1.0 | 23.6 | 4.2 | 1.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 3.6 | 51.1 | 11.4 | 12.7 | 12.6 | 3.4 | 7.6 | 6.5 | 6.6 | 8.8 | 13.8 | 6.1 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 23.7 | 109.1 | 28.3 | 173.2 | 28.7 | 22.8 | 60.8 | 45.1 | 46.7 | 74.7 | 59.1 | 50.9 |
| LnGrp LOS | С | F | С | F | С | С | E | D | D | E | E | D |
| Approach Vol, veh/h | | 3539 | | | 1664 | | | 790 | | | 1139 | |
| Approach Delay, s/veh | | 95.3 | | | 45.3 | | | 49.6 | | | 61.7 | |
| Approach LOS | | F | | | D | | | D | | | E | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.0 | 83.1 | 11.0 | 48.9 | 13.9 | 81.1 | 17.0 | 42.9 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 8.0 | * 69 | 7.0 | 49.0 | 17.0 | * 60 | 13.0 | 43.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 13.0 | 81.1 | 12.0 | 18.6 | 9.5 | 32.1 | 16.6 | 30.5 | | | | |
| Green Ext Time (p_c), s | 0.0 | 0.0 | 0.0 | 4.9 | 0.5 | 21.8 | 0.0 | 5.4 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 73.2 | | | | | | | | | |
| HCM 6th LOS | | | Е | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|----------------------------|-------|----------|-------|-------|-------|-------|-------|-------|-------|-------|----------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 3 | *** | 1 | 5 | *** | 1 | 7 | 44 | 1 | ۲ | ^ | 1 |
| Traffic Volume (vph) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Future Volume (vph) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | | | 0.99 | | | | 1.00 | | | | | 0.99 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5036 | 1477 | 1694 | 5085 | 1506 | 1652 | 3500 | 1478 | 1652 | 3433 | 1478 |
| Flt Permitted | 0.067 | | | 0.068 | | | 0.368 | | | 0.111 | | |
| Satd. Flow (perm) | 121 | 5036 | 1455 | 121 | 5085 | 1506 | 640 | 3500 | 1478 | 193 | 3433 | 1459 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 172 | | | 123 | | | 246 | | | 180 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 329.1 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 19.7 | | | 11.3 | | | 5.7 | |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | | | 3.3 | | | 3.0 | | | 3.0 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | CI+Ex | Cl+Ex | CI+Ex | Cl+Ex | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | CI+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | CI+Ex | | | CI+Ex | | | Cl+Ex | | | CI+Ex | |

06-19-2023

| | ٠ | → | 7 | 1 | + | * | 1 | t | 1 | 1 | ŧ | ~ |
|------------------------------|------------|----------|---------|----------|------------|-------|--------|--------|--------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 7.0 | 20.0 | 20.0 | 7.0 | 20.0 | 20.0 | 7.0 | 10.0 | 10.0 | 7.0 | 10.0 | 10.0 |
| Minimum Split (s) | 11.0 | 52.9 | 52.9 | 11.0 | 52.9 | 52.9 | 11.0 | 56.0 | 56.0 | 11.0 | 56.0 | 56.0 |
| Total Split (s) | 20.0 | 60.0 | 60.0 | 20.0 | 60.0 | 60.0 | 20.0 | 40.0 | 40.0 | 20.0 | 40.0 | 40.0 |
| Total Split (%) | 14.3% | 42.9% | 42.9% | 14.3% | 42.9% | 42.9% | 14.3% | 28.6% | 28.6% | 14.3% | 28.6% | 28.6% |
| Maximum Green (s) | 16.0 | 53.1 | 53.1 | 16.0 | 53.1 | 53.1 | 16.0 | 33.0 | 33.0 | 16.0 | 33.0 | 33.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.7 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 3.3 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | 15.0 | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | 34.0 | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Act Effct Green (s) | 78.8 | 59.0 | 59.0 | 76.3 | 57.3 | 57.3 | 58.2 | 35.7 | 35.7 | 57.3 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.56 | 0.42 | 0.42 | 0.54 | 0.41 | 0.41 | 0.42 | 0.26 | 0.26 | 0.41 | 0.25 | 0.25 |
| v/c Ratio | 0.68 | 0.93 | 0.33 | 0.55 | 1.48 | 0.38 | 1.02 | 1.09 | 1.08 | 0.78 | 0.48 | 0.36 |
| Control Delav | 43.7 | 47.3 | 9.5 | 33.4 | 249.3 | 17.1 | 84.4 | 106.9 | 92.0 | 52.9 | 47.0 | 7.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 43.7 | 47.3 | 9.5 | 33.4 | 249.3 | 17.1 | 84.4 | 106.9 | 92.0 | 52.9 | 47.0 | 7.7 |
| LOS | D | D | A | С | F | В | F | F | F | D | D | А |
| Approach Delay | | 43.3 | | | 223.6 | | | 97.7 | | | 39.7 | |
| Approach LOS | | D | | | F | | | F | | | D | |
| Queue Length 50th (m) | 27.7 | 172.2 | 9.8 | 16.8 | ~398.8 | 24.2 | ~82.7 | ~149.6 | ~124.8 | 36.8 | 47.6 | 0.0 |
| Queue Length 95th (m) | 51.0 | #215.8 | 28.4 | 35.0 | #423.1 | 45.9 | #121.1 | #187.8 | #191.9 | #69.1 | 62.8 | 17.0 |
| Internal Link Dist (m) | | 269.2 | | | 305.1 | | | 164.2 | | | 71.5 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 284 | 2123 | 712 | 281 | 2081 | 689 | 403 | 892 | 560 | 277 | 858 | 499 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.61 | 0.93 | 0.33 | 0.46 | 1.48 | 0.38 | 1.02 | 1.09 | 1.08 | 0.75 | 0.48 | 0.36 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 140 | | | | | | | | | | | | |
| Actuated Cycle Length: 140 | | | | | | | | | | | | |
| Offset: 100 (71%), Reference | ed to phas | e 2:EBTL | and 6:W | BTL, Sta | rt of Gree | n | | | | | | |
| Natural Cycle: 155 | | | | | | | | | | | | |
| Control Type: Actuated-Coo | rdinated | | | | | | | | | | | |

| Maximum v/c Ratio: 1.48 | |
|--|------------------------|
| Intersection Signal Delay: 127.8 | Intersection LOS: F |
| Intersection Capacity Utilization 113.9% | ICU Level of Service H |
| Analysis Period (min) 15 | |
| ~ Volume exceeds capacity, queue is theoretically infinite. | |
| Queue shown is maximum after two cycles. | |
| # 95th percentile volume exceeds capacity, queue may be long | ger. |
| Queue shown is maximum after two cycles. | |
| | |
| Splits and Phases: 1: Ninth Line & Dundas Street East | |

| Ø1 | 🚽 👍 🛛 🖉 🖉 | | Ø3 | 1 Ø4 | |
|---------|------------|----|-----|-------------|--|
| 20 s | 60 s | 20 | Ds | 40 s | |
| ▶ Ø5 | 🛡 🖉 Ø6 (R) | | Ø7 | Ø8 | |
| 20 s | 60 s | 20 |) s | 40 s | |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٠ | → | 7 | 4 | + | * | 1 | t | 1 | 1 | Ŧ | ~ |
|---------------------------------------|-------------------------------------|----------|-------|-------|----------------------|------------|---------|----------|-------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | *** | 1 | 7 | *** | 1 | 3 | ^ | 1 | ۲ | ^ | 1 |
| Traffic Volume (vph) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Future Volume (vph) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.99 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5036 | 1455 | 1694 | 5085 | 1506 | 1651 | 3500 | 1478 | 1652 | 3433 | 1459 |
| Flt Permitted | 0.07 | 1.00 | 1.00 | 0.07 | 1.00 | 1.00 | 0.37 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 |
| Satd. Flow (perm) | 121 | 5036 | 1455 | 122 | 5085 | 1506 | 640 | 3500 | 1478 | 193 | 3433 | 1459 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| RTOR Reduction (vph) | 0 | 0 | 100 | 0 | 0 | 73 | 0 | 0 | 183 | 0 | 0 | 135 |
| Lane Group Flow (vph) | 174 | 1967 | 136 | 128 | 3073 | 191 | 411 | 975 | 424 | 209 | 414 | 45 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 70.8 | 57.1 | 57.1 | 67.4 | 55.4 | 55.4 | 49.7 | 33.7 | 33.7 | 48.3 | 33.0 | 33.0 |
| Effective Green, g (s) | 76.1 | 59.0 | 59.0 | 73.4 | 57.3 | 57.3 | 55.7 | 35.7 | 35.7 | 54.3 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.54 | 0.42 | 0.42 | 0.52 | 0.41 | 0.41 | 0.40 | 0.26 | 0.26 | 0.39 | 0.25 | 0.25 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 255 | 2122 | 613 | 232 | 2081 | 616 | 391 | 892 | 376 | 265 | 858 | 364 |
| v/s Ratio Prot | c0.08 | 0.39 | | 0.06 | c0.60 | | c0.14 | 0.28 | | 0.10 | 0.12 | |
| v/s Ratio Perm | 0.29 | | 0.09 | 0.23 | | 0.13 | 0.27 | | c0.29 | 0.20 | | 0.03 |
| v/c Ratio | 0.68 | 0.93 | 0.22 | 0.55 | 1.48 | 0.31 | 1.05 | 1.09 | 1.13 | 0.79 | 0.48 | 0.12 |
| Uniform Delay, d1 | 37.5 | 38.5 | 25.9 | 28.5 | 41.4 | 28.0 | 37.8 | 52.1 | 52.1 | 36.1 | 44.8 | 40.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 7.6 | 8.5 | 0.8 | 3.1 | 217.2 | 1.3 | 59.6 | 58.8 | 85.5 | 14.7 | 0.5 | 0.2 |
| Delay (s) | 45.1 | 47.0 | 26.7 | 31.6 | 258.5 | 29.3 | 97.4 | 110.9 | 137.7 | 50.8 | 45.3 | 40.8 |
| Level of Service | D | D | С | С | F | С | F | F | F | D | D | D |
| Approach Delay (s) | | 44.8 | | | 232.7 | | | 116.3 | | | 45.7 | |
| Approach LOS | | D | | | F | | | F | | | D | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 136.7 | Н | CM 2000 | Level of | Service | | F | | | |
| CM 2000 Volume to Capacity ratio 1.20 | | | | | | | | | | | | |
| Actuated Cycle Length (s) | Cycle Length (s) 140.0 | | | | Sum of lost time (s) | | | | 12.0 | | | |
| Intersection Capacity Utilization | section Capacity Utilization 113.9% | | | | U Level | of Service |) | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

| | ٠ | → | 7 | - | + | • | 1 | t | 1 | 1 | ŧ | ~ |
|------------------------------|------|----------|-------|------|-------|-------|------|----------|-------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | *** | 1 | ٦ | *** | 1 | ۲ | ^ | 1 | 5 | ^ | 7 |
| Traffic Volume (veh/h) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Future Volume (veh/h) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1841 | 1856 | 1870 | 1870 | 1796 | 1870 | 1796 | 1796 | 1841 | 1796 |
| Adj Flow Rate, veh/h | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 3 | 4 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 2 |
| Cap, veh/h | 235 | 2354 | 712 | 206 | 2232 | 680 | 397 | 888 | 380 | 267 | 835 | 363 |
| Arrive On Green | 0.10 | 0.46 | 0.46 | 0.08 | 0.44 | 0.44 | 0.14 | 0.25 | 0.25 | 0.12 | 0.24 | 0.24 |
| Sat Flow, veh/h | 1781 | 5066 | 1532 | 1767 | 5106 | 1556 | 1710 | 3554 | 1520 | 1710 | 3497 | 1520 |
| Grp Volume(v), veh/h | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1689 | 1532 | 1767 | 1702 | 1556 | 1710 | 1777 | 1520 | 1710 | 1749 | 1520 |
| Q Serve(g_s), s | 9.1 | 47.6 | 13.6 | 5.2 | 61.2 | 16.1 | 19.0 | 35.0 | 35.0 | 12.3 | 14.3 | 14.3 |
| Cycle Q Clear(g_c), s | 9.1 | 47.6 | 13.6 | 5.2 | 61.2 | 16.1 | 19.0 | 35.0 | 35.0 | 12.3 | 14.3 | 14.3 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 235 | 2354 | 712 | 206 | 2232 | 680 | 397 | 888 | 380 | 267 | 835 | 363 |
| V/C Ratio(X) | 0.74 | 0.84 | 0.33 | 0.62 | 1.38 | 0.39 | 1.04 | 1.10 | 1.60 | 0.78 | 0.50 | 0.50 |
| Avail Cap(c_a), veh/h | 294 | 2354 | 712 | 313 | 2232 | 680 | 397 | 888 | 380 | 286 | 874 | 380 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 40.8 | 32.8 | 23.7 | 29.7 | 39.4 | 26.7 | 40.3 | 52.5 | 52.5 | 35.8 | 46.0 | 46.0 |
| Incr Delay (d2), s/veh | 8.2 | 3.7 | 1.2 | 3.7 | 172.5 | 1.7 | 54.5 | 60.4 | 281.0 | 13.0 | 0.6 | 1.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 6.7 | 21.5 | 5.6 | 2.6 | 62.5 | 6.8 | 11.8 | 23.8 | 43.6 | 6.4 | 6.6 | 5.9 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 49.0 | 36.5 | 25.0 | 33.4 | 211.9 | 28.4 | 94.8 | 112.9 | 333.5 | 48.9 | 46.6 | 47.3 |
| LnGrp LOS | D | D | С | С | F | С | F | F | F | D | D | D |
| Approach Vol, veh/h | | 2377 | | | 3465 | | | 1993 | | | 803 | |
| Approach Delay, s/veh | | 36.3 | | | 191.3 | | | 176.4 | | | 47.3 | |
| Approach LOS | | D | | | F | | | F | | | D | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 11.5 | 70.1 | 18.4 | 40.0 | 15.4 | 66.2 | 20.0 | 38.4 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 16.0 | * 53 | 16.0 | 33.0 | 16.0 | * 53 | 16.0 | 33.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 7.2 | 50.6 | 14.3 | 37.0 | 11.1 | 63.2 | 21.0 | 16.3 | | | | |
| Green Ext Time (p_c), s | 0.3 | 2.5 | 0.2 | 0.0 | 0.3 | 0.0 | 0.0 | 4.1 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 131.8 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

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|--------------------------------|------------|-------|------|------------|------------|--------------|
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y | | | 4 † | ħ | |
| Traffic Volume (vph) | 11 | 38 | 23 | 1286 | 727 | 5 |
| Future Volume (vph) | 11 | 38 | 23 | 1286 | 727 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.2 | 3.3 | 3.5 | 3.5 | 3.5 |
| Lane Util. Factor | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 1.00 |
| Ped Bike Factor | | | | | | |
| Frt | 0.896 | | | | 0.999 | |
| Flt Protected | 0.989 | | | 0.999 | | |
| Satd. Flow (prot) | 1577 | 0 | 0 | 3496 | 1840 | 0 |
| Flt Permitted | 0.989 | | | 0.999 | | |
| Satd. Flow (perm) | 1577 | 0 | 0 | 3496 | 1840 | 0 |
| Link Speed (k/h) | 60 | | | 60 | 60 | |
| Link Distance (m) | 47.4 | | | 51.2 | 158.7 | |
| Travel Time (s) | 2.8 | | | 3.1 | 9.5 | |
| Confl. Peds. (#/hr) | | 2 | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 12 | 41 | 25 | 1398 | 790 | 5 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 53 | 0 | 0 | 1423 | 795 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.2 | | | 0.0 | 0.0 | - |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 3.0 | | | 3.0 | 3.0 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.06 | 1.06 | 1.04 | 1.01 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | 15 | 25 | | | 15 |
| Sign Control | Stop | | | Free | Free | |
| Intersection Summary | | | | | | |
| Area Type: 0 | Other | | | | | |
| Control Type: Unsignalized | | | | | | |
| Intersection Capacity Utilizat | tion 62.5% | | | IC | CU Level o | of Service E |
| Analysis Period (min) 15 | | | | | | |

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|----------------------------------|------|------|-------|--------------|------------|------------|---|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | Y | | | - € † | ¢Î, | | |
| Traffic Volume (veh/h) | 11 | 38 | 23 | 1286 | 727 | 5 | |
| Future Volume (Veh/h) | 11 | 38 | 23 | 1286 | 727 | 5 | |
| Sign Control | Stop | | | Free | Free | | |
| Grade | 0% | | | 0% | 0% | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Hourly flow rate (vph) | 12 | 41 | 25 | 1398 | 790 | 5 | |
| Pedestrians | | | | 2 | | | |
| Lane Width (m) | | | | 3.5 | | | |
| Walking Speed (m/s) | | | | 1.1 | | | |
| Percent Blockage | | | | 0 | | | |
| Right turn flare (veh) | | | | | | | |
| Median type | | | | None | None | | |
| Median storage veh) | | | | | | | |
| Upstream signal (m) | | | | 147 | | | |
| pX, platoon unblocked | 0.75 | | | | | | |
| vC, conflicting volume | 1542 | 794 | 795 | | | | |
| vC1, stage 1 conf vol | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | |
| vCu, unblocked vol | 1057 | 794 | 795 | | | | |
| tC, single (s) | 6.8 | 6.9 | 4.1 | | | | |
| tC, 2 stage (s) | | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | | |
| p0 queue free % | 93 | 88 | 97 | | | | |
| cM capacity (veh/h) | 160 | 330 | 822 | | | | |
| Direction, Lane # | EB 1 | NB 1 | NB 2 | SB 1 | | | |
| Volume Total | 53 | 491 | 932 | 795 | | | |
| Volume Left | 12 | 25 | 0 | 0 | | | |
| Volume Right | 41 | 0 | 0 | 5 | | | |
| cSH | 266 | 822 | 1700 | 1700 | | | |
| Volume to Capacity | 0.20 | 0.03 | 0.55 | 0.47 | | | |
| Queue Length 95th (m) | 5.1 | 0.7 | 0.0 | 0.0 | | | |
| Control Delay (s) | 21.9 | 0.9 | 0.0 | 0.0 | | | |
| Lane LOS | С | А | | | | | |
| Approach Delay (s) | 21.9 | 0.3 | | 0.0 | | | |
| Approach LOS | С | | | | | | |
| Intersection Summary | | | | | | | |
| Average Delay | | | 0.7 | | | | |
| Intersection Capacity Utilizatio | n | | 62.5% | IC | CU Level c | of Service | В |
| Analysis Period (min) | | | 15 | | | | |

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|----------------------------|-------|-----------|-------|-------|-------------|---------|-------|-----------|-------|-------|-----------|--------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 5 | *** | 1 | 5 | ** | 1 | 3 | ** | 1 |
| Traffic Volume (vph) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Future Volume (vph) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | 0.0 | 80.0 | 230.0 | 0.0 | 80.0 | 130.0 | 0.0 | 130.0 | 130.0 | 0.0 | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 55.0 | | - | 60.0 | | | 80.0 | | | 70.0 | | _ |
| Lane Util, Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | | 0.01 | 0.98 | | 0.0 | | 1.00 | 0.00 | | | 0.00 | 0.99 |
| Ert | | | 0.850 | | | 0 850 | | | 0 850 | | | 0 850 |
| Elt Protected | 0.950 | | 0.000 | 0 950 | | 0.000 | 0 950 | | 0.000 | 0 950 | | 0.000 |
| Satd Flow (prot) | 1711 | 5036 | 1477 | 1694 | 5085 | 1506 | 1652 | 3500 | 1478 | 1652 | 3433 | 1478 |
| Elt Permitted | 0.059 | 0000 | | 0.058 | 0000 | 1000 | 0.334 | 0000 | 1110 | 0 108 | 0100 | 1110 |
| Satd Flow (perm) | 106 | 5036 | 1455 | 103 | 5085 | 1506 | 580 | 3500 | 1478 | 188 | 3433 | 1459 |
| Right Turn on Red | 100 | 0000 | Yes | 100 | 0000 | Yes | 000 | 0000 | Yes | 100 | 0100 | Yes |
| Satd Flow (RTOR) | | | 156 | | | 126 | | | 54 | | | 136 |
| Link Speed (k/h) | | 70 | 100 | | 60 | 120 | | 60 | 01 | | 60 | 100 |
| Link Distance (m) | | 293.2 | | | 370.6 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 22.2 | | | 11.3 | | | 5.7 | |
| Confl Peds (#/hr) | | 10.1 | 3 | 3 | <i>LL.L</i> | | 1 | 11.0 | | | 0.1 | 1 |
| Peak Hour Factor | 0 92 | 0 92 | 0.92 | 0.92 | 0 92 | 0 92 | 0.92 | 0 92 | 0 92 | 0 92 | 0 92 | 0.92 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adi Flow (vph) | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| Shared Lane Traffic (%) | .,,, | 1001 | 200 | 120 | 0010 | 201 | | 010 | 001 | 200 | | 100 |
| Lane Group Flow (vph) | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | Lon | 3.3 | ragin | Lon | 3.3 | rtigitt | Lon | 3.0 | rught | Lon | 3.0 | rugitu |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Headway Factor | 1 04 | 1 00 | 1 07 | 1 04 | 1 00 | 1 07 | 1 09 | 1 01 | 1 09 | 1 09 | 1 01 | 1 09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | 1.01 | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | – Thru | Right | Left | Thru | Right | Left | – Thru | Right | Left | – Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | CI+Ex | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | CI+Ex | CI+Ex | Cl+Fx | CI+Ex | CI+Ex | Cl+Ex | CI+Ex |
| Detector 1 Channel | 01 24 | 01 24 | 01 24 | | 01 24 | 01 24 | 0. 2. | | | OI LA | 011 2/ | 01 24 |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 0.0 | 94 | 0.0 | 0.0 | 9.4 | 0.0 | 0.0 | 94 | 0.0 | 0.0 | 9.4 | 0.0 |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | CI+Ex | | | CI+Ex | | | CI+Ex | | | CI+Ex | |

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|-------------------------------|---------|----------|----------|-------------|--------|-------|--------|--------|--------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | - | 1 | 6 | | 7 | 4 | 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 1 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 9.0 | 52.9 | 52.9 | 9.0 | 52.9 | 52.9 | 9.0 | 56.0 | 9.0 | 9.0 | 56.0 | 56.0 |
| Total Split (s) | 9.0 | 71.0 | 71.0 | 20.0 | 82.0 | 82.0 | 28.0 | 51.0 | 20.0 | 18.0 | 41.0 | 41.0 |
| Total Split (%) | 5.6% | 44.4% | 44.4% | 12.5% | 51.3% | 51.3% | 17.5% | 31.9% | 12.5% | 11.3% | 25.6% | 25.6% |
| Maximum Green (s) | 5.0 | 64.1 | 64.1 | 16.0 | 75.1 | 75.1 | 24.0 | 44.0 | 16.0 | 14.0 | 34.0 | 34.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.0 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 1.0 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 2.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | | | 0 | 0 |
| Act Effct Green (s) | 79.2 | 67.2 | 67.2 | 90.0 | 77.0 | 77.0 | 68.0 | 46.0 | 67.8 | 57.0 | 36.0 | 36.0 |
| Actuated g/C Ratio | 0.50 | 0.42 | 0.42 | 0.56 | 0.48 | 0.48 | 0.42 | 0.29 | 0.42 | 0.36 | 0.22 | 0.22 |
| v/c Ratio | 1.32 | 0.93 | 0.34 | 0.54 | 1.26 | 0.33 | 0.96 | 0.97 | 0.92 | 0.94 | 0.54 | 0.42 |
| Control Delay | 219.0 | 53.3 | 12.0 | 39.3 | 154.7 | 14.0 | 72.3 | 77.6 | 60.3 | 90.4 | 57.6 | 17.7 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 219.0 | 53.3 | 12.0 | 39.3 | 154.7 | 14.0 | 72.3 | 77.6 | 60.3 | 90.4 | 57.6 | 17.7 |
| LOS | F | D | B | D | F | B | E | E | E | F | E | B |
| Approach Delay | | 61.3 | _ | _ | 139.7 | _ | | 71.3 | | | 57.2 | _ |
| Approach LOS | | E | | | F | | | E | | | E | |
| Queue Length 50th (m) | ~51.5 | 202.3 | 14.5 | 21.0 | ~411.0 | 23.3 | 91.6 | 149.4 | 154.0 | 47.0 | 56.8 | 10.4 |
| Queue Length 95th (m) | #97.6 | #223.4 | 33.6 | 41.5 | #429.3 | 42.3 | #134.8 | #189.6 | #224.4 | #94.4 | 73.3 | 31.8 |
| Internal Link Dist (m) | | 269.2 | | | 346.6 | | | 164.2 | | | 71.5 | •• |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | 0.010 | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 132 | 2114 | 701 | 246 | 2447 | 790 | 427 | 1006 | 668 | 222 | 772 | 433 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.32 | 0.93 | 0.34 | 0.52 | 1.26 | 0.33 | 0.96 | 0.97 | 0.91 | 0.94 | 0.54 | 0.42 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: C | Other | | | | | | | | | | | |
| Cycle Length: 160 | | | | | | | | | | | | |
| Actuated Cycle Length: 160 | | | | | | | | | | | | |
| Offset: 0 (0%), Referenced to | phase 2 | :EBTL an | d 6:WBTL | ., Start of | Green | | | | | | | |
| Natural Cycle: 160 | | | | | | | | | | | | |
| Control Type: Actuated-Coor | dinated | | | | | | | | | | | |
| Ма | iximum v/c Ratio: 1.32 | | | | | | | | | | |
|-----|--|------------------------|--|--|--|--|--|--|--|--|--|
| Int | ersection Signal Delay: 94.7 | Intersection LOS: F | | | | | | | | | |
| Int | ersection Capacity Utilization 113.9% | ICU Level of Service H | | | | | | | | | |
| An | alysis Period (min) 15 | | | | | | | | | | |
| ~ | Volume exceeds capacity, queue is theoretically infinite. | | | | | | | | | | |
| | Queue shown is maximum after two cycles. | | | | | | | | | | |
| # | 95th percentile volume exceeds capacity, queue may be long | ger. | | | | | | | | | |
| | Queue shown is maximum after two cycles. | | | | | | | | | | |
| Sp | lits and Phases: 1: Ninth Line & Dundas Street East | | | | | | | | | | |

| ₩ø1 | ₩ 102 (R) | Ø3 | ₩ Ø4 |
|----------|-----------|------------|-------------|
| 20 s | 71s | 18 s | 51s |
| Ø5 7 Ø6 | R) | Ø 7 | Ø8 |
| 9 s 82 s | | 28 s | 41 s |

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|-----------------------------------|--|------|--------|-------|----------|------------|---------|------|-------|-------|------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 5 | *** | 1 | 5 | ** | 1 | 5 | 44 | 1 |
| Traffic Volume (vph) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Future Volume (vph) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 2.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5036 | 1455 | 1694 | 5085 | 1506 | 1651 | 3500 | 1478 | 1652 | 3433 | 1459 |
| Flt Permitted | 0.06 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.33 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 |
| Satd. Flow (perm) | 105 | 5036 | 1455 | 103 | 5085 | 1506 | 581 | 3500 | 1478 | 188 | 3433 | 1459 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| RTOR Reduction (vph) | 0 | 0 | 90 | 0 | 0 | 65 | 0 | 0 | 33 | 0 | 0 | 105 |
| Lane Group Flow (vph) | 174 | 1967 | 146 | 128 | 3073 | 199 | 411 | 975 | 574 | 209 | 414 | 75 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | | 6 | | 7 | 4 | . 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 70.3 | 65.3 | 65.3 | 84.1 | 75.1 | 75.1 | 62.0 | 44.0 | 58.8 | 48.0 | 34.0 | 34.0 |
| Effective Green, g (s) | 76.3 | 67.2 | 67.2 | 87.1 | 77.0 | 77.0 | 65.0 | 46.0 | 62.8 | 54.0 | 36.0 | 36.0 |
| Actuated g/C Ratio | 0.48 | 0.42 | 0.42 | 0.54 | 0.48 | 0.48 | 0.41 | 0.29 | 0.39 | 0.34 | 0.22 | 0.22 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 4.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 130 | 2115 | 611 | 233 | 2447 | 724 | 416 | 1006 | 580 | 219 | 772 | 328 |
| v/s Ratio Prot | c0.07 | 0.39 | | 0.06 | 0.60 | | c0.17 | 0.28 | c0.10 | 0.10 | 0.12 | |
| v/s Ratio Perm | c0.57 | | 0.10 | 0.24 | | 0.13 | 0.23 | | 0.28 | 0.22 | | 0.05 |
| v/c Ratio | 1.34 | 0.93 | 0.24 | 0.55 | 1.26 | 0.27 | 0.99 | 0.97 | 0.99 | 0.95 | 0.54 | 0.23 |
| Uniform Delay, d1 | 44.9 | 44.2 | 29.9 | 37.7 | 41.5 | 24.8 | 40.9 | 56.3 | 48.3 | 46.6 | 54.6 | 50.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 195.1 | 8.8 | 0.9 | 2.9 | 118.6 | 0.9 | 40.6 | 21.1 | 34.5 | 47.9 | 0.8 | 0.4 |
| Delay (s) | 240.0 | 53.0 | 30.8 | 40.7 | 160.1 | 25.7 | 81.5 | 77.4 | 82.8 | 94.6 | 55.5 | 51.1 |
| Level of Service | F | D | С | D | F | С | F | E | F | F | E | D |
| Approach Delay (s) | | 64.5 | | | 145.5 | | | 79.9 | | | 64.6 | |
| Approach LOS | | Е | | | F | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 100.5 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capaci | HCM 2000 Volume to Capacity ratio 1.18 | | | | | | | | | | | |
| Actuated Cycle Length (s) | Actuated Cycle Length (s) 160.0 | | | | | t time (s) | | | 13.0 | | | |
| Intersection Capacity Utilization | on | | 113.9% | IC | CU Level | of Service | 9 | | Н | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

| | ٠ | - | 7 | 4 | + | • | 1 | Ť | 1 | 1 | ŧ | ~ |
|------------------------------|-------|-------|------|------|-------|-------|------|------|-------|------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | *** | 1 | 7 | *** | 1 | 7 | ** | 1 | ۲ | ^ | 1 |
| Traffic Volume (veh/h) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Future Volume (veh/h) | 160 | 1810 | 217 | 118 | 2827 | 243 | 378 | 897 | 558 | 192 | 381 | 166 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1841 | 1856 | 1870 | 1870 | 1796 | 1870 | 1796 | 1796 | 1841 | 1796 |
| Adj Flow Rate, veh/h | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 3 | 4 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 2 |
| Cap, veh/h | 134 | 2346 | 710 | 187 | 2457 | 749 | 434 | 1022 | 531 | 234 | 787 | 342 |
| Arrive On Green | 0.05 | 0.46 | 0.46 | 0.07 | 0.48 | 0.48 | 0.17 | 0.29 | 0.29 | 0.11 | 0.22 | 0.22 |
| Sat Flow, veh/h | 1781 | 5066 | 1532 | 1767 | 5106 | 1557 | 1710 | 3554 | 1520 | 1710 | 3497 | 1520 |
| Grp Volume(v), veh/h | 174 | 1967 | 236 | 128 | 3073 | 264 | 411 | 975 | 607 | 209 | 414 | 180 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1689 | 1532 | 1767 | 1702 | 1557 | 1710 | 1777 | 1520 | 1710 | 1749 | 1520 |
| Q Serve(g_s), s | 8.0 | 54.5 | 15.6 | 5.6 | 77.0 | 16.9 | 27.0 | 43.1 | 46.0 | 14.8 | 16.6 | 16.7 |
| Cycle Q Clear(g_c), s | 8.0 | 54.5 | 15.6 | 5.6 | 77.0 | 16.9 | 27.0 | 43.1 | 46.0 | 14.8 | 16.6 | 16.7 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 134 | 2346 | 710 | 187 | 2457 | 749 | 434 | 1022 | 531 | 234 | 787 | 342 |
| V/C Ratio(X) | 1.29 | 0.84 | 0.33 | 0.69 | 1.25 | 0.35 | 0.95 | 0.95 | 1.14 | 0.89 | 0.53 | 0.53 |
| Avail Cap(c_a), veh/h | 134 | 2346 | 710 | 276 | 2457 | 749 | 434 | 1022 | 531 | 234 | 787 | 342 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 48.7 | 37.7 | 27.3 | 34.4 | 41.5 | 25.9 | 40.7 | 56.0 | 52.1 | 44.2 | 54.5 | 54.5 |
| Incr Delay (d2), s/veh | 176.5 | 3.8 | 1.3 | 5.3 | 116.3 | 1.3 | 30.1 | 18.2 | 84.9 | 32.2 | 0.8 | 1.7 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(95%),veh/In | 19.5 | 32.9 | 10.6 | 5.1 | 85.8 | 11.5 | 13.2 | 30.6 | 48.4 | 13.6 | 12.4 | 11.2 |
| Unsig. Movement Delay, s/veh | I | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 225.3 | 41.5 | 28.5 | 39.7 | 157.8 | 27.2 | 70.8 | 74.2 | 136.9 | 76.4 | 55.3 | 56.2 |
| LnGrp LOS | F | D | С | D | F | С | E | E | F | E | E | <u> </u> |
| Approach Vol, veh/h | | 2377 | | | 3465 | | | 1993 | | | 803 | |
| Approach Delay, s/veh | | 53.6 | | | 143.5 | | | 92.6 | | | 61.0 | |
| Approach LOS | | D | | | F | | | F | | | E | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 11.9 | 79.1 | 18.0 | 51.0 | 9.0 | 82.0 | 28.0 | 41.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 16.0 | * 64 | 14.0 | 44.0 | 5.0 | * 75 | 24.0 | 34.0 | | | | |
| Max Q Clear Time (g c+I1), s | 7.6 | 57.5 | 16.8 | 48.0 | 10.0 | 79.0 | 29.0 | 18.7 | | | | |
| Green Ext Time (p_c), s | 0.3 | 6.5 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 4.0 | | | | |
| Intersection Summarv | | | | | | | | | | | | |
| HCM 6th Ctrl Delav | | | 99.3 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

User approved changes to right turn type.

Appendix M

2031 Future Background Synchro Intersection Worksheets



Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٠ | - | 7 | 1 | + | * | 1 | t | 1 | 4 | ŧ | ~ |
|----------------------------|-------|-----------------------|-------|-------|-----------------------|-------|-------|--------------|-------|-------|-----------------------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | *** | 1 | 7 | *** | 1 | 7 | ^ | 1 | 7 | ^ | 1 |
| Traffic Volume (vph) | 178 | 2865 | 390 | 195 | 1328 | 145 | 210 | 448 | 196 | 280 | 756 | 175 |
| Future Volume (vph) | 178 | 2865 | 390 | 195 | 1328 | 145 | 210 | 448 | 196 | 280 | 756 | 175 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd, Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.084 | | | 0.060 | | | 0.095 | | | 0.383 | | - |
| Satd, Flow (perm) | 151 | 5085 | 1491 | 104 | 4715 | 1449 | 153 | 3433 | 1422 | 659 | 3466 | 1478 |
| Right Turn on Red | - | | Yes | | | Yes | | | Yes | | | Yes |
| Satd, Flow (RTOR) | | | 196 | | | 136 | | | 120 | | | 145 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 427.0 | | | 188.2 | | | 146.7 | |
| Travel Time (s) | | 15.1 | | | 25.6 | | | 11.3 | | | 8.8 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adi, Flow (vph) | 193 | 3114 | 424 | 212 | 1443 | 158 | 228 | 487 | 213 | 304 | 822 | 190 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 193 | 3114 | 424 | 212 | 1443 | 158 | 228 | 487 | 213 | 304 | 822 | 190 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | | | 3.3 | | | 3.3 | | | 3.3 | - ign |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Riaht | Left | Thru | Riaht | Left | Thru | Riaht | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | CI+Ex | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | CI+Ex | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | Cl+Ex | CI+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | 0.0 | 9.4 | ••• | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | CI+Ex | | | CI+Ex | | | CI+Ex | | | CI+Ex | |
| Detector 2 Channel | | U . L A | | | C . E A | | | . . . | | | C . E A | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |

06-22-2023

Lanes, Volumes, Timings 1: Ninth Line & Dundas Street East

| | ٨ | + | 1 | 4 | Ļ | * | 1 | 1 | 1 | 4 | Ļ | ~ |
|----------------------------|--------------|----------|----------|-------------|------------|----------|-------|-------|-------|--------|--------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | - |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 9.0 | 52.9 | 52.9 | 9.0 | 52.9 | 52.9 | 9.0 | 56.0 | 56.0 | 9.0 | 56.0 | 56.0 |
| Total Split (s) | 25.0 | 80.0 | 80.0 | 12.0 | 67.0 | 67.0 | 23.0 | 51.0 | 51.0 | 17.0 | 45.0 | 45.0 |
| Total Split (%) | 15.6% | 50.0% | 50.0% | 7.5% | 41.9% | 41.9% | 14.4% | 31.9% | 31.9% | 10.6% | 28.1% | 28.1% |
| Maximum Green (s) | 21.0 | 73.1 | 73.1 | 8.0 | 60.1 | 60.1 | 19.0 | 44.0 | 44.0 | 13.0 | 38.0 | 38.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.7 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 3.3 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | 15.0 | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | 34.0 | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Act Effct Green (s) | 91.0 | 75.0 | 75.0 | 81.1 | 66.1 | 66.1 | 67.0 | 46.0 | 46.0 | 60.0 | 40.0 | 40.0 |
| Actuated g/C Ratio | 0.57 | 0.47 | 0.47 | 0.51 | 0.41 | 0.41 | 0.42 | 0.29 | 0.29 | 0.38 | 0.25 | 0.25 |
| v/c Ratio | 0.69 | 1.31 | 0.53 | 1.34 | 0.74 | 0.23 | 0.90 | 0.49 | 0.43 | 0.88 | 0.95 | 0.40 |
| Control Delay | 43.0 | 176.8 | 17.7 | 223.4 | 43.2 | 7.7 | 79.8 | 49.4 | 22.5 | 64.4 | 79.1 | 15.9 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 43.0 | 176.8 | 17.7 | 223.4 | 43.2 | 7.7 | 79.8 | 49.4 | 22.5 | 64.4 | 79.1 | 15.9 |
| LOS | D | F | В | F | D | А | Е | D | С | E | E | В |
| Approach Delay | | 151.8 | | | 61.2 | | | 50.7 | | | 66.6 | |
| Approach LOS | | F | | | Е | | | D | | | E | |
| Queue Length 50th (m) | 33.1 | ~427.2 | 45.8 | ~67.1 | 131.3 | 3.9 | 53.1 | 62.7 | 21.3 | 63.2 | 125.7 | 10.3 |
| Queue Length 95th (m) | 58.0 | #445.0 | 75.2 | #118.2 | 153.4 | 18.1 | #98.8 | 79.3 | 44.3 | #108.1 | #162.1 | 31.2 |
| Internal Link Dist (m) | | 269.2 | | | 403.0 | | | 164.2 | | | 122.7 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 319 | 2383 | 803 | 158 | 1947 | 678 | 253 | 986 | 494 | 344 | 866 | 478 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.61 | 1.31 | 0.53 | 1.34 | 0.74 | 0.23 | 0.90 | 0.49 | 0.43 | 0.88 | 0.95 | 0.40 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 160 | | | | | | | | | | | | |
| Actuated Cycle Length: 160 | | | | | | | | | | | | |
| Offset: 0 (0%), Reference | d to phase 2 | :EBTL an | d 6:WBTI | ., Start of | Green | | | | | | | |
| Natural Cycle: 160 | | | | | | | | | | | | |
| Control Type: Actuated-Co | oordinated | | | | | | | | | | | |
| Maximum v/c Ratio: 1.34 | | | | | | | | | | | | |
| Intersection Signal Delay: | 104.3 | | | li | ntersectio | n LOS: F | | | | | | |

Intersection Capacity Utilization 113.7%

ICU Level of Service H

Analysis Period (min) 15

- Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Ninth Line & Dundas Street East

| ✓ Ø1 + Ø2 (₩) | Ø3 Ø4 |
|---------------|-------------------------|
| 12 s 80 s | 17 s 51 s |
| ≠ Ø5 ♥ Ø6 (R) | ↑ Ø7 ↓ Ø8 |
| 25 s 67 s | 23 s 45 s |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٦ | - | 7 | * | + | * | 1 | Ť | 1 | 1 | ŧ | ~ |
|-----------------------------------|--|-------|------|-------|------------|------------|---------|------|------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | *** | 1 | 5 | *** | 1 | 5 | ** | 1 | ٦ | 44 | 1 |
| Traffic Volume (vph) | 178 | 2865 | 390 | 195 | 1328 | 145 | 210 | 448 | 196 | 280 | 756 | 175 |
| Future Volume (vph) | 178 | 2865 | 390 | 195 | 1328 | 145 | 210 | 448 | 196 | 280 | 756 | 175 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.08 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.10 | 1.00 | 1.00 | 0.38 | 1.00 | 1.00 |
| Satd. Flow (perm) | 151 | 5085 | 1491 | 103 | 4715 | 1449 | 154 | 3433 | 1422 | 659 | 3466 | 1478 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 193 | 3114 | 424 | 212 | 1443 | 158 | 228 | 487 | 213 | 304 | 822 | 190 |
| RTOR Reduction (vph) | 0 | 0 | 104 | 0 | 0 | 80 | 0 | 0 | 86 | 0 | 0 | 109 |
| Lane Group Flow (vph) | 193 | 3114 | 320 | 212 | 1443 | 78 | 228 | 487 | 128 | 304 | 822 | 81 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 85.1 | 73.1 | 73.1 | 72.2 | 64.2 | 64.2 | 61.0 | 44.0 | 44.0 | 51.0 | 38.0 | 38.0 |
| Effective Green, g (s) | 88.1 | 75.0 | 75.0 | 78.2 | 66.1 | 66.1 | 64.0 | 46.0 | 46.0 | 57.0 | 40.0 | 40.0 |
| Actuated g/C Ratio | 0.55 | 0.47 | 0.47 | 0.49 | 0.41 | 0.41 | 0.40 | 0.29 | 0.29 | 0.36 | 0.25 | 0.25 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 277 | 2383 | 698 | 156 | 1947 | 598 | 251 | 986 | 408 | 332 | 866 | 369 |
| v/s Ratio Prot | 0.09 | c0.61 | | c0.09 | 0.31 | | c0.12 | 0.14 | | c0.09 | c0.24 | |
| v/s Ratio Perm | 0.30 | | 0.21 | c0.57 | | 0.05 | 0.24 | | 0.09 | 0.23 | | 0.05 |
| v/c Ratio | 0.70 | 1.31 | 0.46 | 1.36 | 0.74 | 0.13 | 0.91 | 0.49 | 0.31 | 0.92 | 0.95 | 0.22 |
| Uniform Delay, d1 | 34.9 | 42.5 | 28.8 | 49.7 | 39.7 | 29.1 | 48.4 | 47.3 | 44.6 | 44.9 | 59.0 | 47.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 7.7 | 141.2 | 2.2 | 197.3 | 2.6 | 0.5 | 33.7 | 0.5 | 0.5 | 29.1 | 19.3 | 0.4 |
| Delay (s) | 42.5 | 183.7 | 30.9 | 247.0 | 42.3 | 29.6 | 82.1 | 47.8 | 45.1 | 74.0 | 78.3 | 48.0 |
| Level of Service | D | F | С | F | D | С | F | D | D | E | Е | D |
| Approach Delay (s) | | 159.0 | | | 65.1 | | | 55.6 | | | 72.9 | |
| Approach LOS | Approach LOS F | | | | Е | | | Е | | | Е | |
| Intersection Summary | | | | | | | | | | | | |
| ICM 2000 Control Delay | | | | H | CM 2000 | Level of | Service | | F | | | |
| CM 2000 Volume to Capacity ratio | | | 1.14 | | | | | | | | | |
| Actuated Cycle Length (s) | ctuated Cycle Length (s) 16 | | | S | um of lost | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utilization | Intersection Capacity Utilization 113. | | | | CU Level | of Service | 9 | | Н | | | |
| Analysis Period (min) | 15 | | | | | | | | | | | |

c Critical Lane Group

HCM 6th Signalized Intersection Summary 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | 4 | ← | • | 1 | Ť | 1 | 1 | Ļ | ~ |
|------------------------------|------|-------|-------|-------|------|-------|------|----------|------|------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | *** | 1 | 7 | *** | 1 | 7 | ^ | 1 | ۲ | ^ | 1 |
| Traffic Volume (veh/h) | 178 | 2865 | 390 | 195 | 1328 | 145 | 210 | 448 | 196 | 280 | 756 | 175 |
| Future Volume (veh/h) | 178 | 2865 | 390 | 195 | 1328 | 145 | 210 | 448 | 196 | 280 | 756 | 175 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1856 | 1811 | 1752 | 1811 | 1682 | 1841 | 1739 | 1781 | 1856 | 1796 |
| Adj Flow Rate, veh/h | 193 | 3114 | 424 | 212 | 1443 | 158 | 228 | 487 | 213 | 304 | 822 | 190 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 3 | 6 | 10 | 6 | 10 | 4 | 6 | 3 | 3 | 2 |
| Cap, veh/h | 274 | 2418 | 733 | 164 | 2171 | 686 | 272 | 989 | 417 | 338 | 881 | 380 |
| Arrive On Green | 0.09 | 0.47 | 0.47 | 0.07 | 0.45 | 0.45 | 0.13 | 0.28 | 0.28 | 0.10 | 0.25 | 0.25 |
| Sat Flow, veh/h | 1781 | 5106 | 1547 | 1725 | 4782 | 1510 | 1602 | 3497 | 1473 | 1696 | 3526 | 1522 |
| Grp Volume(v), veh/h | 193 | 3114 | 424 | 212 | 1443 | 158 | 228 | 487 | 213 | 304 | 822 | 190 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1702 | 1547 | 1725 | 1594 | 1510 | 1602 | 1749 | 1473 | 1696 | 1763 | 1522 |
| Q Serve(g_s), s | 8.5 | 75.8 | 31.8 | 11.0 | 37.8 | 10.2 | 16.1 | 18.6 | 19.4 | 16.0 | 36.5 | 17.1 |
| Cycle Q Clear(g_c), s | 8.5 | 75.8 | 31.8 | 11.0 | 37.8 | 10.2 | 16.1 | 18.6 | 19.4 | 16.0 | 36.5 | 17.1 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 274 | 2418 | 733 | 164 | 2171 | 686 | 272 | 989 | 417 | 338 | 881 | 380 |
| V/C Ratio(X) | 0.71 | 1.29 | 0.58 | 1.30 | 0.66 | 0.23 | 0.84 | 0.49 | 0.51 | 0.90 | 0.93 | 0.50 |
| Avail Cap(c_a), veh/h | 384 | 2418 | 733 | 164 | 2171 | 686 | 279 | 1005 | 424 | 338 | 881 | 380 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 28.5 | 42.1 | 30.5 | 52.3 | 34.2 | 26.6 | 40.1 | 47.8 | 48.1 | 47.1 | 58.7 | 51.4 |
| Incr Delay (d2), s/veh | 4.0 | 132.8 | 3.3 | 170.7 | 1.6 | 0.8 | 19.8 | 0.5 | 1.2 | 26.0 | 16.5 | 1.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 4.2 | 63.2 | 13.4 | 14./ | 16.0 | 4.2 | 8.1 | 8.6 | 1.1 | 7.9 | 19.0 | 7.0 |
| Unsig. Movement Delay, s/veh | 00.0 | 175.0 | 00.0 | 000.0 | 05.0 | 07.4 | 50.0 | 40.0 | 40.0 | 70.4 | 75.0 | 50.0 |
| LnGrp Delay(d),s/veh | 32.6 | 1/5.0 | 33.9 | 222.9 | 35.8 | 27.4 | 59.9 | 48.3 | 49.3 | /3.1 | 75.2 | 52.6 |
| LnGrp LOS | C | | C | F | D | C | E | | D | E | E | <u>D</u> |
| Approach Vol, veh/h | | 3731 | | | 1813 | | | 928 | | | 1316 | |
| Approach Delay, s/veh | | 151.6 | | | 56.9 | | | 51.4 | | | /1.4 | |
| Approach LOS | | F | | | E | | | D | | | E | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.0 | 80.8 | 17.0 | 50.2 | 15.1 | 77.6 | 22.2 | 45.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 8.0 | * 73 | 13.0 | 44.0 | 21.0 | * 60 | 19.0 | 38.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 13.0 | 78.8 | 18.0 | 21.4 | 10.5 | 39.8 | 18.1 | 38.5 | | | | |
| Green Ext Time (p_c), s | 0.0 | 0.0 | 0.0 | 5.6 | 0.6 | 17.5 | 0.1 | 0.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 104.1 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| | ٠ | 7 | 1 | Ť | ŧ | 4 |
|--------------------------------|-----------|-------|-------|----------|------------|--------------|
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR |
| Lane Configurations | Y | | 7 | ^ | † Ъ | |
| Traffic Volume (vph) | 3 | 4 | 25 | 850 | 1264 | 6 |
| Future Volume (vph) | 3 | 4 | 25 | 850 | 1264 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.2 | 3.3 | 3.5 | 3.5 | 3.5 |
| Storage Length (m) | 0.0 | 0.0 | 30.0 | | | 0.0 |
| Storage Lanes | 1 | 0 | 1 | | | 0 |
| Taper Length (m) | 15.0 | | 15.0 | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 |
| Ped Bike Factor | | | | | | |
| Frt | 0.923 | | | | 0.999 | |
| Flt Protected | 0.979 | | 0.950 | | | |
| Satd. Flow (prot) | 1608 | 0 | 1711 | 3433 | 3463 | 0 |
| Flt Permitted | 0.979 | | 0.950 | | | |
| Satd. Flow (perm) | 1608 | 0 | 1711 | 3433 | 3463 | 0 |
| Link Speed (k/h) | 60 | | | 60 | 60 | |
| Link Distance (m) | 47.4 | | | 146.7 | 158.7 | |
| Travel Time (s) | 2.8 | | | 8.8 | 9.5 | |
| Confl. Bikes (#/hr) | | | | | | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 2% | 4% | 3% | 2% |
| Adj. Flow (vph) | 3 | 4 | 27 | 924 | 1374 | 7 |
| Shared Lane Traffic (%) | | | | | | |
| Lane Group Flow (vph) | 7 | 0 | 27 | 924 | 1381 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No |
| Lane Alignment | Left | Right | Left | Left | Left | Right |
| Median Width(m) | 3.2 | | | 3.3 | 3.3 | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | |
| Crosswalk Width(m) | 3.0 | | | 3.0 | 3.0 | |
| Two way Left Turn Lane | | | | | | |
| Headway Factor | 1.06 | 1.06 | 1.04 | 1.01 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | 15 | 25 | | | 15 |
| Sign Control | Stop | | | Free | Free | |
| Intersection Summary | | | | | | |
| Area Type: 0 | Other | | | | | |
| Control Type: Unsignalized | | | | | | |
| Intersection Capacity Utilizat | ion 45.1% | | | IC | CU Level o | of Service A |
| Analysis Period (min) 15 | | | | | | |

| | ٠ | 7 | 1 | Ť | Ļ | ~ | | |
|-----------------------------------|------|------|-------|------|------------|------------|--|--|
| Movement | EBL | EBR | NBL | NBT | SBT | SBR | | |
| Lane Configurations | ¥ | | 5 | ** | † Ъ | | | |
| Traffic Volume (veh/h) | 3 | 4 | 25 | 850 | 1264 | 6 | | |
| Future Volume (Veh/h) | 3 | 4 | 25 | 850 | 1264 | 6 | | |
| Sign Control | Stop | | | Free | Free | | | |
| Grade | 0% | | | 0% | 0% | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | | |
| Hourly flow rate (vph) | 3 | 4 | 27 | 924 | 1374 | 7 | | |
| Pedestrians | | | | | | | | |
| Lane Width (m) | | | | | | | | |
| Walking Speed (m/s) | | | | | | | | |
| Percent Blockage | | | | | | | | |
| Right turn flare (veh) | | | | | | | | |
| Median type | | | | None | None | | | |
| Median storage veh) | | | | | | | | |
| Upstream signal (m) | | | | 147 | | | | |
| pX, platoon unblocked | 0.89 | | | | | | | |
| vC, conflicting volume | 1894 | 690 | 1381 | | | | | |
| vC1, stage 1 conf vol | | | | | | | | |
| vC2, stage 2 conf vol | | | | | | | | |
| vCu, unblocked vol | 1753 | 690 | 1381 | | | | | |
| tC, single (s) | 6.8 | 6.9 | 4.1 | | | | | |
| tC, 2 stage (s) | | | | | | | | |
| tF (s) | 3.5 | 3.3 | 2.2 | | | | | |
| p0 queue free % | 95 | 99 | 95 | | | | | |
| cM capacity (veh/h) | 64 | 387 | 492 | | | | | |
| Direction, Lane # | EB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | | |
| Volume Total | 7 | 27 | 462 | 462 | 916 | 465 | | |
| Volume Left | 3 | 27 | 0 | 0 | 0 | 0 | | |
| Volume Right | 4 | 0 | 0 | 0 | 0 | 7 | | |
| cSH | 123 | 492 | 1700 | 1700 | 1700 | 1700 | | |
| Volume to Capacity | 0.06 | 0.05 | 0.27 | 0.27 | 0.54 | 0.27 | | |
| Queue Length 95th (m) | 1.3 | 1.2 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Control Delay (s) | 36.1 | 12.7 | 0.0 | 0.0 | 0.0 | 0.0 | | |
| Lane LOS | E | В | | | | | | |
| Approach Delay (s) | 36.1 | 0.4 | | | 0.0 | | | |
| Approach LOS | E | | | | | | | |
| Intersection Summary | | | | | | | | |
| Average Delay | | | 0.3 | | | | | |
| Intersection Capacity Utilization | on | | 45.1% | IC | CU Level o | of Service | | |
| Analysis Period (min) | | | 15 | | | | | |

Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٠ | → | 7 | 4 | + | • | 1 | Ť | 1 | 1 | ţ | ~ |
|----------------------------|-------|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 5 | *** | 1 | 5 | 44 | 1 | 5 | ** | 1 |
| Traffic Volume (vph) | 172 | 1986 | 229 | 127 | 3102 | 262 | 416 | 1040 | 617 | 212 | 475 | 183 |
| Future Volume (vph) | 172 | 1986 | 229 | 127 | 3102 | 262 | 416 | 1040 | 617 | 212 | 475 | 183 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 55.0 | | | 60.0 | | | 80.0 | | | 70.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | | | 0.98 | | | | 1.00 | | | | | 0.99 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5036 | 1477 | 1694 | 5085 | 1506 | 1652 | 3500 | 1478 | 1652 | 3433 | 1478 |
| Flt Permitted | 0.057 | | | 0.056 | | | 0.207 | | | 0.121 | | |
| Satd. Flow (perm) | 103 | 5036 | 1455 | 100 | 5085 | 1506 | 360 | 3500 | 1478 | 210 | 3433 | 1459 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 155 | | | 124 | | | 54 | | | 136 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 455.7 | | | 188.2 | | | 146.7 | |
| Travel Time (s) | | 15.1 | | | 27.3 | | | 11.3 | | | 8.8 | |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 187 | 2159 | 249 | 138 | 3372 | 285 | 452 | 1130 | 671 | 230 | 516 | 199 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 187 | 2159 | 249 | 138 | 3372 | 285 | 452 | 1130 | 671 | 230 | 516 | 199 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | | | 3.3 | | | 3.3 | | | 3.3 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | CI+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | Cl+Ex | CI+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | CI+Ex | | | CI+Ex | | | CI+Ex | | | Cl+Ex | |

06-22-2023

Lanes, Volumes, Timings 1: Ninth Line & Dundas Street East

| | ٨ | + | 1 | 1 | Ļ | * | • | 1 | 1 | * | ţ | ~ |
|------------------------------|-----------|----------|----------|-------------|--------|-------|--------|--------|--------|--------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | . 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 1 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 9.0 | 52.9 | 52.9 | 9.0 | 52.9 | 52.9 | 9.0 | 56.0 | 9.0 | 9.0 | 56.0 | 56.0 |
| Total Split (s) | 9.0 | 74.0 | 74.0 | 17.0 | 82.0 | 82.0 | 32.0 | 57.0 | 17.0 | 12.0 | 37.0 | 37.0 |
| Total Split (%) | 5.6% | 46.3% | 46.3% | 10.6% | 51.3% | 51.3% | 20.0% | 35.6% | 10.6% | 7.5% | 23.1% | 23.1% |
| Maximum Green (s) | 5.0 | 67.1 | 67.1 | 13.0 | 75.1 | 75.1 | 28.0 | 50.0 | 13.0 | 8.0 | 30.0 | 30.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.0 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 1.0 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 2.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | | | 0 | 0 |
| Act Effct Green (s) | 81.0 | 69.0 | 69.0 | 90.0 | 77.0 | 77.0 | 68.0 | 52.0 | 72.0 | 47.0 | 32.0 | 32.0 |
| Actuated g/C Ratio | 0.51 | 0.43 | 0.43 | 0.56 | 0.48 | 0.48 | 0.42 | 0.32 | 0.45 | 0.29 | 0.20 | 0.20 |
| v/c Ratio | 1.42 | 0.99 | 0.35 | 0.64 | 1.38 | 0.36 | 1.12 | 0.99 | 0.97 | 1.44 | 0.75 | 0.50 |
| Control Delay | 256.3 | 62.9 | 12.3 | 48.2 | 206.5 | 15.4 | 118.5 | 78.4 | 66.1 | 260.7 | 68.1 | 23.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 256.3 | 62.9 | 12.3 | 48.2 | 206.5 | 15.4 | 118.5 | 78.4 | 66.1 | 260.7 | 68.1 | 23.3 |
| LOS | F | E | В | D | F | В | F | E | E | F | E | С |
| Approach Delay | | 72.0 | | | 186.4 | | | 82.8 | | | 105.6 | |
| Approach LOS | | E | | | F | | | F | | | F | |
| Queue Length 50th (m) | ~59.1 | 228.9 | 16.6 | 24.7 | ~477.5 | 28.0 | ~126.4 | 174.1 | 179.1 | ~76.6 | 75.8 | 15.6 |
| Queue Length 95th (m) | #107.0 | #263.2 | 36.3 | 46.9 | #493.3 | 48.1 | #190.3 | #218.5 | #257.6 | #127.6 | 95.2 | 39.6 |
| Internal Link Dist (m) | | 269.2 | | | 431.7 | | | 164.2 | | | 122.7 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 132 | 2171 | 715 | 215 | 2447 | 789 | 403 | 1137 | 694 | 160 | 686 | 400 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.42 | 0.99 | 0.35 | 0.64 | 1.38 | 0.36 | 1.12 | 0.99 | 0.97 | 1.44 | 0.75 | 0.50 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 160 | | | | | | | | | | | | |
| Actuated Cycle Length: 160 | | | | | | | | | | | | |
| Offset: 0 (0%), Referenced t | o phase 2 | :EBTL an | d 6:WBTL | ., Start of | Green | | | | | | | |

Natural Cycle: 160

Control Type: Actuated-Coordinated

| Maximum v/c Ratio: 1.44 | |
|---|------------------------|
| Intersection Signal Delay: 123.1 | Intersection LOS: F |
| Intersection Capacity Utilization 125.0% | ICU Level of Service H |
| Analysis Period (min) 15 | |
| Volume exceeds capacity, queue is theoretically infinite. | |
| Queue shown is maximum after two cycles. | |
| # 95th percentile volume exceeds capacity, queue may be lo | nger. |
| Queue shown is maximum after two cycles. | |
| | |

Splits and Phases: 1: Ninth Line & Dundas Street East

| 1 Ø1 | ₩ Ø2 (R) | Ø3 | ▲ ¶ _{Ø4} |
|-------------|----------|--------|--------------------------|
| 17 s | 74s | 12 s 👘 | 57 s |
| 105 | 16 (R) | 07 | Ø8 |
| 9 s 82 s | | 32 s | 37 s |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | 1 | • | • | 1 | Ť | 1 | 4 | ţ | ~ |
|--|-------|------|--------|-------|-----------|------------|---------|------|-------|-------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 5 | *** | 1 | 3 | 44 | 1 | 5 | 44 | 1 |
| Traffic Volume (vph) | 172 | 1986 | 229 | 127 | 3102 | 262 | 416 | 1040 | 617 | 212 | 475 | 183 |
| Future Volume (vph) | 172 | 1986 | 229 | 127 | 3102 | 262 | 416 | 1040 | 617 | 212 | 475 | 183 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 2.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5036 | 1455 | 1694 | 5085 | 1506 | 1652 | 3500 | 1478 | 1652 | 3433 | 1459 |
| Flt Permitted | 0.06 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.21 | 1.00 | 1.00 | 0.12 | 1.00 | 1.00 |
| Satd. Flow (perm) | 103 | 5036 | 1455 | 100 | 5085 | 1506 | 360 | 3500 | 1478 | 211 | 3433 | 1459 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 187 | 2159 | 249 | 138 | 3372 | 285 | 452 | 1130 | 671 | 230 | 516 | 199 |
| RTOR Reduction (vph) | 0 | 0 | 88 | 0 | 0 | 64 | 0 | 0 | 31 | 0 | 0 | 109 |
| Lane Group Flow (vph) | 187 | 2159 | 161 | 138 | 3372 | 221 | 452 | 1130 | 640 | 230 | 516 | 90 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 72.1 | 67.1 | 67.1 | 84.1 | 75.1 | 75.1 | 62.0 | 50.0 | 63.0 | 38.0 | 30.0 | 30.0 |
| Effective Green, g (s) | 78.1 | 69.0 | 69.0 | 87.1 | 77.0 | 77.0 | 65.0 | 52.0 | 67.0 | 44.0 | 32.0 | 32.0 |
| Actuated g/C Ratio | 0.49 | 0.43 | 0.43 | 0.54 | 0.48 | 0.48 | 0.41 | 0.32 | 0.42 | 0.28 | 0.20 | 0.20 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 4.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 130 | 2171 | 627 | 213 | 2447 | 724 | 396 | 1137 | 618 | 157 | 686 | 291 |
| v/s Ratio Prot | c0.07 | 0.43 | | 0.06 | 0.66 | | c0.22 | 0.32 | c0.10 | c0.10 | 0.15 | |
| v/s Ratio Perm | c0.63 | | 0.11 | 0.29 | | 0.15 | 0.24 | | 0.34 | c0.30 | | 0.06 |
| v/c Ratio | 1.44 | 0.99 | 0.26 | 0.65 | 1.38 | 0.30 | 1.14 | 0.99 | 1.03 | 1.46 | 0.75 | 0.31 |
| Uniform Delay, d1 | 45.5 | 45.3 | 29.1 | 43.0 | 41.5 | 25.2 | 41.7 | 53.8 | 46.5 | 51.5 | 60.3 | 54.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 235.4 | 18.1 | 1.0 | 6.9 | 172.7 | 1.1 | 89.7 | 25.1 | 45.5 | 240.6 | 4.8 | 0.7 |
| Delay (s) | 280.9 | 63.4 | 30.1 | 49.9 | 214.2 | 26.3 | 131.3 | 78.9 | 92.0 | 292.1 | 65.1 | 55.3 |
| Level of Service | F | E | С | D | F | С | F | E | F | F | E | E |
| Approach Delay (s) | | 75.9 | | | 194.2 | | | 93.3 | | | 118.3 | |
| Approach LOS | | E | | | F | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 131.0 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capacity ratio 1.38 | | | | | | | | | | | | |
| Actuated Cycle Length (s) | | | 160.0 | S | um of los | t time (s) | | | 13.0 | | | |
| Intersection Capacity Utilizati | ion | | 125.0% | IC | U Level | of Service |) | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM 6th Signalized Intersection Summary 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | - | ← | • | 1 | Ť | 1 | 4 | ŧ | ~ |
|------------------------------|-------|-------|-------|------|-------|-------|-------|------------|-------|-------|----------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | *** | 1 | 7 | *** | 1 | 7 | † † | 1 | 2 | ^ | 1 |
| Traffic Volume (veh/h) | 172 | 1986 | 229 | 127 | 3102 | 262 | 416 | 1040 | 617 | 212 | 475 | 183 |
| Future Volume (veh/h) | 172 | 1986 | 229 | 127 | 3102 | 262 | 416 | 1040 | 617 | 212 | 475 | 183 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1841 | 1856 | 1870 | 1870 | 1796 | 1870 | 1796 | 1796 | 1841 | 1796 |
| Adj Flow Rate, veh/h | 187 | 2159 | 249 | 138 | 3372 | 285 | 452 | 1130 | 671 | 230 | 516 | 199 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 3 | 4 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 2 |
| Cap, veh/h | 134 | 2293 | 694 | 190 | 2457 | 749 | 424 | 1155 | 604 | 167 | 699 | 304 |
| Arrive On Green | 0.05 | 0.45 | 0.45 | 0.08 | 0.48 | 0.48 | 0.19 | 0.32 | 0.32 | 0.07 | 0.20 | 0.20 |
| Sat Flow, veh/h | 1781 | 5066 | 1532 | 1767 | 5106 | 1557 | 1710 | 3554 | 1520 | 1710 | 3497 | 1519 |
| Grp Volume(v), veh/h | 187 | 2159 | 249 | 138 | 3372 | 285 | 452 | 1130 | 671 | 230 | 516 | 199 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1689 | 1532 | 1767 | 1702 | 1557 | 1710 | 1777 | 1520 | 1710 | 1749 | 1519 |
| Q Serve(g_s), s | 8.0 | 65.0 | 17.0 | 7.4 | 77.0 | 18.6 | 31.0 | 50.4 | 52.0 | 11.0 | 22.2 | 19.3 |
| Cycle Q Clear(g_c), s | 8.0 | 65.0 | 17.0 | 7.4 | 77.0 | 18.6 | 31.0 | 50.4 | 52.0 | 11.0 | 22.2 | 19.3 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 134 | 2293 | 694 | 190 | 2457 | 749 | 424 | 1155 | 604 | 167 | 699 | 304 |
| V/C Ratio(X) | 1.39 | 0.94 | 0.36 | 0.72 | 1.37 | 0.38 | 1.07 | 0.98 | 1.11 | 1.38 | 0.74 | 0.65 |
| Avail Cap(c_a), veh/h | 134 | 2293 | 694 | 228 | 2457 | 749 | 424 | 1155 | 604 | 167 | 699 | 304 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 48.2 | 41.8 | 28.6 | 42.8 | 41.5 | 26.4 | 39.9 | 53.4 | 48.2 | 52.8 | 60.1 | 58.9 |
| Incr Delay (d2), s/veh | 215.4 | 9.3 | 1.4 | 9.6 | 170.2 | 1.5 | 62.2 | 21.4 | 70.9 | 203.7 | 4.3 | 5.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 13.8 | 30.5 | 7.0 | 6.2 | 72.7 | 7.8 | 21.1 | 27.0 | 37.2 | 11.4 | 10.7 | 8.2 |
| Unsig. Movement Delay, s/veh | 1 | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 263.6 | 51.1 | 30.1 | 52.4 | 211.7 | 27.8 | 102.1 | 74.8 | 119.1 | 256.5 | 64.3 | 64.2 |
| LnGrp LOS | F | D | С | D | F | С | F | E | F | F | <u> </u> | <u> </u> |
| Approach Vol, veh/h | | 2595 | | | 3795 | | | 2253 | | | 945 | |
| Approach Delay, s/veh | | 64.4 | | | 192.1 | | | 93.5 | | | 111.1 | |
| Approach LOS | | E | | | F | | | F | | | F | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 13.6 | 77.4 | 12.0 | 57.0 | 9.0 | 82.0 | 32.0 | 37.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 13.0 | * 67 | 8.0 | 50.0 | 5.0 | * 75 | 28.0 | 30.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 9.4 | 68.0 | 13.0 | 54.0 | 10.0 | 79.0 | 33.0 | 24.2 | | | | |
| Green Ext Time (p_c), s | 0.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.6 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 126.4 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

| | • | 7 | 1 | 1 | Ŧ | - | |
|---------------------------------|-----------|-------|-------|-------|-------------|--------------|---|
| Lane Group | EBL | EBR | NBL | NBT | SBT | SBR | |
| Lane Configurations | M | | 5 | ** | † Ъ | | |
| Traffic Volume (vph) | 11 | 38 | 26 | 1491 | 906 | 6 | |
| Future Volume (vph) | 11 | 38 | 26 | 1491 | 906 | 6 | |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | |
| Lane Width (m) | 3.2 | 3.2 | 3.3 | 3.5 | 3.5 | 3.5 | |
| Storage Length (m) | 0.0 | 0.0 | 25.0 | | | 0.0 | |
| Storage Lanes | 1 | 0 | 1 | | | 0 | |
| Taper Length (m) | 15.0 | | 15.0 | | | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | |
| Ped Bike Factor | | | | | | | |
| Frt | 0.896 | | | | 0.999 | | |
| Flt Protected | 0.989 | | 0.950 | | | | |
| Satd. Flow (prot) | 1577 | 0 | 1711 | 3500 | 3496 | 0 | |
| Flt Permitted | 0.989 | | 0.950 | | | | |
| Satd. Flow (perm) | 1577 | 0 | 1711 | 3500 | 3496 | 0 | |
| Link Speed (k/h) | 60 | | | 60 | 60 | | |
| Link Distance (m) | 47.4 | | | 146.7 | 158.7 | | |
| Travel Time (s) | 2.8 | | | 8.8 | 9.5 | | |
| Confl. Peds. (#/hr) | | 2 | | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Adj. Flow (vph) | 12 | 41 | 28 | 1621 | 985 | 7 | |
| Shared Lane Traffic (%) | | | | | | | |
| Lane Group Flow (vph) | 53 | 0 | 28 | 1621 | 992 | 0 | |
| Enter Blocked Intersection | No | No | No | No | No | No | |
| Lane Alignment | Left | Right | Left | Left | Left | Right | |
| Median Width(m) | 3.2 | | | 3.3 | 3.3 | | |
| Link Offset(m) | 0.0 | | | 0.0 | 0.0 | | |
| Crosswalk Width(m) | 3.0 | | | 3.0 | 3.0 | | |
| Two way Left Turn Lane | | | | | | | |
| Headway Factor | 1.06 | 1.06 | 1.04 | 1.01 | 1.01 | 1.01 | |
| Turning Speed (k/h) | 25 | 15 | 25 | | | 15 | |
| Sign Control | Stop | | | Free | Free | | |
| Intersection Summary | | | | | | | |
| Area Type: C | Other | | | | | | |
| Control Type: Unsignalized | | | | | | | |
| Intersection Capacity Utilizati | ion 51.9% | | | IC | CU Level of | of Service A | А |
| Analysis Period (min) 15 | | | | | | | |

| Movement EBL EBR NBL NBT SBT SBR Lane Configurations Y | | ٠ | 7 | 1 | Ť | ŧ | ~ | |
|---|------------------------------------|------|------|-------|------------|-------------------------|------------|--|
| Lane Configurations Y <thy< th=""> Y <thy< th=""></thy<></thy<> | Movement | EBL | EBR | NBL | NBT | SBT | SBR | |
| Traffic Volume (veh/h) 11 38 26 1491 906 6 Future Volume (Veh/h) 11 38 26 1491 906 6 Sign Control Stop Free Free Free G Grade 0% 0% 0% 0% 0% Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 Hourly flow rate (vph) 12 41 28 1621 985 7 Pedestrians 2 Lane Width (m) 3.4 Walking Speed (m/s) 1.1 Percent Blockage 0 Right turn flare (veh) None None None Median storage veh) Upstream signal (m) 147 V/2, stage 1 conf vol V/2, stage 2 conf vol V/2, stage 2 conf vol V/2, stage 2 conf vol V/2, stage 1 conf vo | Lane Configurations | Y | | 7 | † † | † 1 ₂ | | |
| Future Volume (Veh/h) 11 38 26 1491 906 6 Sign Control Stop Free Free Free Free Grade 0% 0% 0% 0% 0% Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 Hourly flow rate (vph) 12 41 28 1621 985 7 Pedestrians 2 2 1.1 985 7 Pedestrians 1.1 985 7 985 7 Pedestrians 1.1 985 7 985 7 Pedestrians 1.1 985 7 985 7 Pedestrians 1.1 985 98 90 147 7 Median type None None None None None None Vc, conflicting volume 1855 498 992 5 5 147 5 Vc2, stage 1 conf vol vc2, stage 2 conf vol vc2, stage 4 9 6 6 9 11 | Traffic Volume (veh/h) | 11 | 38 | 26 | 1491 | 906 | 6 | |
| Sign Control Stop Free Free Grade 0% 0% 0% Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 Hourly flow rate (vph) 12 41 28 1621 985 7 Pedestrians 2 2 1.1 985 7 Pedestrians 1.1 985 7 985 Walking Speed (m/s) 1.1 985 7 Wedian type 0 1.1 985 Median storage veh) 147 90.92 90.02 Upstream signal (m) 147 90.06 147 vC2, stage 1 conf vol vC2, stage 2 conf vol vC1, stage 1 conf vol 147 vC1, stage 1 conf vol vC1, stage 1 conf vol vC1, stage 1 conf vol 122 147 vC1, stage (s) 6.8 6.9 4.1 10 10 10 Up queue free % 88 92 96 1323 498 992 10 10 | Future Volume (Veh/h) | 11 | 38 | 26 | 1491 | 906 | 6 | |
| Grade 0% 0% 0% 0% Peak Hour Factor 0.92 1 Pedestrians 2 | Sign Control | Stop | | | Free | Free | | |
| Peak Hour Factor 0.92 0.92 0.92 0.92 0.92 0.92 0.92 Hourly flow rate (vph) 12 41 28 1621 985 7 Pedestrians 2 2 1621 985 7 Pedestrians 2 2 1.1 Percent Blockage 0 Right turn flare (veh) 1.1 Percent Blockage 0 Right turn flare (veh) Median storage veh) Upstream signal (m) 147 2 498 992 VC, conflicting volume 1855 498 992 147 2 147 2 VC1, stage 1 conf vol vC2, stage 2 conf vol vC4, unblocked vol 1323 498 992 141 147 147 VC2, stage 2 conf vol vC2, stage 2 conf vol vC4, unblocked vol 1323 498 992 141 162 163 165 163 165 163 163 163 163 163 163 163 163 164 163 16 | Grade | 0% | | | 0% | 0% | | |
| Hourly flow rate (vph) 12 41 28 1621 985 7 Pedestrians 2< | Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | |
| Pedestrians 2 Lane Width (m) 3.4 Walking Speed (m/s) 1.1 Percent Blockage 0 Right turn flare (veh) Median type Median type None Median type None Upstream signal (m) 147 pX, platoon unblocked 0.68 vC, conflicting volume 1855 498 992 vC1, stage 1 conf vol vC2, stage 2 conf vol vC4, unblocked vol 1323 498 992 vC1, stage 1 conf vol vC2, stage 2 conf vol vC4, unblocked vol 1323 498 992 tC, single (s) 6.8 tF (s) 3.5 go queue free % 88 92 96 cM capacity (veh/h) 97 517 693 Direction, Lane # EB 1 NB 1 NB 2 NB 3 SB 1 SB 2 Volume Total 53 28 810 657 <t< td=""><td>Hourly flow rate (vph)</td><td>12</td><td>41</td><td>28</td><td>1621</td><td>985</td><td>7</td><td></td></t<> | Hourly flow rate (vph) | 12 | 41 | 28 | 1621 | 985 | 7 | |
| Lane Width (m) 3.4 Walking Speed (m/s) 1.1 Percent Blockage 0 Right turn flare (veh) Median type None None None Median storage veh) Upstream signal (m) 147 pX, platoon unblocked 0.68 vC, conflicting volume 1855 498 992 vC1, stage 1 conf vol vC2, stage 2 conf vol vC3, stage 3 conf vol vC4, unblocked vol 1323 498 992 tC, single (s) 6.8 6.9 4.1 tC, 2 stage (s) tF (s) 3.5 3.3 2.2 p0 queue free % 88 92 96 cM capacity (veh/h) 97 517 693 Direction, Lane # EB 1 NB 1 NB 2 NB 3 SB 1 SB 2 Volume Total 53 28 810 810 657 335 Volume Left 12 28 0 0 0 0 vOlume Right 41 0 0 0 0 0 Volume Right 41 0 0 0 0 0 Volume to Capacity 0.20 0.04 0.48 0.48 0.39 0.20 Queue Length 95th (m) 5.2 0.9 0.0 0.0 0.0 Control Delay (s) 22.3 10.4 0.0 0.0 0.0 Lane LOS C B Approach Delay (s) 22.3 0.2 0.0 Approach LOS C Intersection Capacity Utilization 51.9% ICU Level of Service | Pedestrians | | | | 2 | | | |
| Walking Speed (m/s) 1.1 Percent Blockage 0 Right turn flare (veh) None Median storage veh) 147 Upstream signal (m) 147 pX, platoon unblocked 0.68 vC, conflicting volume 1855 498 992 vC1, stage 1 conf vol vC2, stage 2 conf vol vC4, stage 1 conf vol vC2, stage 2 conf vol vC2, stage 2 conf vol vC4, stage (s) 1 1 1 tf (s) 3.5 3.3 2.2 2 0 p0 queue free % 88 92 96 96 1 cf (s) 3.5 3.3 2.2 2 0 0 0 p0 queue free % 88 92 96 1 <td>Lane Width (m)</td> <td></td> <td></td> <td></td> <td>3.4</td> <td></td> <td></td> <td></td> | Lane Width (m) | | | | 3.4 | | | |
| Percent Blockage 0 Right turn flare (veh) None None Median storage veh) Upstream signal (m) 147 pX, platoon unblocked 0.68 | Walking Speed (m/s) | | | | 1.1 | | | |
| Right turn flare (veh) None None None Median storage veh) 147 9000000000000000000000000000000000000 | Percent Blockage | | | | 0 | | | |
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| cSH 261 693 1700 1700 1700 1700 Volume to Capacity 0.20 0.04 0.48 0.48 0.39 0.20 Queue Length 95th (m) 5.2 0.9 0.0 0.0 0.0 0.0 Control Delay (s) 22.3 10.4 0.0 0.0 0.0 0.0 Lane LOS C B | Volume Right | 41 | 0 | 0 | 0 | 0 | 7 | |
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| Control Delay (s) 22.3 10.4 0.0 0.0 0.0 0.0 Lane LOS C B B B Delay (s) 22.3 0.2 0.0 Delay (s) D | Queue Length 95th (m) | 5.2 | 0.9 | 0.0 | 0.0 | 0.0 | 0.0 | |
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| Approach Delay (s) 22.3 0.2 0.0 Approach LOS C 0.0 Intersection Summary 0.5 Intersection Capacity Utilization 51.9% ICU Level of Service | Lane LOS | C | B | 0.0 | 0.0 | 0.0 | 0.0 | |
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| | Intersection Canacity Litilization | on | | 51 9% | IC | | of Service | |
| Analysis Period (min) 15 | Analysis Period (min) | | | 15 | IC. | | | |



Parking and Loading Study Report



Ref: 2023-015



Dymon Group of Companies c/o James Byck, Regional Director – Construction (Toronto) 2-1830 Walkley Road Ottawa, ON K1H 8K3 By email: JByck@Dymon.ca

Re: 3855 Dundas Street Parking and Loading Study

Dear James:

Dymon Group of Companies (Dymon) is proposing to develop 3855 Dundas Street in Mississauga. The site is located on the northeast corner of the intersection of Ninth Line and Dundas Street East and is currently an empty field. The proposed development includes a 25,954 m² Dymon facility and will consist of 15,616 m² (168,091 ft²) of self-storage space, 97 m² (1,048 ft²) of wine cellar space, 5,755 m² (61,941 ft²) of office space, 1,231 m² (13,255 ft²) of industrial condo units, and 1,400 m² (15,065 ft²) of reception and retail spaces that support the self-storage customers.

A total of 190 parking spaces are proposed, of which 97 are at grade and 93 are on one underground level. A total of 12 accessible parking spaces will be provided and will serve all proposed land uses. Ten of the 12 accessible spaces are proposed at grade, and two will be underground. A total of 28 bicycle parking spaces will be provided. The site will include one exterior loading dock south of the interior loading area / drive aisle. There will also be an interior loading / drive-through area located adjacent to the industrial condos and connected via doors in each condo unit. This area will serve the industrial condo tenants as well as providing spaces for additional overflow parking and loading for self-storage customers. Attachment 1 includes the proposed site plan.

This letter has been prepared to address the transportation requirements of the proposed Dymon Self-Storage and Work Refined Facility and will examine the site parking and loading requirements.

Dymon Business Model and Site Context

Dymon offers a unique customer-centric storage solution unlike anything else in the marketplace. Unlike traditional self storage operations, Dymon facilities are located along arterial corridors, in very prominent locations within close proximity to its residential and business customers. With its high level of security, total humidity and climate control environment, and focus on customer service, Dymon offers a reliable extension to people's homes and businesses. The primary access to Dymon's facilities is via an interior loading area (with secure access 24 hours a day) that protects customers from the weather while loading/unloading their possessions. By providing this interior area the reliance on surface parking is significantly reduced, as up to 75% of visitors to the site during any period use the interior loading bay, rather than the provided parking lot. In fact, any visit after the initial visit uses the interior loading area as this is the direct access to the storage lockers. Dymon sites include a reception and a retail area that is not used directly for self-storage. This space has several functions, including allowing space for new customers to come in and rent a storage locker or purchase storage solutions including closet organizers, under counter shelving, and storage bins. This service is now offered at several Ottawa Dymon locations. This development also includes a Work Refined co-working space which provides members with 24/7 secure access to fully equipped office facilities and dedicated high speed wi-fi, on flexible terms with no long-term commitments.

Industrial condos to be provided to this site are a new addition to Dymon facilities. The industrial condo is a condominium development like residential and office condominiums but dedicated to industrial land use. Dymon's industrial condos aim at providing quality small to mid-bay industrial activities. The industrial condos are located in a multi-unit structure and share common driveways, loading areas, parking areas, garbage collection, utilities, sidewalks, lobbies, etc.

Parking Generation / Requirement

The proposed development will provide a total of 97 exterior parking spaces at grade, and 93 underground parking spaces. The development is mixed-use and the total site parking requirements are a sum of the individual parking space requirements for each land use. The zoning by-law does not have an "industrial condo" land use specifically, therefore the parking rates required for all industrial related uses, such as manufacturing facility, warehouse / distribution facility, and contractor service shop, for multiple-occupancy buildings have been reviewed. The industrial condos are expected to be used for a variety of industrial activities, thus the highest unit area parking rate among these has been applied to calculate the minimum parking requirement for this use.

The site is located in Parking Precinct 4, and therefore the Mississauga Zoning By-law 0225-2007 parking rates for Precinct 4 have been applied. Precinct 4 includes the areas outside the City Centre or the areas currently with limited access to rapid transit, thus the minimum parking rates for each land use are on the higher end of the City in the Zoning By-law. The zoning requirements and parking provisions are summarized in Table 1.

| Land Use | GFA (m²) | Parking Rate (Required) | Parking Spaces (Required) | Parking Spaces (Provided) | Difference | |
|---|----------|--|---------------------------------|---------------------------------|------------|--|
| Self Storage incl. Wine Cellar | 15,714 | 0.25 spaces per 100 m ² GFA | 39 | | | |
| Retail (less than 2,000 m ² GFA) | 1,400 | 4.3 spaces per 100 m ² GFA | 60 | 100 | 100 | |
| Office | 5,755 | 3 spaces per 100 m ² GFA | 173 | 190 | -102 | |
| Industrial Condo | 1,231 | 1.6 spaces per 100 m ² GFA | 20 | | | |
| | Total | | 292 | 190 | -102 | |

Table 1: Vehicle Parking Requirement Zoning By-Law Approach

As noted above, the proposed site does not include the number of parking stalls prescribed by the zoning by-law. The proposed site includes 190 parking spaces, whereas the requirement is 292 parking spaces.

To support the proposed parking variance for the self-storage warehouse, a parking survey has been undertaken at a proxy site operated by Dymon at 1460 The Queensway in Etobicoke, Toronto. It has been selected as an appropriate proxy site for comparison, as it has similar features to the proposed development such as the proposed land uses, total gross floor area, and arterial road access. The selected site includes the Dymon self-storage facility with drive-through areas, the retail functions which sell the home storage solutions discussed previously, and a co-working office space. These will operate in the same manner as the proposed site plan at 3855 Dundas Street West. Attachment 2 provides the detailed parking generation counts for 1460 The Queensway. As shown in Table 2, the counts were recorded on the busiest days of the week in February 2022, October 2022, and March 2023, allowing observation of the parking demand increase as the proxy site gradually approached its full occupancy.

| Table 2: Data Dates – 1460 The Queensway | Table | 2: | Data | Dates – | 1460 | The | Queensway |
|--|-------|----|------|---------|------|-----|-----------|
|--|-------|----|------|---------|------|-----|-----------|

| Data Type | Location | Count Date | | | | | |
|----------------|--------------------|-----------------------------|--|--|--|--|--|
| | | Saturday, February 12, 2022 | | | | | |
| | | Tuesday, February 15, 2022 | | | | | |
| | | Thursday, October 20, 2022 | | | | | |
| Parking Counts | 1460 The Queensway | Wednesday, March 29, 2023 | | | | | |
| | | Thursday, March 30, 2023 | | | | | |
| | | Friday, March 31, 2023 | | | | | |
| | | Saturday, April 1, 2023 | | | | | |

Table 3 summarizes the parking supply and parking demand for the site as well as the calculated parking supply rate and parking demand rate for the self-storage component. The exterior parking supply has been included. The sum of self-storage and reception / retail parking demand has been provided for the February 2022 counts as the parking surveys taken then did not separate the two uses.



Mr. James Byck August 1, 2023

Table 4 summarizes the parking supply and parking demand as well as the calculated parking supply rate and parking demand rate for the Work Refined office component of 1460 The Queensway.

Per the City of Mississauga's requirement, parking survey data was collected over a consecutive two-week period for two or three of the busiest days per week. Data has been collected for four days within one week between Wednesday, March 29, 2023, and Saturday, April 1, 2023. The three weekdays were selected as the busiest days during the week according to information supplied by the reception staff at the subject facility. Data was also collected on Saturday to account for the potential alternative peak period due to the increasing self-storage-related traffic and decreasing office-related traffic during the weekend. Data was not collected over a two-week period as the week after the data was collected was a four-day week before the Easter holidays and the survey results would not represent the parking demand of a typical week.

As parking counts from a consecutive two-week period was not available, the dataset was supplemented with earlier parking counts from February 2022 and October 2022. Although those counts were from earlier dates, they could be validated by applying the occupancy rate at the time of the parking surveys.

At the 1460 Queensway location, in February 2022, 59.5% of the self-storage lockers were rented (1548 Units) while 40.5% were available or vacant (1055 Units), and 64.5% of the co-working spaces were rented (129 workstations) while 35.5% (71 workstations) were available for the office. Considering the potential growth from more customers, the parking demands at maximum capacity, assuming that the increase in the parking demand will be linear to the number of rented units, have been calculated for self-storage (including retail) and office land uses and are summarized in Table 3 and Table 4 in the "Adjusted" rows. It is observed that the parking demand rate has been steadily increasing over time, and the parking demand rates from the adjusted February 2022 counts and the parking demand rates directly from the March 2023 counts are converging. Therefore, it is evident that the proxy site is approaching full occupancy in 2023 and the March 2023 peak parking demand rates are representative of the peak parking demand of comparable facilities. The March 2023 peak parking demand rates have been applied to calculate the parking requirement for 3855 Dundas Street.

The proposed parking survey range has been submitted to the transportation staff at the City, but no responses have been received in advance of this resubmission. In this case, we have proceeded with the assumption.

| Site | GFA Storage & Retail (m ²) | Parking Supply (Exterior) | Parking Supply (Interior) | Parking Supply (Total) | Parking Demand | Parking Supply Rate | Parking Demand Rate |
|---|--|---------------------------------|---------------------------------|------------------------------|-------------------|---------------------------|---------------------------|
| 1460 The Queensway (February 2022) | 28,799 | 173 | 59 | 232 | 49 | 0.81/100m ² | 0.17/100m ² |
| Adjusted | | | | | | | 0.29/100m ² |
| 1460 The Queensway (March – April 2023) | 28,799 | 173 | 59 | 232 | 95 | 0.81/100m ² | 0.33/100m ² |
| Storage | 27,568 | 145 | 59 | 204 | 68 | 0.74/100m ² | 0.25/100m ² |
| Retail | 1,231 | 28 | 0 | 28 | 27 | 2.27/100m ² | 2.19/100m ² |

Table 3: Parking Survey Summary – Self-storage and Retail



| Site | GFA Storage & Retail (m ²) | Parking Supply (Exterior) | Parking Supply (Interior) | Parking Supply (Total) | Parking Demand | Parking Supply Rate | Parking Demand Rate |
|---|--|---------------------------------|---------------------------------|------------------------------|-------------------|---------------------------|---------------------------|
| 1460 The Queensway (February 2022) | 2,192 | 40 | 0 | 0 | 25 | 1.82/100m ² | 1.14/100m ² |
| Adjusted | | | | | | | 1.77/100m ² |
| 1460 The Queensway (October 2022) | 2,192 | 40 | 0 | 0 | 29 | 1.82/100m ² | 1.32/100m ² |
| 1460 The Queensway (March – April 2023) | 2,192 | 40 | 0 | 0 | 36 | 1.82/100m ² | 1.64/100m ² |

Table 4: Parking Survey Summary – Office

Based on the proposed site plan for 3855 Dundas Street, the gross floor area, and parking stall provisions, the parking rate provided for the proposed development has been calculated. Table 5 summarizes the 3855 Dundas Street parking provisions.

| Land Use | GFA (m²) | Parking Rate (Required) | Parking Spaces Required | Parking Spaces Provided | Parking Rate (Provided) |
|---------------------------|----------|----------------------------|----------------------------|----------------------------|----------------------------|
| Self-Storage | 15,714 | 0.25/100m ² | 39 | 39 | 0.25/100 m ² |
| Retail / Reception | 1,400 | 2.19/100m ² | 31 | 34 | 2.43/100 m ² |
| Office | 5,755 | 1.64/100m ² | 95 | 97 | 1.69/100 m ² |
| | Subtotal | | 165 | 170 | - |
| Industrial Condo | 1,231 | 1.6/100m ² | 20 | 20 | 1.6/100m ² |
| | Total | | 185 | 190 | - |

Table 5: 3855 Dundas Street Parking Provisions – Dymon

It has been calculated that parking is proposed to be provided at a rate of 0.25 spaces per 100 square metres of non-residential GFA for the self-storage component, 2.43 spaces per 100 square metres of non-residential GFA for the retail component, and 1.69 spaces per 100 square metres of non-residential GFA for the office component. While these are less than the parking rate requested by the City of Mississauga, the rates are higher than the peak surveyed parking demand rates at the comparable Dymon site. No parking variance is proposed for the industrial condo land use, and the Zoning by-law parking rate of 1.6 spaces per 100 square metres of non-residential GFA has been provided.

In addition to the above, patrons will utilize the interior loading space more efficiently than other areas of the site as they will park within the interior loading area to facilitate loading and unloading. The interior loading space can accommodate more vehicles.

Further, future higher order transit is planned along Dundas Street in the form of BRT facilities. It is anticipated that the completion of the Dundas BRT will result in an increase in the transit mode share within the Study Area and will reduce the reliance on personal vehicles and the parking demand along Dundas Street corridor.

Considering the proxy site requirements, the parking provisions for both the Dymon self-storage and office uses are adequate.

Accessible Parking

Accessible parking spaces requirements and provisions are summarized in Table 6. Since a reduction from the zoning by-law requirement is sought for both the self-storage and the office components and this reduction is supported by the proxy site survey data, the accessible parking spaces will be provided based on the number of total parking spaces proposed, instead of the total parking spaces required by the zoning by-law.



| Land Use | Total Number of Required Non-Residential Range Parking Spaces | | Minimum Accessible Parking Rate (Required) | Minimum Accessible Parking Spaces (Required) | Parking Spaces (Provided) | Meeting the Requirement? |
|-------------|---|---------|---|---|---------------------------------|-----------------------------|
| Total | 190 | 101-200 | 1.0 space plus 3% of the total | 3 Type A 4 Type B | 6 Type A 6 Type B | Yes |

Table 6: Accessible Parking Requirement - Zoning By-Law Approach

A total of 12 accessible parking spaces will be provided, including 6 Type A spaces and 6 Type B spaces paired with each other. All accessible parking spaces are provided at grade, immediately next to building entrances. As shown above, the accessible parking provisions exceed the zoning by-law requirements.

Bicycle Parking

Bicycle parking spaces will be provided in accordance with Section 3.1.6 of the Mississauga Zoning By-law 0225-2007 as summarized in Table 7. The bicycle parking provisions are listed for comparison. Class A are long-term bicycle parking spaces and Class B are short-term bicycle parking spaces.

| Land Use | GFA (m²) | Class A Rate (Required) | Class A (Required) | Class A (Provided) | Class B Rate (Required) | Class B (Required) | Class B (Provided) |
|-------------------------------|----------|----------------------------|-----------------------|-----------------------|----------------------------|-----------------------|-----------------------|
| Self Storage + Wine Cellar | 15,714 | n/a | 0 | | 2.0 | 2 | |
| Retail | 1,400 | 0.15* | 2 | 10 | 0.2* | 3 | 16 |
| Office | 5,755 | 0.1* | 6 | 12 | 0.1* | 6 | 10 |
| Industrial Condo** | 1,231 | 0.15* | 2 | | 0.15* | 2 | |
| Total | | | 10 | 12 | | 13 | 16 |

Table 7: Bicycle Parking Requirement - Zoning By-Law Approach

*Unit for parking rates is spaces per 100 m² non-residential GFA.

**For industrial condos, the bicycle parking rates for Manufacturing Facility, Warehouse/Distribution Facility, and Wholesaling Facility have been applied.

The site will provide a total of 28 bicycle parking spaces including 12 long-term spaces on underground level 1 and 16 short-term spaces at grade. The bicycle parking provisions will exceed the zoning by-law requirements of 10 long-term and 13 short-term spaces.

Loading Spaces

Loading Space requirements per Mississauga Zoning By-law 0225-2007 and provisions are summarized in Table 8.

| Land Use | GFA (m²) | Criteria | Minimum Loading Spaces | Loading Spaces Provided | Difference |
|---|-------------|--|---------------------------|----------------------------|------------|
| Warehouse / Distribution Facility | 15,714 | Greater than 14,000 m ² : 3.0 spaces plus 1.0 additional space for each 9,300 m ² GFA - non-residential or portion thereof | 4 | | |
| Retail | 1,400 | Greater than 250 m ² but less than or equal to 2,350 m ² : 1.0 space | 1 | 2 | 2 |
| Office | 5,755 | Greater than 2,350 m ² but less than or equal to 11,600 m ² : 1.0 space | 1 | | |
| Industrial Condos | 1,231 | Greater than 250 m ² but less than or equal to 2,350 m ² : 1.0 space | 1 | | |
| Total | | | 7 | 2 | -5 |

Table 8: Loading Requirement – Zoning By-law Approach



As shown in Table 8, the provided loading spaces are 5 spaces short from the required. However, it is anticipated that the loading space provisions will be able to accommodate the needs of the vehicles on site.

The industrial condo is the only land use where no previously collected proxy site data on loading demand rates is available. As such, the required one loading dock is provided in the interior loading / drive-through area next to the industrial condos, with doors connecting the loading area to each industrial condo.

To support the loading variance for the rest of the land uses, proxy site survey data from 1460 The Queensway has been used to determine the frequency of truck visits. Table 9 summarizes the surveyed heavy vehicle In and Out trips during the heavy truck peak hour of 1460 The Queensway.

| Site | A | M Peak Hou | ır | Р | M Peak Hou | ur | S | at Peak Hou | ır |
|--|----|------------|-----|----|------------|-----|----|-------------|-----|
| Site | In | Out | Net | In | Out | Net | In | Out | Net |
| 1460 The Queensway (February 2022) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1460 The Queensway (October 2022) | 1 | 1 | 0 | 1 | 0 | 1 | - | - | - |
| 5 Nevets Road | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Table 9: Net Peak Hour Trucks

As can be seen in Table 9, trucks entering the proxy Dymon sites vary between zero and one during the truck peak hour periods. The demand for loading docks is expected to be even lower, as the proxy site turning movement counts include moving trucks, as well as garbage trucks. Considering this, two loading spaces will meet the loading space demand at the subject site.

Moreover, the City's Loading Space Regulations do not include specific loading space requirements for the Self-Storage Warehouse land use. The loading space requirement for the City of Mississauga has a general rate for all non-residential land uses excluding office and medical office land uses. Using this general rate, the self-storage portion alone requires a minimum of four loading spaces. Unlike a self-storage facility, where patrons may utilize personal vehicles for loading and unloading, it is expected that the majority of vehicles entering a manufacturing site will be utilizing loading docks. Therefore, the requirement of four spaces is considered overly conservative for a self-storage facility and a provision of two loading docks is recommended. Similarly, the loading requirement of the retail land use on site is also based on the general non-residential rate which is not representative of the storage-related reception / retail area in the proposed development.

The "office" land use provided in the City's Loading Space Regulations is also a general rate for all types of offices instead of the specific rate for co-working spaces. Co-working spaces have less loading / unloading activities than typical office land uses as some visitors use them as temporary locations for work.

In addition, the interior loading area is designed with the intention to provide more freedom to customers using the parking and loading spaces. Apart from the loading space in the centre delineated with pavement markings, the rest of the interior loading area is also intended to be used as loading spaces to accommodate the loading / unloading vehicles. They are not marked on the ground, thus during the operation of the site the users can decide the locations to use depending on the sizes of the vehicles, the sizes of the empty spaces, and the location of the lockers. This feature can potentially result in higher efficiency in utilizing the loading area. Therefore, the actual loading spaces provided will function as more than the two loading docks. On a rare occasion where extra loading spaces for trucks are required, the interior loading area can accommodate more HSU trucks.



Mr. James Byck August 1, 2023

As such, the provision of two loading docks for all proposed land uses satisfies the expected demand based on heavy vehicle trip generation at comparable Dymon sites, and the loading requirements provided in the City's Loading Space Regulations are not considered applicable to this development.

Conclusions

Based on the key requirements of the agreed to scope, the following conclusions are made for this site:

• Based on the proxy site parking surveys, the provided parking will adequately serve the proposed self-storage and office facility.

Based on this Transportation and Parking Summary, the proposed development should be approved, from a transportation perspective.

Zhengxuan Lai, E.I.T. 289-834-0646 may.lai@cghtransportation.com

Mark Crockford, P. Eng. 905-251-4070 mark.crockford@cghtransportation.com

Attachments: Attachment 1 – Proposed Site Plan Attachment 2 – Proxy Site Parking Data and Site Plan





Proposed Site Plan







| 6 Leswyn Road Toronto, Ontaric | a r o, M6A 1K2 | chitect tel fax | in c (416)256- (416)256- | -4440 -4449 |
|--|--|--|--|------------------------------------|
| Design Architect | TA 660R Co | ACT Arch | nitecture et (Rear | e Inc Lane) |
| Plannina, Urban f |)esign & Lan | ioronto tel: (idscape Arch | 010. M6(416) 516 nitect | ∍ 188 -1949 |
| MHE | C Planni Lan 7050 | ng, Urba dscape Weston Ro Woodbridge tel: (9 | In Desig Architec ad, Suite ON. L4L | n & ture 230, 8G7 5588 |
| Civil Engineer | C.F. ((211 | Crozier & Consultin Yonge str Toronto | : Associ g Engin eet, Suite ON. M5E 416) 477 | ates eers 301, 31M4 |
| | | tel: (4 | +ıb) 477- | - 3392 |
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Proxy Site Parking Data and Site Plans





| STATISTIC | CS | | II LE | GEND |
|--|--|---|------------|---|
| | | | | |
| | | | | |
| LEGAL DESCRIPTION OF | PROPERTY: | | | PROPOSED BUILDING LOCATION |
| THE 41,719m ² PROPER QUEENSWAY IS LOCATED ROAD AND THE QUEENS | TY KNOWN MUNICIPALLY .) AT THE NORTHEAST CO ;WAY IN THE CITY OF TOI | AS 1460 THE RNER OF VANSCO RONTO (ETOBICOKE). | | EXISTING NEIGHBORING BUILDINGS |
| BOUNDARY INFORMATION SURVEYING LTD. | I FROM SURVEY BY: DAV | D B. SEARLES | | LANDSCAPED AREA |
| | | | | CONCRETE/ SIDEWALK |
| BUILDING FOOTPRINT | | | | BARRIER FREE PARKING CLEARANCE |
| (INCLUDING INTERIOR LO | DADING): 29,210 m ² | $(314,411 \text{ ft}^2)$ | | INTERLOCKING PAVING STONE (EXISTING TO REMAIN OR REUSE) |
| TOTAL SELF STORAGE | 1,231 m ² (1 | 3,212 ft ²) | | CURB |
| TOTAL OFFICE | 2,192 m² (2 | 24,749 ft²) | <u> </u> | DEPRESSED CURB |
| TOTAL GFA | 30,991 m² | (397,956 ft²) | | NEW TREE/ VEGETATION (REFER TO LANDSCAPE PLAN FOR TYPE, SIZE AND LOCATION) |
| PARKING STATISTICS | | | | |
| REQUIRED | | PROPOSED | | (VEGETATION IS FOR REFERENCE ONLY, REFER TO LANDSCAPE PLAN) |
| CURRENT E1.0 ZONING | FORMER CITY OF ETOBICOKE BY-LAW | | P | KELEK TO LANDSCALE TEAN) |
| 206 SPACES | 359 SPACES | 266 EXT. SPACES 59 INT. SPACES | G. | BARRIER FREE PARKING |
| FOR A COMPLETE LIST | OF THE REREORMANCE S | 325 IOTAL | | INTERIOR PARKING |
| BOTH ZONING CATEGORI APPENDIX A OF THE AS | SOCIATED PLANNING RAT | IONALE REPORT. | <u>□</u> & | CATCH BASIN |
| | | | トレ | SIAMESE CONNECTION |
| | | | | ENTRANCE/ EXIT LOCATION |
| | | | | TRANSFORMER |
| | | | | FENCE & GATE |
| | | | Que | ' MAN HOLE COVER |
| | | | • MP | WOOD POLE (HYDRO) |
| | | | | FIRE HYDRANT |
| | | | | NLS (NEW LIGHT STANDARD, REFER TO ELECTRICAL) |
| | | | • | NEW BOLLARD |
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BOUNDARY INFORMATION FROM SURVEY BY: DAVID B. SEARLES SURVEYING LTD. ONTARIO LAND SURVEYORS. 04 MAY 2016

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2015.0035.01 DYM-ON-ETOBIQUEEN146

Ontario Traffic Inc - Parking Counts

| | | | | Sat | <mark>turday, Feb</mark> | ruary 12, 2 | 022 | | | Tu | <mark>lesday, Feb</mark> l | ruary 15, 20 |)22 | |
|--------------------|----|-------|-------|-----------|--------------------------|-------------|-------------|-----------------|-------|-----------|----------------------------|--------------|--------------------------|----------|
| | | | 1460 | The Queer | isway | | 5 Nevets Ro | ł | 1460 | The Queer | nsway | | <mark>5 Nevets Ro</mark> | ł |
| Time | | | Legal | Illegal | Off-Site | Legal | Disabled | Off-Site | Legal | Illegal | Off-Site | Legal | Disabled | Off-Site |
| 10:00 | to | 10:30 | 15 | 4 | 0 | 8 | 0 | 0 | 42 | 3 | 0 | 6 | 0 | 0 |
| 10:30 | to | 11:00 | 18 | 4 | 0 | 8 | 0 | 0 | 55 | 4 | 0 | 7 | 0 | 0 |
| 11:00 | to | 11:30 | 21 | 4 | 0 | 10 | 0 | 0 | 60 | 3 | 0 | 8 | 0 | 0 |
| 11:30 | to | 12:00 | 26 | 4 | 0 | 9 | 0 | 0 | 67 | 2 | 0 | 9 | 0 | 0 |
| 12:00 | to | 12:30 | 31 | 5 | 0 | 11 | 0 | 0 | 71 | 2 | 0 | 10 | 0 | 0 |
| 12:30 | to | 13:00 | 33 | 4 | 0 | 9 | 0 | 0 | 69 | 2 | 0 | 10 | 0 | 0 |
| 13:00 | to | 13:30 | 30 | 4 | 0 | 9 | 0 | 0 | 66 | 2 | 0 | 9 | 0 | 0 |
| 13:30 | to | 14:00 | 36 | 4 | 0 | 10 | 0 | 0 | 67 | 2 | 0 | 11 | 0 | 0 |
| 14:00 | to | 14:30 | 25 | 4 | 0 | 7 | 0 | 0 | 55 | 2 | 0 | 11 | 0 | 0 |
| 14:30 | to | 15:00 | 32 | 4 | 0 | 10 | 0 | 0 | 59 | 2 | 0 | 8 | 0 | 0 |
| 15:00 | to | 15:30 | 30 | 4 | 0 | 13 | 0 | 0 | 56 | 1 | 0 | 10 | 0 | 0 |
| 15:30 | to | 16:00 | 29 | 4 | 0 | 12 | 0 | 0 | 51 | 1 | 0 | 9 | 0 | 0 |
| Available Spaces = | | | 202 | | | 32 | 2 | | 202 | | | 32 | 2 | |

Location: Site ID: 1460 The Queensway 20-Oct-22

| | | | Th | ursday, October 20, 20 | 022 | Th | ursday, October 20, 2 | 022 | Th | ursday, October 20, 20 | 122 | | Th | ursday, October 20, 20 | 22 |
|-------|--------------|-------|-------|------------------------|----------|-------|------------------------|----------|-------|------------------------|----------|---------------------|-------|------------------------|----------|
| | | | Wor | k Refined Members A | ccess | i | n front of Work Refine | ed | Var | sco access #1 to acces | is #2 | | Var | sco access #2 to acces | s #3 |
| | Time | | Legal | Illegal | Off-Site | Legal | Illegal | Off-Site | Legal | Illegal | Off-Site | Notes | Legal | Illegal | Off-Site |
| 08:00 | to | 08:30 | 5 | 0 | 0 | 1 | 0 | 0 | 13 | 0 | 0 | | | | |
| | | | | | | | | | | | | at least 1 going to | | | |
| 08:30 | to | 09:00 | 7 | 0 | 0 | 5 | 0 | 0 | 18 | 0 | 0 | WR | | | |
| 09:00 | to | 09:30 | 10 | 0 | 0 | 8 | 0 | 0 | 26 | 0 | 0 | 1 | | | |
| 09:30 | to | 10:00 | 11 | 1 | 0 | 9 | 0 | 0 | 27 | 0 | 0 | 2 going to WR | 7 | 0 | 0 |
| 10:00 | to | 10:30 | 11 | 1 | 0 | 10 | 1 | 0 | 28 | 0 | 0 | 2 | 10 | 0 | 0 |
| 10:30 | to | 11:00 | 12 | 1 | 0 | 9 | 0 | 0 | 28 | 0 | 0 | 1 | 14 | 0 | 0 |
| 11:00 | to | 11:30 | 14 | 2 | 0 | 9 | 0 | 0 | 32 | 0 | 0 | 1 | 13 | 0 | 0 |
| 11:30 | to | 12:00 | 15 | 2 | 0 | 9 | 0 | 0 | 31 | 0 | 0 | | 16 | 0 | 0 |
| 12:00 | to | 12:30 | 15 | 2 | 0 | 9 | 0 | 0 | 28 | 0 | 0 | | 17 | 0 | 0 |
| 12:30 | to | 13:00 | 14 | 2 | 0 | 10 | 0 | 0 | 26 | 0 | 0 | | 18 | 0 | 0 |
| 13:00 | to | 13:30 | 13 | 2 | 0 | 10 | 0 | 0 | 29 | 0 | 0 | | 13 | 0 | 0 |
| 13:30 | to | 14:00 | 13 | 2 | 0 | 9 | 1 | 0 | 28 | 0 | 0 | | 13 | 0 | 0 |
| 14:00 | to | 14:30 | 13 | 2 | 0 | 7 | 0 | 0 | 26 | 0 | 0 | | 13 | 0 | 0 |
| 14:30 | to | 15:00 | 13 | 2 | 0 | 7 | 0 | 0 | 24 | 0 | 0 | 1 out from WR | 14 | 0 | 0 |
| 15:00 | to | 15:30 | 14 | 2 | 0 | 7 | 0 | 0 | 26 | 0 | 0 | | 14 | 0 | 0 |
| 15:30 | to | 16:00 | 12 | 2 | 0 | 6 | 0 | 0 | 23 | 0 | 0 | 1 out from WR | 12 | 0 | 0 |
| 16:00 | to | 16:30 | 12 | 2 | 0 | 7 | 0 | 0 | 22 | 0 | 0 | 1 out from WR | | | |
| 16:30 | to | 17:00 | 8 | 2 | 0 | 8 | 0 | 0 | 19 | 0 | 0 | | | | |
| Ava | ilable Space | ces = | 23 | | | 10 | | | 35 | | | | 41 | | |

Ontario Traffic Inc - Parking Study

Location: 1460 The Queensway (Dymon Self-Storage)

Date: Saturday, April 01, 2023

| | | | | | Parking Area | l | |
|-------|---------------|-------|-----|--------|--------------|------------|--------|
| | | | | | | Green | |
| | Time | | Red | Orange | Blue | Drive-Thru | Purple |
| 8:00 | to | 8:30 | 0 | 0 | 1 | 8 | 15 |
| 8:30 | to | 9:00 | 0 | 0 | 1 | 9 | 16 |
| 9:00 | to | 9:30 | 0 | 0 | 2 | 8 | 14 |
| 9:30 | to | 10:00 | 0 | 0 | 1 | 8 | 12 |
| 10:00 | to | 10:30 | 3 | 0 | 2 | 12 | 8 |
| 10:30 | to | 11:00 | 5 | 0 | 4 | 14 | 10 |
| 11:00 | to | 11:30 | 8 | 0 | 3 | 15 | 11 |
| 11:30 | to | 12:00 | 7 | 0 | 4 | 13 | 11 |
| 12:00 | to | 12:30 | 7 | 0 | 6 | 14 | 10 |
| 12:30 | to | 13:00 | 7 | 0 | 4 | 14 | 11 |
| 13:00 | to | 13:30 | 7 | 0 | 3 | 17 | 12 |
| 13:30 | to | 14:00 | 8 | 0 | 3 | 14 | 14 |
| 14:00 | to | 14:30 | 8 | 0 | 3 | 14 | 12 |
| 14:30 | to | 15:00 | 7 | 0 | 2 | 13 | 13 |
| 15:00 | to | 15:30 | 7 | 0 | 2 | 11 | 14 |
| 15:30 | to | 16:00 | 6 | 0 | 3 | 12 | 15 |
| 16:00 | to | 16:30 | 6 | 0 | 3 | 11 | 16 |
| 16:30 | to | 17:00 | 6 | 0 | 4 | 9 | 20 |
| 17:00 | to | 17:30 | 4 | 0 | 2 | 10 | 17 |
| 17:30 | to | 18:00 | 3 | 0 | 1 | 11 | 16 |
| 18:00 | to | 18:30 | 3 | 0 | 1 | 12 | 15 |
| 18:30 | to | 19:00 | 3 | 0 | 1 | 13 | 13 |
| 19:00 | to | 19:30 | 3 | 0 | 1 | 12 | 10 |
| 19:30 | to | 20:00 | 3 | 0 | 1 | 12 | 8 |
| Av | ailable Space | s = | 40 | 53 | 28 | | 145 |



Ontario Traffic Inc - Parking Study

Location: 1460 The Queensway (Dymon Self-Storage)

| | | | | Wednes | sday, March | 29, 2023 | | | Thurse | day, March 3 | 30, 2023 | | | Frida | <mark>iy, March 31</mark> | , 2023 | |
|-------|--------------|-------|-----|--------|--------------|------------|--------|-----|--------|--------------|------------|--------|-----|--------|---------------------------|------------|--------|
| | | | | | Parking Area | a | | | | Parking Are | a | | | | Parking Area | a | |
| | | | | | | Green | | | | | Green | | | | | Green | |
| | Time | | Red | Orange | Blue | Drive-Thru | Purple | Red | Orange | Blue | Drive-Thru | Purple | Red | Orange | Blue | Drive-Thru | Purple |
| 08:30 | to | 09:00 | 13 | 0 | 4 | 13 | 17 | 13 | 0 | 2 | 12 | 17 | 14 | 0 | 4 | 13 | 18 |
| 09:00 | to | 09:30 | 16 | 0 | 7 | 14 | 20 | 24 | 0 | 5 | 15 | 18 | 21 | 0 | 4 | 17 | 17 |
| 09:30 | to | 10:00 | 23 | 0 | 8 | 15 | 22 | 25 | 0 | 12 | 21 | 19 | 27 | 0 | 6 | 15 | 18 |
| 10:00 | to | 10:30 | 26 | 0 | 14 | 19 | 21 | 30 | 0 | 15 | 22 | 20 | 31 | 0 | 15 | 17 | 21 |
| 10:30 | to | 11:00 | 27 | 0 | 14 | 18 | 21 | 32 | 0 | 21 | 24 | 20 | 31 | 0 | 21 | 17 | 20 |
| 11:00 | to | 11:30 | 29 | 0 | 15 | 21 | 23 | 30 | 0 | 21 | 25 | 21 | 31 | 0 | 23 | 17 | 20 |
| 11:30 | to | 12:00 | 30 | 0 | 19 | 27 | 21 | 29 | 0 | 20 | 25 | 23 | 29 | 0 | 25 | 19 | 21 |
| 12:00 | to | 12:30 | 30 | 0 | 19 | 24 | 21 | 28 | 0 | 21 | 25 | 24 | 30 | 0 | 25 | 18 | 21 |
| 12:30 | to | 13:00 | 30 | 0 | 20 | 27 | 23 | 31 | 0 | 17 | 27 | 24 | 31 | 0 | 25 | 18 | 22 |
| 13:00 | to | 13:30 | 32 | 0 | 24 | 30 | 25 | 33 | 0 | 15 | 27 | 22 | 31 | 0 | 23 | 20 | 23 |
| 13:30 | to | 14:00 | 36 | 0 | 27 | 38 | 30 | 32 | 0 | 16 | 25 | 29 | 32 | 0 | 21 | 20 | 33 |
| 14:00 | to | 14:30 | 35 | 0 | 23 | 32 | 26 | 35 | 0 | 19 | 22 | 33 | 31 | 0 | 20 | 20 | 32 |
| 14:30 | to | 15:00 | 35 | 0 | 22 | 30 | 24 | 34 | 0 | 20 | 21 | 32 | 29 | 0 | 20 | 23 | 31 |
| 15:00 | to | 15:30 | 34 | 0 | 20 | 31 | 22 | 34 | 0 | 22 | 22 | 31 | 25 | 0 | 19 | 22 | 25 |
| 15:30 | to | 16:00 | 34 | 0 | 18 | 32 | 20 | 32 | 0 | 21 | 19 | 33 | 24 | 0 | 18 | 20 | 23 |
| 16:00 | to | 16:30 | 31 | 0 | 14 | 30 | 20 | 31 | 0 | 18 | 18 | 34 | 22 | 0 | 16 | 23 | 20 |
| 16:30 | to | 17:00 | 27 | 0 | 10 | 27 | 19 | 31 | 0 | 16 | 18 | 22 | 19 | 0 | 12 | 29 | 17 |
| 17:00 | to | 17:30 | 25 | 0 | 6 | 21 | 17 | 23 | 0 | 14 | 20 | 23 | 15 | 0 | 10 | 25 | 15 |
| Ava | ilable Space | es = | 40 | 53 | 28 | | 145 | 40 | 53 | 28 | | 145 | 40 | 53 | 28 | | 145 |



Trip Generation Proxy Counts


































SURVEYOR & GEOTECH ENGINEER TO LOCATE BUILDING AND TO CONFIRM SOILS AND COMPACTION.

LEGAL DESCRIPTION OF PROPERTY:

BLOCK 4

PLAN 43M-879 CITY OF BRAMPTON

BOUNDARY INFORMATION FROM SURVEY BY: LLOYD & PURCELL LTD,. ONTARIO LAND SURVEYORS, 2015.

| STATISTIC | ZONING | PROPOSED |
|-----------------------------------|---|----------------------|
| LOT AREA | 2,000 m² / 21527sf | 7,972 m² / 85,809 sf |
| LOT COVERAGE | NO MAX. | 45 % |
| MAX. % ACCESSORY RETAIL | 15% OF TOTAL GFA | 4.6% |
| MIN. LOADING SPACE REQUIREMENT | 5 spaces | 16 spaces |
| COMMERCIAL SELF | | |
| STORAGE WAREHOUSE | 109 | - |
| RETAIL ESTABLISHMENT | 41 | - |
| TOTAL | 150 | 41 |
| | | |
| FRONT YARD LANDSCAPE AREA | | 21.5% |
| FRONT YARD LANDSCAPE BUFFEF | २ | 0 m |
| EXTERIOR SIDE YARD LANDSCAPE ARE | A 238.14m ² | 44.86% |
| | | |
| Ground Floor Dymon Warehouse Reta | ail 564 m ² (6,070 sf ²) | |
| * | | |
| Ground Floor Dymon | 696 m² (7,502 sf ²) | |
| Second Floor Dymon | 3,508 m ² (37,759 s | f ²) |
| Third Floor Dymon | 3,544 m² (38,147 s | f ²) |

| Fourth Floor Dymon | 3,544 m² (38,147 sf ²) |
|------------------------------------|--------------------------------------|
| PROPOSED Self-Storage Ground Floor | 1,156 m² (12,443 sf²) |
| TOTAL SELF STORAGE | 12,448 m² (133,998 sf ²) |

TOTAL GFA WITH 4 STOREYS 13,012 m² (140,068 sf²)

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| PROPERTY LINE |
|---|
| LANDS TO BE DEDICATED TO REGION OF PEEL |
| BUILDING ENTRY/EXIT |
| NEW CONCRETE PAVING NEW PRECAST CONCRETE PERMEABLE PAVING LANDSCAPED AREA — SEE LANDSCAPE. |
| NEW CURB |
| NEW MOUNTABLE CURB |
| EXISTING FIRE HYDRANT |
| EXISTING CATCH BASIN |
| EXISTING MANHOLE |
| EXISTING LIGHT STANDARD |
| SIAMESE CONNECTION |
| NEW CATCH BASIN |
| NEW MANHOLE (STORM) |
| NEW MANHOLE (SANITARY) |
| ORNAMENTAL FENCE |
| NLS (NEW LIGHT STANDARD) SEE ELECTRICAL |

| 1. dra dis wor 2. of mu and per | Contractor ma wings, details crepancies to rk. All drawings service and a st be returned may not b rmission. | ust verify all job dim , specifications and r owners before proce and specifications are the property of the a ed at the completion be reproduced without | ensions, all report any reding with instruments inchitects which of the work, their written |
|---|--|---|---|
| | | | |
| | | | |
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| | | | |
| 19 | ISSUED FOR | DISCUSSION | 2020/06/24 |
| 18 17 | ISSUED FOR REVISED TO I | PERMIT PERMIT | 2018/09/21 2017/11/08 |
| 16 15 | REVISED FOR FOR FINAL S | REGION OF PEEL TTE PLAN APPLICATION | 2017/09/08 2017/08/31 |
| 14 13 | ISSUED FOR REVISED FOR | TENDER REGION OF PEEL | 2017/08/17 2017/08/16 |
| 12 | REVISED FOR | APPROVAL | 2017/07/19 |
| 10 | REVISED FOR | APPROVAL | 2017/07/10 |
| 9 8 | FOR PERMIT | APPROVAL APPLICATION | 2017/06/28 2017/05/10 |
| 7 6 | FOR FINAL S FOR PERMIT | ITE PLAN APPLICATION APPLICATION | 2017/04/12 - 2017/03/03 - |
| 5 4 | REVISED FOR FOR CLIENT | R SUBMISSION REVIEW | 2017/02/1 2017/01/23 |
| 3 | REVISED FOR | SUBMISSION VARIENCE SUBMISSION | 2017/01/06 |
| 2 1 nof | FOR SITE PLA | AN APPLICATION REVOI | 2016/08/16 |
| ret re | visions | | date |
| | / | AND ASSOCIATION OF COMPANY | |
| DESIGN | ARCHITECT 66 | TACT A OR College St (Rear Lane) To email: | Architecture Inc. ronto ON M6G 1B8 tel: (416 516 1949) info@tactdesign.ca |
| STRUCT | URAL ENGINEER | Cleland Jardine E | ngineering Ltd. |
| | | 200-580 Terry Fox Drive, H tel: (613) 591-1533 | Kanata ON K2L 4B9 fax: (613) 591-1703 |
| MECHA | NICAL/ELECTRICAL | e-mail: mail@ Tristar E | oclelandjardine.com |
| | 118-30 We | st Beaver Creek Rd., Richmon | nd Hill, ON L4B 3K1 |
| 01.41.5 | | tel: (905) 882 1662 | fax: (905) 882 0736 |
| CIVILE | NGINEER | COIE E 70 Valleywood Drive, Ma | rkham ON L3R 4T5 |
| | tel: (416) | 987-6161 or (905) 940-6161 www. | fax: (905) 940-2064 coleengineering.ca |
| PLANN | NG & URBAN DESIGN | | Fotenn |
| | | 223 McLeod Street, C tel: (613) 730-5709 | Ottawa ON K2P 0Z8 fax: (613) 730-1136 |
| | | | www.fotenn.com |
| OWN | Dym | on Capital Corpora | tion |
| | · | 2-1830 Walkley Road Ottawa ON K1H 8K3 | |
| | tel: 613 | -247-0888 fax: 613-247 | -7730 |
| TRU | E | PROJECT | |
| NOF | | NORTH | |
| | | y | |
| | ·'tt | | |
| arcı | nichol | 137 Pami | lla Street, |
| | caragia | t: 613 2 | UN KIS 3K9 37 6801 |
| | archite | ct 613 2 | s/8289 Incarchitect.ca |
| | | inc. WWW.nc | architect.ca |
| proj | ect & locatio | n | |
| | DYMO | N SELF-STOF | RAGE |
| | Ę | NEVETS ROAD | |
| | В | RAMPTON, ONT. | |
| CITY | FILE NUMBE | R | |
| | | SP16-013 | 3.000 |
| title | of drawing | | |
| | ÷ | SITE PLAN | |
| | | | |
| sca | le | drawing | |
| 1:2 | 250 | | |
| <i>date</i> JAN | , 2016 | Δ1 | _1 |
| dra | wn by | | I |

KL SS DL



| Intersection: | Nevets Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|--|
| Site Code: | 2204600019 |
| Count Date: | Feb 15, 2022 |

| Specified Pe | riod | One Hour Peak | | | | | |
|--------------|----------|---------------|----------|--|--|--|--|
| From: | 07:00:00 | From: | 07:30:00 | | | | |
| To: | 09:00:00 | To: | 08:30:00 | | | | |

Weather conditions:

Clear

** Unsignalized Intersection **







| Intersection: | Nevets Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|--|
| Site Code: | 2204600019 |
| Count Date: | Feb 15, 2022 |
| Period: | 07:00 - 09:00 |

Peak Hour Data (07:30 - 08:30)

| | | l Cor | North <i>A</i> nmeric | Approac al Entra | h ance | | 5 N | evets | outh A Rd (Dy | Approac mon Se | :h lf-Stora | ge) | | | East A | pproach ets Rd | ו | | | | West A Neve | pproacl ets Rd | ı | | Total |
|----------------|---|----------|--------------------------|---------------------|-----------|-------|-----|-------|------------------|-------------------|----------------|-------|------|---|--------|-------------------|------|-------|---|---|----------------|-------------------|------|-------|-------|
| Start Time | 4 | t | • | n | Peds | Total | - | t | • | ŋ | Peds | Total | • | t | • | ŋ | Peds | Total | 4 | t | | n | Peds | Total | es |
| 07:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 07:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 |
| 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 3 |
| 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 2 | 5 |
| Approach % | 0 | 0 | 0 | 0 | | - | 100 | 0 | 0 | 0 | | - | 100 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | |
| Totals % | 0 | 0 | 0 | 0 | | 0 | 40 | 0 | 0 | 0 | | 40 | 20 | 0 | 0 | 0 | | 20 | 0 | 0 | 40 | 0 | | 40 | |
| PHF | 0 | 0 | 0 | 0 | | 0 | 0.5 | 0 | 0 | 0 | | 0.5 | 0.25 | 0 | 0 | 0 | | 0.25 | 0 | 0 | 0.5 | 0 | × | 0.5 | 0.42 |
| Cars | 0 | 0 | 0 | 0 | | 0 | 2 | 0 | 0 | 0 | | 2 | 1 | 0 | 0 | 0 | | 1 | 0 | 0 | 2 | 0 | | 2 | 5 |
| % Cars | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 0 | 0 | | 100 | 100 | 0 | 0 | 0 | | 100 | 0 | 0 | 100 | 0 | | 100 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 1 | - | | | | | 0 | - | | | | | 0 | - | 1 |
| % Peds | | | | | 0 | - | | | | | 100 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Nevets Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|--|
| Site Code: | 2204600019 |
| Count Date: | Feb 15, 2022 |

| Specified Pe | riod | One Hour Peak | | | | | |
|--------------|----------|---------------|----------|--|--|--|--|
| From: | 16:00:00 | From: | 16:00:00 | | | | |
| To: | 18:00:00 | To: | 17:00:00 | | | | |

Weather conditions:

Clear

** Unsignalized Intersection **

Major Road: Nevets Rd runs E/W





| Intersection: | Nevets Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|--|
| Site Code: | 2204600019 |
| Count Date: | Feb 15, 2022 |
| Period: | 16:00 - 18:00 |

Peak Hour Data (16:00 - 17:00)

| | | l Cor | North <i>I</i> nmeric | Approac al Entra | h Ince | | 5 N | South A Rd (Dvi | approaction of the second s | :h lf-Stora | ige) | | | East Ap | pproach ets Rd | ۱ | | West Approach Nevets Rd | | | | | | | |
|----------------|---|----------|--------------------------|---------------------|-----------|-------|------|--------------------|---|----------------|------|-------|------|---------|-------------------|---|------|----------------------------|---|---|------|---|------|-------|--------------|
| Start Time | 4 | 1 | • | J | Peds | Total | 1 | 1 | P | ŋ | Peds | Total | 4 | t | • | ŋ | Peds | Total | • | t | • | ŋ | Peds | Total | Vehicl es |
| 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 3 | 6 |
| 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 16:30 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 5 |
| 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 4 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 5 | 0 | 0 | 5 | 14 |
| Approach % | 0 | 0 | 0 | 0 | | - | 50 | 0 | 50 | 0 | | - | 100 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | |
| Totals % | 0 | 0 | 0 | 0 | | 0 | 28.6 | 0 | 28.6 | 0 | | 57.1 | 7.1 | 0 | 0 | 0 | | 7.1 | 0 | 0 | 35.7 | 0 | | 35.7 | |
| PHF | 0 | 0 | 0 | 0 | | 0 | 0.5 | 0 | 0.5 | 0 | | 0.67 | 0.25 | 0 | 0 | 0 | | 0.25 | 0 | 0 | 0.42 | 0 | | 0.42 | 0.58 |
| Cars | 0 | 0 | 0 | 0 | | 0 | 4 | 0 | 4 | 0 | | 8 | 1 | 0 | 0 | 0 | | 1 | 0 | 0 | 5 | 0 | | 5 | 14 |
| % Cars | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 100 | 0 | | 100 | 100 | 0 | 0 | 0 | | 100 | 0 | 0 | 100 | 0 | | 100 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Airport Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|---|
| Site Code: | 2204600020 |
| Count Date: | Feb 15, 2022 |

| Specified Pe | riod | One Hour Pe | eak |
|---------------------|----------|-------------|----------|
| From: | 07:00:00 | From: | 08:00:00 |
| To: | 09:00:00 | To: | 09:00:00 |

Major Road: Airport Rd runs N/S

Weather conditions:

Clear

** Unsignalized Intersection **

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🚘 - Cars

🖵 - Trucks



| Intersection: | Airport Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|---|
| Site Code: | 2204600020 |
| Count Date: | Feb 15, 2022 |
| Period: | 07:00 - 09:00 |

Peak Hour Data (08:00 - 09:00)

| | | I | North A | pproac | :h | | | : | South A | pproac | :h | | | | East Ap | oproach | | | West Approach | | | | | | Total |
|----------------|---|---|---------|--------|------|-------|---|---|---------|--------|------|-------|-----|--------|---------|---------|----------|-------|---------------|---|---|---|------|-------|--------|
| | | | Airpo | οττ κα | | | | | Airpo | ort ka | | | 5 1 | levets | Ka (Dyr | non se | IT-Stora | ige) | | | | | | | Vehicl |
| Start Time | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | - | 1 | | J | Peds | Total | es |
| 08:00 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 0 |
| 08:15 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 1 |
| 08:30 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 0 |
| 08:45 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 1 | 0 | 0 | 1 | | | | | 0 | | 2 |
| Grand Total | 0 | 0 | | 0 | 0 | 0 | | 0 | 2 | 0 | 0 | 2 | 0 | | 1 | 0 | 0 | 1 | | | | | 0 | 0 | 3 |
| Approach % | 0 | 0 | | 0 | | - | | 0 | 100 | 0 | | - | 0 | | 100 | 0 | | - | | | | | | - | |
| Totals % | 0 | 0 | | 0 | | 0 | | 0 | 66.7 | 0 | | 66.7 | 0 | | 33.3 | 0 | | 33.3 | | | | | | 0 | |
| PHF | 0 | 0 | | 0 | | 0 | | 0 | 0.5 | 0 | | 0.5 | 0 | | 0.25 | 0 | | 0.25 | | | , | | | 0 | 0.38 |
| Cars | 0 | 0 | | 0 | | 0 | | 0 | 2 | 0 | | 2 | 0 | | 1 | 0 | | 1 | | | | | | 0 | 3 |
| % Cars | 0 | 0 | | 0 | | 0 | | 0 | 100 | 0 | | 100 | 0 | | 100 | 0 | | 100 | | | | | | 0 | 100 |
| Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| % Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Airport Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|---|
| Site Code: | 2204600020 |
| Count Date: | Feb 15, 2022 |

North Approach

0

0

0

In Total

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Out

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Peak Hour Diagram

| Specified Pe | riod | One Hour Pe | eak |
|--------------|----------|-------------|----------|
| From: | 16:00:00 | From: | 16:00:00 |
| To: | 18:00:00 | To: | 17:00:00 |

Weather conditions:

Clear

** Unsignalized Intersection **



Major Road: Airport Rd runs N/S





🖵 - Trucks



| Intersection: | Airport Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|---|
| Site Code: | 2204600020 |
| Count Date: | Feb 15, 2022 |
| Period: | 16:00 - 18:00 |

Peak Hour Data (16:00 - 17:00)

| | | I | North A Airpo | opproac | :h | | | | South A Airpo | ort Rd | :h | | 5 N | levets | East A Rd (Dy | pproacł mon Se | า lf-Stora | age) | | | West A | pproac | h | | Total Vehicl |
|----------------|---|---|------------------|---------|------|-------|---|---|------------------|--------|------|-------|-----|--------|------------------|-------------------|---------------|-------|---|---|--------|--------|------|-------|-----------------|
| Start Time | • | 1 | • | ŋ | Peds | Total | • | t | | J | Peds | Total | • | 1 | | J | Peds | Total | • | 1 | | J | Peds | Total | es |
| 16:00 | 0 | 0 | | 0 | 0 | 0 | | 0 | 2 | 0 | 0 | 2 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 2 |
| 16:15 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 0 |
| 16:30 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 0 |
| 16:45 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 1 |
| Grand Total | 0 | 0 | | 0 | 0 | 0 | | 0 | 3 | 0 | 0 | 3 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | 0 | 3 |
| Approach % | 0 | 0 | | 0 | | - | | 0 | 100 | 0 | | - | 0 | | 0 | 0 | | - | | | | | | - | |
| Totals % | 0 | 0 | | 0 | | 0 | | 0 | 100 | 0 | | 100 | 0 | | 0 | 0 | | 0 | | | | | | 0 | |
| PHF | 0 | 0 | | 0 | | 0 | | 0 | 0.38 | 0 | 1 | 0.38 | 0 | | 0 | 0 | 1 | 0 | | | | | | 0 | 0.38 |
| Cars | 0 | 0 | | 0 | | 0 | | 0 | 3 | 0 | | 3 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 3 |
| % Cars | 0 | 0 | | 0 | | 0 | | 0 | 100 | 0 | | 100 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 100 |
| Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| % Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Nevets Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|--|
| Site Code: | 2204600021 |
| Count Date: | Feb 12, 2022 |

| Specified Pe | riod | One Hour Po | eak |
|---------------------|----------|-------------|----------|
| From: | 11:00:00 | From: | 12:15:00 |
| To: | 14:00:00 | To: | 13:15:00 |

Weather conditions:

Clear

** Unsignalized Intersection **







| Intersection: | Nevets Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|--|
| Site Code: | 2204600021 |
| Count Date: | Feb 12, 2022 |
| Period: | 11:00 - 14:00 |

Peak Hour Data (12:15 - 13:15)

| | | l Cor | North <i>I</i> nmeric | Approac al Entra | h ance | | 5 N | evets | South A Rd (Dyr | pproac non Se | :h lf-Stora | ge) | | | East Aj Neve | oproach ets Rd | I | | | | West A Neve | pproach ts Rd | ו | | Total Vehicl |
|----------------|---|----------|--------------------------|---------------------|-----------|-------|------|-------|--------------------|------------------|----------------|-------|-----|---|-----------------|-------------------|------|-------|---|---|----------------|------------------|------|-------|-----------------|
| Start Time | • | 1 | | 9 | Peds | Total | • | t | • | J | Peds | Total | • | t | | 9 | Peds | Total | • | 1 | | J | Peds | Total | es |
| 12:15 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 4 |
| 12:30 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 3 | 0 | 0 | 3 | 6 |
| 12:45 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 5 | 0 | 0 | 5 | 11 |
| 13:00 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 4 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 2 | 0 | 0 | 11 | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 10 | 0 | 0 | 10 | 25 |
| Approach % | 0 | 0 | 0 | 0 | | - | 81.8 | 0 | 18.2 | 0 | | - | 100 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | |
| Totals % | 0 | 0 | 0 | 0 | | 0 | 36 | 0 | 8 | 0 | | 44 | 16 | 0 | 0 | 0 | | 16 | 0 | 0 | 40 | 0 | | 40 | |
| PHF | 0 | 0 | 0 | 0 | | 0 | 0.56 | 0 | 0.25 | 0 | | 0.69 | 0.5 | 0 | 0 | 0 | | 0.5 | 0 | 0 | 0.5 | 0 | | 0.5 | 0.57 |
| Cars | 0 | 0 | 0 | 0 | | 0 | 9 | 0 | 2 | 0 | | 11 | 4 | 0 | 0 | 0 | | 4 | 0 | 0 | 10 | 0 | | 10 | 25 |
| % Cars | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 100 | 0 | | 100 | 100 | 0 | 0 | 0 | | 100 | 0 | 0 | 100 | 0 | | 100 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Airport Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|---|
| Site Code: | 2204600022 |
| Count Date: | Feb 12, 2022 |

North Approach

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In Total

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Out

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Peak Hour Diagram

| Specified Pe | riod | One Hour Pe | eak |
|---------------------|----------|-------------|----------|
| From: | 11:00:00 | From: | 11:45:00 |
| To: | 14:00:00 | To: | 12:45:00 |

| Weather | |
|-------------|--|
| conditions: | |

Clear

** Unsignalized Intersection **



🚘 - Cars

🗔 - Trucks



| Intersection: | Airport Rd & 5 Nevets Rd (Dymon Self-Storage) |
|---------------|---|
| Site Code: | 2204600022 |
| Count Date: | Feb 12, 2022 |
| Period: | 11:00 - 14:00 |

Peak Hour Data (11:45 - 12:45)

| | | ľ | North A Airpo | ort Rd | :h | | | : | South A Airpo | ort Rd | h | | 5 N | levets | East Aj Rd (Dyi | oproach mon Se | า lf-Stora | ige) | | | Total Vehicl | | | | |
|----------------|---|---|------------------|--------|------|-------|---|---|------------------|--------|------|-------|-----|--------|--------------------|-------------------|---------------|-------|---|---|-----------------|---|------|-------|-----|
| Start Time | • | 1 | | J | Peds | Total | • | 1 | • | J | Peds | Total | 1 | 1 | • | J | Peds | Total | - | 1 | • | J | Peds | Total | es |
| 11:45 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 1 |
| 12:00 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 1 | 0 | 0 | 1 | | | | | 0 | | 2 |
| 12:15 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 0 |
| 12:30 | 0 | 0 | | 0 | 0 | 0 | | 0 | 2 | 0 | 0 | 2 | 0 | | 1 | 0 | 0 | 1 | | | | | 0 | | 3 |
| Grand Total | 0 | 0 | | 0 | 0 | 0 | | 0 | 4 | 0 | 0 | 4 | 0 | | 2 | 0 | 0 | 2 | | | | | 0 | 0 | 6 |
| Approach % | 0 | 0 | | 0 | | - | | 0 | 100 | 0 | | - | 0 | | 100 | 0 | | - | | | | | | - | |
| Totals % | 0 | 0 | | 0 | | 0 | | 0 | 66.7 | 0 | | 66.7 | 0 | | 33.3 | 0 | | 33.3 | | | | | | 0 | |
| PHF | 0 | 0 | | 0 | | 0 | | 0 | 0.5 | 0 | | 0.5 | 0 | | 0.5 | 0 | | 0.5 | | | | | | 0 | 0.5 |
| Cars | 0 | 0 | | 0 | | 0 | | 0 | 4 | 0 | | 4 | 0 | | 2 | 0 | | 2 | | | | | | 0 | 6 |
| % Cars | 0 | 0 | | 0 | | 0 | | 0 | 100 | 0 | | 100 | 0 | | 100 | 0 | | 100 | | | | | | 0 | 100 |
| Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| % Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| STATISTIC | CS | | LE | GEND |
|--|---|--|-------------------------|---|
| | | | | |
| | | | | |
| LEGAL DESCRIPTION OF | PROPERTY: | | | PROPOSED BUILDING LOCATION |
| THE 41,719m ² PROPER QUEENSWAY IS LOCATED ROAD AND THE QUEENS | TY KNOWN MUNICIPALLY . O AT THE NORTHEAST CO SWAY IN THE CITY OF TO | AS 1460 THE RNER OF VANSCO RONTO (ETOBICOKE). | | EXISTING NEIGHBORING BUILDINGS |
| BOUNDARY INFORMATION SURVEYING LTD. | N FROM SURVEY BY: DAVI | D B. SEARLES | | LANDSCAPED AREA |
| | | | | CONCRETE/ SIDEWALK |
| BUILDING FOOTPRINT | | | | BARRIER FREE PARKING CLEARANCE |
| (INCLUDING INTERIOR LO | 27,568 m ² | (314,411 ft ²) (371,860 ft ²) | | INTERLOCKING PAVING STONE (EXISTING TO REMAIN OR REUSE) |
| TOTAL RECEPTION | 1,231 m² (1 | 3,212 ft ²) | | CURB |
| TOTAL OFFICE | 2,192 m² (2 | 24,749 ft²) | <u> </u> | DEPRESSED CURB |
| TOTAL GFA | 30,991 m² | (397,956 ft ²) | | NEW TREE/ VEGETATION (REFER TO LANDSCAPE PLAN FOR TYPE, SIZE AND LOCATION) |
| PARKING STATISTICS | | | | |
| REQUIRED | | PROPOSED | | EXISTING TREE (VEGETATION IS FOR REFERENCE ONLY, |
| CURRENT E1.0 ZONING | FORMER CITY OF ETOBICOKE BY-LAW | | | REFER TO LANDSCAPE PLAN) |
| 206 SPACES | 359 SPACES | 266 EXT. SPACES 59 INT. SPACES | 6 | BARRIER FREE PARKING |
| | | 325 TOTAL | | INTERIOR PARKING |
| FOR A COMPLETE LIST BOTH ZONING CATEGORI APPENDIX A OF THE AS | OF THE PERFORMANCE S IES PLEASE REFER TO TH SSOCIATED PLANNING RAT | TANDARDS FOR IE TABLE IN IONALE REPORT. | <u>□</u> ⊗ | CATCH BASIN |
| | | | トレ | SIAMESE CONNECTION |
| | | | | ENTRANCE/ EXIT LOCATION |
| | | | | TRANSFORMER |
| | | | | FENCE & GATE |
| | | | Quit | MAN HOLE COVER |
| | | | • MP(1) | WOOD POLE (HYDRO) |
| | | | \OPERATURE\$ | FIRE HYDRANT |
| | | | ⊢ ∎ | NLS (NEW LIGHT STANDARD, REFER TO ELECTRICAL) |
| | | | • | NEW BOLLARD |
| | | | | |

BOUNDARY INFORMATION FROM SURVEY BY: DAVID B. SEARLES SURVEYING LTD. ONTARIO LAND SURVEYORS. 04 MAY 2016

CIFIC **A** , ר Ú

[10176

36'-0¹⁄2"

[10986]



2015.0035.01 DYM-ON-ETOBIQUEEN146



| Specified Pe | riod | One Hour P | eak |
|--------------|----------|------------|----------|
| From: | 07:00:00 | From: | 07:45:00 |
| To: | 09:00:00 | To: | 08:45:00 |

0

118

118

| Intersection: | Wickman Rd & Dymon Self-Storage |
|---------------|---------------------------------|
| Site Code: | 2204600023 |
| Count Date: | Feb 15, 2022 |

Weather conditions:

Clear

** Unsignalized Intersection ** Major Road: Wickman Rd runs E/W **North Approach Dymon Self-Storage East Approach** In Total In Total Out Out G 0 0 0 10 11 121 64 185 æ 1 0 Ø 1 0 0 0 0 0 1 1 ₽ 딦 0 Totals 1 0 1 10 11 121 65 186 Peds: 0 Wickman Rd Wickman Rd Ν **⊟** Totals Totals ₽ æ ₽ Peds: 0 Peds: 0 0 0 0 0 0 0 7 0 7 3 3 0

West Approach In Total Out 70 118 188 ⊟ 1 0 딦 1 71 118 189

1

63

64

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🚘 - Cars

🗔 - Trucks



| Wickman Rd & Dymon Self-Storage |
|---------------------------------|
| 2204600023 |
| Feb 15, 2022 |
| 07:00 - 09:00 |
| |

Peak Hour Data (07:45 - 08:45)

| | | N Dy | North A mon S | Approac elf-Stor | :h age | | | 9 | South / | Approac | h | | | | East Ap Wickn | oproach nan Rd | ı | | | | Total Vehicl | | | | |
|----------------|------|---------|------------------|---------------------|-----------|-------|---|---|---------|---------|------|-------|---|------|------------------|-------------------|------|-------|------|------|-----------------|---|------|-------|------|
| Start Time | • | 1 | • | J | Peds | Total | • | 1 | | J | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | es |
| 07:45 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | | 25 | 0 | 0 | 0 | 25 | 3 | 17 | | 0 | 0 | 20 | 45 |
| 08:00 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | | 18 | 0 | 0 | 0 | 18 | 0 | 12 | | 0 | 0 | 12 | 30 |
| 08:15 | 1 | | 0 | 0 | 0 | 1 | | | | | 0 | | | 35 | 1 | 0 | 0 | 36 | 1 | 18 | | 0 | 0 | 19 | 56 |
| 08:30 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | | 40 | 2 | 0 | 0 | 42 | 3 | 17 | | 0 | 0 | 20 | 62 |
| Grand Total | 1 | | 0 | 0 | 0 | 1 | | | | | 0 | 0 | | 118 | 3 | 0 | 0 | 121 | 7 | 64 | | 0 | 0 | 71 | 193 |
| Approach % | 100 | | 0 | 0 | | - | | | | | | - | | 97.5 | 2.5 | 0 | | - | 9.9 | 90.1 | | 0 | | - | |
| Totals % | 0.5 | | 0 | 0 | | 0.5 | | | | | | 0 | | 61.1 | 1.6 | 0 | | 62.7 | 3.6 | 33.2 | | 0 | | 36.8 | |
| PHF | 0.25 | | 0 | 0 | | 0.25 | | | | | | 0 | | 0.74 | 0.38 | 0 | | 0.72 | 0.58 | 0.89 | | 0 | | 0.89 | 0.78 |
| Cars | 1 | | 0 | 0 | | 1 | | | | | | 0 | | 118 | 3 | 0 | | 121 | 7 | 63 | | 0 | | 70 | 192 |
| % Cars | 100 | | 0 | 0 | | 100 | | | | | | 0 | | 100 | 100 | 0 | | 100 | 100 | 98.4 | | 0 | | 98.6 | 99.5 |
| Trucks | 0 | | 0 | 0 | | 0 | | | | | | 0 | | 0 | 0 | 0 | | 0 | 0 | 1 | | 0 | | 1 | 1 |
| % Trucks | 0 | | 0 | 0 | | 0 | | | | | | 0 | | 0 | 0 | 0 | | 0 | 0 | 1.6 | | 0 | | 1.4 | 0.5 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Specified Pe | riod | One Hour Po | eak |
|---------------------|----------|-------------|----------|
| From: | 16:00:00 | From: | 16:15:00 |
| To: | 18:00:00 | To: | 17:15:00 |

| Intersection: | Wickman Rd & Dymon Self-Storage |
|---------------|---------------------------------|
| Site Code: | 2204600023 |
| Count Date: | Feb 15, 2022 |

Weather conditions:

Clear

** Unsignalized Intersection ** Major Road: Wickman Rd runs E/W North Approach **Dymon Self-Storage East Approach** In Total In Total Out Out 5 0 0 0 0 271 5 5 145 126 æ Ø 3 2 0 0 0 0 0 0 0 ₽ 딦 2 Totals 3 0 5 0 271 5 145 126 Peds: 4 Wickman Rd Wickman Rd Ν **⊟** Totals Totals ₽ æ ₽ Peds: 0 Peds: 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 124 145 145 124 -Peds: 0 West Approach In Total Out

🚘 - Cars

148

0

148

124

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124

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272

272

0

🖵 - Trucks



| Intersection: | Wickman Rd & Dymon Self-Storage |
|---------------|---------------------------------|
| Site Code: | 2204600023 |
| Count Date: | Feb 15, 2022 |
| Period: | 16:00 - 18:00 |
| | |

Peak Hour Data (16:15 - 17:15)

| | | N Dy | lorth A mon Se | Approace elf-Stor | :h age | | | : | South A | Approac | h | | | | East A Wickr | pproach nan Rd | 1 | | | , | West Aj Wickm | oproach nan Rd | ı | | Total |
|----------------|------|---------|-------------------|----------------------|-----------|-------|---|---|---------|---------|------|-------|---|----------|-----------------|-------------------|------|-------|---|------|------------------|-------------------|------|-------|-------|
| Start Time | • | 1 | • | n | Peds | Total | • | t | | ŋ | Peds | Total | • | t | • | ŋ | Peds | Total | • | t | • | ŋ | Peds | Total | es |
| 16:15 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | | 42 | 0 | 0 | 0 | 42 | 0 | 30 | | 0 | 0 | 30 | 72 |
| 16:30 | 2 | | 1 | 0 | 0 | 3 | | | | | 0 | | | 38 | 0 | 0 | 0 | 38 | 0 | 35 | | 0 | 0 | 35 | 76 |
| 16:45 | 0 | | 0 | 0 | 4 | 0 | | | | | 0 | | | 33 | 0 | 0 | 0 | 33 | 0 | 25 | | 0 | 0 | 25 | 58 |
| 17:00 | 0 | | 2 | 0 | 0 | 2 | | | | | 0 | | | 32 | 0 | 0 | 0 | 32 | 0 | 34 | | 0 | 0 | 34 | 68 |
| Grand Total | 2 | | 3 | 0 | 4 | 5 | | | | | 0 | 0 | | 145 | 0 | 0 | 0 | 145 | 0 | 124 | | 0 | 0 | 124 | 274 |
| Approach % | 40 | | 60 | 0 | | - | | | | | | - | | 100 | 0 | 0 | | - | 0 | 100 | | 0 | | - | |
| Totals % | 0.7 | | 1.1 | 0 | | 1.8 | | | | | | 0 | | 52.9 | 0 | 0 | | 52.9 | 0 | 45.3 | | 0 | | 45.3 | |
| PHF | 0.25 | | 0.38 | 0 | | 0.42 | | | | | | 0 | | 0.86 | 0 | 0 | | 0.86 | 0 | 0.89 | N | 0 | | 0.89 | 0.9 |
| Cars | 2 | | 3 | 0 | | 5 | | | | | | 0 | | 145 | 0 | 0 | | 145 | 0 | 124 | | 0 | | 124 | 274 |
| % Cars | 100 | | 100 | 0 | | 100 | | | | | | 0 | | 100 | 0 | 0 | | 100 | 0 | 100 | | 0 | | 100 | 100 |
| Trucks | 0 | | 0 | 0 | | 0 | | | | | | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | 0 |
| % Trucks | 0 | | 0 | 0 | | 0 | | | | | | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | 0 |
| Peds | | | | | 4 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 4 |
| % Peds | | | | | 100 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Vansco Rd & Dymon Self-Storage (south driveway) |
|---------------|---|
| Site Code: | 2204600024 |
| Count Date: | Feb 15, 2022 |

North Approach

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In Total

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Peak Hour Diagram

| Specified Pe | riod | One Hour Pe | eak |
|---------------------|----------|-------------|----------|
| From: | 07:00:00 | From: | 08:00:00 |
| To: | 09:00:00 | To: | 09:00:00 |

Weather conditions:

Vansco Rd

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Peds: 0

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Peds: 0

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Vansco Rd

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Peds: 0

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Totals

Peds: 0

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Clear

** Unsignalized Intersection **



Major Road: Vansco Rd runs N/S





🚘 - Cars

🗔 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (south driveway) |
|---------------|---|
| Site Code: | 2204600024 |
| Count Date: | Feb 15, 2022 |
| Period: | 07:00 - 09:00 |

Peak Hour Data (08:00 - 09:00)

| | | I | North A | pproad | :h | | | 9 | South A | pproac | :h | | Dym | on Solf | East Ap | proach |) ·h drive | wav) | | | West A | | Total | | |
|----------------|------|---|---------|----------|------|-------|---|---|---------|----------|------|-------|----------|---------|---------|----------|---------------|-------|---|---|--------|---|-------|-------|--------------|
| Start Time | 4 | t | P | 1 | Peds | Total | • | t | P | 1 | Peds | Total | 1 | 1 | r | 1 | Peds | Total | 4 | t | | ŋ | Peds | Total | Vehicl es |
| 08:00 | 0 | 0 | | 0 | 0 | 0 | | 0 | 4 | 0 | 0 | 4 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 4 |
| 08:15 | 0 | 0 | | 0 | 0 | 0 | | 0 | 4 | 0 | 0 | 4 | 0 | | 1 | 0 | 0 | 1 | | | | | 0 | | 5 |
| 08:30 | 1 | 0 | | 0 | 0 | 1 | | 0 | 1 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 2 |
| 08:45 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 1 |
| Grand Total | 1 | 0 | | 0 | 0 | 1 | | 0 | 10 | 0 | 0 | 10 | 0 | | 1 | 0 | 0 | 1 | | | | | 0 | 0 | 12 |
| Approach % | 100 | 0 | | 0 | | - | | 0 | 100 | 0 | | - | 0 | | 100 | 0 | | - | | | | | | - | |
| Totals % | 8.3 | 0 | | 0 | | 8.3 | | 0 | 83.3 | 0 | | 83.3 | 0 | | 8.3 | 0 | | 8.3 | | | | | | 0 | |
| PHF | 0.25 | 0 | | 0 | | 0.25 | | 0 | 0.63 | 0 | | 0.63 | 0 | | 0.25 | 0 | | 0.25 | | | | | | 0 | 0.6 |
| Cars | 1 | 0 | | 0 | | 1 | | 0 | 10 | 0 | | 10 | 0 | | 1 | 0 | | 1 | | | | | | 0 | 12 |
| % Cars | 100 | 0 | | 0 | | 100 | | 0 | 100 | 0 | | 100 | 0 | | 100 | 0 | | 100 | | | | | | 0 | 100 |
| Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| % Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Vansco Rd & Dymon Self-Storage (south driveway) |
|---------------|---|
| Site Code: | 2204600024 |
| Count Date: | Feb 15, 2022 |

North Approach

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In Total

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Peak Hour Diagram

| Specified Pe | riod | One Hour Pe | eak |
|--------------|----------|-------------|----------|
| From: | 16:00:00 | From: | 16:45:00 |
| To: | 18:00:00 | To: | 17:45:00 |

Weather conditions:

Vansco Rd

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Peds: 0

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Peds: 0

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Vansco Rd

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Peds: 0

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Totals

Peds: 0

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Clear

** Unsignalized Intersection **



Major Road: Vansco Rd runs N/S





🚘 - Cars

🗔 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (south driveway) |
|---------------|---|
| Site Code: | 2204600024 |
| Count Date: | Feb 15, 2022 |
| Period: | 16:00 - 18:00 |
| | |

Peak Hour Data (16:45 - 17:45)

| | | I | North A Vans | Approad co Rd | :h | | | | South A Vans | approad co Rd | :h | | Dvm | on Self | East A | pproact ge (sout | n :h drive | ewav) | | | West A | h | | | |
|----------------|---|---|-----------------|------------------|------|-------|---|---|-----------------|------------------|------|-------|-----|---------|--------|---------------------|---------------|-------|---|---|--------|---|------|-------|------|
| Start Time | 4 | t | • | ŋ | Peds | Total | • | t | | ŋ | Peds | Total | 1 | t | | J | Peds | Total | 4 | t | | n | Peds | Total | es |
| 16:45 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 0 |
| 17:00 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 0 |
| 17:15 | 0 | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 0 |
| 17:30 | 0 | 0 | | 0 | 0 | 0 | | 0 | 2 | 0 | 0 | 2 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 2 |
| Grand Total | 0 | 0 | | 0 | 0 | 0 | | 0 | 2 | 0 | 0 | 2 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | 0 | 2 |
| Approach % | 0 | 0 | | 0 | | - | | 0 | 100 | 0 | | - | 0 | | 0 | 0 | | - | | | | | | - | |
| Totals % | 0 | 0 | | 0 | | 0 | | 0 | 100 | 0 | | 100 | 0 | | 0 | 0 | | 0 | | | | | | 0 | |
| PHF | 0 | 0 | | 0 | | 0 | | 0 | 0.25 | 0 | | 0.25 | 0 | | 0 | 0 | | 0 | | | , | | | 0 | 0.25 |
| Cars | 0 | 0 | | 0 | | 0 | | 0 | 2 | 0 | | 2 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 2 |
| % Cars | 0 | 0 | | 0 | | 0 | | 0 | 100 | 0 | | 100 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 100 |
| Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| % Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |


| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 1) |
|---------------|--|
| Site Code: | 2204600025 |
| Count Date: | Feb 15, 2022 |

| Specified Pe | riod | One Hour Peak | | | | | | |
|---------------------|----------|---------------|----------|--|--|--|--|--|
| From: | 07:00:00 | From: | 07:45:00 | | | | | |
| To: | 09:00:00 | To: | 08:45:00 | | | | | |

Weather conditions:

Clear

** Unsignalized Intersection **







🗔 - Trucks



Intersection:Vansco Rd & Dymon Self-Storage (middle driveway 1)Site Code:2204600025Count Date:Feb 15, 2022Period:07:00 - 09:00

Peak Hour Data (07:45 - 08:45)

| | | ľ | North / Vans | Approac sco Rd | :h | | | | South A Vans | pproac co Rd | h | | Dymor | Self-S | East Ap Storage | proach (middl | n e drive | way 1) | West Approach Commerical Entrance | | | | | | Total Vehicl |
|----------------|-----|---|-----------------|-------------------|------|-------|---|---|-----------------|-----------------|------|-------|-------|--------|--------------------|------------------|--------------|--------|--------------------------------------|---|---|---|------|-------|-----------------|
| Start Time | • | 1 | • | J | Peds | Total | • | 1 | | J | Peds | Total | • | t. | • | J | Peds | Total | • | 1 | | J | Peds | Total | es |
| 07:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 08:00 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 08:15 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 08:30 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Grand Total | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 9 | 0 | 0 | 9 | 2 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| Approach % | 100 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | 66.7 | 0 | 33.3 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 25 | 0 | 0 | 0 | | 25 | 0 | 0 | 56.3 | 0 | | 56.3 | 12.5 | 0 | 6.3 | 0 | | 18.8 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0.5 | 0 | 0 | 0 | | 0.5 | 0 | 0 | 0.75 | 0 | | 0.75 | 0.5 | 0 | 0.25 | 0 | | 0.38 | 0 | 0 | 0 | 0 | | 0 | 0.8 |
| Cars | 4 | 0 | 0 | 0 | | 4 | 0 | 0 | 9 | 0 | | 9 | 2 | 0 | 1 | 0 | | 3 | 0 | 0 | 0 | 0 | | 0 | 16 |
| % Cars | 100 | 0 | 0 | 0 | | 100 | 0 | 0 | 100 | 0 | | 100 | 100 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 1) |
|---------------|--|
| Site Code: | 2204600025 |
| Count Date: | Feb 15, 2022 |

| Specified Pe | riod | One Hour Peak | | | | | | | |
|--------------|----------|---------------|----------|--|--|--|--|--|--|
| From: | 16:00:00 | From: | 16:00:00 | | | | | | |
| To: | 18:00:00 | To: | 17:00:00 | | | | | | |

Weather conditions:

Clear

** Unsignalized Intersection **

Major Road: Vansco Rd runs N/S





🖵 - Trucks



| le driveway 1) |
|----------------|
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Peak Hour Data (16:00 - 17:00)

| | | I | North / Vans | Approac sco Rd | :h | | | 2 | South A Vans | pproac co Rd | :h | | Dymon | Self-S | East Ap Storage | proach (middl | ı e drive | way 1) | West Approach Commerical Entrance | | | | | | Total Vehicl |
|----------------|------|---|-----------------|-------------------|------|-------|---|---|-----------------|-----------------|------|-------|-------|--------|--------------------|------------------|--------------|--------|--------------------------------------|---|---|---|------|-------|-----------------|
| Start Time | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | • | 9 | Peds | Total | • | 1 | • | J | Peds | Total | es |
| 16:00 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 16:15 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 16:30 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 16:45 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Grand Total | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 6 | 0 | 0 | 6 | 2 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Approach % | 100 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | 66.7 | 0 | 33.3 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 35.7 | 0 | 0 | 0 | | 35.7 | 0 | 0 | 42.9 | 0 | | 42.9 | 14.3 | 0 | 7.1 | 0 | | 21.4 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0.63 | 0 | 0 | 0 | | 0.63 | 0 | 0 | 0.75 | 0 | | 0.75 | 0.25 | 0 | 0.25 | 0 | | 0.38 | 0 | 0 | 0 | 0 | | 0 | 0.88 |
| Cars | 5 | 0 | 0 | 0 | | 5 | 0 | 0 | 6 | 0 | | 6 | 2 | 0 | 1 | 0 | | 3 | 0 | 0 | 0 | 0 | | 0 | 14 |
| % Cars | 100 | 0 | 0 | 0 | | 100 | 0 | 0 | 100 | 0 | | 100 | 100 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



Clear

Weather

conditions:

| Specified Pe | riod | One Hour Peak | | | | | | | |
|--------------|----------|---------------|----------|--|--|--|--|--|--|
| From: | 07:00:00 | From: | 08:00:00 | | | | | | |
| To: | 09:00:00 | To: | 09:00:00 | | | | | | |

| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 2) |
|---------------|--|
| Site Code: | 2204600026 |
| Count Date: | Feb 15, 2022 |

** Unsignalized Intersection **

Major Road: Vansco Rd runs N/S





🕞 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 2) |
|---------------|--|
| Site Code: | 2204600026 |
| Count Date: | Feb 15, 2022 |
| Period: | 07:00 - 09:00 |

Peak Hour Data (08:00 - 09:00)

| | | I | North / Van | Approad sco Rd | :h | | | | South A Vans | opproad co Rd | :h | | Dymon | Self-S | East Ap Storage | proach (middl | n e drive | way 2) | West Approach Commerical Entrance | | | | | | Total Vehicl |
|----------------|---|---|----------------|-------------------|------|-------|---|---|-----------------|------------------|------|-------|-------|--------|--------------------|------------------|--------------|--------|--------------------------------------|---|---|---|------|-------|-----------------|
| Start Time | • | 1 | | J | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | es |
| 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 08:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 08:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 08:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 6 | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| Approach % | 0 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | 50 | 0 | 50 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 75 | 0 | | 75 | 12.5 | 0 | 12.5 | 0 | | 25 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0.5 | 0 | | 0.5 | 0.25 | 0 | 0.25 | 0 | | 0.5 | 0 | 0 | 0 | 0 | | 0 | 0.5 |
| Cars | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 6 | 0 | | 6 | 1 | 0 | 1 | 0 | | 2 | 0 | 0 | 0 | 0 | | 0 | 8 |
| % Cars | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 100 | 0 | | 100 | 100 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Pea | k H | lour | Diag | ram |
|------|-----|------|------|------|
| r ca | | luui | | siam |

Clear

Weather

conditions:

| Specified Pe | riod | One Hour Pe | eak |
|--------------|----------|-------------|----------|
| From: | 16:00:00 | From: | 16:00:00 |
| To: | 18:00:00 | To: | 17:00:00 |

| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 2) |
|---------------|--|
| Site Code: | 2204600026 |
| Count Date: | Feb 15, 2022 |

** Unsignalized Intersection **

Major Road: Vansco Rd runs N/S





🖵 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 2) |
|---------------|--|
| Site Code: | 2204600026 |
| Count Date: | Feb 15, 2022 |
| Period: | 16:00 - 18:00 |
| | |

Peak Hour Data (16:00 - 17:00)

| | | I | North Van | Approad sco Rd | :h | | | | South A Vans | opproad co Rd | :h | | Dymor | Self-S | East Ap Storage | proach (middl | n e drive | way 2) | West Approach Commerical Entrance | | | | | | Total Vehicl |
|----------------|---|---|--------------|-------------------|------|-------|---|---|-----------------|------------------|------|-------|-------|--------|--------------------|------------------|--------------|--------|--------------------------------------|---|---|---|------|-------|-----------------|
| Start Time | • | 1 | | J | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | es |
| 16:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 16:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 3 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| Approach % | 0 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | 75 | 0 | 25 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 20 | 0 | | 20 | 60 | 0 | 20 | 0 | | 80 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0.25 | 0 | 1 | 0.25 | 0.25 | 0 | 0.25 | 0 | | 0.25 | 0 | 0 | 0 | 0 | | 0 | 0.25 |
| Cars | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 1 | 0 | | 1 | 3 | 0 | 1 | 0 | | 4 | 0 | 0 | 0 | 0 | | 0 | 5 |
| % Cars | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 100 | 0 | | 100 | 100 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Vansco Rd & Dymon Self-Storage (north driveway) |
|---------------|---|
| Site Code: | 2204600027 |
| Count Date: | Feb 15, 2022 |

| Specified Pe | riod | One Hour Pe | eak |
|---------------------|----------|-------------|----------|
| From: | 07:00:00 | From: | 08:00:00 |
| To: | 09:00:00 | To: | 09:00:00 |

Weather conditions:

Clear

** Unsignalized Intersection **







🗔 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (north driveway) |
|---------------|---|
| Site Code: | 2204600027 |
| Count Date: | Feb 15, 2022 |
| Period: | 07:00 - 09:00 |

Peak Hour Data (08:00 - 09:00)

| | | l | North Van | Approac sco Rd | :h | | | 9 | South A Vans | Approad sco Rd | :h | | Dymo | on Self | East Ap Storage | proach e (nort | n :h drive | way) | | West Approach Commerical Entrance | | | | | Total Vehicl |
|----------------|------|---|--------------|-------------------|------|-------|---|---|-----------------|-------------------|------|-------|------|---------|--------------------|-------------------|---------------|-------|---|--------------------------------------|---|---|------|-------|-----------------|
| Start Time | • | 1 | | J | Peds | Total | - | 1 | | J | Peds | Total | • | 1 | | J | Peds | Total | 1 | 1 | • | J | Peds | Total | es |
| 08:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 08:15 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 08:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 2 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 08:45 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Grand Total | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 0 | 3 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Approach % | 100 | 0 | 0 | 0 | | - | 0 | 0 | 0 | 0 | | - | 75 | 0 | 25 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 14.3 | 0 | 0 | 0 | | 14.3 | 0 | 0 | 0 | 0 | | 0 | 64.3 | 0 | 21.4 | 0 | | 85.7 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0.5 | 0 | 0 | 0 | | 0.5 | 0 | 0 | 0 | 0 | | 0 | 0.75 | 0 | 0.38 | 0 | | 0.6 | 0 | 0 | 0 | 0 | | 0 | 0.7 |
| Cars | 2 | 0 | 0 | 0 | | 2 | 0 | 0 | 0 | 0 | | 0 | 9 | 0 | 3 | 0 | | 12 | 0 | 0 | 0 | 0 | | 0 | 14 |
| % Cars | 100 | 0 | 0 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Vansco Rd & Dymon Self-Storage (north driveway) |
|---------------|---|
| Site Code: | 2204600027 |
| Count Date: | Feb 15, 2022 |

| Specified Pe | riod | One Hour Pe | eak |
|--------------|----------|-------------|----------|
| From: | 16:00:00 | From: | 16:30:00 |
| To: | 18:00:00 | To: | 17:30:00 |

Weather conditions:

Clear

** Unsignalized Intersection **







- Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (north driveway) |
|---------------|---|
| Site Code: | 2204600027 |
| Count Date: | Feb 15, 2022 |
| Period: | 16:00 - 18:00 |
| | |

Peak Hour Data (16:30 - 17:30)

| | | l | North Van | Approac sco Rd | :h | | | 9 | South A Vans | Approac sco Rd | :h | | Dyme | on Self | East Ap Storag | proach e (nort | n th drive | way) | West Approach Commerical Entrance | | | | | | Total Vehicl |
|----------------|---|---|--------------|-------------------|------|-------|---|---|-----------------|-------------------|------|-------|------|---------|-------------------|-------------------|---------------|-------|--------------------------------------|---|---|---|------|-------|-----------------|
| Start Time | • | 1 | | J | Peds | Total | • | 1 | | J | Peds | Total | • | 1 | • | J | Peds | Total | 1 | 1 | • | J | Peds | Total | es |
| 16:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 16:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 17:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 17:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 | 0 | 3 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| Approach % | 0 | 0 | 0 | 0 | | - | 0 | 0 | 0 | 0 | | - | 81.3 | 0 | 18.8 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 81.3 | 0 | 18.8 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0.81 | 0 | 0.75 | 0 | | 0.8 | 0 | 0 | 0 | 0 | | 0 | 0.8 |
| Cars | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 13 | 0 | 3 | 0 | | 16 | 0 | 0 | 0 | 0 | | 0 | 16 |
| % Cars | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Specified Pe | riod | One Hour P | eak |
|--------------|----------|------------|----------|
| From: | 11:00:00 | From: | 12:00:00 |
| To: | 14:00:00 | To: | 13:00:00 |

| Intersection: | Wickman Rd & Dymon Self-Storage |
|---------------|---------------------------------|
| Site Code: | 2204600028 |
| Count Date: | Feb 12, 2022 |

Weather conditions:

Clear

** Unsignalized Intersection ** Major Road: Wickman Rd runs E/W North Approach **Dymon Self-Storage East Approach** In Total In Total Out Out G 0 0 0 207 1 129 78 æ 1 2 0 Ø 1 0 0 0 0 0 0 0 ₽ 딦 0 Totals 1 0 1 207 1 2 129 78 Peds: 0 Wickman Rd Wickman Rd Ν **⊟** Totals Totals ₽ æ ₽ Peds: 0 Peds: 0 0 0 0 0 0 0 0 0 1 0 0 1 4 0 0 78 78 129 129 -Peds: 0 West Approach Out

 Out
 In
 Total

 ☞
 79
 130
 209

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 0
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 0

 79 130
 209

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 0
 10
 0







| Intersection: | Wickman Rd & Dymon Self-Storage |
|---------------|---------------------------------|
| Site Code: | 2204600028 |
| Count Date: | Feb 12, 2022 |
| Period: | 11:00 - 14:00 |
| | |

Peak Hour Data (12:00 - 13:00)

| | | | | - | | | | | | | | | | | | | | | | - | | | | | |
|--|------------------|----|--------------------|-------------|------|-------------------------|---|---|----------|---------|------|----------------------------|---|----------------------|-------------|------------------|------|---------------------------|--------------------|---------------------|---------|------------------|------|--------------------------|----------------------|
| | | N | North A | Approad | :h | | | 9 | South A | Approac | h | | | 1 | East A | pproach | 1 | | | | West Ap | oproact | 1 | | Total |
| | | Dy | mon 2 | en-stor | age | | | | | •• | | | | | WICKI | nan ku | | | | | WICKI | idii ku | | | Vehicl |
| Start Time | • | 1 | | 1 | Peds | Total | - | 1 | . | 1 | Peds | Total | - | 1 | • | 1 | Peds | Total | - | 1 | | n | Peds | Total | es |
| 12.00 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | | /2 | 0 | 0 | 0 | /2 | 1 | 10 | | ٥ | 0 | 20 | 62 |
| 12.00 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | | 45 | 0 | 0 | 0 | 45 | 0 | 19 | | 0 | 0 | 20 | 05 |
| 12:15 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | | 38 | 0 | 0 | 0 | 38 | 0 | 25 | | 0 | 0 | 25 | 03 |
| 12:30 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | | 22 | 0 | 0 | 0 | 22 | 0 | 21 | | 0 | 0 | 21 | 43 |
| 12:45 | 0 | | 1 | 0 | 0 | 1 | | | | | 0 | | | 26 | 0 | 0 | 0 | 26 | 0 | 13 | | 0 | 0 | 13 | 40 |
| Grand | | | | | | | | | | | | | | | | | | | | | | | | | |
| Total | 0 | | 1 | 0 | 0 | 1 | | | | | 0 | 0 | | 129 | 0 | 0 | 0 | 129 | 1 | 78 | | 0 | 0 | 79 | 209 |
| | | | | | | | | | | | | | | | | | | | | | | | | | |
| Approach % | 0 | | 100 | 0 | | - | | | | | | - | | 100 | 0 | 0 | | - | 1.3 | 98.7 | | 0 | | - | |
| Totals % | 0 | | 0.5 | 0 | | 0.5 | | | | | | 0 | | 61.7 | 0 | 0 | | 61.7 | 0.5 | 37.3 | | 0 | | 37.8 | |
| | | | | | | | | | | | | | | | | | | | | | | | | | |
| PHF | 0 | | 0.25 | 0 | | 0.25 | | | | | | 0 | | 0.75 | 0 | 0 | | 0.75 | 0.25 | 0.78 | | 0 | | 0.79 | 0.83 |
| Cars | 0 | | 1 | 0 | | 1 | | | | | | 0 | | 129 | 0 | 0 | | 129 | 1 | 78 | | 0 | | 79 | 209 |
| % Cars | 0 | | 100 | 0 | | 100 | | | | | | 0 | | 100 | 0 | 0 | | 100 | 100 | 100 | | 0 | | 100 | 100 |
| Trucks | 0 | | 0 | 0 | | 0 | | | | | | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | 0 |
| % Trucks | 0 | | 0 | 0 | | 0 | | | | | | 0 | | 0 | 0 | 0 | | 0 | 0 | 0 | | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | _ | 0 |
| % Pods | | | | | 0 | _ | | | | | 0 | - | | | | | 0 | _ | | | | | 0 | - | 5 |
| Cars % Cars Trucks % Trucks Peds % Peds | 0 0 0 0 | | 1 100 0 0 | 0 0 0 | 0 | 1 100 0 - - | | | | | 0 | 0 0 0 0 - - | | 129 100 0 0 | 0 0 0 | 0 0 0 0 | 0 | 129 100 0 - - | 1 100 0 0 | 78 100 0 0 | | 0 0 0 0 | 0 | 79 100 0 - - | 209 100 0 0 |



| Intersection: | Vansco Rd & Dymon Self-Storage (south driveway) |
|---------------|---|
| Site Code: | 2204600029 |
| Count Date: | Feb 12, 2022 |

| Specified Pe | riod | One Hour Pe | eak |
|---------------------|----------|-------------|----------|
| From: | 11:00:00 | From: | 12:15:00 |
| To: | 14:00:00 | To: | 13:15:00 |

| Weather | |
|-------------|--|
| conditions: | |

Clear

** Unsignalized Intersection **

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🗔 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (south driveway) |
|---------------|---|
| Site Code: | 2204600029 |
| Count Date: | Feb 12, 2022 |
| Period: | 11:00 - 14:00 |
| | |

Peak Hour Data (12:15 - 13:15)

| | | I | North A Vans | Approad ico Rd | :h | | | : | South A Vans | oproad co Rd | :h | | Dym | on Self | East Ap Storag | oproach e (sout | n :h drive | eway) | | | West A | pproacl | ı | | Total |
|----------------|---|---|-----------------|-------------------|------|-------|---|---|-----------------|-----------------|------|-------|------|---------|-------------------|--------------------|---------------|-------|---|---|--------|---------|------|-------|-------|
| Start Time | • | 1 | | J | Peds | Total | • | t | | J | Peds | Total | • | 1 | | J | Peds | Total | • | 1 | | 9 | Peds | Total | es |
| 12:15 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 1 |
| 12:30 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 1 |
| 12:45 | 0 | 0 | | 0 | 0 | 0 | | 0 | 1 | 0 | 0 | 1 | 0 | | 0 | 0 | 0 | 0 | | | | | 0 | | 1 |
| 13:00 | 0 | 0 | | 0 | 0 | 0 | | 0 | 4 | 0 | 0 | 4 | 1 | | 1 | 0 | 0 | 2 | | | | | 0 | | 6 |
| Grand Total | 0 | 0 | | 0 | 0 | 0 | | 0 | 7 | 0 | 0 | 7 | 1 | | 1 | 0 | 0 | 2 | | | | | 0 | 0 | 9 |
| Approach % | 0 | 0 | | 0 | | - | | 0 | 100 | 0 | | - | 50 | | 50 | 0 | | - | | | | | | - | |
| Totals % | 0 | 0 | | 0 | | 0 | | 0 | 77.8 | 0 | | 77.8 | 11.1 | | 11.1 | 0 | | 22.2 | | | | | | 0 | |
| PHF | 0 | 0 | | 0 | | 0 | | 0 | 0.44 | 0 | | 0.44 | 0.25 | | 0.25 | 0 | | 0.25 | | | | | | 0 | 0.38 |
| Cars | 0 | 0 | | 0 | | 0 | | 0 | 7 | 0 | | 7 | 1 | | 1 | 0 | | 2 | | | | | | 0 | 9 |
| % Cars | 0 | 0 | | 0 | | 0 | | 0 | 100 | 0 | | 100 | 100 | | 100 | 0 | | 100 | | | | | | 0 | 100 |
| Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| % Trucks | 0 | 0 | | 0 | | 0 | | 0 | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | | | | | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 1) |
|---------------|--|
| Site Code: | 2204600030 |
| Count Date: | Feb 12, 2022 |

| Specified Pe | riod | One Hour Pe | eak |
|---------------------|----------|-------------|----------|
| From: | 11:00:00 | From: | 12:00:00 |
| To: | 14:00:00 | To: | 13:00:00 |

Weather conditions:

Clear

** Unsignalized Intersection **

Major Road: Vansco Rd runs N/S



Comments

🚘 - Cars

🖵 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 1) |
|---------------|--|
| Site Code: | 2204600030 |
| Count Date: | Feb 12, 2022 |
| Period: | 11:00 - 14:00 |

Peak Hour Data (12:00 - 13:00)

| | North Approach Vansco Rd | | | | | | | 2 | South A Vans | opproad co Rd | :h | | East Approach Dymon Self-Storage (middle driveway 1) | | | | | | | West Approach Commerical Entrance V | | | | | Total Vehicl |
|----------------|-----------------------------|---|---|---|------|-------|---|---|-----------------|------------------|------|-------|---|---|-----|---|------|-------|---|--|---|---|------|-------|-----------------|
| Start Time | • | 1 | | J | Peds | Total | - | 1 | • | J | Peds | Total | • | 1 | | J | Peds | Total | • | 1 | • | J | Peds | Total | es |
| 12:00 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 12:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 12:30 | 3 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 3 | 0 | 0 | 3 | 2 | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 12:45 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 2 | 1 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| Grand Total | 5 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 8 | 0 | 0 | 8 | 6 | 0 | 2 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 21 |
| Approach % | 100 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | 75 | 0 | 25 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 23.8 | 0 | 0 | 0 | | 23.8 | 0 | 0 | 38.1 | 0 | | 38.1 | 28.6 | 0 | 9.5 | 0 | | 38.1 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0.42 | 0 | 0 | 0 | | 0.42 | 0 | 0 | 0.67 | 0 | | 0.67 | 0.5 | 0 | 0.5 | 0 | | 0.67 | 0 | 0 | 0 | 0 | | 0 | 0.58 |
| Cars | 5 | 0 | 0 | 0 | | 5 | 0 | 0 | 8 | 0 | | 8 | 6 | 0 | 2 | 0 | | 8 | 0 | 0 | 0 | 0 | | 0 | 21 |
| % Cars | 100 | 0 | 0 | 0 | | 100 | 0 | 0 | 100 | 0 | | 100 | 100 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |



| Peak Hour Diagran |
|-------------------|
|-------------------|

Clear

Weather

conditions:

| Specified Pe | riod | One Hour Peak | | | | | | |
|---------------------|----------|---------------|----------|--|--|--|--|--|
| From: | 11:00:00 | From: | 11:15:00 | | | | | |
| To: | 14:00:00 | To: | 12:15:00 | | | | | |

| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 2) |
|---------------|--|
| Site Code: | 2204600031 |
| Count Date: | Feb 12, 2022 |

** Unsignalized Intersection **

Major Road: Vansco Rd runs N/S





🗔 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (middle driveway 2) |
|---------------|--|
| Site Code: | 2204600031 |
| Count Date: | Feb 12, 2022 |
| Period: | 11:00 - 14:00 |
| | |

Peak Hour Data (11:15 - 12:15)

| | North Approach Vansco Rd | | | | | | | 9 | South A Vans | Approad Sco Rd | :h | | East Approach Dymon Self-Storage (middle driveway 2) | | | | | | | West Approach Commerical Entrance | | | | | Total Vehicl |
|----------------|-----------------------------|---|---|---|------|-------|---|---|-----------------|-------------------|------|-------|---|---|---|---|------|-------|---|--------------------------------------|---|---|------|-------|-----------------|
| Start Time | • | 1 | | J | Peds | Total | - | 1 | | J | Peds | Total | 1 | 1 | | J | Peds | Total | - | 1 | • | J | Peds | Total | es |
| 11:15 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 11:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12:00 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| Grand Total | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 2 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Approach % | 100 | 0 | 0 | 0 | | - | 0 | 0 | 100 | 0 | | - | 0 | 0 | 0 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 50 | 0 | 0 | 0 | | 50 | 0 | 0 | 50 | 0 | | 50 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0.5 | 0 | 0 | 0 | | 0.5 | 0 | 0 | 0.5 | 0 | | 0.5 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0.5 |
| Cars | 2 | 0 | 0 | 0 | | 2 | 0 | 0 | 2 | 0 | | 2 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 4 |
| % Cars | 100 | 0 | 0 | 0 | | 100 | 0 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 1 | - | | | | | 0 | - | | | | | 0 | - | 1 |
| % Peds | | | | | 0 | - | | | | | 100 | - | | | | | 0 | - | | | | | 0 | - | |



| Intersection: | Vansco Rd & Dymon Self-Storage (north driveway) |
|---------------|---|
| Site Code: | 2204600032 |
| Count Date: | Feb 12, 2022 |

| Specified Pe | riod | One Hour Peak | | | | | | |
|---------------------|----------|---------------|----------|--|--|--|--|--|
| From: | 11:00:00 | From: | 13:00:00 | | | | | |
| To: | 14:00:00 | To: | 14:00:00 | | | | | |

Weather conditions:

Clear

** Unsignalized Intersection **







🗔 - Trucks



| Intersection: | Vansco Rd & Dymon Self-Storage (north driveway) |
|---------------|---|
| Site Code: | 2204600032 |
| Count Date: | Feb 12, 2022 |
| Period: | 11:00 - 14:00 |
| | |

Peak Hour Data (13:00 - 14:00)

| | North Approach Vansco Rd | | | | | | | 2 | South A Vans | Approad Sco Rd | :h | | East Approach Dymon Self-Storage (north driveway) | | | | | | West Approach Commerical Entrance | | | | | Total Vehicl | |
|----------------|-----------------------------|---|---|---|------|-------|---|---|-----------------|-------------------|------|-------|--|---|------|---|------|-------|--------------------------------------|---|---|---|------|-----------------|------|
| Start Time | • | 1 | | J | Peds | Total | - | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | • | 1 | • | J | Peds | Total | es |
| 13:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 13:15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 13:30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 13:45 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Grand Total | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 3 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| Approach % | 0 | 0 | 0 | 0 | | - | 0 | 0 | 0 | 0 | | - | 72.7 | 0 | 27.3 | 0 | | - | 0 | 0 | 0 | 0 | | - | |
| Totals % | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 72.7 | 0 | 27.3 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | |
| PHF | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0.67 | 0 | 0.75 | 0 | | 0.69 | 0 | 0 | 0 | 0 | | 0 | 0.69 |
| Cars | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 8 | 0 | 3 | 0 | | 11 | 0 | 0 | 0 | 0 | | 0 | 11 |
| % Cars | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 100 | 0 | 100 | 0 | | 100 | 0 | 0 | 0 | 0 | | 0 | 100 |
| Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| % Trucks | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | | 0 | 0 |
| Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | 0 |
| % Peds | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | | | | | 0 | - | |

Location: 1460 The Queensway

Site ID:

Date:

Thursday, October 20, 2022

| | | | Vansco A | Access #1 | Vansco A | Access #2 | Vansco A | Access #3 | Vansco A | Access #4 | Wickman Access | | | |
|-------|-------|-------|--------------|-----------|--------------|-----------|--------------|-----------|--------------|-----------|----------------|----------|--|--|
| | TIME | | All vehicles | combined | All vehicles | combined | | |
| | | | In | Out | In | Out | In | Out | In | Out | In | Out | | |
| 08:30 | to | 08:45 | 6 | 1 | 1 | 0 | 2 | 0 | 0 | 1 | 2 | 0 | | |
| 08:45 | to | 09:00 | 6 | 1 | 8 | 1 | 4 | 1 | 1 | 1 | 0 | 0 | | |
| 09:00 | to | 09:15 | 7 | 1 | 5 | 0 | 4 | 0 | 2 | 2 | 2 | 1 | | |
| 09:15 | to | 09:30 | 3 | 1 | 5 | 0 | 1 | 0 | 1 | 1 | 1 | 0 | | |
| 09:30 | to | 09:45 | 5 | 1 | 2 | 1 | 0 | 1 | 0 | 2 | 1 | 0 | | |
| 09:45 | to | 10:00 | 1 | 0 | 5 | 1 | 1 | 1 | 1 | 5 | 2 | 0 | | |
| 10:00 | to | 10:15 | 3 | 2 | 4 | 1 | 4 | 0 | 4 | 1 | 0 | 0 | | |
| 10:15 | to | 10:30 | 5 | 1 | 5 | 0 | 2 | 5 | 0 | 1 | 0 | 0 | | |
| 10:30 | to | 10:45 | 2 | 3 | 3 | 1 | 2 | 0 | 1 | 2 | 1 | 0 | | |
| 10:45 | to | 11:00 | 3 | 2 | 3 | 0 | 3 | 0 | 5 | 6 | 1 | 0 | | |
| 11:00 | to | 11:15 | 4 | 2 | 4 | 0 | 1 | 1 | 0 | 2 | 2 | 0 | | |
| 11:15 | to | 11:30 | 3 | 2 | 4 | 1 | 4 | 0 | 1 | 2 | 1 | 1 | | |
| | TOTAL | | | | | | | | | | | | | |
| 15:00 | to | 15:15 | 3 | 0 | 1 | 0 | 0 | 0 | 3 | 4 | 1 | 0 | | |
| 15:15 | to | 15:30 | 4 | 4 | 2 | 2 | 2 | 0 | 1 | 2 | 1 | 3 | | |
| 15:30 | to | 15:45 | 5 | 3 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | | |
| 15:45 | to | 16:00 | 2 | 3 | 3 | 0 | 0 | 1 | 0 | 1 | 1 | 0 | | |
| 16:00 | to | 16:15 | 2 | 2 | 1 | 2 | 1 | 0 | 0 | 1 | 1 | 1 | | |
| 16:15 | to | 16:30 | 3 | 1 | 3 | 2 | 1 | 1 | 1 | 1 | 0 | 3 | | |
| 16:30 | to | 16:45 | 3 | 3 | 1 | 3 | 3 | 1 | 0 | 3 | 0 | 2 | | |
| 16:45 | to | 17:00 | 3 | 3 | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 1 | | |
| TOTAL | | | | | | | | | | | | | | |



TTS Trip Distribution Data



| | | | | | | | | | Route Choice | | | | |
|-----------|------|----|------|----|----------------------|-------------------------|------|-------------------------|--------------|-------------------------|------|-------------------------|-----|
| 2006 Zone | | | From | То | Cardinal Direction % | Route (direction) trips | % | Route (direction) trips | % | Route (direction) trips | % | Route (direction) trips | |
| | 3614 | 1 | 47 | 13 | East | 50% Ninth Line(NB) | 23.5 | 50% Dundas(WB) | 23.5 | 50% Ninth Line(SB) | 6.5 | 50% Dundas(EB) | 6.5 |
| | 3633 | 2 | 81 | | East | 40% Ninth Line(NB) | 32.4 | 60% Dundas(WB) | 48.6 | | | | |
| | 3634 | 3 | 36 | 16 | Internal | 50% Ninth Line(SB) | 18 | 50% Dundas(WB) | 18 | 50% Ninth Line(NB) | 8 | 50% Dundas(EB) | 8 |
| | 3635 | 4 | 162 | | North | 50% Ninth Line(SB) | 81 | 50% Dundas(WB) | 81 | | | | |
| | 3644 | 5 | 69 | | East | 50% Ninth Line(NB) | 34.5 | 50% Dundas(WB) | 34.5 | | | | |
| | 3645 | 6 | 61 | | East | 50% Ninth Line(NB) | 30.5 | 50% Dundas(WB) | 30.5 | | | | |
| | 3650 | 7 | 117 | 11 | East | | | 100% Dundas(WB) | 117 | | | 100% Dundas(EB) | 11 |
| | 3651 | 8 | 85 | | East | 50% Ninth Line(NB) | 42.5 | 50% Dundas(WB) | 42.5 | | | | |
| | 3662 | 9 | 194 | 52 | Northeast | | | 100% Dundas(WB) | 194 | | | 100% Dundas(EB) | 52 |
| | 3663 | 10 | 23 | | North | | | 100% Dundas(WB) | 23 | | | | |
| | 3676 | 11 | 155 | | North | 50% Ninth Line(SB) | 77.5 | 50% Dundas(WB) | 77.5 | | | | |
| | 3812 | 12 | 171 | 4 | North | 50% Ninth Line(SB) | 85.5 | 50% Dundas(WB) | 85.5 | 50% Ninth Line(NB) | 2 | 50% Dundas(EB) | 2 |
| | 3813 | 13 | 101 | | North | 50% Ninth Line(SB) | 50.5 | 50% Dundas(WB) | 50.5 | | | | |
| | 3840 | 14 | 37 | | North | 50% Ninth Line(SB) | 18.5 | 50% Dundas(WB) | 18.5 | | | | |
| | 3868 | 15 | 41 | | North | 20% Ninth Line(SB) | 8.2 | 80% Dundas(WB) | 32.8 | | | | |
| | 3870 | 16 | 32 | 14 | East | 50% Ninth Line(NB) | 16 | 50% Dundas(WB) | 16 | 50% Ninth Line(SB) | 7 | 50% Dundas(EB) | 7 |
| | 4020 | 17 | 15 | | East | 80% Ninth Line(NB) | 12 | 20% Dundas(WB) | 3 | | | | |
| | 4023 | 18 | 48 | 38 | East | 80% Ninth Line(NB) | 38.4 | 20% Dundas(WB) | 9.6 | 80% Ninth Line(SB) | 30.4 | 20% Dundas(EB) | 7.6 |
| | 4024 | 19 | 16 | 36 | East | 50% Ninth Line(NB) | 8 | 50% Dundas(WB) | 8 | 50% Ninth Line(SB) | 18 | 50% Dundas(EB) | 18 |
| | 4025 | 20 | 71 | 6 | South | 90% Ninth Line(NB) | 63.9 | 10% Dundas(EB) | 7.1 | 90% Ninth Line(SB) | 5.4 | 10% Dundas(WB) | 0.6 |
| | 4026 | 21 | 51 | | South | 50% Ninth Line(NB) | 25.5 | 50% Dundas(EB) | 25.5 | | | | |
| | 4028 | 22 | 81 | | South | 5% Ninth Line(NB) | 4.05 | 95% Dundas(EB) | 76.95 | | | | |
| | 4029 | 23 | 95 | | South | 30% Ninth Line(NB) | 28.5 | 70% Dundas(EB) | 66.5 | | | | |
| | 4030 | 24 | 18 | 8 | South | 30% Ninth Line(NB) | 5.4 | 70% Dundas(EB) | 12.6 | 30% Ninth Line(SB) | 2.4 | 70% Dundas(WB) | 5.6 |
| | 4031 | 25 | 23 | | South | 50% Ninth Line(NB) | 11.5 | 50% Dundas(EB) | 11.5 | | | | |
| | 4032 | 26 | 30 | | South | 30% Ninth Line(NB) | 9 | 70% Dundas(EB) | 21 | | | | |
| | 4033 | 27 | 188 | | South | 10% Ninth Line(NB) | 18.8 | 90% Dundas(EB) | 169.2 | | | | |
| | 4034 | 28 | 88 | 56 | South | | | 100% Dundas(EB) | 88 | | | 100% Dundas(WB) | 56 |
| | 4035 | 29 | 96 | | South | | | 100% Dundas(EB) | 96 | | | | |
| | 4036 | 30 | 18 | 15 | South | | | 100% Dundas(EB) | 18 | | | 100% Dundas(WB) | 15 |
| | 4037 | 31 | 59 | | South | | | 100% Dundas(EB) | 59 | | | | |
| | 4038 | 32 | 29 | 18 | South | | | 100% Dundas(EB) | 29 | | | 100% DundasWB) | 18 |
| | 4039 | 33 | 40 | | South | | | 100% Dundas(EB) | 40 | | | | |
| | 4040 | 34 | 52 | | South | | | 100% Dundas(EB) | 52 | | | | |
| | 4041 | 35 | 129 | 21 | South | | | 100% Dundas(EB) | 129 | | | 100% Dundas(WB) | 21 |
| | 4042 | 36 | 77 | 13 | South | | | 100% Dundas(EB) | 77 | | | 100% Dundas(WB) | 13 |
| | 4045 | 37 | 66 | | South | | | 100% Dundas(EB) | 66 | | | | |
| | 4183 | 38 | 173 | | West | | | 100% Dundas(EB) | 173 | | | | |
| | 4186 | 39 | 232 | | West | | | 100% Dundas(EB) | 232 | | | | |
| | 4189 | 40 | 107 | | West | | | 100% Dundas(EB) | 107 | | | | |

| Total | 3,214 | | 321 | | | | | |
|--------------|-------|-----|-----|-----|-------|------|------|------|
| | | | | | | | | Use |
| North | 805 | 25% | 38 | 12% | North | 843 | 24% | 25% |
| South | 1211 | 38% | 137 | 43% | South | 1348 | 38% | 35% |
| East | 686 | 21% | 146 | 45% | East | 832 | 24% | 25% |
| West | 512 | 16% | 0 | 0% | West | 512 | 14% | 15% |
| Internal | 36 | | 16 | | Total | 3535 | 100% | 100% |
| Outside GTHA | 0 | | 0 | | | | | |
| Total | 3214 | | 321 | | | | | |

| Route Choice | INBOUND | | OUTBOUND | |
|----------------|---------|-----|----------|-----|
| Ninth Line(NB) | 404 | 13% | 10 | 3% |
| Ninth Line(SB) | 339 | 11% | 70 | 23% |
| Dundas(EB) | 1556 | 48% | 112 | 37% |
| Dundas(WB) | 914 | 28% | 111 | 37% |
| | 3214 | | 303 | |

| | | | | | | | | | Route Choice | | | | |
|-----------|------|----|-----|-----|----------------------|-------------------------|-------|-------------------------|--------------|-------------------------|------|-------------------------|--------|
| 2006 Zone | | Fr | om | То | Cardinal Direction % | Route (direction) trips | % | Route (direction) trips | % | Route (direction) trips | % | Route (direction) trips | |
| | 3614 | 1 | 56 | 56 | East | 50% Ninth Line(NB) | 28 | 50% Dundas(WB) | 28 | 50% Ninth Line(SB) | 28 | 50% Dundas(EB) | 28 |
| | 3633 | 2 | | 30 | East | | | | | 40% Ninth Line(SB) | 12 | 60% Dundas(EB) | 18 |
| | 3634 | 3 | 140 | 115 | Internal | 50% Ninth Line(SB) | 70 | 50% Dundas(WB) | 70 | 50% Ninth Line(NB) | 57.5 | 50% Dundas(EB) | 57.5 |
| | 3635 | 4 | 91 | 59 | North | 50% Ninth Line(SB) | 45.5 | 50% Dundas(WB) | 45.5 | 50% Ninth Line(NB) | 29.5 | 50% Dundas(EB) | 29.5 |
| | 3644 | 5 | 29 | 49 | East | 50% Ninth Line(NB) | 14.5 | 50% Dundas(WB) | 14.5 | 50% Ninth Line(SB) | 24.5 | 50% Dundas(EB) | 24.5 |
| | 3645 | 6 | | 54 | East | | | | | 50% Ninth Line(SB) | 27 | 50% Dundas(EB) | 27 |
| | 3650 | 7 | 238 | 314 | East | | 0 | 100% Dundas(WB) | 238 | | 0 | 100% Dundas(EB) | 314 |
| | 3651 | 8 | 17 | 78 | East | 50% Ninth Line(NB) | 8.5 | 50% Dundas(WB) | 8.5 | 50% Ninth Line(SB) | 39 | 50% Dundas(EB) | 39 |
| | 3662 | 9 | 133 | 224 | Northeast | | 0 | 100% Dundas(WB) | 133 | | 0 | 100% Dundas(EB) | 224 |
| | 3663 | 10 | 46 | 46 | North | | 0 | 100% Dundas(WB) | 46 | | 0 | 100% Dundas(EB) | 46 |
| | 3676 | 11 | 23 | 204 | North | 50% Ninth Line(SB) | 11.5 | 50% Dundas(WB) | 11.5 | 50% Ninth Line(NB) | 102 | 50% Dundas(EB) | 102 |
| | 3677 | 12 | 11 | 77 | North | 50% Ninth Line(SB) | 5.5 | 50% Dundas(WB) | 5.5 | 50% Ninth Line(NB) | 38.5 | 50% Dundas(EB) | 38.5 |
| | 3811 | 13 | 23 | 82 | North | 50% Ninth Line(SB) | 11.5 | 50% Dundas(WB) | 11.5 | 50% Ninth Line(NB) | 41 | 50% Dundas(EB) | 41 |
| | 3812 | 14 | 96 | 230 | North | 50% Ninth Line(SB) | 48 | 50% Dundas(WB) | 48 | 50% Ninth Line(NB) | 115 | 50% Dundas(EB) | 115 |
| | 3813 | 15 | 93 | 51 | North | 50% Ninth Line(SB) | 46.5 | 50% Dundas(WB) | 46.5 | 50% Ninth Line(NB) | 25.5 | 50% Dundas(EB) | 25.5 |
| | 3840 | 16 | | 37 | North | | | | | 50% Ninth Line(NB) | 18.5 | 50% Dundas(EB) | 18.5 |
| | 3868 | 17 | 21 | 18 | North | 50% Ninth Line(SB) | 10.5 | 50% Dundas(WB) | 10.5 | 50% Ninth Line(NB) | 9 | 50% Dundas(EB) | 9 |
| | 3869 | 18 | 12 | | East | 50% Ninth Line(NB) | 6 | 50% Dundas(WB) | 6 | | | | |
| | 3870 | 19 | 24 | 106 | East | 20% Ninth Line(NB) | 4.8 | 80% Dundas(WB) | 19.2 | 20% Ninth Line(SB) | 21.2 | 80% Dundas(EB) | 84.8 |
| | 4020 | 20 | 58 | 28 | East | 60% Ninth Line(NB) | 34.8 | 40% Dundas(WB) | 23.2 | 60% Ninth Line(SB) | 16.8 | 40% Dundas(EB) | 11.2 |
| | 4023 | 21 | 30 | 37 | East | 80% Ninth Line(NB) | 24 | 20% Dundas(WB) | 6 | 80% Ninth Line(SB) | 29.6 | 20% Dundas(EB) | 7.4 |
| | 4024 | 22 | 79 | 104 | East | 50% Ninth Line(NB) | 39.5 | 50% Dundas(WB) | 39.5 | 50% Ninth Line(SB) | 52 | 50% Dundas(EB) | 52 |
| | 4025 | 23 | 202 | 210 | South | 90% Ninth Line(NB) | 181.8 | 10% Dundas(EB) | 20.2 | 90% Ninth Line(SB) | 189 | 10% Dundas(WB) | 21 |
| | 4026 | 24 | 9 | 70 | South | 50% Ninth Line(NB) | 4.5 | 50% Dundas(EB) | 4.5 | 50% Ninth Line(SB) | 35 | 50% Dundas(WB) | 35 |
| | 4028 | 25 | 8 | 109 | South | 5% Ninth Line(NB) | 0.4 | 95% Dundas(EB) | 7.6 | 5% Ninth Line(SB) | 5.45 | 95% Dundas(WB) | 103.55 |
| | 4029 | 26 | | 33 | South | | | | | 30% Ninth Line(SB) | 9.9 | 70% Dundas(WB) | 23.1 |
| | 4030 | 27 | | 152 | South | | | | | 50% Ninth Line(SB) | 76 | 50% Dundas(WB) | 76 |
| | 4031 | 28 | 139 | | South | 50% Ninth Line(NB) | 69.5 | 50% Dundas(EB) | 69.5 | | | | |
| | 4032 | 29 | 14 | 46 | South | 20% Ninth Line(NB) | 2.8 | 80% Dundas(EB) | 11.2 | 20% Ninth Line(SB) | 9.2 | 80% Dundas(WB) | 36.8 |
| | 4033 | 30 | 82 | 167 | South | 40% Ninth Line(NB) | 32.8 | 60% Dundas(EB) | 49.2 | 40% Ninth Line(SB) | 66.8 | 60% Dundas(WB) | 100.2 |
| | 4034 | 31 | 19 | 133 | South | 0% Ninth Line(NB) | 0 | 100% Dundas(EB) | 19 | 0% Ninth Line(SB) | 0 | 100% Dundas(WB) | 133 |
| | 4035 | 32 | 12 | 85 | South | 0% Ninth Line(NB) | 0 | 100% Dundas(EB) | 12 | 0% Ninth Line(SB) | 0 | 100% Dundas(WB) | 85 |
| | 4036 | 33 | 62 | 60 | South | Ninth Line(NB) | 0 | 100% Dundas(EB) | 62 | Ninth Line(SB) | 0 | 100% Dundas(WB) | 60 |
| | 4038 | 34 | 20 | 29 | South | Ninth Line(NB) | 0 | 100% Dundas(EB) | 20 | Ninth Line(SB) | 0 | 100% Dundas(WB) | 29 |
| | 4039 | 35 | 45 | 38 | South | Ninth Line(NB) | 0 | 100% Dundas(EB) | 45 | Ninth Line(SB) | 0 | 100% Dundas(WB) | 38 |
| | 4040 | 36 | 80 | 55 | South | Ninth Line(NB) | 0 | 100% Dundas(EB) | 80 | Ninth Line(SB) | 0 | 100% Dundas(WB) | 55 |
| | 4041 | 37 | 105 | 102 | South | Ninth Line(NB) | 0 | 100% Dundas(EB) | 105 | Ninth Line(SB) | 0 | 100% Dundas(WB) | 102 |
| | 4042 | 38 | | 17 | South | | | | | Ninth Line(SB) | 0 | 100% Dundas(WB) | 17 |
| | 4045 | 39 | 85 | 66 | South | Ninth Line(NB) | 0 | 100% Dundas(EB) | 85 | Ninth Line(SB) | 0 | 100% Dundas(WB) | 66 |
| | 4182 | 40 | 15 | | West | | 0 | 100% Dundas(EB) | 15 | | | | |
| | 4183 | 41 | 9 | 113 | West | | 0 | 100% Dundas(EB) | 9 | | 0 | 100% Dundas(WB) | 113 |
| | 4186 | 42 | | 215 | West | | | | | | 0 | 100% Dundas(WB) | 215 |
| | 4189 | 43 | | 112 | West | | | | | | 0 | 100% Dundas(WB) | 112 |

| Total | 2,126 | | 3811 | | | | | | |
|------------------------|---------|-----|------|---------|-------------|--------------|-------|------|------|
| | | | | | | | | Use | |
| North | 541 | 25% | 974 | 26% | North | 1514 | 26% | | 25% |
| South | 882 | 41% | 1372 | 36% | South | 2254 | 38% | | 35% |
| East | 680 | 32% | 1026 | 27% | East | 1705 | 29% | | 30% |
| West | 24 | 1% | 440 | 12% | West | 464 | 8% | | 10% |
| Internal | 140 | | 115 | | Total | 5937 | 100% | | 100% |
| Total | 2126 | | 3811 | | | | | | |
| | | | | | Sum of AM a | and PM Peaks | | Use | |
| | | | | | North | 2357 | 25% | | 25% |
| | | | | | South | 3602 | 38% | | 35% |
| | | | | | East | 2537 | 27% | | 30% |
| | | | | | West | 976 | 10% | | 10% |
| | | | | | Total | 9472 | 100% | | 100% |
| | | | | | | | | | |
| Route Choice | INBOUND | | OL | JTBOUND | | | | | |
| Ninth Line(NB) | 452 | 21% | | 437 | 11% | | | | |
| Ninth Line(SB) | 249 | 12% | | 641 | 17% | | | | |
| Dundas(EB) | 614 | 29% | | 1312 | 34% | | | | |
| Dundas(WB) | 811 | 38% | | 1421 | 37% | | | | |
| | 2126 | | | 3811 | | | | | |
| Sum of AM and PM Peaks | | | | | | | | | |
| Route Choice | INBOUND | | OL | JTBOUND | | Comb | bined | | |
| Ninth Line(NB) | 856 | 16% | | 447 | 11% | North | 1,035 | 11% | |
| Ninth Line(SB) | 588 | 11% | | 711 | 17% | South | 1,568 | 17% | |
| Dundas(EB) | 2,171 | 41% | | 1,425 | 35% | East | 3,149 | 33% | |
| Dundas(WB) | 1,725 | 32% | | 1,532 | 37% | West | 3,702 | 39% | |
| | 5,340 | | | 4,114 | | Total | 9,454 | 100% | |
| | | | | | | | | | |



Left Turn Lane Warrant



| Design Speed | Northbound Left | | | | | | Yes | | | | | | | | | |
|--------------|-----------------|-------|--------|-------|-----|-----|-----|----|-------|-----|-----|------|----|----------|------------------|-----------------|
| 70 km/h | E | BL EE | BT EBF | R WBL | WBT | WBR | NBL | NB | T NBR | SBL | SBT | SBR | %L | eft Turn | Volume Advancing | Volume Opposing |
| | AM | 3 | 0 | 4 | 19 | 0 | 1 | 25 | 953 | 85 | 5 | 1418 | 6 | 2.4% | 1063 | 1429 |
| | PM | 11 | 0 | 38 | 47 | 0 | 3 | 26 | 1876 | 40 | 2 | 1094 | 6 | 1.3% | 1942 | 1102 |



| Design Speed | Southbound Left | | | | | | | | | Yes | | | | | | |
|--------------|-----------------|--------|-----|-----|-----|-----|-----|-----|------|-----|-----|------|-----|----------|------------------|-----------------|
| 70 km/h | EE | BL EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR | %Le | eft Turn | Volume Advancing | Volume Opposing |
| | AM | 3 | 0 | 4 | 19 | 0 | 1 | 25 | 953 | 85 | 5 | 1418 | 6 | 0.3% | 1429 | 1063 |
| | PM | 11 | 0 | 38 | 47 | 0 | 3 | 26 | 1876 | 40 | 2 | 1094 | 6 | 0.2% | 1102 | 1942 |



Appendix R

2026 Future Total Synchro Intersection Worksheets



Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٨ | → | 7 | 4 | + | • | 1 | Ť | 1 | 1 | ţ | ~ |
|----------------------------|-------|------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | *** | 1 | 5 | *** | 1 | 7 | 44 | 1 | ۲ | ** | 1 |
| Traffic Volume (vph) | 225 | 2710 | 372 | 181 | 1214 | 154 | 191 | 373 | 177 | 258 | 639 | 169 |
| Future Volume (vph) | 225 | 2710 | 372 | 181 | 1214 | 154 | 191 | 373 | 177 | 258 | 639 | 169 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.111 | | | 0.058 | | | 0.126 | | | 0.409 | | |
| Satd. Flow (perm) | 200 | 5085 | 1491 | 100 | 4715 | 1449 | 203 | 3433 | 1422 | 704 | 3466 | 1478 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd, Flow (RTOR) | | | 202 | | | 153 | | | 134 | | | 166 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 329.1 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 19.7 | | | 11.3 | | | 5.7 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adi, Flow (vph) | 245 | 2946 | 404 | 197 | 1320 | 167 | 208 | 405 | 192 | 280 | 695 | 184 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 245 | 2946 | 404 | 197 | 1320 | 167 | 208 | 405 | 192 | 280 | 695 | 184 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | Ŭ | | 3.3 | Ű | | 3.0 | Ŭ | | 3.0 | Ŭ |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | CI+Ex | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | CI+Ex | CI+Ex | CI+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | 0.0 | 9.4 | | | 9.4 | 0.0 | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | CI+Ex | | | CI+Ex | | | CI+Ex | | | CI+Ex | |
| Detector 2 Channel | | - , | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |

Lanes, Volumes, Timings 1: Ninth Line & Dundas Street East

| | ٦ | - | ¥ | 4 | ← | • | 1 | t | 1 | 4 | ŧ | ~ |
|----------------------------|------------|----------|----------|-------------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 9.0 | 52.9 | 52.9 | 9.0 | 52.9 | 52.9 | 9.0 | 56.0 | 56.0 | 9.0 | 56.0 | 56.0 |
| Total Split (s) | 31.0 | 82.0 | 82.0 | 13.0 | 64.0 | 64.0 | 20.0 | 48.0 | 48.0 | 17.0 | 45.0 | 45.0 |
| Total Split (%) | 19.4% | 51.3% | 51.3% | 8.1% | 40.0% | 40.0% | 12.5% | 30.0% | 30.0% | 10.6% | 28.1% | 28.1% |
| Maximum Green (s) | 27.0 | 75.1 | 75.1 | 9.0 | 57.1 | 57.1 | 16.0 | 41.0 | 41.0 | 13.0 | 38.0 | 38.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.7 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 3.3 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | 15.0 | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | 34.0 | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 00 | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Act Effct Green (s) | 95.0 | 77.0 | 77.0 | 84.7 | 67.3 | 67.3 | 62.1 | 41.1 | 41.1 | 58.1 | 38.1 | 38.1 |
| Actuated g/C Ratio | 0.59 | 0.48 | 0.48 | 0.53 | 0.42 | 0.42 | 0.39 | 0.26 | 0.26 | 0.36 | 0.24 | 0.24 |
| v/c Ratio | 0.72 | 1 20 | 0.49 | 1.05 | 0.67 | 0.24 | 0.88 | 0.46 | 0.41 | 0.80 | 0.84 | 0.38 |
| Control Delay | 38.6 | 133.0 | 15.3 | 124 7 | 40.5 | 6.9 | 72 7 | 51.7 | 18.1 | 56.5 | 68.3 | 11.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 38.6 | 133.0 | 15.3 | 124 7 | 40.5 | 6.9 | 72.7 | 51.7 | 18.1 | 56.5 | 68.3 | 11.2 |
| | D | F | B | F | D | A | F | D | B | F | F | B |
| Approach Delay | 2 | 113.3 | 2 | • | 47 0 | 7. | _ | 491 | 2 | _ | 56 4 | 5 |
| Approach LOS | | F | | | D | | | D | | | F | |
| Queue Length 50th (m) | 40.5 | ~382.8 | 38.3 | ~56.0 | 116 6 | 25 | 42.6 | 52 1 | 13 1 | 59.2 | 101 4 | 4 1 |
| Queue Length 95th (m) | 67.7 | #402.2 | 65.1 | #106.7 | 140.7 | 17.4 | #85.5 | 67.4 | 34.3 | #88.5 | 123.5 | 23.2 |
| Internal Link Dist (m) | 0111 | 269.2 | 00.1 | 110011 | 305.1 | | 100.0 | 164.2 | 01.0 | 100.0 | 71.5 | 20.2 |
| Turn Bay Length (m) | 220.0 | 200.2 | 80.0 | 230.0 | 000.1 | 80.0 | 130.0 | 101.2 | 130.0 | 130.0 | 11.0 | 70 0 |
| Base Capacity (vph) | 403 | 2447 | 822 | 187 | 1984 | 698 | 236 | 922 | 480 | 349 | 866 | 494 |
| Starvation Can Reductn | 0 | 0 | 0 | 0 | 0 | 000 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Can Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.61 | 1.20 | 0.49 | 1.05 | 0.67 | 0.24 | 0.88 | 0.44 | 0.40 | 0.80 | 0.80 | 0.37 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 160 | | | | | | | | | | | | |
| Actuated Cycle Length: 160 |) | | | | | | | | | | | |
| Offset: 0 (0%), Referenced | to phase 2 | :EBTL an | d 6:WBTI | L, Start of | Green | | | | | | | |
| Natural Cycle: 160 | | | | | | | | | | | | |
| Control Type: Actuated-Coo | ordinated | | | | | | | | | | | |

Maximum v/c Ratio: 1.20 Intersection Signal Delay: 81.7

Intersection LOS: F

Intersection Capacity Utilization 105.6%

ICU Level of Service G

Analysis Period (min) 15

- Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Ninth Line & Dundas Street East

| 🖌 Ø1 🔶 Ø2 (R) | • | Ø3 | ¶ø₄ |
|---------------|------------|-------------|------|
| 13 s 82 s | | 17 s | 48 s |
| ▶ Ø5 | ♥ ♥ Ø6 (R) | 1 Ø7 | Ø8 |
| 31 s | 64 s | 20 s | 45 s |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | 4 | + | * | 1 | t | 1 | 4 | Ļ | ~ |
|-------------------------------------|-------|-------|--------|-------|-----------|------------|----------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | ٦ | *** | 1 | 5 | ^ | 1 | ٦ | ^ | 1 |
| Traffic Volume (vph) | 225 | 2710 | 372 | 181 | 1214 | 154 | 191 | 373 | 177 | 258 | 639 | 169 |
| Future Volume (vph) | 225 | 2710 | 372 | 181 | 1214 | 154 | 191 | 373 | 177 | 258 | 639 | 169 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.11 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.13 | 1.00 | 1.00 | 0.41 | 1.00 | 1.00 |
| Satd. Flow (perm) | 200 | 5085 | 1491 | 101 | 4715 | 1449 | 203 | 3433 | 1422 | 704 | 3466 | 1478 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 245 | 2946 | 404 | 197 | 1320 | 167 | 208 | 405 | 192 | 280 | 695 | 184 |
| RTOR Reduction (vph) | 0 | 0 | 105 | 0 | 0 | 89 | 0 | 0 | 100 | 0 | 0 | 126 |
| Lane Group Flow (vph) | 245 | 2946 | 299 | 197 | 1320 | 78 | 208 | 405 | 92 | 280 | 695 | 58 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 90.0 | 75.1 | 75.1 | 76.3 | 65.4 | 65.4 | 55.1 | 39.1 | 39.1 | 49.1 | 36.1 | 36.1 |
| Effective Green, g (s) | 93.0 | 77.0 | 77.0 | 82.3 | 67.3 | 67.3 | 59.1 | 41.1 | 41.1 | 55.1 | 38.1 | 38.1 |
| Actuated g/C Ratio | 0.58 | 0.48 | 0.48 | 0.51 | 0.42 | 0.42 | 0.37 | 0.26 | 0.26 | 0.34 | 0.24 | 0.24 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 339 | 2447 | 717 | 186 | 1983 | 609 | 232 | 881 | 365 | 335 | 825 | 351 |
| v/s Ratio Prot | 0.11 | c0.58 | | c0.09 | 0.28 | | c0.11 | 0.12 | | 0.08 | 0.20 | |
| v/s Ratio Perm | 0.31 | | 0.20 | 0.45 | | 0.05 | 0.22 | | 0.06 | c0.20 | | 0.04 |
| v/c Ratio | 0.72 | 1.20 | 0.42 | 1.06 | 0.67 | 0.13 | 0.90 | 0.46 | 0.25 | 0.84 | 0.84 | 0.16 |
| Uniform Delay, d1 | 30.7 | 41.5 | 26.9 | 52.9 | 37.3 | 28.4 | 41.0 | 50.1 | 47.3 | 44.4 | 58.1 | 48.3 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 7.7 | 95.9 | 1.8 | 82.5 | 1.8 | 0.4 | 33.1 | 0.5 | 0.4 | 16.7 | 8.0 | 0.3 |
| Delay (s) | 38.4 | 137.4 | 28.7 | 135.4 | 39.1 | 28.8 | 74.2 | 50.5 | 47.7 | 61.1 | 66.1 | 48.6 |
| Level of Service | D | F | С | F | D | С | E | D | D | Е | E | D |
| Approach Delay (s) | | 118.5 | | | 49.3 | | | 56.0 | | | 62.1 | |
| Approach LOS | | F | | | D | | | Е | | | Е | |
| Intersection Summary | | | • • • | | | | . | | | | | |
| HCM 2000 Control Delay | | | 86.4 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capacity ratio 1 | | | 1.04 | | | | | | | | | |
| Actuated Cycle Length (s) 160. | | | 160.0 | S | um of los | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utilizat | ion | | 105.6% | IC | C Level | of Service | ; | | G | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group
HCM 6th Signalized Intersection Summary 1: Ninth Line & Dundas Street East

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|------------------------------|------|-------|------|-------|------|-------|-------------|--------------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 5 | *** | 1 | ٢ | ** | 1 | 7 | ^ | 1 |
| Traffic Volume (veh/h) | 225 | 2710 | 372 | 181 | 1214 | 154 | 191 | 373 | 177 | 258 | 639 | 169 |
| Future Volume (veh/h) | 225 | 2710 | 372 | 181 | 1214 | 154 | 191 | 373 | 177 | 258 | 639 | 169 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1856 | 1811 | 1752 | 1811 | 1682 | 1841 | 1739 | 1781 | 1856 | 1796 |
| Adj Flow Rate, veh/h | 245 | 2946 | 404 | 197 | 1320 | 167 | 208 | 405 | 192 | 280 | 695 | 184 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 3 | 6 | 10 | 6 | 10 | 4 | 6 | 3 | 3 | 2 |
| Cap, veh/h | 325 | 2544 | 771 | 174 | 2251 | 711 | 264 | 881 | 371 | 340 | 822 | 355 |
| Arrive On Green | 0.10 | 0.50 | 0.50 | 0.08 | 0.47 | 0.47 | 0.12 | 0.25 | 0.25 | 0.10 | 0.23 | 0.23 |
| Sat Flow, veh/h | 1781 | 5106 | 1547 | 1725 | 4782 | 1510 | 1602 | 3497 | 1473 | 1696 | 3526 | 1522 |
| Grp Volume(v), veh/h | 245 | 2946 | 404 | 197 | 1320 | 167 | 208 | 405 | 192 | 280 | 695 | 184 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1702 | 1547 | 1725 | 1594 | 1510 | 1602 | 1749 | 1473 | 1696 | 1763 | 1522 |
| Q Serve(g_s), s | 10.4 | 79.7 | 28.4 | 12.0 | 32.3 | 10.5 | 15.0 | 15.7 | 17.9 | 16.0 | 30.1 | 16.9 |
| Cycle Q Clear(g_c), s | 10.4 | 79.7 | 28.4 | 12.0 | 32.3 | 10.5 | 15.0 | 15.7 | 17.9 | 16.0 | 30.1 | 16.9 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 325 | 2544 | 771 | 174 | 2251 | 711 | 264 | 881 | 371 | 340 | 822 | 355 |
| V/C Ratio(X) | 0.75 | 1.16 | 0.52 | 1.13 | 0.59 | 0.23 | 0.79 | 0.46 | 0.52 | 0.82 | 0.85 | 0.52 |
| Avail Cap(c_a), veh/h | 477 | 2544 | 771 | 174 | 2251 | 711 | 264 | 940 | 396 | 340 | 881 | 380 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 25.8 | 40.1 | 27.3 | 54.0 | 31.0 | 25.2 | 40.9 | 50.6 | 51.5 | 46.4 | 58.6 | 53.5 |
| Incr Delay (d2), s/veh | 4.6 | 76.0 | 2.5 | 107.2 | 1.1 | 0.8 | 15.0 | 0.5 | 1.3 | 15.4 | 1.5 | 1.4 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/in | 5.4 | 52.9 | 11.9 | 12.6 | 13.6 | 4.3 | 7.4 | 7.3 | 1.1 | 5.3 | 14.9 | 6.9 |
| Unsig. Movement Delay, s/veh | 00.4 | 440.4 | 00.0 | 404.0 | 20.4 | 00.0 | 55 0 | F A A | 50.0 | C4 7 | 00.4 | 54.0 |
| LnGrp Delay(d),s/ven | 30.4 | 116.1 | 29.8 | 161.2 | 32.1 | 26.0 | 55.9 | 51.1 | 52.8 | 61.7 | 66.1 | 54.9 |
| LnGrp LOS | C | | C | F | 0 | C | E | D | D | E | E | D |
| Approach Vol, veh/h | | 3595 | | | 1684 | | | 805 | | | 1159 | |
| Approach Delay, s/veh | | 100.6 | | | 46.6 | | | 52.8 | | | 63.3 | |
| Approach LOS | | F | | | D | | | D | | | E | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 13.0 | 84.7 | 17.0 | 45.3 | 17.4 | 80.3 | 20.0 | 42.3 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 9.0 | * 75 | 13.0 | 41.0 | 27.0 | * 57 | 16.0 | 38.0 | | | | |
| Max Q Clear Time (g_c+l1), s | 14.0 | 82.7 | 18.0 | 19.9 | 12.4 | 34.3 | 17.0 | 32.1 | | | | |
| Green Ext Time (p_c), s | 0.0 | 0.0 | 0.0 | 4.5 | 1.0 | 18.5 | 0.0 | 3.2 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 76.7 | | | | | | | | | |
| HCM 6th LOS | | | Е | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Lanes, Volumes, Timings 2: Ninth Line & Glen Oaks Access/Site Access

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|---------------------------------|----------|----------|-------|------|------------|------------|------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | | đ þ | | 5 | f) | |
| Traffic Volume (vph) | 3 | 0 | 4 | 17 | 0 | 2 | 22 | 682 | 83 | 10 | 1064 | 5 |
| Future Volume (vph) | 3 | 0 | 4 | 17 | 0 | 2 | 22 | 682 | 83 | 10 | 1064 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.5 | 3.2 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Storage Length (m) | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 15.0 | | 0.0 |
| Storage Lanes | 0 | | 0 | 0 | | 0 | 0 | | 0 | 1 | | 0 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | | | | | | | | | | | | |
| Frt | | 0.923 | | | 0.986 | | | 0.984 | | | 0.999 | |
| Flt Protected | | 0.979 | | | 0.957 | | | 0.999 | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1665 | 0 | 0 | 1738 | 0 | 0 | 3383 | 0 | 1750 | 1822 | 0 |
| Flt Permitted | | 0.979 | | | 0.957 | | | 0.999 | | 0.950 | | |
| Satd. Flow (perm) | 0 | 1665 | 0 | 0 | 1738 | 0 | 0 | 3383 | 0 | 1750 | 1822 | 0 |
| Link Speed (k/h) | | 60 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 47.4 | | | 48.5 | | | 51.2 | | | 157.3 | |
| Travel Time (s) | | 2.8 | | | 2.9 | | | 3.1 | | | 9.4 | |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% | 2% | 3% | 2% |
| Adj. Flow (vph) | 3 | 0 | 4 | 18 | 0 | 2 | 24 | 741 | 90 | 11 | 1157 | 5 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 7 | 0 | 0 | 20 | 0 | 0 | 855 | 0 | 11 | 1162 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.5 | | | 3.5 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | Yes | | | Yes | |
| Headway Factor | 1.06 | 1.01 | 1.06 | 1.01 | 1.01 | 1.01 | 1.04 | 1.01 | 1.01 | 1.01 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: C | Other | | | | | | | | | | | |
| Control Type: Unsignalized | | | | | | | | | | | | |
| Intersection Capacity Utilizati | on 66.3% | | | IC | CU Level (| of Service | С | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |

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|-------------------------------|-------|------|-------|------|-----------|------------|------|-------|------|------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | đ þ | | 7 | ĥ | |
| Traffic Volume (veh/h) | 3 | 0 | 4 | 17 | 0 | 2 | 22 | 682 | 83 | 10 | 1064 | 5 |
| Future Volume (Veh/h) | 3 | 0 | 4 | 17 | 0 | 2 | 22 | 682 | 83 | 10 | 1064 | 5 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 3 | 0 | 4 | 18 | 0 | 2 | 24 | 741 | 90 | 11 | 1157 | 5 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (m) | | | | | | | | | | | | |
| Walking Speed (m/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | TWLTL | | | TWLTL | |
| Median storage veh) | | | | | | | | 2 | | | 2 | |
| Upstream signal (m) | | | | | | | | 147 | | | | |
| pX, platoon unblocked | 0.90 | 0.90 | | 0.90 | 0.90 | 0.90 | | | | 0.90 | | |
| vC, conflicting volume | 1602 | 2060 | 1160 | 2017 | 2018 | 416 | 1162 | | | 831 | | |
| vC1, stage 1 conf vol | 1182 | 1182 | | 834 | 834 | | | | | | | |
| vC2, stage 2 conf vol | 420 | 879 | | 1183 | 1184 | | | | | | | |
| vCu, unblocked vol | 1455 | 1961 | 1160 | 1913 | 1915 | 143 | 1162 | | | 602 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | 6.5 | 5.5 | | 6.5 | 5.5 | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 98 | 100 | 98 | 88 | 100 | 100 | 96 | | | 99 | | |
| cM capacity (veh/h) | 191 | 215 | 189 | 154 | 205 | 795 | 597 | | | 878 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total | 7 | 20 | 394 | 460 | 11 | 1162 | | | | | | |
| Volume Left | 3 | 18 | 24 | 0 | 11 | 0 | | | | | | |
| Volume Right | 4 | 2 | 0 | 90 | 0 | 5 | | | | | | |
| cSH | 190 | 167 | 597 | 1700 | 878 | 1700 | | | | | | |
| Volume to Capacity | 0.04 | 0.12 | 0.04 | 0.27 | 0.01 | 0.68 | | | | | | |
| Queue Length 95th (m) | 0.8 | 2.8 | 0.9 | 0.0 | 0.3 | 0.0 | | | | | | |
| Control Delay (s) | 24.7 | 29.4 | 1.2 | 0.0 | 9.1 | 0.0 | | | | | | |
| Lane LOS | С | D | А | | А | | | | | | | |
| Approach Delay (s) | 24.7 | 29.4 | 0.6 | | 0.1 | | | | | | | |
| Approach LOS | С | D | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 0.7 | | | | | | | | | |
| Intersection Capacity Utiliza | ation | | 66.3% | IC | U Level o | of Service | | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Lanes, Volumes, Timings 1: Ninth Line & Dundas Street East

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|----------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 7 | *** | 1 | 5 | ** | 1 | 5 | * * | 1 |
| Traffic Volume (vph) | 182 | 1810 | 217 | 118 | 2827 | 250 | 378 | 903 | 558 | 203 | 389 | 194 |
| Future Volume (vph) | 182 | 1810 | 217 | 118 | 2827 | 250 | 378 | 903 | 558 | 203 | 389 | 194 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Ped Bike Factor | | | 0.98 | | | | 1.00 | | | | | 0.99 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5036 | 1477 | 1694 | 5085 | 1506 | 1652 | 3500 | 1478 | 1652 | 3433 | 1478 |
| Flt Permitted | 0.059 | | | 0.059 | | | 0.319 | | | 0.111 | | |
| Satd. Flow (perm) | 106 | 5036 | 1455 | 105 | 5085 | 1506 | 554 | 3500 | 1478 | 193 | 3433 | 1459 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 154 | | | 127 | | | 54 | | | 136 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 415.5 | | | 188.2 | | | 95.5 | |
| Travel Time (s) | | 15.1 | | | 24.9 | | | 11.3 | | | 5.7 | |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 198 | 1967 | 236 | 128 | 3073 | 272 | 411 | 982 | 607 | 221 | 423 | 211 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 198 | 1967 | 236 | 128 | 3073 | 272 | 411 | 982 | 607 | 221 | 423 | 211 |
| Enter Blocked Intersection | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | | | 3.3 | | | 3.0 | | | 3.0 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | Cl+Ex | Cl+Ex | CI+Ex | Cl+Ex | CI+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | Cl+Ex | | | CI+Ex | | | CI+Ex | | | CI+Ex | |

07-17-2023

Lanes, Volumes, Timings 1: Ninth Line & Dundas Street East

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|----------------------------|--------|--------|-------|-------|--------|-------|--------|--------|--------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | | 6 | | 7 | 4 | . 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 1 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 9.0 | 52.9 | 52.9 | 9.0 | 52.9 | 52.9 | 9.0 | 56.0 | 9.0 | 9.0 | 56.0 | 56.0 |
| Total Split (s) | 10.0 | 70.0 | 70.0 | 20.0 | 80.0 | 80.0 | 30.0 | 51.0 | 20.0 | 19.0 | 40.0 | 40.0 |
| Total Split (%) | 6.3% | 43.8% | 43.8% | 12.5% | 50.0% | 50.0% | 18.8% | 31.9% | 12.5% | 11.9% | 25.0% | 25.0% |
| Maximum Green (s) | 6.0 | 63.1 | 63.1 | 16.0 | 73.1 | 73.1 | 26.0 | 44.0 | 16.0 | 15.0 | 33.0 | 33.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.0 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 1.0 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 2.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | | | 0 | 0 |
| Act Effct Green (s) | 79.2 | 66.2 | 66.2 | 89.0 | 75.0 | 75.0 | 69.0 | 46.0 | 67.8 | 57.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.50 | 0.41 | 0.41 | 0.56 | 0.47 | 0.47 | 0.43 | 0.29 | 0.42 | 0.36 | 0.22 | 0.22 |
| v/c Ratio | 1.39 | 0.94 | 0.34 | 0.54 | 1.29 | 0.35 | 0.94 | 0.98 | 0.92 | 0.95 | 0.56 | 0.50 |
| Control Delay | 246.5 | 55.7 | 12.5 | 39.1 | 169.6 | 15.1 | 66.6 | 79.0 | 60.3 | 92.3 | 59.1 | 23.8 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 246.5 | 55.7 | 12.5 | 39.1 | 169.6 | 15.1 | 66.6 | 79.0 | 60.3 | 92.3 | 59.1 | 23.8 |
| LOS | F | E | В | D | F | В | Е | E | E | F | E | С |
| Approach Delay | | 67.2 | | | 152.7 | | | 70.8 | | | 59.0 | |
| Approach LOS | | E | | | F | | | E | | | E | |
| Queue Length 50th (m) | ~63.3 | 204.6 | 15.1 | 20.9 | ~418.1 | 25.4 | 90.5 | 150.8 | 154.0 | 50.6 | 58.7 | 18.5 |
| Queue Length 95th (m) | #111.9 | #235.4 | 34.5 | 41.4 | #436.4 | 45.3 | #134.7 | #191.9 | #224.4 | #99.1 | 75.4 | 43.2 |
| Internal Link Dist (m) | | 269.2 | | | 391.5 | | | 164.2 | | | 71.5 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 142 | 2082 | 691 | 247 | 2383 | 773 | 437 | 1006 | 668 | 232 | 750 | 425 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.39 | 0.94 | 0.34 | 0.52 | 1.29 | 0.35 | 0.94 | 0.98 | 0.91 | 0.95 | 0.56 | 0.50 |
| Intersection Summary | 01 | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 160 | | | | | | | | | | | | |
| Actuated Cycle Length: 160 | J | | | | | | | | | | | |

Offset: 0 (0%), Referenced to phase 2:EBTL and 6:WBTL, Start of Green Natural Cycle: 160

Control Type: Actuated-Coordinated

| Maximum v/c Ratio: 1.39 | |
|---|------------------------|
| Intersection Signal Delay: 101.2 | Intersection LOS: F |
| Intersection Capacity Utilization 115.9% | ICU Level of Service H |
| Analysis Period (min) 15 | |
| ~ Volume exceeds capacity, queue is theoretically infinite. | |
| Queue shown is maximum after two cycles. | |
| # 95th percentile volume exceeds capacity, queue may be lon | ger. |
| Queue shown is maximum after two cycles. | |
| Splits and Phases: 1: Ninth Line & Dundas Street East | |

| Øø1 | ₩Ø2 (R) | Ø3 | √ Ø4 |
|-----------|---------|-------------|-------------|
| 20 s | 70 s | 19 s | 51s |
| 1 Ø5 7 Ø6 | (R) | 1 Ø7 | Ø8 |
| 10 s 80 s | | 30 s | 40 s |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | 1 | • | • | 1 | Ť | 1 | 4 | ŧ | ~ |
|---------------------------------|-----------|------|--------|-------|-----------|------------|---------|------|-------|-------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 5 | *** | 1 | 7 | *** | 1 | 5 | ** | 1 | 5 | * * | 1 |
| Traffic Volume (vph) | 182 | 1810 | 217 | 118 | 2827 | 250 | 378 | 903 | 558 | 203 | 389 | 194 |
| Future Volume (vph) | 182 | 1810 | 217 | 118 | 2827 | 250 | 378 | 903 | 558 | 203 | 389 | 194 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 2.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frpb, ped/bikes | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.99 |
| Flpb, ped/bikes | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5036 | 1455 | 1694 | 5085 | 1506 | 1651 | 3500 | 1478 | 1652 | 3433 | 1459 |
| Flt Permitted | 0.06 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.32 | 1.00 | 1.00 | 0.11 | 1.00 | 1.00 |
| Satd. Flow (perm) | 107 | 5036 | 1455 | 104 | 5085 | 1506 | 554 | 3500 | 1478 | 193 | 3433 | 1459 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 198 | 1967 | 236 | 128 | 3073 | 272 | 411 | 982 | 607 | 221 | 423 | 211 |
| RTOR Reduction (vph) | 0 | 0 | 90 | 0 | 0 | 67 | 0 | 0 | 33 | 0 | 0 | 106 |
| Lane Group Flow (vph) | 198 | 1967 | 146 | 128 | 3073 | 205 | 411 | 982 | 574 | 221 | 423 | 105 |
| Confl. Peds. (#/hr) | | | 3 | 3 | | | 1 | | | | | 1 |
| Heavy Vehicles (%) | 2% | 3% | 4% | 3% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 70.3 | 64.3 | 64.3 | 83.1 | 73.1 | 73.1 | 63.0 | 44.0 | 58.8 | 48.0 | 33.0 | 33.0 |
| Effective Green, g (s) | 76.3 | 66.2 | 66.2 | 86.1 | 75.0 | 75.0 | 66.0 | 46.0 | 62.8 | 54.0 | 35.0 | 35.0 |
| Actuated g/C Ratio | 0.48 | 0.41 | 0.41 | 0.54 | 0.47 | 0.47 | 0.41 | 0.29 | 0.39 | 0.34 | 0.22 | 0.22 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 4.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 141 | 2083 | 602 | 232 | 2383 | 705 | 427 | 1006 | 580 | 229 | 750 | 319 |
| v/s Ratio Prot | c0.08 | 0.39 | | 0.06 | 0.60 | | c0.17 | 0.28 | c0.10 | c0.11 | 0.12 | |
| v/s Ratio Perm | c0.59 | | 0.10 | 0.23 | | 0.14 | 0.22 | | 0.28 | 0.22 | | 0.07 |
| v/c Ratio | 1.40 | 0.94 | 0.24 | 0.55 | 1.29 | 0.29 | 0.96 | 0.98 | 0.99 | 0.97 | 0.56 | 0.33 |
| Uniform Delay, d1 | 46.7 | 45.1 | 30.6 | 37.7 | 42.5 | 26.1 | 39.0 | 56.5 | 48.3 | 47.5 | 55.7 | 52.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 218.8 | 10.4 | 1.0 | 3.1 | 133.6 | 1.0 | 33.9 | 22.6 | 34.5 | 49.4 | 1.1 | 0.7 |
| Delay (s) | 265.5 | 55.5 | 31.5 | 40.8 | 176.1 | 27.2 | 72.9 | 79.0 | 82.8 | 96.9 | 56.8 | 53.3 |
| Level of Service | F | E | С | D | F | С | E | E | F | F | E | D |
| Approach Delay (s) | | 70.5 | | | 159.4 | | | 78.9 | | | 66.3 | |
| Approach LOS | | E | | | F | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 107.4 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capac | ity ratio | | 1.21 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 160.0 | S | um of los | t time (s) | | | 13.0 | | | |
| Intersection Capacity Utilizati | on | | 115.9% | IC | U Level | of Service | 9 | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

c Critical Lane Group

HCM 6th Signalized Intersection Summary 1: Ninth Line & Dundas Street East

| | ٠ | + | * | • | + | * | 1 | 1 | 1 | 1 | Ŧ | ~ |
|------------------------------|-------|-------|-------|------|----------|-------|------|----------|-------|------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٢ | *** | 1 | 7 | ^ | 1 | 7 | ^ | 1 | 7 | † † | 1 |
| Traffic Volume (veh/h) | 182 | 1810 | 217 | 118 | 2827 | 250 | 378 | 903 | 558 | 203 | 389 | 194 |
| Future Volume (veh/h) | 182 | 1810 | 217 | 118 | 2827 | 250 | 378 | 903 | 558 | 203 | 389 | 194 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1856 | 1841 | 1856 | 1870 | 1870 | 1796 | 1870 | 1796 | 1796 | 1841 | 1796 |
| Adj Flow Rate, veh/h | 198 | 1967 | 236 | 128 | 3073 | 272 | 411 | 982 | 607 | 221 | 423 | 211 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 3 | 4 | 3 | 2 | 2 | 2 | 2 | 2 | 2 | 4 | 2 |
| Cap, veh/h | 146 | 2312 | 699 | 186 | 2393 | 730 | 444 | 1022 | 532 | 244 | 765 | 332 |
| Arrive On Green | 0.06 | 0.46 | 0.46 | 0.07 | 0.47 | 0.47 | 0.18 | 0.29 | 0.29 | 0.11 | 0.22 | 0.22 |
| Sat Flow, veh/h | 1/81 | 5066 | 1532 | 1/6/ | 5106 | 1557 | 1/10 | 3554 | 1520 | 1/10 | 3497 | 1520 |
| Grp Volume(v), veh/h | 198 | 1967 | 236 | 128 | 3073 | 272 | 411 | 982 | 607 | 221 | 423 | 211 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1689 | 1532 | 1767 | 1702 | 1557 | 1710 | 1777 | 1520 | 1710 | 1749 | 1520 |
| Q Serve(g_s), s | 9.0 | 55.2 | 15.8 | 5.7 | 75.0 | 18.0 | 29.0 | 43.5 | 46.0 | 15.7 | 17.2 | 20.2 |
| Cycle Q Clear(g_c), s | 9.0 | 55.2 | 15.8 | 5.7 | 75.0 | 18.0 | 29.0 | 43.5 | 46.0 | 15.7 | 17.2 | 20.2 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 146 | 2312 | 699 | 186 | 2393 | 730 | 444 | 1022 | 532 | 244 | 765 | 332 |
| V/C Ratio(X) | 1.36 | 0.85 | 0.34 | 0.69 | 1.28 | 0.37 | 0.92 | 0.96 | 1.14 | 0.91 | 0.55 | 0.63 |
| Avail Cap(c_a), veh/h | 146 | 2312 | 699 | 274 | 2393 | 730 | 444 | 1022 | 532 | 244 | 765 | 332 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 50.1 | 38.6 | 27.9 | 34.6 | 42.5 | 27.4 | 38.4 | 56.1 | 52.0 | 44.3 | 55.5 | 56.7 |
| Incr Delay (d2), s/veh | 199.9 | 4.2 | 1.3 | 5.4 | 131.1 | 1.5 | 25.3 | 19.4 | 84.3 | 33.8 | 1.0 | 4.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 14.3 | 25.1 | 6.6 | 2.9 | 62.2 | 7.6 | 16.2 | 23.2 | 34.8 | 9.4 | 8.1 | 8.5 |
| Unsig. Movement Delay, s/veh | 050.0 | 40.0 | 00.0 | 10.0 | 170.0 | 00.0 | 00 7 | 75.0 | 100.0 | 70.0 | 50.5 | 00.0 |
| LnGrp Delay(d),s/veh | 250.0 | 42.8 | 29.2 | 40.0 | 1/3.6 | 28.8 | 63.7 | /5.6 | 136.3 | /8.2 | 56.5 | 60.9 |
| LnGrp LOS | F | D | C | D | F | C | E | E | F | E | E | E |
| Approach Vol, veh/h | | 2401 | | | 3473 | | | 2000 | | | 855 | |
| Approach Delay, s/veh | | 58.6 | | | 157.3 | | | 91.6 | | | 63.2 | |
| Approach LOS | | E | | | F | | | F | | | E | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 12.0 | 78.0 | 19.0 | 51.0 | 10.0 | 80.0 | 30.0 | 40.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 16.0 | * 63 | 15.0 | 44.0 | 6.0 | * 73 | 26.0 | 33.0 | | | | |
| Max Q Clear Time (g_c+I1), s | 7.7 | 58.2 | 17.7 | 48.0 | 11.0 | 77.0 | 31.0 | 22.2 | | | | |
| Green Ext Time (p_c), s | 0.3 | 4.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.5 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 105.9 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Lanes, Volumes, Timings 2: Ninth Line & Glen Oaks Access/Dymon Site Access

| | ٨ | → | 7 | 1 | + | * | 1 | Ť | 1 | 1 | ŧ | ~ |
|-----------------------------------|----------|----------|-------|------|------------|------------|------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | -fî† | | ۲ | ĥ | |
| Traffic Volume (vph) | 11 | 0 | 38 | 47 | 0 | 6 | 23 | 1286 | 36 | 4 | 727 | 5 |
| Future Volume (vph) | 11 | 0 | 38 | 47 | 0 | 6 | 23 | 1286 | 36 | 4 | 727 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.5 | 3.2 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.5 | 3.3 | 3.5 | 3.5 |
| Storage Length (m) | 0.0 | | 0.0 | 0.0 | | 0.0 | 0.0 | | 0.0 | 15.0 | | 0.0 |
| Storage Lanes | 0 | | 0 | 0 | | 0 | 0 | | 0 | 1 | | 0 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 0.95 | 1.00 | 1.00 | 1.00 |
| Ped Bike Factor | | | | | | | | | | | | |
| Frt | | 0.896 | | | 0.984 | | | 0.996 | | | 0.999 | |
| Flt Protected | | 0.989 | | | 0.958 | | | 0.999 | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1632 | 0 | 0 | 1736 | 0 | 0 | 3482 | 0 | 1711 | 1840 | 0 |
| Flt Permitted | | 0.989 | | | 0.958 | | | 0.999 | | 0.950 | | |
| Satd. Flow (perm) | 0 | 1632 | 0 | 0 | 1736 | 0 | 0 | 3482 | 0 | 1711 | 1840 | 0 |
| Link Speed (k/h) | | 60 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 47.4 | | | 58.5 | | | 51.2 | | | 158.7 | |
| Travel Time (s) | | 2.8 | | | 3.5 | | | 3.1 | | | 9.5 | |
| Confl. Peds. (#/hr) | | | 2 | | | | | | | | | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 12 | 0 | 41 | 51 | 0 | 7 | 25 | 1398 | 39 | 4 | 790 | 5 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 53 | 0 | 0 | 58 | 0 | 0 | 1462 | 0 | 4 | 795 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.3 | | | 3.3 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | Yes | | | Yes | |
| Headway Factor | 1.06 | 1.01 | 1.06 | 1.01 | 1.01 | 1.01 | 1.04 | 1.01 | 1.01 | 1.04 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: C | other | | | | | | | | | | | |
| Control Type: Unsignalized | | | | | | | | | | | | |
| Intersection Capacity Utilization | on 69.0% | | | IC | CU Level o | of Service | С | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |

| | ٨ | - | 7 | 1 | - | * | 1 | 1 | 1 | 1 | Ŧ | ~ |
|------------------------------|-------|------|-------|------|-------------|------------|------|-------------|------|------|-------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | | ≜ 12 | | 5 | î, | |
| Traffic Volume (veh/h) | 11 | 0 | 38 | 47 | 0 | 6 | 23 | 1286 | 36 | 4 | 727 | 5 |
| Future Volume (Veh/h) | 11 | 0 | 38 | 47 | 0 | 6 | 23 | 1286 | 36 | 4 | 727 | 5 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 12 | 0 | 41 | 51 | 0 | 7 | 25 | 1398 | 39 | 4 | 790 | 5 |
| Pedestrians | | | | | | | | 2 | | | | |
| Lane Width (m) | | | | | | | | 3.5 | | | | |
| Walking Speed (m/s) | | | | | | | | 1.1 | | | | |
| Percent Blockage | | | | | | | | 0 | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | TWLTL | | | TWLTL | |
| Median storage veh) | | | | | | | | 2 | | | 2 | |
| Upstream signal (m) | | | | | | | | 147 | | | | |
| pX, platoon unblocked | 0.72 | 0.72 | | 0.72 | 0.72 | 0.72 | | | | 0.72 | | |
| vC, conflicting volume | 1556 | 2288 | 794 | 2308 | 2270 | 718 | 795 | | | 1437 | | |
| vC1, stage 1 conf vol | 800 | 800 | | 1468 | 1468 | | | | | | | |
| vC2, stage 2 conf vol | 756 | 1487 | | 841 | 803 | | | | | | | |
| vCu, unblocked vol | 1006 | 2016 | 794 | 2045 | 1992 | 0 | 795 | | | 841 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | 6.5 | 5.5 | | 6.5 | 5.5 | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 96 | 100 | 88 | 68 | 100 | 99 | 97 | | | 99 | | |
| cM capacity (veh/h) | 316 | 203 | 330 | 159 | 205 | 785 | 822 | | | 572 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | SB 1 | SB 2 | | | | | | |
| Volume Total | 53 | 58 | 724 | 738 | 4 | 795 | | | | | | |
| Volume Left | 12 | 51 | 25 | 0 | 4 | 0 | | | | | | |
| Volume Right | 41 | 7 | 0 | 39 | 0 | 5 | | | | | | |
| cSH | 327 | 176 | 822 | 1700 | 572 | 1700 | | | | | | |
| Volume to Capacity | 0.16 | 0.33 | 0.03 | 0.43 | 0.01 | 0.47 | | | | | | |
| Queue Length 95th (m) | 4.0 | 9.5 | 0.7 | 0.0 | 0.1 | 0.0 | | | | | | |
| Control Delay (s) | 18.1 | 35.3 | 0.8 | 0.0 | 11.3 | 0.0 | | | | | | |
| Lane LOS | С | Е | А | | В | | | | | | | |
| Approach Delay (s) | 18.1 | 35.3 | 0.4 | | 0.1 | | | | | | | |
| Approach LOS | С | E | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 1.5 | | | | | | | | | |
| Intersection Capacity Utiliz | ation | | 69.0% | IC | CU Level of | of Service | | | С | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Appendix S

2031 Future Total Synchro Intersection Worksheets



Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٠ | → | 7 | 4 | + | • | 1 | Ť | 1 | 1 | ţ | ~ |
|----------------------------|-------|----------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ۲ | *** | 1 | 5 | *** | 1 | 7 | 44 | 1 | ۲ | ** | 1 |
| Traffic Volume (vph) | 229 | 2865 | 390 | 195 | 1328 | 164 | 210 | 462 | 196 | 284 | 759 | 186 |
| Future Volume (vph) | 229 | 2865 | 390 | 195 | 1328 | 164 | 210 | 462 | 196 | 284 | 759 | 186 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.071 | | | 0.064 | | | 0.090 | | | 0.328 | | |
| Satd. Flow (perm) | 128 | 5085 | 1491 | 111 | 4715 | 1449 | 145 | 3433 | 1422 | 565 | 3466 | 1478 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd. Flow (RTOR) | | | 196 | | | 146 | | | 111 | | | 158 |
| Link Speed (k/h) | | 70 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 329.1 | | | 188.2 | | | 146.7 | |
| Travel Time (s) | | 15.1 | | | 19.7 | | | 11.3 | | | 8.8 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Adj. Flow (vph) | 249 | 3114 | 424 | 212 | 1443 | 178 | 228 | 502 | 213 | 309 | 825 | 202 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 249 | 3114 | 424 | 212 | 1443 | 178 | 228 | 502 | 213 | 309 | 825 | 202 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 3.3 | Ŭ | | 3.3 | Ŭ | | 3.3 | Ŭ | | 3.3 | Ŭ |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | | | | Yes | |
| Headway Factor | 1.04 | 1.00 | 1.07 | 1.04 | 1.00 | 1.07 | 1.09 | 1.01 | 1.09 | 1.09 | 1.01 | 1.09 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 | 1 | 2 | 1 |
| Detector Template | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right | Left | Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 | 2.0 | 0.6 | 2.0 |
| Detector 1 Type | CI+Ex | CI+Ex | CI+Ex | Cl+Ex | CI+Ex | CI+Ex |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | CI+Ex | | | CI+Ex | | | CI+Ex | | | Cl+Ex | |
| Detector 2 Channel | | | | | | | | | | | | |
| Detector 2 Extend (s) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |

Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

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|----------------------------|--------------|----------|----------|-------------|------------|----------|--------|-------|-------|-------|--------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 4 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 9.0 | 52.9 | 52.9 | 9.0 | 52.9 | 52.9 | 9.0 | 56.0 | 56.0 | 9.0 | 56.0 | 56.0 |
| Total Split (s) | 29.0 | 80.0 | 80.0 | 11.0 | 62.0 | 62.0 | 21.0 | 50.0 | 50.0 | 19.0 | 48.0 | 48.0 |
| Total Split (%) | 18.1% | 50.0% | 50.0% | 6.9% | 38.8% | 38.8% | 13.1% | 31.3% | 31.3% | 11.9% | 30.0% | 30.0% |
| Maximum Green (s) | 25.0 | 73.1 | 73.1 | 7.0 | 55.1 | 55.1 | 17.0 | 43.0 | 43.0 | 15.0 | 41.0 | 41.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.7 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 3.3 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | -3.0 | -1.9 | -1.9 | -3.0 | -1.9 | -1.9 | -3.0 | -2.0 | -2.0 | -3.0 | -2.0 | -2.0 |
| Total Lost Time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | 15.0 | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | 34.0 | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | 0 | | 0 | 0 |
| Act Effct Green (s) | 90.8 | 75.0 | 75.0 | 75.9 | 61.1 | 61.1 | 67.2 | 44.2 | 44.2 | 64.2 | 42.2 | 42.2 |
| Actuated g/C Ratio | 0.57 | 0.47 | 0.47 | 0.47 | 0.38 | 0.38 | 0.42 | 0.28 | 0.28 | 0.40 | 0.26 | 0.26 |
| v/c Ratio | 0.79 | 1.31 | 0.53 | 1.36 | 0.80 | 0.28 | 0.97 | 0.53 | 0.45 | 0.89 | 0.90 | 0.40 |
| Control Delay | 58.7 | 176.8 | 17.7 | 232.3 | 49.0 | 9.4 | 97.2 | 51.3 | 25.3 | 63.4 | 70.6 | 14.3 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 58.7 | 176.8 | 17.7 | 232.3 | 49.0 | 9.4 | 97.2 | 51.3 | 25.3 | 63.4 | 70.6 | 14.3 |
| LOS | E | F | В | F | D | А | F | D | С | E | E | В |
| Approach Delay | | 151.3 | | | 66.3 | | | 56.5 | | | 60.5 | |
| Approach LOS | | F | | | E | | | E | | | E | |
| Queue Length 50th (m) | 53.7 | ~427.2 | 45.8 | ~71.4 | 141.9 | 6.1 | 53.9 | 65.5 | 23.9 | 63.7 | 123.0 | 9.8 |
| Queue Length 95th (m) | 82.9 | #445.0 | 75.2 | #121.7 | 161.7 | 22.6 | #104.5 | 82.5 | 47.3 | #85.8 | #152.7 | 30.8 |
| Internal Link Dist (m) | | 269.2 | | | 305.1 | | | 164.2 | | | 122.7 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 350 | 2383 | 803 | 156 | 1801 | 643 | 234 | 965 | 479 | 347 | 931 | 512 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.71 | 1.31 | 0.53 | 1.36 | 0.80 | 0.28 | 0.97 | 0.52 | 0.44 | 0.89 | 0.89 | 0.39 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 160 | | | | | | | | | | | | |
| Actuated Cycle Length: 16 | 60 | | | | | | | | | | | |
| Offset: 0 (0%), Referenced | d to phase 2 | :EBTL an | d 6:WBTI | _, Start of | Green | | | | | | | |
| Natural Cycle: 160 | | | | | | | | | | | | |
| Control Type: Actuated-Co | oordinated | | | | | | | | | | | |
| Maximum v/c Ratio: 1.36 | | | | | | | | | | | | |
| Intersection Signal Delay: | 104.9 | | | li | ntersectio | n LOS: F | | | | | | |

Intersection Capacity Utilization 113.8%

ICU Level of Service H

Analysis Period (min) 15

- Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.
- # 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: Ninth Line & Dundas Street East

| ✓ Ø1 → Ø2 (R) | Ø3 Ø4 |
|---------------------|-----------|
| 11 s 80 s | 19 s 50 s |
| ≠ Ø5 0 6 (R) | ↑ Ø7 Ø8 |
| 29 s 62 s | 21 s 48 s |

HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

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|-------------------------------|------------|-------|--------|-------|-----------|------------|---------|----------|------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٢ | *** | 1 | ۲ | *** | 1 | ň | ^ | 1 | ۲ | ^ | 1 |
| Traffic Volume (vph) | 229 | 2865 | 390 | 195 | 1328 | 164 | 210 | 462 | 196 | 284 | 759 | 186 |
| Future Volume (vph) | 229 | 2865 | 390 | 195 | 1328 | 164 | 210 | 462 | 196 | 284 | 759 | 186 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 | 1.0 | 5.0 | 5.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5085 | 1491 | 1646 | 4715 | 1449 | 1532 | 3433 | 1422 | 1636 | 3466 | 1478 |
| Flt Permitted | 0.07 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.09 | 1.00 | 1.00 | 0.33 | 1.00 | 1.00 |
| Satd. Flow (perm) | 129 | 5085 | 1491 | 111 | 4715 | 1449 | 146 | 3433 | 1422 | 564 | 3466 | 1478 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 249 | 3114 | 424 | 212 | 1443 | 178 | 228 | 502 | 213 | 309 | 825 | 202 |
| RTOR Reduction (vph) | 0 | 0 | 104 | 0 | 0 | 90 | 0 | 0 | 80 | 0 | 0 | 116 |
| Lane Group Flow (vph) | 249 | 3114 | 320 | 212 | 1443 | 88 | 228 | 502 | 133 | 309 | 825 | 86 |
| Heavy Vehicles (%) | 2% | 2% | 3% | 6% | 10% | 6% | 10% | 4% | 6% | 3% | 3% | 2% |
| Bus Blockages (#/hr) | 0 | 0 | 4 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 84.9 | 73.1 | 73.1 | 67.1 | 59.3 | 59.3 | 59.2 | 42.2 | 42.2 | 55.2 | 40.2 | 40.2 |
| Effective Green, g (s) | 87.9 | 75.0 | 75.0 | 73.1 | 61.2 | 61.2 | 64.2 | 44.2 | 44.2 | 61.2 | 42.2 | 42.2 |
| Actuated g/C Ratio | 0.55 | 0.47 | 0.47 | 0.46 | 0.38 | 0.38 | 0.40 | 0.28 | 0.28 | 0.38 | 0.26 | 0.26 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 7.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 314 | 2383 | 698 | 154 | 1803 | 554 | 231 | 948 | 392 | 336 | 914 | 389 |
| v/s Ratio Prot | 0.12 | c0.61 | | c0.09 | 0.31 | | c0.12 | 0.15 | | 0.10 | 0.24 | |
| v/s Ratio Perm | 0.31 | | 0.21 | c0.53 | | 0.06 | 0.27 | | 0.09 | c0.25 | | 0.06 |
| v/c Ratio | 0.79 | 1.31 | 0.46 | 1.38 | 0.80 | 0.16 | 0.99 | 0.53 | 0.34 | 0.92 | 0.90 | 0.22 |
| Uniform Delay, d1 | 45.5 | 42.5 | 28.8 | 48.1 | 44.0 | 32.5 | 50.2 | 49.1 | 46.2 | 41.8 | 56.9 | 46.0 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 13.2 | 141.2 | 2.2 | 204.8 | 3.8 | 0.6 | 55.2 | 0.6 | 0.6 | 29.5 | 12.3 | 0.3 |
| Delay (s) | 58.7 | 183.7 | 30.9 | 252.9 | 47.8 | 33.1 | 105.3 | 49.7 | 46.8 | 71.3 | 69.2 | 46.4 |
| Level of Service | E | F | С | F | D | С | F | D | D | E | E | D |
| Approach Delay (s) | | 158.4 | | | 70.1 | | | 62.5 | | | 66.2 | |
| Approach LOS | | F | | | E | | | E | | | E | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 110.9 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capa | city ratio | | 1.16 | | | | | | | | | |
| Actuated Cycle Length (s) | | | 160.0 | S | um of los | t time (s) | | | 12.0 | | | |
| Intersection Capacity Utiliza | tion | | 113.8% | IC | CU Level | of Service | Э | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM 6th Signalized Intersection Summary 1: Ninth Line & Dundas Street East

| | ۶ | → | 7 | 4 | ← | * | 1 | t | 1 | 1 | ŧ | ~ |
|-------------------------------|------|----------|-------|-------|------|-------|------|----------|------|------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 1 | *** | 1 | ٦ | *** | 1 | 7 | ^ | 1 | 7 | <u>^</u> | 1 |
| Traffic Volume (veh/h) | 229 | 2865 | 390 | 195 | 1328 | 164 | 210 | 462 | 196 | 284 | 759 | 186 |
| Future Volume (veh/h) | 229 | 2865 | 390 | 195 | 1328 | 164 | 210 | 462 | 196 | 284 | 759 | 186 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 0.98 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1856 | 1811 | 1752 | 1811 | 1682 | 1841 | 1739 | 1781 | 1856 | 1796 |
| Adj Flow Rate, veh/h | 249 | 3114 | 424 | 212 | 1443 | 178 | 228 | 502 | 213 | 309 | 825 | 202 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 3 | 6 | 10 | 6 | 10 | 4 | 6 | 3 | 3 | 2 |
| Cap, veh/h | 305 | 2425 | 735 | 153 | 2022 | 639 | 267 | 962 | 405 | 348 | 926 | 400 |
| Arrive On Green | 0.11 | 0.47 | 0.47 | 0.06 | 0.42 | 0.42 | 0.13 | 0.28 | 0.28 | 0.11 | 0.26 | 0.26 |
| Sat Flow, veh/h | 1781 | 5106 | 1547 | 1725 | 4782 | 1510 | 1602 | 3497 | 1473 | 1696 | 3526 | 1522 |
| Grp Volume(v), veh/h | 249 | 3114 | 424 | 212 | 1443 | 178 | 228 | 502 | 213 | 309 | 825 | 202 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1702 | 1547 | 1725 | 1594 | 1510 | 1602 | 1749 | 1473 | 1696 | 1763 | 1522 |
| Q Serve(g_s), s | 12.5 | 76.0 | 31.7 | 10.0 | 39.9 | 12.3 | 15.8 | 19.4 | 19.6 | 18.0 | 36.0 | 18.1 |
| Cycle Q Clear(g_c), s | 12.5 | 76.0 | 31.7 | 10.0 | 39.9 | 12.3 | 15.8 | 19.4 | 19.6 | 18.0 | 36.0 | 18.1 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 305 | 2425 | 735 | 153 | 2022 | 639 | 267 | 962 | 405 | 348 | 926 | 400 |
| V/C Ratio(X) | 0.82 | 1.28 | 0.58 | 1.39 | 0.71 | 0.28 | 0.85 | 0.52 | 0.53 | 0.89 | 0.89 | 0.51 |
| Avail Cap(c a), veh/h | 413 | 2425 | 735 | 153 | 2022 | 639 | 267 | 984 | 414 | 348 | 947 | 409 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 33.6 | 42.0 | 30.4 | 49.6 | 38.2 | 30.2 | 38.9 | 49.1 | 49.1 | 43.2 | 56.8 | 50.2 |
| Incr Delay (d2), s/veh | 9.7 | 131.2 | 3.3 | 209.3 | 2.2 | 1.1 | 23.1 | 0.6 | 1.4 | 23.4 | 10.6 | 1.2 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/In | 11.0 | 63.0 | 13.4 | 15.4 | 17.0 | 5.0 | 8.3 | 9.1 | 7.8 | 6.9 | 18.2 | 7.4 |
| Unsig. Movement Delay, s/veh | | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 43.3 | 173.2 | 33.7 | 258.9 | 40.3 | 31.3 | 61.9 | 49.6 | 50.5 | 66.7 | 67.4 | 51.4 |
| LnGrp LOS | D | F | С | F | D | С | E | D | D | E | E | D |
| Approach Vol. veh/h | | 3787 | | | 1833 | | | 943 | | | 1336 | |
| Approach Delay, s/yeh | | 149.0 | | | 64.7 | | | 52.8 | | | 64.8 | |
| Approach LOS | | F | | | E | | | D | | | E | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 11.0 | 81.0 | 19.0 | 49.0 | 19.3 | 72.7 | 21.0 | 47.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 7.0 | * 73 | 15.0 | 43.0 | 25.0 | * 55 | 17.0 | 41.0 | | | | |
| Max Q Clear Time (q. c+l1), s | 12.0 | 79.0 | 20.0 | 21.6 | 14.5 | 41.9 | 17.8 | 38.0 | | | | |
| Green Ext Time (p_c), s | 0.0 | 0.0 | 0.0 | 5.6 | 0.9 | 11.8 | 0.0 | 2.0 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delay | | | 103.7 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

User approved changes to right turn type.

Lanes, Volumes, Timings 2: Ninth Line & Glen Oaks Access/Site Access

| | ٨ | → | 7 | - | + | * | 1 | Ť | 1 | 1 | ŧ | ~ |
|---------------------------------|----------|----------|-------|------|----------|------------|-------|-------------------------|-------|-------|-------------------------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | 7 | † 1 ₂ | | 7 | † 1 ₂ | |
| Traffic Volume (vph) | 3 | 0 | 4 | 17 | 0 | 2 | 25 | 850 | 83 | 10 | 1264 | 6 |
| Future Volume (vph) | 3 | 0 | 4 | 17 | 0 | 2 | 25 | 850 | 83 | 10 | 1264 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.5 | 3.2 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Storage Length (m) | 15.0 | | 0.0 | 15.0 | | 0.0 | 30.0 | | 0.0 | 0.0 | | 0.0 |
| Storage Lanes | 0 | | 0 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Ped Bike Factor | | | | | | | | | | | | |
| Frt | | 0.923 | | | 0.986 | | | 0.987 | | | 0.999 | |
| Flt Protected | | 0.979 | | | 0.957 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1665 | 0 | 0 | 1738 | 0 | 1711 | 3394 | 0 | 1750 | 3463 | 0 |
| Flt Permitted | | 0.979 | | | 0.957 | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 0 | 1665 | 0 | 0 | 1738 | 0 | 1711 | 3394 | 0 | 1750 | 3463 | 0 |
| Link Speed (k/h) | | 60 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 47.4 | | | 56.2 | | | 146.7 | | | 158.7 | |
| Travel Time (s) | | 2.8 | | | 3.4 | | | 8.8 | | | 9.5 | |
| Confl. Bikes (#/hr) | | | | | | | | | | | | 1 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (%) | 2% | 2% | 2% | 2% | 2% | 2% | 2% | 4% | 2% | 2% | 3% | 2% |
| Adj. Flow (vph) | 3 | 0 | 4 | 18 | 0 | 2 | 27 | 924 | 90 | 11 | 1374 | 7 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 7 | 0 | 0 | 20 | 0 | 27 | 1014 | 0 | 11 | 1381 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.5 | | | 3.5 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | Yes | | | Yes | |
| Headway Factor | 1.06 | 1.01 | 1.06 | 1.01 | 1.01 | 1.01 | 1.04 | 1.01 | 1.01 | 1.01 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: C | other | | | | | | | | | | | |
| Control Type: Unsignalized | | | | | | | | | | | | |
| Intersection Capacity Utilizati | on 45.1% | | | IC | CU Level | of Service | Α | | | | | |
| Analysis Period (min) 15 | | | | | | | | | | | | |

| | ▲ | - | 7 | 4 | + | * | 1 | 1 | 1 | 1 | Ŧ | ~ |
|------------------------------|-------|------|-------|------|------------|------------|------|-------------|------|------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | 7 | ≜ 1≽ | | ۲ | † Ъ | |
| Traffic Volume (veh/h) | 3 | 0 | 4 | 17 | 0 | 2 | 25 | 850 | 83 | 10 | 1264 | 6 |
| Future Volume (Veh/h) | 3 | 0 | 4 | 17 | 0 | 2 | 25 | 850 | 83 | 10 | 1264 | 6 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 3 | 0 | 4 | 18 | 0 | 2 | 27 | 924 | 90 | 11 | 1374 | 7 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (m) | | | | | | | | | | | | |
| Walking Speed (m/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | TWLTL | | | TWLTL | |
| Median storage veh) | | | | | | | | 2 | | | 2 | |
| Upstream signal (m) | | | | | | | | 147 | | | | |
| pX, platoon unblocked | 0.88 | 0.88 | | 0.88 | 0.88 | 0.88 | | | | 0.88 | | |
| vC, conflicting volume | 1918 | 2468 | 690 | 1736 | 2426 | 507 | 1381 | | | 1014 | | |
| vC1, stage 1 conf vol | 1400 | 1400 | | 1023 | 1023 | | | | | | | |
| vC2, stage 2 conf vol | 518 | 1068 | | 713 | 1403 | | | | | | | |
| vCu, unblocked vol | 1771 | 2395 | 690 | 1565 | 2348 | 170 | 1381 | | | 745 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | 6.5 | 5.5 | | 6.5 | 5.5 | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 98 | 100 | 99 | 92 | 100 | 100 | 95 | | | 99 | | |
| cM capacity (veh/h) | 140 | 166 | 387 | 232 | 153 | 744 | 492 | | | 756 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 | | | | |
| Volume Total | 7 | 20 | 27 | 616 | 398 | 11 | 916 | 465 | | | | |
| Volume Left | 3 | 18 | 27 | 0 | 0 | 11 | 0 | 0 | | | | |
| Volume Right | 4 | 2 | 0 | 0 | 90 | 0 | 0 | 7 | | | | |
| cSH | 220 | 250 | 492 | 1700 | 1700 | 756 | 1700 | 1700 | | | | |
| Volume to Capacity | 0.03 | 0.08 | 0.05 | 0.36 | 0.23 | 0.01 | 0.54 | 0.27 | | | | |
| Queue Length 95th (m) | 0.7 | 1.8 | 1.2 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 | | | | |
| Control Delay (s) | 21.9 | 20.7 | 12.7 | 0.0 | 0.0 | 9.8 | 0.0 | 0.0 | | | | |
| Lane LOS | С | С | В | | | А | | | | | | |
| Approach Delay (s) | 21.9 | 20.7 | 0.3 | | | 0.1 | | | | | | |
| Approach LOS | С | С | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 0.4 | | | | | | | | | |
| Intersection Capacity Utiliz | ation | | 45.1% | IC | CU Level o | of Service | | | А | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |

Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٠ | + | 7 | 4 | + | • | 1 | Ť | 1 | 1 | ţ | ~ |
|----------------------------|-----------|-----------|----------|-----------|-----------|--------|---------|-----------|--------|-------|-----------|--------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | *** | 1 | 7 | *** | 1 | 7 | ^ | 1 | 7 | ^ | 1 |
| Traffic Volume (vph) | 194 | 1986 | 229 | 127 | 3102 | 269 | 416 | 1046 | 617 | 223 | 483 | 211 |
| Future Volume (vph) | 194 | 1986 | 229 | 127 | 3102 | 269 | 416 | 1046 | 617 | 223 | 483 | 211 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Storage Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Storage Lanes | 1 | | 1 | 1 | | 1 | 1 | | 1 | 1 | | 1 |
| Taper Length (m) | 55.0 | | | 60.0 | | | 80.0 | | | 70.0 | | |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | | | 0.850 | | | 0.850 | | | 0.850 | | | 0.850 |
| Flt Protected | 0.950 | | | 0.950 | | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 1711 | 5085 | 1531 | 1711 | 5085 | 1531 | 1652 | 3500 | 1478 | 1652 | 3500 | 1478 |
| Flt Permitted | 0.061 | | | 0.057 | | | 0.191 | | | 0.129 | | |
| Satd. Flow (perm) | 110 | 5085 | 1531 | 103 | 5085 | 1531 | 332 | 3500 | 1478 | 224 | 3500 | 1478 |
| Right Turn on Red | | | Yes | | | Yes | | | Yes | | | Yes |
| Satd, Flow (RTOR) | | | 150 | | | 119 | | | 54 | | | 136 |
| Link Speed (k/h) | | 70 | | | 60 | - | | 60 | | | 60 | |
| Link Distance (m) | | 293.2 | | | 526.7 | | | 188.2 | | | 146.7 | |
| Travel Time (s) | | 15.1 | | | 31.6 | | | 11.3 | | | 8.8 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adi Flow (vph) | 211 | 2159 | 249 | 138 | 3372 | 292 | 452 | 1137 | 671 | 242 | 525 | 229 |
| Shared Lane Traffic (%) | | 2100 | 2.10 | 100 | 0012 | 202 | 102 | | 011 | | 020 | 220 |
| Lane Group Flow (vph) | 211 | 2159 | 249 | 138 | 3372 | 292 | 452 | 1137 | 671 | 242 | 525 | 229 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | Lon | 3.3 | rtigitt | Lon | 3.3 | rtight | Lon | 3.3 | rugitu | Lon | 3.3 | rugitu |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | 0.0 | | | 0.0 | | | 0.0 | | | Yes | |
| Headway Eactor | 1 04 | 1 00 | 1 04 | 1 04 | 1 00 | 1 04 | 1 09 | 1 01 | 1 09 | 1 09 | 1 01 | 1 09 |
| Turning Speed (k/h) | 25 | 1.00 | 1.04 | 25 | 1.00 | 1.04 | 25 | 1.01 | 1.00 | 25 | 1.01 | 1.05 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 | 10 | 1 | 2 | 1 | 1 | 2 | 10 |
| Detector Template | ا ftما | ∠ Thru | Right | ا ام ا | ∠ Thru | Right | ا ft | ∠ Thru | Right | ا ما | ∠ Thru | Right |
| Leading Detector (m) | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 | 2.0 | 10.0 | 2.0 |
| Trailing Detector (m) | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 |
| Detector 1 Position(m) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Size(m) | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 | 2.0 | 0.0 | 2.0 |
| Detector 1 Size(iii) | | | | | | | | | | | | |
| Detector 1 Channel | | | | | | | | | | | | |
| Detector 1 Extend (a) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Outputs (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 1 Queue (S) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector I Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Detector 2 Position(m) | | 9.4 | | | 9.4 | | | 9.4 | | | 9.4 | |
| Detector 2 Size(m) | | 0.6 | | | 0.6 | | | 0.6 | | | 0.6 | |
| Detector 2 Type | | CI+EX | | | CI+EX | | | CI+EX | | | CI+EX | |
| Detector 2 Unannel | | 0.0 | | | 0.0 | | | 0.0 | | | ~ ~ ~ | |
| Detector 2 Extend (s) | | 0.0 | D | | 0.0 | D | 1 | 0.0 | | , | 0.0 | D |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | 1 | 3 | 8 | |

07-17-2023

Lanes, Volumes, Timings <u>1: Ninth Line & Dundas Street East</u>

| | ٨ | - | 7 | • | + | * | 1 | t | 1 | 4 | ŧ | ~ |
|--|-------------|----------|----------|-------------|------------|-----------|--------|--------|--------|--------|-------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Detector Phase | 5 | 2 | 2 | 1 | 6 | 6 | 7 | 4 | 1 | 3 | 8 | 8 |
| Switch Phase | | | | | | | | | | | | |
| Minimum Initial (s) | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 10.0 | 5.0 | 10.0 | 5.0 | 5.0 | 10.0 | 10.0 |
| Minimum Split (s) | 9.0 | 52.9 | 52.9 | 9.0 | 52.9 | 52.9 | 9.0 | 56.0 | 9.0 | 9.0 | 56.0 | 56.0 |
| Total Split (s) | 12.0 | 73.0 | 73.0 | 17.0 | 78.0 | 78.0 | 32.0 | 54.0 | 17.0 | 16.0 | 38.0 | 38.0 |
| Total Split (%) | 7.5% | 45.6% | 45.6% | 10.6% | 48.8% | 48.8% | 20.0% | 33.8% | 10.6% | 10.0% | 23.8% | 23.8% |
| Maximum Green (s) | 8.0 | 66.1 | 66.1 | 13.0 | 71.1 | 71.1 | 28.0 | 47.0 | 13.0 | 12.0 | 31.0 | 31.0 |
| Yellow Time (s) | 3.0 | 4.2 | 4.2 | 3.0 | 4.2 | 4.2 | 3.0 | 3.7 | 3.0 | 3.0 | 3.7 | 3.7 |
| All-Red Time (s) | 1.0 | 2.7 | 2.7 | 1.0 | 2.7 | 2.7 | 1.0 | 3.3 | 1.0 | 1.0 | 3.3 | 3.3 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 4.0 | 4.0 | 7.0 | 7.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag | Lead | Lag | Lead | Lead | Lag | Lag |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes | Yes |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None | None | None |
| Walk Time (s) | | 14.0 | 14.0 | | 14.0 | 14.0 | | 15.0 | | | 15.0 | 15.0 |
| Flash Dont Walk (s) | | 32.0 | 32.0 | | 32.0 | 32.0 | | 34.0 | | | 34.0 | 34.0 |
| Pedestrian Calls (#/hr) | | 0 | 0 | | 0 | 0 | | 0 | | | 0 | 0 |
| Act Effct Green (s) | 77.0 | 66.1 | 66.1 | 86.0 | 71.1 | 71.1 | 66.0 | 47.0 | 67.0 | 46.0 | 31.0 | 31.0 |
| Actuated g/C Ratio | 0.48 | 0.41 | 0.41 | 0.54 | 0.44 | 0.44 | 0.41 | 0.29 | 0.42 | 0.29 | 0.19 | 0.19 |
| v/c Ratio | 1.60 | 1.03 | 0.35 | 0.74 | 1.49 | 0.39 | 1.23 | 1.11 | 1.03 | 1.42 | 0.77 | 0.58 |
| Control Delay | 329.7 | 72.8 | 13.5 | 58.2 | 257.3 | 18.7 | 160.3 | 112.9 | 85.1 | 250.5 | 70.0 | 29.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 329.7 | 72.8 | 13.5 | 58.2 | 257.3 | 18.7 | 160.3 | 112.9 | 85.1 | 250.5 | 70.0 | 29.6 |
| LOS | F | E | В | E | F | В | F | F | F | F | E | С |
| Approach Delay | | 87.9 | | | 231.8 | | | 114.1 | | | 104.6 | |
| Approach LOS | | F | | | F | | | F | | | F | |
| Queue Length 50th (m) | ~73.5 | ~246.4 | 18.2 | 25.3 | ~498.4 | 32.8 | ~138.8 | ~198.9 | ~200.3 | ~80.6 | 77.7 | 24.5 |
| Queue Length 95th (m) | #123.3 | #271.1 | 38.2 | #54.7 | #514.2 | 54.9 | #202.7 | #238.2 | #271.0 | #132.8 | 97.4 | 51.3 |
| Internal Link Dist (m) | | 269.2 | | | 502.7 | | | 164.2 | | | 122.7 | |
| Turn Bay Length (m) | 220.0 | | 80.0 | 230.0 | | 80.0 | 130.0 | | 130.0 | 130.0 | | 70.0 |
| Base Capacity (vph) | 132 | 2100 | 720 | 186 | 2259 | 746 | 367 | 1028 | 650 | 171 | 678 | 396 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 1.60 | 1.03 | 0.35 | 0.74 | 1.49 | 0.39 | 1.23 | 1.11 | 1.03 | 1.42 | 0.77 | 0.58 |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |
| Cycle Length: 160 | | | | | | | | | | | | |
| Actuated Cycle Length: 16 | 0 | | | | | | | | | | | |
| Offset: 0 (0%), Referenced | to phase 2 | :EBTL an | d 6:WBTL | ., Start of | Green | | | | | | | |
| Natural Cycle: 160 | | | | | | | | | | | | |
| Control Type: Actuated-Co | ordinated | | | | | | | | | | | |
| Maximum v/c Ratio: 1.60 | | | | | | | | | | | | |
| Intersection Signal Delay: | 152.3 | | | l | ntersectio | n LOS: F | | | | | | |
| Intersection Capacity Utiliz Analysis Period (min) 15 | ation 130.2 | % | | ļ | CU Level | of Servic | e H | | | | | |

Volume exceeds capacity, queue is theoretically infinite.
 Queue shown is maximum after two cycles.

95th percentile volume exceeds capacity, queue may be longer.Queue shown is maximum after two cycles.

Splits and Phases: 1: Ninth Line & Dundas Street East



HCM Signalized Intersection Capacity Analysis 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | 4 | + | • | 1 | t | 1 | 4 | ŧ | ~ |
|--------------------------------|--------------|------|--------|-------|-----------|------------|---------|----------|-------|-------|----------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ٦ | *** | 1 | ۲ | *** | 1 | ٦ | ^ | 1 | ۲ | ^ | 1 |
| Traffic Volume (vph) | 194 | 1986 | 229 | 127 | 3102 | 269 | 416 | 1046 | 617 | 223 | 483 | 211 |
| Future Volume (vph) | 194 | 1986 | 229 | 127 | 3102 | 269 | 416 | 1046 | 617 | 223 | 483 | 211 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width | 3.3 | 3.6 | 3.3 | 3.3 | 3.6 | 3.3 | 3.0 | 3.5 | 3.0 | 3.0 | 3.5 | 3.0 |
| Total Lost time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 4.0 | 4.0 | 7.0 | 7.0 |
| Lane Util. Factor | 1.00 | 0.91 | 1.00 | 1.00 | 0.91 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1711 | 5085 | 1531 | 1711 | 5085 | 1531 | 1652 | 3500 | 1478 | 1652 | 3500 | 1478 |
| Flt Permitted | 0.06 | 1.00 | 1.00 | 0.06 | 1.00 | 1.00 | 0.19 | 1.00 | 1.00 | 0.13 | 1.00 | 1.00 |
| Satd. Flow (perm) | 109 | 5085 | 1531 | 103 | 5085 | 1531 | 332 | 3500 | 1478 | 224 | 3500 | 1478 |
| Peak-hour factor, PHF | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 211 | 2159 | 249 | 138 | 3372 | 292 | 452 | 1137 | 671 | 242 | 525 | 229 |
| RTOR Reduction (vph) | 0 | 0 | 88 | 0 | 0 | 66 | 0 | 0 | 34 | 0 | 0 | 110 |
| Lane Group Flow (vph) | 211 | 2159 | 161 | 138 | 3372 | 226 | 452 | 1137 | 637 | 242 | 525 | 119 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | pm+pt | NA | pm+ov | pm+pt | NA | Perm |
| Protected Phases | 5 | 2 | | 1 | 6 | | 7 | 4 | 1 | 3 | 8 | |
| Permitted Phases | 2 | | 2 | 6 | | 6 | 4 | | 4 | 8 | | 8 |
| Actuated Green, G (s) | 74.1 | 66.1 | 66.1 | 83.1 | 71.1 | 71.1 | 63.0 | 47.0 | 60.0 | 43.0 | 31.0 | 31.0 |
| Effective Green, g (s) | 74.1 | 66.1 | 66.1 | 83.1 | 71.1 | 71.1 | 63.0 | 47.0 | 60.0 | 43.0 | 31.0 | 31.0 |
| Actuated g/C Ratio | 0.46 | 0.41 | 0.41 | 0.52 | 0.44 | 0.44 | 0.39 | 0.29 | 0.38 | 0.27 | 0.19 | 0.19 |
| Clearance Time (s) | 4.0 | 6.9 | 6.9 | 4.0 | 6.9 | 6.9 | 4.0 | 7.0 | 4.0 | 4.0 | 7.0 | 7.0 |
| Vehicle Extension (s) | 3.5 | 5.5 | 5.5 | 3.5 | 5.5 | 5.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Lane Grp Cap (vph) | 130 | 2100 | 632 | 184 | 2259 | 680 | 361 | 1028 | 554 | 167 | 678 | 286 |
| v/s Ratio Prot | c0.08 | 0.42 | | 0.06 | 0.66 | | c0.22 | 0.32 | c0.09 | c0.11 | 0.15 | |
| v/s Ratio Perm | c0.67 | | 0.11 | 0.33 | | 0.15 | 0.27 | | 0.34 | c0.28 | | 0.08 |
| v/c Ratio | 1.62 | 1.03 | 0.25 | 0.75 | 1.49 | 0.33 | 1.25 | 1.11 | 1.15 | 1.45 | 0.77 | 0.42 |
| Uniform Delay, d1 | 44.2 | 47.0 | 30.8 | 44.3 | 44.5 | 29.0 | 42.2 | 56.5 | 50.0 | 52.0 | 61.2 | 56.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 312.7 | 27.2 | 1.0 | 16.2 | 224.1 | 1.3 | 134.3 | 61.8 | 87.0 | 232.3 | 5.7 | 1.2 |
| Delay (s) | 356.9 | 74.2 | 31.8 | 60.4 | 268.6 | 30.3 | 176.5 | 118.3 | 137.0 | 284.4 | 66.9 | 57.7 |
| Level of Service | F | E | С | E | F | С | F | F | F | F | E | E |
| Approach Delay (s) | | 92.9 | | | 242.7 | | | 135.5 | | | 117.6 | |
| Approach LOS | | F | | | F | | | F | | | F | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 2000 Control Delay | | | 164.2 | Н | CM 2000 | Level of | Service | | F | | | |
| HCM 2000 Volume to Capac | ity ratio | | 1.48 | | | | | | | | | |
| Actuated Cycle Length (s) | th (s) 160.0 | | | | um of los | t time (s) | | | 21.9 | | | |
| Intersection Capacity Utilizat | ion | | 130.2% | IC | CU Level | of Service | e | | Н | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |
| c Critical Lane Group | | | | | | | | | | | | |

HCM 6th Signalized Intersection Summary 1: Ninth Line & Dundas Street East

| | ٠ | - | 7 | • | ← | * | 1 | t | 1 | 4 | ŧ | ~ |
|------------------------------|-------|-------|-------|------|----------|-------|-------|------------|-------|-------|------------|----------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | *** | 1 | ٢ | ^ | 1 | 7 | † † | 1 | ٢ | † † | 1 |
| Traffic Volume (veh/h) | 194 | 1986 | 229 | 127 | 3102 | 269 | 416 | 1046 | 617 | 223 | 483 | 211 |
| Future Volume (veh/h) | 194 | 1986 | 229 | 127 | 3102 | 269 | 416 | 1046 | 617 | 223 | 483 | 211 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Work Zone On Approach | | No | | | No | | | No | | | No | |
| Adj Sat Flow, veh/h/ln | 1870 | 1870 | 1870 | 1870 | 1870 | 1870 | 1796 | 1870 | 1796 | 1796 | 1870 | 1796 |
| Adj Flow Rate, veh/h | 211 | 2159 | 249 | 138 | 3372 | 292 | 452 | 1137 | 671 | 242 | 525 | 229 |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Percent Heavy Veh, % | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Cap, veh/h | 134 | 2198 | 682 | 160 | 2269 | 704 | 381 | 1044 | 544 | 173 | 689 | 295 |
| Arrive On Green | 0.05 | 0.43 | 0.43 | 0.06 | 0.44 | 0.44 | 0.17 | 0.29 | 0.29 | 0.08 | 0.19 | 0.19 |
| Sat Flow, veh/h | 1781 | 5106 | 1585 | 1781 | 5106 | 1585 | 1710 | 3554 | 1522 | 1710 | 3554 | 1522 |
| Grp Volume(v), veh/h | 211 | 2159 | 249 | 138 | 3372 | 292 | 452 | 1137 | 671 | 242 | 525 | 229 |
| Grp Sat Flow(s),veh/h/ln | 1781 | 1702 | 1585 | 1781 | 1702 | 1585 | 1710 | 1777 | 1522 | 1710 | 1777 | 1522 |
| Q Serve(g_s), s | 8.0 | 66.7 | 17.0 | 8.1 | 71.1 | 20.1 | 28.0 | 47.0 | 47.0 | 12.0 | 22.4 | 22.9 |
| Cycle Q Clear(g_c), s | 8.0 | 66.7 | 17.0 | 8.1 | 71.1 | 20.1 | 28.0 | 47.0 | 47.0 | 12.0 | 22.4 | 22.9 |
| Prop In Lane | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 | 1.00 | | 1.00 |
| Lane Grp Cap(c), veh/h | 134 | 2198 | 682 | 160 | 2269 | 704 | 381 | 1044 | 544 | 173 | 689 | 295 |
| V/C Ratio(X) | 1.57 | 0.98 | 0.36 | 0.86 | 1.49 | 0.41 | 1.19 | 1.09 | 1.23 | 1.40 | 0.76 | 0.78 |
| Avail Cap(c_a), veh/h | 134 | 2198 | 682 | 191 | 2269 | 704 | 381 | 1044 | 544 | 173 | 689 | 295 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay (d), s/veh | 46.8 | 44.9 | 30.8 | 45.6 | 44.5 | 30.3 | 42.7 | 56.5 | 51.4 | 52.6 | 61.0 | 61.2 |
| Incr Delay (d2), s/veh | 290.9 | 15.4 | 1.5 | 28.8 | 221.1 | 1.8 | 107.3 | 55.4 | 120.2 | 209.7 | 5.2 | 12.6 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| %ile BackOfQ(50%),veh/ln | 16.6 | 32.8 | 7.3 | 4.4 | 78.0 | 8.6 | 24.0 | 30.1 | 41.0 | 11.8 | 11.0 | 10.3 |
| Unsig. Movement Delay, s/veh | l | | | | | | | | | | | |
| LnGrp Delay(d),s/veh | 337.7 | 60.4 | 32.3 | 74.4 | 265.6 | 32.1 | 150.0 | 111.9 | 171.6 | 262.3 | 66.2 | 73.9 |
| LnGrp LOS | F | E | С | E | F | С | F | F | F | F | E | <u> </u> |
| Approach Vol, veh/h | | 2619 | | | 3802 | | | 2260 | | | 996 | |
| Approach Delay, s/veh | | 80.0 | | | 240.7 | | | 137.2 | | | 115.6 | |
| Approach LOS | | F | | | F | | | F | | | F | |
| Timer - Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | | | | |
| Phs Duration (G+Y+Rc), s | 14.2 | 75.8 | 16.0 | 54.0 | 12.0 | 78.0 | 32.0 | 38.0 | | | | |
| Change Period (Y+Rc), s | 4.0 | * 6.9 | 4.0 | 7.0 | 4.0 | * 6.9 | 4.0 | 7.0 | | | | |
| Max Green Setting (Gmax), s | 13.0 | * 66 | 12.0 | 47.0 | 8.0 | * 71 | 28.0 | 31.0 | | | | |
| Max Q Clear Time (q c+l1), s | 10.1 | 69.7 | 14.0 | 49.0 | 10.0 | 73.1 | 30.0 | 24.9 | | | | |
| Green Ext Time (p_c), s | 0.1 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 2.8 | | | | |
| Intersection Summary | | | | | | | | | | | | |
| HCM 6th Ctrl Delav | | | 160.2 | | | | | | | | | |
| HCM 6th LOS | | | F | | | | | | | | | |

Notes

User approved pedestrian interval to be less than phase max green.

* HCM 6th computational engine requires equal clearance times for the phases crossing the barrier.

Lanes, Volumes, Timings 2: Ninth Line & Glen Oaks Access

| | ٠ | - | \mathbf{r} | * | ← | • | 1 | t | 1 | 4 | ŧ | ~ |
|----------------------------|-------|-------|--------------|------|-------|-------|-------|-------------|-------|-------|-------------|-------|
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | \$ | | | \$ | | ٢ | † 1> | | ٦ | † 1> | |
| Traffic Volume (vph) | 11 | 0 | 38 | 47 | 0 | 6 | 26 | 1491 | 36 | 4 | 906 | 6 |
| Future Volume (vph) | 11 | 0 | 38 | 47 | 0 | 6 | 26 | 1491 | 36 | 4 | 906 | 6 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Lane Width (m) | 3.2 | 3.5 | 3.2 | 3.5 | 3.5 | 3.5 | 3.3 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| Storage Length (m) | 0.0 | | 0.0 | 0.0 | | 0.0 | 30.0 | | 0.0 | 30.0 | | 0.0 |
| Storage Lanes | 0 | | 0 | 0 | | 0 | 1 | | 0 | 1 | | 0 |
| Taper Length (m) | 15.0 | | | 15.0 | | | 15.0 | | | 15.0 | | |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.95 | 0.95 | 1.00 | 0.95 | 0.95 |
| Frt | | 0.896 | | | 0.984 | | | 0.996 | | | 0.999 | |
| Flt Protected | | 0.989 | | | 0.958 | | 0.950 | | | 0.950 | | |
| Satd. Flow (prot) | 0 | 1632 | 0 | 0 | 1736 | 0 | 1711 | 3486 | 0 | 1750 | 3496 | 0 |
| Flt Permitted | | 0.989 | | | 0.958 | | 0.950 | | | 0.950 | | |
| Satd. Flow (perm) | 0 | 1632 | 0 | 0 | 1736 | 0 | 1711 | 3486 | 0 | 1750 | 3496 | 0 |
| Link Speed (k/h) | | 60 | | | 60 | | | 60 | | | 60 | |
| Link Distance (m) | | 47.4 | | | 62.7 | | | 146.7 | | | 158.7 | |
| Travel Time (s) | | 2.8 | | | 3.8 | | | 8.8 | | | 9.5 | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Adj. Flow (vph) | 12 | 0 | 41 | 51 | 0 | 7 | 28 | 1621 | 39 | 4 | 985 | 7 |
| Shared Lane Traffic (%) | | | | | | | | | | | | |
| Lane Group Flow (vph) | 0 | 53 | 0 | 0 | 58 | 0 | 28 | 1660 | 0 | 4 | 992 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(m) | | 0.0 | | | 0.0 | | | 3.5 | | | 3.5 | |
| Link Offset(m) | | 0.0 | | | 0.0 | | | 0.0 | | | 0.0 | |
| Crosswalk Width(m) | | 3.0 | | | 3.0 | | | 3.0 | | | 3.0 | |
| Two way Left Turn Lane | | | | | | | | Yes | | | Yes | |
| Headway Factor | 1.06 | 1.01 | 1.06 | 1.01 | 1.01 | 1.01 | 1.04 | 1.01 | 1.01 | 1.01 | 1.01 | 1.01 |
| Turning Speed (k/h) | 25 | | 15 | 25 | | 15 | 25 | | 15 | 25 | | 15 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Intersection Summary | | | | | | | | | | | | |
| Area Type: | Other | | | | | | | | | | | |

Control Type: Unsignalized Intersection Capacity Utilization 58.3% Analysis Period (min) 15

ICU Level of Service B

HCM Unsignalized Intersection Capacity Analysis 2: Ninth Line & Glen Oaks Access

| | ٦ | → | 7 | 4 | + | • | 1 | Ť | 1 | 4 | ŧ | ~ |
|-------------------------------|-------|----------|-------|------|------------|------------|------|------------|------|------|------------|------|
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | | 4 | | | 4 | | ٦ | † Ъ | | 7 | † Ъ | |
| Traffic Volume (veh/h) | 11 | 0 | 38 | 47 | 0 | 6 | 26 | 1491 | 36 | 4 | 906 | 6 |
| Future Volume (Veh/h) | 11 | 0 | 38 | 47 | 0 | 6 | 26 | 1491 | 36 | 4 | 906 | 6 |
| Sign Control | | Stop | | | Stop | | | Free | | | Free | |
| Grade | | 0% | | | 0% | | | 0% | | | 0% | |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Hourly flow rate (vph) | 12 | 0 | 41 | 51 | 0 | 7 | 28 | 1621 | 39 | 4 | 985 | 7 |
| Pedestrians | | | | | | | | | | | | |
| Lane Width (m) | | | | | | | | | | | | |
| Walking Speed (m/s) | | | | | | | | | | | | |
| Percent Blockage | | | | | | | | | | | | |
| Right turn flare (veh) | | | | | | | | | | | | |
| Median type | | | | | | | | TWLTL | | | TWLTL | |
| Median storage veh) | | | | | | | | 2 | | | 2 | |
| Upstream signal (m) | | | | | | | | 147 | | | | |
| pX, platoon unblocked | 0.71 | 0.71 | | 0.71 | 0.71 | 0.71 | | | | 0.71 | | |
| vC, conflicting volume | 1870 | 2712 | 496 | 2238 | 2696 | 830 | 992 | | | 1660 | | |
| vC1, stage 1 conf vol | 996 | 996 | | 1696 | 1696 | | | | | | | |
| vC2, stage 2 conf vol | 874 | 1716 | | 542 | 1000 | | | | | | | |
| vCu, unblocked vol | 1411 | 2596 | 496 | 1929 | 2573 | 0 | 992 | | | 1116 | | |
| tC, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 | | | 4.1 | | |
| tC, 2 stage (s) | 6.5 | 5.5 | | 6.5 | 5.5 | | | | | | | |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 | | | 2.2 | | |
| p0 queue free % | 95 | 100 | 92 | 61 | 100 | 99 | 96 | | | 99 | | |
| cM capacity (veh/h) | 240 | 145 | 519 | 130 | 147 | 771 | 693 | | | 442 | | |
| Direction, Lane # | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB 2 | SB 3 | | | | |
| Volume Total | 53 | 58 | 28 | 1081 | 579 | 4 | 657 | 335 | | | | |
| Volume Left | 12 | 51 | 28 | 0 | 0 | 4 | 0 | 0 | | | | |
| Volume Right | 41 | 7 | 0 | 0 | 39 | 0 | 0 | 7 | | | | |
| cSH | 411 | 145 | 693 | 1700 | 1700 | 442 | 1700 | 1700 | | | | |
| Volume to Capacity | 0.13 | 0.40 | 0.04 | 0.64 | 0.34 | 0.01 | 0.39 | 0.20 | | | | |
| Queue Length 95th (m) | 3.1 | 12.1 | 0.9 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 | | | | |
| Control Delay (s) | 15.0 | 45.6 | 10.4 | 0.0 | 0.0 | 13.2 | 0.0 | 0.0 | | | | |
| Lane LOS | С | E | В | | | В | | | | | | |
| Approach Delay (s) | 15.0 | 45.6 | 0.2 | | | 0.1 | | | | | | |
| Approach LOS | С | E | | | | | | | | | | |
| Intersection Summary | | | | | | | | | | | | |
| Average Delay | | | 1.4 | | | | | | | | | |
| Intersection Capacity Utiliza | ition | | 58.3% | IC | CU Level o | of Service | | | В | | | |
| Analysis Period (min) | | | 15 | | | | | | | | | |



Vehicle Turning Templates











Appendix U

TAC Section 8.8 Figure 8.8.2 for Minimum Corner Clearance Dimensions





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Figure 8.8.2: Suggested Minimum Corner Clearances to Accesses or Public Lanes at Major Intersections

Inadequate corner clearance between accesses and signalized intersections along a major road, such as a major arterial, can create serious operational problems including: