

**NYX Tannery LP
Functional Servicing and
Stormwater Management Report
51 & 57 Tannery St. and 208 Emby Drive.
Mississauga, ON.**

City File (OPZR - 104636)

April 19, 2024
(Revised July 4, 2024)

GE Project #: 23-904

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1.0 Introduction

1.1 General Information

Greystone Engineering Inc. have been retained by Montcrest Asset Management to prepare a Functional Servicing and Stormwater Management Report for the proposed development at 51 and 57 Tannery Street in the City of Mississauga.

The property is located at the Southeast corner of Tannery Street and Broadway Street with a CPR Rail line to the East, Mullet Creek to the West, Tannery Street to the North and Emby Drive with existing commercial / industrial to the South. Refer to **Figure 1** for site location.

This Functional Servicing and Stormwater Management Report (FSR) has been completed to support the OPA/ZBA and future Site Plan Approval (SPA) applications.

1.2 Objectives

The objectives of this Functional Servicing and Stormwater Management Report are to:

- Confirm the location of existing infrastructure both internal and adjacent to the subject site.
- Evaluate and confirm capacity for sanitary servicing.
- Evaluate and confirm adequate supply and on-site distribution of municipal water to meet domestic and fire flow requirements.
- Provide Stormwater Management design in keeping with the City of Mississauga and Credit Valley Conservation Authority (CVC) requirements.
- Provide on-site retention and re-use of the 5.0mm storm as part of the City of Mississauga SWM design requirements.
- Quantity control of the 2-100 yr post development flows to the 10 yr pre development flow will be required for flows discharging to the City sewer.
- Provide Level 1 quality control with a minimum of 80% TSS removal.
- Implement LID features to the development where feasible.

All the above will be done in accordance with accepted engineering practices.

1.3 Existing Conditions

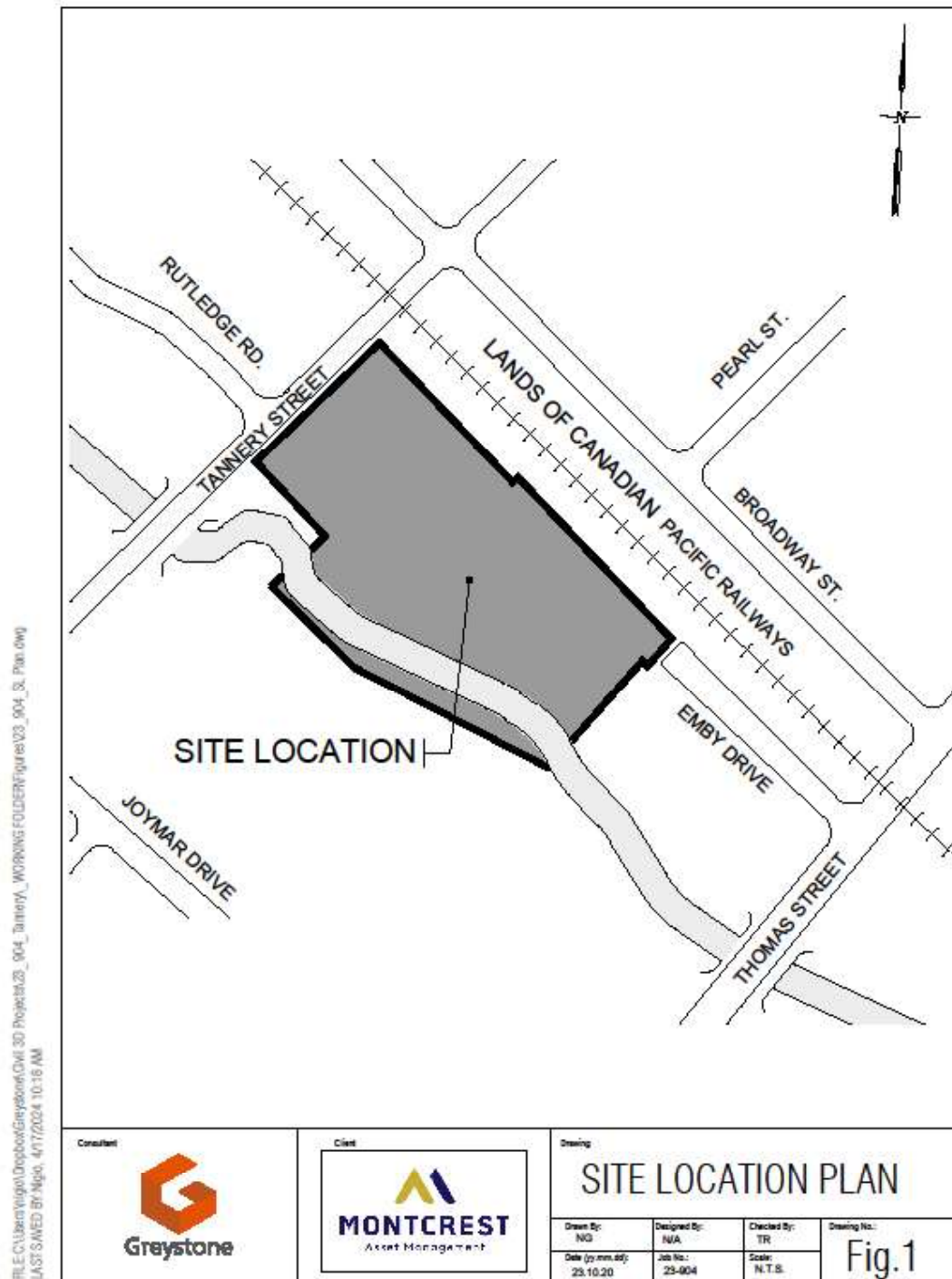
The site is currently a mixed-use development of residential and commercial / industrial. As mentioned above, the site is located at the Southeast corner of Tannery Street and Broadway Street with a CPR Rail line to the East, Mullet Creek to the West, Tannery Street to the North and Emby Drive with existing commercial / industrial to the South. Refer to **Figure 1** for site location.

The site generally drains East to West overland to Mullet Creek. There is an existing 500 mm diameter CSP culvert that bisects the property picking up external drainage from the CPR lands to the East (0.35 ha) and discharging to Mullet Creek. Other than the 500mm CSP, there are no storm systems in place on the site.

Servicing (storm, sanitary and water) are existing within Tannery St. to the North.

Refer to **drawing DR1** and **ESC1** in **Appendix A** for existing drainage details.

Figure 1 Site Location



1.4 Proposed Development

The proposed development will consist of a 14 Storey residential building with 633 units and underground parking. The total site area is 1.85 ha. As part of the development plan there will be a road dedication (0.023 ha) and valley land dedication (0.404 ha) leaving the proposed development area as 1.42 ha. For the purposes of this report, the site development area of 1.42 ha will be used.

The site will be serviced by existing municipal infrastructure for storm, water and sanitary within Tannery Street. Access to the site will be off of Tannery Street.

Refer to **drawing DR1-DR4 in Appendix A** for existing drainage details.

2.0 Sanitary Servicing

2.1 Existing and Proposed Sanitary Sewer Infrastructure

There is an existing 250 mm diameter PVC sanitary sewer at 1.6% slope within Tannery St. and an existing 250 mm sanitary at 2.2% within Emby Drive. The existing Tannery sewer starts at EX MH 6A servicing the existing residential on both the north (Retirement residence at 175 Rutledge St) and south (within the proposed development) sides of Tannery St. We estimate a total sanitary contribution from the existing developments to be **5.2 L/s**.

A sanitary connection is proposed to the Tannery sewer with a new sanitary manhole (MH 01A). This sanitary sewer has a full flow capacity of **73.5 L/s**.

The Region of Peel Design standard 2-9-2 was used to analyze the proposed sanitary flows. Sewage flows are based on 302.8 Litres per capita day (Lpcd). Using the Regions allowance of 302.8 Lpcd, the proposed sanitary flow is estimated as follows:

$633 \text{ units} \times 2.7 \text{ ppu} = 1709.1 \text{ people} \times 302.8 \text{ Lpcd} \times 3.64 \text{ PF} = \mathbf{21.79 \text{ L/s}}$
Infiltration allowance = $1.42 \text{ ha} \times 0.28 \text{ L/s/ha} = 0.40 \text{ L/s}$
Total combined flow = **22.2 L/s**.

This represents approximately 30% of the total capacity of the existing 250 mm sewer.

Refer to **Appendix A, dwg S1** for proposed design and **Appendix B** for sanitary information.

The existing sanitary infrastructure has sufficient capacity to service the proposed development.

3.0 Water Supply and Distribution

3.1 Existing and Proposed Water Infrastructure

There is an existing 12" (300mm) diameter PVC watermain within Tannery Street and an existing 300mm diameter PVC watermain within Emby Drive connecting to the existing 300 mm watermain within Thomas St. The existing watermain within Emby drive services the existing commercial / industrial lands that are part of the proposed redevelopment.

Flow tests were completed by Classic Fire Protection Inc. for both Thomas St. and Tannery St. dated May 10, 2019 and June 15, 2017 respectively. On Thomas St. the existing static water pressure is **75 psi** with an estimated residual flow of **2867 GPM** at **20 psi**. On Tannery St. the existing static water pressure is **62 psi** with an estimated residual flow of **3522 GPM** at **20 psi**. Refer to **Appendix D** for flow test results.

The site will be serviced using the existing 300 mm watermain within Tannery St. using a 200 mm PVC connection per Region of Peel standard 1-8-6. Refer to **Drawing S1** for details.

Property line valves will be added as well as a private hydrant within the site. Private hydrants are proposed with a maximum distance of 45 m to Siamese locations to meet OBC and NFPA requirements.

Using the Fire Underwriters Survey (FUS) for fireflow calculations, the estimated Peak Day Domestic Demand is **166 GPM** and Fire Flow demand for the development is **3386 GPM**. There is sufficient water pressure and volume to provide fire protection and domestic water to the proposed development. Based on the height of the building a booster pump will be required for fire protection.

Refer to **Appendix A, Drawings S1** for the proposed connections. Refer to **Appendix D** for flow test results, water demand calculations and Region of Peels water-wastewater design tables.

4.0 Stormwater Management

4.1 Design Criteria

The site is subject to the stormwater management design criteria outlined in the City of Mississauga development criteria Section 8 – Storm Drainage Design Requirements and the Credit Valley Conservation Authority (CVC) stormwater management design criteria. Stormwater design criteria is as follows:

- Provide on-site storage, reuse and retention of the 5.0mm storm as part of the City of Mississauga and TRCA SWM design requirements for water balance.
- Post to pre quantity control is required for all storm events from the 2 -100 year discharging to Mullett creek per CVC requirements. For stormwater discharging to City sewers, post development flows must be controlled to the 10 year storm ($C = 0.5$.) per the City of Mississauga standards.
- Provide Level 1 Quality control with a minimum of 80% TSS.
- Where feasible, provide low impact development measures (LID).
- Implement erosion and sediment control measures prior to construction to prevent sediment transport and erosion during construction.

4.2 Existing Storm Drainage System

As mentioned in Section 1.3, the site generally drains East to West overland to Mullet Creek. There is an existing 500 mm diameter CSP culvert that bisects the property picking up external drainage from the CPR lands to the East (0.352 ha) and discharging to Mullet Creek. The 100 year external flow is estimated to be 54.1 L/s (Lea Consulting Stormwater Management Brief, March 2021). Other than the 500mm CSP, there are no storm systems in place on the site.

Refer to “Pre Development Drainage Plans” provided in **Appendix A**.

Refer to **drawing DR1** and **ESC1** in **Appendix A** for existing drainage details.

4.3 Proposed Storm Drainage System

The Modified Rational Method (MRM) was used to calculate runoff rates from the site to quantify peak flows and required detention storage. Intensity-Duration-

Frequency curves from the City of Mississauga were used to simulate rainfall data. SWMHYMO was used to generate flows and storage requirements for the Regional storm.

Post development drainage for the site will be directed to a stormwater vault located within the building at the Northwest corner of the site. Refer to the Post Development Drainage Plan provided in **Appendix A**. The existing CPR external flows will be redirected to the existing 1050 mm diameter concrete storm sewer at 0.5% on Tannery St. which discharges to Mullet Creek approximately 45m upstream of its current discharge location.

The site has an allowable release rate of **195.61 L/s** being the 10 year design storm at a runoff coefficient of C=0.50.

Table 1 below outlines the site statistics and runoff coefficients used in the stormwater analysis. **Table 2** below outlines post development flows as well as storage requirements based on the 10 year design storm at a runoff coefficient of C=0.50.

Table 1: Site Statistics

Location	Current Area (ha)	Proposed Area (ha)
Building Area C=0.90	0.28	0.47
Landscaped Area C=0.25	0	0.38
Impervious Area C=0.90	1.14	0.57
Total Area:	1.42	1.42
Runoff Coeff:	0.90	0.73

Table 2: Peak Post Development Flows and Required Storage

Site	Q (L/s) 2 yr	Q (L/s) 5 yr	Q (L/s) 10 yr	Q (L/s) 25 yr	Q (L/s) 50 yr	Q (L/s) 100 yr	Q (L/s) Reg
Post Dev't Flow	172	231	284	359	407	454	206
Storage Required to meet 10 yr (m ³)	0	32	79.6	147	191	233	113

Refer to **Appendix C** for calculations.

The site will control the 100 yr post development flows to the 10 year storm at a runoff coefficient of $C=0.5$, $Q= 195.6 \text{ L/s}$. Storage requirements are shown above in Table 2. During the 100 yr storm event approximately **233 m³** of storage is required.

Site drainage will be directed to a stormwater vault with (17.0m x 10.5 m x 1.4 m deep) to provide a minimum of **250 m³** of storage at elevation . The invert of the storm inlet will be set to 153.67 m with a tank bottom elevation of 152.27 m. Stormwater will be pumped out at the 10 yr allowable release rate of 195.6 L/s with a backup pump system.

Refer to SWM calculations in **Appendix C**

An emergency overland flow pipe and DICB will be provided on the West side of the vault in case of pump failure on both pumps or power failure.

The 5.0 mm site water balance will be provided through irrigation reuse in the proposed stormwater vault between elevation 152.27 m and 152.67 m to meet the required 5.0 mm reuse volume of **71 m³** (1.42 ha x 5.0mm).

As part of the LID initiative, the site has been designed with larger than typical landscaped areas around the site. A combination of grassed areas, grassed swales and permeable pavers in landscaped areas to promote infiltration have been incorporated into the design. As mentioned above, the bottom 0.4 m of the SWM Vault will be used for irrigation of the landscaped areas.

Level 1 quality control will be provided using a Stormceptor EF04 providing 92% TSS removal.

Erosion and Sediment Controls will be implemented prior to construction as outlined on **Drawing ESC1, Appendix A**, consisting of Silt Fence, Mud mat at construction entrance and siltation control devices on existing CB's. These interim measures will ensure that all sediment laden runoff is maintained within the site and not transported downstream.

Refer to **Appendix A (Drawings S1/G1)** for proposed design and **Appendix C** for stormwater design calculations.

5.0 Conclusions and Recommendations

The servicing analysis provided within this report is summarized as follows:

- A sanitary connection is proposed to the Tannery sewer with a new sanitary manhole (MH 01A). This sanitary sewer has a full flow capacity of **73.5 L/s**. The estimated sanitary flows from the proposed development is **22.2 L/s**.
- Flow tests were completed by Classic Fire Protection Inc. for both Thomas St. and Tannery St. On Thomas St. the existing static water pressure is **75 psi** with an estimated residual flow of **2867 GPM** at **20 psi**. On Tannery St. the existing static water pressure is **62 psi** with an estimated residual flow of **3522 GPM** at **20 psi**.
- The site will be serviced by a 200 mm watermain to the 300 mm watermain within Tannery St. The fire flow demand is estimated at **3386 GPM**. There is sufficient water pressure and volume to provide fire protection and domestic water to the proposed development.
- A new private hydrant will be provided within 45 m of proposed Siamese locations to meet OBC and NFPA requirements.
- The 100 yr post development flow of **454 L/s** will be controlled to the allowable 10 yr storm at C=0.5 of **195.6 L/s** requiring approximately **233m³** of storage.
- The 5.0 mm site water balance will be provided through irrigation reuse in the proposed stormwater vault between elevation 152.27 m and 152.67 m to meet the required 5.0 mm reuse volume of **71 m³**
- Level 1 quality control will be provided using a Stormceptor EF04 providing 92% TSS removal.
- Erosion and Sediment Controls will be implemented prior to construction as outlined on **Drawing ESC1**.

Functional Servicing and Stormwater Management Report
July 4, 2024

This Functional Servicing and Stormwater Management Report has been submitted in support of the 51 and 57 Tannery Street OPA/ZBA and SPA applications. The proposed development can be completed with the servicing designs outlined in this report.

Prepared by:

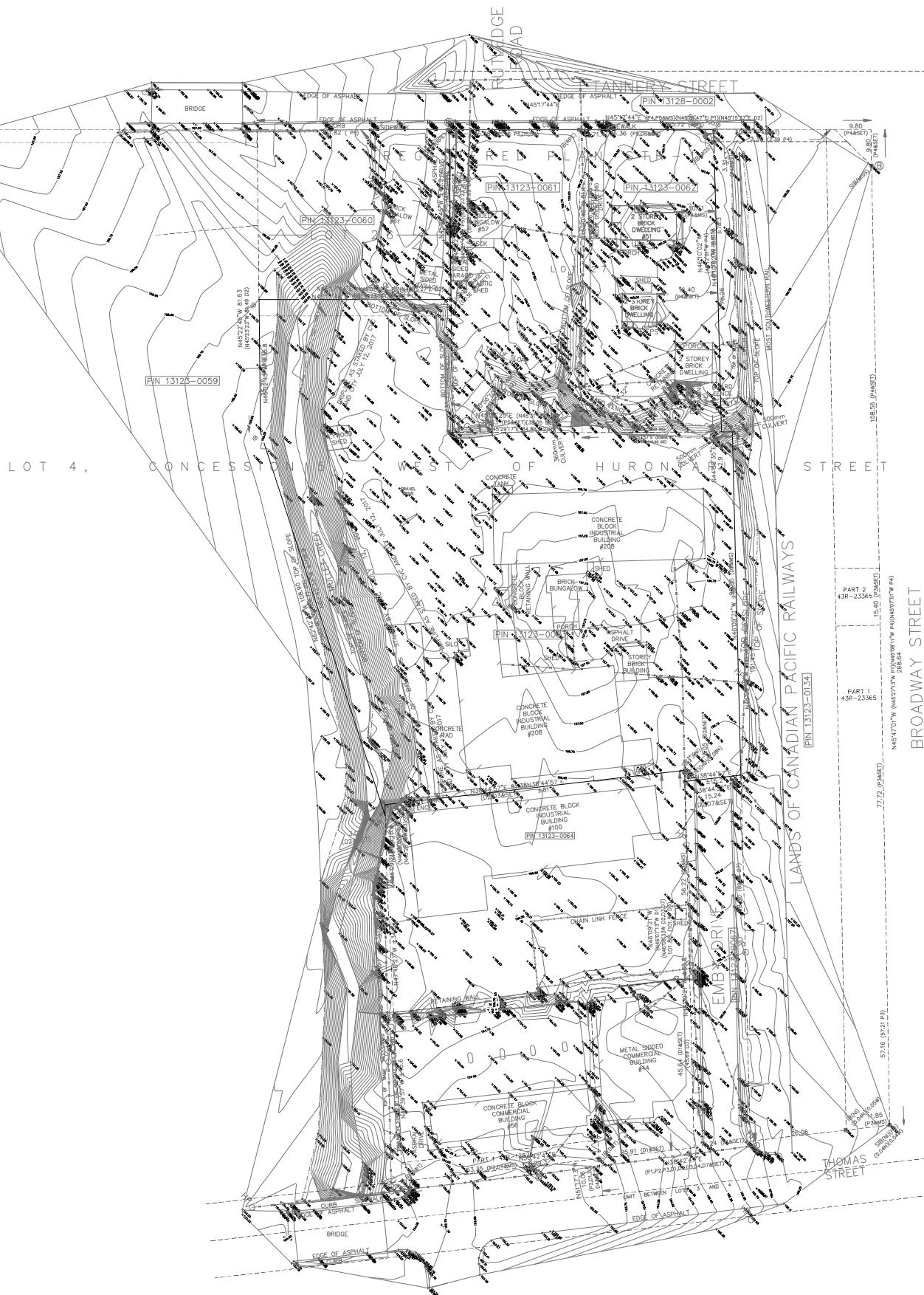
Greystone Engineering Inc.

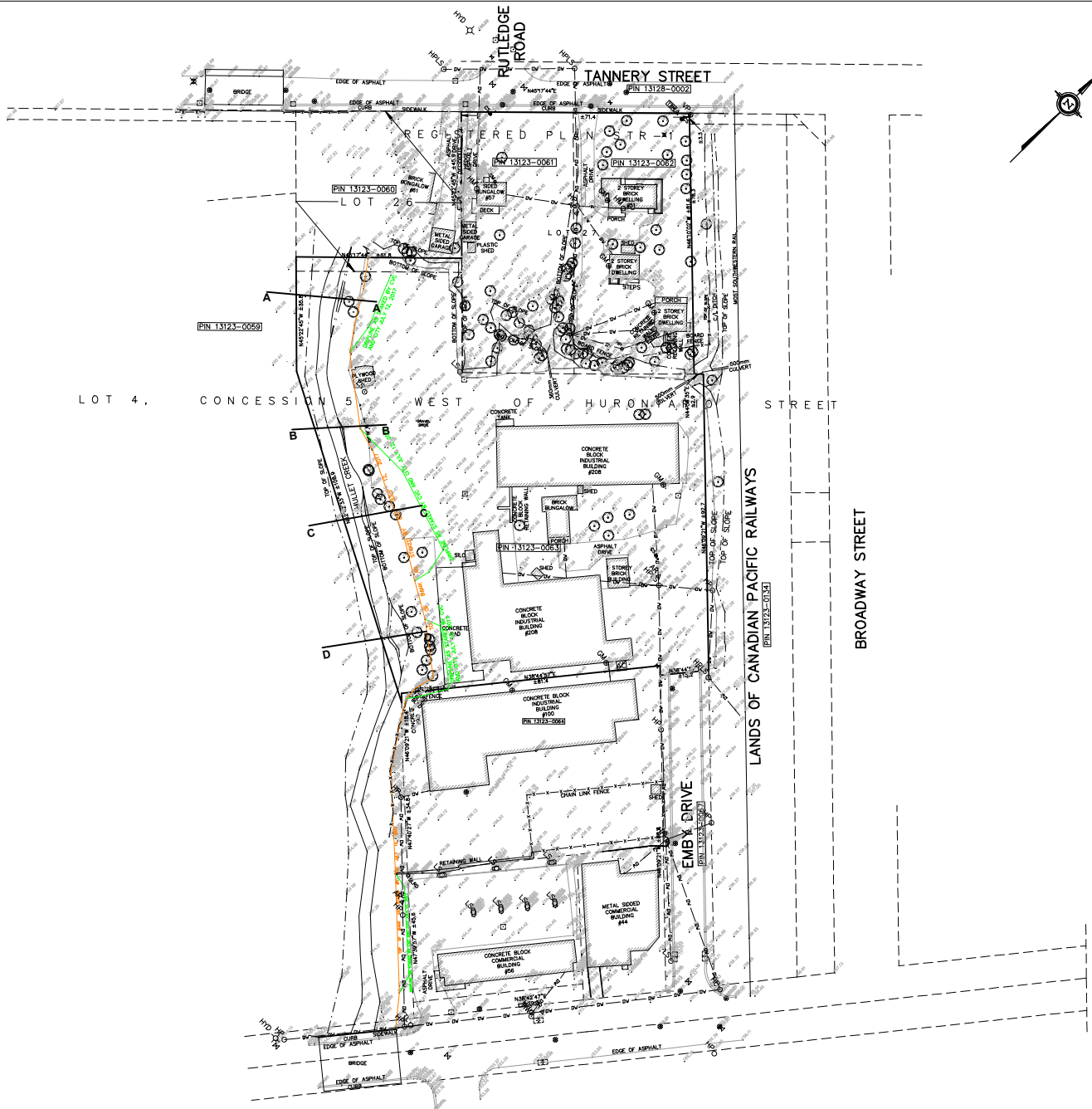


Todd Ricketts, P.Eng.
Principal.

Appendix A

Proposed Development and Existing Information





NOTES

TOPOGRAPHIC INFORMATION

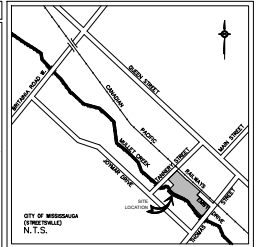
TOPOGRAPHIC INFORMATION MEASURED 19 MAY 2017. BOUNDARY IS APPROXIMATE. THIS IS NOT A PLAN OF SURVEY.

TEMPORARY BENCHMARK

ELEVATION 159.56

CUT CROSS ON THE SIDEWALK OPPOSITE #51 TANNERY STREET. CUT CROSS IS LOCATED 18.1m SOUTHWESTERLY FROM THE MOST WESTERLY RAIL OF CANADIAN PACIFIC RAILWAYS LINE, 4.3m SOUTHWESTERLY FROM THE GAS VENT PIPE AND 21.2m NORTHEASTERLY FROM THE WATER VALVE IN TANNERY STREET.

The location and extent of all existing utilities are not necessarily shown on this plan, and where shown, are to be considered approximate only. All Contractors shall inform themselves of the exact location and extent of all existing services prior to the start of construction, and shall assume all liabilities for damage to them or delays resulting from their actual extent and location.



LEGEND

TEMPORARY BENCHMARK
EX. GAS METER
EX. GAS VENT PIPE
EX. AIR CONDITIONER
EX. ANCHOR
EX. HYDRO METER
EX. UTILITY POLE
EX. HAND WELL
EX. UTILITY POLE / LIGHT STANDARD
EX. LIGHT STANDARD
EX. TRAFFIC LIGHT
EX. CATCH BASIN
EX. MANHOLE
EX. CURB STOP
EX. FIRE HYDRANT
EX. WATER VALVE
EX. MONITORING WELL
EX. BOLLARD
EX. SIGN
EX. TREE
EX. OVERHEAD WIRES

NO.	DATE	ADD WATERCOURSE CROSS SECTIONS
1	23 JAN 2019	ADD WATERCOURSE CROSS SECTIONS
2	18 JUL 2017	DATE ISSUED
3	18 JUL 2017	DATE ISSUED
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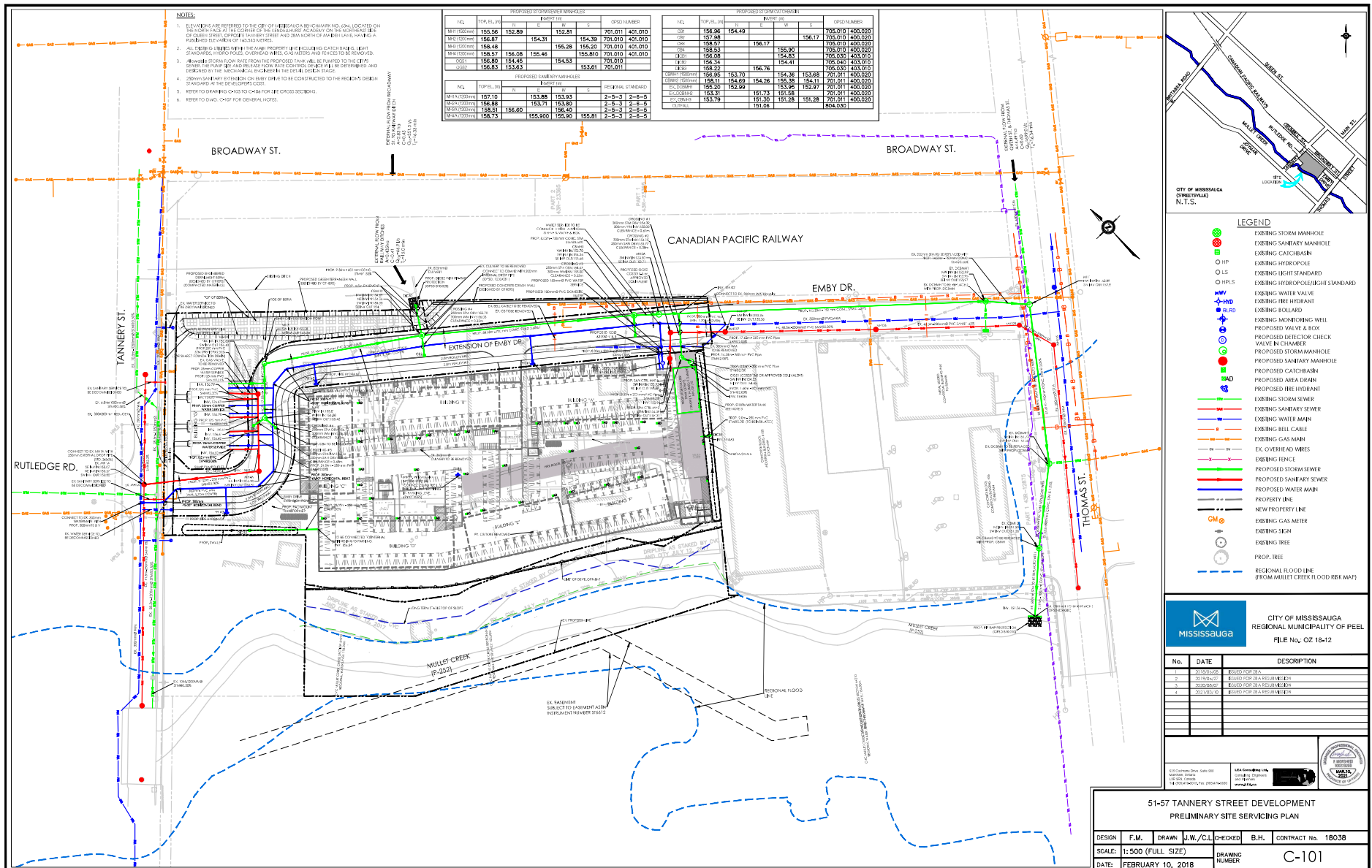
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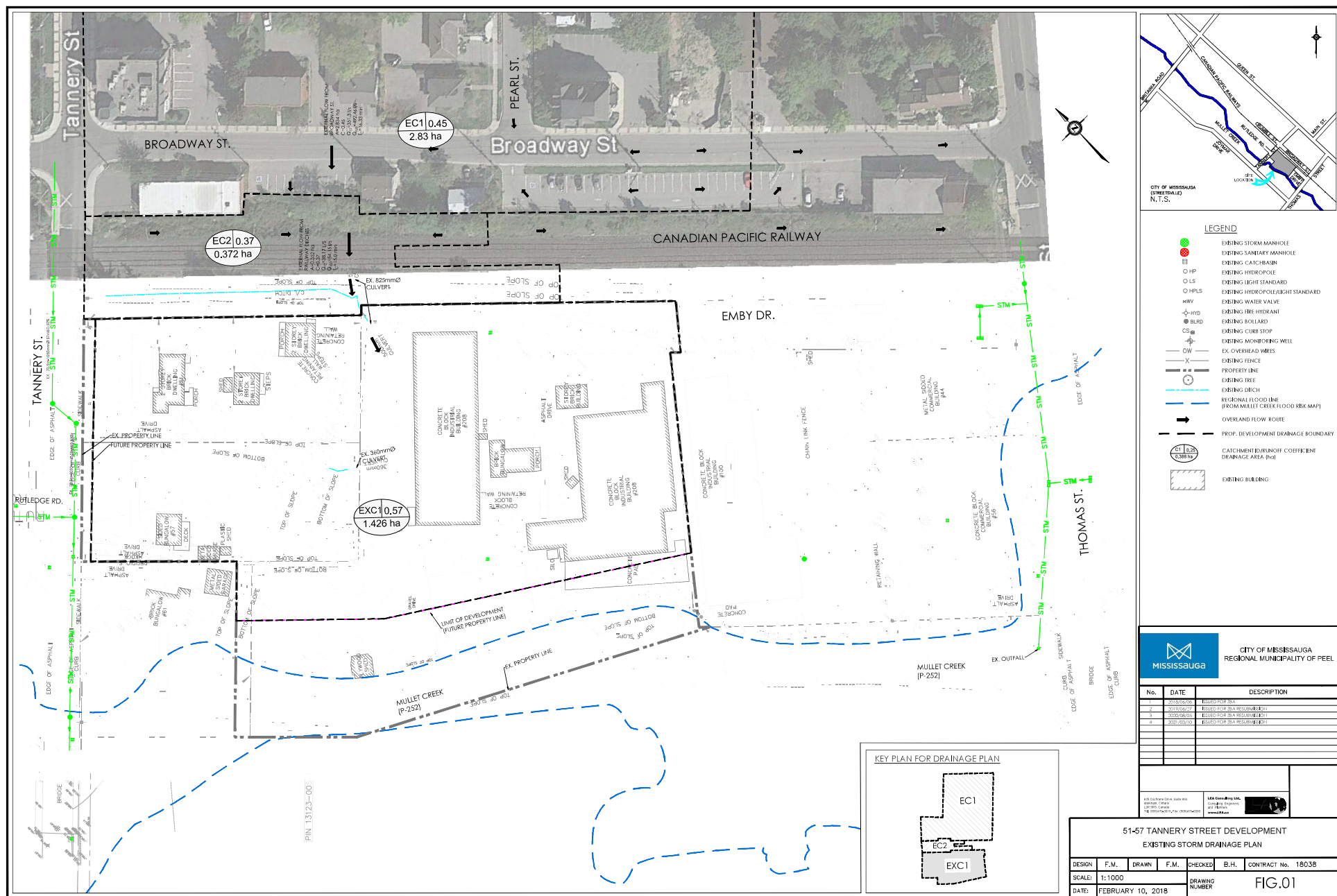
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TORONTO, ON

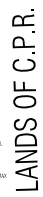
FIDDES CLIPSHAM INC.
Consulting Engineering & Land Surveying
10 Macmillan Road Suite 101, Mississauga, Ontario L4X 1L6
905.877.2211 info@fiddesclipsham.com fiddesclipsham.com

TOPOGRAPHICAL PLAN
LOT 27 AND PART LOT 26 REGISTERED PLAN STR-1 AND PART OF EAST HALF LOT 4 CONCESSION 5 W.H.S. (TORONTO)
CITY OF MISSISSAUGA
REGIONAL MUNICIPALITY OF PEEL

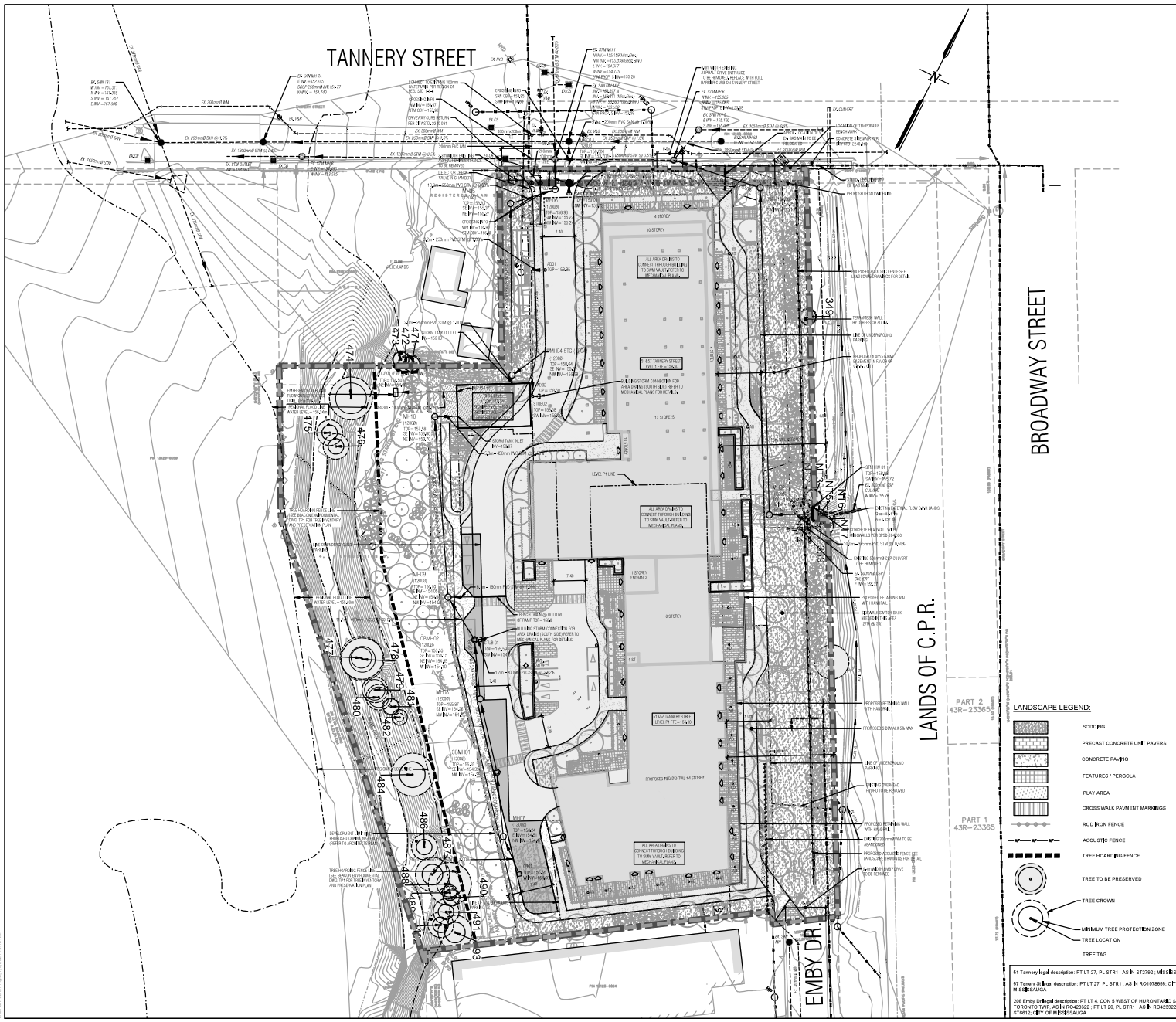
PROJECT No. 17-5362 **DRAWING No.** T-1







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GENERAL NOTES:

1. ALL WORK SHALL BE CARRIED OUT IN COMPLIANCE WITH THE APPLICABLE HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS.
2. ALL THE CONSTRUCTION WORK FOR THE PROJECT SHALL COMPLY WITH THE STANDARD DRAWINGS AND SPECIFICATIONS OF THE CITY OF MISSISSAUGA AND THE STANDARD PROGRAM, STANDARDS AND SPECIFICATIONS.
3. THE CONTRACTOR IS ADVISED THAT WORKS BY OTHERS MAY BE Ongoing DURING THE PERIOD OF THIS CONTRACT. THE CONTRACTOR SHALL COORDINATE CONSTRUCTION ACTIVITIES WITH ALL OTHER CONTRACTORS AND PREVENT CONSTRUCTION CONFLICTS.
4. THE INFORMATION SHOWN FOR EXISTING UTILITIES WAS PROVIDED BY THE CONTRACTOR. THE CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING ALL UTILITIES DURING CONSTRUCTION. ALL EXISTING UTILITIES MUST BE LOCATED AND SPECIFICALLY IDENTIFIED TO THE COMMENCEMENT OF WORK. ANY VARIANCE IS TO BE IMMEDIATELY REPORTED TO THE ENGINEER. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE ENGINEER TO CONFIRM UTILITY LOCATIONS AND NOTIFY THE ENGINEER OF ANY CONFLICT PRIOR TO CONSTRUCTION. IT IS THE CONTRACTOR'S RESPONSIBILITY.
5. ROAD OCCUPANCY PERMITS MUST BE OBTAINED 48 HOURS PRIOR TO COMMENCING ANY WORKS WITHIN THE MUNICIPAL ROAD ALLOCATIONS.

STORM AND SANITARY:

1. MANHOLE SHALL BE AS PER OPD 10110 AND OPD 10111. FRAMES AND COVERS SHALL BE AS PER OPD 10110. SAFETY PLATFORMS TO BE RETAINED AS PER REGION OF PEEL STANDARDS 10110 WHERE DEPTH EXCEEDS 1.8M.
2. SINGLE CATCH BASIN SHALL BE AS PER OPD 10110. WHEN FRAMES AND COVERS AS PER OPD 40120. DOUBLE CATCH BASIN SHALL BE AS PER OPD 10110.
3. CONCRETE PIPE SEWER BEDDING SHALL BE AS PER OPD 10110 AND OPD 10111. SEWER BEDDING SHALL BE AS PER OPD 10110. TO BE CORRECTED TO TOP OF SEWER, NATIVE BACKFILL TO BE CORRECTED TO TOP OF SEWER, NATIVE BACKFILL TO BE CORRECTED TO TOP OF SEWER, NATIVE BACKFILL TO BE CORRECTED TO TOP OF SEWER.
4. ALL STORM SEWER PIPES UP TO 400MM SHALL BE PVC 10110 ON APPROVED EARTH. ALL STORM SEWER PIPES 400MM AND LARGER SHALL BE CONCRETE 10110. ALL STORM SEWER PIPES SHALL BE REINFORCED CONCRETE AS SPECIFIED (10110, 10111, 10112 OR LATEST AMENDMENT) UNLESS OTHERWISE SPECIFIED.
5. ALL SANITARY PVC SEWER PIPES SHALL BE 10110. ALL SANITARY PVC SEWER PIPES SHALL BE 10110. ALL SANITARY PVC SEWER PIPES SHALL BE 10110. ALL SANITARY PVC SEWER PIPES SHALL BE 10110.
6. ALL MANHOLE AND CATCH BASIN EXCAVATIONS TO BE BACKFILLED WITH GRANULAR MATERIAL, COMPACTED TO 90% STANDARD PROCTOR DENSITY.
7. ALL CATCH BASIN AND CATCH BASIN MANHOLES ARE TO BE LOCATED SUBMITTANT TREATMENT AS PER DETAIL ON DRAWING 10110.
8. ALL RISING CONNECTIONS TO MATCH THE INVERT OF THE CATCH BASIN LEAD TO THE SPRING OF THE STORM MAIN, CONFORMING DETAIL THE CATCH BASIN LEAD AT A MAXIMUM 45° AND DROP INTO 10110.
9. UNLESS NOTED OTHERWISE, CATCH BASIN SHALL BE 10110 AT 10110. UNLESS NOTED OTHERWISE, CATCH BASIN SHALL BE 10110 AT 10110.
10. THE CONTRACTOR IS TO PROVIDE CITY CAMERA INSPECTIONS OF ALL SANITARY AND STORM SEWERS INCLUDING (10110, 10111, 10112 OR LATEST AMENDMENT) IN A FORMAT SATISFACTORY TO THE ENGINEER. ALL SEWERS ARE TO BE FLUSHED PRIOR TO CAMERA INSPECTIONS.
11. THE CONTRACTOR IS TO VERIFY PIPE SIZE AND INVERT PRIOR TO CONSTRUCTION.

WATERMANS' REGION OF PEEL NOTES:

1. WATERMANS SHALL HAVE A MINIMUM VERTICAL CLEARANCE OF 300MM OVER AND UNDER SEWERS AND ALL OTHER UTILITIES BENEATH THEM.
2. HYDRANT AND VALVE SET TO REGION STANDARD 10110. 10110 AND 10111. 10110 AND 10111. 10110 AND 10111. 10110 AND 10111.
3. PROVIDING FOR FLUSHING WATER LINE PRIOR TO TESTING, ETC. PROVIDING FOR FLUSHING WATER LINE PRIOR TO TESTING, ETC. PROVIDING FOR FLUSHING WATER LINE PRIOR TO TESTING, ETC. PROVIDING FOR FLUSHING WATER LINE PRIOR TO TESTING, ETC.
4. ALL PROPOSED WATER PIPES MUST BE ISOLATED FROM EXISTING MAINS BY OPENING TO ALLOW REPLENISHMENT PRESSURE TESTING AND BACKFLOW PREVENTION.
5. ALL MATERIALS AND CONSTRUCTION METHODS MUST CORRESPOND TO THE CURRENT REGION OF PEEL STANDARDS AND SPECIFICATIONS.
6. WATERMANS AND/OR SERVICE MATERIALS 10110 AND LARGER MUST BE PVC 10110. CONSTRUCTION AS PER 10110. 10110 AND 10111. 10110 AND 10111. 10110 AND 10111.
7. WATERMANS AND/OR WATER SERVICES ARE TO HAVE A MINIMUM COVER OF 10110. 10110 AND 10111. 10110 AND 10111. 10110 AND 10111.
8. WATERMANS TO BE INSTALLED TO GRADES AS SHOWN ON APPROVED PLAN. COPY OF GRADE SHEET MUST BE SUPPLIED TO INSPECTOR PRIOR TO COMMENCEMENT OF WORK, WHERE REQUESTED BY INSPECTOR.
9. ALL LIFE TAPPING AND OPERATION OF REGION WATER VALVES SHALL BE ARRANGED THROUGH THE REGIONAL INSPECTOR ADVISED BY CONTRACTOR THE OPENING AND MAINTENANCE (10110, 10111, 10112 OR LATEST AMENDMENT) IN THE FIELD TO BE ESTABLISHED BY THE CONTRACTOR.
10. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR LOCATED, EXPOSURE, SUPPORTING AND PROTECTING OF ALL UNDERGROUND AND OVERHEAD UTILITIES AND STRUCTURES EXISTING AT THE TIME OF CONSTRUCTION. IN THE AREA OF WORK, WHETHER SHOWN ON THE PLAN OR NOT, AND FOR ALL REPAIRS AND CONSEQUENCES RESULTING FROM DAMAGE TO SAME.
11. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE TO OBTAIN 10110. 10110 AND 10111. 10110 AND 10111. 10110 AND 10111.
12. ALL PROPOSED WATER PIPES MUST BE ISOLATED THROUGH A TEMPORARY CONNECTION THAT ALLOW AN APPROPRIATE DISCONNECTION CONTROL DEVICE, CONFORMANT WITH THE DEGREE OF ISOLATION FOR BACKFLOW PREVENTION OF THE ACTIVE DISTRIBUTION SYSTEM, CONFORMING TO REGION OF PEEL STANDARD 10110 AND 10111.
13. ALL WATER METERS MUST BE INSTALLED IN HEATED AND ACCESSIBLE SPACES.
14. ALL CURB STOPS TO BE 10110 (10110) OFF THE FACE OF THE BUILDING UNLESS OTHERWISE NOTED.

WATERMANS' CONSULTANTS' NOTES:

1. WATERMANS SHALL BE MANUFACTURED TO 10110. 10110 AND 10111. 10110 AND 10111. 10110 AND 10111.
2. WATERMANS SHALL BE MANUFACTURED TO 10110. 10110 AND 10111. 10110 AND 10111. 10110 AND 10111.
3. ALL WATERMANS HORIZONTAL AND VERTICAL BENDS, JOINTS AND PLUGS TO BE MECHANICALLY RESTRAINED. SINGLE BLOCKED MECHANICAL RESTRAINTS MUST BE INSTALLED ON ALL WATERMANS, TIES AND PLUGS AS PER LOCAL MUNICIPAL STANDARDS.
4. ALL HYDRANT FLANGE ELEVATIONS TO BE INSTALLED 10110 ABOVE PROPOSED FINISH GRADE AT HYDRANT.
5. BUILDING SERVICE VALVES TO BE 10110 OFF THE FACE OF THE BUILDING UNLESS OTHERWISE NOTED AND MUST BE RESTRAINED A MINIMUM OF 10110 FROM STUB.
6. ALL WATERMANS SHALL BE HYDROSTATICALLY TESTED IN ACCORDANCE WITH REGION OF PEEL STANDARDS AND SPECIFICATIONS. ALL WATERMANS SHALL BE HYDROSTATICALLY TESTED IN ACCORDANCE WITH REGION OF PEEL STANDARDS AND SPECIFICATIONS.

LANDSCAPE LEGEND:

- SOILING
- PRECAST CONCRETE LINE PAVERS
- CONCRETE PAVING
- FEATURES/PERCOLA
- PLAY AREA
- CROSS WALK PAVEMENT MARKINGS
- ROAD BOUND FENCE
- ACoustic FENCE
- TREE SHIELDING FENCE
- TREE TO BE PRESERVED
- TREE CROWN
- MINIMUM TREE PROTECTION ZONE
- TREE LOCATION
- TREE TAG

KEY PLAN:

LEGEND:

- 1. LIMIT OF CONSTRUCTION
- 2. PROJECT BOUNDARY
- 3. EXPOSED FOUNDATION
- 4. RETAINING WALL
- 5. BUILDING ENTRANCE
- 6. CATCH BASIN
- 7. TRENCH
- 8. HEADWALL
- 9. VALVE AND BOX
- 10. HYDRANT AND BOX
- 11. HYDRANT CONNECTION
- 12. WATER METER
- 13. BACKFLOW PREVENTOR
- 14. SANITARY MANHOLE
- 15. STORM MANHOLE
- 16. CATCH BASIN MANHOLE
- 17. CATCH BASIN DOUBLE CATCH BASIN
- 18. AREA DRAIN
- 19. PROPOSED WATERMAIN
- 20. PROPOSED SANITARY SEWER
- 21. PROPOSED STORM SEWER
- 22. EXISTING SANITARY MANHOLE
- 23. EXISTING CATCH BASIN
- 24. EXISTING SANITARY SEWER
- 25. EXISTING STORM SEWER
- 26. EXISTING WATERMAIN
- 27. EXISTING SLOPES
- 28. PROPOSED SLOPES
- 29. HYDRANT FOR SCALE
- 30. PROPOSED GROUND ELEVATION
- 31. TOP OF CURB ELEVATION
- 32. PROPOSED OVERLAND FLOW ROUTE
- 33. EMBANKMENT BEAM
- 34. EXISTING OVERLAND FLOW ROUTE
- 35. EXISTING CONTOURS
- 36. EXISTING AREA
- 37. PROPOSED HEAVY DUTY ASPHALT

NOT FOR CONSTRUCTION

Greystone Engineering

NYX TANNERY LP.

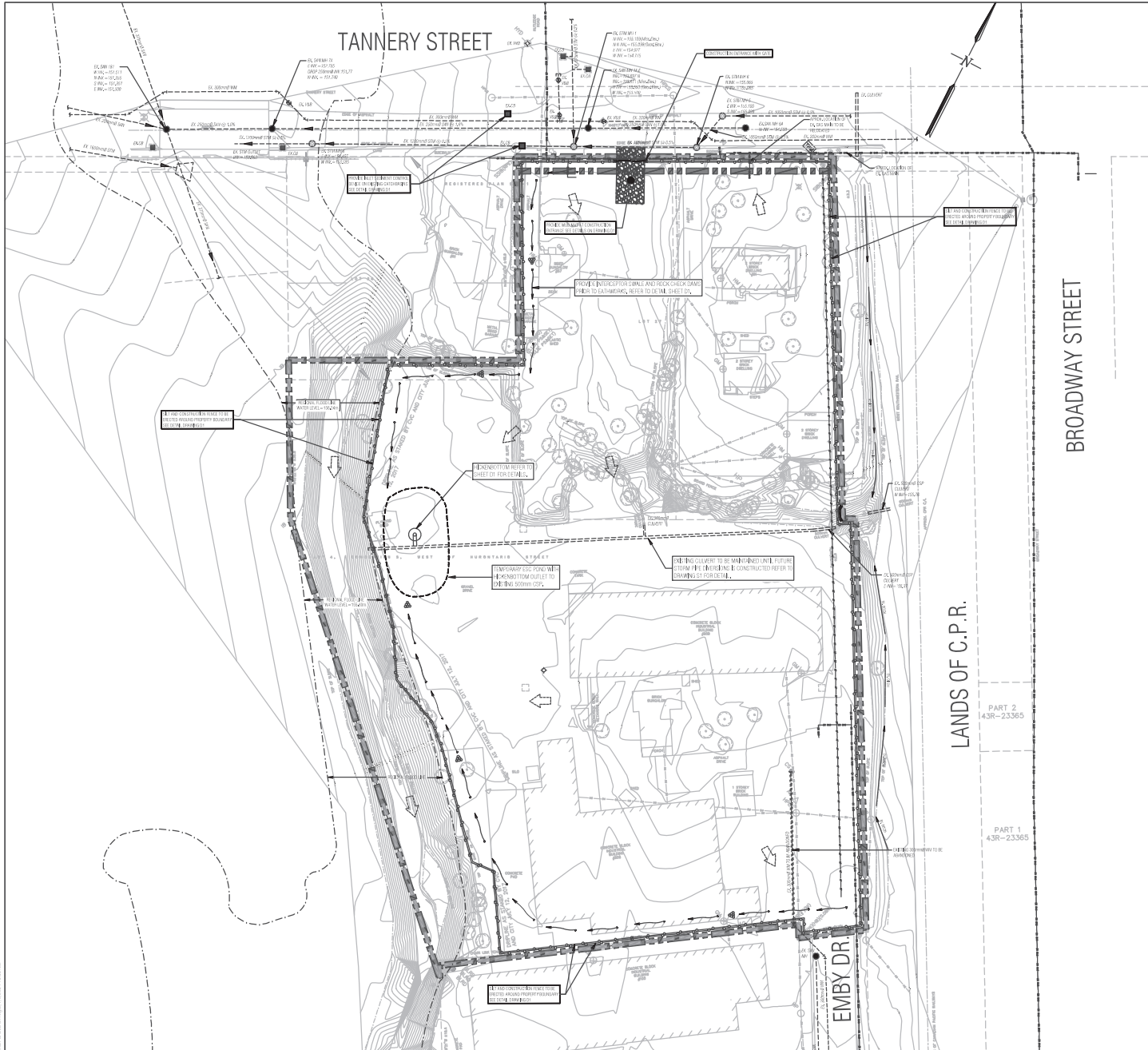
SERVICING PLAN

51 & 57 TANNERY STREET & 208 EMBY DRIVE (E.V. & E.V. & E.V.)

RESIDENTIAL DEVELOPMENT

S1

THIS DOCUMENT IS THE PROPERTY OF GREYSTONE ENGINEERING. IT IS TO BE USED ONLY FOR THE PROJECT AND SITE SPECIFICALLY IDENTIFIED. IT IS NOT TO BE REPRODUCED, COPIED, OR DISTRIBUTED IN ANY MANNER WITHOUT THE WRITTEN PERMISSION OF GREYSTONE ENGINEERING. ANY VIOLATION OF THESE TERMS WILL BE CONSIDERED A BREACH OF CONTRACT AND WILL BE PROSECUTED TO THE FULL EXTENT OF THE LAW.



GENERAL NOTES:

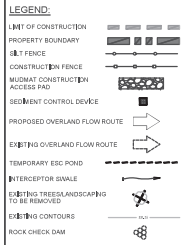
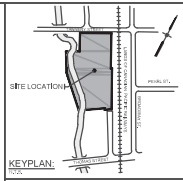
1. ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE INSTALLED AND IN PROPER WORKING ORDER PRIOR TO THE STARTING OF ANY TOPSOIL. THE EXACT LOCATION TO BE DETERMINED BY THE EROSION AND SEDIMENT CONTROL ARCHITECT TO BE APPROVED BY THE CITY.
2. ANY TREES SELECTED BY THE LAND ARCHITECT FOR PROTECTION TO BE PROTECTED BY SHOCK FENCES, LAND ARCHITECT TO INDICATE ANY TREES THAT ARE TO BE TRANSPORTED.
3. ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE ROUTINELY INSPECTED AND MAINTAINED IN PROPER WORKING ORDER AND CLEANED PERIODICALLY.
4. ALL CONSTRUCTION VEHICLES SHALL ENTER AND EXIT THE SITE IN THE APPROVED CONSTRUCTION ACCESS ONLY.
5. ALL TOPSOIL PILES SHALL BE SURROUNDED WITH SEDIMENTATION CONTROL FENCING, ALL PILES WHICH ARE STOCKED FOR MORE THAN 30 DAYS SHALL BE SEED.
6. SEDIMENT WHICH COLLECTS IN THE TEMPORARY SEDIMENT CONTROL FACILITIES WILL BE REMOVED WHEN FACILITY IS HALF FULL.

NOTES:

1. ALL EROSION AND SEDIMENT CONTROL MEASURES TO BE INSTALLED PRIOR TO ANY CONSTRUCTION ACTIVITIES.
2. ADDITIONAL SILT FENCING SHOULD BE AVAILABLE IN CASE OF EXCESSIVE RAINFALL OR EROSION.
3. CONTRACTOR TO STABILIZE THE SITE AS SOON AS POSSIBLE BY RESEEDING AND COVERING WITH EROSION CONTROL MATS. SOIL AREAS, ALL AREAS INCLUDING STOCKPILES WHERE SITE IMPROVEMENTS ARE NOT EXPECTED TO OCCUR IMMEDIATELY SHALL BE REVEGETATED WITH 100% OF TOPSOIL AND HYDROSEEDS.
4. ALL DRAINAGE WORKS REQUIRE EROSION / SEDIMENT CONTROL SATISFACTORY TO THE APPROVAL AGENCIES DURING THE CONSTRUCTION PERIOD AND MUST BE MAINTAINED AND MONITORED ON A REGULAR BASIS TO ENSURE EROSION CONTROL MEASURES REMAIN EFFECTIVE.
5. ALL EROSION AND SEDIMENT CONTROL MEASURES SHALL BE CHECKED AND MAINTAINED ON A REGULAR BASIS AND INSPECTED AFTER EVERY RAINFALL.
6. TEMPORARY EROSION CONTROL MEASURES TO BE REMOVED FROM SITE UPON COMPLETION OF ALL EROSION AND SEDIMENTATION OF EXPOSED SOILS.
7. ALL EXTERNAL AREAS DISTURBED BY CONSTRUCTION ACTIVITIES TO BE RESTORED TO EXISTING CONDITIONS OR BETTER.
8. EMERGENCY CONTACTS:
1000 RICHETTE RD
GREYSTONE ENGINEERING INC
(416) 464-8808
TIM JESSUP
MONTFORT ASSET MANAGEMENT
(847) 864-2554

EROSION CONTROL PLAN:

- STAGE 1: INSTALL EROSION CONTROL MEASURES AT CONSTRUCTION ENTRANCE
- STAGE 2: INSTALL SILT FENCE AND CONSTRUCTION FENCE AROUND SITE
- STAGE 3: INSTALL TEMPORARY SEDIMENT CONTROL DEVICES ON ALL CATCH BASINS AND INLETS
- STAGE 4: PROVIDE REGULAR MAINTENANCE AND REPAIR OF EROSION CONTROL MEASURES DURING CONSTRUCTION ACTIVITIES AND PROVIDE INSPECTION AFTER EACH RAINFALL



NOT FOR CONSTRUCTION

1. 01/24/2019 REVIEW 2403/19 TS

2. 02/14/2019 REVIEW 2403/19 TS



1	01/24/2019 REVIEW	2403/19 TS
2	02/14/2019 REVIEW	2403/19 TS
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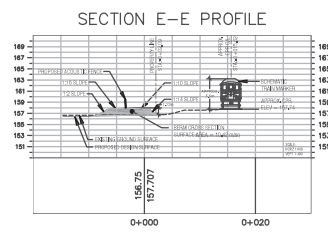
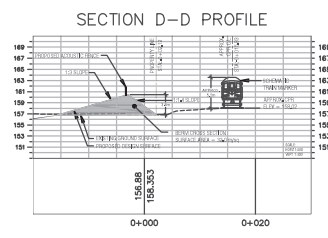
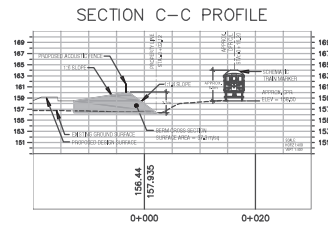
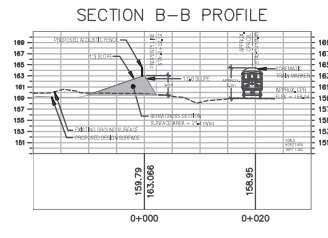
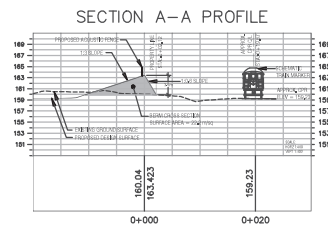
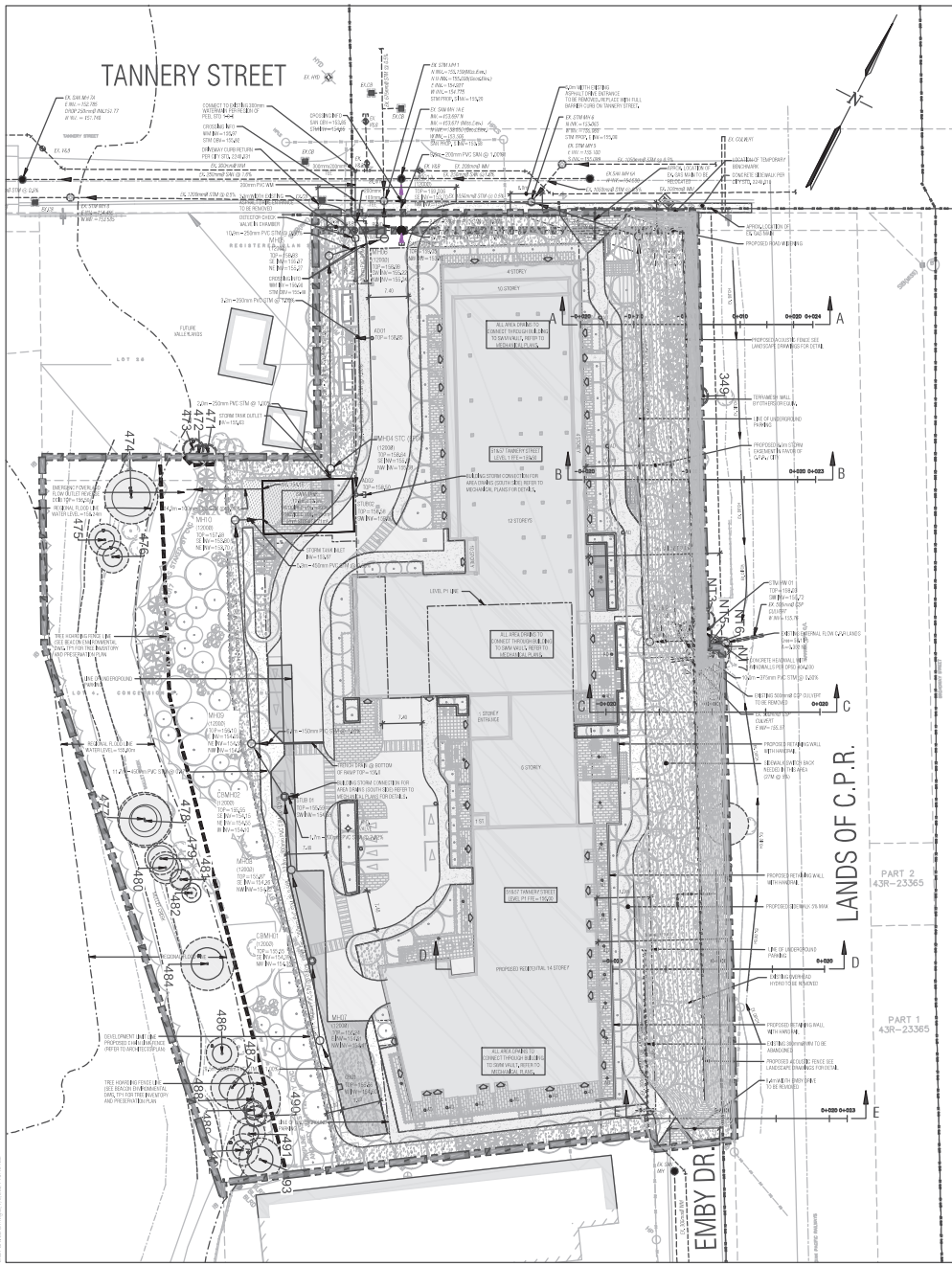
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100 King Street East
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(416) 593-1111
www.greystone.ca

NYX TANNERY LP.

EROSION & SEDIMENT CONTROL PLAN
51 & 57 TANNERY STREET
& 208 EMBY DRIVE
(CITY OF GREYSTONE)
RESIDENTIAL DEVELOPMENT
HURONTARIO, ON

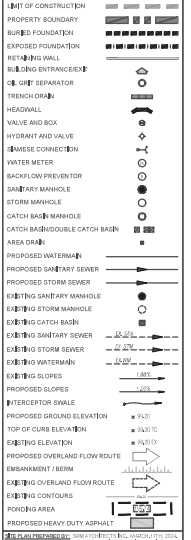
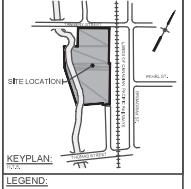
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- GENERAL NOTES:**
- ALL WORK SHALL BE CARRIED OUT IN COMPLIANCE WITH THE APPROPRIATE HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS.
 - ALL THE CONSTRUCTION WORK FOR THIS PROJECT SHALL COMPLY WITH THE STANDARD DRAWINGS AND SPECIFICATIONS OF THE CITY OF MISSISSAUGA AND THE ONTARIO PROVINCIAL STANDARDS AND SPECIFICATIONS.
 - THE CONTRACTOR SHALL ADVISE THAT WORKS BY OTHERS MAY BE ONSITE DURING THE PERIOD OF THE CONTRACT. THE CONTRACTOR SHALL COORDINATE CONSTRUCTION ACTIVITIES WITH ALL OTHER CONTRACTORS AND PREVENT CONSTRUCTION CONFLICTS.
 - THE INFORMATION SHOWN FOR EXISTING UTILITIES WAS PROVIDED BY OTHERS. THE CONTRACTOR IS RESPONSIBLE FOR VERIFYING THE LOCATION AND DEPTH OF ALL UTILITIES PRIOR TO CONSTRUCTION. ALL EXISTING UTILITIES MUST BE LOCATED AND VERIFIED BY EACH UTILITY PRIOR TO THE COMMENCEMENT OF ANY WORK. ANY VARIANCE IS TO BE IMMEDIATELY REPORTED TO THE ENGINEER. THE CITY OF MISSISSAUGA IS NOT RESPONSIBLE FOR THE LOCATION OF UTILITIES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE LOCATION OF UTILITIES. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE LOCATION OF UTILITIES.
 - WORK REQUIRING EXCAVATION SHALL BE CARRIED OUT IN ACCORDANCE WITH THE CITY OF MISSISSAUGA STANDARD SPECIFICATIONS FOR CONSTRUCTION.

- LANDSCAPE LEGEND:**
- EXISTING GRASSED AREAS SHALL BE RESTORED TO ORIGINAL CONDITION OR BETTER. THE RELOCATION OF TREES AND SHRUBS SHALL BE SUBJECT TO APPROVAL BY THE PROJECT LANDSCAPE ARCHITECT OR ENGINEER.
 - ALL GRANULAR BASE AND SUBGRADE MATERIALS SHALL BE GRADED AND COMPACTED TO 100% STANDARD PROCTOR DENSITY. FREE OF DEPRESSIONS.
 - THE PAVEMENT STRUCTURE SHALL BE CONSTRUCTED OF THE FOLLOWING THICKNESSES OF MATERIALS AS PER THE STANDARD SPECIFICATIONS OF THE CITY OF MISSISSAUGA:
- CAR PARK AREA (LIGHT DUTY ASPHALT)**
- 80mm + ASPHALT HOT MIX
 - 150mm + CRPS 100 GRANULAR 'A' BASE
 - 300mm + CRPS 100 GRANULAR 'A' SUBGRADE
- FIRE ROUTER/STREET ENTRANCE (HEAVY DUTY ASPHALT)**
- 140mm + ASPHALT HOT MIX
 - 140mm + ASPHALT HOT MIX
 - 150mm + CRPS 100 GRANULAR 'A' BASE
 - 300mm + CRPS 100 GRANULAR 'A' SUBGRADE
- PROPOSED SUBGRADE: MINIMUM LENGTH OF 50M EXTENDING FROM ALL CATCHBASINS AND CATCHMAN MANHOLES TO OPEN THE GRANULAR SUBGRADE LAYER AS PER DETAIL ON DRAWING 24.**
- ALL BARRIERS CURBS WITHIN THE SITE TO BE CONSTRUCTED AS PER DETAIL ON DRAWING 24 UNLESS OTHERWISE SPECIFIED.**
- TRENCH BACKFILL WITHIN THE SITE TO BE CONSTRUCTED AS PER DETAIL ON DRAWING 24 UNLESS OTHERWISE SPECIFIED.**
- PROPOSED SLOPES:**
- BY INTERIOR SLOPE
 - PROPOSED GROUND ELEVATION
 - TOP OF CURB ELEVATION
 - EXISTING ELEVATION
 - PROPOSED OVERLAND FLOW ROUTE
 - EMBANKMENT / BERM
 - EXISTING OVERLAND FLOW ROUTE
 - EXISTING CONTOURS
 - PROPOSED AREA
 - PROPOSED HEAVY DUTY ASPHALT

- LANDSCAPE LEGEND:**
- SOODING
 - PRECAST CONCRETE UNIT PAVERS
 - CONCRETE PAVING
 - FEATURES / PERIODS
 - PLAY AREA
 - CROSS WALK PAVEMENT MARKINGS
 - ROD IRON FENCE
 - ACQUISITION FENCE
 - TREE HOARDING FENCE
 - TREE TO BE PRESERVED
 - TREE CROWN
 - MINIMUM TREE PROTECTION ZONE
 - TREE LOCATION
 - TREE TAG



NYX TANNERY LP.

C.P.R. BERM CROSS SECTIONS 51 & 57 TANNERY STREET & 208 EMBY DRIVE (CITY OF MISSISSAUGA) RESIDENTIAL DEVELOPMENT

SE1

Appendix B

Sanitary Design Information

2. DESIGN FLOWS

Design calculations for sanitary sewer systems shall be completed on Standard Drawing 2-5-4 **2-9-1** (appended hereto).

2.1. Population Equivalents based on Land Use

Residential

Population equivalent densities are to be calculated based upon the following criteria:

Density	Pop./Hectare
Single family (greater than 10m frontage)	50 persons/hectare
Single family (less than 10m frontage)	70 persons/hectare
Semi-detached	70 persons/hectare
Row dwellings	175 persons/hectare
Apartments	475 persons/hectare

Apartments

If the proposed population equivalent is greater than 475 persons/hectare, based on a rate of 2.7 people per unit (ppu), then the calculated population equivalent shall be used for design.

$$\frac{2.7 \text{ ppu} \times (\# \text{ units})}{\text{area}} = \text{pop/hectare}$$

Standard Drawing 2-5-2 **2-9-2** (appended hereto) lists domestic sewage flows versus population including a peaking factor.

Industrial

For light industrial areas, use an equivalent population of 70 persons per hectare. Refer to Standard Drawing 2-5-2 **2-9-2** for sanitary sewage flows. Individual studies are to be made for special industries and major industrial areas.

Population	Peak Flow (m ³ /sec)	Population	Peak Flow (m ³ /sec)	Population	Peak Flow (m ³ /sec)
1000	0.0130	4750	0.0542	13000	0.1292
1050	0.0139	5000	0.0569	14000	0.1376
1100	0.0145	5250	0.0594	15000	0.1459
1150	0.0151	5500	0.0618	16000	0.1540
1200	0.0157	5750	0.0640	17000	0.1620
1300	0.0169	6000	0.0666	18000	0.1700
1400	0.0181	6250	0.0691	19000	0.1779
1500	0.0193	6500	0.0710	20000	0.1857
1600	0.0204	6750	0.0737	25000	0.2236
1700	0.0217	7000	0.0762	30000	0.2601
1800	0.0228	7250	0.0784	35000	0.2955
1900	0.0239	7500	0.0809	40000	0.3298
2000	0.0251	7750	0.0830	45000	0.3634
2200	0.0273	8000	0.0854	50000	0.3963
2400	0.0296	8250	0.0878	55000	0.4286
2600	0.0318	8500	0.0898	60000	0.4603
2800	0.0340	8750	0.0922	65000	0.4915
3000	0.0361	9000	0.0945	70000	0.5224
3250	0.0387	9250	0.0968	75000	0.5528
3500	0.0415	9500	0.0981	80000	0.5828
3750	0.0441	9750	0.1010	85000	0.6126
4000	0.0467	10000	0.1033	90000	0.6420
4250	0.0492	11000	0.1120	95000	0.6711
4500	0.0518	12000	0.1210	100000	0.7000

Notes:

1. Domestic sewage flows are based upon a unit sewage flow of 302.8 Lpcd.
2. The flows in the above table include the Harmon Peaking Factor.
3. Domestic sewage flow for less than 1000 persons shall be 0.013m³/sec.
4. Domestic sewage flow for greater than 100,000 persons shall be 7.0 x 10⁻⁶ m³/sec per capita.
5. Lpcd = Litres per capita per day 1 Litre = 0.001 metre³



Date: June 2005 Rev: 1

Approved:

SEWAGE FLOWS
(EXCLUDING INFILTRATION)

STD. DWG. 2-5-2
2-9-2

Project Name: 51 + 57 Tannery St, Mississauga
Project Number: 23-904
Date: 18-Apr-24

Design by: T.Ricketts
Title: **PROPOSED SANITARY CALCULATIONS**



Region of Peel Sanitary Design Calculations*

The Region of Peel uses a contributing flow of 302.8 L/person/day as
 sanitary flow with a peaking factor dependent on population
 Therefore residential flows are equal to: 0.00350463 L/person/s

Total Units = 633

This is an equivalent population of: **1709.10**
 This population gives a peaking factor of: 3.64

Proposed Residential peak flows from the site are: 21.79 L/s

Commercial Sanitary Contribution

Commercial area = - m²
 at 180,000 L/floor ha/day (incl. PF)
 - L/day
 - L/sec

Infiltration

Infiltration allowance = 0.280 L/sec/ha (all areas)
 Total site area = 1.420 ha
 Infiltration = **0.398 L/sec**

Total prop. Infiltration flows from site:

Total Peak Flow = **0.40 L/sec**

Total Proposed Sanitary Contribution 22.2 L/sec

* Calculations completed using Region of Peel Design Criteria - Sanitary Sewers (July 2009)

Residential Data - SRM Architects

Unit Size	# of Units	ppu equiv.*	Total persons
Studio	31	2.7	83.7
1 Bedroom	342	2.7	923.4
2 Bedroom	187	2.7	504.9
3 Bedroom	73	2.7	197.1

Total 633 1709.1

* Average 2.7 ppu Region of Peel std

Commercial Data - NOT USED

Location	GFA sq.m	ppu equiv. 1.1p/100 m2	Total persons
P2	0	1.1	0
P1	0	1.1	0
Level 1	0	1.1	0
Level 2	0	1.1	0
Level 4	0	1.1	0

Total 0 0.0

Appendix C

Stormwater Management Design Information

Project: 51 + 57 Tannery			Prepared by: Todd Ricketts		
Task: 10 yr Post-Development Flowrates			Checked by: Todd Ricketts		
Date: 18-Apr-24			Project # : 23-904		
2-year Post-Dev Flow		IDF Values: City of Mississauga			
A	610				
B	4.6				
C	0.78				
Tc	15.000	minutes			
Land Use Description		Runoff Coefficient	Intensity (mm/hr)	Area (ha)	Runoff (L/s)
Parking Area		0.9	59.89	0.5700	85.3
Landscape		0.25	59.89	0.3800	15.8
Building		0.9	59.89	0.4700	70.4
Total				1.42	171.5
$Q = \frac{CiA}{0.36}$					
		= 171.5 L/s			

Project: 51 + 57 Tannery			Prepared by: Todd Ricketts		
Task: 10 yr Post-Development Flowrates			Checked by: Todd Ricketts		
Date: 18-Apr-24			Project # : 23-904		
5-year Post-Dev Flow		IDF Values: City of Mississauga			
A	820				
B	4.6				
C	0.78				
Tc	15.000	minutes			
Land Use Description		Runoff Coefficient	Intensity (mm/hr)	Area (ha)	Runoff (L/s)
Parking Area		0.9	80.51	0.5700	114.7
Landscape		0.25	80.51	0.3800	21.2
Building		0.9	80.51	0.4700	94.6
Total				1.42	230.6
$Q = \frac{CiA}{0.36}$					
= 230.6 L/s					

Project: 51 + 57 Tannery			Prepared by: Todd Ricketts		
Task: 10 yr Allowable Release			Checked by: Todd Ricketts		
Date: 18-Apr-24			Project # : 23-904		
10-year Allowable C=0.5			IDF Values: City of Mississauga		
A	1010				
B	4.6				
C	0.78				
Tc	15.000	minutes			
Land Use Description		Runoff Coefficient	Intensity (mm/hr)	Area (ha)	Runoff (L/s)
Total Site		0.5	99.17	1.4200	195.6
		0.5	99.17	0.0000	0.0
		0.5	99.17	0.0000	0.0
Total				1.420	195.6
Q = $\frac{CiA}{0.36}$					
= 195.6 L/s					

Project: 51 + 57 Tannery			Prepared by: Todd Ricketts		
Task: 10 yr Post-Development Flowrates			Checked by: Todd Ricketts		
Date: 18-Apr-24			Project # : 23-904		
10-year Post-Dev Flow Proposed			IDF Values: City of Mississauga		
A	1010				
B	4.6				
C	0.78				
Tc	15.000	minutes			
Land Use Description		Runoff Coefficient	Intensity (mm/hr)	Area (ha)	Runoff (L/s)
Parking Area		0.9	99.17	0.5700	141.3
Landscape		0.25	99.17	0.3800	26.2
Building		0.9	99.17	0.4700	116.5
Total				1.42	284.0
Q = $\frac{CiA}{0.36}$					
		= 284 L/s			

Project: 51 + 57 Tannery			Prepared by: Todd Ricketts		
Task: 25 yr Post-Development Flowrates			Checked by: Todd Ricketts		
Date: 18-Apr-24			Project # : 23-904		
25 year Post-Dev Flow Proposed			IDF Values: City of Mississauga		
A	1160				
B	4.6				
C	0.78				
Tc	15.000	minutes	Note Runoff Coefficient factor of 1.1 applied - max C=1.0		
Land Use Description		Runoff Coefficient	Intensity (mm/hr)	Area (ha)	Runoff (L/s)
Parking Area		0.99	113.89	0.5700	178.5
Landscape		0.275	113.89	0.3800	33.1
Building		0.99	113.89	0.4700	147.2
Total				1.420	358.8
$Q = \frac{CiA}{0.36}$					
= 358.8 L/s					



Project: 51 + 57 Tannery			Prepared by: Todd Ricketts		
Task: 50 yr Post-Development Flowrates			Checked by: Todd Ricketts		
Date: 18-Apr-24			Project # : 23-904		
50-year Post-Dev Flow Proposed			IDF Values: City of Mississauga		
A	1300				
B	4.7				
C	0.78				
Tc	15.000	minutes	Note Runoff Coefficient factor of 1.2 applied - max C=1.0		
Land Use Description		Runoff Coefficient	Intensity (mm/hr)	Area (ha)	Runoff (L/s)
Parking Area		1	127.13	0.5700	201.3
Landscape		0.3	127.13	0.3800	40.3
Building		1	127.13	0.4700	166.0
Total				1.420	407.5
$Q = \frac{CiA}{0.36}$					
= 407.5 L/s					

Project: 51 + 57 Tannery		Prepared by: Todd Ricketts			
Task: 100 yr Post-Dev Flowrates - Proposed		Checked by: Todd Ricketts			
Date: 18-Apr-24		Project # : 23-904			
100-year Post Dev Flow Proposed		IDF Values: City of Mississauga			
A	1450				
B	4.9				
C	0.78				
Tc	15.000	minutes	Note Runoff Coefficient factor of 1.25 applied - max C=1.0		
Land Use Description		Runoff Coefficient	Intensity (mm/hr)	Area (ha)	Runoff (L/s)
Parking Area		1	140.69	0.5700	222.8
Landscape		0.32	140.69	0.3800	47.5
Building		1	140.69	0.4700	183.7
Total				1.420	454.0
$Q = \frac{CiA}{0.36}$					
		= 454 L/s			



Project: **51 + 57 Tannery**

Prepared by: **Todd Ricketts**

Task **On-site Storage**

Checked by: **Todd Ricketts**

Date: **18-Apr-24**

Project no.: **23-904**

10 - YR Design Storm
Mississauga

A= 1010
B= 4.6
C= 0.78

	Site
Runoff Coeff. (C):	0.726
Drainage Area (ha):	1.4200
Control Flow (m3/s)	0.196

TIME minutes	I mm/HR		Inflow CIA/360 cms	Storage Rate cms	Max Stor Reqd (cu.m.)	
15.00	99.17		0.284	0.088	79.6	max
20.00	83.06		0.238	0.042	50.8	
25.00	71.90		0.206	0.010	15.5	
30.00	63.66		0.182	0.000	0.0	
35.00	57.30		0.164	0.000	0.0	
40.00	52.22		0.150	0.000	0.0	
45.00	48.07		0.138	0.000	0.0	
50.00	44.60		0.128	0.000	0.0	
55.00	41.65		0.119	0.000	0.0	
60.00	39.11		0.112	0.000	0.0	
65.00	36.91		0.106	0.000	0.0	
70.00	34.96		0.100	0.000	0.0	
75.00	33.24		0.095	0.000	0.0	
80.00	31.69		0.091	0.000	0.0	
85.00	30.31		0.087	0.000	0.0	
90.00	29.05		0.083	0.000	0.0	
95.00	27.90		0.080	0.000	0.0	
100.00	26.86		0.077	0.000	0.0	
105.00	25.90		0.074	0.000	0.0	
110.00	25.01		0.072	0.000	0.0	
115.00	24.19		0.069	0.000	0.0	
120.00	23.43		0.067	0.000	0.0	
125.00	22.72		0.065	0.000	0.0	

Project: **51 + 57 Tannery**

Prepared by: **Todd Ricketts**

Task **On-site Storage**

Checked by: **Todd Ricketts**

Date: **18-Apr-24**

Project no.: **23-904**

25 - YR Design Storm
Mississauga

A= **1160**

B= **4.6**

C= **0.78**

Note Runoff Coefficient factor of 1.1 applied - max C=1.0

	Site
Runoff Coeff. (C):	0.799
Drainage Area (ha):	1.4200
Control Flow (m3/s)	0.196

TIME minutes	I mm/HR		Inflow CIA/360 cms	Storage Rate cms	Max Stor Reqd (cu.m.)	
15.00	113.89		0.359	0.163	146.9	max
20.00	95.40		0.301	0.105	125.9	
25.00	82.58		0.260	0.065	96.8	
30.00	73.11		0.230	0.035	62.5	
35.00	65.80		0.207	0.012	24.6	
40.00	59.98		0.189	0.000	0.0	
45.00	55.21		0.174	0.000	0.0	
50.00	51.22		0.161	0.000	0.0	
55.00	47.84		0.151	0.000	0.0	
60.00	44.92		0.142	0.000	0.0	
65.00	42.39		0.134	0.000	0.0	
70.00	40.15		0.126	0.000	0.0	
75.00	38.17		0.120	0.000	0.0	
80.00	36.40		0.115	0.000	0.0	
85.00	34.81		0.110	0.000	0.0	
90.00	33.36		0.105	0.000	0.0	
95.00	32.05		0.101	0.000	0.0	
100.00	30.85		0.097	0.000	0.0	
105.00	29.74		0.094	0.000	0.0	
110.00	28.73		0.090	0.000	0.0	
115.00	27.79		0.088	0.000	0.0	
120.00	26.91		0.085	0.000	0.0	
125.00	26.10		0.082	0.000	0.0	



Project: **51 + 57 Tannery**

Prepared by: **Todd Ricketts**

Task **On-site Storage**

Checked by: **Todd Ricketts**

Date: **18-Apr-24**

Project no.: **23-904**

50 - YR Design Storm
Mississauga

A= 1300

B= 4.7

C= 0.78

Note Runoff Coefficient factor of 1.2 applied - max C=1.0

	Site
Total Site	Runoff Coeff. (C): 0.813
Rainfall (50 Year)	Drainage Area (ha): 1.4200
	Control Flow (m3/s): 0.196

TIME minutes	I mm/HR		Inflow CIA/360 cms	Storage Rate cms	Max Stor Reqd (cu.m.)	
15.00	127.13		0.408	0.212	190.8	max
20.00	106.57		0.342	0.146	175.3	
25.00	92.30		0.296	0.100	150.4	
30.00	81.75		0.262	0.066	119.7	
35.00	73.60		0.236	0.040	84.7	
40.00	67.10		0.215	0.020	46.8	
45.00	61.77		0.198	0.002	6.6	
50.00	57.32		0.184	0.000	0.0	
55.00	53.54		0.172	0.000	0.0	
60.00	50.28		0.161	0.000	0.0	
65.00	47.45		0.152	0.000	0.0	
70.00	44.95		0.144	0.000	0.0	
75.00	42.74		0.137	0.000	0.0	
80.00	40.76		0.131	0.000	0.0	
85.00	38.97		0.125	0.000	0.0	
90.00	37.36		0.120	0.000	0.0	
95.00	35.89		0.115	0.000	0.0	
100.00	34.54		0.111	0.000	0.0	
105.00	33.31		0.107	0.000	0.0	
110.00	32.17		0.103	0.000	0.0	
115.00	31.12		0.100	0.000	0.0	
120.00	30.14		0.097	0.000	0.0	
125.00	29.23		0.094	0.000	0.0	

Project: **51 + 57 Tannery**

Prepared by: **Todd Ricketts**

Task **On-site Storage**

Checked by: **Todd Ricketts**

Date: **18-Apr-24**

Project no.: **23-904**

100 - YR Design Storm
Mississauga

A= 1450

B= 4.9

C= 0.78

Note Runoff Coefficient factor of 1.25 applied - max C=1.0

		Site			
Total Site Rainfall (100 Year)		Runoff Coeff. (C):	0.818		
		Drainage Area (ha):	1.4200		
		Control Flow (m3/s)	0.196		
TIME minutes	I mm/HR	Inflow CIA/360 cms	Storage Rate cms	Max Stor Reqd (cu.m.)	
15.00	140.69	0.454	0.258	232.5	max
20.00	118.12	0.381	0.186	222.7	
25.00	102.41	0.330	0.135	202.3	
30.00	90.77	0.293	0.097	175.2	
35.00	81.77	0.264	0.068	143.4	
40.00	74.58	0.241	0.045	108.2	
45.00	68.68	0.222	0.026	70.3	
50.00	63.75	0.206	0.010	30.4	
55.00	59.56	0.192	0.000	0.0	
60.00	55.95	0.181	0.000	0.0	
65.00	52.81	0.170	0.000	0.0	
70.00	50.03	0.161	0.000	0.0	
75.00	47.58	0.154	0.000	0.0	
80.00	45.38	0.146	0.000	0.0	
85.00	43.39	0.140	0.000	0.0	
90.00	41.60	0.134	0.000	0.0	
95.00	39.97	0.129	0.000	0.0	
100.00	38.47	0.124	0.000	0.0	
105.00	37.10	0.120	0.000	0.0	
110.00	35.84	0.116	0.000	0.0	
115.00	34.66	0.112	0.000	0.0	
120.00	33.58	0.108	0.000	0.0	
125.00	32.57	0.105	0.000	0.0	



Project: **51 + 57 Tannery**

Prepared by: **Todd Ricketts**

Task **On-site Storage**

Checked by: **Todd Ricketts**

Date: **18-Apr-24**

Project no.: **23-904**

2 - YR Design Storm
Mississauga

A= 610
B= 4.6
C= 0.78

	Site	
Total Site	Runoff Coeff. (C): 0.726	
Rainfall (2 Year)	Drainage Area (ha): 1.4200	
	Control Flow (m3/s): 0.196	

TIME minutes	I mm/HR		Inflow CIA/360 cms	Storage Rate cms	Max Stor Reqd (cu.m.)	
15.00	59.89		0.172	0.000	0.0	max
20.00	50.16		0.144	0.000	0.0	max
25.00	43.42		0.124	0.000	0.0	max
30.00	38.45		0.110	0.000	0.0	max
35.00	34.60		0.099	0.000	0.0	max
40.00	31.54		0.090	0.000	0.0	max
45.00	29.03		0.083	0.000	0.0	max
50.00	26.94		0.077	0.000	0.0	max
55.00	25.16		0.072	0.000	0.0	max
60.00	23.62		0.068	0.000	0.0	max
65.00	22.29		0.064	0.000	0.0	max
70.00	21.12		0.060	0.000	0.0	max
75.00	20.07		0.057	0.000	0.0	max
80.00	19.14		0.055	0.000	0.0	max
85.00	18.30		0.052	0.000	0.0	max
90.00	17.54		0.050	0.000	0.0	max
95.00	16.85		0.048	0.000	0.0	max
100.00	16.22		0.046	0.000	0.0	max
105.00	15.64		0.045	0.000	0.0	max
110.00	15.11		0.043	0.000	0.0	max
115.00	14.61		0.042	0.000	0.0	max
120.00	14.15		0.041	0.000	0.0	max
125.00	13.72		0.039	0.000	0.0	max



Project: **51 + 57 Tannery**

Prepared by: **Todd Ricketts**

Task **On-site Storage**

Checked by: **Todd Ricketts**

Date: **18-Apr-24**

Project no.: **23-904**

5 - YR Design Storm
Mississauga

A= 820
B= 4.6
C= 0.78

				Site	
Total Site Rainfall (5 Year)		Runoff Coeff. (C):		0.726	
		Drainage Area (ha):		1.4200	
		Control Flow (m3/s)		0.196	
TIME minutes	I mm/HR	Inflow CIA/360 cms	Storage Rate cms	Max Stor Reqd (cu.m.)	
15.00	80.51	0.231	0.035	31.5	max
20.00	67.43	0.193	0.000	0.0	
25.00	58.37	0.167	0.000	0.0	
30.00	51.68	0.148	0.000	0.0	
35.00	46.52	0.133	0.000	0.0	
40.00	42.40	0.121	0.000	0.0	
45.00	39.02	0.112	0.000	0.0	
50.00	36.21	0.104	0.000	0.0	
55.00	33.82	0.097	0.000	0.0	
60.00	31.76	0.091	0.000	0.0	
65.00	29.96	0.086	0.000	0.0	
70.00	28.38	0.081	0.000	0.0	
75.00	26.98	0.077	0.000	0.0	
80.00	25.73	0.074	0.000	0.0	
85.00	24.60	0.070	0.000	0.0	
90.00	23.58	0.068	0.000	0.0	
95.00	22.66	0.065	0.000	0.0	
100.00	21.81	0.062	0.000	0.0	
105.00	21.03	0.060	0.000	0.0	
110.00	20.31	0.058	0.000	0.0	
115.00	19.64	0.056	0.000	0.0	
120.00	19.02	0.054	0.000	0.0	
125.00	18.45	0.053	0.000	0.0	

```

2      Metric units
*#*****
*****
*# Project Name: [Tannery]      Project Number: [23-904]
*# Date           : July 2024
*# Modeller       : [T. Ricketts, P.Eng.]
*# Company        : Greystone Engineering Inc
*# License #      : 4842139
*#
*# Modeling proposed development conditions Regional Storm
*#
*#
*#*****
*****
*#*****
*****
START      TZERO=[0.0],  METOUT=[2],  NSTORM=[1],  NRUN=[1]
           ["C:\SWM\Tannery\Hazel.stm"] <--storm filename
*%-----|-----
-----|
READ STORM      STORM_FILENAME=["STORM.001"]
*%-----|-----
-----|
*#*****
*****
*# Catchment 201 - To vault
*#*****
*****
DESIGN STANDHYD      ID=[1],  NHYD=["201"],  DT=[15]min,  AREA=[1.42] (ha),
                    XIMP=[0.82],  TIMP=[0.82],  DWF=[0.0] (cms),  LOSS=[2],
CN=[74],
                    SLOPE=[2] (%),  RAINFALL=[ , , , , ] (mm/hr),  END=-1
*%-----|-----
-----|
*%-----|-----
-----|
ROUTE RESERVOIR      IDout=[2],  NHYD=["SWM VAULT"],  IDin=[1],
                    RDT=[ 15 ] (min),
                    TABLE of ( OUTFLOW-STORAGE ) values
                                (cms) - (ha-m)
                                [ 0.0 , 0.0 ]
                                [ 0.196 , 0.0089 ]
                                [ 0.196 , 0.0250 ]
                                [ -1 , -1 ] (max twenty pts)
                    IDovf=[3],  NHYDovf=["OV-S1"]
*#-----|-----
-----|
*%-----|-----
-----|
FINISH

```

=====

```
SSSSS  W  W  M  M  H  H  Y  Y  M  M  OOO          222
000    11  5555  =====
S      W W W  MM MM  H  H  Y Y  MM MM  O  O          2  0
0    11  5
SSSSS  W W W  M M M  HHHHH  Y  M M M  O  O          2  0
0    11  5      Ver 5.500
S      W W  M  M  H  H  Y  M  M  O  O          222  0
0    11  555    FEB  2015
SSSSS  W W  M  M  H  H  Y  M  M  OOO          2  0
0    11  5      =====
                                           2  0
0    11  5  # 4842139
      StormWater Management HYdrologic Model          222
000    11  555  =====
```

```
*****
*****
***** SWMHYMO Ver 5.500
*****
***** A single event and continuous hydrologic simulation
model *****
***** based on the principles of HYMO and its
successors *****
***** OTTHYMO-83 and OTTHYMO-89.
*****
```

```
*****
*****
***** Distributed by: J.F. Sabourin and Associates Inc.
*****
***** Ottawa, Ontario: (613) 836-3884
*****
***** Gatineau, Quebec: (819) 243-6858
*****
***** E-Mail: swmhymo@jfsa.Com
*****
```

```
*****
*****
```

```
+++++
+++++
+++++ Licensed user: Greystone Engineering Inc.]
+++++
+++++ Pickering SERIAL#:4842139
+++++
```


R0001:C00001-----

*# Project Name: [Tannery] Project Number: [23-904]
*# Date : July 2024
*# Modeller : [T. Ricketts, P.Eng.]
*# Company : Greystone Engineering Inc
*# License # : 4842139
*#
*# Modeling proposed development conditions Regional Storm
*#
*#

| START | Project dir.:C:\SWM\Tannery\
----- Rainfall dir.:C:\SWM\Tannery\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 0001
NSTORM= 1
1=C:\SWM\Tannery\Hazel.stm

R0001:C00002-----

| READ STORM | Filename: C:\SWM\Tannery\Hazel.stm
| Ptotal= 285.08 mm| Comments: Hurricane Hazel

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hh:mm	mm/hr	hh:mm	mm/hr	hh:mm	mm/hr	hh:mm	mm/hr
1:00	2.030	9:00	2.030	17:00	2.030	25:00	2.030
33:00	2.030	41:00	17.000				
	2:00 2.030	10:00 2.030	18:00 2.030	26:00 2.030			
34:00	2.030	42:00 13.000					
	3:00 2.030	11:00 2.030	19:00 2.030	27:00 2.030			
35:00	2.030	43:00 23.000					
	4:00 2.030	12:00 2.030	20:00 2.030	28:00 2.030			
36:00	2.030	44:00 13.000					
	5:00 2.030	13:00 2.030	21:00 2.030	29:00 2.030			
37:00	6.000	45:00 13.000					
	6:00 2.030	14:00 2.030	22:00 2.030	30:00 2.030			
38:00	4.000	46:00 53.000					
	7:00 2.030	15:00 2.030	23:00 2.030	31:00 2.030			
39:00	6.000	47:00 38.000					
	8:00 2.030	16:00 2.030	24:00 2.030	32:00 2.030			
40:00	13.000	48:00 13.000					

R0001:C00003-----

*#*****

*# Catchment 201 - To vault

*#*****

| DESIGN STANDHYD | Area (ha)= 1.42
| 01:201 DT=15.00 | Total Imp(%)= 82.00 Dir. Conn.(%)=
82.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha)=	1.16	.26
Dep. Storage	(mm)=	.80	1.50
Average Slope	(%)=	2.00	2.00
Length	(m)=	97.30	40.00
Mannings n	=	.013	.250

Max.eff.Inten.(mm/hr)=	53.00	48.75
over (min)	15.00	15.00
Storage Coeff. (min)=	2.63 (ii)	12.04 (ii)
Unit Hyd. Tpeak (min)=	15.00	15.00
Unit Hyd. peak (cms)=	.11	.08

TOTALS

PEAK FLOW (cms)=	.17	.03	.206 (iii)
TIME TO PEAK (hrs)=	45.75	46.00	46.000
RUNOFF VOLUME (mm)=	284.28	215.69	271.934
TOTAL RAINFALL (mm)=	285.08	285.08	285.080
RUNOFF COEFFICIENT =	1.00	.76	.954

*** WARNING: Storage Coefficient is smaller than DT! Use a smaller DT or a larger area.

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:

CN* = 74.0 Ia = Dep. Storage (Above)

(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL THAN THE STORAGE COEFFICIENT.

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

R0001:C00004-----

| ROUTE RESERVOIR -> | Requested routing time step = 15.0 min.

| IN>01:201 |

| OUT<02:SWM VAULT | ===== OUTFLOW STORAGE TABLE

STORAGE| OUTFLOW STORAGE| OUTFLOW STORAGE| OUTFLOW
STORAGE| OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.) | (cms)
(ha.m.) | (cms) (ha.m.)

.000 .0000E+00| .196 .8900E-02| .196
.2500E-01| .000 .0000E+00

ROUTING RESULTS	AREA	QPEAK	TPEAK	R.V.
-----	(ha)	(cms)	(hrs)	(mm)
INFLOW > 01:201	1.420	.206	46.000	271.934
OUTFLOW < 02:SWM VAULT	1.420	.196	45.500	271.934
OVERFLOW < 03:OV-S1	.000	.000	.000	.000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin] (%)= 95.260
TIME SHIFT OF PEAK FLOW (min)= -30.00
MAXIMUM STORAGE USED (ha.m.)=.1127E-01

R0001:C00005-----

*#-----|-----

FINISH

WARNINGS / ERRORS / NOTES

R0001:C00003 DESIGN STANDHYD

*** WARNING: Storage Coefficient is smaller than DT! Use a smaller DT or a larger area.

Simulation ended on 2024-07-04 at 15:34:18

=====
=====


 Welcome, todd Ricketts | [My Projects](#) | [Logout](#) | [Find a Rep](#)

Imbrium® OGS Net Annual Sediment Load Reduction Sizing Tool

Project Summary Site Details Sizing Result

[< Back](#) [Cancel](#) [Save Sizing Report](#)

Project Name: 51 + 57 Tannery

Site Name: 51 + 57 Tannery

Location: Mississauga / ON

Site has been saved successfully.

[Download Stormceptor Specifications & Drawings](#)
[Download Stormceptor EFO Sizing Report](#)

Design Summary

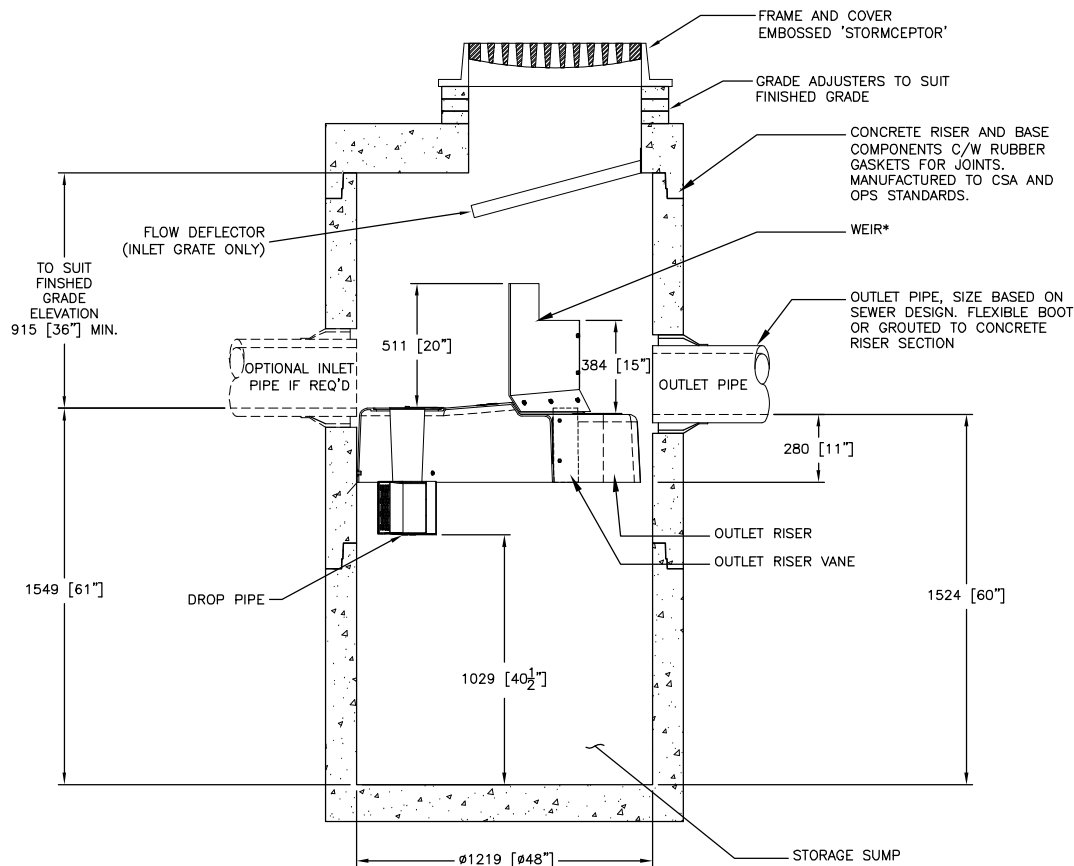
Net Annual Sediment (TSS) Load Reduction Sizing Summary	
Stormceptor Model	TSS Removal Provided (%)
EFO4	92
EFO6	99
EFO8	100
EFO10	100
EFO12	100

Recommended Stormceptor EFO Model: EFO4

Estimated Net Annual Sediment (TSS) Load Reduction (%): 92

Water Quality Runoff Volume Capture (%): > 90

Rainfall Intensity (mm/hr)	Percent Rainfall Volume	Cumulative Rainfall Volume	Flow Rate (L/s)	Flow Rate (L/min)	Surface Loading Rate (L/min/m ²)	Removal Efficiency (%)	Incremental Removal (%)	Cumulative Removal (%)
0.5	8.5%	8.5%	1.48	88.8	74.0	100	8.5	8.5
1	20.6%	29.1%	2.96	177.6	148.0	100	20.6	29.1
2	16.8%	45.9%	5.92	355.3	296.1	100	16.8	45.9
3	10.8%	56.7%	8.88	532.9	444.1	100	10.8	56.7
4	8.5%	65.2%	11.84	710.6	592.1	100	8.5	65.2
5	6.4%	71.6%	14.80	888.2	740.2	100	6.4	71.6
6	5.5%	77.0%	17.76	1065.9	888.2	100	5.5	77.0
7	3.9%	81.0%	20.72	1243.5	1036.2	98	3.9	80.9
8	2.9%	83.9%	23.69	1421.1	1184.3	88	2.6	83.4
9	2.7%	86.5%	26.65	1598.8	1332.3	79	2.1	85.5
10	2.2%	88.7%	29.61	1776.4	1480.4	70	1.5	87.1
11	1.0%	89.7%	32.57	1954.1	1628.4	64	0.6	87.7
12	1.7%	91.3%	35.53	2131.7	1776.4	59	1.0	88.7
13	1.4%	92.8%	38.49	2309.3	1924.5	54	0.8	89.4
14	1.0%	93.7%	41.45	2487.0	2072.5	50	0.5	89.9
15	0.3%	94.0%	44.41	2664.6	2220.5	47	0.1	90.1
16	0.8%	94.8%	47.37	2842.3	2368.6	44	0.3	90.4
17	0.8%	95.7%	50.33	3019.9	2516.6	41	0.3	90.7
18	0.2%	95.8%	53.29	3197.6	2664.6	40	0.1	90.8
19	1.5%	97.3%	56.25	3375.2	2812.7	37	0.6	91.4
20	0.2%	97.5%	59.21	3552.8	2960.7	36	0.1	91.4
21	0.6%	98.2%	62.17	3730.5	3108.7	33	0.2	91.6
22	0.0%	98.2%	65.14	3908.1	3256.8	32	0.0	91.6
23	0.2%	98.4%	68.10	4085.8	3404.8	30	0.1	91.7
24	0.2%	98.6%	71.06	4263.4	3552.8	30	0.1	91.8
25	0.2%	98.9%	74.02	4441.1	3700.9	28	0.1	91.9
30	1.1%	100.0%	88.82	5329.3	4441.1	24	0.3	92.1
35	0.0%	100.0%	103.62	6217.5	5181.2	20	0.0	92.1
40	0.0%	100.0%	118.43	7105.7	5921.4	18	0.0	92.1
45	0.0%	100.0%	133.23	7993.9	6661.6	16	0.0	92.1



SECTION VIEW

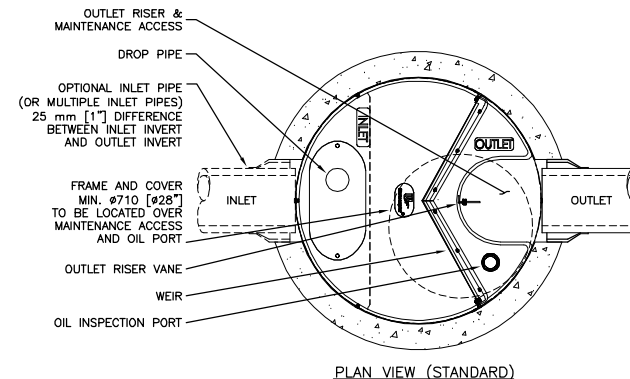
GENERAL NOTES:

- * MAXIMUM SURFACE LOADING RATE (SLR) INTO LOWER CHAMBER THROUGH DROP PIPE IS 1135 L/min/m² (27.9 gpm/ft²) FOR STORMCEPTOR EF4 AND 535 L/min/m² (13.1 gpm/ft²) FOR STORMCEPTOR EF04 (OIL CAPTURE CONFIGURATION). WEIR HEIGHT IS 150 mm (6 INCH) FOR EF04.
- ALL DIMENSIONS INDICATED ARE IN MILLIMETERS (INCHES) UNLESS OTHERWISE SPECIFIED.
- STORMCEPTOR STRUCTURE INLET AND OUTLET PIPE SIZE AND ORIENTATION SHOWN FOR INFORMATIONAL PURPOSES ONLY.
- UNLESS OTHERWISE NOTED, BYPASS INFRASTRUCTURE, SUCH AS ALL UPSTREAM DIVERSION STRUCTURES, CONNECTING STRUCTURES, OR PIPE CONDUITS CONNECTING TO COMPLETE THE STORMCEPTOR SYSTEM SHALL BE PROVIDED AND ADDRESSED SEPARATELY.
- DRAWING FOR INFORMATION PURPOSES ONLY. REFER TO ENGINEER'S SITE/UTILITY PLAN FOR STRUCTURE ORIENTATION.
- NO PRODUCT SUBSTITUTIONS SHALL BE ACCEPTED UNLESS SUBMITTED 10 DAYS PRIOR TO PROJECT BID DATE, OR AS DIRECTED BY THE ENGINEER OF RECORD.

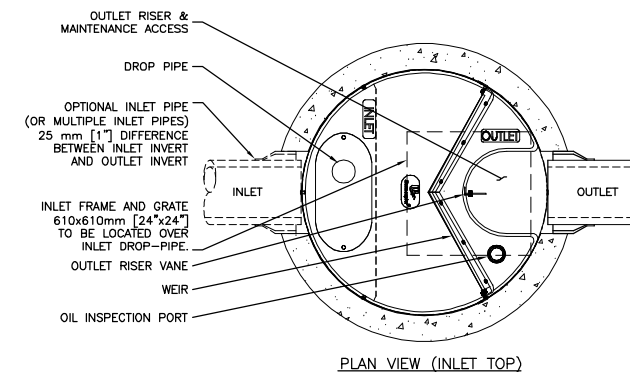
INSTALLATION NOTES

- ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE STRUCTURE (LIFTING CLUTCHES PROVIDED).
- CONTRACTOR WILL INSTALL AND LEVEL THE STRUCTURE, SEALING THE JOINTS, LINE ENTRY AND EXIT POINTS (NON-SHRINK GROUT WITH APPROVED WATERSTOP OR FLEXIBLE BOOT).
- CONTRACTOR TO TAKE APPROPRIATE MEASURES TO PROTECT THE DEVICE FROM CONSTRUCTION-RELATED EROSION RUNOFF.
- DEVICE ACTIVATION, BY CONTRACTOR, SHALL OCCUR ONLY AFTER SITE HAS BEEN STABILIZED AND THE STORMCEPTOR UNIT IS CLEAN AND FREE OF DEBRIS.

STANDARD DETAIL
NOT FOR CONSTRUCTION



PLAN VIEW (STANDARD)



PLAN VIEW (INLET TOP)

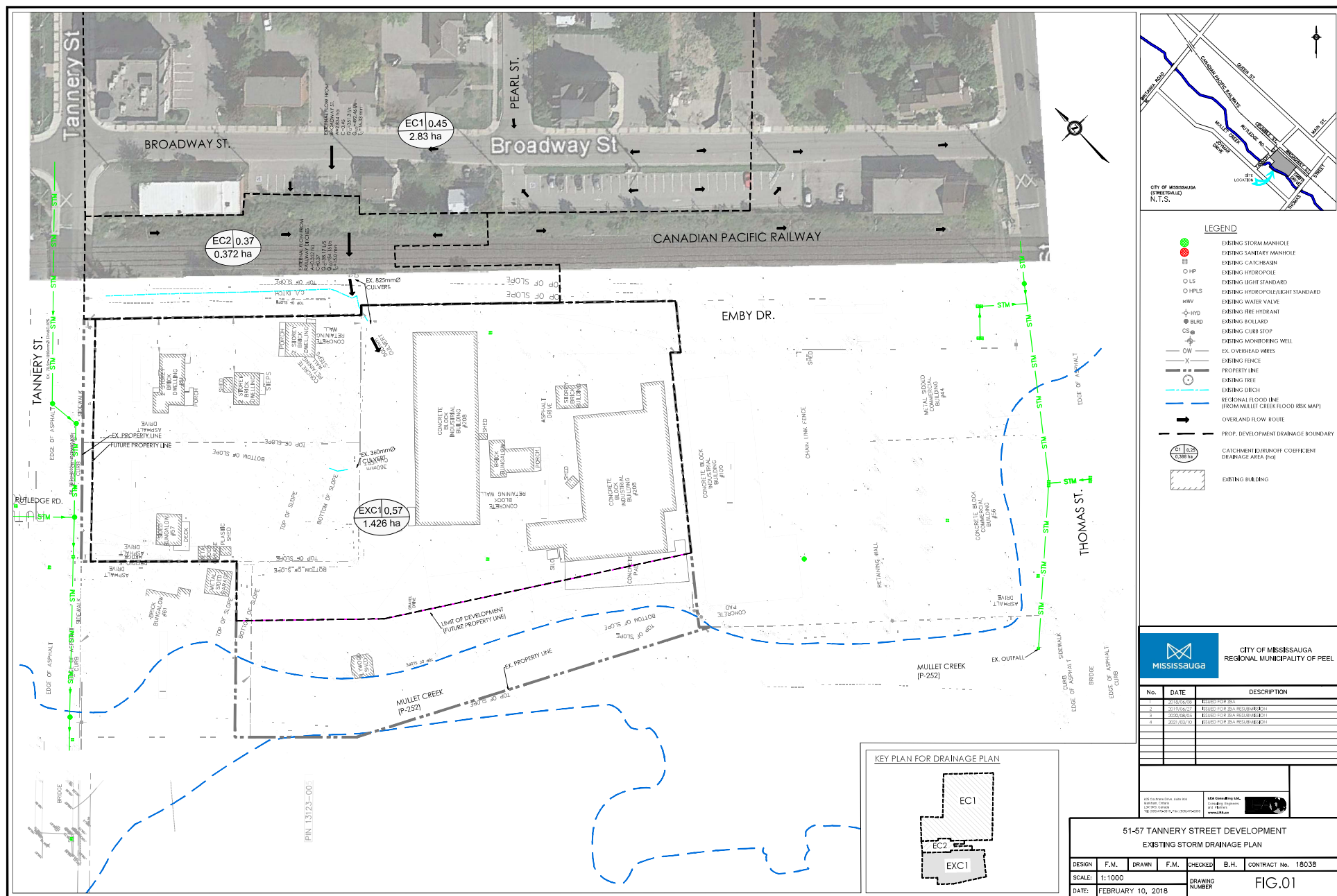
FOR SITE SPECIFIC DRAWINGS PLEASE CONTACT YOUR LOCAL STORMCEPTOR REPRESENTATIVE. SITE SPECIFIC DRAWINGS ARE BASED ON THE BEST AVAILABLE INFORMATION AT THE TIME. SOME FIELD REVISIONS TO THE SYSTEM LOCATION OR CONNECTION PIPING MAY BE NECESSARY BASED ON AVAILABLE SPACE OR SITE CONFIGURATION REVISIONS. ELEVATIONS SHOULD BE MAINTAINED EXCEPT WHERE NOTED ON BYPASS STRUCTURE (IF REQUIRED).

SITE SPECIFIC DATA REQUIREMENTS

STORMCEPTOR MODEL	EF4				
STRUCTURE ID	*				
WATER QUALITY FLOW RATE (L/s)	*				
PEAK FLOW RATE (L/s)	*				
RETURN PERIOD OF PEAK FLOW (yrs)	*				
DRAINAGE AREA (HA)	*				
DRAINAGE AREA IMPERVIOUSNESS (%)	*				
PIPE DATA:	I.E.	MAT'L	DIA	SLOPE %	HGL
INLET #1	*	*	*	*	*
INLET #2	*	*	*	*	*
OUTLET	*	*	*	*	*

* PER ENGINEER OF RECORD

<p>Stormceptor® EF</p> <p>imbrum</p> <p>7801 HIGHT ROAD, SUITE 200, VANUVER, BC V2Y 2Y9 CAN. 800-875-6888 CA 800-898-0871 INT. +1-604-886-8888</p> <p>DATE: 5/26/2017</p> <p>DESIGNED: JSK DRAWN: JSK</p> <p>CHECKED: BSF APPROVED: SP</p> <p>PROJECT No.: EF4 SEQUENCE No.: *</p> <p>SHEET: 1 OF 1</p>		<p>BY</p> <p>DATE</p> <p>REVISION DESCRIPTION</p> <p>INITIAL RELEASE</p> <p>UPDATES</p> <p>JSK</p> <p>JSK</p>
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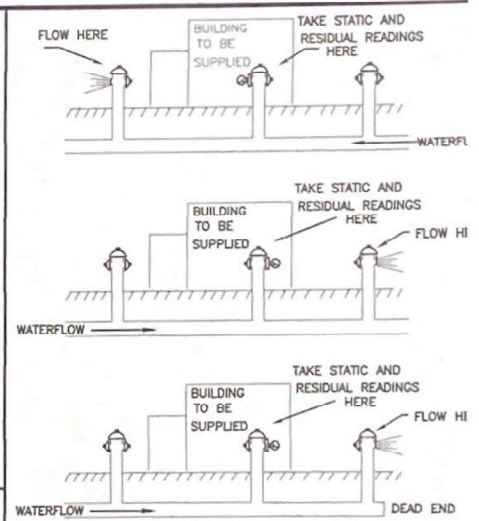


Appendix D

Water Design Information



DURING THE FLOW TEST AS PER THE CITY WATER PERSONNEL, THE FLOW HYDRANT MAY HAVE BEEN DEFECTIVE. CITY TO INVESTIGATE.



TEST:	PLAY PIPE	C=	STATIC(PSI)	RESIDUAL(PSI)	PITOT(PSI)	FLOW(USGPM)
	1x1 1/8					
	2x1 1/8					
	3x1 1/8					
	4x1 1/8					
	1x1 3/4					
	2x1 3/4					
	3x1 3/4					
	4x1 3/4					
HYDRANT BUTT						
1	1x2 1/2	.835	75	73	15	602.9
2	2x2 1/2	.835	75	71	5	696.2
	3x2 1/2					
	4x2 1/2					
FM NOZZLE						
	1x2 1/4	.88				
	2x2 1/4	.88				
	3x2 1/4	.88				
	4x2 1/4	.88				

OUTLET TYPE

- ☐ COEF = 0.80
OUTLET SMOOTH
AND WELL ROUNDED
- ☐ COEF = 0.80
OUTLET SQUARE
AND SHARP
- ☐ COEF = 0.70
OUTLET SQUARE
AND PROJECTING
INTO BARREL
- ☒ COEF = 0.833
MODEL LPD-250A
DECHLORINATOR
DIFFUSER
PITOT TUBE

Client: LEA CONSULTING LTD.

625 COCHRANE DR.

MARKHAM, ON

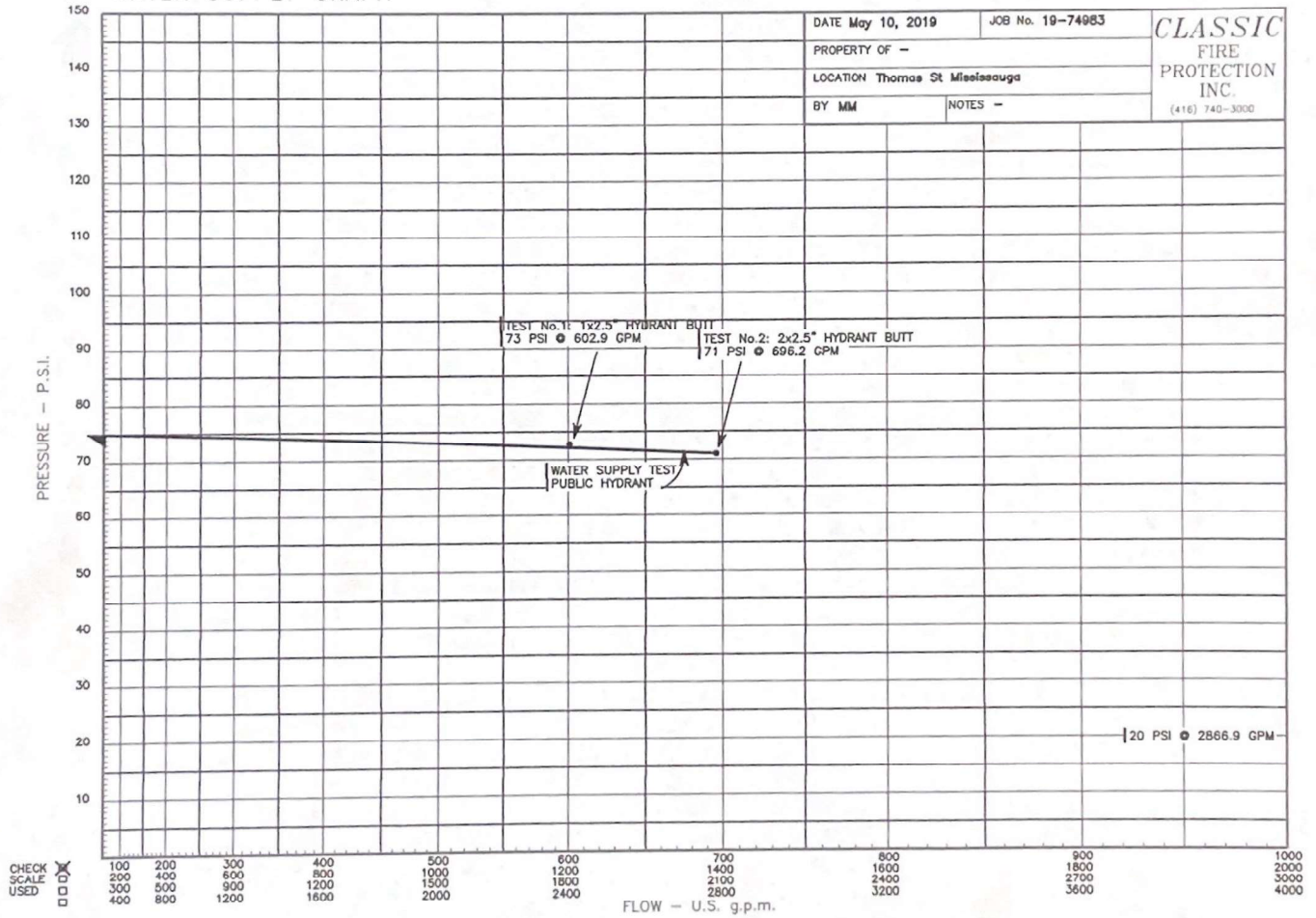
Location:

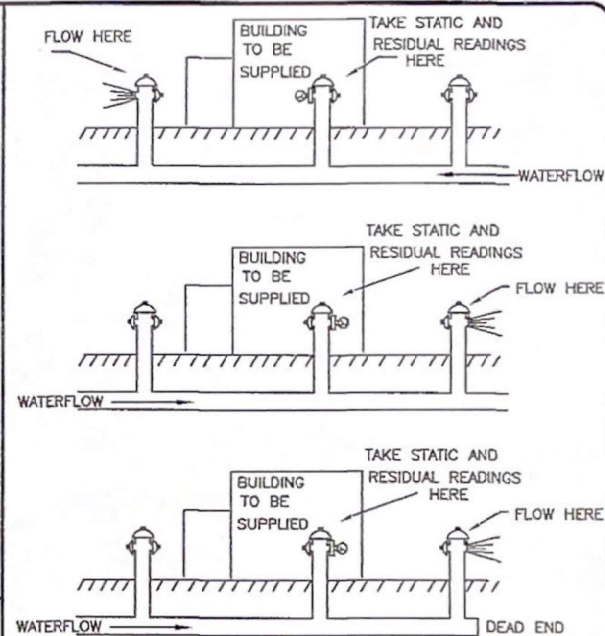
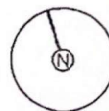
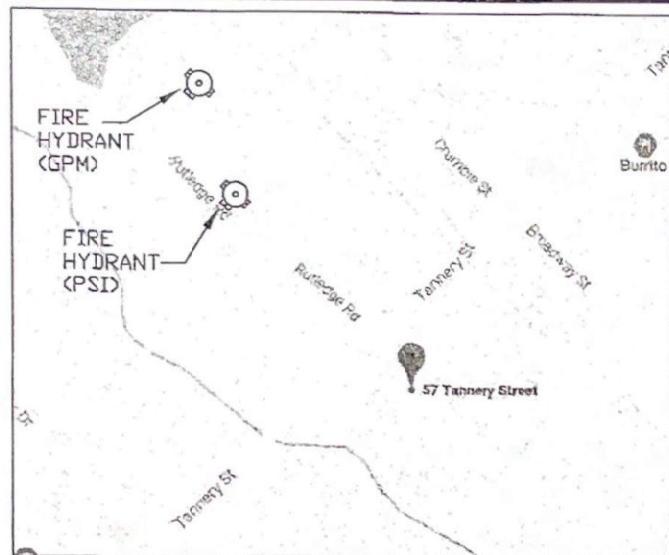
Thomas St

Mississauga, ON

1988
CLASSIC
FIRE PROTECTION INC.
645 GARYWAY
North York, I
MIL. 1P9
(416) 740-3
Web: www.classicfire.com




WATER SUPPLY GRAPH





TEST:	PLAY PIPE	C=	STATIC(PSI)	RESIDUAL(PSI)	PITOT(PSI)	FLOW(USGPM)
	1x1 1/8					
	2x1 1/8					
	3x1 1/8					
	4x1 1/8					
	1x1 3/4					
	2x1 3/4					
	3x1 3/4					
	4x1 3/4					
HYDRANT BUTT						
1	1x2 1/2	.80	62	54	21	683.5
2	2x2 1/2	.80	62	58	11	983.3
	3x2 1/2					
	4x2 1/2					
FM NOZZLE						
	1x2 1/4	.88				
	2x2 1/4	.88				
	3x2 1/4	.88				
	4x2 1/4	.88				

OUTLET TYPE

- ☐  COEF.=0.90
OUTLET SMOOTH
AND WELL ROUNDED
- ☒  COEF.=0.80
OUTLET SQUARE
AND SHARP
- ☐  COEF.=0.70
OUTLET SQUARE
AND PROJECTING
INTO BARREL

Client:

Location:

51-57 Tannery St

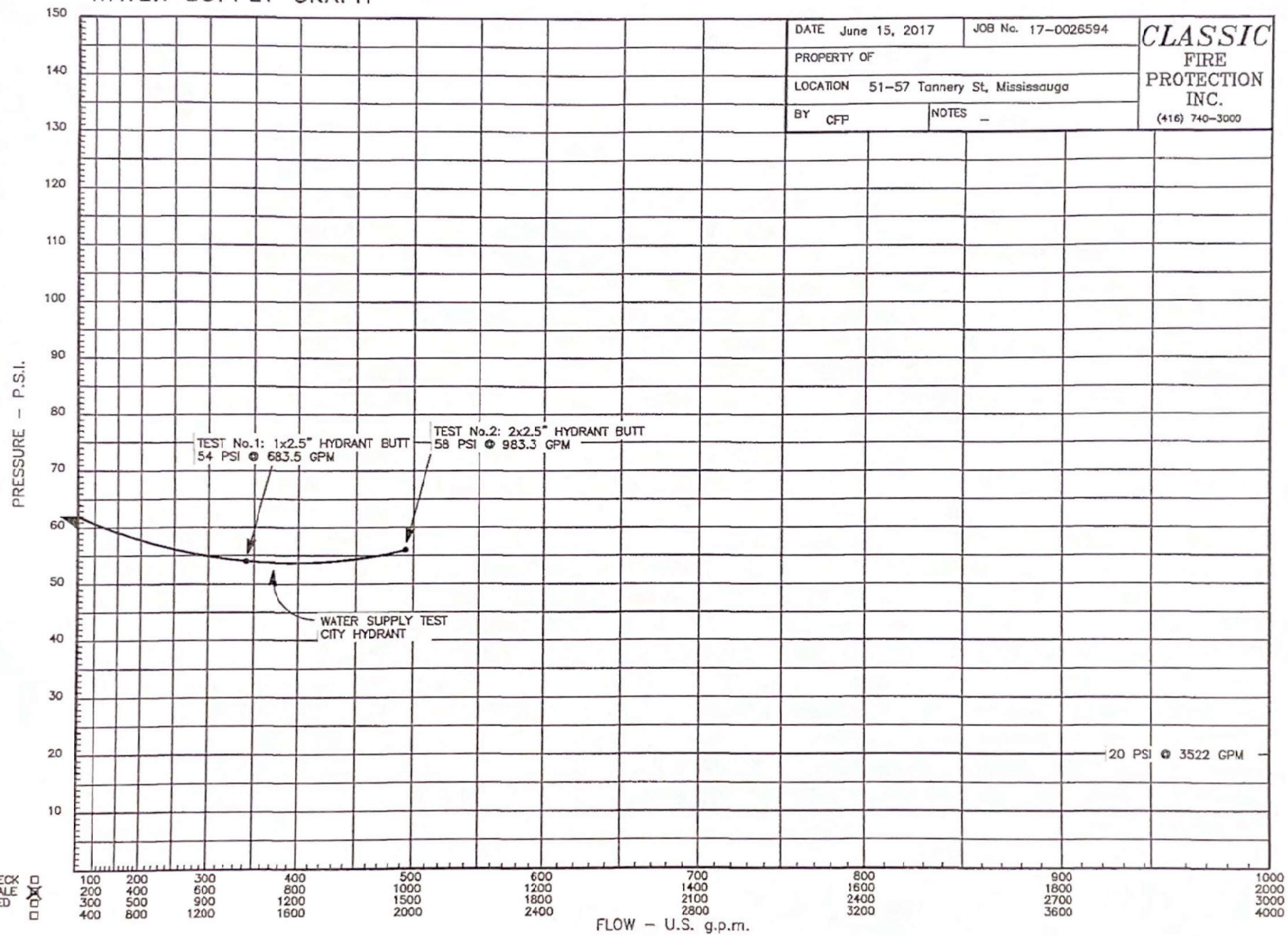
Mississauga, ON



645 CARRWAY DR.
North York, ON
M2L 1P9
(416) 740-3000

Web: www.classicfire.com

WATER SUPPLY GRAPH



2.3 Water Demands

Water demands are to be calculated as follows:

Table #1 – Typical Water Demand Criteria

Population Type	Unit	Avg. Consumption Rate	Max Day Factor	Peak Hour Factor
Residential	L/cap • d	280	2.0	3.0
ICI	L/Employee • d	300	1.4	3.0

ICI = Industrial, Commercial or Institutional

Custom demands for larger volume consumers or those with exceptional peak demands require special considerations regarding flow calculations. Each case will be reviewed on an individual basis.

It has been noted that some new development can generate higher water demands during the first years of occupancy. Factors for this elevated water use include additional lawn watering for new sod and changes in water use patterns. Table #2 states the potential short term water demand criteria for new development. However, over the long term, it is estimated that water use would ultimately be reduced through water conservation programs and other potential factor including rates. As such, for the purpose of projecting long term water requirements, the water demand criteria in Table #1 should be used.

Table #2 – Potential short term water demand criteria for new development

Population Type	Unit	Avg. Consumption Rate	Max Day Factor	Peak Hour Factor
Residential	L/cap • d	409	2.0	3.0
ICI	L/Employee • d	300	2.0	3.0

The Region may impose the higher short-term water demand criteria for new developments where water supply capacity or residual pressure may be marginal.

Project Name: 51 + 57 Tannery Street.
 Project Number: 23-904
 Date: 17-Apr-24



Design by: T.Ricketts
 Title: **WATER DEMAND AND FIRE FLOW CALCULATION**

Based on Fire Underwriters Survey

1 $F = 220 C (\sqrt{A})$

Where F= Fire flow in Lpm

C= construction type coefficient

= 0.6 fire resistive construction

A = total floor area in sq.m. excluding basements (garage or areas with 50% underground)

Floor	Area (sq.m)	%
Level 2	13,940	25%
Level 1	14,403	100%
P1	8,061	25%

Vertical openings protected (1 hr rating)

Largest Floor plus 25% of each adjoining floor

Largest Area= 19,903 sq.m

F = 18,622 L/min

Round to nearest 1000 l/min

F = 19,000 L/min

2 Occupancy Reduction

25% reduction for non-combustible

Reduction = 4750 L/min

F = 14,250 L/min

3 Separation Charge

5% North Side 32 m

0% East Side 52.8 m

20% South Side 10.4 m

5% West Side 34.4 m

30% Total Separation Charge, **4275** L/min

F = **18,525** L/min

Separation Charge

0 to 3 m 25%

3.1 to 10 m 20%

10.1 to 20 m 15%

20.1 to 30 m 10%

30.1 to 45 m 5%

45 m > 0%

4 Sprinkler Reduction

40% Reduction for NFPA Sprinkler System

Reduction = **5700** L/min

5 Domestic Flow Calculations

Population 1709 (633 units x 2.7 ppu)

Ave. Day Demand = 280 L/cap/day

332 L/min

Max. Day Peaking Factor = 2.0 Residential

Max. Domestic Flow Rate F_{dom} = **665** L/min

Water Demand = Fire Flow - Sprinkler Reduction + Domestic Flow ($F_3 - F_4 + F_5$)

F = 18,525 - 5700 + 665 = 13,490 l/min

F = 225 L/s

F = **3561** GPM

