

# FUNCTIONAL SERVICING AND STORMWATER MANAGEMENT REPORT

# 1315 Silver Spear Road

City of Mississauga

Prepared for

**Starlight Group Property Holdings Inc.** 

Project #: 23-314W

1<sup>st</sup> Submission - November 2023



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#### 1. INTRODUCTION

Urbantech has been retained as consulting engineers by Starlight Group Property Holdings Inc. to complete a Functional Servicing and Stormwater Management Report in support of Site Plan Approval for the 0.85 ha development located at 1315 Sliver Spear Road in the City of Mississauga.

The site is bounded:

- To the north by Burnhamthorpe Road East
- To the south by Silver Spear Road
- To the west by existing residential buildings
- To the east by the Burnhamthorpe Public Library

The legal description of the site is Block A, Registered Plan 750, City of Mississauga, as shown on Lloyd & Purcell Ltd. Plan of Survey, dated October 24, 2017.

The site is currently occupied by existing 8-storey residential apartment building (which is to remain) with surface parking. The proposed development consists of 9-storey building, 3 levels of underground parking and some alterations to the surface parking.

The subject development lies outside of the limits of a Credit Valley Conservation Authority (CVC) regulated watershed. The site falls within the City of Mississauga Ward 3 area.

### 1.1 Study Purpose

The objective of this study is to outline the servicing requirements of the subject lands at a functional design level. This study will:

- 1. Recommend site grading, water supply and wastewater servicing strategies for the site.
- 2. Demonstrate compliance with City, Conservation and MECP design criteria for municipal services and stormwater management (SWM) measures.

The functional servicing design has been prepared in accordance with design criteria and requirements of the City of Mississauga, Region of Peel and Credit Valley Conservation Authority. The information in this report is intended to assist the regulatory agencies in their review of the planning applications for the proposed development.



#### 2. DEVELOPMENT CONCEPT

Refer to the development concept plan prepared by John D. Rogers and Associates Inc, dated November 7, 2023. The proposed development plan consists of:

- 1. 9-storey building with 272 units, including 25 accessible units.
- 2. 3 levels of underground parking.
- 3. 0.20 ha of amenity space.
- 4. 0.59 ha of landscape area.

The existing development consists of:

- 1. 8-storey building with 93 units.
- 2. 0.46 ha of landscape area.
- 3. Surface parking area.

The proposed development will connect to Burnhamthorpe Road East on North via private driveway and there is an existing connection to the Silver Spear Road on South via private driveway.

### 2.1 Background Studies

There are no background studies conducted at the moment.



### 3. GRADING DESIGN

## 3.1 Design Standards

The proposed grading design for the site takes into consideration the following requirements and constraints:

- 1. Conforms to the City of Mississauga design criteria.
- 2. Match existing boundary lot and road grading conditions to be compatible with abutting properties.
- 3. Provides overland flow conveyance for major storm conditions.
- 4. Provides appropriate cover for proposed servicing.
- 5. Ensures compatibility of driveway access to surrounding public streets.

#### 3.2 Grading Design

A grading plan for the subject property has been prepared in conjunction with the storm, sanitary, and water servicing system design for the subject development.

Drawings 201 illustrate the proposed grading plan for the site.



#### 4. STORM DRAINAGE AND STORMWATER MANAGEMENT

#### 4.1 Drainage Criteria

The City of Mississauga and Credit Valley Conservation outline the following design criteria for the site as follows:

- 1. Limiting post-development stormwater discharge to pre-development 10-year storm event which is the capacity of the storm sewers.
- 2. Pre-development runoff coefficients are to not exceed 0.5 for a site that is already developed.
- 3. Ensure minimum 80% TSS removal on site for quality control.
- 4. First 5 mm of runoff to be retained on-site.
- 5. Provide safe overland flow conveyance of the 100-year event.

#### 4.2 Storm Sewer Design

Under the current development, an existing 8-storey apartment building and a surface parking drains South to the existing storm sewer located on Silver Spear Road. Under the proposed development, a 9-storey building, and underground parking will be added with some changes to the surface parking spaces, while the existing 8-storey building remains. The drainage from the proposed building and adjacent surface parking area will drain to the proposed SWM Tank located South-West of the site. Refer to the Storm Drainage Plan **Drawing 301**.

Storm sewers within the site will be sized to convey the 10-year storm in accordance with the City of Mississauga standards. The site is full coverage with an underground parking. All surface drainage will be collected by area drains and catchbasins that are connected to the building plumbing system. Routing of the storm sewers within the proposed building will be determined later as the building design is advanced.

Flows from the proposed SWM tank will drain to Proposed MH 2 and eventually connect to the existing 300mm storm sewer on the Silver Spear Road via 300 mm storm sewer connection as shown on **Drawing 301**.

#### 4.3 Quality Control

As identified in section 4.1 above, the proposed 0.55 ha site is required to meet a minimum of 80% TSS removal on site for quality control. To achieve the required TSS removal an Oil Grit Separator (OGS) will be used upstream of the proposed storage tank. **Table 1** below outlines preliminary sizing for the OGS devices. Sizing specifications are to be verified by the manufacturer during detailed design.

**Table 1 OGS Parameters** 

OGS#	Size	Area (ha)	Efficiency (%)
1	EF4	0.55	85

Refer to Appendix B for the Stormceptor Sizing Report.



#### 4.4 Quantity Control

Under current scenario, the total 0.85 ha site drains South, uncontrolled to the existing storm sewer on Silver Spear Road. However, under the proposed scenario, for the 0.55 ha of proposed 9-storey building, underground parking, and alterations to the surface parking, a Visual Otthymo model was created to model the drainage from the site to determine the pre-development 10-year flow and required storage volume to control the 100-year post-development flows. As the site is fully developed under existing conditions, a runoff coefficient of 0.5 was used as prescribed by the City of Mississauga standards. **Table 2** below outlines the pre-development 10-year flow.

A 24-hour Chicago rainfall Distribution was used to simulate the rainfall on the site using the City of Mississauga IDF parameters, originally derived from the Pearson International Airport rainfall data.

Table 2: 10-year Pre-development Target

Scenario	Area (ha)	Runoff Coefficient	10-year Target (m³/s)
Proposed Development	0.55	0.5	0.153

The proposed SWM tank will be located on the South-West corner of the site and discharges flows to the existing storm sewer system on Silver Spear Road, providing water quantity control for the proposed 0.55 ha site. The 0.3 ha of existing 8-storey building will continue to drain South, uncontrolled to the existing storm sewer system on the Silver Spear Road.

**Table 3** summarizes the flow and storage values required for proposed development based on the VO6 calculations.

Table 3: Proposed Development - Flow and Required Storage Volume Results

Outlet	Area (ha)	Runoff Coefficient	Controlled Post Development Flows (VO6 Results) m³/s	Required Volume (VO6 Results) (m³)	Provided Volume (m³)
Tank (NHYD 13)	0.55	0.9	0.143	114	127

Refer to SWM Calculations in **Appendix B** for supporting calculations and **Drawing 301** for Storm Drainage Plan.

#### 4.5 Water Balance/Water Re-use

The City of Mississauga requires retention of the first 5 mm of runoff to promote water balance and erosion control. Based on the proposed site development area of 0.55 ha and 100% imperviousness, approximately 27.5 m³ should be retained on site. As the majority of the site plan is a full coverage building there are limited/nil opportunities for infiltration on site as landscaped areas not above the parking garage are too close to the building to allow infiltration in accordance with the Ontario building code. Reusing the stormwater onsite is permitted where retention via infiltration is not feasible. **Table 4** outlines various measures that could be implemented for the subject development. Details of the design will be provided during site plan approvals.



# **Table 4: Potential 5 mm Retention Options**

LID Measure	Notes
Landscaped Areas	The planting media (landscape above parking garage and planting boxes)
	within the proposed development will retain the first 5 mm of rainwater through
	initial abstraction and provide the opportunity for evapotranspiration.
Green Roofs	The benefits of green roofs could be attenuation of flows, filtration and
	increased water available for evapotranspiration. This would be an additional
	element including the stormwater tank and OGS.
Rainwater Harvesting	Rainwater not captured by the landscaped area or green roofs is collected in
-Irrigation	the sump of the storage tank and used for irrigation for the proposed
	landscaped areas and planters.
Rainwater Harvesting	Water that is not able to be used for irrigation could be used for other
<ul> <li>Mechanical Uses</li> </ul>	mechanical re-use measures.



### 5. WASTEWATER SERVICING

#### 5.1 Design Criteria

Wastewater sewers will be designed in accordance with Region of Peel standards and specifications. The following criteria were used:

- 3 people/unit for large apartments (larger than 750 square feet)
- 1.6 people/unit for small apartments (less than 750 square feet)
- 0.2 L/s/ha for infiltration
- 302.8 L/person/day for domestic sewage flow

#### 5.2 Existing Conditions

The existing sanitary sewer in proximity to the site is as follows:

1. 250 mm diameter sanitary sewer located within Silver Spear Road.

There is an existing sanitary connection made to the 250 mm sanitary sewer on the Silver Spear Road via a 200 mm diameter sanitary sewer, serving the existing the 8-storey apartment building. The location of the existing sewer and sanitary connection is shown on **Drawing 101**.

#### 5.3 Local Wastewater Design

The estimated sanitary flow from the entire site is 8.78 L/s. Refer to Wastewater Demand Calculations in **Appendix C** for calculations and Region of Peel Multi Use Demand Table.

Sanitary servicing within the site will be designed by the project mechanical engineer as the building design advances. Proposed sanitary flows from the proposed development will be conveyed via a new 200 mm sanitary sewer connection to the existing sanitary plug on the site and eventually discharge to the 250 mm sanitary sewer on the Silver Spear Road. Refer to **Drawings 101 and 302** for the anticipated connection location and drainage areas.



#### 6. WATER SERVICING

### 6.1 Design Criteria

The proposed watermain design will comply with the Region of Peel design criteria as follows:

- Residential Consumption = 280 l/c/day, max day = 3
- Residential and Commercial Peak Hour = 3
- Minimum operating pressure = 40 psi
- Maximum operating pressure = 100 psi

#### 6.2 Existing Conditions

The existing water network, which falls under the jurisdiction of the Region of Peel, in the vicinity of the site includes:

1. A 300 mm local watermain on Silver Spear Road.

There is an existing 100 mm and 150 mm watermain connection for domestic and firefighting requirements respectively, to the 300 mm watermain on the Silver Spear Road, serving the existing the 8-storey apartment building. The location of the existing watermain and watermain connections are shown on **Drawing 101**.

#### 6.3 Local Watermains

The proposed development will be serviced by extending a connection from the existing 100 mm domestic and 150 mm fire-fighting watermain plugs on the site, which is serviced by an existing 300 mm watermain on Silver Spear Road as shown on **Drawing 101**. The onsite water supply system will be designed by the project mechanical engineer as the building design advances.

Table 5 below outlines the water demand calculations for the development.

**Table 5: Water Demand** 

Fire Flow (L/s)	Domestic (L/s)		
File Flow (L/S)	Max Daily Demand	Max Peak Hour	
183.3	3.9	5.9	

A hydrant flow test will be undertaken on Silver Spear Road. Results will be provided to the Region of Peel once the test has been conducted.

Water demand, internal servicing and proposed connection points are to be provided to the Region of Peel to identify if there are any water capacity constraints.

Refer to **Appendix D** for water demand calculation results.



### 7. EROSION AND SEDIMENT CONTROL AND CONSTRUCTION DEWATERING

Erosion and sediment controls measures as follows:

- 1. Installing heavy duty silt control fencing along the perimeter of the site at strategic locations.
- 2. Installing a temporary mud mat at the construction site entrance.
- 3. Wrapping the tops of all inlet structures with filter fabric and using install silt sacks.
- Inspecting all sediment and erosion control controls to maintain them in good repair until such time as the Engineer or the City approves their removal.
- 5. Safe discharge of construction water in accordance with City and provincial guidelines.

Refer to Drawing 1001 for site-specific erosion and sediment control measures for the property.



#### 8. CONCLUSIONS

This report has demonstrated that:

- The proposed site will be graded to match to existing elevations at all property lines.
- Building Storm drains will be designed by the project mechanical engineer at the building permit stage.
- Water quality will be provided using an OGS device upstream of the stormwater tank.
- Storm water quantity control for the 0.55 ha of proposed development estimated to be 127 m<sup>3</sup> and will be required to control flows from the post development 100-year storm to the predevelopment 10-year as per the City of Mississauga.
- The 0.3 ha of the existing building will continue to drain uncontrolled to the existing storm sewers on Silver Spear Road.
- Proposed SWM Tank will be located on the South-West corner of the site.
- The site will utilize an existing storm sewer connection to the existing MH2.
- Water balance objectives will be met by retaining the first 5 mm of rain events onsite within the proposed landscaped areas as well as in the storage tank. Retained water from the storage tank will be re-used.
- Wastewater servicing to the site is provided by an existing 200 mm diameter sanitary connection to the sewer on Silver Spear Road. Wastewater servicing for the proposed development will be done by plugging to the existing sanitary connection for current development.
- Water servicing to the site is provided by existing 100 mm domestic and 150 mm fire-fighting watermain connections to the watermain on Silver Spear Road. Water servicing for the proposed development will be done by extending the existing watermain connections from current development.
- Erosion and sediment control and groundwater control measures will be implemented during construction in accordance with City and Provincial requirements.

Report Prepared by:



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Keval Vejani, M.Eng. Water Resources Designer



# **APPENDIX A**Drawings and Figures

Drawing 101 Servicing Plan

Drawing 102 Removals Plan

Drawing 201 Grading Plan

Drawing 301 Storm Drainage Plan

Drawing 302 Sanitary Drainage Plan

Drawing 701 Details

Drawing 1001 Erosion and Sediment Control Plan

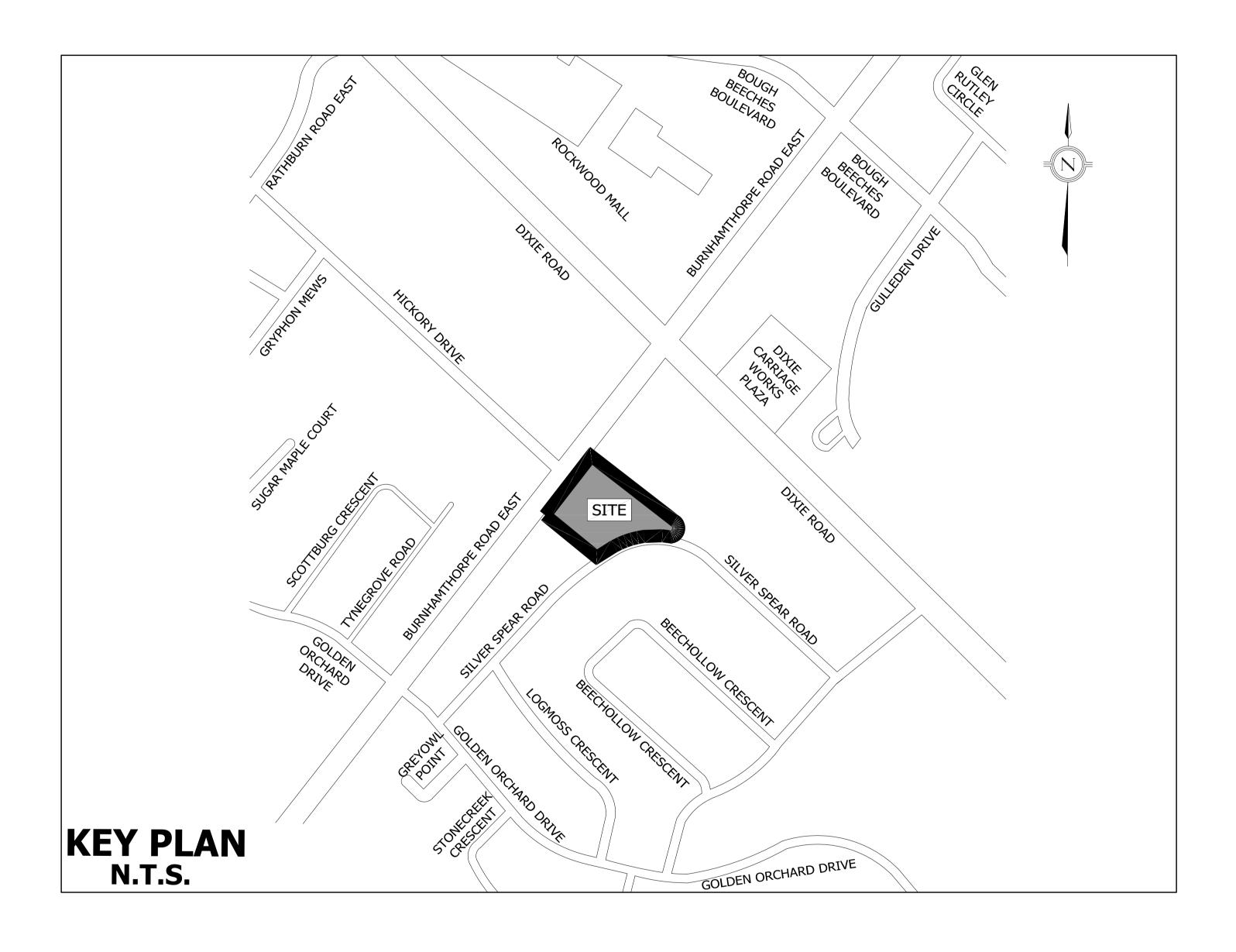
Drawing 1002 Erosion and Sediment Control Plan Details

# CITY OF MISSISSAUGA 1315 SILVER SPEAR ROAD

CITY FILE No. SP.XX-XX

REGION FILE No.: C-XXXXXX

# FIRST SUBMISSION - NOV. 13, 2023



# LIST OF DRAWINGS

**NOTES** 

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# GENERAL PLANS

101 - SERVICING PLAN 102 - REMOVAL PLAN

# **GRADING PLANS**

201 - GRADING PLAN

# DRAINAGE PLANS

301 - STORM DRAINAGE PLAN 302 - SANITARY DRAINAGE PLAN

# STANDARD DETAILS

701 - DETAILS

# EROSION AND SEDIMENT CONTROL PLANS

1001 - EROSION & SEDIMENT CONTROL PLAN 1002 - EROSION & SEDIMENT CONTROL DETAILS

# **LEGEND:**



LIMIT OF PROPERTY



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# **GENERAL NOTES**

# **STORM SEWERS:**

- ALL CONCRETE PIPE SMALLER THAN 450mm DIAMETER SHALL BE C-14, CLASS 2, CONCRETE PIPE 450mm DIAMETER AND LARGER SHALL BE C-76, CLASS 65-D, UNLESS OTHERWISE NOTED.
- 2. ALL POLYVINYL CHLORIDE (PVC.) PIPE SHALL MEET THE C.S.A. REQUIREMENTS AS NOTED WITHIN OPSS. 1841. THE PIPE MATERIAL SHALL HAVE A CELL CLASSIFICATION OF 12454-B OR 12454-C OR ASTM. STD. D-3034 & OPSS. 1841.
- 3. ALL CONCRETE SEWER PIPES SHALL HAVE RUBBER GASKET JOINTS.
- 4. CLASS "B" BEDDING IS TO BE USED AS PER CITY STANDARD 2112.08 SEWER BEDDING AND COVER MATERIAL SHALL CONFIRM WITH CITY STANDARDS 2112.09 AND 2112.10. IF WATER IS PRESENT IN THE TRENCH EXCAVATION THEN 19mm. CLEAR STONE IS TO BE USED FOR BEDDING IN ACCORDANCE WITH CITY STANDARD 2112.11 AND 2112.14 RESPECTIVELY. WHERE WET OR SOFT TRENCH SUBGRADE CONDITIONS ARE ENCOUNTERED, FURTHER ON-SITE GEOTECHNICAL ASSESSMENT MAY BE REQUIRED TO DETERMINE THE APPROPRIATE BEDDING IN ORDER TO STABILIZE THE SUBGRADE FOR SEWER CONSTRUCTION.
- 5. MANHOLE STEPS SHALL BE AS PER OPSD. 405.010.
- 6. MANHOLE COVERS AND FRAMES SHALL BE AS PER OPSD. 401.010.
- 7. SINGLE CATCHBASINS WITHIN ROAD ALLOWANCES SHALL BE AS PER OPSD. 705.010, WITH A 250mm DIAMETER LEAD, DOUBLE CATCHBASINS WITHIN ROAD ALLOWANCES SHALL BE AS PER OPSD. 705.020, WITH A 300mm DIAMETER LEAD.
- 8. ALL CATCHBASIN FRAME AND GRATES SHALL BE AS PER OPSD. 400.020.
- 9. THE TRENCH WIDTH AT THE TOP OF PIPE SHALL BE AS PER STD. 2112.08. IF THE MAXIMUM TRENCH WIDTH IS EXCEEDED, THE CONTRACTOR SHALL BE RESPONSIBLE FOR SUPPLYING EXTRA BEDDING AND/OR STRONGER PIPE AS REQUIRED.
- 10. ALL STORM SEWER AND APPURTENANCES SHALL BE CONSTRUCTED IN ACCORDANCE WITH CURRENT CITY OF MISSISSAUGA STANDARDS AND SPECIFICATIONS.
- 11. STORM SERVICE CONNECTION IS TO BE ON THE LEFT OF SANITARY SERVICE FACING THE HOUSE. (EXCEPT
- 12. SERVICE CONNECTION AT THE STREET LINE IS TO BE HIGHER THAN THE SANITARY CONNECTION AT THAT
- 13. ALL CATCHBASINS ARE TO BE PLACED ON GRANULAR BEDDING (MINIMUM DEPTH 150mm).
- 14. TRENCH BACKFILLING ON PROPOSED ROADS SHALL WITH CITY'S ENGINEERING POLICY STATEMENT AS PROVIDED IN THE "DEVELOPMENT REQUIREMENTS MANUAL" (SECTION 4.02.06-TRENCH BACKFILLING ON ROADS). TRENCH BACKFILL SHALL BE COMPACTED TO A MINIMUM OF 95% S.P.D. WITHIN 2.0% OF THE OPTIMUM CONTENT.
- 15. SAND BACKFILLING IS REQUIRED ADJACENT TO MANHOLES, CATCHBASINS AND SERVICE CROSSING.

# **GENERAL:**

- 1. ANY RELOCATION OF EXISTING UTILITIES REQUIRED BY THE DEVELOPMENT OF THE SUBJECT LANDS, IS TO BE UNDERTAKEN AT DEVELOPER'S EXPENSE.
- 2. ALL UNDERGROUND SERVICE CONNECTIONS WITHIN PAVED PORTION OF ANY EXISTING ROAD TO BE BACKFILLED WITH UNSHRINKABLE FILL TO THE LATEST CITY OF MISSISSAUGA OR REGION OF PEEL SPECIFICATIONS.
- 3. SNOW FENCE AND SEDIMENT TRAP CONTROL FENCE ARE TO BE INSTALLED PRIOR TO THE COMMENCEMENT OF ANY SITE CONSTRUCTION AND SHALL REMAIN IN PLACE AND IN GOOD REPAIR THROUGHOUT THE CONSTRUCTION AND GRADING PHASES.
- PRIOR TO THE START OF CONSTRUCTION, SNOW FENCING IS TO BE ERECTED ALONG THE PROPERTY BOUNDARIES ADJACENT TO ALL EXISTING RESIDENTIAL LOTS, PARKS AND ALL EXISTING SCHOOL
- 5. THE LOCATION AND ELEVATION OF ALL EXISTING SERVICES AND UTILITIES ARE TO BE VERIFIED IN THE FIELD BY THE CONTRACTOR. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE RESTORATION TO THE REPAIR OF EXISTING UTILITIES DISTURBED DURING CONSTRUCTION.
- 6. ALL AREAS BEYOND THE PLAN OF SUBDIVISION WHICH ARE DISTURBED DURING CONSTRUCTION SHALL BE RESTORED TO THE SATISFACTION OF THE AUTHORITY HAVING JURISDICTION AT THE CONTRACTOR'S
- 7. ALL CONSTRUCTION SIGNING MUST CONFORM TO THE M.T.O. MANUAL OF "UNIFORM TRAFFIC CONTROL
- 8. ALL WORK SHALL BE COMPLETED IN ACCORDANCE WITH THE "OCCUPATIONAL HEALTH AND SAFETY ACT". THE GENERAL CONTRACTOR SHALL BE DEEMED TO BE THE CONSTRUCTOR AS DEFINED IN THE ACT.

# **BOREHOLES:**

1. BOREHOLE LOGS SHOWN ARE FOR GENERAL INFORMATION ONLY AND LOCATIONS ARE APPROXIMATE. CONTRACTOR IS TO VERIFY AND SATISFY HIMSELF AS TO THE NATURE OF THE SUBSURFACE CONDITIONS.

# **ROADWORKS:**

- 1. ALL FILL WITHIN ROAD ALLOWANCE TO BE COMPACTED TO A MINIMUM OF 95% STANDARD PROCTOR DENSITY. THE SUITABILITY AND COMPACTION OF ALL FILL MATERIALS ARE TO BE CONFIRMED BY A RECOGNIZED SOIL CONSULTANT TO THE CITY ENGINEER PRIOR TO THE INSTALLATION OF ANY ROAD BASE MATERIALS.
- 2. ALL CONNECTIONS WITHIN PAVED PORTION OF ANY EXISTING ROAD TO BE BACKFILLED WITH GRANULAR MATERIAL AND/OR UNSHRINKABLE FILL AS PER THE LATEST OF CITY OF MISSISSAUGA STANDARDS AND SPECIFICATIONS.
- a. TRENCH BACKFILLING ON PROPOSED ROADS SHALL COMPLY WITH THE CITY'S ENGINEERING POLICY STATEMENTS PROVIDED IN THE "DEVELOPMENT REQUIREMENTS MANUAL" (SECTION 4.02.06 - TRENCH
- b. ALL BACKFILL FOR SEWERS, WATERMAINS AND UTILITIES WITHIN ROAD ALLOWANCE SHALL BE COMPACTED TO 95% STANDARD PROCTOR DENSITY WITHIN 2% OF THE OPTIMUM MOISTURE CONTENT.
- c. THE TOP 1000mm OF THE SUB-GRADE IS TO BE COMPACTED TO A MINIMUM 98% STANDARD PROCTOR DENSITY WITHIN 2% OF THE OPTIMUM MOISTURE CONTENT.
- 4. ALL ROADWORKS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE CITY OF MISSISSAUGA STANDARDS AND SPECIFICATIONS.
- 5. ALL INTERSECTING ROADS SHALL BE PROVIDED WITH AN ADDITIONAL 150mm THICKNESS OF OPSS. GRANULAR "B". THIS EXTRA DEPTH SHALL EXTEND FOR A MINIMUM OF 15m BEYOND PROPERTY LINE OF INTERSECTING STREET, AS NOTED.
- 6. SUB-DRAINS ARE TO BE INSTALLED AS PER CITY STANDARD 2220.04 ALONG THE ENTIRE LENGTH OF THE

- 7. PAVEMENT THICKNESS AND COMPOSITION TO BE AS SHOWN ON INDIVIDUAL PLAN AND PROFILE DRAWINGS
- 8. CONCRETE CURB & GUTTER OPSD. 600.070.
- 9. SAND BACKFILL IS TO BE USED ADJACENT TO MANHOLES, CATCHBASINS AND SERVICE CROSSINGS.

# **EXISTING WATERCOURSE/GREENBELT:**

- 1. PRIOR TO COMMENCEMENT OF ANY GRADING OR CONSTRUCTION, TEMPORARY SNOW FENCE AND SILT FENCE TO BE ERECTED ALONG ALL LOTS AND BLOCKS ADJACENT TO THE EXISTING WATERCOURSE/GREENBELT, PARKS AND MAINTAINED UNTIL COMPLETION OF CONSTRUCTION.
- 2. NO STOCKPILES OF FILL MATERIAL ARE TO BE PLACED WITHIN 10.0m OF THE EXISTING WATERCOURSE BLOCK.

# **TOPSOIL STOCKPILE PROTECTION:**

ALL TOPSOIL STOCKPILE CONTAINING MORE THAN 100m3 OF MATERIAL SHALL BE LOCATED A MINIMUM OF 10m AWAY FROM A ROADWAY, DRAINAGE CHANNEL OR AN OCCUPIED RESIDENTIAL LOT. THE MAXIMUM SIDE SLOPES FOR TOPSOIL STOCKPILES SHALL BE 1.5 HORIZONTAL TO 1.0 VERTICAL.

RUNOFF FROM ALL TOPSOIL STOCKPILES SHALL BE CONTROLLED BY A SEDIMENT CONTROL FENCE OR OTHER APPROVED DEVICES. IF REMAINING FOR MORE THAN 30 DAYS, TOPSOIL STOCKPILES SHALL BE STABILIZED BY VEGETATIVE COVER, OR OTHER MEANS.

# **REGION OF PEEL**

# **GENERAL NOTES:**

- 1. THE APPLICANT, APPLICANT'S REPRESENTATIVE, CONSULTANT, CONTRACTOR AND SUB CONTRACTORS ARE RESPONSIBLE TO ENSURE THAT THEIR DESIGN MATERIALS AND CONSTRUCTION PRACTICES CONFORM TO THE LATEST REGION OF PEEL'S WEBSITE (www.peelregion.ca/pw/standards). IN THE ABSENCE OF REGION SPECIFICATIONS, THE ONTARIO PROVINCIAL STANDARDS SPECIFICATIONS (OPSS) SHALL APPLY.
- ALL WORKS SHALL BE COMPLETED IN ACCORDANCE WITH THE "OCCUPATIONAL HEALTH AND SAFETY ACT". THE GENERAL CONTRACTOR SHALL BE DEEMED TO BE THE CONSTRUCTOR AS DEFINED IN THE ACT.
- THE CONTRACTOR AT THEIR EXPENSE SHALL VERIFY THE LOCATION, DIMENSION AND ELEVATION OF ALL EXISTING SERVICES
- AND UTILITIES IN THE FIELD. PRIOR TO EXCAVATION OR BORING CONTRACTOR AT THEIR EXPENSE SHALL EXPOSE AND VERIFY THE LOCATION AND ELEVATION OF ALL EXISTING UTILITIES AND SERVICES TO BE CROSSED AND MUST NOTIFY THE DESIGN ENGINEER AND THE

AGENCY FIELD INSPECTOR AND/OR PROJECT MANAGER IMMEDIATELY, IN WRITING, OF ANY CONFLICTS OR DISCREPANCIES.

- CONTRACTOR SHALL BE RESPONSIBLE FOR EXPOSING THE EXISTING UTILITIES FAR ENOUGH IN ADVANCE OF CONSTRUCTION TO MAKE NECESSARY DESIGN MODIFICATIONS FOR REVIEW AND APPROVAL, IF REQUIRED, WITHOUT DELAYING THE WORK. THE CONTRACTOR, AT THEIR EXPENSE AND TO THE SATISFACTION OF THE REGION OF PEEL, SHALL BE RESPONSIBLE FOR THE RESTORATION AND THE REPAIR OF THE EXISTING UTILITIES AND ALL AREAS BEYOND THE PLAN OF SUBDIVISION DISTURBED
- DURING CONSTRUCTION. 6. THE SUPPORT OF ALL UTILITIES SHALL BE IN ACCORDANCE WITH THE REQUIREMENTS OF THE AUTHORITY HAVING
- JURISDICTION. ALL BACKFILL FOR SEWERS, WATERMAINS AND UTILITIES ON THE ROAD ALLOWANCE MUST BE MECHANICALLY COMPACTED.
- ALL BOREHOLES SHOWN ON DRAWING ARE FOR INFORMATION ONLY, REFER TO GEOTECHNICAL REPORT.
- 9. ALL DIMENSIONS ARE IN METRES UNLESS OTHERWISE SPECIFIED.

# **WATERMAIN NOTES:**

- THE REGION OF PEEL SHALL CONDUCT THE OPERATION OF EXISTING VALVES AND HYDRANTS IF REQUIRED.
- CONTRACTOR MUST USE BATTER BOARD OR ROD-AND-LEVEL METHOD FOR WATERMAIN INSTALLATION. 3. ALL WATERMAINS SHALL HAVE 1.70m MINIMUM COVER FOR URBAN ROAD DESIGN AND 2.1m MINIMUM COVER FOR RURAL
- 4. ALL WATERMAINS SHALL MAINTAIN A MINIMUM 1.5m CLEARANCE FROM ALL MANHOLES AND CATCH BASINS, WHERE APPLICABLE.
- FOR WATERMAIN CROSSING OVER OR UNDER SEWERS A MINIMUM 0.5m VERTICAL CLEARANCE SHALL BE PROVIDED. 6. FOR WATERMAIN CROSSING A SANITARY SEWER, WATERMAIN JOINTS ARE TO BE OFFSET A MINIMUM OF 2.5m HORIZONTALLY FROM THE CENTERLINE OF THE SANITARY SEWER.
- 7. WATERMAIN BEDDING SHOULD BE AS PER TRENCH DETAIL ON THE PLAN AND PROFILE DRAWING AND COMPACTED TO 100%
- 8. WATERMAINS TO BE INSTALLED TO GRADES AS SHOWN ON APPROVED PLANS, COPY OF GRADE SHEET MUST BE SUPPLIED TO THE REGION OF PEEL INSPECTOR PRIOR TO COMMENCEMENT OF WORK.
- 9. ANY JOINT DEFLECTION SHALL BE 50% OF MANUFACTURER'S SPECIFICATIONS. PIPE BARREL DEFLECTION IS PROHIBITED. 10. FIRE HYDRANTS TO BE INSTALLED AS PER REGION STD. DWG. 1-6-1 AND 1-6-2 WITH FLANGE SET BETWEEN 50mm AND 150mm
- 11. ALL HYDRANTS SHALL HAVE 1.2m MINIMUM HORIZONTAL CLEARANCE FROM ALL OTHER UTILITIES AND STRUCTURES MEASURED FROM THE NEAREST POINT OF THE STRUCTURE.
- 12. MECHANICAL RESTRAINERS ARE REQUIRED FOR ALL FITTINGS, VALVES, DEAD ENDS, CAPS AND HYDRANTS ON ALL PVC
- WATERMAINS; MINIMUM RESTRAINED PIPE LENGTH AS PER REGION'S STANDARD DRAWING 1-5-9. 13. STAINLESS STEEL NUTS AND BOLTS ARE TO BE USED ON ALL METALLIC FITTINGS AND JOINT RESTRAINTS.
- 14. ALL METALLIC VALVES, FITTINGS, THROUGH WALL METAL PIPING AND JOINT RESTRAINTS TO BE C/W. DENSO PASTE, DENSO
- MASTIC & DENSO TAPE OR APPROVED EQUAL APPLIED TO MANUFACTURER'S RECOMMENDATIONS. 15. WHERE PLASTIC PIPE IS USED, INSTALL A 12 GAUGE TWU STRANDED COPPER, LIGHT COLOURED, PLASTIC COATED TRACER
- WIRE ATTACHED TO THE PIPE WITH APPROVED WIRE SPLICE. THE WIRE SHOULD BE BROUGHT TO THE SURFACE AT EACH SERVICE & VALVE BOX AND HYDRANT VALVES.
- 16. 50mm DIAMETER WATERMAIN SHALL BE TYPE K SOFT COPPER. WATERMAIN INSTALLATION IN CUL-DE-SACS TO BE INSTALLED AS PER REGION STD. DWG. 1-7-4.
- 17. A PHYSICAL SEPARATION MUST BE MAINTAINED AT ALL CONNECTION POINTS OF NEW WATERMAIN TO THE EXISTING SYSTEM UNTIL BACTERIOLOGICAL TESTS HAVE PASSED, AS PER STD. DWG. 1-7-7 AND 1-7-8.
- 18. PROVISION FOR FLUSHING OF NEW WATERMAINS PRIOR TO TESTING MUST BE PROVIDED WITH AT LEAST A 50mm OUTLET ON WATERMAINS SMALLER THAN 300mm IN DIAMETER, AND MINIMUM 100mm OUTLET ON WATERMAINS 300mm AND LARGER. COPPER WATERMAINS ARE TO HAVE FLUSHING POINTS AT THE END, THE SAME SIZE AS THE WATERMAIN, AS PER STD. DWG.
- 19. ALL SERVICE CONNECTIONS TO PVC PIPES ARE TO BE MADE USING APPROVED WIDE BAND SERVICE SADDLE. DIRECT TAPPING IS NOT ALLOWED.

- 20. ALL WATER SERVICES SHALL BE MINIMUM 25mm DIA.NOMINAL COPPER PIPE SIZE OR 32mm DIA. POLYETHYLENE PIPE. IN GENERAL, NON METALLIC SERVICES SHALL BE ONE SIZE LARGER THAN THE NOMINAL COPPER PIPE SIZE AS PER LATEST APPROVED REGIONAL PRODUCT LIST AND SIZES C/W. TRACER WIRE.
- 21. THE MINIMUM LATERAL DISTANCE BETWEEN WATER SERVICES AND OTHER UTILITIES SHALL BE 1.2m.
- 22. ALL RESIDENTIAL WATER SERVICE BOXES/CURB STOPS SHALL BE INSTALLED WITHIN SODDED AREAS WITH MINIMUM
- DISTANCE OF 1.0 METRES FROM THE EDGE OF THE DRIVEWAY, BE FLUSH WITH GRADE AND ACCESSIBLE AT ALL TIME. 23. VALVE AND BOXES SHALL BE CAST IRON SLIDING TYPE, COMPLETED WITH VALVE GUIDE PLATES INSTALLED AS PER REGION STD. 1-3-8.AND BOXES SHALL BE INSTALLED AS PER REGION STD. 1-3-8. MAINLINE VALVES TO BE RESTRAINED AS PER REGION STD. 1-3-3A. VALVES SHALL OPEN TO THE LEFT (COUNTER-CLOCKWISE).
- 24. ALL WATER SERVICES BOXES SHOULD BE "LEAD FREE" AS PER REGION'S MATERIAL SPECIFICATIONS.
- 25. THE REGION WILL COMPLETE THE NECESSARY WATER TESTING (PRESSURE TEST, FLUSHING, CHLORINATION AND SAMPLING). CONTRACTOR MAY PROCEED WITH HIS OWN PRESSURE TEST AND FLUSHING PRIOR TO REGION'S TESTING.
- 26. ALL METALLIC WATER PIPES INCLUDING 'K' COPPER WATER SERVICES, INSTALLED OR REPAIRED, SHALL HAVE ZINC ANODE AS PER REGION OF PEEL STANDARD 1-7-1, OPSS422 AND OPSD 1109.011 AND TO CONFORM TO ASTM B-418 TYPE.
- 27. WATERMAIN PIPES SHALL BE BROUGHT ON SITE WITH MANUFACTURER'S PLUGS AND STORED SO NO DEBRIS ENTER THE PIPE. THE CONTRACTOR IS NOT ALLOWED TO INSTALL ANY WATERMAIN UNTIL HE HAS A NIGHT PLUG ON SITE. THE NIGHT PLUG IS TO BE USED EVERY TIME WHEN WORK IS STOPPED.

# **WATERMAIN IN FILL AREA NOTES:**

- NO WATERMAIN TO BE LAID ON FILL UNTIL THE FIELD DENSITY TEST REPORTS HAVE BEEN SUBMITTED TO AND APPROVED BY
- THE REGION OF PEEL OR THE CONSULTING ENGINEER.
- PIPE JOINTS DEFLECTIONS ARE NOT ALLOWED IN FILL AREA. JOINTS SHALL BE MECHANICALLY RESTRAINED THE WHOLE LENGTH.
- ALL HYDRANTS, TEE BRANCH VALVES AND HORIZONTAL BENDS ARE TO BE MECHANICALLY RESTRAINED WITH TIE RODS.
- IN EXISTING MUNICIPAL RIGHT-OF-WAY OR EASEMENT, FILL TO BE PLACED TO 600mm MINIMUM ABOVE THE OBVERT OF THE WATERMAIN AND TO 300mm LIFTS; AND THEREAFTER, FOR EVERY 300mm LIFT ALONG THE CENTERLINE, AND 1.5m TO EITHER SIDE, OF WATERMAIN AT MAXIMUM INTERVAL OF 30.0m. TEST RESULTS MUST BE SUBMITTED TO AND APPROVED BY THE CONSULTANT OR AGENCY.

# **SANITARY SEWER NOTES:**

- ALL SANITARY SEWER BEDDING AS PER STD. 2-3-1.
- MAINLINE SANITARY SEWER PIPE SIZE SHALL BE MINIMUM 250mm DIAMETER INSTALLED AT THE APPROVED DESIGN GRADE.
- PIPE CLASS AND APPURTENANCES AS PER REGION'S SPECIFICATIONS. 3. ALL SEWERS CONSTRUCTED WITH GRADES 0.5% OR LESS SHALL BE APPROVED BY THE ENGINEER AND THE AGENCY PROJECT MANAGER OR DESIGNATED AND BE INSTALLED WITH LASER AND CHECKED PRIOR TO BACKFILL.
- 4. MINIMUM SANITARY SEWER PIPE SLOPE FOR LAST LEG SHALL BE 1% AND DESIRABLE SLOPE 2%. 5. ALL MANHOLES SHALL BE AS PER REGION STD. DWG. 2-5-2, 2-5-3, 2-5-4, 2-5-5 AND 2-5-6 AND BENCHING AS PER STD. DWG.
- 6. FRAME AND COVERS SHALL BE AS PER REGION STD. DWG. 2-5-13, 2-6-1 TO 2-6-8.
- MANHOLE STEPS OR LADDERS TO BE AS PER REGION STD. DWG. 2-6-9 TO 2-6-11.
- MANHOLES DEEPER THAN 5.0m MUST BE EQUIPPED WITH SAFETY PLATFORMS, AS PER STD. 2-6-13 AND 2-6-14. MANHOLE DROP STRUCTURES SHALL BE AS PER REGION STD. DWG. 2-5-26 AND 2-5-27.
- 10. SANITARY SERVICE LATERALS SHALL BE MINIMUM 125mm DIAMETER.
- SANITARY SERVICE SHALL BE LOWER THAN AND TO THE RIGHT OF THE STORM SERVICE AT THE PROPERTY LINE WHEN FACING THE LOT FROM THE STREET.
- CONNECTIONS TO SEWERS SHALL BE MADE WITH MANUFACTURED TEES OR WYES WHERE APPLICABLE AND SHALL BE COLOUR CODED AS NON-WHITE, AS PER STD. DWG. 2-4-1, TO 2-4-7.

# **REGIONAL ROADS NOTES:**

- 1. CONSTRUCTION AND DETOUR SIGNAGE MUST CONFORM TO "MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES" AND LATEST REVISION OF THE ONTARIO MINISTRY OF TRANSPORTATION "TRAFFIC CONTROL MANUAL FOR ROADWAY WORK OPERATIONS" 2. ALL TEMPORARY SIGNAGE AND TRAFFIC CONTROL MEASURES SHALL BE IN ACCORDANCE WITH REQUIREMENTS OF ONTARIO
- TRAFFIC MANUAL, BOOK 7 "TEMPORARY CONDITIONS" AND OPS SPECIFICATIONS AND STANDARD DRAWINGS. 3. PAVEMENT MARKINGS MUST BE IN ACCORDANCE WITH THE ONTARIO TRAFFIC MANUAL, BOOK II "PAVEMENT HAZARD AND
- **DELINEATION MARKINGS".** 4. THE CONTRACTOR SHALL NOTIFY IN ADVANCE, AS REQUIRED, THE APPROPRIATE AUTHORITY HAVING JURISDICTION FOR THE ROAD PRIOR TO COMMENCING ANY WORK AND SHALL ACQUIRE AND SATISFY THE REQUIREMENTS OF APPROPRIATE PERMITS
- (FEES, INSPECTIONS, SIGNAGE, TRAFFIC, MAINTENANCE, DIVERSION, ETC...). 5. REGIONAL ROAD CLOSURE IS NOT PERMITTED AT ANY TIME UNLESS APPROVAL FROM REGIONAL COUNCIL WAS OBTAINED FOR
- THE WORKS, WHERE A MINIMUM TWO MONTH LEAD TIME IS REQUIRED, AS PER REGIONAL POLICY W30-12. 6. WORK OPERATIONS THAT REQUIRE DIVERTING TRAFFIC TO ONE LANE ARE SUBJECT TO TIME RESTRICTIONS AND /OR NIGHT TIME OPERATIONS AS SPECIFIED IN ROAD OCCUPANCY PERMIT. THROUGH LANES MUST BE MINIMUM 3.5m, UNLESS
- 7. FOR TEMPORARY DELINEATION OF TRAFFIC IN OPPOSITE DIRECTIONS A YELLOW CENTRE LINE ON PAVEMENT MUST BE
- PAINTED. TRAFFIC CONTROL BARRELS (CONES) ARE NOT PERMITTED FOR THIS USE ON REGIONAL ROADS. 8. NEW JERSEY BARRIERS (NJB) WITH CRASH ATTENUATION DEVICES MUST BE USED ON LONG TERM PROJECTS AS OPPOSED TO TRAFFIC CONTROL DELINEATORS (BARRELS).
- 9. ACCESS TO EXISTING ENTRANCES AND SIDE STREETS, INCLUDING PEDESTRIAN ACCESS, SHALL BE MAINTAINED. ACCESS REQUIREMENTS MUST COMPLY WITH REGION OF PEEL CONTROLLED ACCESS BY-LAW.
- 10. LOCATION OF EXISTING UTILITIES TO BE ESTABLISHED BY THE CONTRACTOR. ALL EXISTING UTILITY ELEVATIONS (SANITARY AND WATERMAIN) INCLUDING CENTRE LINE OF THE ROAD ELEVATIONS HAVE TO BE VERIFIED BY CONTRACTOR PRIOR TO COMMENCING ANY WORK ON SITE. ANY DISCREPANCIES SHALL BE REPORTED TO THE REGION IMMEDIATELY.
- 11. THE CONTRACTOR(S) SHALL BE SOLELY RESPONSIBLE FOR LOCATING, SUPPORTING AND PROTECTING ALL UNDERGROUND AND OVERHEAD UTILITIES AND STRUCTURES EXISTING AT THE TIME OF CONSTRUCTION IN THE AREA OF HIS WORK, WHETHER SHOWN ON THE PLANS OR NOT, AND FOR ALL REPAIRS AND CONSEQUENCES RESULTING FROM DAMAGE TO SAME.
- 12. THE CONTRACTOR(S) SHALL BE SOLELY RESPONSIBLE TO GIVE 72 HOURS WRITTEN NOTICE TO UTILITY AUTHORITY PRIOR TO CROSSING SUCH UTILITIES FOR THE PURPOSE OF INSPECTION. THIS INSPECTION WILL BE FOR THE DURATION OF CONSTRUCTION WITH THE CONTRACTOR RESPONSIBLE FOR ALL COSTS ARISING FROM SUCH INSPECTIONS.
- 13. ALL ROAD BASE SHALL BE AS PER REGION OF PEEL STD. DWG. 5-1-1 AND 5-1-2. 14. ASPHALT PRESERVATIVE SEALER SUCH AS RE-CLIMATE OR APPROVED EQUIVALENT SHALL BE APPLIED AFTER THE ONE-YEAR
- MAINTENANCE PERIOD FOR THE TOP COURSE ASPHALT. 15. ALL EXISTING PAVEMENTS, CURBS, SIDEWALKS AND BOULEVARDS, AND OTHER AREAS DISTURBED BY THE WORK, TO BE REINSTATED EQUAL TO EXISTING AND TO THE SATISFACTION OF APPLICABLE AUTHORITY HAVING JURISDICTION OVER THE ROAD ALLOWANCE. EXISTING PAVEMENT AND CURBS TO BE SAW- CUT TO PROVIDE A SMOOTH JOINT.
- 17. FOR ROAD PROJECTS THAT WILL NOT BE COMPLETED PRIOR TO THE END OF THE CONSTRUCTION SEASON, THE FOLLOWING WILL NEED TO BE CONSIDERED IN ORDER TO WINTERIZE THE CONSTRUCTION PROJECT TO ENSURE SAFE CONDITIONS
- a. WHERE APPLICABLE, CURB AND GUTTER SECTIONS ARE TO BE COMPLETED, THE BASE COURSE ASPHALT SHALL BE IN PLACE.
- CATCH BASINS AND MAINTENANCE HOLES SET TO EXISTING BASE GRADE. STEEL PLATING NOT PERMITTED.
- HOT MIX ASPHALT (HMA) ONLY.
- LANE DELINEATION AND PAVEMENT MARKING COMPLETED.

16. EROSION CONTROL MEASURES TO BE IMPLEMENTED AS REQUIRED.

- WHERE NEW JERSEY BARRIERS USED, OFFSET NO LESS THAN 4.25m FROM EDGE OF TRAVELED LANE. ROAD AND BOULEVARD MUST BE FREE OF OBSTRUCTIONS AND ACCOMMODATE SAFE SNOW PLOW OPERATION CONSIDERING
- THAT A WING AND PLOW IS 6m WIDE AND 1.52m SNOW STORAGE MINIMUM REQUIRED.
- h. ALL CATCH BASIN GRATES SHALL BE SIDE INLET, OPSD 400.081 (LATEST VERSION) UNLESS OTHERWISE NOTED. WINTER SHUT-DOWN MEETINGS WITH THE REGION OF PEEL ROAD MAINTENANCE STAFF ARE REQUIRED PRIOR TO
- SEASONAL SHUT-DOWN AND SHALL BE ORGANIZED BY THE CONSULTANT OR PROJECT MANAGER OR DESIGNATE.

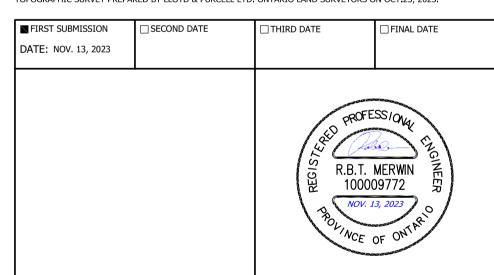
# TRAFFIC SIGNS AND SIGNALS ON REGIONAL ROADS:

- 1. ALL REOUIRED TRAFFIC SIGNS, WHETHER REGULATORY, WARNING, TEMPORARY OR GUIDE/DIRECTIONAL IN NATURE SHALL BE INSTALLED IN ACCORDANCE WITH THE STANDARDS SPECIFICATIONS AND LEGISLATION CONTAINED IN THE OTM MANUALS, THE HTA AND REGION OF PEEL TRAFFIC BY-LAW.
- 2. ELECTRICAL WORKS SHALL CONFORM TO THE ONTARIO PROVINCIAL STANDARD DRAWINGS AND REGION OF PEEL STANDARD DRAWINGS AND SPECIFICATIONS.
- TRAFFIC CONTROLLERS MUST BE INSTALLED AS PER APPROVED LOCATIONS, EQUIPMENT MUST NOT ENCROACH ON PRIVATE PROPERTY WITHOUT PERMISSION TO ENTER, EASEMENT, PERMANENT OR TEMPORARY UNDERTAKINGS.



# BENCHMARK NOTE

ELEVATIONS SHOWN ON THIS PLAN ARE GEODETIC AND ARE REFERRED TO CITY OF MISSISSAUGA BENCHMARK No.688, TOPOGRAPHIC SURVEY PREPARED BY LLOYD & PURCELL LTD. ONTARIO LAND SURVEYORS ON OCT.23, 2023.





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**1315 SILVER SPEAR** 

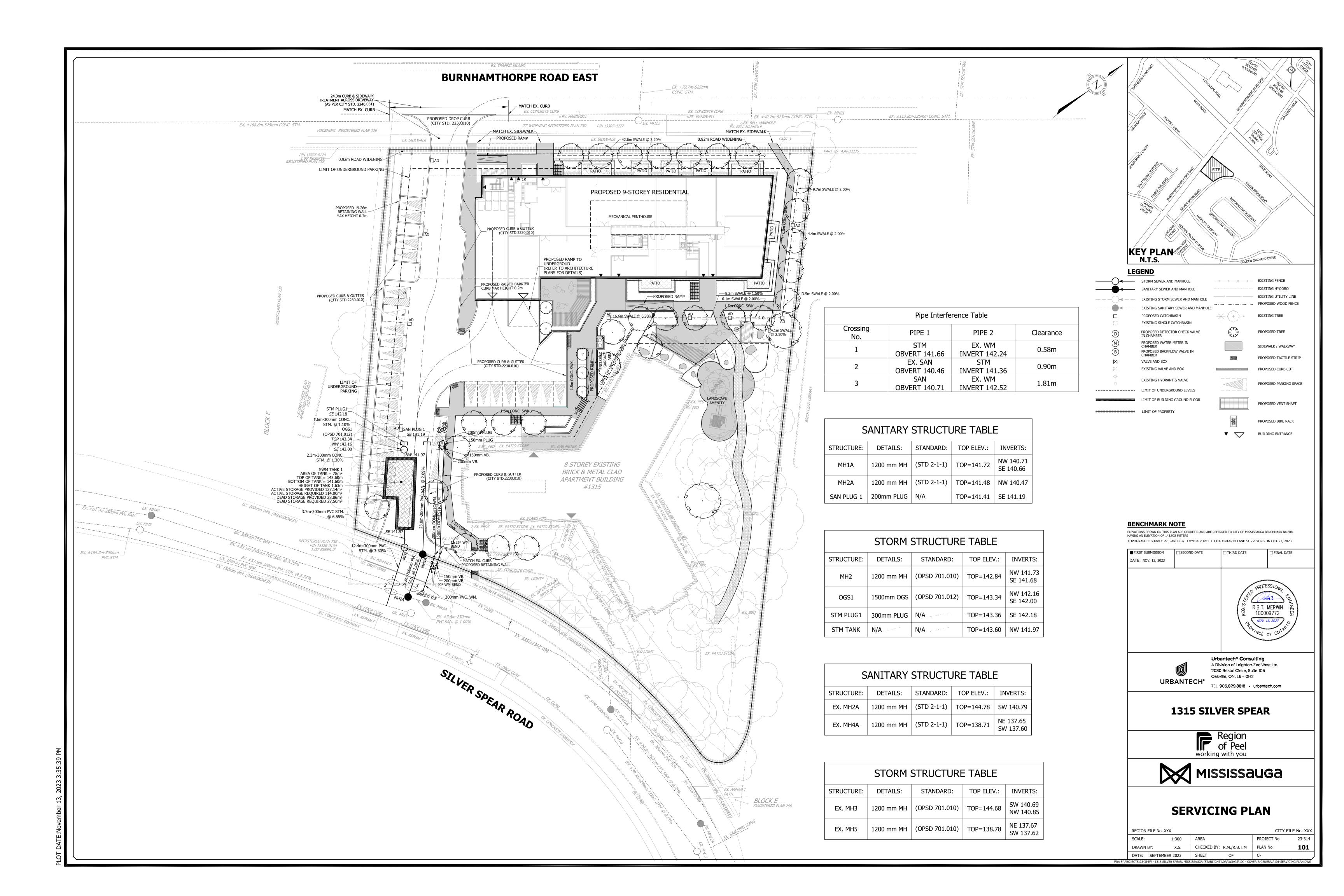


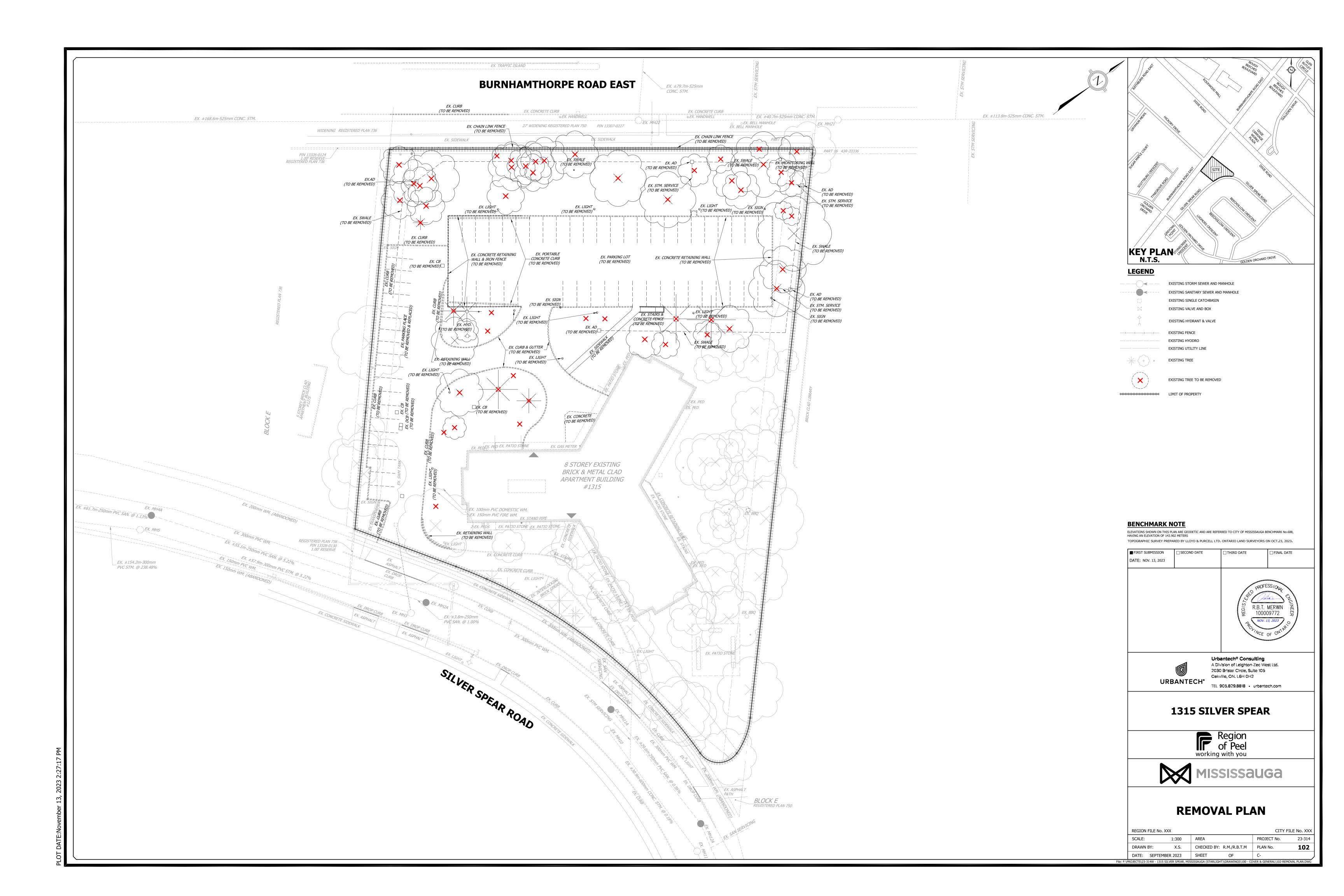
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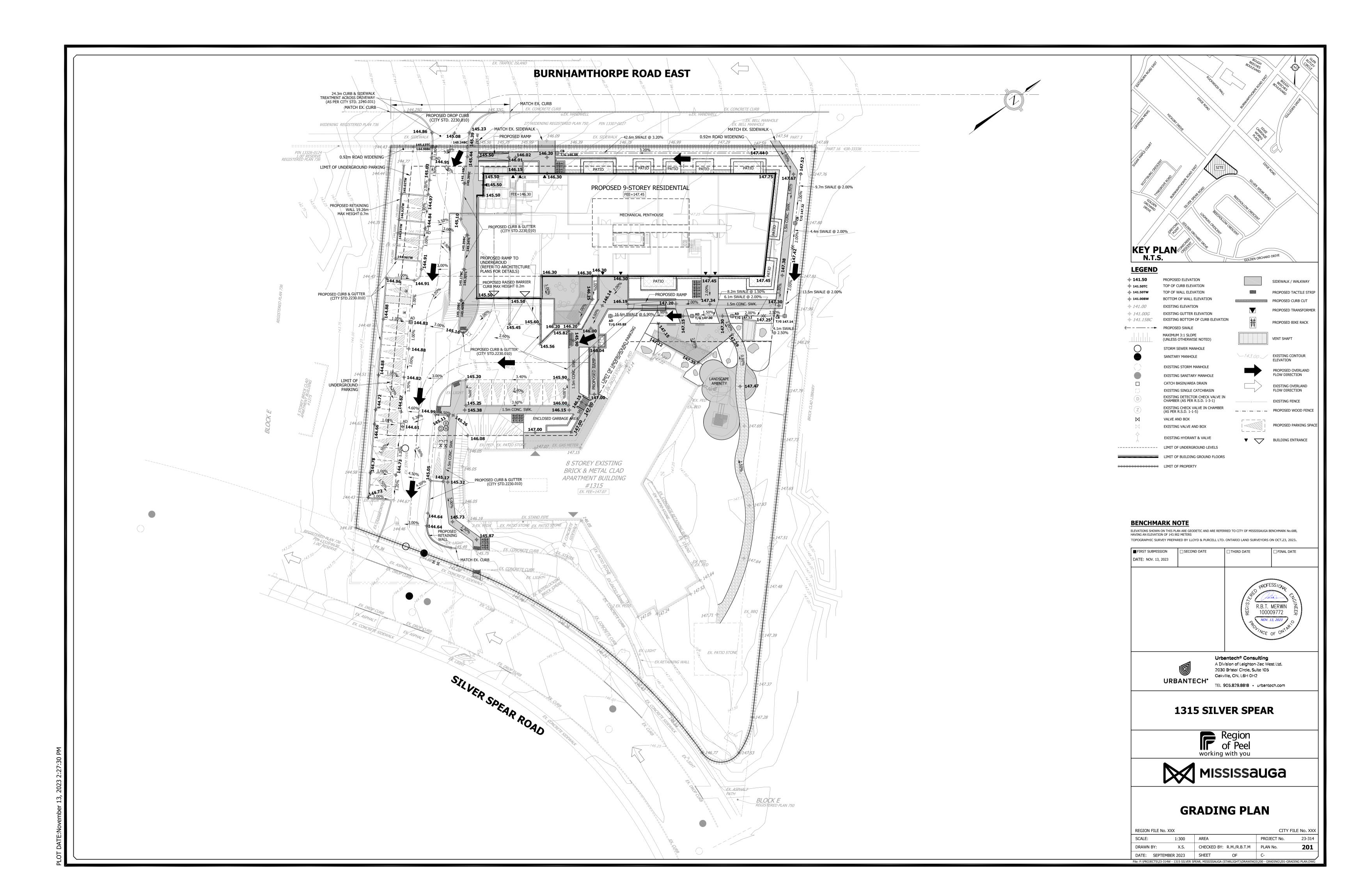
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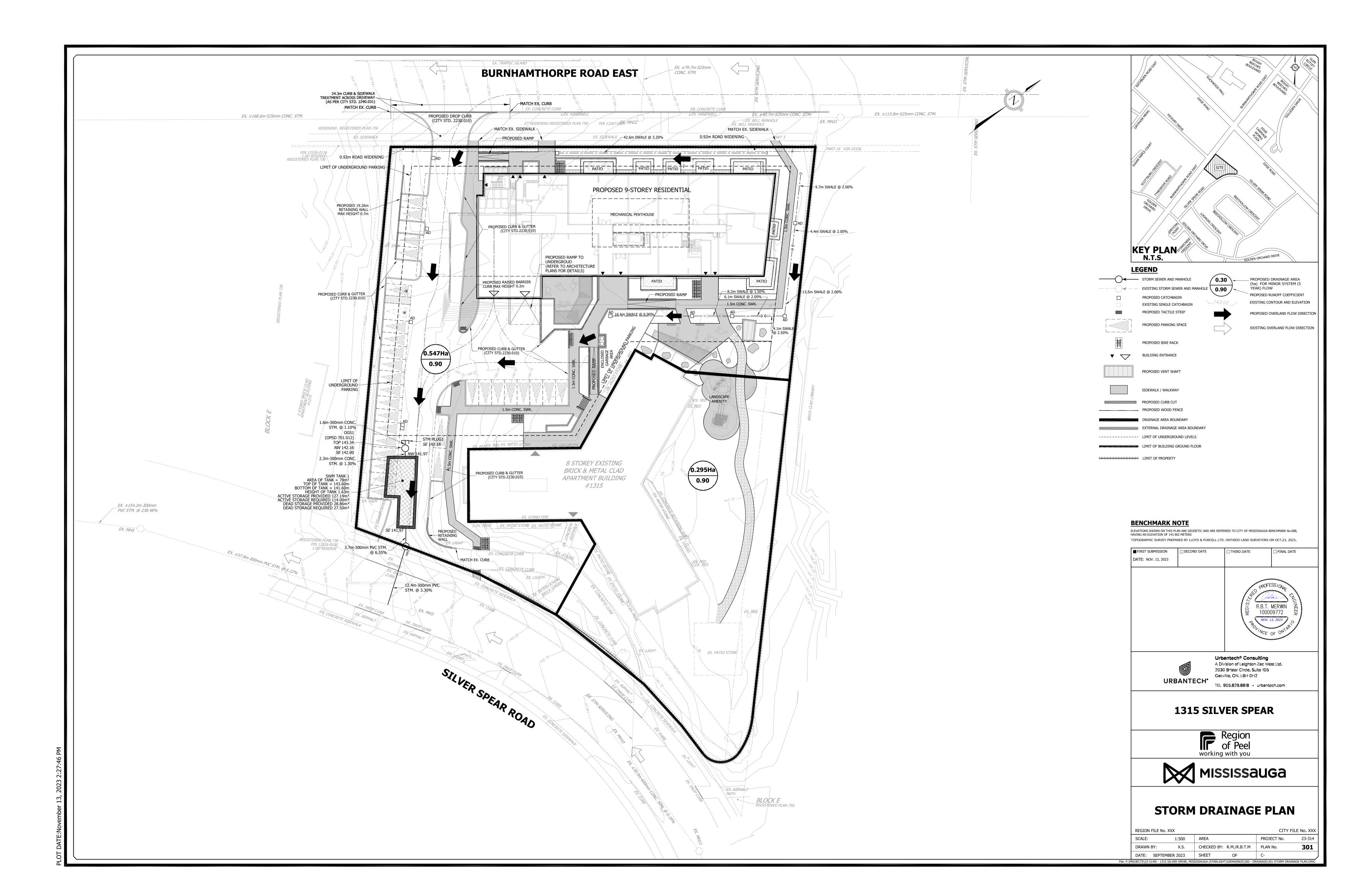
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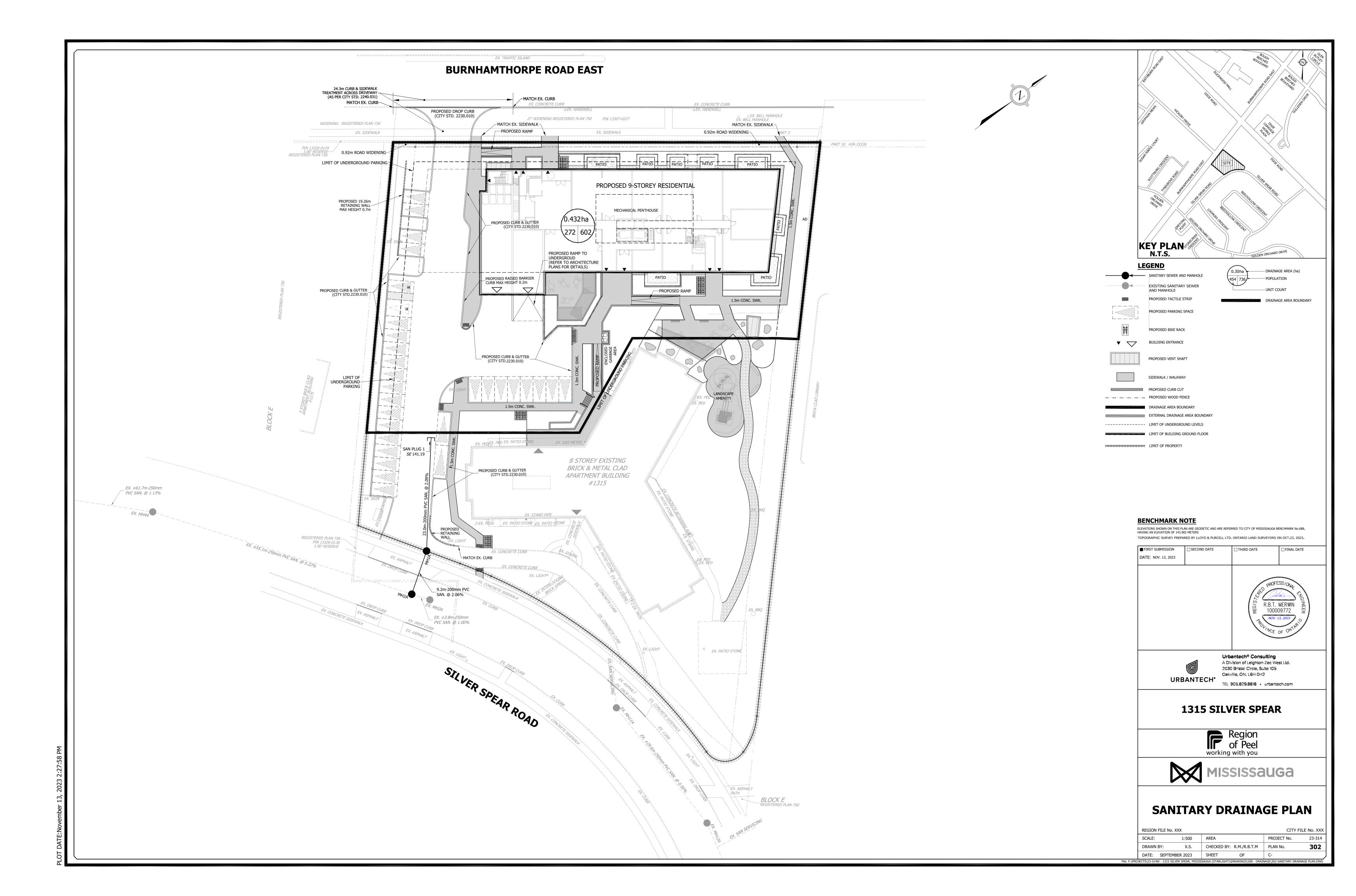
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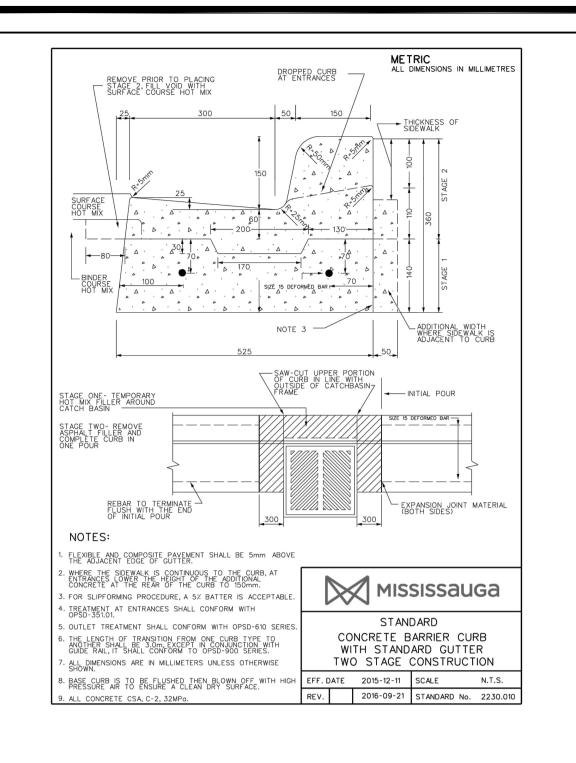


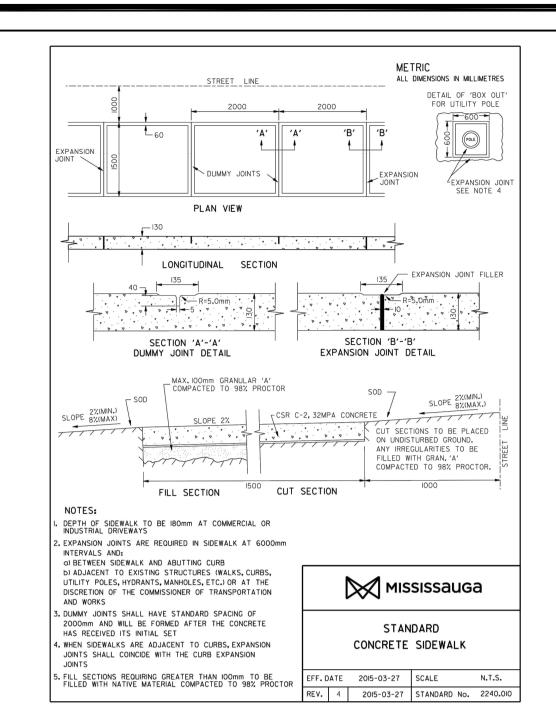


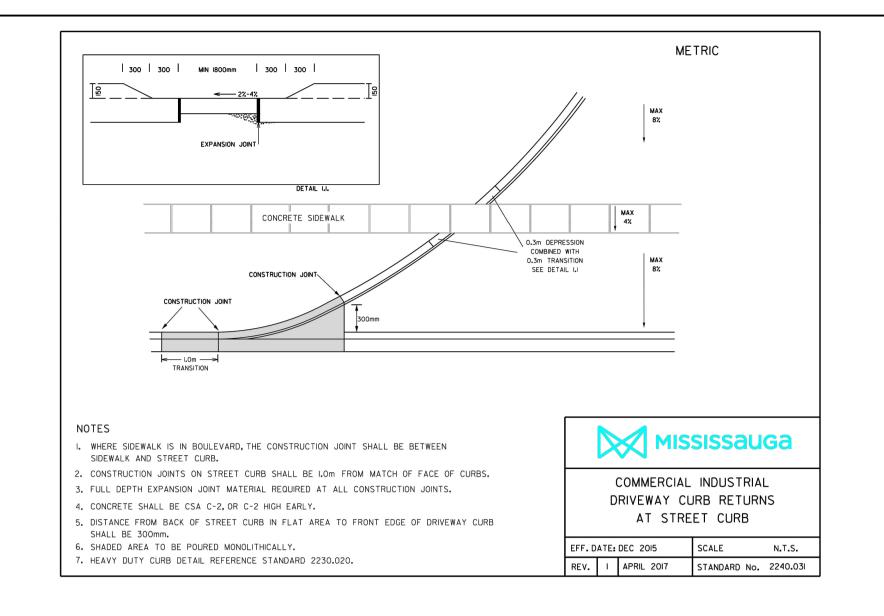


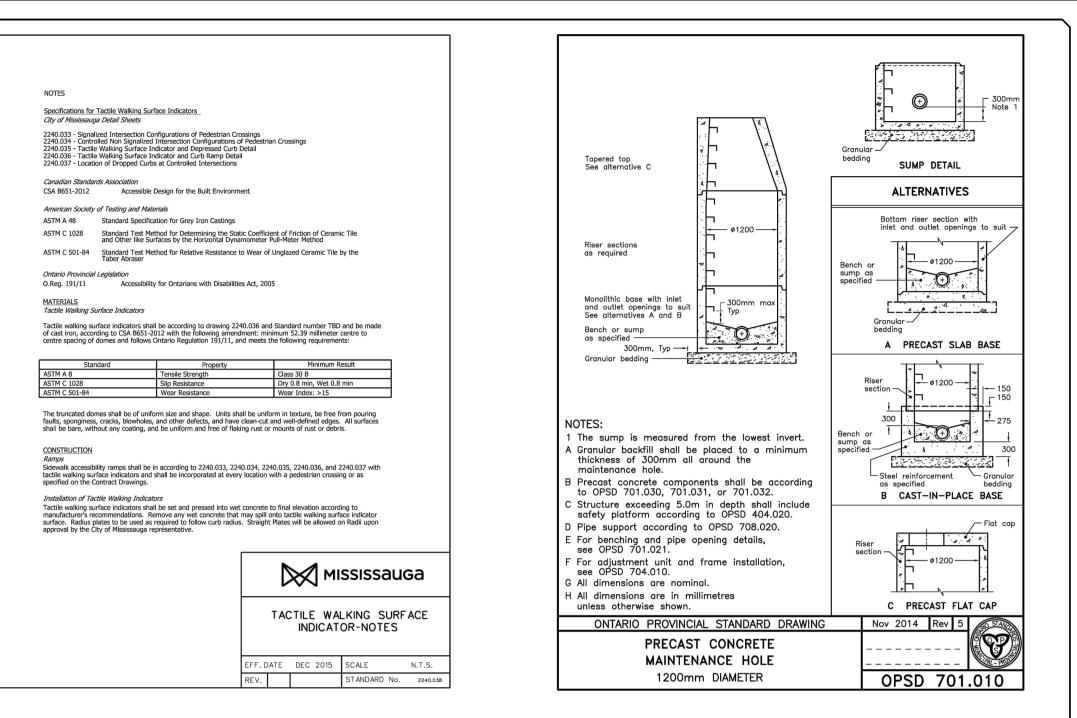


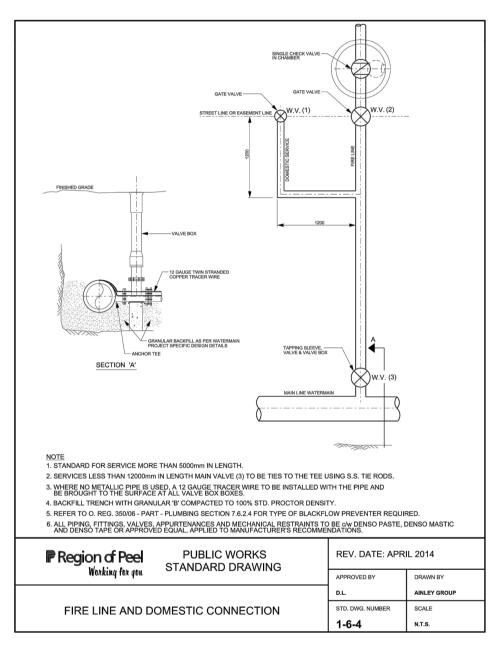


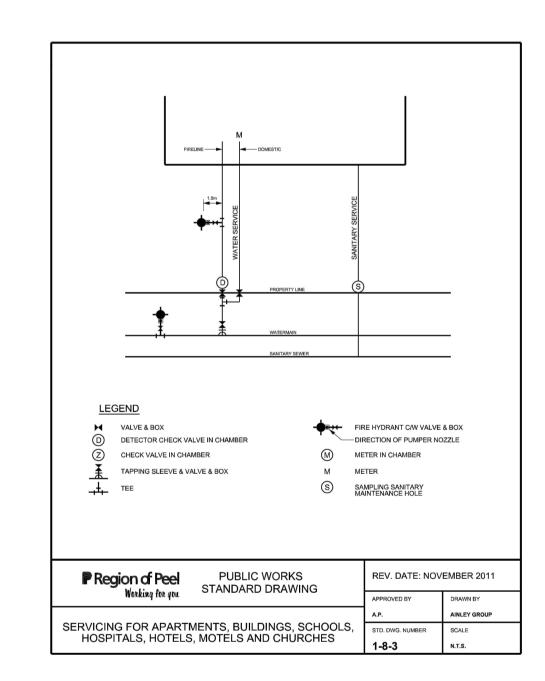


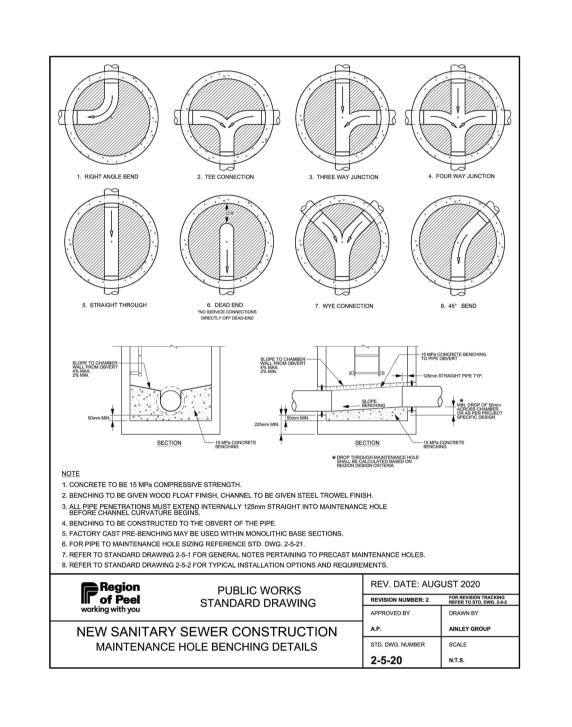


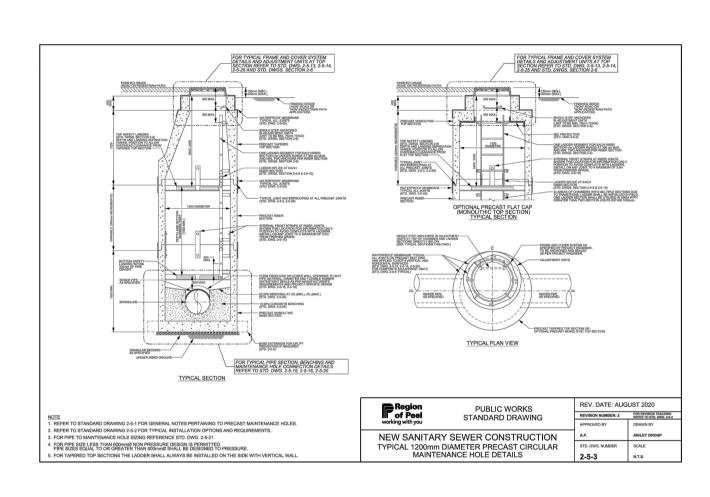


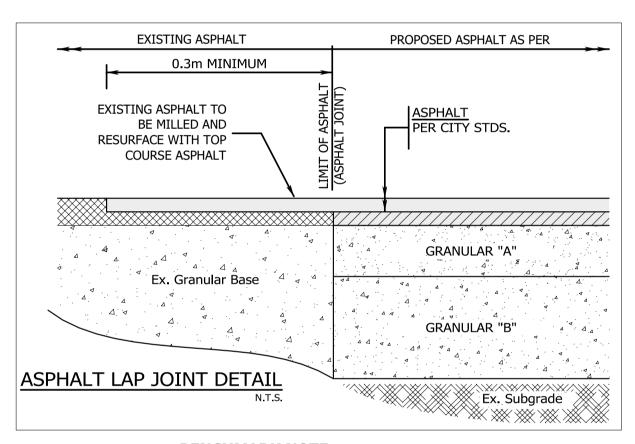








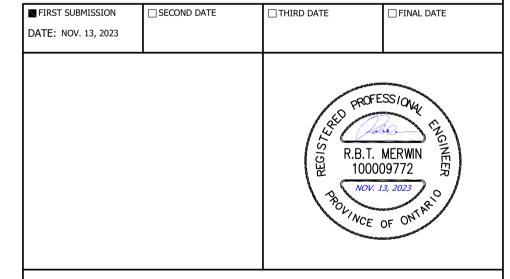




# BENCHMARK NOTE

ELEVATIONS SHOWN ON THIS PLAN ARE GEODETIC AND ARE REFERRED TO CITY OF MISSISSAUGA BENCHMARK No.688, HAVING AN ELEVATION OF 143.902 METERS

TOPOGRAPHIC SURVEY PREPARED BY LLOYD & PURCELL LTD. ONTARIO LAND SURVEYORS ON OCT.23, 2023.





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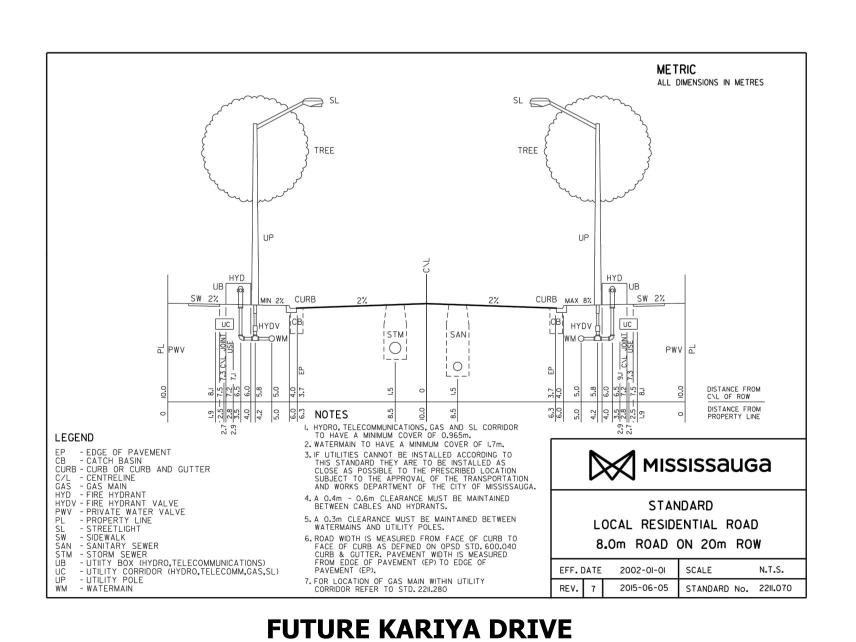


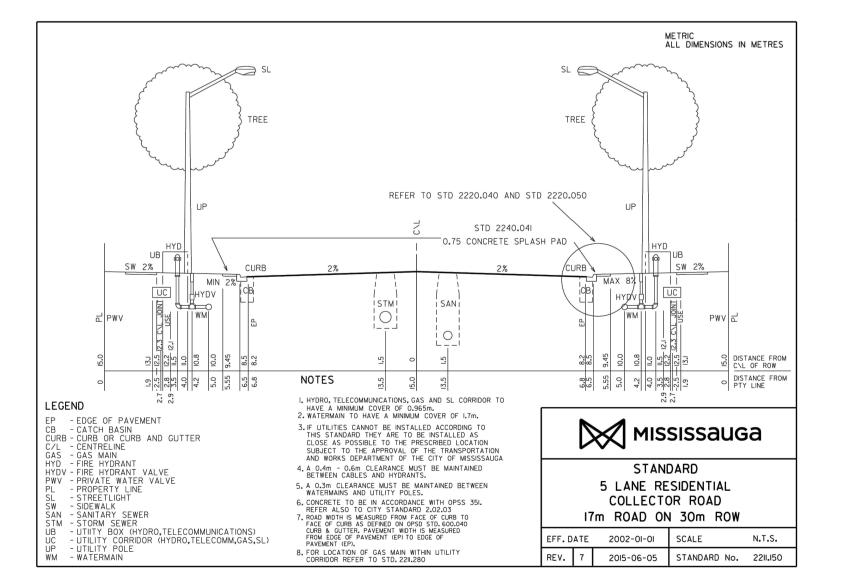
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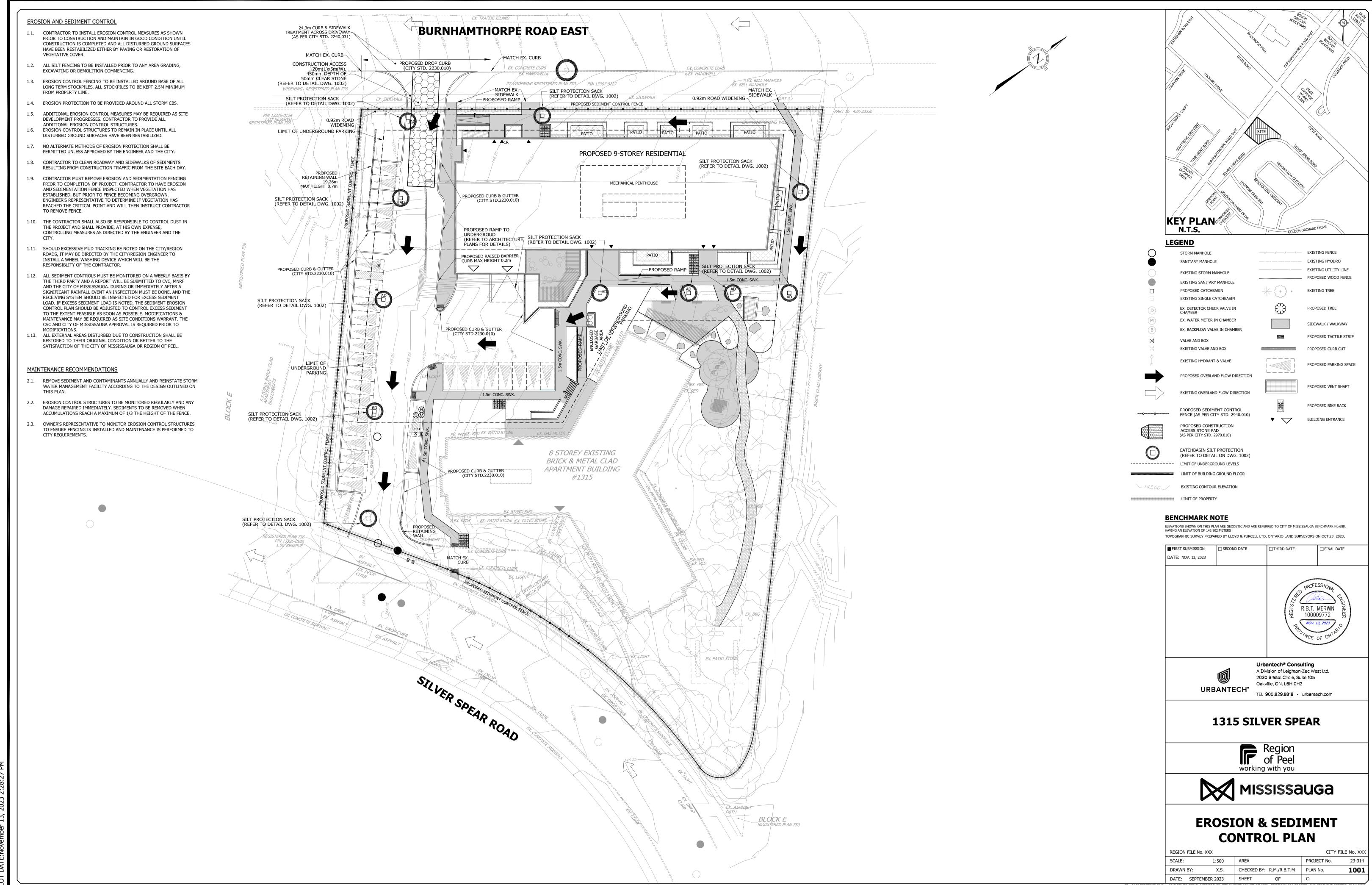
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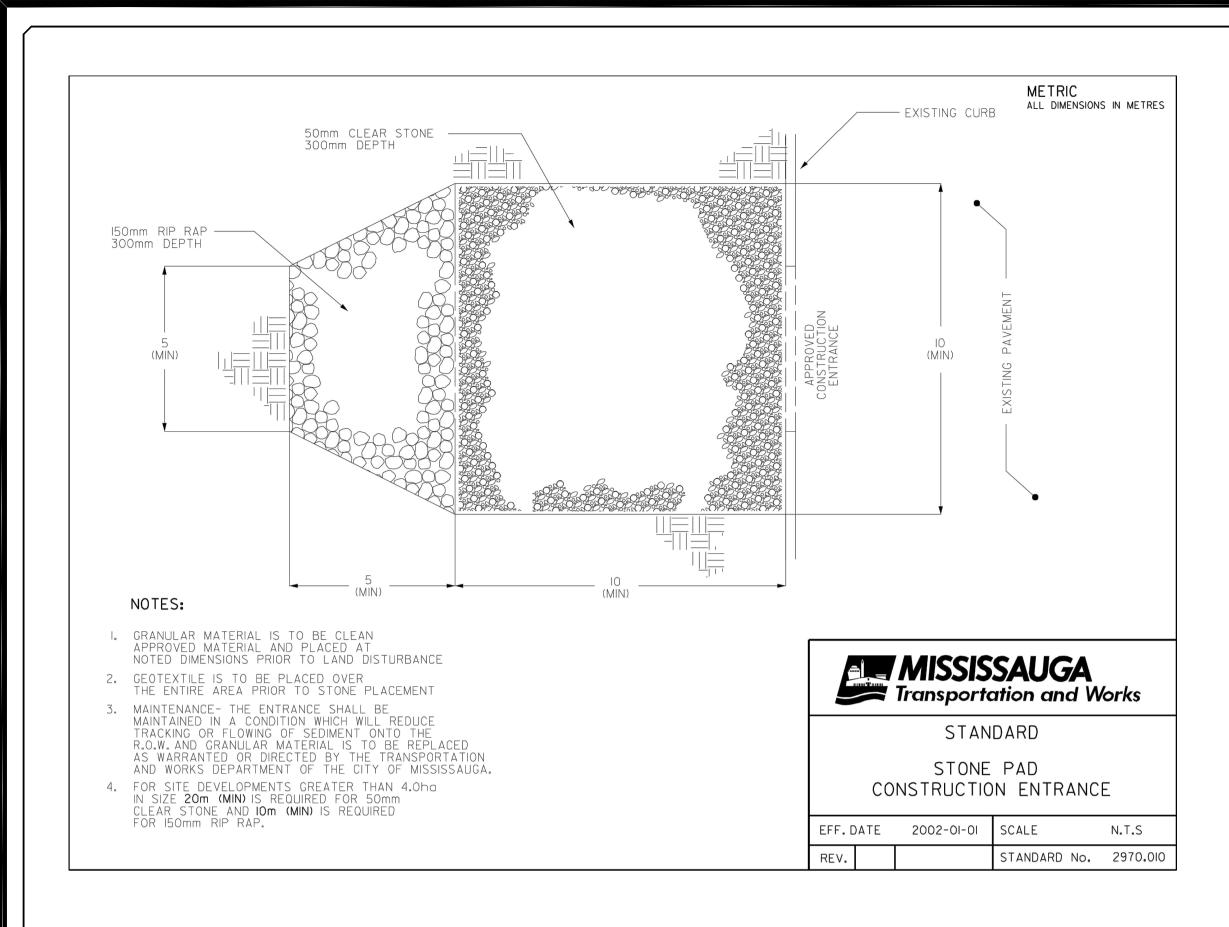
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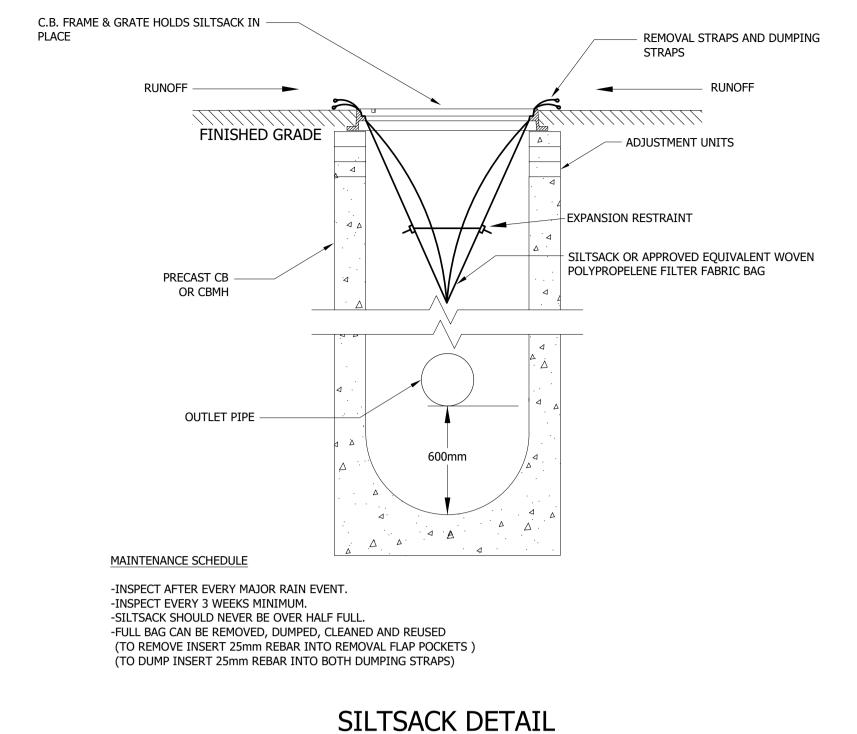
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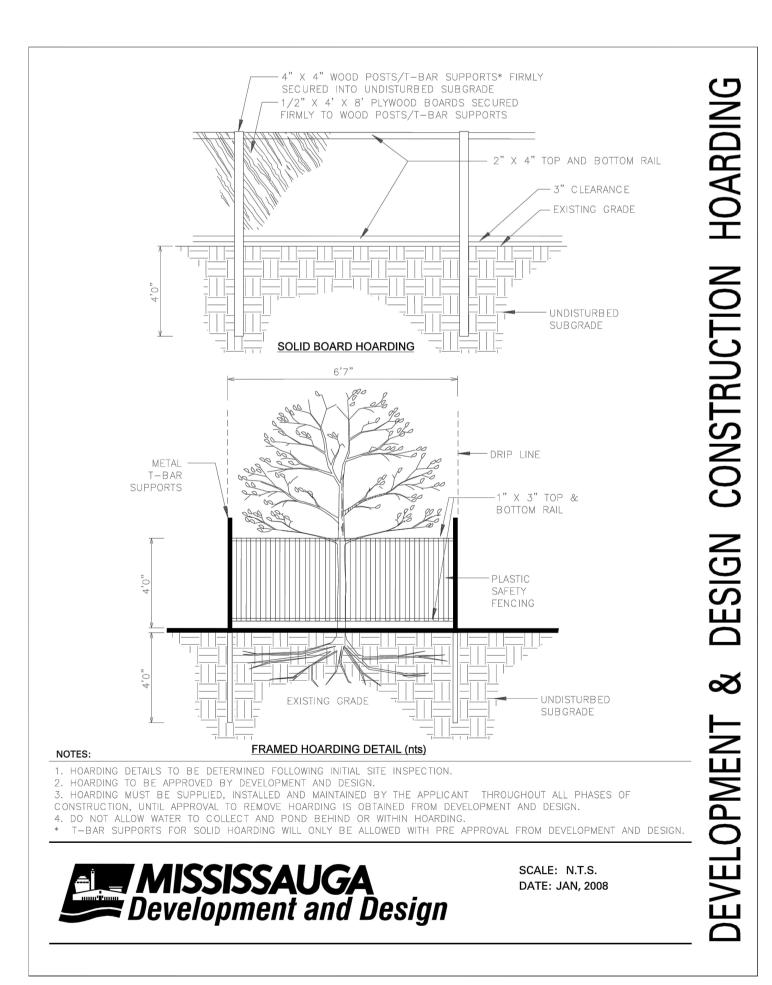


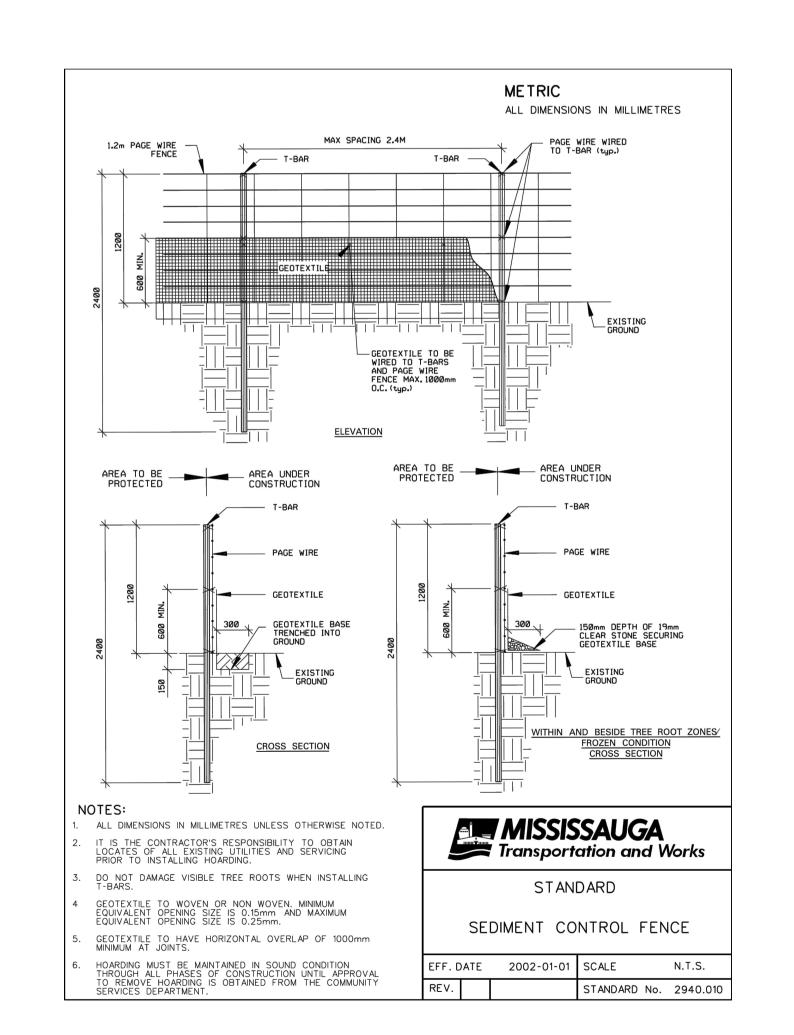






N.T.S.





# **BENCHMARK NOTE**

ELEVATIONS SHOWN ON THIS PLAN ARE GEODETIC AND ARE REFERRED TO CITY OF MISSISSAUGA BENCHMARK No.688, HAVING AN ELEVATION OF 143.902 METERS

TOPOGRAPHIC SURVEY PREPARED BY LLOYD & PURCELL LTD. ONTARIO LAND SURVEYORS ON OCT.23, 2023.

■ FIRST SUBMISSION  DATE: NOV. 13, 2023	SECOND DATE	☐THIRD DATE	☐ FINAL DATE
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1315 SILVER SPEAR





EROSION & SEDIMENT CONTROL DETAILS

REGION FILE No. XXX

SCALE: NTS AREA PROJECT No. 23-314

DRAWN BY: X.S. CHECKED BY: R.M./R.B.T.M PLAN No. 1002

DATE: SEPTEMBER 2023 SHEET OF C-



# **APPENDIX B**SWM Calculations





# Imbrium® Systems **ESTIMATED NET ANNUAL SEDIMENT (TSS) LOAD REDUCTION**

11/13/2023

Province:	Ontario	
City:	Oakville	
Nearest Rainfall Station:	TORONTO INTL AP	
Climate Station Id:	6158731	
Years of Rainfall Data:	20	
Site Name:	1315 Silver Spear Road	

Fine

80.0

0.55 Drainage Area (ha): Runoff Coefficient 'c':

Particle Size Distribution:

Target TSS Removal (%):

0.90

Required Water Quality Runoff Volume Capture (%): 90.00 Estimated Water Quality Flow Rate (L/s): 15.39 Oil / Fuel Spill Risk Site? No **Upstream Flow Control?** No Peak Conveyance (maximum) Flow Rate (L/s): Influent TSS Concentration (mg/L): 200 574 Estimated Average Annual Sediment Load (kg/yr): Estimated Average Annual Sediment Volume (L/yr): 467

Project Name:	Silver Spear Road
Project Number:	23-314W
Designer Name:	Nava Pokharel
Designer Company:	Urbantech Consulting
Designer Email:	kvejani@urbantech.com
Designer Phone:	647-451-6102
EOR Name:	
EOR Company:	
EOR Email:	
EOR Phone:	

# **Net Annual Sediment** (TSS) Load Reduction **Sizing Summary**

Stormceptor Model	TSS Removal Provided (%)
EF4	85
EF6	92
EF8	96
EF10	98
EF12	99

**Recommended Stormceptor EF Model:** EF4

Estimated Net Annual Sediment (TSS) Load Reduction (%):

85

**Water Quality Runoff Volume Capture (%):** 

> 90





### THIRD-PARTY TESTING AND VERIFICATION

► Stormceptor® EF and Stormceptor® EFO are the latest evolutions in the Stormceptor® oil-grit separator (OGS) technology series, and are designed to remove a wide variety of pollutants from stormwater and snowmelt runoff. These technologies have been third-party tested in accordance with the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators and performance has been third-party verified in accordance with the ISO 14034 Environmental Technology Verification (ETV) protocol.

### **PERFORMANCE**

▶ Stormceptor® EF and EFO remove stormwater pollutants through gravity separation and floatation, and feature a patent-pending design that generates positive removal of total suspended solids (TSS) throughout each storm event, including high-intensity storms. Captured pollutants include sediment, free oils, and sediment-bound pollutants such as nutrients, heavy metals, and petroleum hydrocarbons. Stormceptor is sized to remove a high level of TSS from the frequent rainfall events that contribute the vast majority of annual runoff volume and pollutant load. The technology incorporates an internal bypass to convey excessive stormwater flows from high-intensity storms through the device without resuspension and washout (scour) of previously captured pollutants. Proper routine maintenance ensures high pollutant removal performance and protection of downstream waterways.

# PARTICLE SIZE DISTRIBUTION (PSD)

► The Canadian ETV PSD shown in the table below was used, or in part, for this sizing. This is the identical PSD that is referenced in the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators for both sediment removal testing and scour testing. The Canadian ETV PSD contains a wide range of particle sizes in the sand and silt fractions, and is considered reasonably representative of the particle size fractions found in typical urban stormwater runoff.

Particle Size (µm)	Percent Less Than	Particle Size Fraction (µm)	Percent	
1000	100	500-1000	5	
500	95	250-500	5	
250	90	150-250	15	
150	75	100-150	15	
100	60	75-100	10	
75	50	50-75	5	
50	45	20-50	10	
20	35	8-20	15	
8	20	5-8	10	
5	10	2-5	5	
2	5	<2	5	





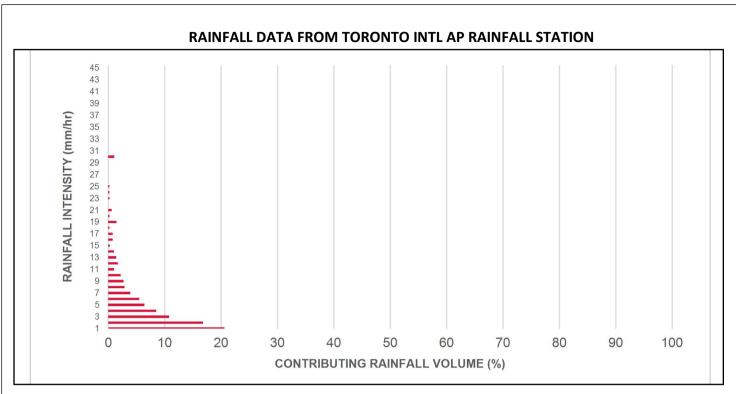
Rainfall Intensity (mm / hr)	Percent Rainfall Volume (%)	Cumulative Rainfall Volume (%)	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)	
0.50	8.5	8.5	0.69	41.0	34.0	100	8.5	8.5	
1.00	20.6	29.1	1.38	83.0	69.0	100	20.6	29.1	
2.00	16.8	45.9	2.75	165.0	138.0	92	15.5	44.6	
3.00	10.8	56.7	4.13	248.0	206.0	83	8.9	53.5	
4.00	8.5	65.2	5.50	330.0	275.0	80	6.7	60.3	
5.00	6.4	71.6	6.88	413.0	344.0	77	4.9	65.2	
6.00	5.5	77.0	8.26	495.0	413.0	74	4.0	69.2	
7.00	3.9	81.0	9.63	578.0	482.0	73	2.9	72.1	
8.00	2.9	83.9	11.01	661.0	550.0	72	2.1	74.2	
9.00	2.7	86.5	12.38	743.0	619.0	71	1.9	76.1	
10.00	2.2	88.7	13.76	826.0	688.0	70	1.5	77.6	
11.00	1.0	89.7	15.14	908.0	757.0	70	0.7	78.3	
12.00	1.7	91.3	16.51	991.0	826.0	69	1.1	79.4	
13.00	1.4	92.8	17.89	1073.0	894.0	69	1.0	80.4	
14.00	1.0	93.7	19.27	1156.0	963.0	68	0.7	81.0	
15.00	0.3	94.0	20.64	1238.0	1032.0	68	0.2	81.2	
16.00	0.8	94.8	22.02	1321.0	1101.0	70	0.5	81.8	
17.00	0.8	95.7	23.39	1404.0	1170.0	71	0.6	82.4	
18.00	0.2	95.8	24.77	1486.0	1238.0	72	0.1	82.5	
19.00	1.5	97.3	26.15	1569.0	1307.0	73	1.1	83.6	
20.00	0.2	97.5	27.52	1651.0	1376.0	75	0.2	83.8	
21.00	0.6	98.2	28.90	1734.0	1445.0	73	0.5	84.2	
22.00	0.0	98.2	30.27	1816.0	1514.0	70	0.0	84.2	
23.00	0.2	98.4	31.65	1899.0	1583.0	67	0.1	84.4	
24.00	0.2	98.6	33.03	1982.0	1651.0	64	0.2	84.5	
25.00	0.2	98.9	34.40	2064.0	1720.0	61	0.1	84.7	
30.00	1.1	100.0	41.28	2477.0	2064.0	51	0.6	85.2	
35.00	0.0	100.0	48.16	2890.0	2408.0	44	0.0	85.2	
40.00	0.0	100.0	55.04	3303.0	2752.0	39	0.0	85.2	
45.00	0.0	100.0	61.92	3715.0	3096.0	35	0.0	85.2	
	Estimated Net Annual Sediment (TSS) Load Reduction =								

Climate Station ID: 6158731 Years of Rainfall Data: 20

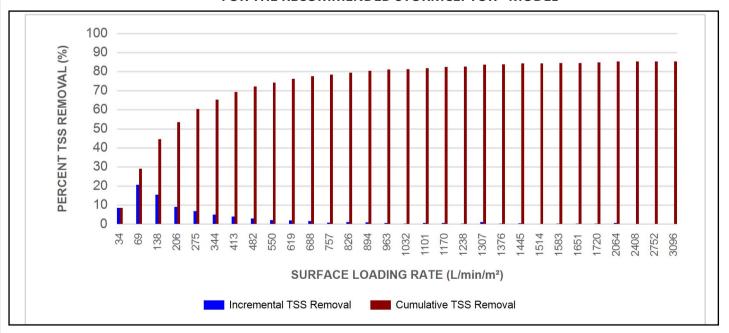








# INCREMENTAL AND CUMULATIVE TSS REMOVAL FOR THE RECOMMENDED STORMCEPTOR® MODEL







### **Maximum Pipe Diameter / Peak Conveyance**

Stormceptor EF / EFO	Model Diameter		Min Angle Inlet / Outlet Pipes	Max Inlet Pipe Diameter		Max Outlet Pipe Diameter		Peak Conveyance Flow Rate	
	(m)	(ft)		(mm)	(in)	(mm)	(in)	(L/s)	(cfs)
EF4 / EFO4	1.2	4	90	609	24	609	24	425	15
EF6 / EFO6	1.8	6	90	914	36	914	36	990	35
EF8 / EFO8	2.4	8	90	1219	48	1219	48	1700	60
EF10 / EFO10	3.0	10	90	1828	72	1828	72	2830	100
EF12 / EFO12	3.6	12	90	1828	72	1828	72	2830	100

### SCOUR PREVENTION AND ONLINE CONFIGURATION

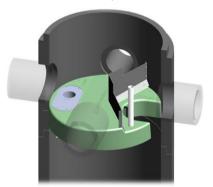
► Stormceptor® EF and EFO feature an internal bypass and superior scour prevention technology that have been demonstrated in third-party testing according to the scour testing provisions of the Canadian ETV Procedure for Laboratory Testing of Oil-Grit Separators, and the exceptional scour test performance has been third-party verified in accordance with the ISO 14034 ETV protocol. As a result, Stormceptor EF and EFO are approved for online installation, eliminating the need for costly additional bypass structures, piping, and installation expense.

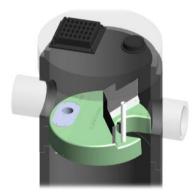
### **DESIGN FLEXIBILITY**

► Stormceptor® EF and EFO offers design flexibility in one simplified platform, accepting stormwater flow from a single inlet pipe or multiple inlet pipes, and/or surface runoff through an inlet grate. The device can also serve as a junction structure, accommodate a 90-degree inlet-to-outlet bend angle, and can be modified to ensure performance in submerged conditions.

### **OIL CAPTURE AND RETENTION**

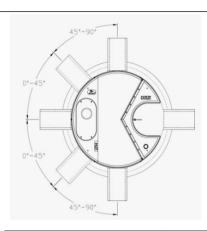
▶ While Stormceptor® EF will capture and retain oil from dry weather spills and low intensity runoff, **Stormceptor® EFO** has demonstrated superior oil capture and greater than 99% oil retention in third-party testing according to the light liquid reentrainment testing provisions of the Canadian ETV **Procedure for Laboratory Testing of Oil-Grit Separators**. Stormceptor EFO is recommended for sites where oil capture and retention is a requirement.











#### **INLET-TO-OUTLET DROP**

Elevation differential between inlet and outlet pipe inverts is dictated by the angle at which the inlet pipe(s) enters the unit.

 $0^{\circ}$  -  $45^{\circ}$  : The inlet pipe is 1-inch (25mm) higher than the outlet pipe.

45° - 90°: The inlet pipe is 2-inches (50mm) higher than the outlet pipe.

#### **HEAD LOSS**

The head loss through Stormceptor EF is similar to that of a 60-degree bend structure. The applicable K value for calculating minor losses through the unit is 1.1. For submerged conditions the applicable K value is 3.0.

### **Pollutant Capacity**

Stormceptor EF / EFO	Model Diameter		Depth (Outlet Pipe Invert to Sump Floor)		Oil Vo	Oil Volume		Sediment Sediment Volume *		Maxim Sediment		
	(m)	(ft)	(m)	(ft)	(L)	(Gal)	(mm)	(in)	(L)	(ft³)	(kg)	(lb)
EF4 / EFO4	1.2	4	1.52	5.0	265	70	203	8	1190	42	1904	5250
EF6 / EFO6	1.8	6	1.93	6.3	610	160	305	12	3470	123	5552	15375
EF8 / EFO8	2.4	8	2.59	8.5	1070	280	610	24	8780	310	14048	38750
EF10 / EFO10	3.0	10	3.25	10.7	1670	440	610	24	17790	628	28464	78500
EF12 / EFO12	3.6	12	3.89	12.8	2475	655	610	24	31220	1103	49952	137875

<sup>\*</sup>Increased sump depth may be added to increase sediment storage capacity

\*\* Average density of wet packed sediment in sump = 1.6 kg/L (100 lb/ft³)

Feature	Benefit	Feature Appeals To
Patent-pending enhanced flow treatment and scour prevention technology	Superior, verified third-party performance	Regulator, Specifying & Design Engineer
Third-party verified light liquid capture and retention for EFO version	Proven performance for fuel/oil hotspot locations	Regulator, Specifying & Design Engineer, Site Owner
Functions as bend, junction or inlet structure	Design flexibility	Specifying & Design Engineer
Minimal drop between inlet and outlet	Site installation ease	Contractor
Large diameter outlet riser for inspection and maintenance	Easy maintenance access from grade	Maintenance Contractor & Site Owner

### STANDARD STORMCEPTOR EF/EFO DRAWINGS

For standard details, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef

#### STANDARD STORMCEPTOR EF/EFO SPECIFICATION

For specifications, please visit http://www.imbriumsystems.com/stormwater-treatment-solutions/stormceptor-ef







# STANDARD PERFORMANCE SPECIFICATION FOR "OIL GRIT SEPARATOR" (OGS) STORMWATER QUALITY TREATMENT DEVICE

#### PART 1 - GENERAL

#### 1.1 WORK INCLUDED

This section specifies requirements for selecting, sizing, and designing an underground Oil Grit Separator (OGS) device for stormwater quality treatment, with third-party testing results and a Statement of Verification in accordance with ISO 14034 Environmental Management – Environmental Technology Verification (ETV).

### 1.2 REFERENCE STANDARDS & PROCEDURES

ISO 14034:2016 Environmental management – Environmental technology verification (ETV)

Canadian Environmental Technology Verification (ETV) Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

### 1.3 SUBMITTALS

- 1.3.1 All submittals, including sizing reports & shop drawings, shall be submitted upon request with each order to the contractor then forwarded to the Engineer of Record for review and acceptance. Shop drawings shall detail all OGS components, elevations, and sequence of construction.
- 1.3.2 Alternative devices shall have features identical to or greater than the specified device, including: treatment chamber diameter, treatment chamber wet volume, sediment storage volume, and oil storage volume.
- 1.3.3 Unless directed otherwise by the Engineer of Record, OGS stormwater quality treatment product substitutions or alternatives submitted within ten days prior to project bid shall not be accepted. All alternatives or substitutions submitted shall be signed and sealed by a local registered Professional Engineer, based on the exact same criteria detailed in Section 3, in entirety, subject to review and approval by the Engineer of Record.

### **PART 2 - PRODUCTS**

#### 2.1 OGS POLLUTANT STORAGE

The OGS device shall include a sump for sediment storage, and a protected volume for the capture and storage of petroleum hydrocarbons and buoyant gross pollutants. The <u>minimum</u> sediment & petroleum hydrocarbon storage capacity shall be as follows:

2.1.1 4 ft (1219 mm) Diameter OGS Units: 1.19 m³ sediment / 265 L oil
6 ft (1829 mm) Diameter OGS Units: 3.48 m³ sediment / 609 L oil
8 ft (2438 mm) Diameter OGS Units: 8.78 m³ sediment / 1,071 L oil
10 ft (3048 mm) Diameter OGS Units: 17.78 m³ sediment / 1,673 L oil
12 ft (3657 mm) Diameter OGS Units: 31.23 m³ sediment / 2,476 L oil

## PART 3 - PERFORMANCE & DESIGN

3.1 GENERAL







The OGS stormwater quality treatment device shall be verified in accordance with ISO 14034:2016 Environmental management – Environmental technology verification (ETV). The OGS stormwater quality treatment device shall remove oil, sediment and gross pollutants from stormwater runoff during frequent wet weather events, and retain these pollutants during less frequent high flow wet weather events below the insert within the OGS for later removal during maintenance. The Manufacturer shall have at least ten (10) years of local experience, history and success in engineering design, manufacturing and production and supply of OGS stormwater quality treatment device systems, acceptable to the Engineer of Record.

#### 3.2 SIZING METHODOLOGY

The OGS device shall be engineered, designed and sized to provide stormwater quality treatment based on treating a minimum of 90 percent of the average annual runoff volume and a minimum removal of an annual average 60% of the sediment (TSS) load based on the Particle Size Distribution (PSD) specified in the sizing report for the specified device. Sizing of the OGS shall be determined by use of a minimum ten (10) years of local historical rainfall data provided by Environment Canada. Sizing shall also be determined by use of the sediment removal performance data derived from the ISO 14034 ETV third-party verified laboratory testing data from testing conducted in accordance with the Canadian ETV protocol Procedure for Laboratory Testing of Oil-Grit Separators, as follows:

- 3.2.1 Sediment removal efficiency for a given surface loading rate and its associated flow rate shall be based on sediment removal efficiency demonstrated at the seven (7) tested surface loading rates specified in the protocol, ranging 40 L/min/m² to 1400 L/min/m², and as stated in the ISO 14034 ETV Verification Statement for the OGS device.
- 3.2.2 Sediment removal efficiency for surface loading rates between 40 L/min/m² and 1400 L/min/m² shall be based on linear interpolation of data between consecutive tested surface loading rates.
- 3.2.3 Sediment removal efficiency for surface loading rates less than the lowest tested surface loading rate of 40 L/min/m² shall be assumed to be identical to the sediment removal efficiency at 40 L/min/m². No extrapolation shall be allowed that results in a sediment removal efficiency that is greater than that demonstrated at 40 L/min/m².
- 3.2.4 Sediment removal efficiency for surface loading rates greater than the highest tested surface loading rate of 1400 L/min/m² shall assume zero sediment removal for the portion of flow that exceeds 1400 L/min/m², and shall be calculated using a simple proportioning formula, with 1400 L/min/m² in the numerator and the higher surface loading rate in the denominator, and multiplying the resulting fraction times the sediment removal efficiency at 1400 L/min/m².

The OGS device shall also have sufficient annual sediment storage capacity as specified and calculated in Section 2.1.

### 3.3 CANADIAN ETV or ISO 14034 ETV VERIFICATION OF SCOUR TESTING

The OGS device shall have Canadian ETV or ISO 14034 ETV Verification of third-party scour testing conducted in accordance with the Canadian ETV Program's **Procedure for Laboratory Testing of Oil-Grit Separators**.

3.3.1 To be acceptable for on-line installation, the OGS device must demonstrate an average scour test effluent concentration less than 10 mg/L at each surface loading rate tested, up to and including 2600 L/min/m<sup>2</sup>.

# CALCULATION OF STORAGE SIZE AND RATING CURVE BASED ON ORIFICE SIZE PROPOSED DEVELOPMENT - PROPOSED SWM TANK

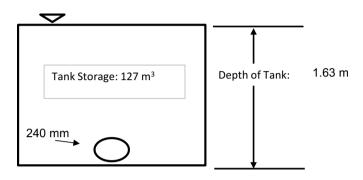


**Project Name:** 1315 Silver Spear Road **Municipality:** City of Mississauga

Project No.: 23-314W
Date: 13-Nov-23

Prepared by: K.V. Checked by: N.P. Submission #: 1

Elevation (m)	Height (m)	Volume (m³)	Flow rate (m³/s)
0.00	0.00	0.00	0.000
0.20	0.20	15.60	0.035
0.40	0.40	31.20	0.066
0.60	0.60	46.80	0.086
0.80	0.80	62.40	0.102
1.00	1.00	78.00	0.117
1.20	1.20	93.60	0.129
1.40	1.40	109.20	0.141
1.60	1.60	124.80	0.151
1.63	1.63	127.14	0.153



Calculation of Orifice	
$A = \pi D^2 \div 4$ $h = Depth \ of \ Tank \ - (\frac{D}{2})$	0.045 m²
$n = Depth of Tank$ $\binom{2}{2}$	1.510 m
С	0.6
$2g = 2 \times 9.81$	19.62 m/s²
$Q = CA\sqrt{2gh}$	0.153 m³/s
Q target (from VO model)	<b>0.153</b> m³/s
Q and Q target are matched	
Therefore, orifice is 240 mm	

Orifice size:	<b>240</b> mm

Name	Description	Result
	Quantity control only	
	Proposed SWM tank footprint	<b>78.0</b> m <sup>2</sup>
Proposed Development	Depth of Proposed SWM Tank	<b>1.63</b> m
	Storage Volume in Proposed SWM Tank	127 m³
	Maximum Storage Volume utilized (from VO6)	106 m³

V V I SSSSS U U A L (v 6.2.2015) V V I SS U U AA L V V I SS U U AAAAA L V V I SS U U A A L VVI SSSS UUUUU A A LLLLL OOO TTTTT TTTTT H H Y Y M M OOO TM OOTT H H Y Y MM MM O O OOTT H H Y M M O O 000 T H H Y M M OOO Т Developed and Distributed by Smart City Water Inc Copyright 2007 - 2022 Smart City Water Inc All rights reserved. \*\*\*\*\* DETAILED OUTPUT \*\*\*\*\* Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2-2015\VO2\voin.dat Output filename: C:\Users\kvejani\AppData\Local\Civica\VH5\330dbc01-652f-4134-9a76-fa0957765e60\b2865c93-4eae-4a1d-8944-bc85ee6524ba\scen Summary filename: C:\Users\kvejani\AppData\Local\Civica\VH5\330dbc01-652f-4134-9a76-fa0957765e60\b2865c93-4eae-4a1d-8944-bc85ee6524ba\scen DATE: 11-13-2023 TIME: 01:39:06 **USER:** COMMENTS: \_\_\_\_\_ \*\* SIMULATION : 10yr \*\*\*\*\*\*\*\*\*\*\*\*\*\*\* | CHICAGO STORM | IDF curve parameters: A=1010.000 | Ptotal= 83.16 mm | B = 4.600C = 0.780used in: INTENSITY =  $A/(t+B)^{C}$ Duration of storm = 24.00 hrsStorm time step = 5.00 minTime to peak ratio = 0.33

file: ///F/...nal%20 Servicing%20 Report/Calculations%20 &%20 Models/Hydrology%20 Model/VO6%20 Output%20-%20 Current%20 Scenario.txt [2023-11-13 3:15:00 PM]

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN

hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr

0.00	0.78	6.00		12.00	2.29	18.00	1.11
0.08	0.78	6.08		12.08	2.25	18.08	1.10
0.17	0.79	6.17	2.61	12.17	2.21	18.17	1.10
0.25	0.80	6.25	2.72	12.25	2.18	18.25	1.09
0.33	0.80	6.33	2.84	12.33	2.15	18.33	1.08
0.42	0.81	6.42		12.42		18.42	1.07
0.50	0.82			12.50		18.50	1.07
0.58	0.83			12.58		18.58	1.06
0.67	0.83			12.67		18.67	1.06
0.75	0.84			12.75		18.75	1.05
0.83	0.85			12.83		18.83	1.04
0.92	0.86			12.92		18.92	1.04
1.00	0.87			13.00		19.00	1.03
1.08	0.87			13.08		19.08	1.02
1.17	0.88			13.17		19.17	1.02
1.25	0.89			13.25		19.25	1.01
1.33	0.90			13.23		19.33	1.01
1.42	0.91			13.42		19.42	1.00
1.50	0.92			13.50		19.50	0.99
1.58	0.93			13.58		19.58	0.99
1.67	0.94			13.56		19.67	0.98
1.75	0.95			13.75		19.75	0.98
1.83	0.96			13.73		19.83	0.97
1.92	0.97			13.92		19.92	0.97
2.00	0.98			14.00		20.00	0.96
2.08	0.99			14.08		20.08	0.96
2.17	1.00			14.17		20.17	0.95
2.25	1.01			14.25		20.25	0.95
2.33	1.03			14.33		20.23	0.94
2.42	1.04			14.42		20.42	0.94
2.50	1.05			14.50		20.50	0.93
2.58	1.06			14.58		20.58	0.93
2.67	1.08			14.67		20.67	0.92
2.75	1.09			14.75		20.75	0.92
2.83		8.83		14.83		20.83	0.91
2.92	1.12			14.92		20.92	0.91
3.00	1.13			15.00		21.00	0.90
3.08	1.15			15.08		21.08	0.90
3.17	1.17			15.17		21.17	0.89
3.25	1.18		5.78			21.25	0.89
3.33	1.20			15.33		21.33	0.89
3.42	1.22			15.42		21.42	0.88
3.50	1.24			15.50		21.50	0.88
3.58		9.58		15.58		21.58	0.87
3.67		9.67		15.67		21.67	0.87
3.75		9.75		15.75		21.75	0.86
3.83		9.83		15.83		21.83	0.86
3.92		9.92		15.92		21.92	0.86
4.00		10.00		16.00		22.00	0.85
4.08		10.08		16.08		22.08	0.85
4.17		10.17		16.17		22.17	0.84
4.25		10.25		16.25		22.25	0.84
4.33		10.33		16.33		22.33	0.84
4.42		10.42		16.42		22.42	0.83
4.50		10.50		16.50		22.50	0.83
						•	

```
4.58
                    3.24 | 16.58
                                  1.25 | 22.58
      1.55 | 10.58
                                                 0.83
4.67
      1.58 | 10.67
                    3.16 | 16.67
                                  1.24 | 22.67
                                                 0.82
4.75
      1.61 | 10.75
                    3.08 | 16.75
                                  1.23 | 22.75
                                                 0.82
4.83
      1.65 | 10.83
                    3.01 | 16.83
                                  1.22 | 22.83
                                                0.81
4.92
      1.69 | 10.92
                    2.94 | 16.92
                                  1.21 | 22.92
                                                0.81
5.00
      1.72 | 11.00
                    2.87 | 17.00
                                  1.21 | 23.00
                                                0.81
5.08
      1.76 | 11.08
                    2.81 | 17.08
                                  1.20 | 23.08
                                                 0.80
5.17
      1.81 | 11.17
                    2.75 | 17.17
                                  1.19 | 23.17
                                                 0.80
5.25
      1.85 | 11.25
                    2.70 | 17.25
                                  1.18 | 23.25
                                                0.80
5.33
      1.90 | 11.33
                    2.64 | 17.33
                                  1.17 | 23.33
                                                 0.79
5.42
      1.95 | 11.42
                   2.59 | 17.42
                                  1.16 | 23.42
                                                 0.79
5.50
      2.01 | 11.50
                   2.54 | 17.50
                                  1.16 | 23.50
                                                0.79
5.58
      2.07 | 11.58
                   2.50 | 17.58
                                  1.15 | 23.58
                                                0.78
5.67
      2.13 | 11.67
                    2.45 | 17.67
                                  1.14 | 23.67
                                                 0.78
      2.19 | 11.75
                   2.41 | 17.75
                                  1.13 | 23.75
                                                 0.78
5.75
5.83
      2.27 | 11.83
                   2.37 | 17.83
                                  1.12 | 23.83
                                                 0.77
5.92 2.34 | 11.92 2.33 | 17.92
                                 1.12 | 23.92
                                                0.77
```

-----

IMPERVIOUS PERVIOUS (i) 0.28 0.28 Surface Area (ha)= Dep. Storage (mm)=1.00 1.50 Average Slope (%) =1.00 2.00 Length (m)=60.55 40.00

Mannings n = 0.013 0.250

Max.Eff.Inten.(mm/hr)= 173.04 78.28 over (min) 5.00 10.00 Storage Coeff. (min)= 1.52 (ii) 9.30 (ii)

Unit Hyd. Tpeak (min)= 5.00 10.00

Unit Hyd. peak (cms)= 0.33 0.12

\*TOTALS\*

PEAK FLOW (cms)= 0.13 0.04 0.153 (iii)
TIME TO PEAK (hrs)= 8.00 8.08 8.00
RUNOFF VOLUME (mm)= 82.16 52.72 67.43
TOTAL PAINTALL (mm)= 83.16 83.16 83.16

TOTAL RAINFALL (mm)= 83.16 83.16 83.16 RUNOFF COEFFICIENT = 0.99 0.63 0.81

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

 $CN^* = 85.0$  Ia = Dep. Storage (Above)

- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

## **FINISH**

	<del></del>	<del></del>	

V V I SSSSS U U A L (v 6.2.2015) V V I SS U U AA L V V I SS U U AAAAA L V V I SS U U A A L VVI SSSS UUUUU A A LLLLL OOO TTTTT TTTTT H H Y Y M M OOO TM OOTT H H Y Y MM MM O O OOTT H H Y M M O O 000 T H H Y M M OOO Т Developed and Distributed by Smart City Water Inc Copyright 2007 - 2022 Smart City Water Inc All rights reserved. \*\*\*\*\* DETAILED OUTPUT \*\*\*\*\* Input filename: C:\Program Files (x86)\Visual OTTHYMO 6.2-2015\VO2\voin.dat Output filename: C:\Users\kvejani\AppData\Local\Civica\VH5\330dbc01-652f-4134-9a76-fa0957765e60\7eee4ae0-3d3b-41ad-87da-939cce1e4293\scen Summary filename: C:\Users\kvejani\AppData\Local\Civica\VH5\330dbc01-652f-4134-9a76-fa0957765e60\7eee4ae0-3d3b-41ad-87da-939cce1e4293\scen DATE: 11-13-2023 TIME: 02:16:01 **USER:** COMMENTS: \_\_\_\_\_ \*\* SIMULATION : 100yr \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* | CHICAGO STORM | IDF curve parameters: A=1450.000 | Ptotal=119.37 mm | B = 4.900C = 0.780used in: INTENSITY =  $A/(t+B)^{C}$ Duration of storm = 24.00 hrsStorm time step = 5.00 minTime to peak ratio = 0.33

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN

hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr

0.00	1.12	6.00	3.49	12.00	3.29	18.00	1.59
0.08	1.13	6.08		12.08	3.24	18.08	1.58
0.17	1.14	6.17	3.76	12.17	3.18	18.17	1.57
0.25	1.15	6.25	3.92	12.25	3.14	18.25	1.56
0.33	1.16	6.33	4.09	12.33	3.09	18.33	1.55
0.42	1.17	6.42	4.27	12.42	3.04	18.42	1.54
0.50	1.18	6.50	4.48	12.50	3.00	18.50	1.53
0.58	1.19	6.58	4.72	12.58	2.95	18.58	1.53
0.67	1.20	6.67	4.98	12.67	2.91	18.67	1.52
0.75	1.21	6.75	5.28	12.75	2.87	18.75	1.51
0.83	1.22	6.83		12.83		18.83	
0.92		6.92		12.92		18.92	
1.00		7.00		13.00	2.76	19.00	1.48
1.08	1.26		7.05	13.08		19.08	
1.17	1.27	7.17	7.72	13.17	2.69	19.17	1.46
1.25	1.28			13.25		19.25	1.45
1.33	1.29		9.66	13.33	2.62	19.33	1.45
1.42		7.42		13.42		19.42	1.44
1.50	1.32			13.50		19.50	
1.58	1.33			13.58		19.58	
1.67	1.35			13.67		19.67	
1.75	1.36			13.75		19.75	
1.83		7.83		13.83		19.83	
1.92	1.39			13.92		19.92	1.39
2.00	1.41			14.00		20.00	1.38
2.08	1.42			14.08		20.08	
2.17	1.44			14.17		20.17	
2.25	1.46			14.25		20.25	
2.33	1.47			14.33		20.33	1.35
2.42	1.49			14.42		20.42	
2.50	1.51			14.50		20.50	
2.58	1.53			14.58		20.58	
2.67		8.67		14.67		20.67	
2.75	1.57			14.75		20.75	1.32
2.83		8.83		14.83		20.83	1.31
2.92		8.92		14.92		20.92	1.30
3.00		9.00		15.00		21.00	1.30
3.08	1.65			15.08		21.08	1.29
3.17	1.68	'		15.17		21.17	1.28
3.25	1.70			15.25		21.25	1.28
3.33	1.72			15.33		21.33	1.27
3.42	1.75			15.42		21.42	1.27
3.50	1.78			15.50		21.50	1.26
3.58		9.58		15.58		21.58	1.25
3.67		9.67		15.67		21.67	1.25
3.75		9.75		15.75		21.75	1.24
3.83		9.83		15.83		21.83	1.24
3.92		9.92		15.92		21.92	1.23
4.00		10.00		16.00		22.00	1.22
4.08		10.08		16.08		22.08	1.22
4.17		10.17		16.17		22.17	1.21
4.25		10.25		16.25		22.25	1.21
4.33		10.33		16.33		22.33	1.20
4.42		10.42		16.42		22.42	1.20
4.50	4.10	10.50	4./0	16.50	1.01	22.50	1.19

```
4.58
                   4.66 | 16.58
                                 1.80 | 22.58
      2.23 | 10.58
                                               1.19
4.67
      2.27 | 10.67
                   4.54 | 16.67
                                 1.79 | 22.67
                                               1.18
4.75
      2.32 | 10.75
                   4.43 | 16.75
                                 1.77 | 22.75
                                               1.18
4.83
      2.37 | 10.83
                   4.33 | 16.83
                                 1.76 | 22.83
                                               1.17
                                 1.75 | 22.92
4.92
      2.42 | 10.92
                   4.23 | 16.92
                                               1.16
5.00
      2.48 | 11.00
                   4.14 | 17.00
                                 1.73 | 23.00
                                               1.16
5.08
      2.54 | 11.08
                   4.05 | 17.08
                                 1.72 | 23.08
                                               1.15
5.17
      2.60 | 11.17
                    3.96 | 17.17
                                 1.71 | 23.17
                                               1.15
5.25
      2.67 | 11.25
                   3.88 | 17.25
                                 1.70 | 23.25
                                               1.14
5.33
      2.74 | 11.33
                   3.80 | 17.33
                                 1.68 | 23.33
                                               1.14
5.42
     2.81 | 11.42
                   3.73 | 17.42
                                 1.67 | 23.42
                                               1.14
5.50
      2.89 | 11.50
                   3.66 | 17.50
                                 1.66 | 23.50
                                               1.13
5.58
      2.97 | 11.58
                   3.59 | 17.58
                                 1.65 | 23.58
                                               1.13
5.67
      3.06 | 11.67
                   3.53 | 17.67
                                 1.64 | 23.67
                                               1.12
5.75
      3.16 | 11.75 | 3.46 | 17.75
                                1.63 | 23.75
                                              1.12
5.83
      3.26 | 11.83 | 3.40 | 17.83
                                 1.62 | 23.83
                                               1.11
5.92 3.37 | 11.92 3.35 | 17.92
                                1.61 | 23.92
                                              1.11
```

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IMPERVIOUS PERVIOUS (i)

0.54 0.01 Surface Area (ha)= Dep. Storage (mm)=1.00 1.50 Average Slope (%)= 1.00 2.00 Length (m)=60.55 40.00 Mannings n 0.013 0.250

242.53 Max.Eff.Inten.(mm/hr)= 127.71 over (min) 5.00 5.00 Storage Coeff. (min)= 1.33 (ii) 2.11 (ii) Unit Hyd. Tpeak (min)= 5.00 5.00 Unit Hyd. peak (cms)= 0.33 0.31 \*TOTALS\* PEAK FLOW 0.36 0.00 (cms)=0.364 (iii) TIME TO PEAK (hrs)= 8.00 8.00 8.00 RUNOFF VOLUME (mm)= 118.37 85.40 118.04 TOTAL RAINFALL (mm)= 119.37 119.37 119.37

\*\*\*\*\* WARNING: STORAGE COEFF. IS SMALLER THAN TIME STEP!

0.99

0.72

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES: CN\* = 85.0 Ia = Dep. Storage (Above)
  - (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

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| RESERVOIR( 0013)| OVERFLOW IS OFF

RUNOFF COEFFICIENT =

0.99

| IN = 2 - - > OUT = 1 || DT= 5.0 min | OUTFLOW STORAGE | OUTFLOW STORAGE (cms) (ha.m.) | (cms) (ha.m.) 0.0000 0.0000 | 0.1170 0.0078 0.0350 0.0016 | 0.1290 0.0094 0.0660 0.0031 | 0.1410 0.0109 0.0860 0.0047 | 0.1510 0.0125 0.1020 0.0062 | 0.1530 0.0127 AREA OPEAK TPEAK R.V. (ha) (cms) (hrs) (mm) INFLOW: ID= 2 (0003) 0.550 0.364 8.00 118.04 OUTFLOW: ID= 1 ( 0013) 0.550 0.143 8.08 118.03 PEAK FLOW REDUCTION [Qout/Qin](%)= 39.34 TIME SHIFT OF PEAK FLOW (min)= 5.00 (ha.m.) = 0.0114MAXIMUM STORAGE USED **FINISH** 



# **APPENDIX C**Wastewater Servicing



## WASTEWATER DEMAND CALCULATIONS

Project Name: 1315 Silver Spear Road Prepared by: K.V. Municipality: City of Mississauga Checked by: N.P. **Project No.:** 23-314 Last Revised: 13-Nov-23

## **Proposed Apartment**

### Residential

	# of Units	PPU
Small Apartments - Studio, 1B, 1B+D (<750 sq ft) =	144	1.6
Large Apartment - 2B and 3B (>750 sq ft) =	35	3

Total Units = 179 Population = 336

persons

 $(1+14/(4+P^{0.5})$ Harmon Peak Factor for Site, Me = 4.06

Unit Sewage Flow = 302.8 L/person/day

Domestic Sewage Flow = 4.78

### **Existing Apartment**

### Residential

	# of Units	PPU
Small Apartments - Studio, 1B, 1B+D (<750 sq ft) =	9	1.6
Large Apartment - 2B and 3B (>750 sq ft) =	84	3

Total Units = 93 Population = 267

(1+14/(4+P<sup>0.5</sup>)

Harmon Peak Factor for Site, Me = 4.10

> Unit Sewage Flow = 302.8 L/person/day Domestic Sewage Flow = 3.84 L/s

persons

Site Area = 0.85 ha Infiltration Allowance = 0.20 L/s/ha Total Infiltration = 0.17 L/s

Total wastewater flow = 8.78 L/s



# APPENDIX D Water Servicing



#### WATER DEMAND CALCULATIONS

Project Name:1315 Silver Spear RoadPrepared by: K.V.Municipality:City of MississaugaChecked by: N.P.Project No.:23-314WLast Revised:13-Nov-23

Fire Flow Calculations
Proposed Conditions

Based on the Water Supply for Public Fire Protection, 1999 by Fire Underwriters Survey

1 Estimate of Fire Flow

F = 220 C (A)1/2

F = Fire Flow (L/min)

C = Construction Type Coefficient

= 0.6 ,for fire-resistive construction (fully protected frame, floors, roof)

A = Total flow area (m<sup>2</sup>)

 If vertical openings and exterior vertical communications are properly protected (one hour rating),

Largest Floor + 25% of two immediately adjoining floors

### **Proposed 9-storey Building**

Floor	Area (m <sup>2</sup> )	%
	1,298	25%
Ground Floor	1,298	100%
	1,298	25%

= 1946 m<sup>2</sup>

F = 5823 L/min

= 6000 L/min, rounded to the nearest 1000 L/min

2 Occupancy Reduction

15% for low hazard occupancies (apartments)

F = 5100 L/min

3 Sprinkler Reduction

30% for adequately designed sprinkler protection

conforming to NFPA 13 and other NFPA sprinkler standards

3570 L/min

4 Separation Charge

Direction	Separation (m)	Charge
North	55.0	FALSE
West	13.0	15%
South	6.0	20%
East	8.0	20%

Total Charge = 55%

F =

F = 2805 L/min

Required Fire Flow

F = 6375 L/min

6000 L/min, rounded to the nearest 1000 L/min

Fire Flow Demand (Porosed Development) = 100.0 L/s = 1585 USGPM



### WATER DEMAND CALCULATIONS

Project Name:1315 Silver Spear RoadPrepared by: K.V.Municipality:City of MississaugaChecked by: N.P.Project No.:23-314WLast Revised:13-Nov-23

**Existing Conditions** 

Based on the Water Supply for Public Fire Protection, 1999 by Fire Underwriters Survey

1 Estimate of Fire Flow

F = 220 C (A)1/2

F = Fire Flow (L/min)

C = Construction Type Coefficient

= 0.6 ,for fire-resistive construction (fully protected frame, floors, roof)

A = Total flow area (m<sup>2</sup>)

= If vertical openings and exterior vertical communications are properly

### **Existing 8-storey Building**

Floor	Area (m <sup>2</sup> )	%
	1,134	25%
Ground Floor	1,134	100%
	1,134	25%

= 1701 m<sup>2</sup>

F = 5444 L/min

= 5000 L/min, rounded to the nearest 1000 L/min

2 Occupancy Reduction

15% for low hazard occupancies (apartments)

F = 4250 L/min

3 Sprinkler Reduction

30% for adequately designed sprinkler protection

conforming to NFPA 13 and other NFPA sprinkler

standards

F = 2975 L/min

#### 4 Separation Charge

Direction	Separation (m)	Charge
North	6.0	20%
West	33.0	5%
South	38.0	5%
East	20.0	15%

Total Charge = 45%

F = 1913 L/min

Required Fire Flow

F = 4888 L/min

= 5000 L/min, rounded to the nearest 1000 L/min

Fire Flow Demand (Existing Development) =	83.3 L/s
=	1321 USGPM
-	

Total Fire Flow Demand = 183.3 L/s = 2906 USGPM



### WATER DEMAND CALCULATIONS

Project Name: 1315 Silver Spear Road Prepared by: K.V. Checked by: N.P. Municipality: City of Mississauga Project No.: 23-314W Last Revised: 13-Nov-23

**Domestic Flow Calculations** 

**Proposed Condtions** 

Residential Population = 336 persons, from Sanitary Calculations

Residential Average Day Demand = 280 L/person/day, from Region of Peel design criteria

1.1 L/s

Use Peaking Factor the Greater of

Residential Max Daily Demand PF = 2, from Region of Peel design criteria

Max Daily Demand = 2.18 L/s

Max Peak Hour PF = 3 , from Region of Peel design criteria

Max Peak Hour Demand = 3.27 L/s

Domestic Flow Demand (Proposed Development) =	3.27 L/s
` ` ` ` · · · · · · · · · · · · · · · ·	52 USGPM

**Existing Condtions** 

Residential Population = 267 persons, from Sanitary Calculations

280 L/person/day, from Region of Peel design criteria Residential Average Day Demand =

0.9 L/s

Use Peaking Factor the Greater of

Residential Max Daily Demand PF = 2, from Region of Peel design criteria

Max Daily Demand = 1.73 L/s

Max Peak Hour PF = 3, from Region of Peel design criteria

Max Peak Hour Demand = 2.60 L/s

Domestic Flow Demand (Existing Development) =	2.60 L/s
=	41 USGPM

Total Domestic Flow Demand =	5.9 L/s
=	93 USGPM