



City of Mississauga

FUNCTIONAL SERVICING AND STORMWATER MANAGEMENT REPORT

Weston Consulting.

3016-3032 Kirwin Ave & 3031 Little John Lane

November 07, 2023

21111

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TABLE OF CONTENTS

1	INTRODUCTION	1
1.1	<i>Scope of the SWM and Servicing brief</i>	1
1.2	<i>Site Location</i>	1
1.3	<i>Stormwater Management Plan Objectives</i>	1
1.4	<i>SWM Design Criteria – Credit Valley Conservation Authority</i>	1
2	EXISTING CONDITIONS	2
2.1	<i>General</i>	2
2.2	<i>Rainfall Information</i>	2
2.3	<i>Peak Flow Rates under Existing Condition</i>	3
2.4	<i>Allowable Release Rate</i>	3
3	POST-DEVELOPMENT CONDITIONS	4
3.1	<i>General</i>	4
3.2	<i>Peak Flow Rates under Proposed Condition</i>	4
3.3	<i>Overcontrol to meet allowable release rate</i>	5
3.4	<i>Impact on Water Environment</i>	6
4	PROPOSED SWM PLAN	6
4.1	<i>Water Balance Requirement</i>	6
4.2	<i>Water Quantity Control Requirement</i>	7
4.3	<i>Water Quality Control Requirement</i>	8
4.4	<i>EROSION AND SEDIMENT CONTROL DURING CONSTRUCTION</i>	9
5	FLOODPLAIN review SUMMARY	9
6	GROUNDWATER DISCHARGE	9
6.1	<i>Construction Dewatering</i>	10
6.2	<i>Long-Term Dewatering</i>	10
7	SITE SERVICING	11
7.1	<i>Existing Municipal Services</i>	11
7.2	<i>Proposed Site Service Connections</i>	11
7.3	<i>Adequacy of Existing Municipal Services</i>	12
8	CONCLUSIONS	14

LIST OF TABLES

Table 1: Pre-Development Runoff Coefficient.....	2
Table 2: Rainfall Parameters	3
Table 3: Pre-Development Peak Flow Rates (L/s)	3
Table 5: Post-Development Input Parameter.....	4
Table 7: Post-Development Peak Flow Rates (L/s)	5
Table 9: Key Hydrologic Parameters	6
Table 10: Post Development Quantity Control as Per City's Requirement.....	8
Table 11: TTS Removal Assessment Sub-Catchment OC1.....	8
Table 13: Site Servicing Requirement	12
Table 14: Downstream Sewer Capacity – Proposed Condition.....	13

APPENDICES

APPENDIX A	STORMWATER PEAK FLOW AND STORAGE CALCULATION AND SWM DETAILS FOR SUB-CATCHMENT AREA EC1, OC1 and UC1
APPENDIX B	STORMWATER PEAK FLOW CALCULATIONS FOR SUB-CATCHMENT AREA EC2 AND PC2
APPENDIX C	SANITARY AND WATER DEMAND CALCULATIONS
APPENDIX D	STORM SEWER CAPACITY ASSESSMENT AND CCTV ASSESSMENT RESULTS
APPENDIX E	HYDRANT FLOW TEST DATA AND WATERMAIN ADEQUACY ASSESSMENT DATA
APPENDIX F	FLOODLINES INFORMATION
APPENDIX G	FIGURES AND DRAWING
APPENDIX H	WATERTIGHT FOUNDATION LETTER AND HYDROGEOLOGICAL REPORT

1 INTRODUCTION

1.1 SCOPE OF THE SWM AND SERVICING BRIEF

LEA Consulting Ltd has been retained by Weston Consulting, to prepare a Functional Servicing and Stormwater Management Report for the proposed residential development project in the City of Mississauga. This Servicing and stormwater management report shall:

- ▶ Examine the potential water quality and quantity impacts of the proposed 8-storey apartment development and summarize how each will be addressed in accordance with the City of Mississauga and Credit Valley Conservation (CVC) stormwater management requirements.
- ▶ Review the existing water supply, storm, sanitary services, and propose a site servicing plan.

1.2 SITE LOCATION

The proposed development site is located at the southwest quadrant of Kirwin Avenue and Dundas Street East, contributory to Cooksville Creek watershed, and under the jurisdiction of Credit Valley Conservation (CVC). The site is approximately 0.64 ha in area.

1.3 STORMWATER MANAGEMENT PLAN OBJECTIVES

The objectives of the stormwater management plan are to review the stormwater environment impact by the proposed residential development and address the City's requirements for stormwater quantity control and quality control as required;

1.4 SWM DESIGN CRITERIA – CREDIT VALLEY CONSERVATION AUTHORITY

Since the Project Site is located within the City of Mississauga and the Cooksville Creek watershed, which is under jurisdiction of the Credit Valley Conservation (CVC), the following SWM criteria and guidelines were referenced during SWM analysis and design to provide direction on how to manage rainfall and runoff inside CVC and City's jurisdiction:

- ▶ City of Mississauga Development Requirements Manual, Section 8, City of Mississauga, November 2020;
- ▶ Credit Valley Conservation (CVC), Stormwater Management Criteria, August 2012;

A summary of the stormwater management criteria applied for this project is provided below:

- ▶ Storm Water Quality Control: Cooksville Creek is classified as requiring an Enhanced level of protection (80% TSS removal) by CVC quality control criteria.
- ▶ Water Quantity Control: all storm events up to 100-year post-development peak flow shall be controlled to the 2-year pre-development flow with a maximum runoff coefficient of 0.5 as required by CVC and the City of Mississauga within the Cooksville Creek Sub-watershed.
- ▶ Water Balance: The minimum on-site runoff retention will require the site to retain all runoff from a 5mm storm event through infiltration, evapotranspiration or rainwater reuse.
- ▶ Erosion Control: On-site retention of 5mm for small infill/redevelopment sites < 2.0 ha within the Cooksville Creek sub-watershed.

2 EXISTING CONDITIONS

2.1 GENERAL

The existing site is located between Kirwin Avenue and Little John Lane and consists of four single-family houses and 0.53 ha of lawn and treed area.

During rainfall events, surface rainfall-runoff of houses flows to Kirwin Avenue and runoff of the rest of the site drains to the Cooksville Creek. The total drainage area is approximately 0.64 ha.

For the purpose of SWM analysis, the development site catchment divided into the following two sub-catchment areas based on the existing drainage pattern.

- ▶ EC1 – Existing houses drains to Kirwin Ave.;
- ▶ EC2 – The green area which drains to Cooksville Creek.

The composite runoff coefficients of two sub-catchment areas are, as estimated in Appendix A and B, listed in Table 1.

Table 1: Pre-Development Runoff Coefficient

Sub-catchment No	Catchment Description	Catchment Area (ha)	Runoff Coefficient
EC1	Existing Houses	0.195	0.62*
EC2	Existing green area	0.444	0.25

* As per City of Mississauga Design Requirements, maximum runoff coefficient of 0.5 has been considered in storm flow calculations under existing condition.

The current site does not accept any external drainage. Overland flow routes, grading and land use details under existing conditions are illustrated in Figure 1, Appendix G.

Based on our review of the topographic survey, there is no on-site stormwater management facility under the existing condition.

2.2 RAINFALL INFORMATION

The rainfall intensity for the site was calculated using the following equation:

$$I = A / (T_c + B)^{0.78}$$

Where; I = rainfall intensity in mm/hr,

T_c = time of concentration in minutes,

A, B = constant parameters (see below)

The parameters (A and B) recommended for use in the City of Mississauga are defined in City Standard Drawing No. 2111.010 and are summarized in Table 2.

Table 2: Rainfall Parameters

Return Period (Year)	2 - Yr	5 - Yr	10 - Yr	25 - Yr	50 - Yr	100 - Yr
A	610	820	1010	1160	1300	1450
B	4.6	4.6	4.6	4.6	4.7	4.9

The initial time of concentration, TC, of 15 minutes is recommended in the City's Development Requirements Manual.

2.3 PEAK FLOW RATES UNDER EXISTING CONDITION

Based on the existing site condition and rainfall parameters, the Rational Method is adopted to calculate peak flows at different design storm events.

The calculated peak flow rates for each sub-catchment under pre-development condition are calculated and summarized below in Table 3. Detailed calculations are provided in Appendix A.

Table 3: Pre-Development Peak Flow Rates (L/s)

Sub-catchment ID	Sub-Catchment Description	2 - Yr	5 - Yr	10 - Yr	25 - Yr	50 - Yr	100 - Yr
EC1	Existing Houses	16.21	21.80	26.85	30.83	34.42	38.09
EC2	Existing green area	18.45	24.80	30.54	35.08	39.16	43.33

Maximum runoff coefficient of 0.5 has been considered in pre-development peak flow calculation of sub-catchment EC1.

2.4 Allowable Release Rate

Based on the City's record drawings, storm drainage area plan design sheets, under the existing condition, the flow from the proposed site to the Kirwin Avenue includes only the rainfall runoff from the existing houses.

In order to maintain the existing drainage condition of Kirwin Avenue, the allowable discharge flow rate from the proposed site to the existing municipal sewer on Kirwin Avenue under the proposed condition will be 16.21 l/s which is equal to the 2-yr existing flow from sub-catchment EC1 with a maximum runoff coefficient of 0.5.

3 POST-DEVELOPMENT CONDITIONS

3.1 GENERAL

The proposed development consists of construction of an 8-storey residential building with 2 underground parking levels on the northern part of the site. The proposed storm drainage condition is as follows:

Sub-catchment OC1:

This sub-catchment includes the entire development area except building frontage along the Kirwin Avenue. During rainfall events, surface storm runoff of the site will be captured by building's roof and terrace drains and proposed at-grade area drains, conveyed through internal storm piping within the underground parking to the proposed concrete storm tank and outlet to the existing municipal storm sewer on Kirwin Avenue.

Minimal landscape areas at the south and northwest side of the site will drain to the dedicated parkland. Since the land use of these small areas will remain as-is and with regard to the grading constraints, the runoff from these small areas will not be controlled.

Sub-catchment PC2:

This sub-catchment consists of the lands to be dedicated for parkland and a small portion of the development area at the west of the proposed building which will remain as-is. The existing drainage pattern will not be changed, and all storm runoff will convey and discharge to Cooksville Creek under the proposed condition

Refer to Figure 2 in Appendix G for the proposed sub-catchments, overland flow route and drainage condition.

The relevant drainage parameters of the post-development drainage areas are provided in Table 5. Refer to Appendices A and B for details. As per City's requirement, the runoff coefficient of 0.9 and was considered in the required storm storage calculation for catchment area PC1.

Sub-catchment UC1:

This sub-catchment is located North of the proposed building. Since this area is graded towards Kirwin Avenue and the flow pattern remains the runoff will not be controlled.

Table 5: Post-Development Input Parameter

Sub-Catchment No.	Drainage Area (ha)	C	Tc (min.)
OC1	0.330	0.76 (Considered 0.9 in Storm Calculations)	15
PC2 (Parkland area)	0.295	0.25	15
UC1	0.013	0.88	15

3.2 PEAK FLOW RATES UNDER PROPOSED CONDITION

Based on the proposed site condition and rainfall parameters, the Rational Method is adopted to calculate peak flows at different design storm events.

According to the City of Mississauga Development Requirements Manual, 2016, in order to account for the increase in runoff due to saturation of the catchment surface, for storms having a return period of more than 10 years, runoff coefficients shall be increased by the adjustment factors, up to a maximum coefficient of 1.0. Table 6 illustrate the proposed adjustment factors. Table 6: Runoff Coefficient Adjustment Factors

Return Period (Year)	Adjustment Factor
10yr	1.00
25yr	1.10
50yr	1.20
100yr	1.25

The calculated peak flow rates for sub-catchment PC1 and PC2 under the post-development condition are summarized below in Table 7. Detailed calculations are provided in Appendices A and B.

Table 7: Post-Development Peak Flow Rates (L/s)

Sub-catchment ID	Sub-Catchment Description	2 - Yr	5 - Yr	10 - Yr	25 - Yr	50 - Yr	100 - Yr
OC1	Overcontrolled Development area	49.42	66.44	81.83	103.38 *	116.57 *	129.00 *
PC2	Parkland	12.28	16.51	20.34	23.36	26.07	28.85
UC1	Uncontrolled area	1.91	2.57	3.17	3.64	4.06	4.50

The adjusted runoff coefficients are used to calculate 25-yr to 100-yr flow.

3.3 OVERCONTROL TO MEET ALLOWABLE RELEASE RATE

As mentioned in Section 1.4, the proposed site is located within Cooksville Creek sub-watershed and required to control 100-year post-development flow to 2-year pre-development flow with a maximum runoff coefficient of 0.5.

Based on the City's record drawings, storm drainage area plan design sheets, under the existing condition, the flow from the proposed site to the Kirwin Avenue includes only the rainfall runoff from the existing houses.

In order to maintain the existing drainage condition of Kirwin Avenue, the allowable discharge flow rate from the proposed site to the existing municipal sewer on Kirwin Avenue under the proposed condition will be the 2-year existing flow from sub-catchment OC1.

Furthermore, as mentioned in Section 3.1, under post-development condition it is not feasible to implement discharge control for sub-catchment UC1. Therefore, the discharge from proposed residential development (sub-catchment OC1) will be overcontrolled to satisfy the City's quantity control criteria.

As a result, the allowable flow rate from proposed residential development or sub-catchment OC1 is estimated at 11.72 L/s. Detailed calculations are provided on page A-04 of Appendix A.

3.4 IMPACT ON WATER ENVIRONMENT

Based on the review and analysis for existing and proposed site conditions, Table 8 summarizes the key hydrologic parameters of the site under the proposed condition.

Table 9: Key Hydrologic Parameters

Sub-Catchment ID	Area (ha)		Imperviousness (%)		Runoff Coefficient		100-year Peak Flow Rate (L/s)	
	Pre-Dev	Post-Dev	Pre-Dev	Post-Dev	Pre-Dev	Post-Dev	Pre-Dev	Post-Dev
EC1 & PC1(OC1+UC1)	0.195	0.343	57.4	77.1	0.62 *	0.76 **	38.09	133.50 ***
EC2 & PC2	0.444	0.295	0	0	0.25	0.25	43.33	28.85

*As per City's criteria, Maximum runoff coefficient of 0.5 has been considered in pre-development peak flow calculation.

**As per City's comment, the overall runoff coefficient of 0.90 has been considered for sub-catchment OC1.

***The adjusted runoff coefficient is used to calculate 100-yr flow.

The hydrologic parameters show the changes before and after the proposed development. Mitigation measures are required for sub-catchment OC1 in accordance with the CVC's design criteria. Since the land-use of the sub-catchment PC2 will not be changed and storm flow rates to the Cooksville Creek will be decreased under post development condition, no mitigation measures are required for sub-catchment PC2.

With regards to the abovementioned, the stormwater management plan is provided only for sub-catchment OC1.

4 PROPOSED SWM PLAN

4.1 WATER BALANCE REQUIREMENT

Based on the water balance criteria of the City of Mississauga, the minimum on-site runoff retention requires retaining all runoff of the first 5mm from each rainfall through infiltration, evapotranspiration or rainwater reuse.

For the required on-site retention volume from a 5mm rainfall event, the total required water balance volume for the catchment OC1 is 13.2m³ based on the proposed impervious area of the site (green roof and landscape areas are excluded). This retention volume will be collected into the proposed underground storage tank. Refer to page A03 of Appendix A for detailed calculation.

The Low Impact Development (LID) methods to address the retention criteria are outlined as follows:

- Irrigation: Based on the monthly irrigation estimate provided by the design team landscape architect, the average 72-hour irrigation water use is 14.49 m³. Detailed calculations are provided in Appendix A.
- Bio-retention swale: 500 mm of 50 mm washed clear stone below the bio-retention area will provide approximately 1.2 m³ of retention volume. Details and drawdown calculations for the bio-retention

swales are provided in page A15 of Appendix A.

- Extensive green roof: The proposed 466m² green roof reduces runoff but, does not provide retention capacity beyond the first 5mm of each storm event.

Based on the provided information, a total of 15.69 m³ of water retention can be re-used through irrigation and infiltration. Therefore, it is satisfactory to City's water balance requirement.

The total stormwater volume of 14.5 m³ will be retained within the proposed concrete tank in the P1 parking level. The retained water will be pumped to the appropriate locations for irrigation. The pump is to be designed by the mechanical engineer in the next design stage.

In addition to the above, a water balance calculation is provided in the Hydrogeological Report. The report identified that the subject site would have a groundwater recharge deficit of 450 m³/year without any mitigation measures. The yearly irrigation demand of the subject site is 709.72 m³/year. As such, it is expected that the yearly runoff exceedance will be balanced with the irrigation of the subject site. As such, the entire water balance deficit will be covered by irrigation during the summer months.

4.2 WATER QUANTITY CONTROL REQUIREMENT

According to the CVC's stormwater quantity control criteria, all rainwater shall be collected by area drains, conveyed to a concrete cistern at underground parking level P1, and discharged to City's storm sewers at a 2-year pre-development flow rate with a maximum runoff coefficient of 0.5 for all storms up to and including 100-year storm.

A concrete cistern will be provided to accommodate the required stormwater storage at underground parking level P1. The location and size of the proposed cistern is shown on Architectural drawings and Dwg. C-02. A section of cistern is provided on Dwg. C-05. The detained stormwater will be discharged to Kirwin Avenue storm sewer at an overcontrolled flow rate of 11.72 L/s through a flow control device. The required orifice size to achieve the target flow would be smaller than the minimum 75mm requirement by Ministry of the Environment Conservation, and Parks (MECP). Therefore, a Contech Vortex Valve Model FA1416 will be installed at the outlet of tank to control the discharge flow refer to [page A-16 in Appendix A for Vortex Valve sizing details.

The tank drawdown time calculation shows the 100-year storm storage will be discharged in 5.67 hours. Refer to page A-13 and A-14 of Appendix A for the calculation details.

Detail of the Vortex control device is provided in Appendix A and Dwg. C-05.

The required and provided on-site stormwater storage volumes as well as the total flow from the proposed site are calculated as shown in Appendix A and summarized in Table 10 below.

Table 10: Post Development Quantity Control as Per City's Requirement

Storm Event	Allowable Discharge Flow (L/s)	Required 5mm on-site Retention (m ³)	Total Detention Storage Required (m ³)	Underground Storage Provided (m ³)
2-Year	11.72	15.4	36.17	170.00
5-Year			56.00	
10-Year			75.45	
25-Year			104.62	
50-Year			123.97	
100-Year			143.56	

4.3 WATER QUALITY CONTROL REQUIREMENT

In order to achieve the long-term average removal of 80% of Total Suspended Solids (TSS) on an annual basis from all runoff leaving the site, the following quality control measures will be provided:

Sub-catchment UC1: Based on the SWM design criteria, the residential building's rooftop area is not subject to vehicular traffic, and the application of sand and de-icing salt constituents, petroleum hydrocarbons and heavy metals. As such, runoff from the roof surface is generally considered to be clean. Table 11 provides a preliminary estimate of the TSS removal level of stormwater leaving the site.

Table 11: TTS Removal Assessment Sub-Catchment OC1

Land Use	Area (m ²)	TSS Removal Efficiency (%)	Composite TSS Removal Efficiency (%)
Roof and Terraces	1300	80	31.4
Driveway and surface parking	1312	0	0
Green roof	403.0	80	9.7
Landscape	300.0	80	7.2
Jellyfish	1312.0	80	80.0
Total	3315.0	-	>80.0

To achieve a TSS removal of 80%, a stormwater quality treatment facility (StormFilter SFPD0806 or approved equivalent) is proposed to treat the flow from the proposed driveway and surface parking areas. Refer to Appendix A and page A-17 for the sizing details and page A-06 for the flow calculation to the Jellyfish unit.

This quality treatment unit will be installed at the inlet of the storage tank at the southeast corner of the site and outside of the underground parking footprint and will receive the flow from driveway and surface parking areas only through internal storm piping. The exact location of the unit and proper internal piping will be determined in coordination with the project team's mechanical engineer and architect in the next design stage.

4.4 EROSION AND SEDIMENT CONTROL DURING CONSTRUCTION

During site construction, it is recommended that all erosion and sediment control Best Management Practices (BMPs) shall be constructed and maintained in accordance with the Toronto and Region Conservation Authority (TRCA) Erosion & Sediment Control Guidelines for Urban Construction (dated 2019). In brief, the measures below are proposed to be provided on-site during the entire period of construction:

- ▶ Siltation control fence along the perimeter of the construction site before commencement of construction;
- ▶ Sediment control measures to prevent silt entry at all the existing catch basins;
- ▶ Granular mud-mats at all construction egress locations (see mud-mat details);
- ▶ An inspection and monitoring program following the *Erosion & Sediment Control Guideline for Urban Construction* (dated 2019).

An erosion and sediment control plan during construction is provided for the proposed development. Refer to Dwg. C-04 Erosion and Sediment Control Plan.

5 FLOODPLAIN REVIEW SUMMARY

The Cooksville Creek watershed is located within the City of Mississauga, east of the Credit River, that drains an area of approximately 33.9 Km² (3,390 ha) and outlets to Lake Ontario.

The Cooksville Creek has been modelled by R.V. Anderson Ltd. in February 1996, subsequently updated and completed by Credit Valley Conservation (CVC). The most updated floodplain map was received from CVC on September 16th, 2020 which includes the proposed development.

It should be noted that the City of Mississauga and Credit Valley Conservation approved and executed a Site Plan Agreement to permit the development of Hotel Mississauga Royale on November 27, 2012, for the proposed site. This previous approval, designed by MSAI Architects, included a northern 22-storey tower (Tower B), a southern 40-storey tower (Tower A) and a 2-story building as a connection between towers.

The previously approved regulatory floodlines, prepared by AMEC, dated February 11, 2011, and the most updated floodplain by CVC are delineated on the grading and servicing plans which are presented in Appendix G. The original floodlines drawing is provided in Appendix F.

6 GROUNDWATER DISCHARGE

In order to obtain information about the subsurface condition, assess any potential subsurface environmental impacts, and investigate the requirement for groundwater discharge from the development site, Azure Group Incorporated (Azure Group) is retained by Weston Consulting to provide a geotechnical investigation and hydrogeological assessment. A map of the borehole & monitoring well investigations from the the hydrogeological assessment report prepared by Azure Group dated October 24, 2022, is provided in Appendix H.

As per the hydrogeological report, ten (10) boreholes were drilled to a maximum depth of 9.0 meters below grade and five of them were completed as groundwater monitoring wells. The hydrogeological assessment provided the following condition with respect to sub-surface soil groundwater conditions:

- ▶ The site is underlain by a thin layer (10cm) overtop of fill mixture consisting of sand, silt and clay of different compositional percentages to a depth of around 3.5 mbgs (meter below ground surface). Below this level the boreholes intersect a native silty-clay layer to the upper contact of the underlain watershed shale bedrock which was encountered in five of the advance boreholes below 7 mbgs. The inclusion of the fragments indicate that the bedrock interface is very close to this depth.
- ▶ Groundwater depths at installed monitoring wells ranged from 4.21 to 5.29 meters below ground surface as measured on May 11th, 2022. The corresponding geodetic groundwater elevations range from approximate elevations of 107.27 and 109.10 meters above sea level (masl);
- ▶ One groundwater sample was collected from monitoring well BH-3 on May 11th, 2022. Groundwater quality analysis of the unfiltered sample was checked against the most stringent objectives of potential discharge points (i.e., Provincial Water Quality Objectives (PWQO), 1994). It is indicated that the only exceedance was with the Total Phosphorous for discharge to storm sewer or natural environment. To confirm the effluent discharge into the storm sewer system, a secondary sample meeting all of the requirements of the City By-Law would need to be collected, which can be confirmed ahead of any potential construction dewatering.

Based on the design of the proposed development, the total depth of the underground structure will extend to a maximum depth of approximately 6.7 meters below the ground surface (mbgs) (107.45 masl). Since the proposed construction will be below the groundwater table, groundwater will be encountered during the excavation. As such, management of groundwater will be required for both construction dewatering and long-term conditions for the proposed development site.

6.1 CONSTRUCTION DEWATERING

According to the Hydrogeology Assessment from Azure, a maximum rate of discharge of 83,160 L/day (0.96 L/s) will be expected from the site with a safety factor of 3, See Appendix G for more details. It is therefore anticipated that there will be groundwater discharge in excess of 50m³/day. As such, the submission of an Environmental Activity and Sector Registration (EASR) to the MECP will be required for construction dewatering. Additional dewatering would be required to manage stormwater capture during construction. However, this is expected to not trigger the need for a Permit to Take Water (PTTW) during rainfall events less than the 5-year return period. If the site experiences a 5-year storm event (56mm across 24 hours) during the excavation, an additional 289 m³ must be discharged from the site. In this event, pumping could continue under the registered ESAR. Storm events above the 5-year return period can be discharged over multiple days to avoid the need for a PTTW.

During construction, the groundwater will discharge from the excavation site to the existing 250mm sanitary sewer along Kirwin Avenue or the existing 400mm storm sewer along Kirwin Avenue. The water quality of the groundwater sample indicated only an exceedance of Total Phosphorous based on the PWQO requirements. As such, the groundwater will require Total Phosphorous treatment prior to discharge.

6.2 LONG-TERM DEWATERING

The building is currently proposed to be constructed to watertight standards as identified in a letter signed by the Owner. The planned watertight foundation will limit potential concerns with respect to groundwater at

the site with regards to permanent dewatering of the site. The signed letter from the Owner has been provided in Appendix H.

7 SITE SERVICING

The purpose of this site servicing study is to review the site servicing requirement of the proposed new 8-storey apartment development and recommend a site servicing plan, including water supply, sanitary and storm services. Refer to Drawing C-02 in Appendix G -Site Servicing Plan for details of the proposed site service connections.

7.1 EXISTING MUNICIPAL SERVICES

The proposed development will require new service connections to the existing municipal storm sewers, sanitary sewers, and watermain located on Kirwin Avenue adjacent to the site. Existing underground municipal services/utilities on Kirwin Avenue are summarized below:

- a) 400mm dia. concrete storm sewer;
- b) 250mm dia. concrete sanitary sewer;
- c) 300mm dia. ductile iron watermain on the Northside of Kirwin Ave.;

7.2 PROPOSED SITE SERVICE CONNECTIONS

The sanitary demands have been assessed by determining the total population, sanitary generation rates, and peaking factors as outlined in the Region of Peel Criteria and the 2020 Peel Region DC Background Study. Based on the 2020 Peel Region DC Background study, the population to be considered for units less than 750 sq.ft. (69.7m²) in size and greater than 750 sq.ft. (69.7m²) in size shall be 1.6 and 3.0 respectively. As such, the total population on the subject site is 297. Using the Region of Peel standard rates and the Harmon Peaking Factor, this would result in a total domestic demand of 4.25 L/s. However, based on the total Region of Peel STD.DWG 2-5-2, the total domestic flow for populations less than 1000 should be considered as 13 L/s. Therefore, after accounting for infiltration, the total sanitary flow is 13.08 L/s.

Water demands have been calculated based on the same population estimate determined for the sanitary servicing of 297 persons. This population estimate was used in conjunction with the demand rates and factors provided by the Region of Peel to determine the maximum day demand of 0.96 L/s and the Peak Hour demand of 2.89 L/s. Using the Fire Underwriters Survey (2020) to calculate the fire demand yields a fire flow demand of 166.67 L/s. As such, the fire flow plus maximum day demand is 168.59 L/s.

Based on the project statistics of the proposed development provided by the architect, and design criteria of City and Region, sanitary flow and water demand are estimated in Appendix C and summarized in Table 13. The site storm flow discharge rate has been provided in the previous section of this report. A Single-Use Demand Table has been provided in Appendix C for use by the Region of Peel.

Table 13: Site Servicing Requirement

Site	Storm Discharge Rate (L/s)	Sanitary Discharge Rate (L/s)	Water Demand (L/s)
8-storey apartment	11.72	13.08	168.59

Through discussion with the design team, the locations and sizes of the proposed site service connections have been determined to satisfy the requirements of the City of Mississauga, Region of Peel and the Ontario Building Code (OBC). In summary:

1. Sanitary Service: A 150mm dia. sanitary service connection will be installed to service the proposed 8-storey apartment building and discharge to proposed manhole No. MH1B on the exiting 250mm concrete sanitary sewer on Kirwin Avenue.
2. Storm Service: A 200mm dia. storm service connection will be installed to drain the 8-storey apartment building area to the proposed manhole No. MH1A on the existing 400mm storm sewer on Kirwin Avenue.
3. Water service:
 - ▶ Domestic Water Service: A 100mm dia. domestic water service connection will be installed to service the proposed 8-storey apartment building and connected to the proposed 150mm dia. fire protection water service with a cut-in Tee.
 - ▶ Fire Protection Service: A 150mm fire protection PVC water service will be provided.

The existing 300mm diameter watermain on Kirwin Avenue will be utilized to service the proposed development site.

Based on the proposed underground parking P2 elevation of 107.45 m, sanitary flow from this floor will not be able to discharge to the City's sanitary sewer (Inv. 109.23m) by gravity. Therefore, pumps will be required. Pumps, piping and backflow preventers will be designed by a mechanical engineer in the next design phase.

Refer to Drawing C-02 in Appendix G for details of proposed service connections.

7.3 ADEQUACY OF EXISTING MUNICIPAL SERVICES

Sanitary

The subject development is anticipated to have a population of 297 people based on the latest architectural plans and the rates provided in the 2020 DC background study. When considering the per person sanitary demand and the Harmon peaking factor, and infiltration, the actual design flow is expected to be 4.33 L/s. However, based on the Region of Peel STD. DWG. 2-5-2 (Region of Peel, Sanitary Sewer Design Criteria, 2009), total domestic flow for areas with less than 1000 persons shall be considered to have a design flow of 13 L/s. Thus, the design flow after considering infiltration is 13.08 L/s. Refer to Appendix C for detailed calculations on the sanitary demands.

The Region of Peel will perform a capacity assessment of the downstream sanitary sewers for the subject development based on the above calculations.

Storm

Based on the City's design criteria, drainage area plan, record drawings, and CCTV investigation, an assessment of the existing storm sewers from the site in Kirwin Ave to the existing culvert in Dundas Street East are reviewed below:

The existing 400mm storm sewer in Kirwin Ave (identified and confirmed through the CCTV inspection), as shown on the storm drainage areas plan, is designed based on a 10-year design storm and a runoff coefficient of $C=0.45$. The review of the drainage plan shows that the existing plaza (157 Dundas St. E.) at the northeast quadrant of Kirwin Ave and Dundas Street East has been developed later. The CCTV inspection identified the location of area drains and storm sewers within the development at the northeast quadrant of Kirwin Avenue and Dundas Street East. The drainage area plan for the downstream capacity analysis has been updated based on the location and extent of the storm management system in the property in the northeast quadrant of Kirwin Avenue and Dundas Street East.

Based on the above assumption, the runoff coefficient is updated according to the existing land use. The flow is calculated and summarized in Table 14.

Table 14: Downstream Sewer Capacity – Proposed Condition

Street	Manhole To-From	Accumulative Drainage Area (ha)*	Q 10-yr Flow (L/S)	Q _{full} Full Capacity (L/S)	Q _{full} /Q
Kirwin Avenue	MH31 to 5	1.019	156	233	0.67
Kirwin Avenue	5 to 4 (MH30)	1.285	218	233	0.94
Dundas Street East	4 (MH30) to 3	36.925	4013	4431	0.91
Dundas Street East	3 to 2	37.285	4013	4416	0.91
Dundas Street East	2 to 1 (culvert)	37.465	3985	4507	0.88

*Accumulative Drainage Area in this table includes the area from the Subject Site in post-development conditions.

Under post-development conditions, the discharge storm flows from the site will be controlled to 2-yr pre-development or 16.21 L/s which is less than the 10-yr flow rate of 33.29 L/s under the existing condition. As described in Section 4, the site is overcontrolled to account for the 100-year uncontrolled release to Kirwin Avenue. In the downstream sewer analysis, this flow is accounted for as the 10-year flow. Therefore, the total flow to the existing storm sewer in Kirwin Avenue will be decreased from 240 L/s to 218 L/s which is less than the existing 400mm storm sewer capacity. The flow calculation and updated runoff coefficient and design sheets are provided in Appendix D. It should be noted that only a small portion of the 400mm sewer on Kirwin Avenue experiences a Q/Q_{full} ratio of 0.94. This occurs downstream of the location where the catch basins in the intersection of Kirwin and Dundas connect into the sewer. Refer to Figure 3 in Appendix D for details on the location of this connection point. As such, the majority of the 400mm sewer on Kirwin Avenue experiences a Q/Q_{full} ratio of 0.67 in post-development conditions.

Since the proposed conditions do not demonstrate a surcharge condition within the downstream sewers, it is not expected that any upgrades will be required within the downstream storm sewer network.

Watermain

The design water demand is estimated as 168.59 L/s (1879.68 US GPM) based on the project statistics. In order to evaluate the adequacy of the 300mm watermain located on Kirwin Avenue, a hydrant flow test was conducted on June 15, 2017, by Focus Fire Protection. Test results are included in Appendix E.

As shown by the test readings, the available water pressure ranges from 74 psi with a flow of 1521 US GPM to 76 psi with a flow of 1000 US GPM during the flow test with a static pressure of 80 psi. At the design water demand of 168.59 L/s (2672.18 US GPM) generated from the development, the flow test results show a residual pressure of 57.4 psi, which is greater than the minimum requirement of 20 psi (150 kPa). Therefore, adequate water supply and pressure are available to serve the proposed development.

It should be noted that the design and location of the building does not allow for all portions of the building faces to be less than 90m from the nearest hydrant. As such, a private hydrant is proposed on the site at the northern limit of the site. This private hydrant will provide the required coverage of all portions of all faces of the building. Please refer to Drawing C-02 for details on the location of the private hydrant.

8 CONCLUSIONS

Stormwater Management Plan

- ▶ Under the existing condition, there are no existing on-site stormwater management facilities.
- ▶ An on-site storage volume of approximately 15.40 m³ will be provided by the underground cistern and bio-swale for retaining the first 5mm of rainfall runoff as required to achieve the water balance target. This portion of water will be re-used on-site for irrigation during 72 hours and a small portion will infiltrate into soil through bio-swale.
- ▶ An on-site storage tank with approximately 170 m³ in volume will be provided in order to control the post-development 100-year stormwater flows to 2-year pre-development level.
- ▶ To satisfy the City's 80% TSS removal, a stormwater quality treatment facility (StormFilter SFPD0806 or approved equivalent) is proposed for Sub-Catchment Area OC1.
- ▶ Sub-catchment C2 includes the land to be dedicated to the parkland and to remain as the existing condition. Therefore, no stormwater management plan is required.

Temporary Erosion & Sediment Control Measures

- ▶ Temporary erosion and sediment control measures will be provided before construction and maintained during construction in accordance with CVC CA's "Stormwater Management Criteria"

Groundwater Discharge

- ▶ According to the Hydrogeology Assessment from Azure, a maximum rate of discharge of 83,160 L/day (0.96 L/s) of groundwater will be expected from the site with a safety factor of 3 and 289,000 L/day stormwater based on the 5-year storm event. The submission of an Environmental Activity and Sector Registration (EASR) to the MECP will be required for construction dewatering.

- ▶ The building is currently proposed to be constructed to watertight standards. Therefore, no long-term groundwater discharge is expected.

Site Servicing

Proposed site service connections for the proposed development site:

- ▶ Storm service: 200mm dia. PVC pipes
- ▶ Sanitary service: 150mm dia. PVC pipes
- ▶ Water service:
 - 100mm dia. PVC pipe for domestic water supply
 - 150mm dia. PVC pipe for fire water supply

Prepared By:
LEA Consulting Ltd.




Farshid Morshedi, P.Eng.
Water Resources Engineer

A handwritten signature in black ink, appearing to read "Pavel Recnik".

Pavel Recnik, EIT
Hydraulic Modelling Lead

APPENDIX A

Stormwater Peak Flow and Storage Calculation
and SWM Details for Sub-Catchment Area EC1,
OC1 and UC1

 LEA Consulting Ltd. Consulting Engineers and Planners	Land Use			
	Prepared:	P.R.	Page No.	A-01
	Checked:	F.M.		
	Proj. #	21111		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Date:	25-Oct-23		

Pre-Development CONDITION

Sub-Catchment EC1

Existing Land Use	Area (m ²)
Building	360.0
Asphalt	759.0
Lawn & Tree	830.0
Sum. Area:	1949.0


Post-Development Condition:

Sub-Catchment OC1

Proposed Land Use	Area (m ²)
Building (without green roof)	1421.5
Paved Area	1096.6
Green Roof	466.0
Landscaped Area	316.4
Sum. Area:	3300.5

Sub-Catchment UC1

Proposed Land Use	Area (m ²)
Paved Area	126.7
Landscaped Area	3.9
Sum. Area:	130.6

 LEA Consulting Ltd. Consulting Engineers and Planners	Composite "C" Calculation			
	Prepared:	P.R.	Page No.	A-02
	Checked:	F.M.		
	Proj. #	21111		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga		Date:	25-Oct-23	
SUB-CATCHMENT EC1 & PC1 (OC1+UC1)				

Pre-Development Composite Runoff Coefficient "C"

Sub-Catchment EC1

Existing Land Use	Area (ha)	C	Composite "C"
Building	0.036	0.90	
Asphalt	0.076	0.90	
Lawn & Tree	0.083	0.25	
Sum. Area:	0.195		0.62
			0.50 As per City's Criteria
Imperviousness Percent:	57.4		


Post-Development Composite Runoff Coefficient "C"

Sub-Catchment OC1

Proposed Land Use	Area (ha)	C	Composite "C"
Building (without green roof)	0.142	0.90	
Paved Area	0.110	0.90	
Green Roof	0.047	0.25	
Landscaped Area	0.032	0.4	
Sum. Area:	0.330		0.76
			0.90 As per City's request
Imperviousness Percent:	76.3		

Sub-Catchment UC1

Proposed Land Use	Area (ha)	C	Composite "C"
Paved Area	0.013	0.90	
Landscaped Area	0.0004	0.25	
Sum. Area:	0.013		0.88
Imperviousness Percent:	97.0		
Total Site Area:			0.343
Composite runoff coefficient for entire site:			0.76
Total impervious percent:			77.1

 LEA Consulting Ltd. Consulting Engineers and Planners	5mm Rainfall Retention Volume			
	(Water Balance)			
	Prepared:	P.R.	Page No.	A-03
	Checked:	F.M.		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Proj. #	21111		
	Date:	25-Oct-23		


According to the CVC Guidelines, in order to achieve the water balance target, it is required to retain all runoff from a small event - typically 5mm (in Toronto, storms with 24 hour volumes of 5mm or less contribute about 50% of the total average annual rainfall volume) through infiltration, evapotranspiration & rainwater reuse.

Site Area: 0.343 ha
Total Site Impervious Area: 0.264 ha

Runoff volume from 5mm rainfall event on site:

$$V = 0.264 \times 10 \times 5 = 13.2 \text{ m}^3$$

Required on-site retention volume for 5mm rainfall event: 13.2 m³

 LEA Consulting Ltd. Consulting Engineers and Planners	Pre-Development Peak Flow Rates Calculation			
	Prepared:	P.R.	Page No.	A-04
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Checked:	F.M.		
	Proj. #	21111		
	Date:	25-Oct-23		

Rational Formulae: $Q = 2.78 \text{ CIA (L/s)}$

Site Area: 0.195 ha
Time of Concentration 15 minutes as per City Guidelines
Runoff Coefficient : 0.50 As per City's Criteria

Rainfall Intensity: $I = a/(Tc+b)^c$ (City Std. 2111.010)

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Rainfall Intensity (mm/hr):	59.89	80.51	99.17	113.89	127.13	140.69


Peak Flow Rate (L/s):

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Under existing site conditions (L/s):	16.21	21.80	26.85	30.83	34.42	38.09

The proposed site is under Cooksville Creek and requires to control post development flow to 2-year pre development flow for storm events that include the regional storm based on the CVC stormwater management Criteria, 2012.
Furthermore, the storm runoff from the building frontage along the Kirwin Avenue (Sub-catchment UC1) is not feasible to be controlled due to the site constraint, therefore, the stormwater discharge from catchment OC1 will be overcontrolled. I.e. allowable discharge flow rate from sub-catchment OC1 will be:

Sub-catchment UC1 (Post Development 100-yr storm): 4.50 L/s
Sub-catchment OC1 (Pre-development 2-yr storm): 16.21 L/s

Overcontrolled discharge rate from sub-Catchment OC1 into municipal storm sewer on Kirwin Avenue: 11.72 L/s

 LEA Consulting Ltd. Consulting Engineers and Planners	Post-Development Peak Flow Rates Calculation (Uncontrolled)			
	Prepared:	P.R.	Page No.	A-05
	Checked:	F.M.		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Proj. #	21111		
	Date:	25-Oct-23		

Rational Formulae: $Q = 2.78 \text{ CIA (L/s)}$

Overcontrolled Area (OC1): 0.330 ha
Time of Concentration: 15 minutes as per City Guidelines
Runoff Coefficient : 0.90 As per City's request

Uncontrolled Area (UC1): 0.013 ha
Time of Concentration: 15 minutes as per City Guidelines
Runoff Coefficient : 0.88

Runoff Coefficient Adjustment Factors	Adjusted runoff coefficient
1.00 (10-year)	0.9
1.10 (25-year)	0.99
1.20 (50-year)	1.0
1.25 (100-year)	1.0

Rainfall Intensity: $I = a/(Tc+b)^c$ (City Std. 2111.010)

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Rainfall Intensity (mm/hr):	59.89	80.51	99.17	113.89	127.13	140.69


Peak Flow Rates (L/s):

Sub-Catchment OC1

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Under Post development site conditions (L/s):	49.42	66.44	81.83	93.98	104.91	116.10
Under Post development condition with Adjustment Factors (L/s):	49.42	66.44	81.83	103.38	116.57	129.00

Sub-Catchment UC1

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Under Post development site conditions (L/s):	1.91	2.57	3.17	3.64	4.06	4.50

 LEA Consulting Ltd. Consulting Engineers and Planners	Post-Development Peak Flow Rates to Jellyfish Filter			
	Prepared:	P.R.	Page No.	A-06
	Checked:	F.M.		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Proj. #	21111		
	Date:	25-Oct-23		

Rational Formulae: $Q = 2.78 \text{ CIA (L/s)}$

Non-clean drainage area 0.064 ha
 Time of Concentration: 15 minutes as per City Guidelines
 Runoff Coefficient : 0.90 As per City's request

Runoff Coefficient Adjustment Factors	Adjusted runoff coefficient
1.00 (10-year)	0.9
1.10 (25-year)	0.99
1.20 (50-year)	1.0
1.25 (100-year)	1.0


Rainfall Intensity: $I = a/(Tc+b)^c$ (City Std. 2111.010)

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Rainfall Intensity (mm/hr):	59.89	80.51	99.17	113.89	127.13	140.69

Peak Flow Rates (L/s):

Non-clean drainage area

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Under Post development site conditions (L/s):	9.54	12.82	15.79	18.14	20.25	22.41
Under Post development condition with Adjustment Factors (L/s):	9.54	12.82	15.79	19.95	22.50	24.90


 LEA Consulting Ltd. Consulting Engineers and Planners	On-Site Storage Calculation (2-Year Storm)			
	Prepared:	P.R.	Page No.	A-07
	Checked:	F.M.		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Proj. #	21111		
	Date:	25-Oct-23		

Total Drainage Area (ha) = 0.330 ha
Drainage Area Composite C = 0.90
Allowable Release Rate = 11.72 L/s
Return Period = 2 Year

Site storage Requirement:

Time (minutes)	Rainfall Intensity (mm/hr)	Peak Flow (L/s)	Storm Runoff Volume (m ³)	Release Rate (L/s)	Release Flow Volume (m ³)	Required Storage Volume (m ³)
15	59.89	49.42	44.48	11.72	10.55	33.93
20	50.16	41.40	49.67	11.72	14.06	35.61
25	43.42	35.83	53.75	11.72	17.58	36.17
30	38.45	31.73	57.11	11.72	21.09	36.02
35	34.60	28.55	59.97	11.72	24.61	35.36
40	31.54	26.03	62.46	11.72	28.12	34.34
45	29.03	23.96	64.68	11.72	31.64	33.04
50	26.94	22.23	66.68	11.72	35.16	31.52
55	25.16	20.76	68.50	11.72	38.67	29.83
60	23.62	19.49	70.18	11.72	42.19	27.99
65	22.29	18.39	71.73	11.72	45.70	26.03
70	21.12	17.42	73.18	11.72	49.22	23.96
75	20.07	16.56	74.54	11.72	52.73	21.81
80	19.14	15.80	75.82	11.72	56.25	19.57
85	18.30	15.10	77.03	11.72	59.76	17.27
90	17.54	14.48	78.18	11.72	63.28	14.90
95	16.85	13.91	79.27	11.72	66.79	12.48
100	16.22	13.39	80.32	11.72	70.31	10.01
105	15.64	12.91	81.32	11.72	73.83	7.49
110	15.11	12.47	82.27	11.72	77.34	4.93

Required Storage Volume = 36.17 m³


 LEA Consulting Ltd. Consulting Engineers and Planners	On-Site Storage Calculation (5-Year Storm)			
	Prepared:	P.R.	Page No.	A-08
	Checked:	F.M.		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Proj. #	21111		
	Date:	25-Oct-23		

Total Drainage Area (ha) = 0.330 ha
Drainage Area Composite C = 0.90
Allowable Release Rate = 11.72 L/s
Return Period = 23.44 Year

Site storage Requirement:

Time (minutes)	Rainfall Intensity (mm/hr)	Peak Flow (L/s)	Storm Runoff Volume (m ³)	Release Rate (L/s)	Release Flow Volume (m ³)	Required Storage Volume (m ³)
15	80.51	66.44	59.79	11.72	10.55	49.24
20	67.43	55.65	66.78	11.72	14.06	52.72
25	58.37	48.17	72.25	11.72	17.58	54.67
30	51.68	42.65	76.76	11.72	21.09	55.67
35	46.52	38.39	80.61	11.72	24.61	56.00
40	42.40	34.99	83.97	11.72	28.12	55.85
45	39.02	32.20	86.95	11.72	31.64	55.31
50	36.21	29.88	89.64	11.72	35.16	54.48
55	33.82	27.90	92.09	11.72	38.67	53.42
60	31.76	26.21	94.34	11.72	42.19	52.15
65	29.96	24.72	96.43	11.72	45.70	50.73
70	28.38	23.42	98.37	11.72	49.22	49.15
75	26.98	22.27	100.20	11.72	52.73	47.47
80	25.73	21.23	101.92	11.72	56.25	45.67
85	24.60	20.30	103.55	11.72	59.76	43.79
90	23.58	19.46	105.09	11.72	63.28	41.81
95	22.66	18.70	106.56	11.72	66.79	39.77
100	21.81	17.99	107.97	11.72	70.31	37.66
105	21.03	17.35	109.31	11.72	73.83	35.48
110	20.31	16.76	110.60	11.72	77.34	33.26

Required Storage Volume = 56.00 m³


 LEA Consulting Ltd. Consulting Engineers and Planners	On-Site Storage Calculation (10-Year Storm)			
	Prepared:	P.R.	Page No.	A-09
	Checked:	F.M.		
	Proj. #	21111		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Date:	25-Oct-23		

Total Drainage Area (ha) = 0.330 ha
Drainage Area Composite C = 0.90
Allowable Release Rate = 11.72 L/s
Return Period = 10 Year

Site storage Requirement:

Time (minutes)	Rainfall Intensity (mm/hr)	Peak Flow (L/s)	Storm Runoff Volume (m ³)	Release Rate (L/s)	Release Flow Volume (m ³)	Required Storage Volume (m ³)
15	99.17	81.83	73.65	11.72	10.55	63.10
20	83.06	68.54	82.25	11.72	14.06	68.19
25	71.90	59.33	88.99	11.72	17.58	71.41
30	63.66	52.53	94.55	11.72	21.09	73.46
35	57.30	47.28	99.29	11.72	24.61	74.68
40	52.22	43.09	103.42	11.72	28.12	75.30
45	48.07	39.66	107.09	11.72	31.64	75.45
50	44.60	36.80	110.40	11.72	35.16	75.24
55	41.65	34.37	113.42	11.72	38.67	74.75
60	39.11	32.28	116.20	11.72	42.19	74.01
65	36.91	30.45	118.77	11.72	45.70	73.07
70	34.96	28.85	121.17	11.72	49.22	71.95
75	33.24	27.43	123.42	11.72	52.73	70.69
80	31.69	26.15	125.54	11.72	56.25	69.29
85	30.31	25.01	127.54	11.72	59.76	67.78
90	29.05	23.97	129.44	11.72	63.28	66.16
95	27.90	23.03	131.25	11.72	66.79	64.46
100	26.86	22.16	132.98	11.72	70.31	62.67
105	25.90	21.37	134.64	11.72	73.83	60.81
110	25.01	20.64	136.22	11.72	77.34	58.88

Required Storage Volume = 75.45 m³


 LEA Consulting Ltd. Consulting Engineers and Planners	On-Site Storage Calculation (25-Year Storm)			
	Prepared:	P.R.	Page No.	A-010
	Checked:	F.M.		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Proj. #	21111		
	Date:	25-Oct-23		

Total Drainage Area (ha) = 0.330 ha
Drainage Area Composite C = 0.90
Allowable Release Rate = 11.72 L/s
Return Period = 25 Year
adjusted Runoff coefficient = 1.1
Adjustment runoff coefficient = 0.99

Site storage Requirement:

Time (minutes)	Rainfall Intensity (mm/hr)	Peak Flow (L/s)	Storm Runoff Volume (m ³)	Release Rate (L/s)	Release Flow Volume (m ³)	Required Storage Volume (m ³)
15	113.89	103.38	93.04	11.72	10.55	82.49
20	95.40	86.59	103.91	11.72	14.06	89.85
25	82.58	74.95	112.43	11.72	17.58	94.85
30	73.11	66.36	119.45	11.72	21.09	98.36
35	65.80	59.73	125.44	11.72	24.61	100.83
40	59.98	54.44	130.66	11.72	28.12	102.54
45	55.21	50.11	135.30	11.72	31.64	103.66
50	51.22	46.49	139.48	11.72	35.16	104.32
55	47.84	43.42	143.29	11.72	38.67	104.62
60	44.92	40.78	146.80	11.72	42.19	104.61
65	42.39	38.47	150.05	11.72	45.70	104.35
70	40.15	36.45	153.08	11.72	49.22	103.86
75	38.17	34.65	155.92	11.72	52.73	103.19
80	36.40	33.04	158.60	11.72	56.25	102.35
85	34.81	31.59	161.13	11.72	59.76	101.37
90	33.36	30.28	163.53	11.72	63.28	100.25
95	32.05	29.09	165.82	11.72	66.79	99.03
100	30.85	28.00	168.00	11.72	70.31	97.69
105	29.74	27.00	170.10	11.72	73.83	96.27
110	28.73	26.08	172.10	11.72	77.34	94.76

Required Storage Volume = 104.62 m³


 LEA Consulting Ltd. Consulting Engineers and Planners	On-Site Storage Calculation (50-Year Storm)			
	Prepared:	P.R.	Page No.	A-11
	Checked:	F.M.		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Proj. #	21111		
	Date:	25-Oct-23		

Total Drainage Area (ha) = 0.330 ha
Drainage Area Composite C = 0.90
Allowable Release Rate = 11.72 L/s
Return Period = 50 Year
Runoff coefficient adjustment factor = 1.2
Adjustment runoff coefficient = 1.0

Site storage Requirement:

Time (minutes)	Rainfall Intensity (mm/hr)	Peak Flow (L/s)	Storm Runoff Volume (m ³)	Release Rate (L/s)	Release Flow Volume (m ³)	Required Storage Volume (m ³)
15	127.13	116.57	104.91	11.72	10.55	94.36
20	106.57	97.71	117.26	11.72	14.06	103.20
25	92.30	84.63	126.94	11.72	17.58	109.36
30	81.75	74.95	134.92	11.72	21.09	113.83
35	73.60	67.48	141.72	11.72	24.61	117.11
40	67.10	61.52	147.65	11.72	28.12	119.53
45	61.77	56.64	152.92	11.72	31.64	121.28
50	57.32	52.56	157.67	11.72	35.16	122.51
55	53.54	49.09	162.00	11.72	38.67	123.33
60	50.28	46.11	165.98	11.72	42.19	123.79
65	47.45	43.50	169.67	11.72	45.70	123.97
70	44.95	41.22	173.11	11.72	49.22	123.89
75	42.74	39.18	176.33	11.72	52.73	123.60
80	40.76	37.37	179.37	11.72	56.25	123.12
85	38.97	35.73	182.24	11.72	59.76	122.48
90	37.36	34.25	184.97	11.72	63.28	121.69
95	35.89	32.91	187.56	11.72	66.79	120.77
100	34.54	31.67	190.04	11.72	70.31	119.73
105	33.31	30.54	192.41	11.72	73.83	118.58
110	32.17	29.50	194.69	11.72	77.34	117.35

Required Storage Volume = 123.97 m³


 LEA Consulting Ltd. Consulting Engineers and Planners	On-Site Storage Calculation (100 - Year Storm)			
	Prepared:	P.R.	Page No.	A-12
	Checked:	F.M.		
3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga SUB-CATCHMENT EC1 & PC1 (OC1+UC1)	Proj. #	21111		
	Date:	25-Oct-23		

Total Drainage Area (ha) = 0.330 ha
Drainage Area Composite C = 0.90
Allowable Release Rate = 11.72 L/s
Return Period = 100 Year
Runoff coefficient adjustment factor = 1.25
Adjustment runoff coefficient = 1.0

Site storage Requirement:

Time (minutes)	Rainfall Intensity (mm/hr)	Peak Flow (L/s)	Storm Runoff Volume (m ³)	Release Rate (L/s)	Release Flow Volume (m ³)	Required Storage Volume (m ³)
15	140.69	129.00	116.10	11.72	10.55	105.55
20	118.12	108.30	129.96	11.72	14.06	115.90
25	102.41	93.90	140.85	11.72	17.58	123.27
30	90.77	83.23	149.81	11.72	21.09	128.72
35	81.77	74.98	157.45	11.72	24.61	132.84
40	74.58	68.38	164.11	11.72	28.12	135.99
45	68.68	62.97	170.03	11.72	31.64	138.39
50	63.75	58.45	175.36	11.72	35.16	140.20
55	59.56	54.61	180.22	11.72	38.67	141.55
60	55.95	51.30	184.68	11.72	42.19	142.49
65	52.81	48.42	188.82	11.72	45.70	143.12
70	50.03	45.88	192.68	11.72	49.22	143.46
75	47.58	43.62	196.29	11.72	52.73	143.56
80	45.38	41.60	199.70	11.72	56.25	143.45
85	43.39	39.79	202.92	11.72	59.76	143.16
90	41.60	38.14	205.97	11.72	63.28	142.69
95	39.97	36.65	208.88	11.72	66.79	142.09
100	38.47	35.28	211.65	11.72	70.31	141.34
105	37.10	34.02	214.31	11.72	73.83	140.48
110	35.84	32.86	216.86	11.72	77.34	139.52

Required Storage Volume = 143.56 m³

	LEA Consulting Ltd. Consulting Engineers and Planners	Storm Tank Drawdown Time				
		Prepared:	P.R.	Page No.	A-13	
		Checked:	F.M.			
		Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga		Proj. #	21111	
				Date:	25-Oct-23	

Calculating the change in the stage within the tank over time using the Storage-Indication method.

Storage Indication Method calculations based on the method presented in Water Resources Engineering, Third Edition, David A. Chin,)

The calculation is based on the below formula

$$(I_1 + I_2) + \left(\frac{2S_1}{\Delta t} - O_1 \right) = \left(\frac{2S_2}{\Delta t} - O_2 \right)$$

Where subscript 1 indicates the current time step and sub-script 2 indicates the next time step

I: Inflow

dt: Time Interval

S: Storage

O: Outflow


To simplify the calculation, the individual components are calculated using the below table. Stage-Storage outflow table is presented in A-14 based on the tank geometry and the vortex control structure

The tank is assumed to start with the 100-year level and receive no additional flow

Initialize stage: 1.74 m
Time Step: 20 minutes

Time (minutes)	I (m3/s)	2S/dt-O (m3/s)	2S/dt+O (m3/s)	O (m3/s)	stage (m)
0	0	0.17	0.19	0.01	1.74
20	0	0.15	0.17	0.01	1.53
40	0	0.13	0.15	0.01	1.33
60	0	0.11	0.13	0.01	1.14
80	0	0.09	0.11	0.01	0.96
100	0	0.07	0.09	0.01	0.79
120	0	0.06	0.07	0.01	0.64
140	0	0.05	0.06	0.01	0.50
160	0	0.03	0.05	0.01	0.39
180	0	0.02	0.03	0.00	0.29
200	0	0.02	0.02	0.00	0.20
220	0	0.01	0.02	0.00	0.12
240	0	0.00	0.01	0.00	0.06
260	0	0.00	0.00	0.00	0.03
280	0	0.00	0.00	0.00	0.02
300	0	0.00	0.00	0.00	0.01
320	0	0.00	0.00	0.00	0.01
340	0	0.00	0.00	0.00	0.00
360	0	0.00	0.00	0.00	0.00
380	0	0.00	0.00	0.00	0.00
400	0	0.00	0.00	0.00	0.00
420	0	0.00	0.00	0.00	0.00
440	0	0.00	0.00	0.00	0.00

Tank Drawdown Time 340 minutes
5:40 Hours

	LEA Consulting Ltd. Consulting Engineers and Planners		Storm Tank Stage-Storage Calculation			
			Prepared:	P.R.	Page No.	A-14
	Checked:	F.M.				
	Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE- City of Mississauga		Proj. #	21111		
Date:			25-Oct-23			

In order to perform the Storage-Indication Method, the follow table needed to be developed. Storage is developed from Stage based on the area of the tank, and outfall is developed from stage based on the Vortex Valve control structure.

Time Step: 20 minutes

Stage Storage Outflow Curve

stage	S	O	2S/dt+O
m	m3	m3/s	m3/s
0	0	0	0
0.038	2.34	0.0012	0.0051
0.076	4.69	0.0024	0.0102
0.114	7.03	0.0037	0.0154
0.152	9.38	0.0044	0.0200
0.191	11.78	0.0045	0.0242
0.229	14.13	0.0045	0.0281
0.267	16.47	0.0045	0.0320
0.305	18.82	0.0049	0.0363
0.343	21.16	0.0053	0.0405
0.381	23.50	0.0056	0.0448
0.419	25.85	0.0059	0.0489
0.457	28.19	0.0062	0.0531
0.61	37.63	0.0072	0.0699
0.762	47.01	0.0081	0.0864
0.914	56.39	0.0089	0.1029
1.067	65.82	0.0095	0.1192
1.219	75.20	0.0099	0.1352
1.372	84.64	0.0102	0.1513
1.524	94.02	0.0105	0.1672
1.676	103.39	0.0108	0.1831
1.829	112.83	0.0110	0.1990
1.981	122.21	0.0112	0.2149
2.134	131.65	0.0114	0.2308
2.286	141.03	0.0116	0.2466
2.438	150.40	0.0117	0.2624
2.591	159.84	0.0119	0.2783
2.743	169.22	0.0121	0.2941
2.896	178.66	0.0122	0.3100
3.048	188.03	0.0123	0.3257

APPENDIX A-15

Estimation of the Percolation Rate and
Permeability of the Soil Letter

Azure Group





October 13, 2022

2202-001

Page 1 of 2

Weston Consulting
201 Millway Avenue #19, Concord
ON L4K 5K8

Attention: Mr. Kaveh Wahdat - Planner

Re: **Estimation of the Percolation Rate and Permeability of the Soil at**
3016 - 3032 Kirwin Avenue and 3031 Little John Lane, Mississauga

Dear Sir,

Azure Group carried out geotechnical investigations for the site located at 3016 - 3031 Kirwin Avenue and 3031 Little John Lane in Mississauga, Ontario, project number 2202-001 dated April 2022 to provide recommendations for the design and construction of multi storey building. Ten (10) boreholes were advanced at various locations to depths ranging between ± 8 m and refusal depth of ± 11 m below the existing ground surface and were sampled at 0.75 m (up to 3 m depth) and 1.5 m interval below 3 m depth with a conventional 50 mm diameter split barrel samplers when Standard Penetration Test (SPT) was carried out. The soil samples obtained from the spoons were then tested to obtain the engineering parameters and properties to be used for the design of the building.

However, parameters to obtain the percolation rate "T" and permeability "K" of the soils (for the design of Storm Water Managements "SWM" and/or swells) were not determined since they were not in the scope of work.

The percolation rate "T" and permeability "K" may be obtained directly from field test or indirectly from soil description (grain size analysis) as recommended by the Ontario Building Code (OBC) Supplementary Standard SP-7 Table 2. Table 2 provides an estimate of percolation Rate "T" and coefficient of permeability "K" of the soil based on soil description.

Since field percolation tests were not carried out at the time of the geotechnical investigation, OBC Supplementary Standard tables were used to estimate the percolation rate and permeability of the soil.

Table 1 provides a summary of the percolation and permeability of the soils obtained from the boreholes at various depths:

BH No.	Depth (m)	Type of soil	K (cm/sec)	T (min./cm)	Comments
BH101	0 - 2.3	Silty clay/clayey silt	$10^{-5} - 10^{-6}$	20 - 50	Medium to low permeability
	2.3 - 4.6	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
BH102	0 - 1.5	Silty clay/clayey silt	$10^{-5} - 10^{-6}$	20 - 50	Medium to low permeability
	1.5 - 2.3	Silty clay/clayey silt	$10^{-5} - 10^{-6}$	20 - 50	Medium to low permeability



	2.3 - 4.6	Sand & gravel	$10^{-1} - 10^{-3}$	2 - 8	Medium to low permeability
BH103	0 - 2.3	Silty clay	$10^{-5} - 10^{-6}$	20 - 50	Medium to low permeability
	2.3 - 4.6	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
BH104	0 - 0.8	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
	0.8 - 4.6	Clayey silt/silty clay	$10^{-5} - 10^{-6}$	20 - 50	Medium to low permeability
BH105	0 - 0.8	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
	0.8 - 1.5	Sand trace clay	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
	1.5 - 4.6	Sand/silty sand	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
BH106	0 - 1.5	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
	1.5 - 4.6	Clayey silt	$10^{-5} - 10^{-6}$	20 - 50	Medium to low permeability
BH107	0 - 4.6	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
BH108	0 - 4.6	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
BH109	0 - 1.5	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
	1.5 - 4.6	Clayey silt trace gravel	$10^{-5} - 10^{-6}$	20 - 50	Medium to low permeability
BH110	0 - 1.5	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability
	1.5 - 3.0	Clayey silt/sandy silt	$10^{-5} - 10^{-6}$	20 - 50	Medium to low permeability
	3.0 - 4.6	Silty sand/sandy silt	$10^{-3} - 10^{-5}$	8 - 20	Medium permeability

Table 1: Percolation and Permeability of the Soil

Discussion:

The percolation and permeability of the soils were obtained indirectly from soil description based on Table 2 of the OBC Supplementary Standard SP-7. In general, the soils tested may be classified as of Medium Permeability. However, the soils at some locations and depths may be classified as of medium to low permeability.

Recommendations:

The Percolation Rate “T” and Permeability “K” which were estimated from the soil description, do not represent the actual values since there were only a limited portion of samples collected from the layer tested. For more accurate values, additional field testing should be carried out at the location of the proposed Storm Water Management (SWM).


Should you have any questions, please contact us at your convenience.

Yours very truly,

AZURE GROUP INC.

Janan Sulaiman, Ph.D., P.Eng.
Senior Geotechnical Engineer
jsulaiman@azuregroup.ca

Ahmed Al-Temimi, M.Sc., P.Eng., QP_(ESA)
Ontario Designated Consulting Engineer
aaltemimi@azuregroup.ca

 LEA Consulting Ltd. Consulting Engineers and Planners	Drawdown Time Calculation			
	Prepared:	P.R.	Table No.	A-15
	Checked:	F.M.		
	Project: 3016-3032 Kirwin Avenue Bio-swale	Proj. #	21111	
	Date	25-Oct-23		

Based on the Estimation of the Percolation and Permeability of the Soil by Azur Group (dated October 13, 2022)

Hydraulic Conductivity (K): 1×10^{-6} m/s
Infiltration Rate Estimated from Hydraulic Conductivity: 46.264 mm/hr
Safety factor: 4.5

The Hydraulic Conductivity (K) of soil was selected to produce the smallest infiltration rate based on the range provided by Azure. This results in a conservative estimation of the drawdown time.

Due to high conductivity soils in lower strata, it is expected that the factor should be 2.5. However, this calculation uses a conservative safety factor to demonstrate that the drawdown will be sufficient.

Adjusted infiltration rate: 10.3 mm/hr

Drainage to Bioswale: 73.0 m²

Runoff from a 10mm storm event: 0.73 m³

Clear Stone Detention Design Parameters:

Depth of Granular Stones: 500.0 mm
Porosity (n): 0.40
Granular Area (A): 5.8 m²
Distance to Water Table (D_{WT}): 3.3 m
Water Storage Volume (V): 1.2 m³

$$A = (1000V) / Pnt$$

Drawdown time (t) 48.63 hrs

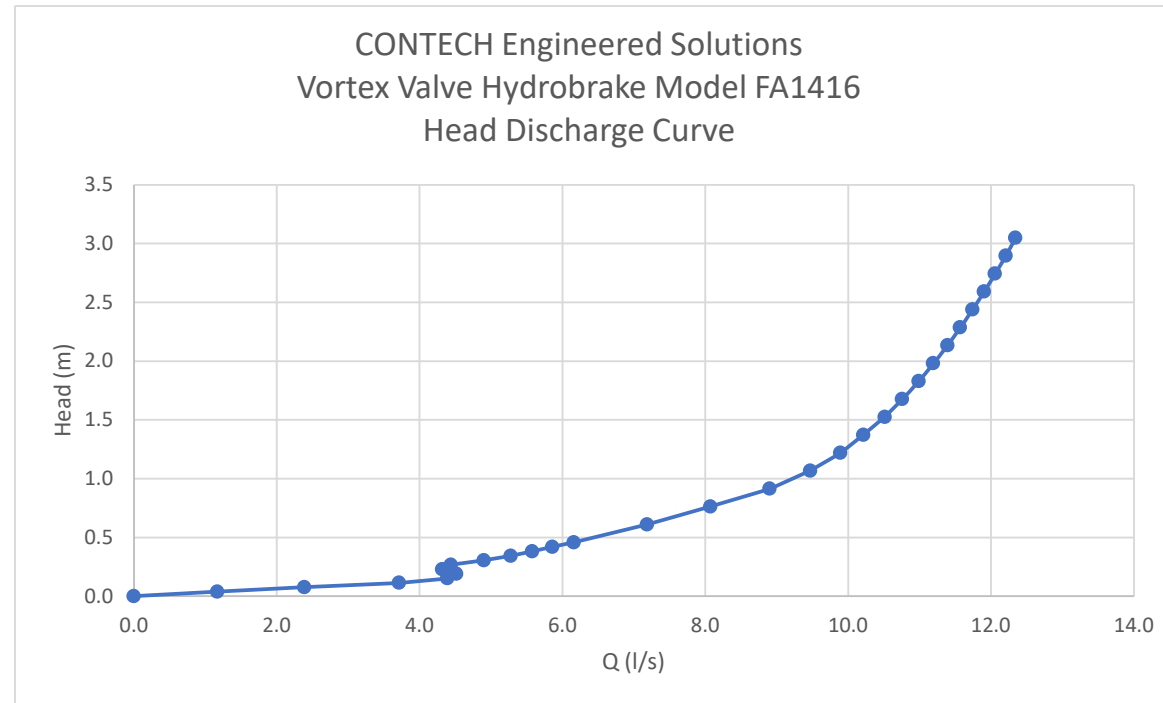
A = Bottom Area n = Porosity
V = Volume t = Drawdown time
P = Infiltration Rate (mm/hr)

APPENDIX A-16

Vortex Valve Flow Control Device



	FA1416 with 105 mm Outlet
Head (m)	Flow (l/s)
0.000	0.000
0.038	1.168
0.076	2.389
0.114	3.713
0.152	4.389
0.191	4.513
0.229	4.318
0.267	4.439
0.305	4.902
0.343	5.278
0.381	5.578
0.419	5.858
0.457	6.159
0.610	7.185
0.762	8.070
0.914	8.902
1.067	9.468
1.219	9.893
1.372	10.212
1.524	10.513
1.676	10.757
1.829	10.990
1.981	11.192
2.134	11.394
2.286	11.567
2.438	11.741
2.591	11.904
2.743	12.056
2.896	12.208
3.048	12.343



NOTES

1. FLUIDIC-AMP SIZES VARY BASED ON SITE REQUIREMENTS (SEE FLOW CHARTS)

2. SLEEVE DIAMETER & LENGTH DEPEND ON PIPE SIZE AND MATERIAL.

3. ATTACHMENT MAY BE MADE BY A PLATE, A SLEEVE (AS SHOWN) OR A BOLTING FLANGE

4. OUTLET SIZE VARIES BASED ON DESIRED OUTFLOW RATES ($\varnothing 3"$ MINIMUM)

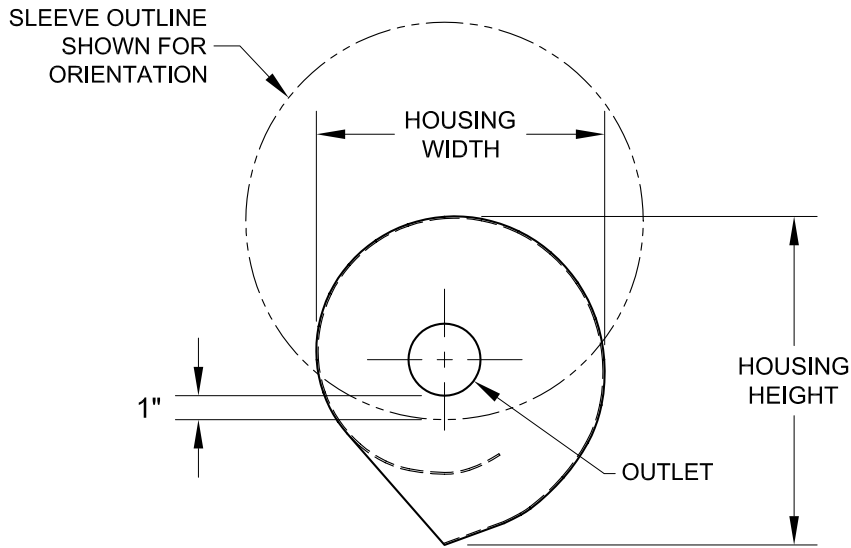
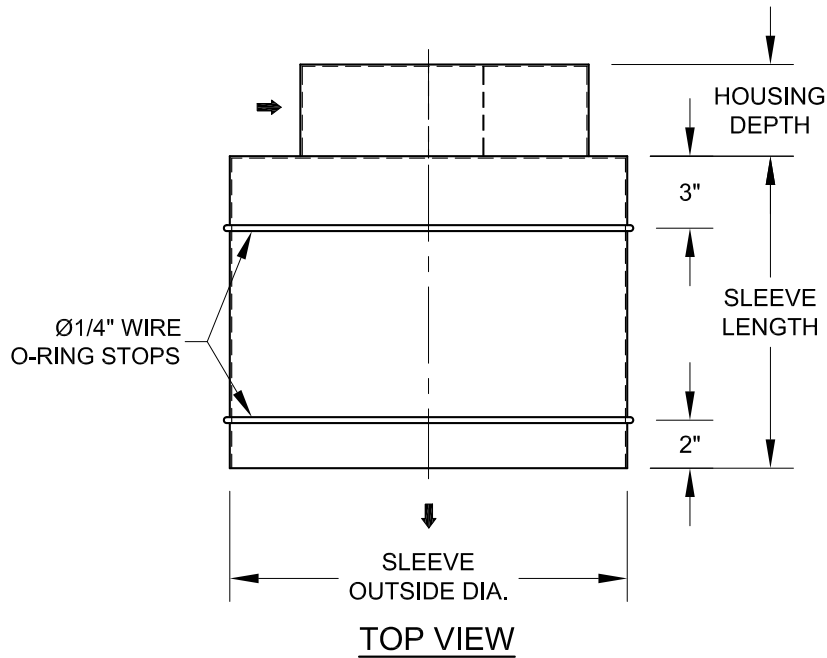
5. ALL WELDS CONTINUOUS UNLESS NOTED OTHERWISE

MATERIALS:

12 GA. 304L STAINLESS STEEL

(1) $\varnothing 5/8"$ AND (1) $\varnothing 9/16"$

BUNA N, 50 DUROMETER O-RINGS



FRONT VIEW
(SLEEVE DETAILS OMITTED THIS VIEW)

This CADD file is for the purpose of specifying stormwater flow control devices to be furnished by CONTECH Stormwater Solutions and may only be transferred to other documents exactly as provided by CONTECH Stormwater Solutions. Title block information, excluding the CONTECH Stormwater Solutions logo and the Fluidic-Cone or Fluidic-Amp HydroBrake designation and patent number, may be deleted if necessary. Revisions to any part of this CADD file without prior coordination with CONTECH Stormwater Solutions shall be considered unauthorized use of proprietary information.



TYPICAL DETAIL FLUIDIC-AMP™ HYDROBRAKE WITH SLEEVE ATTACHMENT

NOT INTENDED FOR CONSTRUCTION PURPOSES

DATE: 4/10/06

SCALE: NONE

FILE NAME: TYPFASLV

DRAWN: JBS

CHECKED: NDG

NOTES

1. FLUIDIC-AMP SIZES VARY BASED ON SITE REQUIREMENTS (SEE FLOW CHARTS)

2. ATTACHMENT PLATE WIDTH AND HEIGHT VARIES BASED ON CONCRETE OPENING SIZE

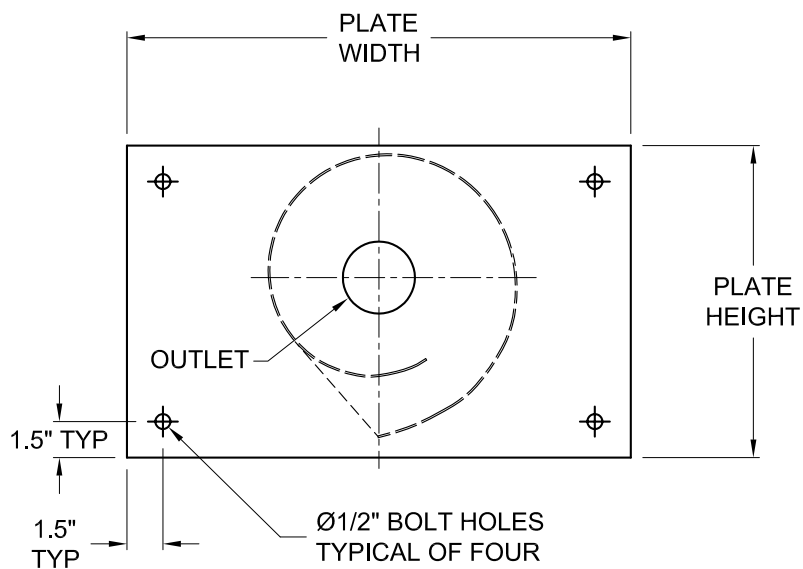
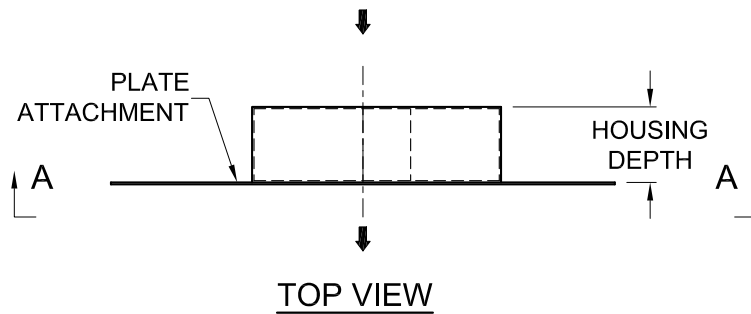
3. ATTACHMENT MAY BE MADE BY A PLATE (AS SHOWN), A SLEEVE OR A BOLTING FLANGE

4. OUTLET SIZE VARIES BASED ON DESIRED OUTFLOW RATES (Ø3" MINIMUM)

5. ALL WELDS CONTINUOUS UNLESS NOTED OTHERWISE

MATERIALS:

12 GA. 304L STAINLESS STEEL



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TYPICAL DETAIL FLUIDIC-AMP™ HYDROBRAKE WITH PLATE ATTACHMENT

NOT INTENDED FOR CONSTRUCTION PURPOSES

DATE: 4/10/06

SCALE: NONE

FILE NAME: TYPFAPLT

DRAWN: JBS

CHECKED: NDG



CONTECH VORTEX VALVES

FLOW CONTROL FOR STORMWATER DRAINAGE AND STORAGE SYSTEMS

OPERATIONS AND MAINTENANCE GUIDE

OPERATION of a CONTECH Vortex Valve

A Vortex Valve is a self-activating vortex flow control with no moving parts. When the upstream water level reaches a suitable level the water entering the unit spins within it. This causes the formation of an air-filled core which takes up a significant proportion of the outlet of the unit. Water discharges around the periphery of the outlet from the Vortex Valve enabling the use of a significantly larger outlet than if a simple orifice was used. The outlet diameter is typically 2 to 4 times larger than an equivalent simple orifice required to meet the same stage and discharge condition. Because of the large outlet diameter there is less potential for blockage.

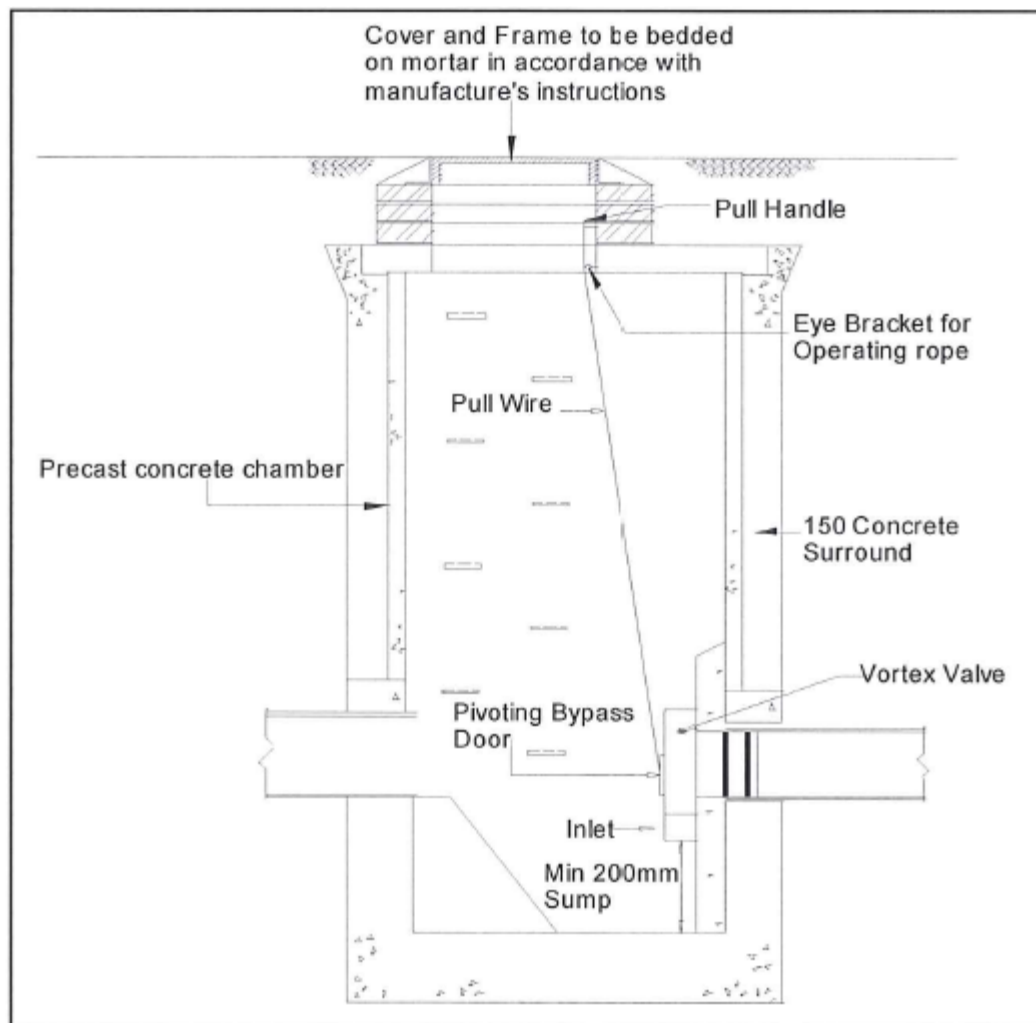
In the case of a downstream surcharge condition an air vent pipe may be required to ensure that the air core can form within the valve. The flow through a Vortex Valve is dependent upon the physical size of the unit itself and the differential head of water acting upon it.

MAINTENANCE

The need for maintenance will be site specific and depend on the following: 1) the size of the Vortex Valve (the larger the unit the less the likelihood of a blockage occurring); 2) the pollutant loading (e.g., a unit would be more susceptible to blockage were it placed on a foul system than a stormdrain catching a relatively clean impervious surface); 3) the physical characteristics of the control chamber itself (adequate benching or sump depth is essential); 4) and the presence of any pretreatment measures such as a sediment and debris removal structure.

All parts are made of corrosion resistant 304 stainless steel material which provides for exceptional design life in comparison to other drainage structures on the site.

The Vortex Valve flow control is fitted with an integral pivoting bypass door mounted to the front face of the unit. If a blockage occurs it is likely to occur on the intake of the flow control. The bypass door is fitted with a stainless steel wire rope that can be pulled from ground level, the door opens exposing a larger aperture on the front plate of the unit allowing the system to be drained of water. Once the water level in the housing structure subsides, which is typically a round manhole, the blockage can be easily accessed and cleared with a rod, debris grabbing or jetting device. Figure 1 shows a typical Vortex Valve installation.



APPENDIX A-17

Jellyfish Filter Unit Sizing and Design



Determining Number of Cartridges for Flow Based Systems

Date

26/05/2022

Black Cells = Calculation

Site Information

Project Name

3016-3032 Kirwin Avenue

Project Location

Mississauga, ON

OGS ID

OGS 1

Drainage Area, Ad

0.16 ac (0.0637 ha)

Impervious Area, Ai

0.16 ac

Pervious Area, Ap

0.00

% Impervious

100%

Runoff Coefficient, Rc

0.90

Treatment storm flow rate, Q_{treat}

0.07 cfs (2.1 L/s)

Peak storm flow rate, Q_{peak}

0.88 cfs (24.9 L/s)

Filter System

Filtration brand

StormFilter

Cartridge height

18 in

Specific Flow Rate

1.67 gpm/ft²

Flow rate per cartridge

12.53 gpm

SUMMARY

Number of Cartridges

3

Media Type

Perlite

Event Mean Concentration (EMC)

150 mg/L

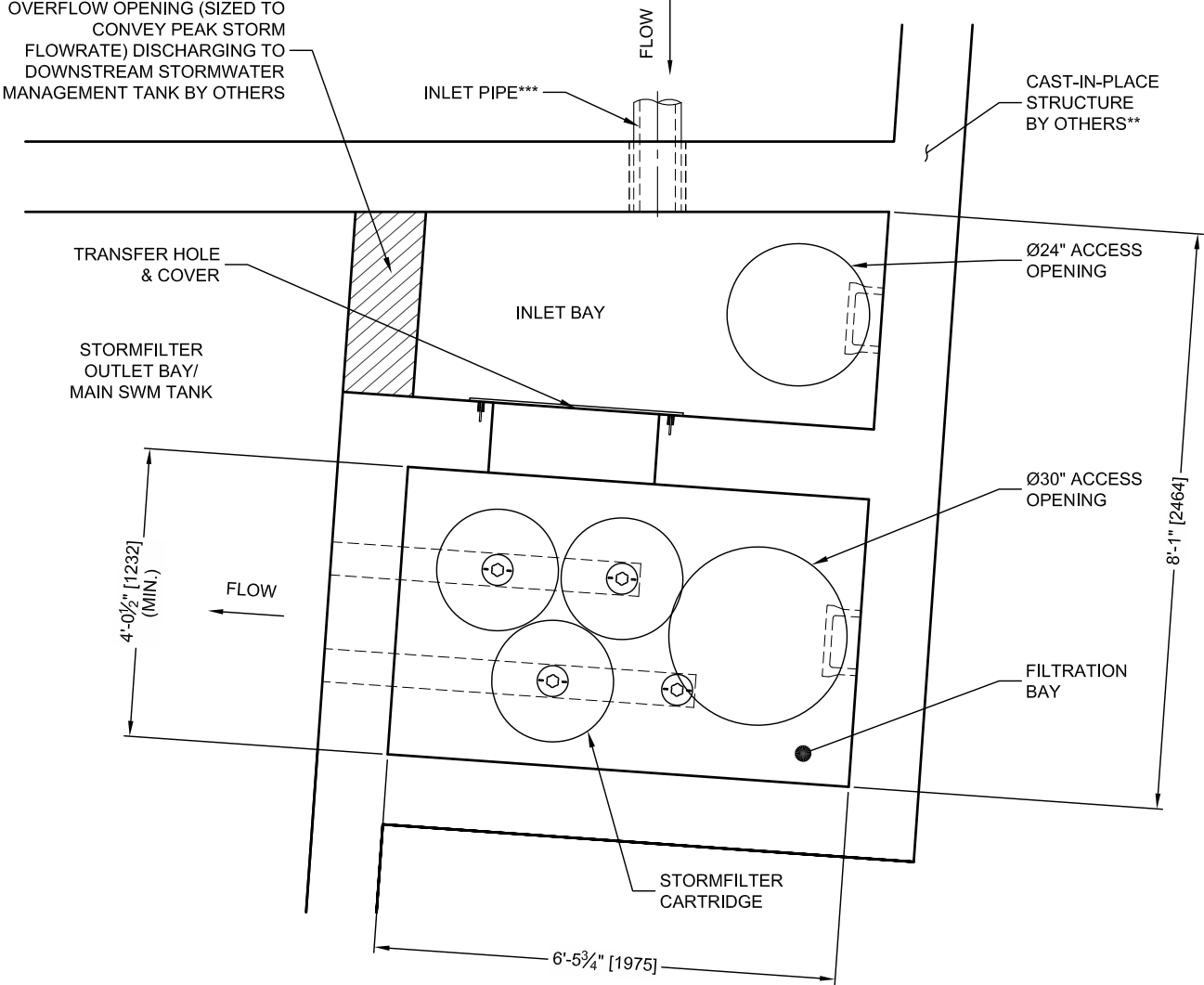
Annual TSS Removal

80%

Percent Runoff Capture

90%

Recommend SFPD0806 vault or CIP



PLAN VIEW
SCALE 1:50

SITE DESIGN DATA

WATER QUALITY FLOW RATE	2.1 l/s
PEAK FLOW RATE	24.9 l/s
RETURN PERIOD OF PEAK FLOW	100 YRS
FILTER MEDIA TYPE	PERLITE

NOTES
NOT FOR CONSTRUCTION

* CRITICAL ELEVATIONS.
** STRUCTURAL DESIGN BY OTHERS.
MINIMUM INTERNAL DIMENSIONS TO REMAIN.
*** INLET & OUTLET PIPE SIZE, LOCATION
AND MATERIAL TO BE CONFIRMED.



CONTECH
PROPOSAL
DRAWING

STORMFILTER DESIGN TABLE

- THE 8' x 6' PEAK DIVERSION STORMFILTER TREATMENT CAPACITY VARIES BY CARTRIDGE COUNT AND LOCALLY APPROVED SURFACE AREA SPECIFIC FLOW RATE. PEAK CONVEYANCE CAPACITY TO BE DETERMINED BY ENGINEER OF RECORD.
- THE PEAK DIVERSION STORMFILTER IS AVAILABLE IN A LEFT INLET (AS SHOWN) OR RIGHT INLET CONFIGURATION.
- ALL PARTS AND INTERNAL ASSEMBLY PROVIDED BY CONTECH UNLESS OTHERWISE NOTED.

CARTRIDGE HEIGHT	27"		18"		LOW DROP	
SYSTEM HYDRAULIC DROP (H - REQ'D. MIN.)	3.05'		2.3'		1.8'	
HEIGHT OF WEIR (W)	3.00'		2.25'		1.75'	
TREATMENT BY MEDIA SURFACE AREA	2 gpm/ft²	1 gpm/ft²	2 gpm/ft²	1 gpm/ft²	2 gpm/ft²	1 gpm/ft²
CARTRIDGE FLOW RATE (gpm)	22.5	11.25	15	7.5	10	5

MATERIAL LIST

COUNT	DESCRIPTION	SUPPLIED BY	INSTALLED BY
3	18", PERLITE CARTRIDGE	CONTECH	CONTRACTOR
4	RESTRICTOR DISK, 12.53 GPM,	CONTECH	CONTRACTOR
1	2" PVC SLIP PLUG	CONTECH	CONTRACTOR
1	FLOW KIT (CUSTOM)	CONTECH	CONTRACTOR
1	36" x 14" TRANSFER HOLE COVER	CONTECH	CONTRACTOR
1	Ø24" x 4" EJIW #41600389, OR EQUIVALENT FRAME AND COVER	CONTECH	CONTRACTOR
1	Ø30" x 4" EJIW #41600484, OR EQUIVALENT FRAME AND COVER	CONTECH	CONTRACTOR
TBD	STEPS, OR EQUIVALENT	CONTRACTOR	CONTRACTOR

PERFORMANCE SPECIFICATION

FILTER CARTRIDGES SHALL BE MEDIA-FILLED, PASSIVE, SIPHON ACTUATED, RADIAL FLOW, AND SELF CLEANING. **RADIAL MEDIA DEPTH SHALL BE 7-INCHES.** FILTER MEDIA CONTACT TIME SHALL BE AT LEAST **37 SECONDS.** SPECIFIC FLOW RATE SHALL BE **2 GPM/SF (MAXIMUM).** SPECIFIC FLOW RATE IS THE MEASURE OF THE FLOW (GPM) DIVIDED BY THE MEDIA SURFACE CONTACT AREA (SF). MEDIA VOLUMETRIC FLOW RATE SHALL BE **6 GPM/CF OF MEDIA (MAXIMUM).**

GENERAL NOTES

1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
2. DIMENSIONS MARKED WITH () ARE REFERENCE DIMENSIONS. ACTUAL DIMENSIONS MAY VARY.
3. FOR FABRICATION DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHTS, PLEASE CONTACT YOUR CONTECH REPRESENTATIVE. www.ContechES.com
4. STORMFILTER WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING. CONTRACTOR TO CONFIRM STRUCTURE MEETS REQUIREMENTS OF PROJECT.
5. CASTINGS SHALL MEET AASHTO M306 AND BE CAST WITH THE CONTECH LOGO.

INSTALLATION NOTES

- A. CONTRACTOR TO INSTALL JOINT SEALANT BETWEEN ALL SECTIONS AND ASSEMBLE STRUCTURE (IF APPLICABLE).
- B. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT PIPES. MATCH OUTLET PIPE INVERT WITH OUTLET BAY FLOOR (IF APPLICABLE).
- C. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO PROTECT CARTRIDGES FROM CONSTRUCTION-RELATED EROSION RUNOFF.
- D. CONTRACTOR TO REMOVE THE TRANSFER HOLE COVER WHEN THE SYSTEM IS BROUGHT ONLINE.
- E. CONTRACTOR TO NOTIFY ECHELON ENVIRONMENTAL WHEN THEY INTEND TO INSTALL COMPONENTS SO STAFF CAN BE PRESENT FOR SUPERVISION.



www.ContechES.com
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800-338-1122 513-645-7000 513-645-7993 FAX

3016-3032 KIRWIN AVENUE, MISSISSAUGA, ON
THE STORMWATER MANAGEMENT STORMFILTER
PEAK DIVERSION STORMFILTER CAST-IN-PLACE

VERIFICATION STATEMENT

GLOBE Performance Solutions

Verifies the performance of

The Stormwater Management StormFilter®

Developed by CONTECH Engineered Solutions LLC
Scarborough, Maine, USA

Registration: GPS-ETV_2020-06-15_NJDEP

In accordance with

ISO 14034:2016

**Environmental Management —
Environmental Technology Verification (ETV)**



John D. Wiebe, PhD
Executive Chairman
GLOBE Performance Solutions

June 15, 2020
Vancouver, BC, Canada



Verification Body
GLOBE Performance Solutions
404 – 999 Canada Place | Vancouver, B.C | Canada | V6C 3E2

Verification Overview

This Environmental Technology Verification (ETV) of The Stormwater Management StormFilter® (StormFilter) is the first part of a two-part verification process and entails the verification of performance claims (#1 & 2) based on laboratory testing in accordance with the New Jersey Department of Environmental Protection (NJDEP) *Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device* (January, 2013). This verification complements the subsequent verification of field testing data, collected in accordance with The Washington State Department of Ecology emerging stormwater treatment technologies, in accordance with guidelines identified by Ecology (2011) in the Technology Assessment Protocol – Ecology (TAPE).

Technology description and application

The Stormwater Management StormFilter® (StormFilter) is a manufactured treatment device that is provided by Contech Engineered Solutions LLC (Contech). The StormFilter improves the quality of stormwater runoff before it enters receiving waterways through the use of its customizable filter media, which removes non-point source pollutants. As illustrated in **Figure I**, the StormFilter is typically comprised of a vault or manhole structure that houses rechargeable, media-filled filter cartridges. Stormwater entering the system percolates through these media-filled cartridges, which trap particulates and remove pollutants. Once filtered through the media, the treated stormwater is discharged through an outlet pipe to a storm sewer system or receiving water.

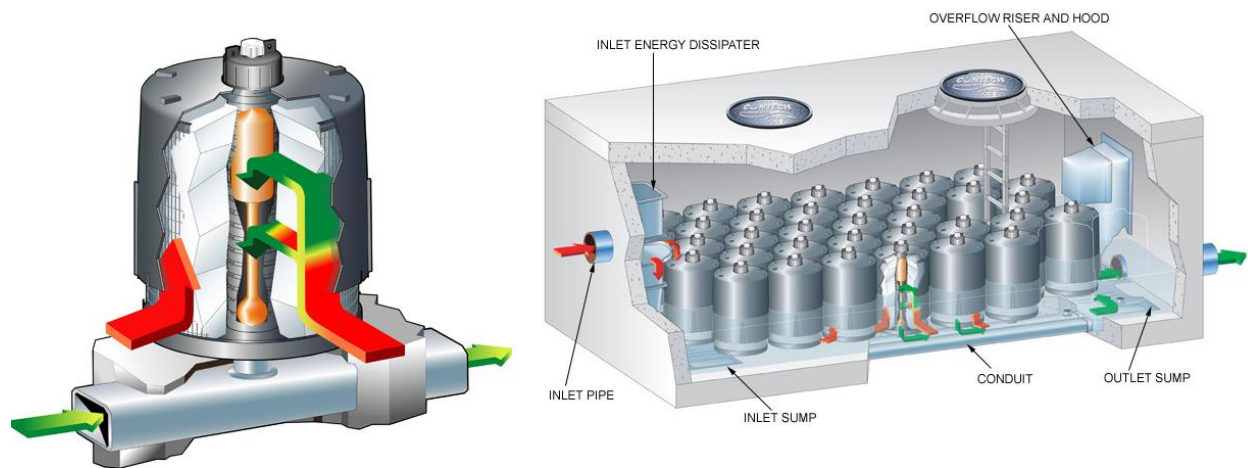


Figure I Individual StormFilter Cartridge (Left) and Typical Vault StormFilter Installation (Right)

Depending on the treatment requirements and expected pollutant characteristics at an individual site, the per cartridge filtration flow rate and driving head can be adjusted. The flow rate is individually controlled for each cartridge by a restrictor disc located at the connection point between the cartridge and the underdrain manifold. Driving head is managed by positioning of the inlet, outlet, and overflow elevations. The StormFilter is typically designed so that the restrictor disc passes the design treatment rate once the water surface reaches the shoulder of the cartridge which is equivalent to the cartridge height. Since the StormFilter uses a restrictor disc to restrict treatment flows below the hydraulic capacity of the media

the system typically operates under consistent driving head for the useful life of the media. Site specific head constraints are also addressed by three different cartridge heights (low drop (effective height of 12 inches), 18, and 27 inches) which operate on the same principal and surface area specific loading rates. The StormFilter requires a minimum of 1.8 ft, 2.3 ft and 3.05 ft of drop between inlet invert and outlet invert to accommodate the low drop, 18 and 27 inch cartridges, respectively, without backing up flow into the upstream piping during operation. When site conditions limit the amount of drop available across the StormFilter then flow is typically backed up into the upstream piping during operation to ensure sufficient driving head is provided. If desirable the StormFilter can be designed to operate under additional driving head.

The StormFilter is offered in multiple configurations including plastic, steel, and concrete catch basins; and precast concrete manholes, and vaults. Other configurations include panel vaults, CON/SPAN®, box culverts, and curb inlets. The filter cartridges operate consistently and act independently regardless of housing which enables linear scaling.

The StormFilter cartridge can house different types of media including perlite, zeolite, granular activated carbon (GAC), CSF® leaf media, MetalRx™, PhosphoSorb® or various media blends such as ZPG™ (perlite, zeolite and GAC). All of the media use processes associated with depth filtration to remove solids. Some media configurations also provide additional treatment mechanisms such as cation exchange, and/or adsorption, chelation, and precipitation. This verification is specific to a laboratory evaluation of the StormFilter using perlite media.

Performance conditions

The data and results published in this Verification Statement were obtained from the laboratory testing conducted on The Stormwater Management StormFilter® device, in accordance with the New Jersey Department of Environmental Protection Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device (January, 2013) (NJDEP Filtration Protocol). Prior to starting the performance testing program, a quality assurance project plan (QAPP) was submitted to and approved by the New Jersey Corporation for Advanced Technology (NJCAT).

Performance claim(s)

Performance Claim 1 (NJCAT)

The Stormwater Management StormFilter®, with perlite media, demonstrated at least 80% removal of total suspended solids at a design hydraulic loading rate of 1.44 l/s/m² (2.12 gpm/ft²) of media surface area and at a constant influent test sediment concentration of 200 mg/L in laboratory testing conducted under the 2013 NJDEP Protocol (removal efficiency test). This performance claim was verified at a 95% level of confidence.

Performance Claim 2 (NJCAT)

During the load testing (mass sediment load capacity) conducted under the 2013 NJDEP Protocol, The Stormwater Management StormFilter®, with perlite media, maintained at least 80% removal of total suspended solids at a design hydraulic loading rate of 1.44 l/s/m² (2.12 gpm/ft²) of media surface area to a cumulative mass sediment load of 54.3 lbs by a single 45.72 cm tall and 18in cartridge. This performance claim was verified statistically at a 95% level of confidence.

Performance results

Performance Claim 1 (NJCAT):

Raw data summarizing the percent removal of influent total suspended solids (TSS) by The Stormwater Management StormFilter®, at a concentration of 200 mg/L and a loading rate of 2.12 gpm/sq. ft. of media surface area.

Run #	Average Influent TSS Concentration (mg/L)	Background (mg/L)	Adjusted Effluent (mg/L)	TSS Removed (%)
1	203	2.11	37.7	81.8
2	210	1.83	35.4	83.7
3	207	2.84	40.5	81.2
4	213	2.04	36.8	83.3
5	212	2.17	35.8	83.7
6	208	2.34	38.0	82.3
7	212	2.08	38.4	82.5
8	203	2.42	35.8	83.0
9	206	2.86	35.2	83.5
10	207	3.16	35.6	83.3

Sum	823
N (COUNT)	10
Mean (AVG)	82.3
STDEV.s	0.871
VAR.s	0.758
Z (alpha)	1.65
Z (beta)	1.29
Hypothesized mean	80.0

Performance Claim 2 (NJCAT):

Raw data summarizing the percent removal of influent total suspended solids (TSS) and its capture by The Stormwater Management StormFilter®, at 200 mg/L (Run 1-45) and 400mg/L (Run 46-66).

Run #	Average Influent TSS Concentration (mg/L)	Background (mg/L)	Adjusted Effluent (mg/L)	Mass Captured (lbs)	TSS Removed (%)
1	203	2.11	37.7	0.640	81.8
2	210	1.83	35.4	1.32	83.7
3	207	2.84	40.5	1.96	81.2
4	213	2.04	36.8	2.65	83.3
5	212	2.17	35.8	3.33	83.7
6	208	2.34	38.0	3.99	82.3
7	212	2.08	38.4	4.67	82.5
8	203	2.42	35.8	5.32	83.0
9	206	2.86	35.2	5.98	83.5
10	207	3.16	35.6	6.65	83.3
11	200	1.78	37.4	7.29	81.8
12	209	1.55	36.0	7.96	83.4
13	211	2.29	40.9	8.62	81.3
14	206	1.96	37.7	9.21	<i>excluded</i>
15	209	2.32	36.2	9.87	83.2
16	202	2.07	36.5	10.5	82.6
17	206	1.97	39.9	11.2	81.3
18	203	3.13	35.1	11.8	83.2
19	204	2.57	37.2	12.5	82.4
20	210	2.64	35.6	13.1	83.6
21	199	3.17	39.8	13.8	80.7
22	206	3.07	40.5	14.4	80.9
23	203	3.32	37.1	15.1	82.3
24	206	2.91	38.5	15.7	81.8
25	203	3.44	37.4	16.3	82.1
26	204	2.77	40.4	17.0	80.8
27	208	2.85	29.4	17.6	<i>excluded</i>
28	199	2.46	37.7	18.2	81.5
29	199	3.72	37.6	18.8	81.6
30	202	3.66	37.6	19.5	82.0
31	200	3.41	42.4	20.1	79.3
32	202	3.17	43.4	20.7	79.1
33	204	4.52	42.5	21.3	79.8
34	200	5.11	40.0	22.0	80.6
35	198	4.11	44.4	22.5	78.1
36	204	3.90	43.1	23.2	79.5
37	203	4.55	43.1	23.8	79.4
38	202	4.84	41.4	24.4	80.0
39	203	5.55	34.8	25.1	83.3
40	203	6.34	39.9	25.7	80.9
41	199	3.53	43.3	26.3	78.7
42	199	3.21	45.1	26.9	77.9
43	200	3.21	40.9	27.5	80.1

44	203	3.41	40.0	28.2	80.9
45	202	3.61	46.6	28.8	77.4
46	401	1.78	79.2	30.0	80.8
47	402	1.91	81.6	31.3	80.2
48	401	2.38	85.6	32.5	79.2
49	396	2.83	87.0	33.7	78.5
50	412	1.62	85.5	35.0	79.6
51	396	3.66	87.6	36.2	78.3
52	396	4.12	90.1	37.3	77.6
53	403	4.05	92.4	38.5	77.4
54	403	4.85	89.9	39.8	78.1
55	400	3.59	86.3	41.0	78.8
56	400	1.85	89.0	42.2	78.2
57	403	2.33	88.7	43.4	78.5
58	407	3.25	89.6	44.6	78.2
59	395	3.22	92.5	45.8	76.9
60	404	3.01	88.2	47.0	78.5
61	410	1.82	90.7	48.2	<i>excluded</i>
62	398	2.15	86.6	49.4	78.6
63	401	2.60	88.1	50.6	78.3
64	402	2.75	91.5	51.9	77.6
65	403	4.10	89.1	53.1	78.2
66	402	3.65	89.5	54.3	77.8
Sum	5069				
N (COUNT)	63				
Median	80.7				
STDEV.s	2.03				
VAR.s	4.12				
Z (alpha)	1.65				
Z (beta)	1.29				
Hypothesized median	80.0				

Performance Claims were statistically analyzed and verified using the *mean* percent removal values for Claim #1, which utilized normally distributed data. The data set for Claims #2 was not normally distributed, which required the use of the *median* of the data as a surrogate for the mean, in order to be verified statistically at a 95% level of confidence.

Verification

This verification was completed by the Verification Expert, the Centre for Advancement of Water and Wastewater Technologies (“CAWT”), contracted by GLOBE Performance Solutions, applying the International Standard **ISO 14034:2016 Environmental management – Environmental technology verification (ETV)**. Data and information provided by Contech Engineered Solutions LLC to support the performance claim included the following:

- Performance test report “NJCAT TECHNOLOGY VERIFICATION, Stormwater Management StormFilter® (StormFilter) With Perlite Media” prepared by Contech Engineered Solutions, November 2016. This report is based on a test program was conducted at Contech’s Portland, Oregon laboratory under the direct supervision of *Scott A. Wells, Ph.D. and Associates* in accordance with the New Jersey Department of Environmental Protection (NJDEP) *Laboratory Protocol to Assess Total Suspended Solids Removal by a Filtration Manufactured Treatment Device (January, 2013)* and in compliance with the requirements of ISO/IEC 17025.

What is ISO 14034:2016 Environmental management – Environmental technology verification (ETV)?

ISO 14034:2016 specifies principles, procedures and requirements for environmental technology verification (ETV) and was developed and published by the International Organization for Standardization (ISO). The objective of ETV is to provide credible, reliable and independent verification of the performance of environmental technologies. An environmental technology is a technology that either results in an environmental added value or measures parameters that indicate an environmental impact. Such technologies have an increasingly important role in addressing environmental challenges and achieving sustainable development.

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Limitation of verification - Registration: GPS-ETV_2020-06-15_NJDEP

GLOBE Performance Solutions and the Verification Expert provide the verification services solely on the basis of the information supplied by the applicant or vendor and assume no liability thereafter. The responsibility for the information supplied remains solely with the applicant or vendor and the liability for the purchase, installation, and operation (whether consequential or otherwise) is not transferred to any other party as a result of the verification.

StormFilter Inspection and Maintenance Procedures



Maintenance Guidelines

The primary purpose of the Stormwater Management StormFilter® is to filter and prevent pollutants from entering our waterways. Like any effective filtration system, periodically these pollutants must be removed to restore the StormFilter to its full efficiency and effectiveness.

Maintenance requirements and frequency are dependent on the pollutant load characteristics of each site. Maintenance activities may be required in the event of a chemical spill or due to excessive sediment loading from site erosion or extreme storms. It is a good practice to inspect the system after major storm events.

Maintenance Procedures

Although there are many effective maintenance options, we believe the following procedure to be efficient, using common equipment and existing maintenance protocols. The following two-step procedure is recommended::

1. Inspection

- Inspection of the vault interior to determine the need for maintenance.

2. Maintenance

- Cartridge replacement
- Sediment removal

Inspection and Maintenance Timing

At least one scheduled inspection should take place per year with maintenance following as warranted.

First, an inspection should be done before the winter season. During the inspection the need for maintenance should be determined and, if disposal during maintenance will be required, samples of the accumulated sediments and media should be obtained.

Second, if warranted, a maintenance (replacement of the filter cartridges and removal of accumulated sediments) should be performed during periods of dry weather.

In addition to these two activities, it is important to check the condition of the StormFilter unit after major storms for potential damage caused by high flows and for high sediment accumulation that may be caused by localized erosion in the drainage area. It may be necessary to adjust the inspection/maintenance schedule depending on the actual operating conditions encountered by the system. In general, inspection activities can be conducted at any time, and maintenance should occur, if warranted, during dryer months in late summer to early fall.

Maintenance Frequency

The primary factor for determining frequency of maintenance for the StormFilter is sediment loading.

A properly functioning system will remove solids from water by trapping particulates in the porous structure of the filter media inside the cartridges. The flow through the system will naturally decrease as more and more particulates are trapped. Eventually the flow through the cartridges will be low enough to require replacement. It may be possible to extend the usable span of the cartridges by removing sediment from upstream trapping devices on a routine as-needed basis, in order to prevent material from being re-suspended and discharged to the StormFilter treatment system.

The average maintenance lifecycle is approximately 1-5 years. Site conditions greatly influence maintenance requirements. StormFilter units located in areas with erosion or active construction may need to be inspected and maintained more often than those with fully stabilized surface conditions.

Regulatory requirements or a chemical spill can shift maintenance timing as well. The maintenance frequency may be adjusted as additional monitoring information becomes available during the inspection program. Areas that develop known problems should be inspected more frequently than areas that demonstrate no problems, particularly after major storms. Ultimately, inspection and maintenance activities should be scheduled based on the historic records and characteristics of an individual StormFilter system or site. It is recommended that the site owner develop a database to properly manage StormFilter inspection and maintenance programs..





Inspection Procedures

The primary goal of an inspection is to assess the condition of the cartridges relative to the level of visual sediment loading as it relates to decreased treatment capacity. It may be desirable to conduct this inspection during a storm to observe the relative flow through the filter cartridges. If the submerged cartridges are severely plugged, then typically large amounts of sediments will be present and very little flow will be discharged from the drainage pipes. If this is the case, then maintenance is warranted and the cartridges need to be replaced.

Warning: In the case of a spill, the worker should abort inspection activities until the proper guidance is obtained. Notify the local hazard control agency and Contech Engineered Solutions immediately.

To conduct an inspection:

Important: Inspection should be performed by a person who is familiar with the operation and configuration of the StormFilter treatment unit and the unit's role, relative to detention or retention facilities onsite.

1. If applicable, set up safety equipment to protect and notify surrounding vehicle and pedestrian traffic.
2. Visually inspect the external condition of the unit and take notes concerning defects/problems.
3. Open the access portals to the vault and allow the system vent.
4. Without entering the vault, visually inspect the inside of the unit, and note accumulations of liquids and solids.
5. Be sure to record the level of sediment build-up on the floor of the vault, in the forebay, and on top of the cartridges. If flow is occurring, note the flow of water per drainage pipe. Record all observations. Digital pictures are valuable for historical documentation.
6. Close and fasten the access portals.
7. Remove safety equipment.
8. If appropriate, make notes about the local drainage area relative to ongoing construction, erosion problems, or high loading of other materials to the system.
9. Discuss conditions that suggest maintenance and make decision as to whether or not maintenance is needed.

Maintenance Decision Tree

The need for maintenance is typically based on results of the inspection. The following Maintenance Decision Tree should be used as a general guide. (Other factors, such as Regulatory Requirements, may need to be considered).

Please note Stormwater Management StormFilter devices installed downstream of, or integrated within, a stormwater storage facility typically have different operational parameters (i.e. draindown time). In these cases, the inspector must understand the relationship between the retention/detention facility and the treatment system by evaluating site specific civil engineering plans, or contacting the engineer of record, and make adjustments to the below guidance as necessary. Sediment deposition depths and patterns within the StormFilter are likely to be quite different compared to systems without upstream storage and therefore shouldn't be used exclusively to evaluate a need for maintenance.

1. Sediment loading on the vault floor.
 - a. If $>4"$ of accumulated sediment, maintenance is required.
2. Sediment loading on top of the cartridge.
 - a. If $>1/4"$ of accumulation, maintenance is required.
3. Submerged cartridges.
 - a. If $>4"$ of static water above cartridge bottom for more than 24 hours after end of rain event, maintenance is required. (Catch basins have standing water in the cartridge bay.)
4. Plugged media.
 - a. While not required in all cases, inspection of the media within the cartridge may provide valuable additional information.
 - b. If pore space between media granules is absent, maintenance is required.
5. Bypass condition.
 - a. If inspection is conducted during an average rain fall event and StormFilter remains in bypass condition (water over the internal outlet baffle wall or submerged cartridges), maintenance is required.
6. Hazardous material release.
 - a. If hazardous material release (automotive fluids or other) is reported, maintenance is required.
7. Pronounced scum line.
 - a. If pronounced scum line (say $\geq 1/4"$ thick) is present above top cap, maintenance is required.

Maintenance

Depending on the configuration of the particular system, maintenance personnel will be required to enter the vault to perform the maintenance.

Important: If vault entry is required, OSHA rules for confined space entry must be followed.

Filter cartridge replacement should occur during dry weather. It may be necessary to plug the filter inlet pipe if base flows is occurring.

Replacement cartridges can be delivered to the site or customers facility. Information concerning how to obtain the replacement cartridges is available from Contech Engineered Solutions.

Warning: In the case of a spill, the maintenance personnel should abort maintenance activities until the proper guidance is obtained. Notify the local hazard control agency and Contech Engineered Solutions immediately.

To conduct cartridge replacement and sediment removal maintenance:

1. If applicable, set up safety equipment to protect maintenance personnel and pedestrians from site hazards.
2. Visually inspect the external condition of the unit and take notes concerning defects/problems.
3. Open the doors (access portals) to the vault and allow the system to vent.
4. Without entering the vault, give the inside of the unit, including components, a general condition inspection.
5. Make notes about the external and internal condition of the vault. Give particular attention to recording the level of sediment build-up on the floor of the vault, in the forebay, and on top of the internal components.
6. Using appropriate equipment offload the replacement cartridges (up to 150 lbs. each) and set aside.
7. Remove used cartridges from the vault using one of the following methods:

Method 1:

- A. This activity will require that maintenance personnel enter the vault to remove the cartridges from the under drain manifold and place them under the vault opening for lifting (removal). Disconnect each filter cartridge from the underdrain connector by rotating counterclockwise 1/4 of a turn. Roll the loose cartridge, on edge, to a convenient spot beneath the vault access.

Using appropriate hoisting equipment, attach a cable from the boom, crane, or tripod to the loose cartridge. Contact Contech Engineered Solutions for suggested attachment devices.

- B. Remove the used cartridges (up to 250 lbs. each) from the vault.



Important: Care must be used to avoid damaging the cartridges during removal and installation. The cost of repairing components damaged during maintenance will be the responsibility of the owner.

- C. Set the used cartridge aside or load onto the hauling truck.
- D. Continue steps a through c until all cartridges have been removed.

Method 2:

- A. This activity will require that maintenance personnel enter the vault to remove the cartridges from the under drain manifold and place them under the vault opening for lifting (removal). Disconnect each filter cartridge from the underdrain connector by rotating counterclockwise 1/4 of a turn. Roll the loose cartridge, on edge, to a convenient spot beneath the vault access.
- B. Unscrew the cartridge cap.
- C. Remove the cartridge hood and float.
- D. At location under structure access, tip the cartridge on its side.
- E. Empty the cartridge onto the vault floor. Reassemble the empty cartridge.
- F. Set the empty, used cartridge aside or load onto the hauling truck.
- G. Continue steps a through e until all cartridges have been removed.

8. Remove accumulated sediment from the floor of the vault and from the forebay. This can most effectively be accomplished by use of a vacuum truck.
9. Once the sediments are removed, assess the condition of the vault and the condition of the connectors.
10. Using the vacuum truck boom, crane, or tripod, lower and install the new cartridges. Once again, take care not to damage connections.
11. Close and fasten the door.
12. Remove safety equipment.
13. Finally, dispose of the accumulated materials in accordance with applicable regulations. Make arrangements to return the used **empty** cartridges to Contech Engineered Solutions.

Related Maintenance Activities - Performed on an as-needed basis

StormFilter units are often just one of many structures in a more comprehensive stormwater drainage and treatment system.

In order for maintenance of the StormFilter to be successful, it is imperative that all other components be properly maintained. The maintenance/repair of upstream facilities should be carried out prior to StormFilter maintenance activities.

In addition to considering upstream facilities, it is also important to correct any problems identified in the drainage area. Drainage area concerns may include: erosion problems, heavy oil loading, and discharges of inappropriate materials.

Material Disposal

The accumulated sediment found in stormwater treatment and conveyance systems must be handled and disposed of in accordance with regulatory protocols. It is possible for sediments to contain measurable concentrations of heavy metals and organic chemicals (such as pesticides and petroleum products). Areas with the greatest potential for high pollutant loading include industrial areas and heavily traveled roads.

Sediments and water must be disposed of in accordance with all applicable waste disposal regulations. When scheduling maintenance, consideration must be made for the disposal of solid and liquid wastes. This typically requires coordination with a local landfill for solid waste disposal. For liquid waste disposal a number of options are available including a municipal vacuum truck decant facility, local waste water treatment plant or on-site treatment and discharge.



Inspection Report

Date: _____ Personnel: _____

Location: _____ System Size: _____ Months in Service: _____

System Type: Vault ☐ Cast-In-Place ☐ Linear Catch Basin ☐ Manhole ☐ Other: _____

Sediment Thickness in Forebay: _____ Date: _____

Sediment Depth on Vault Floor: _____

Sediment Depth on Cartridge Top(s): _____

Structural Damage: _____

Estimated Flow from Drainage Pipes (if available): _____

Cartridges Submerged: Yes ☐ No ☐ Depth of Standing Water: _____

StormFilter Maintenance Activities (check off if done and give description)

☐ Trash and Debris Removal: _____

☐ Minor Structural Repairs: _____

☐ Drainage Area Report _____

Excessive Oil Loading: Yes ☐ No ☐ Source: _____

Sediment Accumulation on Pavement: Yes ☐ No ☐ Source: _____

Erosion of Landscaped Areas: Yes ☐ No ☐ Source: _____

Items Needing Further Work: _____

Owners should contact the local public works department and inquire about how the department disposes of their street waste residuals.

Other Comments:

Review the condition reports from the previous inspection visits.

StormFilter Maintenance Report

Date: _____ Personnel: _____

Location: _____ System Size: _____

System Type: Vault ☐ Cast-In-Place ☐ Linear Catch Basin ☐ Manhole ☐ Other: _____

List Safety Procedures and Equipment Used: _____

System Observations

Months in Service: _____

Oil in Forebay (if present): Yes ☐ No ☐

Sediment Depth in Forebay (if present): _____

Sediment Depth on Vault Floor: _____

Sediment Depth on Cartridge Top(s): _____

Structural Damage: _____

Drainage Area Report

Excessive Oil Loading: Yes ☐ No ☐ Source: _____

Sediment Accumulation on Pavement: Yes ☐ No ☐ Source: _____

Erosion of Landscaped Areas: Yes ☐ No ☐ Source: _____

StormFilter Cartridge Replacement Maintenance Activities

Remove Trash and Debris: Yes ☐ No ☐ Details: _____

Replace Cartridges: Yes ☐ No ☐ Details: _____

Sediment Removed: Yes ☐ No ☐ Details: _____

Quantity of Sediment Removed (estimate?): _____

Minor Structural Repairs: Yes ☐ No ☐ Details: _____

Residuals (debris, sediment) Disposal Methods: _____

Notes:



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- Site-specific design support is available from our engineers.

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APPENDIX A-18

Area Drain Typical Details



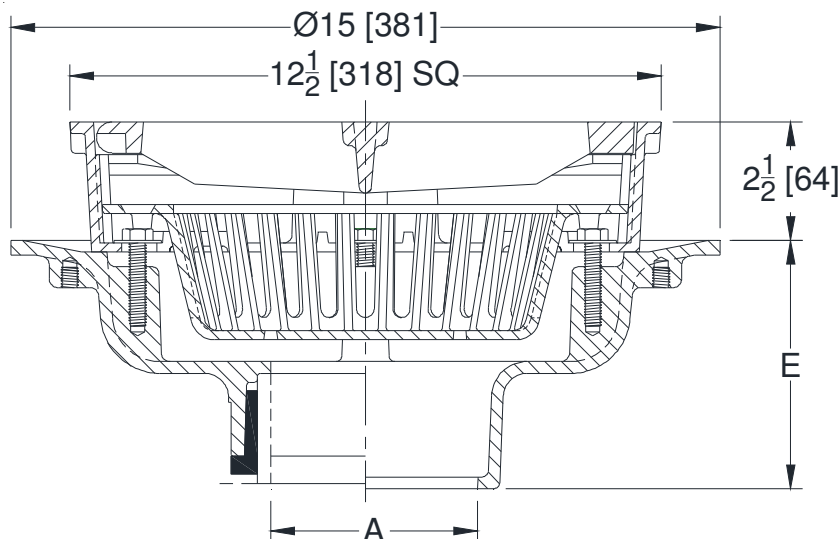
**Z610**

12-1/2 [318] SQUARE TOP HEAVY-DUTY DRAIN

SPECIFICATION SHEET

TAG _____

Dimensional Data (inches and [mm]) are Subject to Manufacturing Tolerances and Change Without Notice



A Pipe Size In. [mm]	Approx. Wt. Lbs. [kg]	Grate Open Area Sq. In. [cm ²]
2, 3, 4, 6 [51, 76, 102, 152]	54 [24]	42 [271]
8 [203]	56 [25]	

ENGINEERING SPECIFICATION: ZURN Z610

12-1/2" [305mm] Square top drain, Dura-Coated cast iron body with bottom outlet, seepage pan and combination membrane flashing clamp and frame for heavy-duty cast iron loose slotted duresist grate, with suspended polypropylene sediment bucket.

OPTIONS (Check/specify appropriate options)**PIPE SIZE**

3, 4, 6 [76, 102, 152]
3, 4, 6 [76, 102, 152]
2, 3, 4, 6, [51, 76, 102, 152]
2, 3, 4, 6, 8 [51, 76, 102, 152, 203]
2, 3, 4 [51, 76, 102]

(Specify size/type) **OUTLET**

_____ IC Inside Caulk
_____ IG Inside Gasket
_____ IP Threaded
_____ NH No-Hub
_____ NL Neo-Loc

'E' BODY HT. DIM.

5-1/4 [133]
5-1/4 [133]
3-3/4 [95]
5-1/4 [133]
4-5/8 [117]

PREFIXES

_____ Z D.C.C.I. Body and Top*
_____ ZB D.C.C.I Body w/Polished Bronze Top (Add 3/16 [5] to 2-1/2 [64] Dim. and 3/4 [19] to 12-1/2 [318] Dim.)
_____ ZN D.C.C.I Body w/Polished Nickel Bronze Top (Add 3/16 [5] to 2-1/2 [64] Dim. and 3/4 [19] to 12-1/2 [318] Dim.)

SUFFIXES

_____ -AR	Acid Resistant Epoxy Coated Cast Iron	_____ -S	Secondary Strainer
_____ -DS	Ductile Iron Solid Cover	_____ -SC	Solid Cover
_____ -DX	Dex-O-Tex Flange (ZB, ZN Only)	_____ -SS	Stainless Steel Mesh Liner for Bucket
_____ -F	2 [51] High Extension	_____ -TC	Neo-Loc Test Cap Gasket (2, 3, 4 [51, 76, 102] NL Bottom Outlet Only)
_____ -G	Galvanized Cast Iron	_____ -TS	Top Secured with Slotted Screws
_____ -H	Hinged Grate	_____ -V	Backwater Valve (See Z1099)
_____ -HC	Hinged Solid Cover	_____ -VP	Vandal-Proof Secured Top
_____ -HL	Hinged Locking Grate	_____ -YA	Aluminum Sediment Bucket
_____ -HLC	Hinged Locking Cover	_____ -YC	Cast Iron Sediment Bucket
_____ -LY	(Less) Sediment Bucket	_____ -90	90° Threaded Side Outlet Body
_____ -P	Trap Primer Connection		

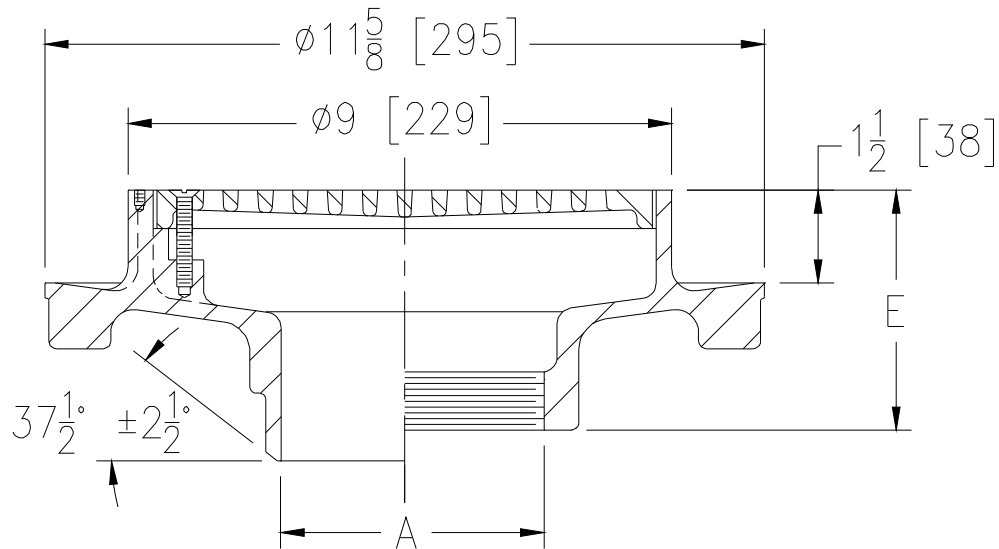
* Regularly furnished unless otherwise specified.

Zurn Industries, LLC | Specification Drainage Operation
1801 Pittsburgh Avenue, Erie, PA 16502, Ph. 855.663.9876
In Canada | Zurn Industries Limited
7900 Goreway Drive, Unit 10, Brampton, Ontario L6T 5W6, Ph. 877.892.5216
www.zurn.com

Rev. J
Date: 10/16/2019
C.N. No. 141246
Prod. | Dwg. No. Z610

**Z1730****9 [229] DIAMETER FLOOR DRAIN
SHALLOW TYPE****SPECIFICATION SHEET****TAG** _____

Dimensional Data (inches and [mm]) are Subject to Manufacturing Tolerances and Change Without Notice



A Pipe Size In.[mm]	Approx. Wt. Lbs. [kg]	Grate Open Area Sq. In. [cm ²]
2, 3, 4 [51, 76, 102]	20 [9]	21 [135]

ENGINEERING SPECIFICATION: ZURN Z1730

9" [229mm] Diameter shallow type heavy-duty floor drain, all Type 304 (CF8) stainless steel with integral anchor flange, and non-tilt grate with plain finish.

OPTIONS (Check/specify appropriate options)**PIPE SIZE**

2, 3, 4 [51, 76, 102]

(Specify size/type) **OUTLET**

____ BW Butt-Weld
(Specify Schedule 10 or 40)
____ NH No-Hub
____ IP Threaded

'E' BODY HT. DIM.

4-13/16 [122]

2, 3, 4 [51, 76, 102]

4-13/16 [122]

2, 3, 4 [51, 76, 102]

4-13/16 [122]

PREFIXES

____ Z Type 304 (CF8) Stainless Steel Body*
____ ZM Type 316 (CF8M) Stainless Steel Body

SUFFIXES

____ -K Seepage Holes Only
____ -KC Clamp Collar with Seepage Holes
____ -TS Top Secured with Slotted Screws
____ -VP Vandal-Proof Secured Top


* Regularly furnished unless otherwise specified.

Zurn Industries, LLC | Specification Drainage Operation
1801 Pittsburgh Avenue, Erie, PA U.S.A. 16502 • Ph. 855-663-9876, Fax 814-454-7929
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www.zurn.com

Rev. F
Date: 09/28/2017
C.N. No. 138051
Prod. | Dwg. No. Z1730

APPENDIX B

Stormwater Peak Flow Calculation for Sub-Catchment Area UC2

 LEA Consulting Ltd. Consulting Engineers and Planners	Land Use			
	Prepared:	P.R.	Page No.	B-01
	Checked:	F.M.		
	Proj. #	21111		
Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE SUB-CATCHMENT EC2 & PC2	Date:	25-Oct-23		

Pre-Development CONDITION


Sub-Catchment EC2

Existing Land Use	Area (m ²)
Lawn & Tree	4435.0
Total Area:	4435.0

Post-Development Condition:

Sub-Catchment PC2

Proposed Land Use	Area (m ²)
Lawn & Tree	2953.0
Total Area	2953.0

 LEA Consulting Ltd. Consulting Engineers and Planners	Composite "C" Calculation			
	Prepared:	P.R.	Page No.	B-02
	Checked:	F.M.		
Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE SUB-CATCHMENT EC2 & PC2	Proj. #	21111		
	Date:	25-Oct-23		

Pre-Development Composite Runoff Coefficient "C"


Sub-Catchment EC2

Location	Area (ha)	C	Composite "C"
Lawn & Tree	0.444	0.25	
Total Area:	0.444		0.25
Imperviousness Percent:			0.0

Post-Development Composite Runoff Coefficient "C"

Sub-Catchment PC2

Location	Area (ha)	C	Composite "C"
Lawn & Tree	0.295	0.25	
Total Area	0.295		0.25
Imperviousness Percent:			0.0

 LEA Consulting Ltd. Consulting Engineers and Planners	Pre-Development Peak Flow Rates Calculation			
	Prepared:	P.R.	Page No.	B-03
	Checked:	F.M.		
	Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE SUB-CATCHMENT EC2 & PC2	Proj. # 21111 Date: 25-Oct-23		

Rational Formulae: $Q = 2.78 \text{ CIA (L/s)}$


Site Area: 0.444 ha
Time of Concentration 15 minutes as per City Guidelines
Runoff Coefficient : 0.25 Pre-development condition

Rainfall Intensity: $I = aT^c$

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Rainfall Intensity (mm/hr):	59.89	80.51	99.17	113.89	127.13	140.69

Peak Flow Rate (L/s):

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Under existing site conditions (L/s):	18.45	24.80	30.54	35.08	39.16	43.33

 LEA Consulting Ltd. Consulting Engineers and Planners	Post-Development Peak Flow Rates Calculation (Uncontrolled)			
	Prepared:	P.R.	Page No.	B-04
	Checked:	F.M.		
Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE SUB-CATCHMENT EC2 & PC2				
		Date:	25-Oct-23	

Rational Formulae: $Q = 2.78 \text{ CIA (L/s)}$

Site Area: 0.295 ha
 Time of Concentration 15 minutes as per City Guidelines
 Runoff Coefficient : 0.25 Pre-development condition

Rainfall Intensity: $I = aT^c$

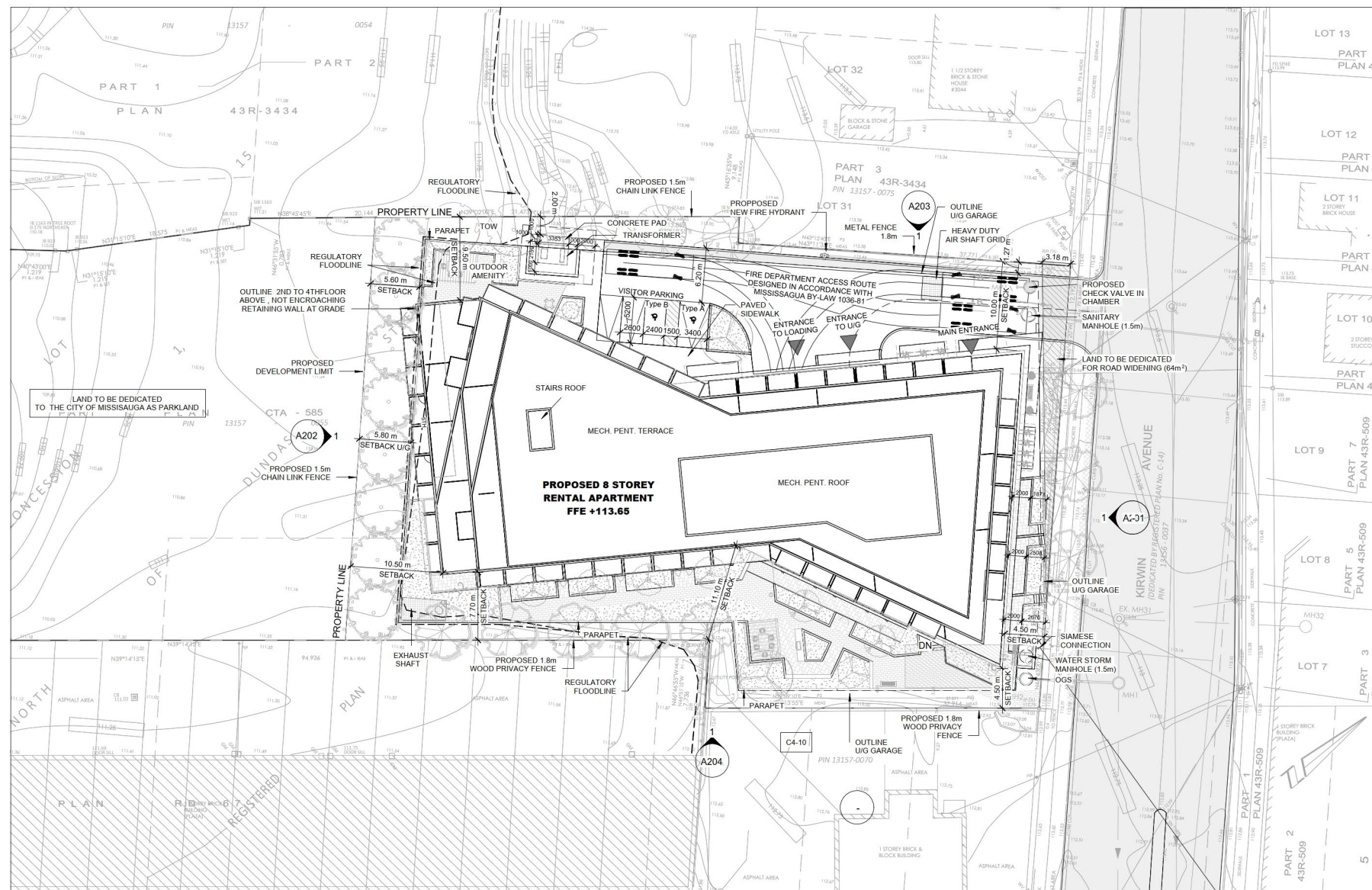
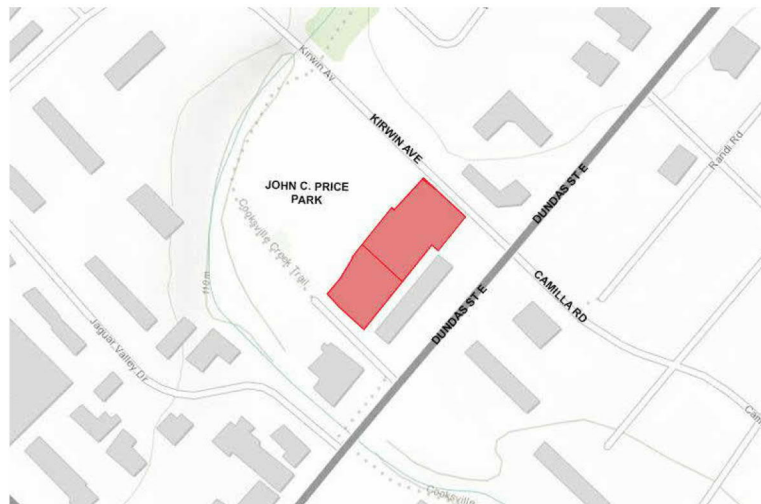
Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Rainfall Intensity (mm/hr):	59.89	80.51	99.17	113.89	127.13	140.69

Peak Flow Rate (L/s):

Return Period:	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
Under existing site conditions (L/s):	12.28	16.51	20.34	23.36	26.07	28.85

APPENDIX C

Sanitary and Water Demand Calculations



3016-3022 Kirwin Ave

Review: Sept 18th, 2023

Legal Description

ALL OF LOTS 27 TO 30 REGISTERED PLAN No. C-14 AND PART OF LOT 5 REGISTERED PLAN TOR-12 AND PART OF LOT 15 CONCESSION 1, NORTH OF DUNDAS STREET CITY OF MISSISSAUGA REGIONAL MUNICIPALITY OF PEEL

Site

Gross Site Area	6,385.0 m²
Parkland Dedication	2,450.0 m²
Road Widening Area	12.0 m²
Net Site Area	3,923.0 m²
Lot Frontage	50.3 m
Lot Depth	131.4 m

Building proposal

Building Footprint	1,703.0 m ²	
Building Height	25.5 m	<i>*Mech. Pent. Excluded</i>
Gross Floor Area	(Based on GFA - Apartment Zone)	10,520.0 m ²
Lot Coverage (%)	(Based on Gross Site Area)	27%
Lot Coverage (%)	(Based on Net Site Area)	43%
FSI	(GFA / Gross Site Area)	1.65
FSI	(GFA / Net Site Area)	2.68

Proposed Areas	Floor	GCA** (m²)	GFA* (m²)	Total (m²)
	Ground Floor	1,583.0	930.0	10,011
	2nd Floor	1,585.0	1,525.0	16,415
	3rd Floor	1,703.0	1,628.0	17,524
	4th Floor	1,508.0	1,448.0	16,587
	5th Floor	1,427.0	1,387.0	14,715
	6th Floor	1,370.0	1,297.0	13,961
	7th Floor	1,311.0	1,265.0	13,617
	8th Floor	1,106.0	1,060.0	11,410
	Total GFA	11,593.0	10,520.0	113,240

Total Proposed GFA	10,520.0 m²	113,240 ft²
---------------------------	-------------------------------	-------------------------------

***Gross Floor Area (GFA) - Apartment Zone** means the sum of the areas of each storey of a building above or below established grade, measured from the exterior of outside walls of the building including floor area occupied by interior walls but excluding any part of the building used for mechanical floor area, stairwells, elevators, motor vehicle parking, bicycle parking, storage lockers, below-grade storage, any enclosed area used for the collection or storage of disposable or recyclable waste generated within the building, common facilities for the use of the residents of the building, a day care and amenity area.

²² **Gross Construction Area (GCA)** - The total enclosed area of a floor or building measured to the outside surface of the permanent exterior walls of the building or structure or to a predetermined surface, or plane as in the case of overhangs and projections to the outside surface of the building.

Unit Count	Units	1 Bed	2 Bed	3 Bed
Ground Floor	10	6	4	
2nd Floor	18	17	1	
3rd Floor	23	21	1	1
4th Floor	22	18	4	0
5th Floor	20	15	5	
6th Floor	19	14	5	
7th Floor	18	12	6	
8th Floor	16	14	1	1
Total Units	146	117	27	2
		80.1%	18.5%	1.4%

Vehicular Parking

Parking Required	UNITS	PARKING	RATIO		
Rental Residential @0.8 per unit	146	117	0.80		
		Tot: 117			
Rental Visitors @ 0.2 per unit	146	29	0.20		
Total Vehicular Parking Required		Tot: 146			
Parking Provided (estimated)					
	At Grade	P1 Level	P2 Level	Sub Total	Ratio
Residential	0	55	87	142	0.97
Residential Visitor	4	25	0	29	0.20
	4	80	87	171	
Total Vehicular Parking Provided				Tot: 171	1.17

Bicycle Parking

Required		
	Ratio	
Short Term Residential	0.08 x unit	12
Long Term Residential	0.7 x unit	102
	Tot:	114

Provided (estimated)		Tot:	114
	At Grade	P1 Level	
Short Term Residential	14	0	
Long Term Residential	0	100	
			Tot: 114

Landscaped Area

Soft Landscaping	912.0 m ²
Hard Landscaping	760.0 m ²
Green Roof	466.0 m ²
Total Landscape	2138.0 m²

Amenity Area

Amenity Area Required

5.6 m ² per unit	817.6 m ²
Total Amenities Required	817.6 m²

Amenity Area Provided (estimated)

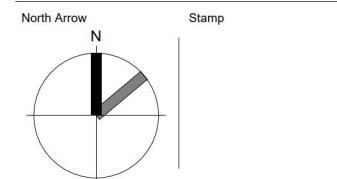
1) Indoor		
	Ground Floor	330.0 m²
2) Outdoor		
	Ground Floor	100.0 m²
	Roof	450.0 m²

Total Amenities	880.0 m ²	6.0 sqm x unit
-----------------	----------------------	----------------

**3016
KIRWIN AVE**

3016-3022 Kirwin Avenue
Mississauga - ON - Canada

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[illegible]

Project No: 20009

Scale: 1 : 300

Date: Feb. 04, 2020


Drawn by: _____ FC

Drawing Title

SITE PLAN & STATS

Drawing
Number

A001

 <div>LEA Consulting Ltd. Consulting Engineers and Planners</div>	Sanitary Flow Rate Calculation			
	Prepared:	P.R.	Page No.	C-01
	Checked:	F.M.		
	Proj. #	21111		
	Date:	25-Oct-23		
Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE				

POPULATION CALCULATION


Net Site Area 3923 m²
 Number of Townhomes 148 units

Proposed Building		Density (P.P.U)	Population
Type	Units		
Residential			0.00
>750 SQF	43	3	129
<=750 SQF	105	1.6	168
Total			297.00

SANITARY FLOW CALCULATION

Harmon Peaking Factor: $M=1+14/(4+P^{0.5})$

Peaking Factor 4.08
 Average Daily Wastewater Flow 302.8 L/cap/day
 Total Actual Domestic Flow 4.25 L/sec
 Total Domestic Flow (For less than 1000 person shall be 13.0 L/sec-STD.DWG. 2-5-2, Region of Peel) 13.00 L/sec
 Infiltration Allowance (@ 0.2 L/sec/ha) 0.08 L/sec
Actual Design flow 4.33 L/sec
Standard Design Flow 13.08 L/sec

 LEA Consulting Ltd. Consulting Engineers and Planners	Water Demand Calculation BLK A			
	Prepared:	P.R.	Page No.	C-02
	Checked:	F.M.		
Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE	Proj. #	21111		
	Date:	25-Oct-23		

This calculation is following the "Water Supply for Public Fire Protection" by Fire Underwriters Survey.

Formula: $F = 220C\sqrt{A}$

where

F = the required fire flow in litres per minute

C = coefficient related to the type of construction.

= 0.8 for non-combustible construction

A = the total floor area in square metres. For non-combustible buildings with unprotected openings, the areas shall be calculated by taking the largest two adjoining floors plus 50% of each floor above, up to 8 floors.

STEP 1

According the building stats, Dated Nov. 12, 2020	BLK A Area (m2)	
1st Floor	1583.0	Not Used
2nd Floor	1585.0	Largest joined floor
3rd Floor	1703.0	Largest joined floor
4th Floor	1508.0	Above Floor
5th Floor	1427.0	Above Floor
6th Floor	1370.0	Above Floor
7th Floor	1311.0	Above Floor
8th Floor	1106.0	Above Floor
A	6649	

Therefore, F (l/min)= 14000

STEP 2

Occupancy reduction:

For occupancies with a low contents fire hazard, the reduction rate is 25%,

Therefore: F (l/min)= 10500

Reduction for sprinkler protection:

Using the NFPA sprinkler system, a reduction rate of 30% is used.

Therefore: F (l/min)= 7350

STEP 3

Separation charge:

Charge for the separations on each side:

Exposure Charge		Charge	
0 to 3m	25%	0%	West
3.1 to 10m	20%	15%	North
10.1 to 20m	15%	15%	South
20.1 to 30m	10%	10%	East
30.1 to 45m	5%		
>45m	0%		
Total charge in %		40%	
Total charge in l/min		2900	


STEP 4

Required Fire Flow:

10000 l/min

or 166.67 l/s

or 2642 US GPM

 LEA Consulting Ltd. Consulting Engineers and Planners	Water Demand Calculation			
	Prepared:	P.R.	Page No.	C-03
	Checked:	F.M.		
	Proj. #	21111		
Project: 3016-3032 KIRWIN AVE & 3031 LITTLE JOHN LANE	Date:	25-Oct-23		

Total Population: 297 (See Page C-01)

Average Day Demand Calculation:

Residential Per Capita Demand 280 L/cap/day
Average Day Flow 0.963 L/sec

Peak Hour Demand Calculation:

Residential Per Capita Demand 280 L/cap/day
 Peaking Factor 3
Peak Hour Demand 2.888 L/sec


Maximum Day Demand Calculation:

Residential Per Capita Demand 280 L/cap/day
 Peaking Factor 2
Maximum Day Demand 1.925 L/sec

Fire Flow for Residential: 166.67 L/sec

Max. Day Demand plus Fire Flow: 168.59 L/sec

Design Water Demand 168.59 L/sec
 or 2672.18 US GPM

 LEA Consulting Ltd. Consulting Engineers and Planners	Connection Demand Table			
	Prepared:	P.R.	Page No.	C-04
	Checked:	F.M.		
	Proj. #	21111		
Project: 3016-3032 KIRWIN AVE & LITTLE JOHN LANE City Of Mississauga	Date:	25-Oct-23		

Connection Demand Table

WATER CONNECTION

Connection Point	Kirwin Ave
Pressure zone of connection point	Zone 2
Total equivalent population to be serviced	297 Based on Region of Peel 2020 Criteria
Total lands to be serviced	0.392 ha

HYDRANT FLOW TEST

Hydrant flow test location	KIRWIN AVE		
	Pressure (kPa)	Flow (l/s)	Time
Minimum water pressure	20	332.8	
Maximum water pressure	76	63.1	

No.	Wate Demand	Demand	Units
	Demand type		
1	Average day flow	0.96	l/s
2	Maximum day flow	1.93	l/s
3	Peak hour flow	2.89	l/s
4	Fire flow	166.67	l/s
Analysis			
5	Maximum day plus fire flow	168.59	l/s

HYDRANT FLOW TEST

Connection Point	Existing 300mm Watermain on Kirwin Ave
Total equivalent population to be serviced	297
Total lands to be serviced	0.392 ha
Standard Wastewater Sewer Effluent (L/s)	13.08
Actual Wastewater Sewer Effluent (L/s)	4.33

APPENDIX D

Storm Sewer Capacity Assessment

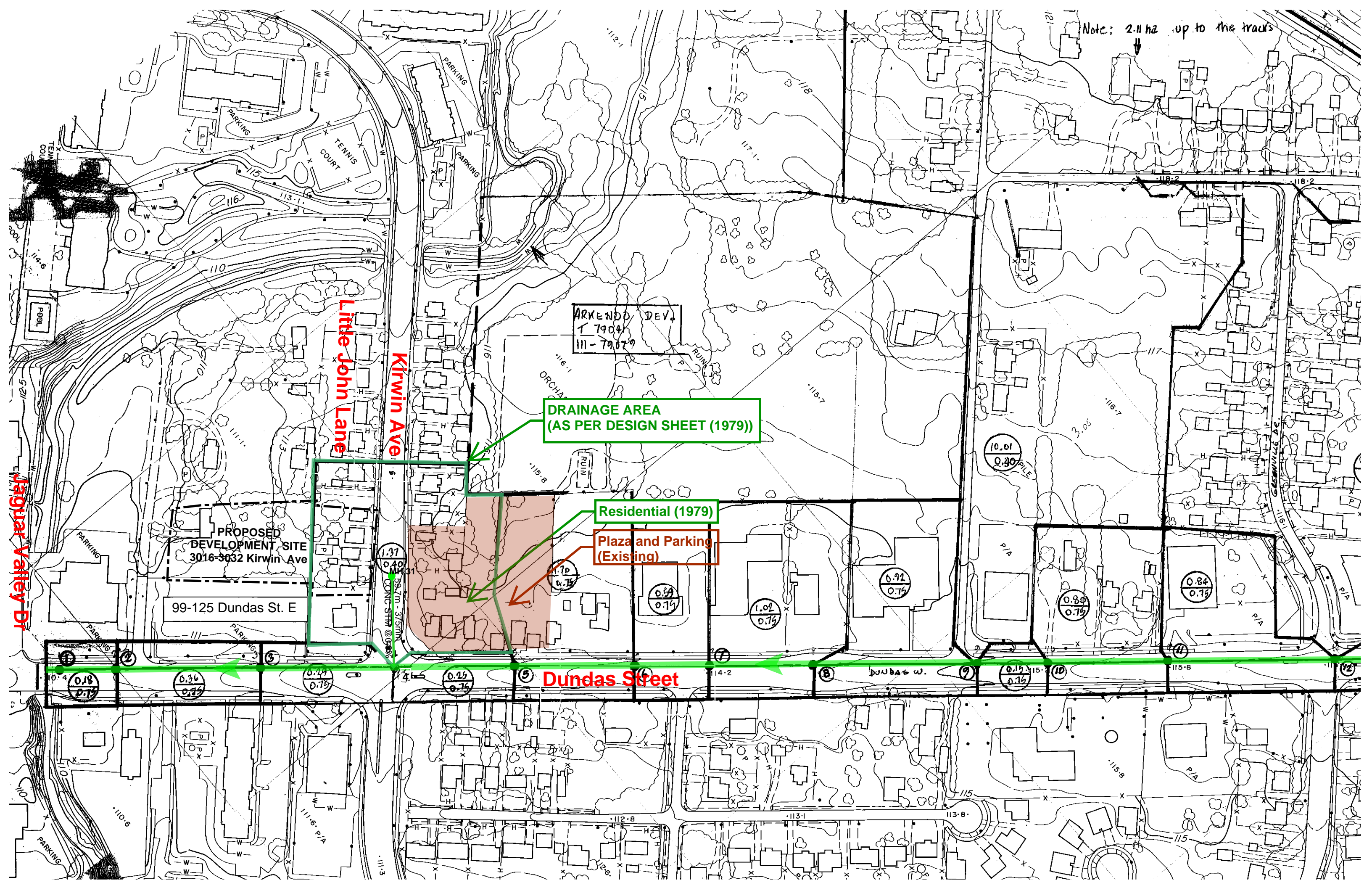


APPENDIX D-01

Historic Drainage Area Plan 1979

City of Mississauga





Note: 2.11 ha up to the tracks

ARKENDD DEV.
1 79041
111-79041

DRAINAGE AREA
(AS PER DESIGN SHEET (1979))

Residential (1979)

Plaza and Parking
(Existing)

Dundas Street

PROPOSED
DEVELOPMENT SITE
3016-3032 Kirwin Ave

99-125 Dundas St. E

Little John Lane

Kirwin Ave

Jaguar Valley Dr

APPENDIX D-02

Historic Design Sheet 1979

City of Mississauga



CANADA | INDIA | AFRICA | MIDDLE EAST

DESIGN SHEET (1979)

SUBDIVISION _____		CITY OF MISSISSAUGA												SHEET No. <u>2</u> OF <u>3</u> DATE _____								
CONSULTANT _____		STORM DRAINAGE DESIGN CHART FOR CIRCULAR DRAINS FLOWING FULL												PROJECT No. _____								
MAJOR DRAINAGE AREA _____														DESIGNED BY _____								
LOCATION OF SECTION	FROM UPSTREAM	TO DOWNSTREAM	ADJACENT CONTRIBUTORY AREA	RUNOFF COEFFICIENT		ACCUMULATIVE AREA DRAINED BY SECTION	ACCUMULATIVE AREA TIMES RUNOFF COEFFICIENT FOR SECTION	FLOW TIME TO SECTION (FROM EXTREME UPSTREAM INLET)	INITIAL TIME OF CONCENTRATION AT EXTREME UPSTREAM INLET	TIME OF CONCENTRATION AT UPSTREAM END OF SECTION	INTENSITY OF RAINFALL	QUANTITY OF FLOW TO BE ACCOMMODATED IN SECTION.	TYPE OF PIPE	MANNINGS ROUGHNESS COEFFICIENT	SLOPE	DIAMETER	LENGTH OF SECTION	VELOCITY OF FLOW WITH PIPE FLOWING FULL	CAPACITY OF PIPE FLOWING FULL	PIPE INVERT AT UPSTREAM M.H.	PIPE INVERT AT DOWNSTREAM M.H.	TIME OF FLOW IN SECTION
	MH#	MH#	A _A (ha)	C _A	A _A x C _A	A = Σ A _A (ha)	A x C = Σ A _A x C _A	t _{CF} (min)	t _{C1} (min)	t _C = t _{C1} + t _{CF} (min)	I mm/hr	Q = 1.48 360 m ³ /sec		n	S	D mm	L m	V m/sec	Q m ³ /sec	m	m	t = L V x 60 min
DUNDAS ST	9	8	10.01	0.40	4.00																	
			0.92	0.75	0.69	31.79	17.00			23.50	75	3.54			0.44	1050	105	2.11	1.29			0.83
								PSS							0.45	1050	91	2.14	1.90			
																		3.79				
	8	7	1.02	0.75	0.77	32.81	17.77			24.33	73	3.60			0.47	1050	65	2.23	1.99			0.47
								PSS							0.45	1050	91	2.14	1.90			
																		3.89				
	7	6	0.59	0.75	0.44	33.40	18.21			24.82	72	3.64			0.29	1050	47	1.73	1.55			0.45
	6	5	1.70	0.75	1.28	35.10	19.49			25.27	71	3.84			0.63	1050	76	2.55	2.26			0.50
								PSS							0.63	1050	91	2.55	2.26			
																		4.52				
	5	4	0.25	0.75	0.19	35.35	19.68			25.77	70	3.84			0.81	1050	74	2.87	2.56			0.43
								PSS							0.80	975	91	2.71	2.09			
																		4.65				
	4	3	1.37	0.40	0.55																	
			0.29	0.75	0.22	27.01	20.45			26.20	69	3.92			0.79	1050	86	2.87	2.53			0.50
								PSS							0.80	975	91	2.71	2.09			
																		4.62				

MAJOR DRAINAGE AREA _____

STORM DRAINAGE DESIGN CHART FOR CIRCULAR DRAINS FLOWING FULL

DESIGNED BY _____

[illegible]

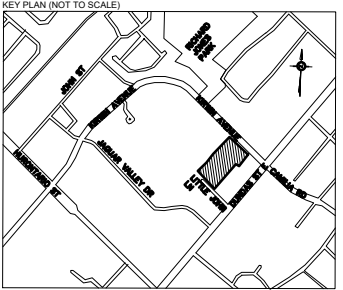
APPENDIX D-03

Updated Existing Drainage Area Plan for Kirwin



UPDATED EXISTING DRAINAGE AREAS (2022)

SUBJECT SITE



- LEGEND**
- MH EXISTING MANHOLE
 - CB EXISTING CATCHBASIN
 - SUBJECT SITE
 - EXISTING PROPERTY LINE
 - DRAINAGE BOUNDARY
 - DRAINAGE ID/RUNOFF COEFFICIENT DRAINAGE AREA (ha)

1		ISSUED FOR SPA SUBMISSION	2022-11-16	P.R.	F.M.
No.	Revision	Date	By	App.	

625 Cochrane Drive, Suite 900
Markham, Ontario
L3R 9R9, Canada
Tel: (905) 470-0015
Fax: (905) 470-0030



Owner/Client:
DASS METAL

Location:
3031 LITTLE JOHN & 3016-3032 KIRWIN AVE DEVELOPMENT

Title:
KIRWIN AVE STORM SEWER ANALYSIS EXISTING DRAINAGE PLAN

Designed By:	F.M.	Drawn By:	J.W.	Checked By:	F.M.
Scale:	1:500	Date:	FEB., 2021	Drawing No.:	FIG-3
Project No.:	21111				

APPENDIX D-04

Updated Design Sheet



DEVELOPMENT: 3016 Kirwin Ave

CONSULTANT: LEA Consulting Ltd

MAJOR DRAINAGE AREA: Cooksville Creek

MISSISSAUGA
Transportation and Works
STORM DRAINAGE DESIGN CHART
FOR CIRCULAR DRAINS FLOWING FULL

SHEET No.:

DATE: 16-Nov-22



DESIGNED BY: F.M.

CHECKED BY: F.F.

City of Mississauga Intensity 10yr = $1010/(tc+4.6)^{0.78}$

Pre-Development Condition

FROM UPSTREAM	TO DOWNSTREAM	Drainage area ID	Catchment AREA	RUNOFF COEFFICIENT	AREA TIMES RUNOFF COEFFICIENT	ACCUMULATIVE AREA DRAINED BY SECTION	ACCUMULATIVE AREA TIMES RUNOFF COEFFICIENT FOR SECTION	FLOW TIME TO SECTION FROM EXTREME UPSTREAM INLET	INITIAL TIME OF CONCENTRATION AT EXTREME UPSTREAM INL.	TIME OF CONCENTRATION UPSTREAM END OF SECTION	INTENSITY OF RAINFALL	QUANTITY OF FLOW ACCUMULATED IN SECTION	TYPE OF PIPE	MANNING ROUGHNESS COEFFICIENT	SLOPE	DIAMETER	LENGTH OF SECTION	VELOCITY OF FLOW WITH PIPE FLOWING FULL	CAPACITY OF PIPE FLOWING FULL	PIPE INVERT AT UPSTREAM M.H.	PIPE INVERT AT DOWNSTREAM M.H.	TIME OF FLOW IN SECTION	QUANTITY OF FLOW TO PIPE FLOWING FULL	NOTES	
MH#	MH#		A ha	C	AxC	SUM. A ha	SUM AxC	tc _i min	tc _i min	tc=tc _i +tc _i min	i mm/hr	Q=iAC/360 m3/sec		n	S %	D mm	L m	V m/sec	Q _f m3/sec	m	m	t=L/Vx60 min	Q/Q _f %		
																						0			
MH31	5	E1	0.682	0.75	0.51	0.682	0.51	0	15	15	99.2	0.141	CONC	0.013	1.25	400	49.33	1.85	0.233	110.35	N/A	0.44	0.71		Surcharged
		E2	0.138*	0.62	0.09	0.138	0.09	0	15	15	99.2	0.024**													
5	4 (MH30)	E4	0.266	0.90	0.24	1.143	0.87	0.44	15	15.44	97.5	0.236***	CONC	0.013	1.25	400	4.56	1.85	0.233	N/A	109.69	0.04	1.01		
		E3	0.057*	0.62	0.04																				
Flow from STM Sewer on Dundas Street						35.350	19.68			25.77	70.5	3.85										0.43			SUM AxC= 19.68, Q=3840l/s, Tc=25.77 min
4 (MH30)	3		0.290	0.75	0.22	36.783	20.77	0.43	25.77	26.20	69.7	4.02	CONC	0.013	0.79	1050	86.00	2.80	2.43			0.51	0.91		
													CONC	0.013	0.80	975	91.00	2.68	2.00			0.56			
																			4.43						
3	2		0.360	0.75	0.27	37.143	21.04	0.51	26.20	26.71	68.8	4.02	CONC	0.013	0.78	1050	91.00	2.79	2.41			0.54	0.91		
													CONC	0.013	0.80	975	76.00	2.68	2.00			0.47			
																			4.42						
2	CULVERT		0.180	0.75	0.14	37.323	21.17	0.54	26.71	27.26	67.9	3.99	CONC	0.013	0.84	1050	35.97	2.89	2.50			0.21	0.89		
													CONC	0.013	0.80	975	35.00	2.68	2.00			0.22			
																			4.51						

* Drainage area from Subject Site

** 10-yr storm flow from the proposed site under existing conditions, using actual runoff coefficient. (i.e. not discounting to 0.5)

*** includes flow from 0.057 ha from the subject site, equivalent to 9.7 L/s

Post-Development Condition

FROM UPSTREAM	TO DOWNSTREAM		Catchment AREA	RUNOFF COEFFICIENT	AREA TIMES RUNOFF COEFFICIENT	ACCUMULATIVE AREA DRAINED BY SECTION***	ACCUMULATIVE AREA TIMES RUNOFF COEFFICIENT FOR SECTION	FLOW TIME TO SECTION FROM EXTREME UPSTREAM INLET	INITIAL TIME OF CONCENTRATION AT EXTREME UPSTREAM INL.	TIME OF CONCENTRATION UPSTREAM END OF SECTION	INTENSITY OF RAINFALL	QUANTITY OF FLOW ACCUMULATED IN SECTION	TYPE OF PIPE	MANNING ROUGHNESS COEFFICIENT	SLOPE	DIAMETER	LENGTH OF SECTION	VELOCITY OF FLOW WITH PIPE FLOWING FULL	CAPACITY OF PIPE FLOWING FULL	PIPE INVERT AT UPSTREAM M.H.	PIPE INVERT AT DOWNSTREAM M.H.	TIME OF FLOW IN SECTION	QUANTITY OF FLOW TO PIPE FLOWING FULL	NOTES
MH#	MH#		A ha	C	AxC	SUM. A ha	SUM AxC	tc _i min	tc _i min	tc=tc _i +tc _i min	i mm/hr	Q=iAC/360 m3/sec		n	S %	D mm	L m	V m/sec	Q _f m3/sec	m	m	t=L/Vx60 min	Q/Q _f %	
																						0		
MH31	5	E1 E2+E3	0.682 0.337*	0.75	0.51	0.682	0.51	0	15	15	99.2	0.141 0.015 **	CONC	0.013	1.25	400	49.33	1.85	0.233	110.35	N/A	0.44	0.67	
5	4 (MH30)	E4	0.266	0.90	0.24	0.948	0.75	0.44	15	15.44	97.5	0.218	CONC	0.013	1.25	400	4.56	1.85	0.233	N/A	0.00	0.04	0.94	
Flow from STM Sewer on Dundas Street						35.350	19.68			25.77	70.5	3.85										0.43		
4	3		0.290	0.75	0.22	36.588	20.65	0.43	25.77	26.20	69.7	4.013	CONC	0.013	0.79	1050	86.00	2.80	2.43			0.51	0.91	
													CONC	0.013	0.80	975	91.00	2.68	2.00			0.56		
																			4.431					
3	2		0.360	0.75	0.27	36.948	20.92	0.51	26.20	26.71	68.8	4.013	CONC	0.013	0.78	1050	91.00	2.79	2.41			0.54	0.91	
													CONC	0.013	0.80	975	76.00	2.68	2.00			0.47		
																			4.416					
2	CULVERT		0.180	0.75	0.14	37.128	21.05	0.54	26.71	27.26	67.9	3.985	CONC	0.013	0.84	1050	35.97	2.89	2.50			0.21	0.88	
													CONC	0.013	0.80	975	35.00	2.68	2.00			0.22		
																			4.507					

* Controlled Drainage area from Subject Site, post-development conditions.

** Overcontrolled flows based on the 2-year pre-development with C = 0.5 was used for flow from the proposed site under post-development condition. Includes 10-year uncontrolled flow from the subject site under post-development conditions.

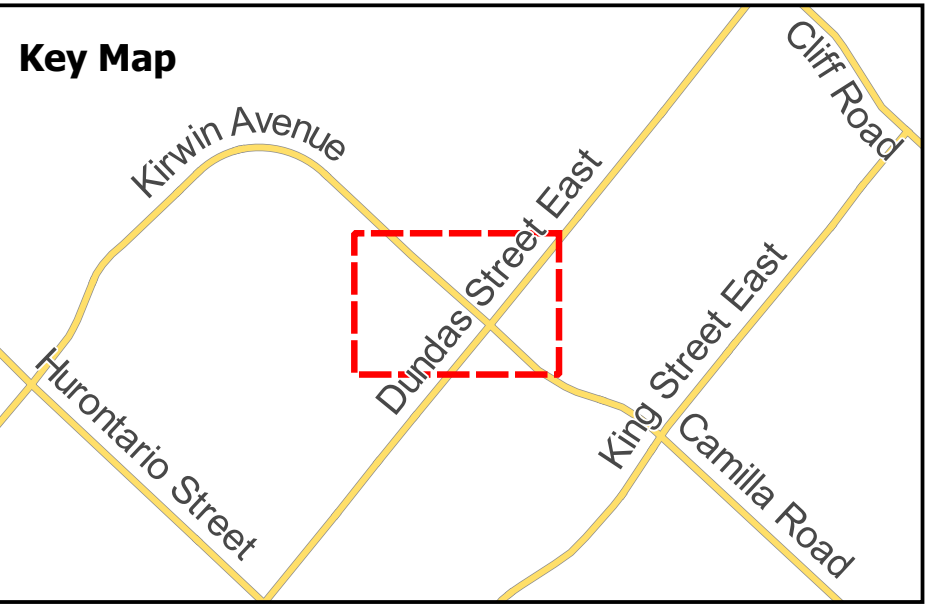
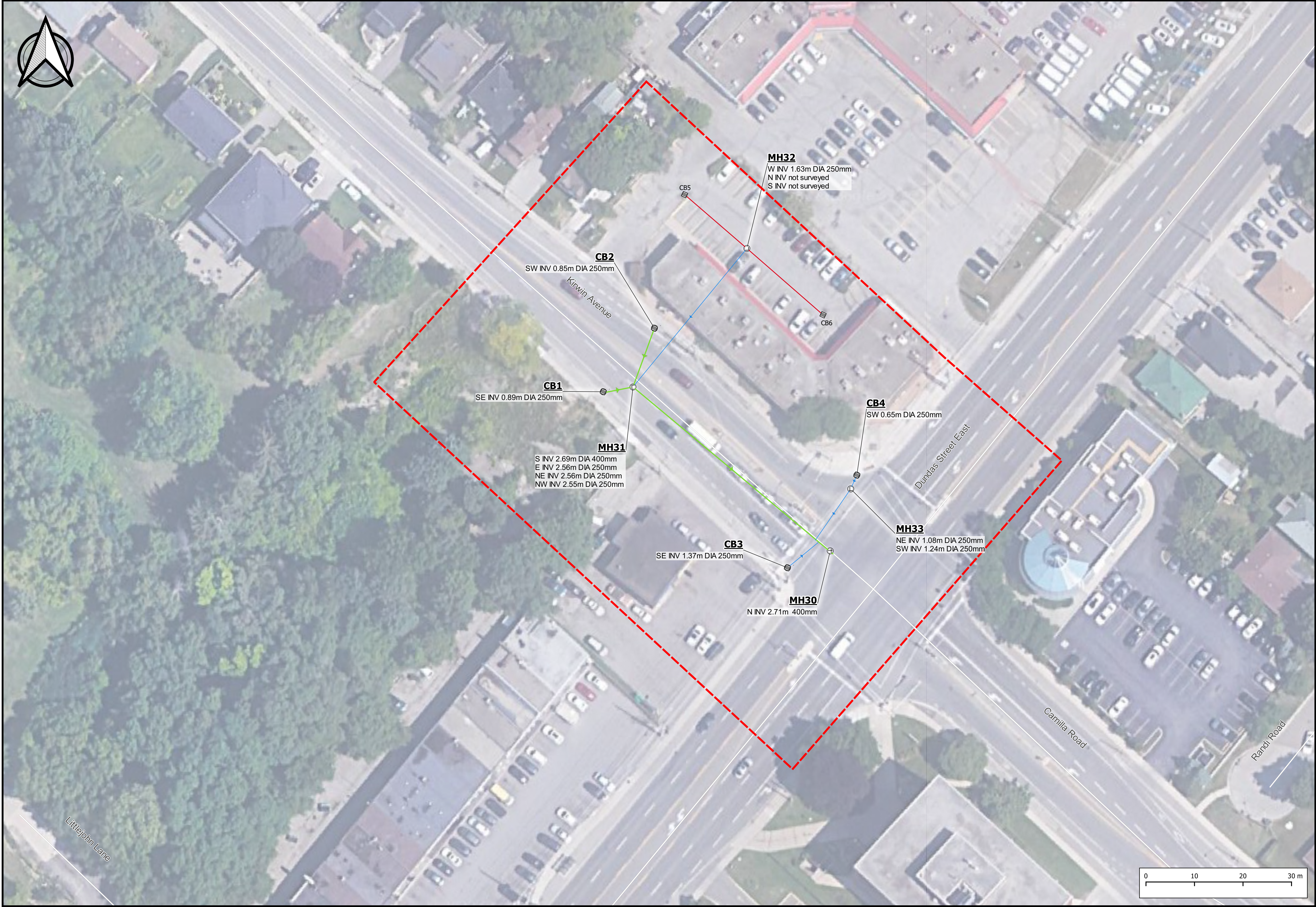
Note: Area from Overcontrolled site is not included in the Accumulated Area so that it does not impact the flow calculation. The overcontrolled flow has been directly included in the flow in all downstream sewers.

*** Cumulative Drainage area does not include controlled/uncontrolled area from the subject site.

APPENDIX D-05

CCTV Report





General Notes

1. Field inspection was performed on March 31, 2022. The scope of work included sewer flushing, sewer CCTV inspections, and invert measurements.

2. The location of the sewers and direction of flow were defined based on line-of-sight and judgment of the field technician.

3. Other buried utilities within the Investigation Limits are not shown.

Map Legend

Sewerlines

- Storm Sewer
- Lateral Lines
- Sewer not Surveyed

Point Features

- CB
- MH

Sources:
Projection System: NAD 83 UTM ZONE 17N

Revision History

Project: Dundas Street E and Kirwin Avenue, Mississauga

[illegible]

Asset

Owner: City of Mississauga

PSR: CB1MH31

Upstream MH: CB1

Downstream MH: MH31

	USMH	DSMH
Rim to Invert:	0.89 m	2.55 m
Rim to Grade:		

Pipe Geometry: 250 mm (Circular)

Material: Concrete Pipe (non-reinforced)

Lining Method:

Coating Method:

Year Constructed:

Pipe Use: Stormwater Pipe

Total Length: (unspecified)

Project

Project: 2022-602

Work Order:

Customer: Lea Consulting Ltd.

PO Number:

Additional Info:

Inspection

Media Date/Time: 31 • Mar • 2022 10:28

Surveyed By: Markus Hirani - I2S inc

Reviewed By:

Camera Direction: Downstream

Purpose: Sewer System Evaluation Survey

Technology: CCTV

Pre-Cleaning: No Pre-Cleaning

Date Cleaned:

Flow Control:

Length Surveyed: 005.40 m

Weather: Light Rain

Location

Address: Kirwin Ave, Mississauga

Drainage Area:

Latitude:

Longitude:

Elevation:

GPS Accuracy:

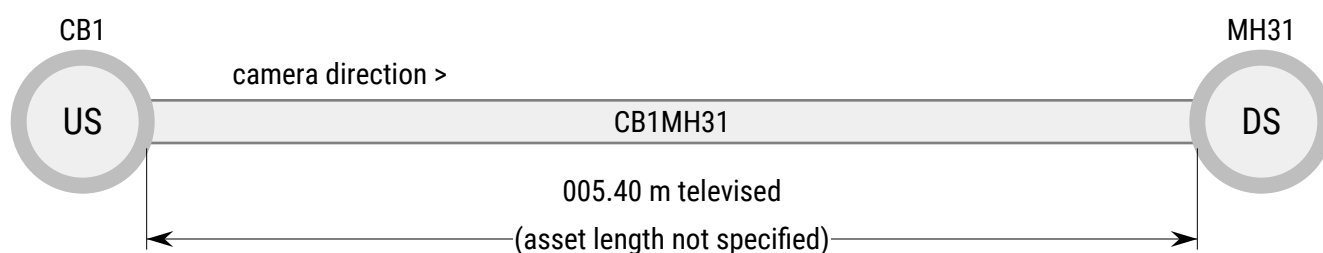
Location Code: Secondary Road

Location Details:

Ratings

	Structural	O & M	Overall
Quick:	4131	0000	4131
$\sum_{i=1}^5 SG_i$ Pipe Rating (OR):	7	0	7
Rating Index (RI):	3.5	0	3.5
Consequence of Failure:			

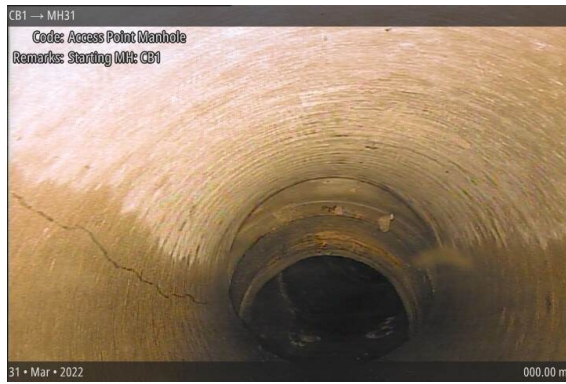
Summary



Observations



Snapshots



Access Point Manhole at 000.00 m | Starting MH: CB1. Cannot view cb due to slope



Miscellaneous Water Level at 000.00 m



Fracture Longitudinal at 003.20 m, 9 o'clock



Joint Offset Large at 005.30 m



Miscellaneous Survey Abandoned at 005.40 m | Survey abandoned due to offset joint.

Asset

Owner:

PSR:

Upstream MH:

Downstream MH:

USMH **DSMH**

Rim to Invert:

Rim to Grade:

Pipe Geometry:

Material:

Lining Method:

Coating Method:

Year Constructed:

Pipe Use:

Total Length:

Project

Project:

Work Order:

Customer:

PO Number:

Additional Info:

Inspection

Media Date/Time:

Surveyed By:

Reviewed By:

Camera Direction:

Purpose:

Technology:

Pre-Cleaning:

Date Cleaned:

Flow Control:

Length Surveyed:

Weather:

Location

Address:

Drainage Area:

Latitude:

Longitude:

Elevation:

GPS Accuracy:

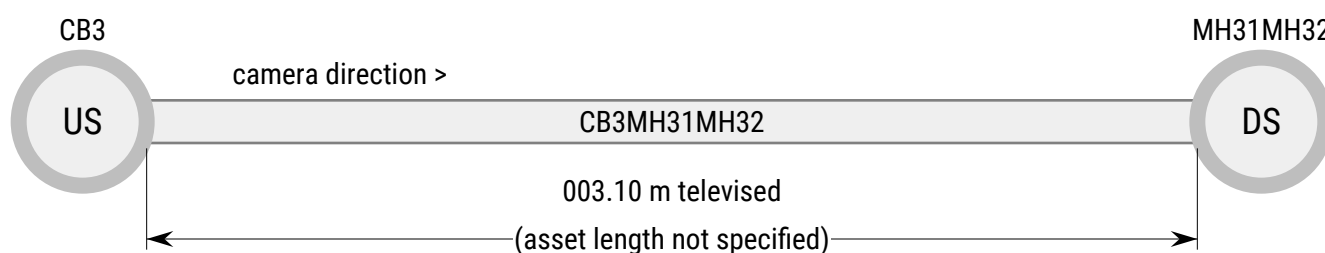
Location Code:

Location Details:

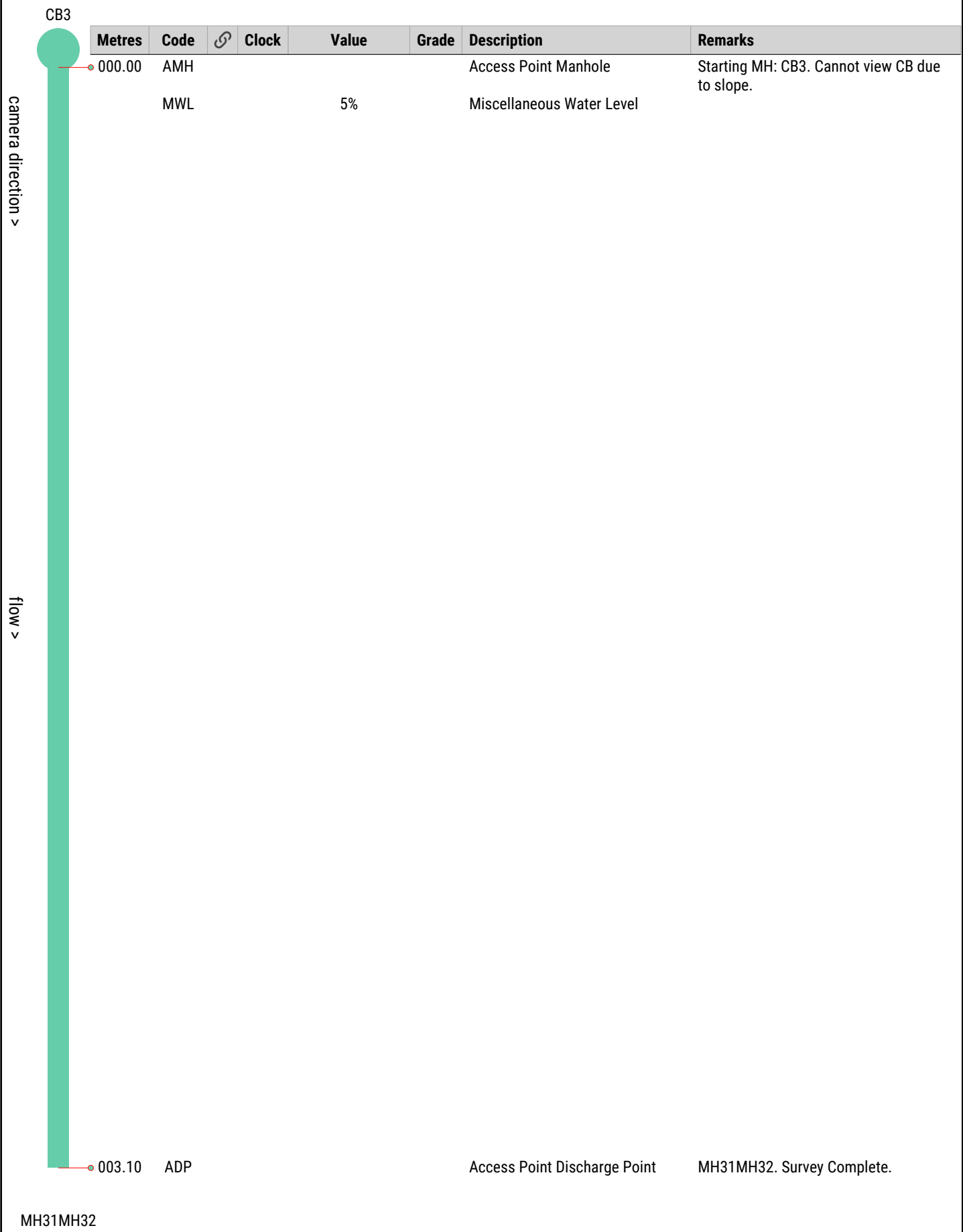
Ratings

	Structural	O & M	Overall
Quick:	<input type="text" value="0000"/>	<input type="text" value="0000"/>	<input type="text" value="0000"/>
$\sum_{i=1}^5 SG_i$ Pipe Rating (OR):	<input type="text" value="0"/>	<input type="text" value="0"/>	<input type="text" value="0"/>
Rating Index (RI):	<input type="text" value="0"/>	<input type="text" value="0"/>	<input type="text" value="0"/>
Consequence of Failure:	<input type="text"/>		

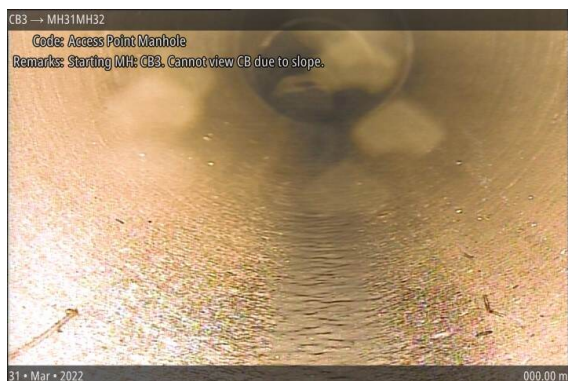
Summary



Observations



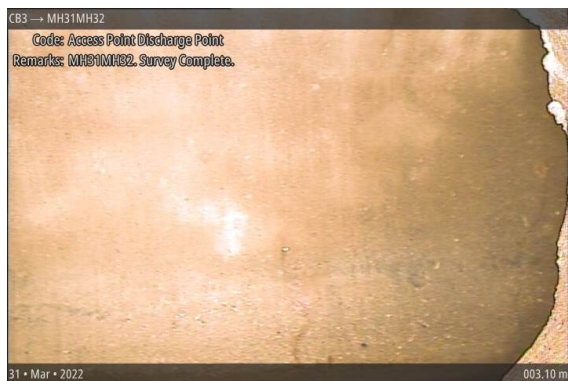
Snapshots



Access Point Manhole at 000.00 m | Starting MH: CB3. Cannot view CB due to slope.



Miscellaneous Water Level at 000.00 m



Access Point Discharge Point at 003.10 m | MH31MH32. Survey Complete.

Asset

Owner: City of Mississauga

PSR: CB4MH31MH32

Upstream MH: CB4

Downstream MH: MH31MH32

Rim to Invert: **USMH** 0.65 m **DSMH**

Rim to Grade:

Pipe Geometry: 250 mm (Circular)

Material: Concrete Pipe (non-reinforced)

Lining Method:

Coating Method:

Year Constructed:

Pipe Use: Stormwater Pipe

Total Length: (unspecified)

Project

Project: 2022-602

Work Order:

Customer: Lea Consulting Ltd.

PO Number:

Additional Info:

Inspection

Media Date/Time: 31 • Mar • 2022 11:33

Surveyed By: Markus Hirani - I2S inc

Reviewed By:

Camera Direction: Downstream

Purpose: Sewer System Evaluation Survey

Technology: CCTV

Pre-Cleaning: No Pre-Cleaning

Date Cleaned:

Flow Control:

Length Surveyed: 003.40 m

Weather: Dry - No Precipitation During Survey

Location

Address: Kirwin Ave, Mississauga

Drainage Area:

Latitude:

Longitude:

Elevation:

GPS Accuracy:

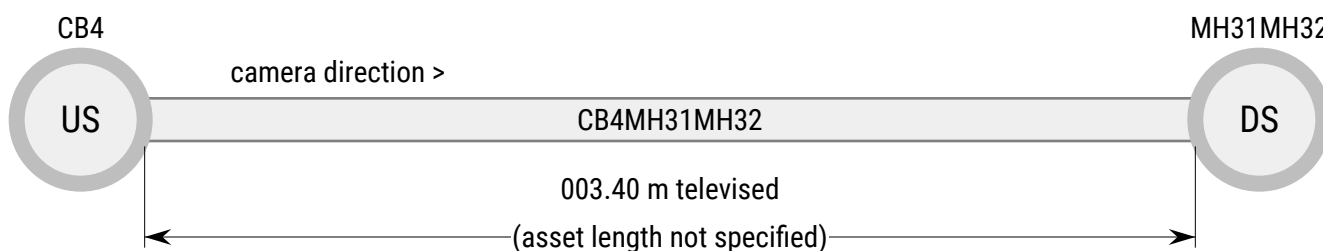
Location Code: Secondary Road

Location Details:

Ratings

	Structural	O & M	Overall
Quick:	3100	0000	3100
$\sum_{i=1}^5 SG_i$ Pipe Rating (OR):	3	0	3
Rating Index (RI):	3	0	3
Consequence of Failure:			

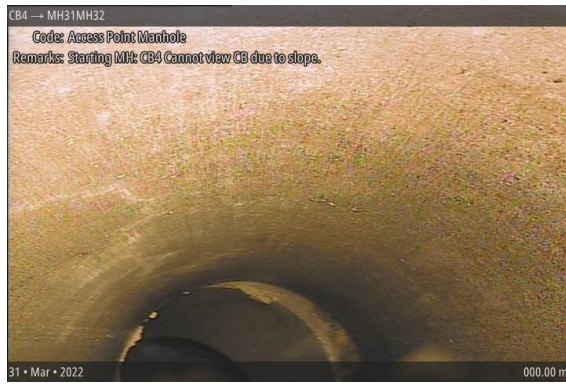
Summary



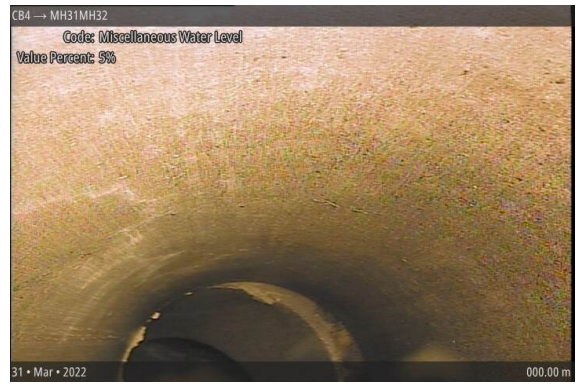
Observations



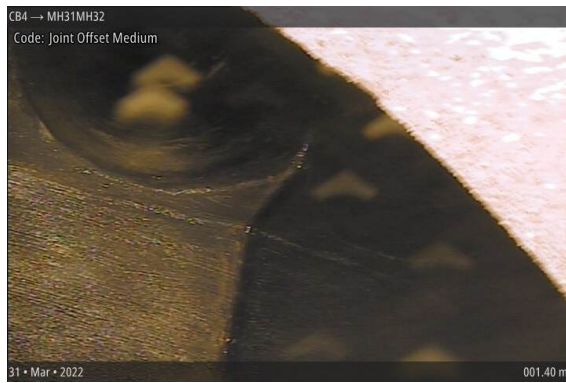
Snapshots



Access Point Manhole at 000.00 m | Starting MH:
CB4 Cannot view CB due to slope.



Miscellaneous Water Level at 000.00 m



Joint Offset Medium at 001.40 m



Access Point Discharge Point at 003.40 m |
MH31MH32. Survey Complete.

Asset

Owner: City of Mississauga

PSR: CB1MH31

Upstream MH: CB1

Downstream MH: MH31

	USMH	DSMH
Rim to Invert:	0.89 m	2.55 m
Rim to Grade:		

Pipe Geometry: 250 mm (Circular)

Material: Concrete Pipe (non-reinforced)

Lining Method:

Coating Method:

Year Constructed:

Pipe Use: Stormwater Pipe

Total Length: (unspecified)

Project

Project: 2022-602

Work Order:

Customer: Lea Consulting Ltd.

PO Number:

Additional Info: Reverse to Upstream.

Inspection

Media Date/Time: 31 • Mar • 2022 10:41

Surveyed By: Markus Hirani - I2S inc

Reviewed By:

Camera Direction: Upstream

Purpose: Sewer System Evaluation Survey

Technology: CCTV

Pre-Cleaning: No Pre-Cleaning

Date Cleaned:

Flow Control:

Length Surveyed: 002.10 m

Weather: Light Rain

Location

Address: Kirwin Ave, Mississauga

Drainage Area:

Latitude:

Longitude:

Elevation:

GPS Accuracy:

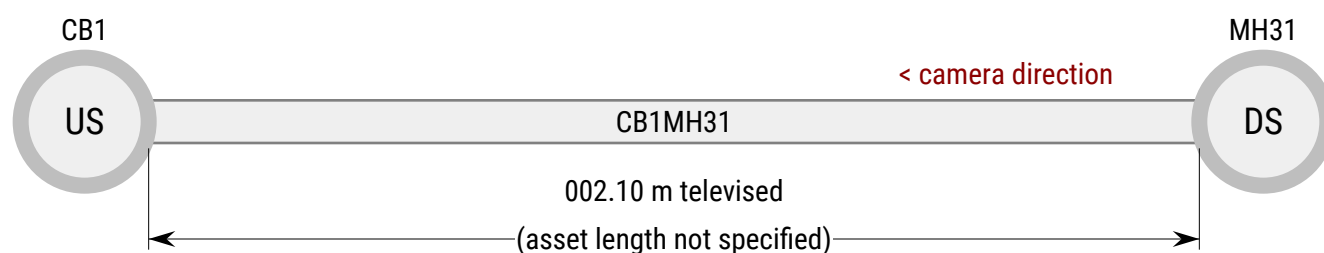
Location Code: Secondary Road

Location Details:

Ratings

	Structural	O & M	Overall
Quick:	0000	0000	0000
$\sum_{i=1}^5 SG_i$ Pipe Rating (OR):	0	0	0
Rating Index (RI):	0	0	0
Consequence of Failure:			

Summary



Observations

CB1

Metres	Code		Clock	Value	Grade	Description	Remarks
--------	------	---	-------	-------	-------	-------------	---------

002.10	AM					Access Point Meter	Cannot get to reversal point do to offset joint. Reversal complete.
--------	----	--	--	--	--	--------------------	---

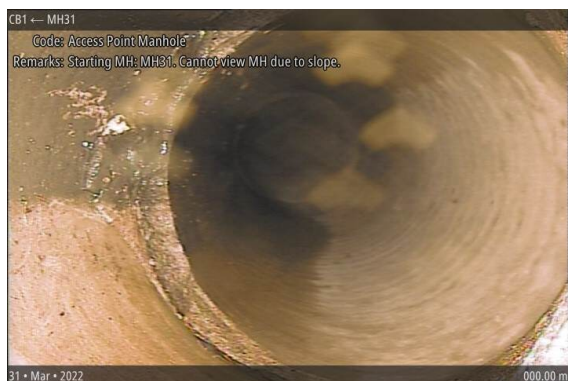
< flow

camera direction >

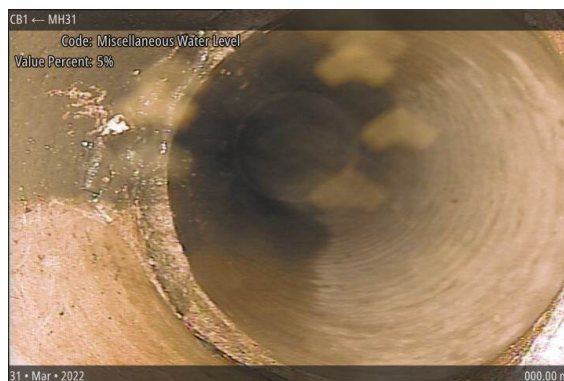
000.00	MWL AMH			5%		Miscellaneous Water Level Access Point Manhole	Starting MH: MH31. Cannot view MH due to slope.
--------	------------	--	--	----	--	---	---

MH31

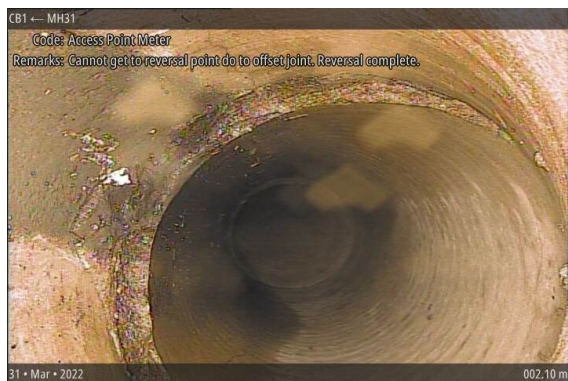
Snapshots



Access Point Manhole at 000.00 m | Starting MH: MH31. Cannot view MH due to slope.



Miscellaneous Water Level at 000.00 m



Access Point Meter at 002.10 m | Cannot get to reversal point do to offset joint. Reversal complete.

Asset

Owner: City of Mississauga

PSR: CB2MH31

Upstream MH: CB2

Downstream MH: MH31

	USMH	DSMH
Rim to Invert:	0.92 m	1.63 m
Rim to Grade:		

Pipe Geometry: 250 mm (Circular)

Material: Concrete Pipe (non-reinforced)

Lining Method:

Coating Method:

Year Constructed:

Pipe Use: Stormwater Pipe

Total Length: (unspecified)

Project

Project: 2022-602

Work Order:

Customer: Lea Consulting Ltd.

PO Number:

Additional Info:

Inspection

Media Date/Time: 31 • Mar • 2022 10:13

Surveyed By: Markus Hirani - I2S inc

Reviewed By:

Camera Direction: Upstream

Purpose: Sewer System Evaluation Survey

Technology: CCTV

Pre-Cleaning: No Pre-Cleaning

Date Cleaned:

Flow Control:

Length Surveyed: 012.70 m

Weather: Light Rain

Location

Address: Kirwin Ave, Mississauga

Drainage Area:

Latitude:

Longitude:

Elevation:

GPS Accuracy:

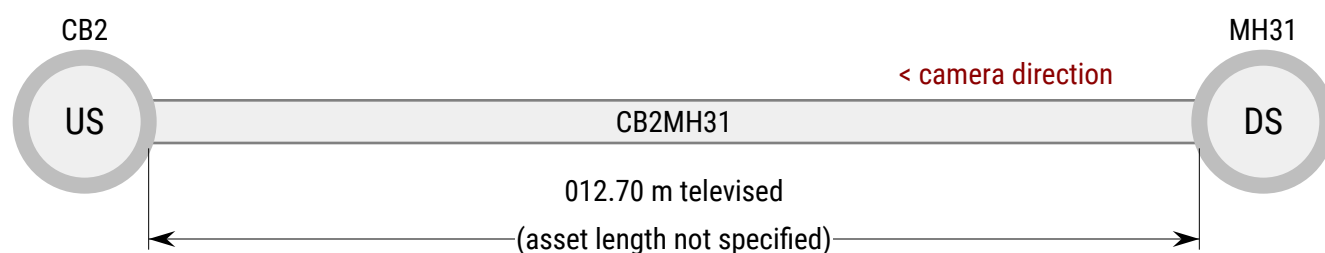
Location Code: Secondary Road

Location Details:

Ratings

	Structural	O & M	Overall
Quick:	0000	0000	0000
$\sum_{i=1}^5 SG_i$ Pipe Rating (OR):	0	0	0
Rating Index (RI):	0	0	0
Consequence of Failure:			

Summary



Observations

CB2

Metres	Code		Clock	Value	Grade	Description	Remarks
--------	------	---	-------	-------	-------	-------------	---------

012.70	AMH					Access Point Manhole	Ending MH: CB2. Survey Complete.
--------	-----	--	--	--	--	----------------------	----------------------------------

< flow

camera direction >

000.00	MWL AMH			5%		Miscellaneous Water Level Access Point Manhole	Starting MH: MH31. Cannot view MH due to slope.
--------	------------	--	--	----	--	---	--

MH31

Snapshots



Access Point Manhole at 000.00 m | Starting MH: MH31. Cannot view MH due to slope.



Miscellaneous Water Level at 000.00 m



Access Point Manhole at 012.70 m | Ending MH: CB2. Survey Complete.

Asset

Owner: City of Mississauga

PSR: MH31MH30

Upstream MH: MH31

Downstream MH: MH30

USMH **DSMH**

Rim to Invert: 2.69 m

Rim to Grade:

Pipe Geometry: 400 mm (Circular)

Material: Concrete Pipe (non-reinforced)

Lining Method:

Coating Method:

Year Constructed:

Pipe Use: Stormwater Pipe

Total Length: (unspecified)

Project

Project: 2022-602

Work Order:

Customer: Lea Consulting Ltd.

PO Number:

Additional Info:

Inspection

Media Date/Time: 31 • Mar • 2022 08:32

Surveyed By: Markus Hirani - I2S inc

Reviewed By:

Camera Direction: Downstream

Purpose: Sewer System Evaluation Survey

Technology: CCTV

Pre-Cleaning: Light Cleaning

Date Cleaned: 2022-03-31

Flow Control:

Length Surveyed: 058.10 m

Weather: Light Rain

Location

Address: Kirwin Ave, Mississauga

Drainage Area:

Latitude:

Longitude:

Elevation:

GPS Accuracy:

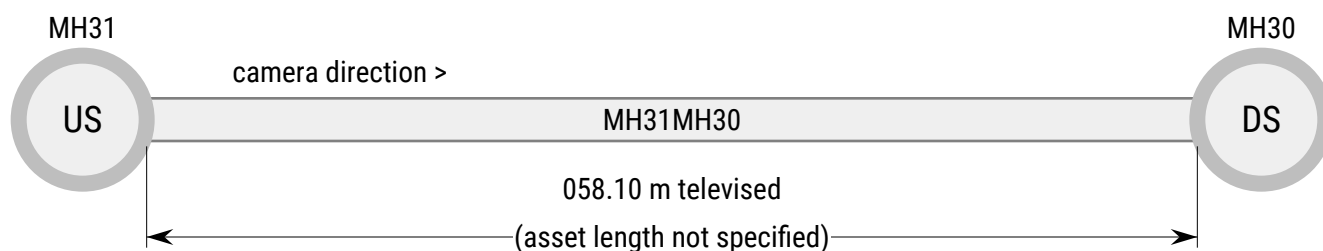
Location Code: Secondary Road

Location Details:

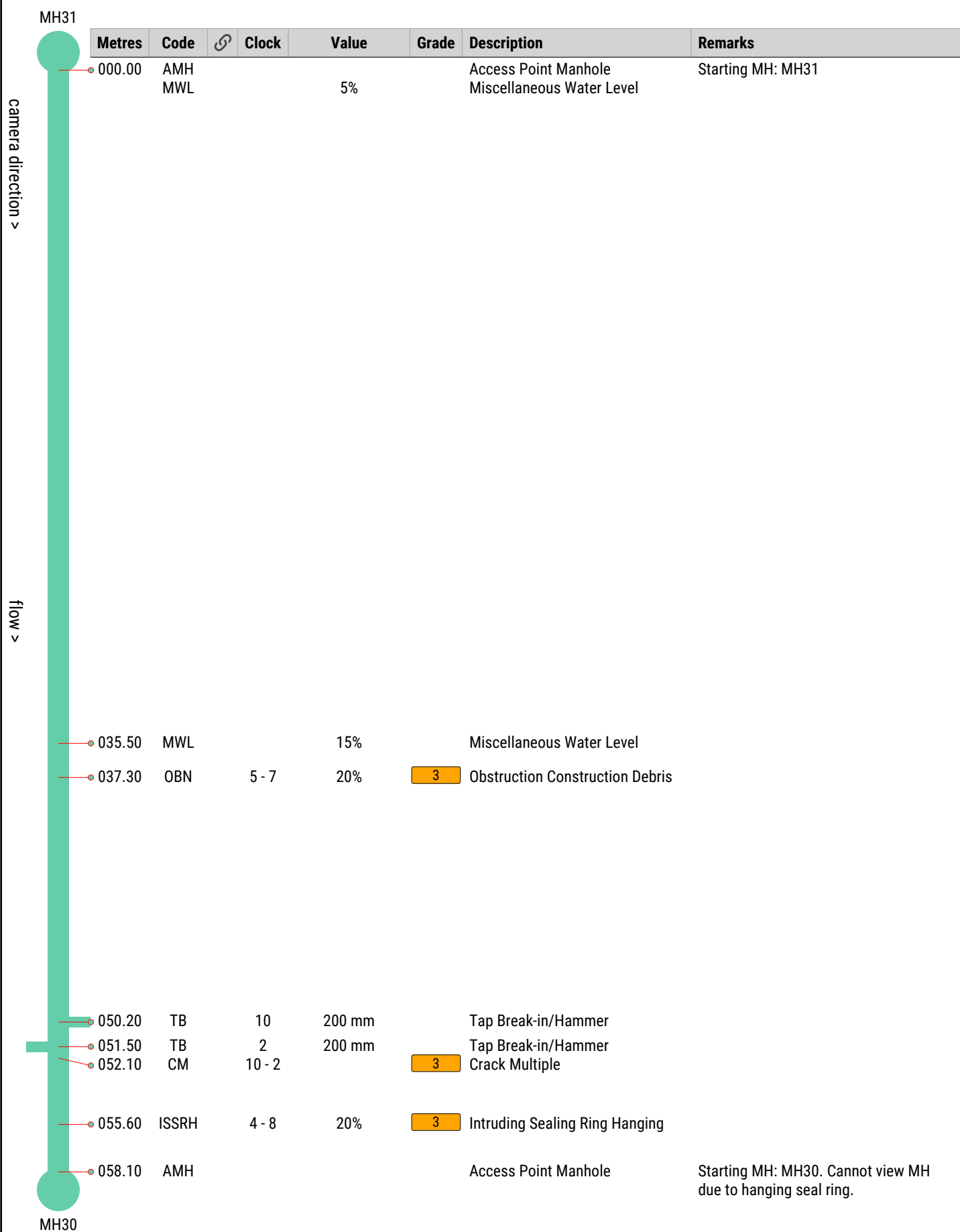
Ratings

	Structural	O & M	Overall
Quick:	3100	3200	3300
$\sum_{i=1}^5 SG_i$ Pipe Rating (OR):	3	6	9
Rating Index (RI):	3	3	3
Consequence of Failure:			

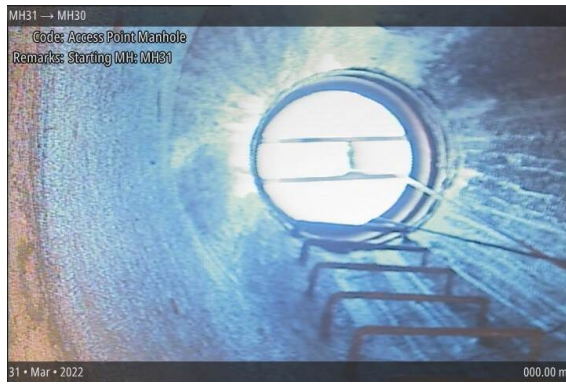
Summary



Observations



Snapshots



Access Point Manhole at 000.00 m | Starting MH: MH31



Miscellaneous Water Level at 000.00 m



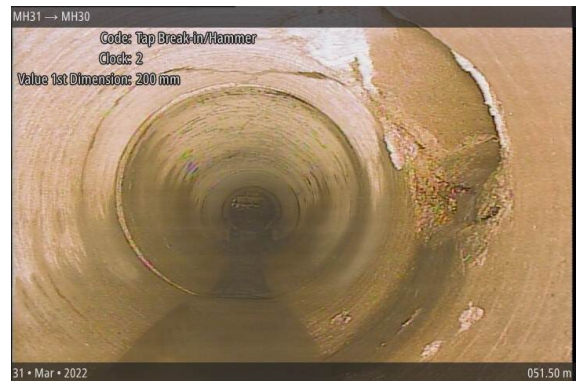
Miscellaneous Water Level at 035.50 m



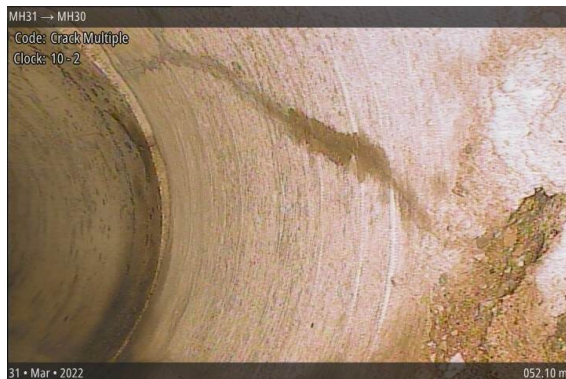
Obstruction Construction Debris at 037.30 m, 5 - 7 o'clock



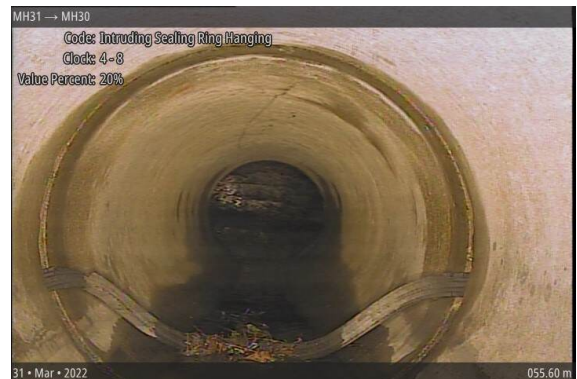
Tap Break-in/Hammer at 050.20 m, 10 o'clock



Tap Break-in/Hammer at 051.50 m, 2 o'clock

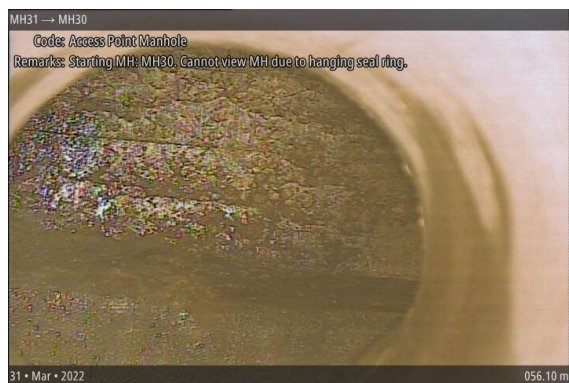


Crack Multiple at 052.10 m, 10 - 2 o'clock



Intruding Sealing Ring Hanging at 055.60 m, 4 - 8 o'clock

Snapshots



Access Point Manhole at 056.10 m | Starting MH:
MH30. Cannot view MH due to hanging seal ring.

Asset

Owner: City of Mississauga

PSR: MH31MH32

Upstream MH: MH32

Downstream MH: MH31

	USMH	DSMH
Rim to Invert:	1.63 m	2.56 m

Rim to Grade:

Pipe Geometry: 250 mm (Circular)

Material: Concrete Pipe (non-reinforced)

Lining Method:

Coating Method:

Year Constructed:

Pipe Use: Stormwater Pipe

Total Length: (unspecified)

Project

Project: 2022-602

Work Order:

Customer: Lea Consulting Ltd.

PO Number:

Additional Info:

Inspection

Media Date/Time: 31 • Mar • 2022 09:51

Surveyed By: Markus Hirani - I2S inc

Reviewed By:

Camera Direction: Upstream

Purpose: Sewer System Evaluation Survey

Technology: CCTV

Pre-Cleaning: Light Cleaning

Date Cleaned: 2022-03-31

Flow Control:

Length Surveyed: 035.20 m

Weather: Light Rain

Location

Address: Kirwin Ave, Mississauga

Drainage Area:

Latitude:

Longitude:

Elevation:

GPS Accuracy:

Location Code: Secondary Road

Location Details:

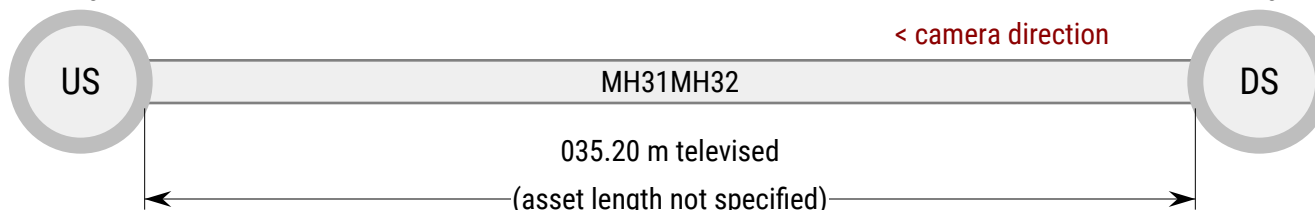
Ratings

	Structural	O & M	Overall
Quick:	0000	0000	0000
$\sum_{i=1}^5 SG_i$ Pipe Rating (OR):	0	0	0
Rating Index (RI):	0	0	0
Consequence of Failure:			

Summary

MH32

MH31



Observations

MH32

Metres	Code		Clock	Value	Grade	Description	Remarks
--------	------	---	-------	-------	-------	-------------	---------

035.20	AMH					Access Point Manhole	Ending MH: MH32. Survey Complete.
--------	-----	--	--	--	--	----------------------	-----------------------------------

024.70	TB	2	100 mm			Tap Break-in/Hammer	
--------	----	---	--------	--	--	---------------------	--

< flow

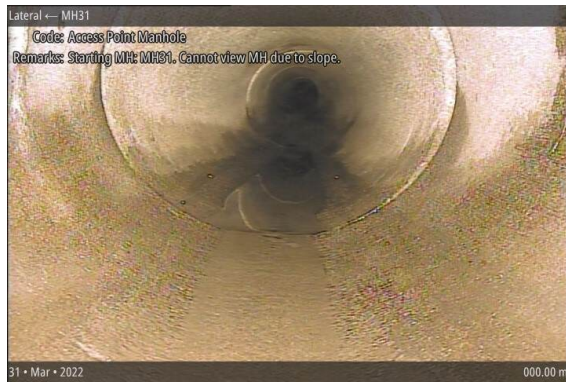
camera direction >

000.00	MWL AMH			5%		Miscellaneous Water Level Access Point Manhole	
--------	------------	--	--	----	--	---	--

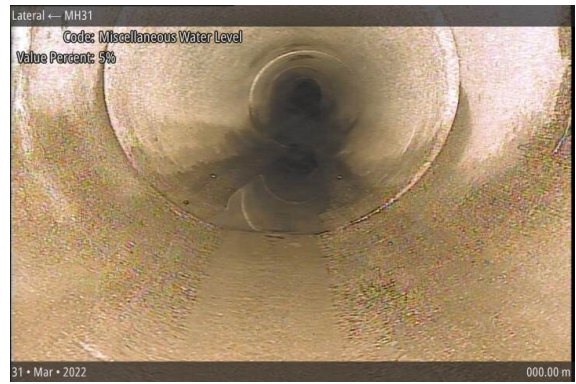
Starting MH: MH31. Cannot view MH due to slope.

MH31

Snapshots



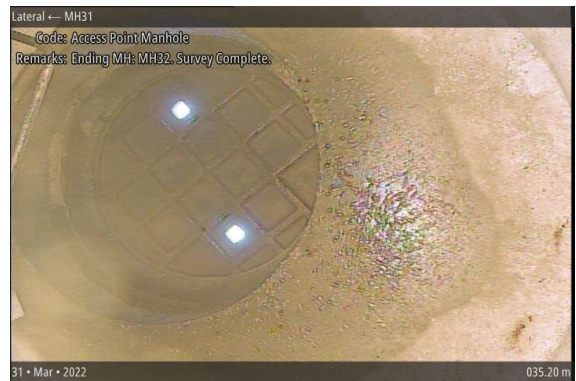
Access Point Manhole at 000.00 m | Starting MH: MH31. Cannot view MH due to slope.



Miscellaneous Water Level at 000.00 m



Tap Break-in/Hammer at 024.70 m, 2 o'clock



Access Point Manhole at 035.20 m | Ending MH: MH32. Survey Complete.

Asset

Owner: City of Mississauga

PSR: MH33MH31MH32

Upstream MH: MH33

Downstream MH: MH31MH32

USMH **DSMH**

Rim to Invert: 1.24 m

Rim to Grade:

Pipe Geometry: 250 mm (Circular)

Material: Concrete Pipe (non-reinforced)

Lining Method:

Coating Method:

Year Constructed:

Pipe Use: Stormwater Pipe

Total Length: (unspecified)

Project

Project: 2022-602

Work Order:

Customer: Lea Consulting Ltd.

PO Number:

Additional Info:

Inspection

Media Date/Time: 31 • Mar • 2022 11:44

Surveyed By: Markus Hirani - I2S inc

Reviewed By:

Camera Direction: Downstream

Purpose: Sewer System Evaluation Survey

Technology:

Pre-Cleaning: No Pre-Cleaning

Date Cleaned:

Flow Control:

Length Surveyed: 015.90 m

Weather: Light Rain

Location

Address: Kirwin Ave, Mississauga

Drainage Area:

Latitude:

Longitude:

Elevation:

GPS Accuracy:

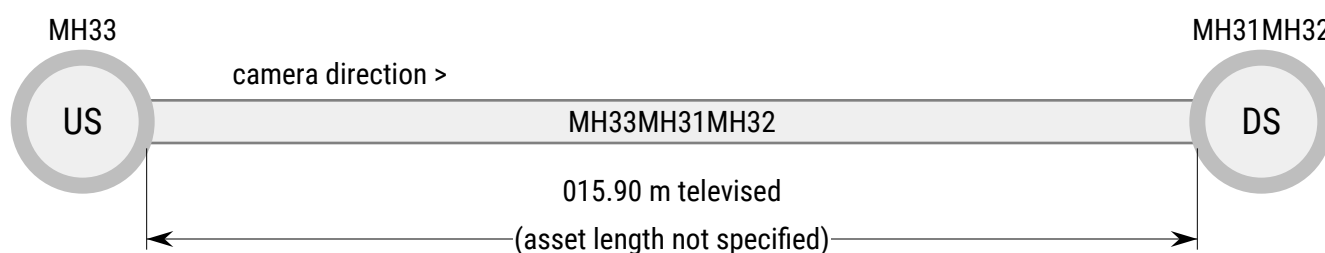
Location Code: Secondary Road

Location Details:

Ratings


	Structural	O & M	Overall
Quick:	0000	0000	0000
$\sum_{i=1}^5 SG_i$ Pipe Rating (OR):	0	0	0
Rating Index (RI):	0	0	0
Consequence of Failure:			

Summary



Observations

MH33

Metres	Code		Clock	Value	Grade	Description	Remarks
000.00	AMH					Access Point Manhole	Starting MH: MH33. Cannot view MH due to slope.
	MWL			10%		Miscellaneous Water Level	

camera direction >

flow >

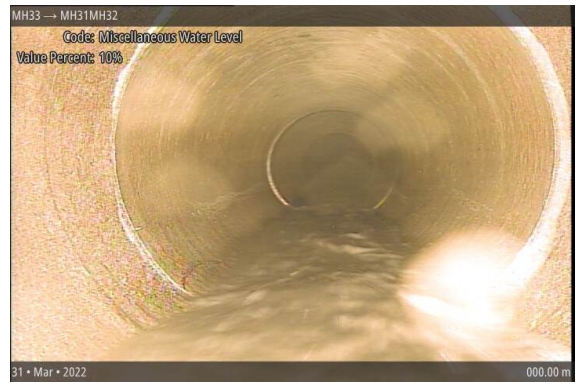
015.90	ADP					Access Point Discharge Point	MH31MH30. Survey Complete.
--------	-----	--	--	--	--	------------------------------	----------------------------

MH31MH32

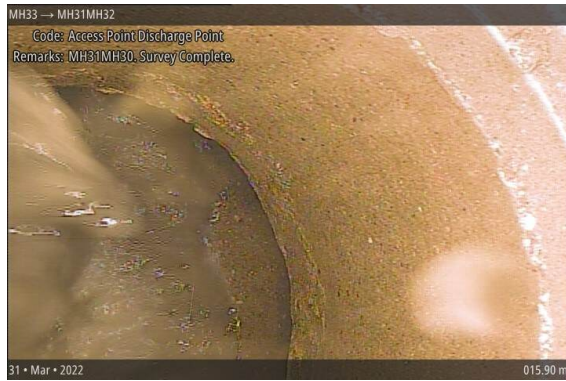
Snapshots



Access Point Manhole at 000.00 m | Starting MH: MH33. Cannot view MH due to slope.



Miscellaneous Water Level at 000.00 m




Access Point Discharge Point at 015.90 m | MH31MH30. Survey Complete.

APPENDIX E

Hydrant Flow Test Data and Watermain Adequacy Assessment Data



 LEA Consulting Ltd. Consulting Engineers and Planners	Residual Pressure			
	Prepared:	P.R.	Page No.	E-01
	Checked:	F.M.		
Project: Proposed Development 3016 Kirwin Ave, Mississauga	Proj. #	21111		
	Date:	25-Oct-23		

Hydrant Test Readings (300mm watermain, 3016 Kirwin Ave)
undertaken on June 15, 2017, by Focus Fire Protection

Flow	Residual Pressure	
0 US GPM	80 psi	
1000 US GPM	76 psi	
1521 US GPM	74 psi	
5274 US GPM	20 psi	Focus Fire Protection Estimate

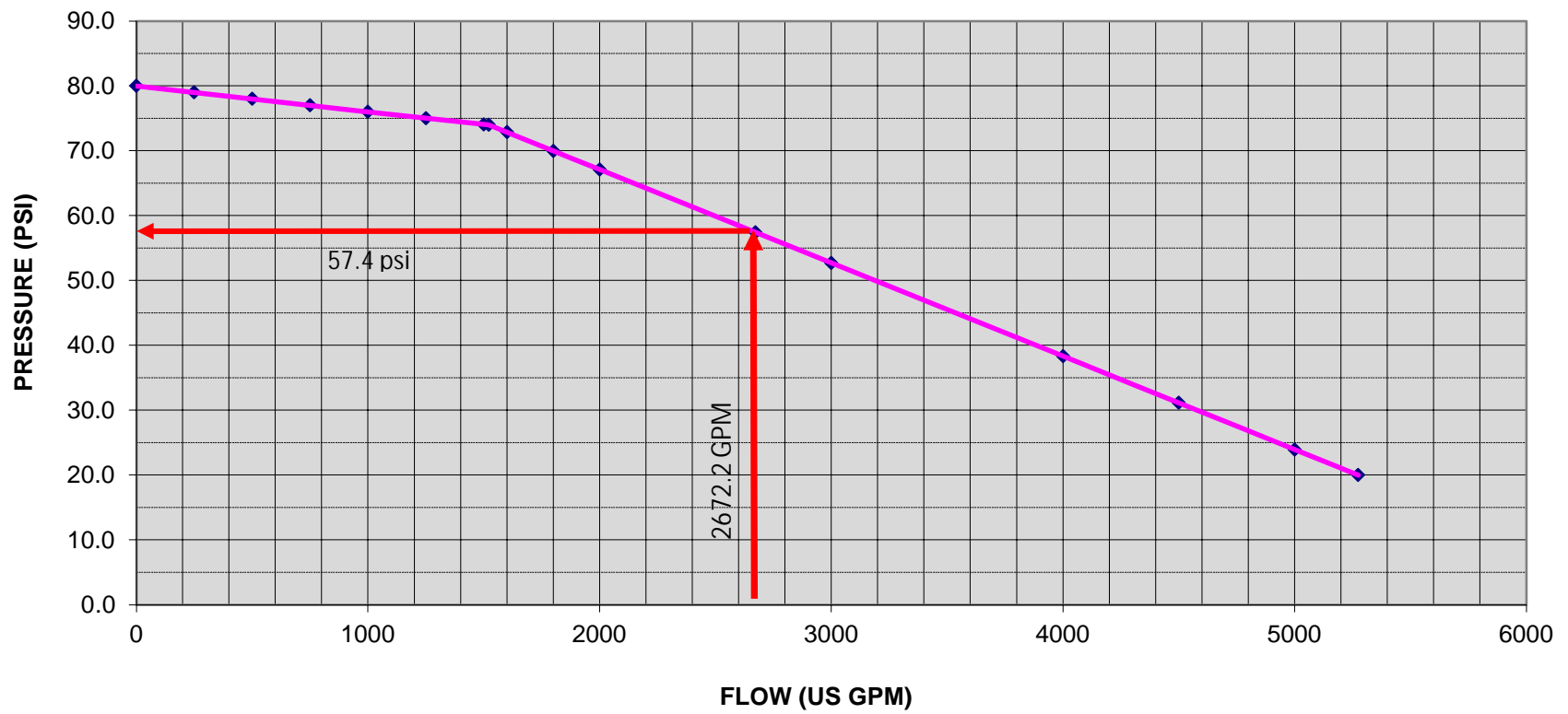
Interpolated

Flow (US GPM)	Residual Pressure (psi)
0	80.0
250	79.0
500	78.0
750	77.0
1000	76.0
1250	75.0
1500	74.1
1521	74.0
1600	72.9
1800	70.0
2000	67.1
2672.2	57.4
3000	52.7
4000	38.3
4500	31.1
5000	23.9
5274	20.0

Existing 300mm Watermain on Kirwin Ave, Mississauga

FLOW TEST CHART (BASED ON FOCUS FIRE PROTECTION TEST, JUN. 15, 2017)

Page: E-02



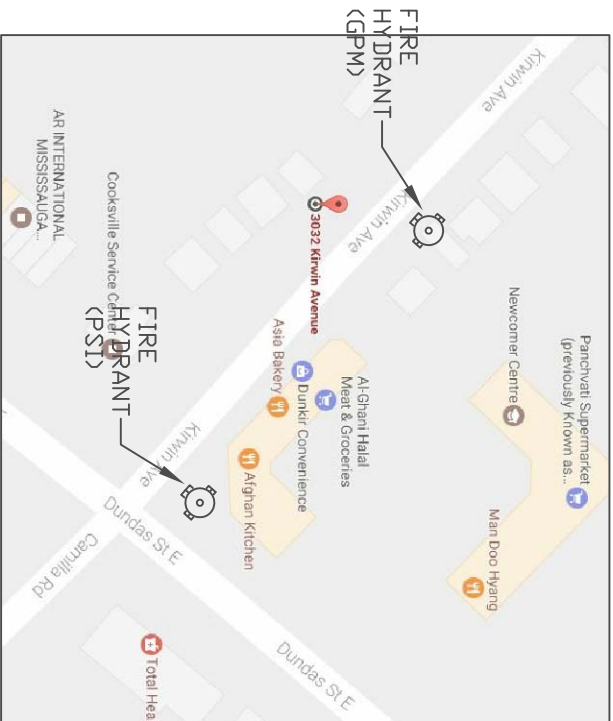
APPENDIX E-02

Hydrant Test

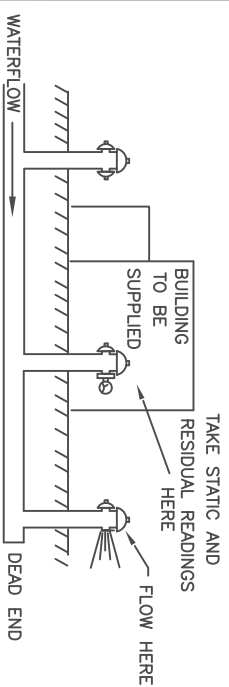
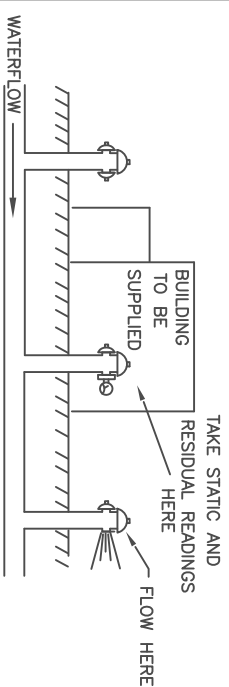
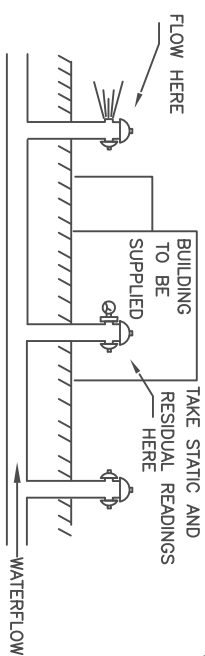
Classic Fire Protection 2017-06-15



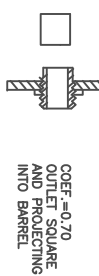
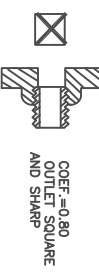
CANADA | INDIA | AFRICA | MIDDLE EAST



TEST:	PLAY PIPE	C=	STATIC(Psi)	RESIDUAL(Psi)	PITOT(Psi)	FLOW(USGPM)
	1x1 1/8					
	2x1 1/8					
	3x1 1/8					
	4x1 1/8					
	1x1 3/4					
	2x1 3/4					
	3x1 3/4					
	4x1 3/4					
HYDRANT BUTT						
1	1x2 1/2	.80	80	76	45	1000
2	2x2 1/2	.80	80	74	26	1521
	3x2 1/2					
	4x2 1/2					
FM NOZZLE						
	1x2 1/4	.88				
	2x2 1/4	.88				
	3x2 1/4	.88				
	4x2 1/4	.88				



OUTLET
TYPE



Client:

Location:

3016-3032 Kirwin Ave

Mississauga, ON



WATER SUPPLY GRAPH

DATE	June 15, 2017	JOB No.	17-0026593
PROPERTY OF			
LOCATION	3016-3032 Kiwin Ave, Mississauga		
BY CFP	NOTES	-	
CLASSIC FIRE PROTECTION INC. (416) 740-3000			



FLOW - U.S. g.p.m.

APPENDIX F

Floodlines Information



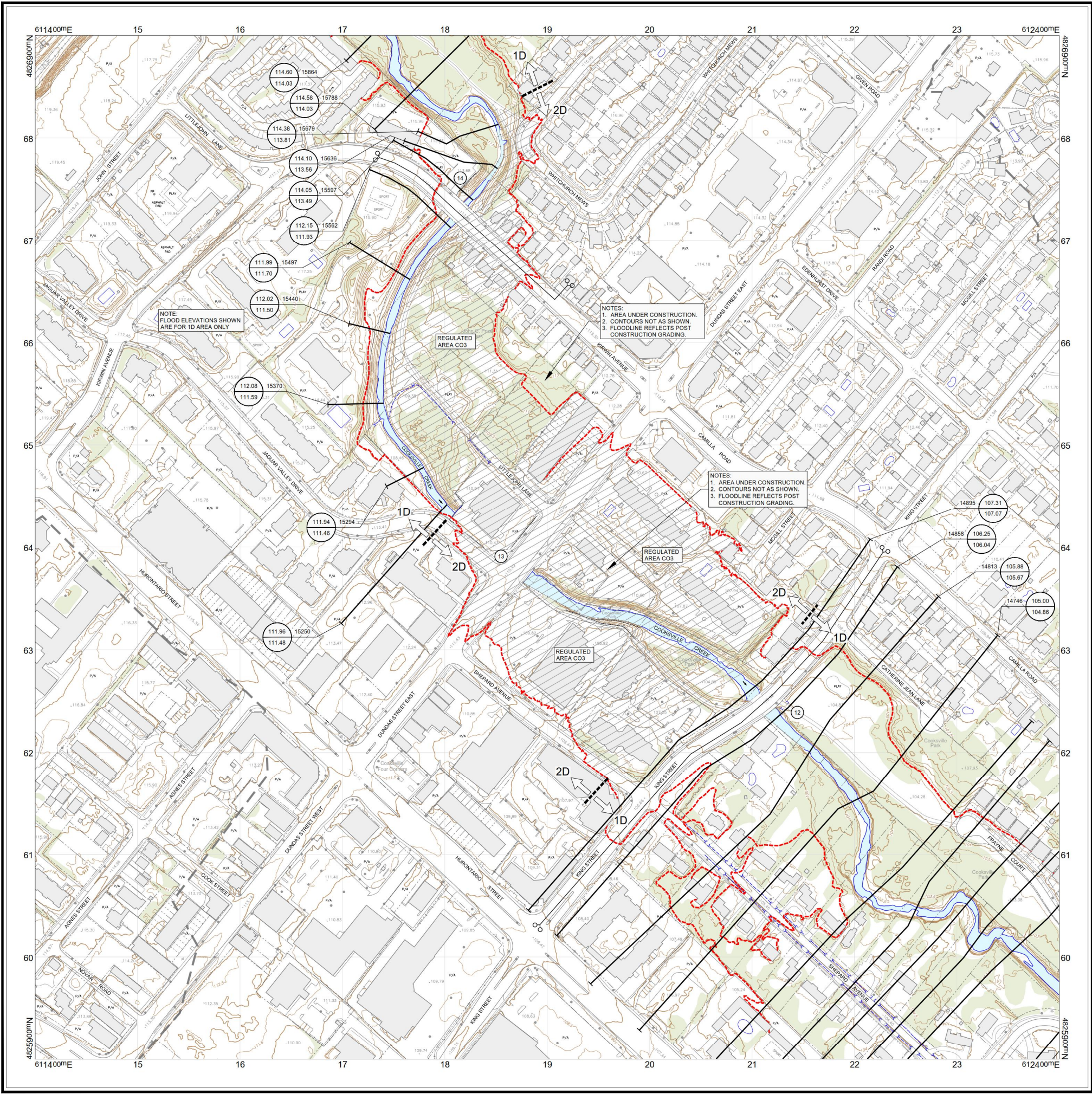
CANADA | INDIA | AFRICA | MIDDLE EAST



COOKSVILLE CREEK - 2D AREA CO3
REGULATED AREAS (2D MODELLING)



FIGURE NO:	CO3-2D
Date:	Sep. 16, 2020
Dwn By:	JGS
SCALE:	AS SHOWN



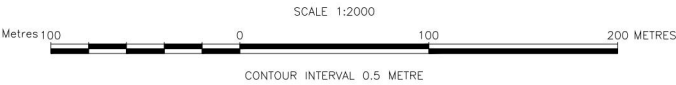
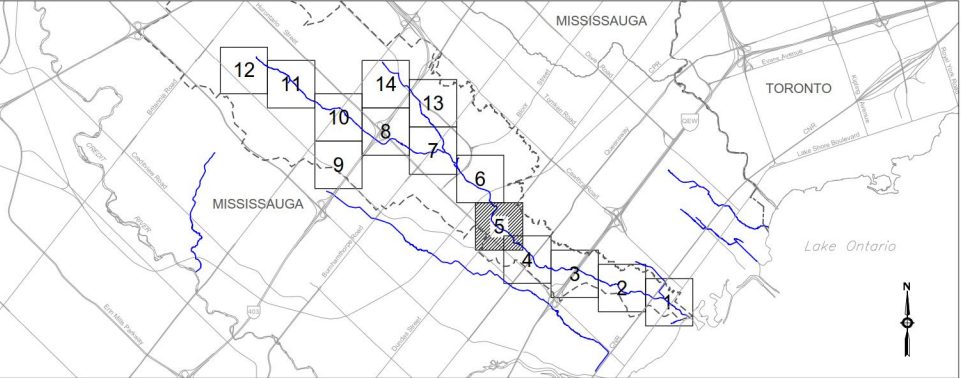
FLOOD HAZARD MAP

COOKSVILLE CREEK WATERSHED

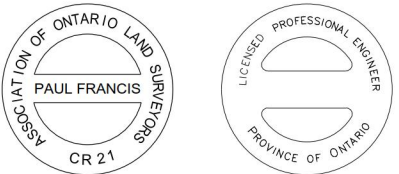
LEGEND

Bridges.....	Marsh.....	Spot Height.....
Building.....	Municipal Boundary.....	Trail.....
Building Ruin.....	Overhead Walkway.....	Wall.....
Building Under Construction.....	Parcel Fabric.....	Watershed Boundary.....
Contour Index.....	Parking Lot.....	Waterbody Elevation.....
Contour Intermediate.....	Pile.....	Wooded Area.....
Culvert Symbol.....	Pipe.....	
Culvert to Scale.....	Pit.....	
Dam.....	Playground.....	
Ditch.....	Pole.....	
Dock, Wharf, Pier.....	Pool.....	
Driveway.....	Railway.....	
Falls, Rapids.....	Railway Abandoned.....	
Fire Hydrant.....	River, Creek, Shoreline.....	
Flow Direction.....	Road.....	
Footbridge.....	Road Shoulder.....	
Guidedail.....	Road Understruction (UC).....	
Headwall.....	Sidewalk.....	
Hedge.....	Silo.....	

SHEET INDEX



- General Notes:
1. Contourlines on this map were generated by Airborne Imaging using the Spring of 2015 LiDAR point cloud, breaklines and hydrologic enforcement at bridges. The vertical accuracy of the original points is 0.10 metres RMSE.
 2. The planimetric data was obtained from the City of Mississauga in 2017.
 3. The vertical datum is mean sea level established by the CGVD 28, 1978 Southern Ontario adjustment.
 4. The horizontal datum is North American Datum 1983 CSRS (Epoch 2010) UTM Zone 17.
 5. To obtain City of Mississauga datum, add 0.121 metres to elevation data.



No	Amendment/Revision	By	Date

\\work\103068\land\dwg\contract\sub4\cvc\1_floodupdate.dwg

5.12 112.47 (111.80)

5.110 112.44 (111.73)

5.089 112.44 (111.74)

5.088 112.44 (111.74)

5.087 112.44 (111.74)

5.086 112.44 (111.74)

5.085 112.42 (111.70)

5.084 112.42 (111.70)

5.083 112.42 (111.70)

5.082 112.40 (111.68)

5.080 112.20 (111.42)
5.053 111.01 (110.70)

LITTLE JOHN LANE

Hotel Gardens

Block A
40 Storeys

Courtyard

Block B
22 Storeys

KIRWIN AVENUE

DUNDAS STREET

NOTE:
MAXIMUM REGIONAL FLOOD ELEVATION = 112.47m
MINIMUM PROPOSED FLOOR ELEVATION = 113.65m
PROPOSED FREEBOARD = 0.77m

LEGEND

- 5.053 HEC-2 CROSS SECTION AND LABEL
- FUT WITH HOTEL
- 111.03 (109.78) REGIONAL FLOOD LEVEL
100 YEAR FLOOD LEVEL
- EXISTING REGIONAL FLOODLINE
- CUT AREA = 365m²
- FILL AREA = 272m²

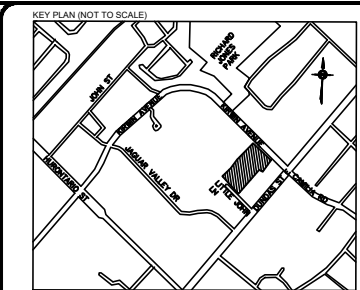
LITTLE JOHN LANE
HYDRAULIC ASSESSMENT
ACTIVE MANAGEMENT LTD.
PROPOSED DEVELOPMENT
FLOODPLAIN

amec

PROJECT No.	103068
DATE	FEBRUARY 2011
SCALE	1:750
DRAWING No.	2

APPENDIX G

Figures and Drawings



- LEGEND**
- ^{RM} EXISTING MANHOLE
 - ^{CB} EXISTING CATCHBASIN
 - ^{WV} EXISTING WV
 - PROPERTY LINE
 - OVERLAND FLOW ROUTE
 - - - DRAINAGE BOUNDARY
 - ^{C1} 0.25 0.388 ha DRAINAGE ID/RUNOFF COEFFICIENT DRAINAGE AREA (ha)
 - EXISTING TREE
 - ▨ EXISTING BUILDING

No.	Revision	Date	By	App.
2	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	P.R.	F.M.
1	ISSUED FOR ZBA SUBMISSION	2021-03-19	M.N.	B.H.

625 Cochrane Drive, Suite 900 Markham, Ontario L3R 9R9, Canada Tel: (905) 470-0015 Fax: (905) 470-0030	
--	--

Owner/Client:

DASS METAL

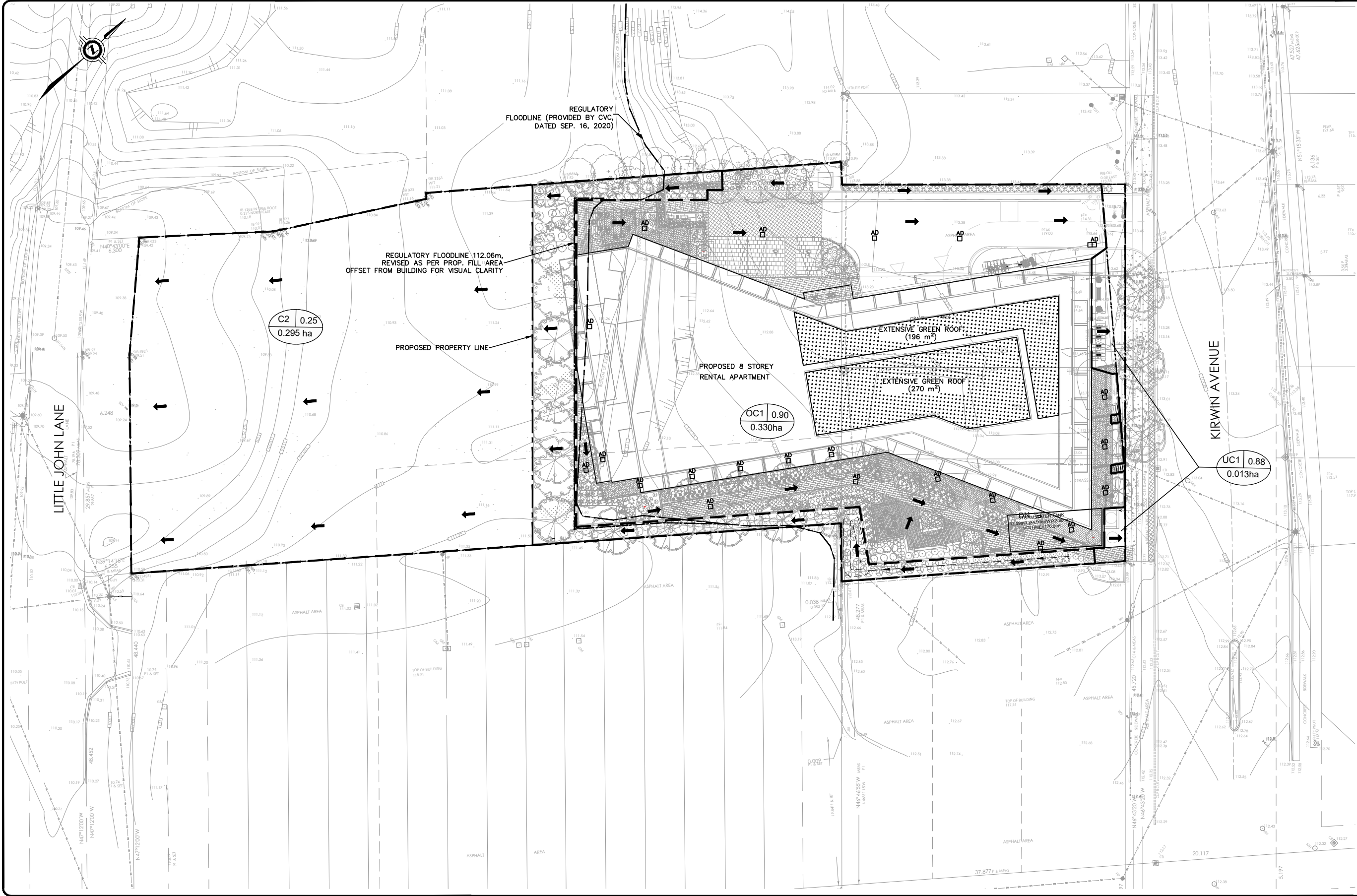
Location:

**3031 LITTLE JOHN & 3016-3032
KIRWIN AVE DEVELOPMENT**

Title:

EXISTING DRAINAGE PLAN

Designed By:	F.M.	Drawn By:	J.W.	Checked By:	F.M.
Scale:	1:500	Date:	FEB., 2021	Drawing No.:	FIG-1
Project No.:	21111				



KEY PLAN (NOT TO SCALE)

LEGEND

- MH EXISTING MANHOLE
- CB EXISTING CATCHBASIN
- WV EXISTING WV
- — — — — PROPERTY LINE
- OVERLAND FLOW ROUTE
- - - - - DRAINAGE BOUNDARY
- C1 0.25
0.388 ha DRAINAGE ID/RUNOFF COEFFICIENT DRAINAGE AREA (ha)
- PROPOSED TREE
- SOFT LANDSCAPE AREA
- UNCONTROLLED AREA
- AD PROPOSED AREA DRAIN
- CB PROPOSED CATCHBASIN
- - - - - PROPOSED SWALE

No.	Revision	Date	By	App.
2	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	F.R.	F.M.
1	ISSUED FOR ZBA SUBMISSION	2021-03-19	M.N.	B.H.

625 Cochrane Drive, Suite 900
Markham, Ontario
L3R 9R9, Canada
Tel: (905)470-0015
Fax: (905)470-0030

Owner/Client:

DASS METAL

Location:

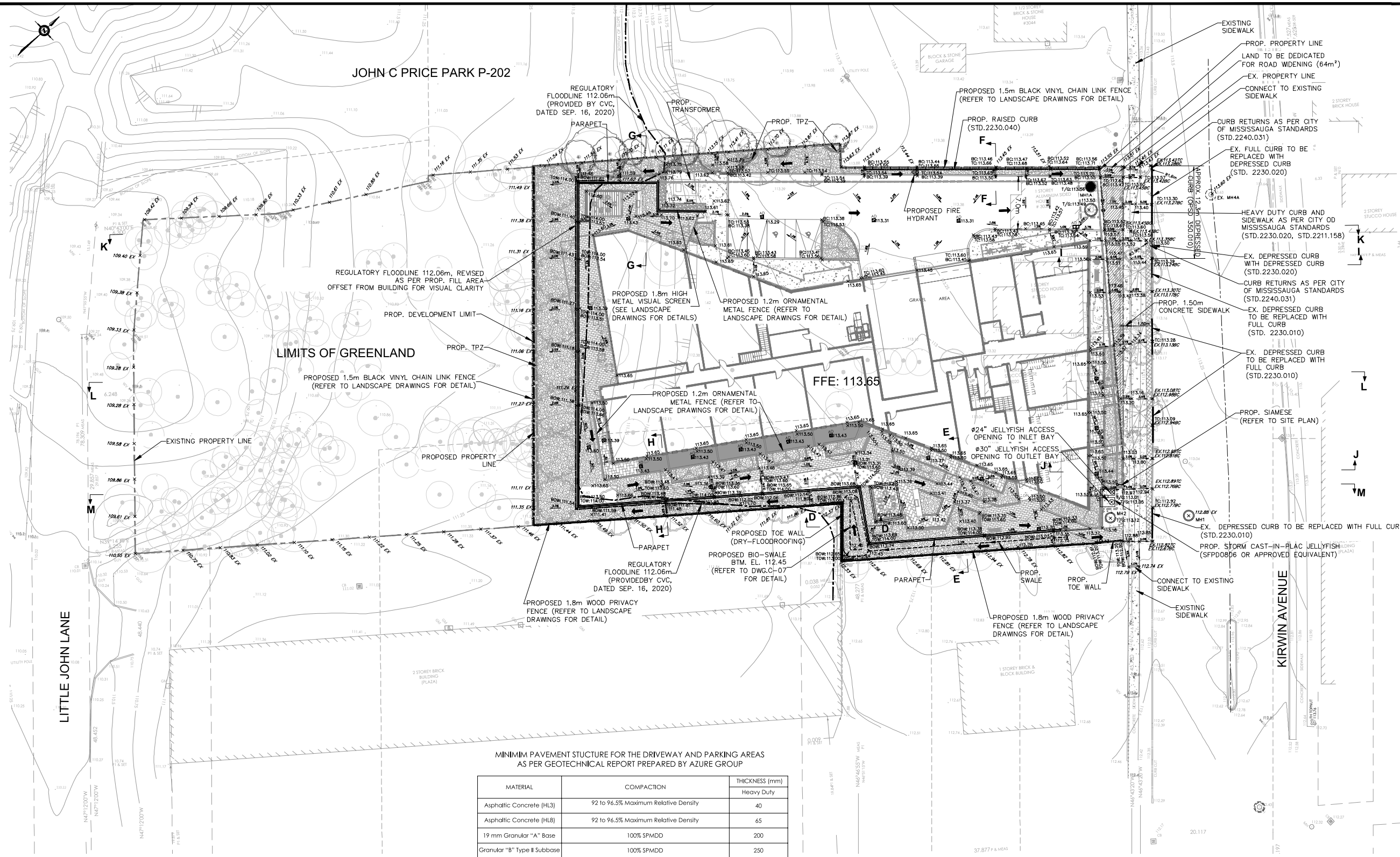
**3031 LITTLE JOHN & 3016-3032
KIRWIN AVE DEVELOPMENT**

Title:

PROPOSED DRAINAGE PLAN

Designed By:	F.M.	Drawn By:	J.W.	Checked By:	F.M.
Scale:	1:500	Date:	FEB., 2021	Drawing No.:	FIG-2
Project No.:	21111				

P:\21111 1108-12-2021\DWG\21111-1108-12-2021\21111-1108-12-2021-FIG-2.dwg



KEY PLAN (NOT TO SCALE)

LEGEND:

- PROPOSED V & B
- PROPOSED DETECTOR CHECK VALVE CHAMBER
- PROPERTY LINE
- EXISTING CATCHBASIN
- EXISTING SANITARY MANHOLE
- EXISTING STORM MANHOLE
- PROPOSED SANITARY MANHOLE
- PROPOSED STORM MANHOLE
- EXISTING FIRE HYDRANT
- EXISTING FIRE HYDRANT
- EXISTING HYDRO POLE
- PROPOSED AREA DRAIN
- PROPOSED CATCHBASIN
- EXISTING GROUND ELEVATION (WHERE THE EXISTING GRADES ARE TO BE MATCHED)
- EXISTING BOTTOM OF CURB ELEVATION
- EXISTING GROUND ELEVATION
- PROPOSED GROUND ELEVATION
- TOP OF CURB ELEVATION
- BOTTOM OF CURB ELEVATION
- TOP OF WALL ELEVATION
- BOTTOM OF WALL ELEVATION
- TOP OF GRADE ELEVATION
- OVERLAND FLOW ROUTE
- UNDERGROUND PARKING WALL
- OUTLINE OF THE BUILDING
- PROPOSED SWALE
- ACOUSTIC WALL
- 1.5m BLACK VINYL CHAIN LINK FENCE
- 1.8m WOOD PRIVACY FENCE
- TREE PROTECTION FENCING
- ARCHITECTURAL CROSS SECTIONS

GENERAL NOTES:

- ELEVATIONS ARE REFERRED TO THE CANADIAN GEODETIC DATUM, 1928 AND WERE DERIVED FROM THE CITY OF MISSISSAUGA BENCHMARK NO. 793 LOCATED ON THE NORTH FACE AT THE EAST CORNER OF CONCRETE END POST OF BOX CULVERT UNDER DUNDAS STREET EAST ON SOUTH SIDE OF DUNDAS STREET EAST, 15M EAST OF JAGUAR VALLEY DRIVE HAVING A PUBLISHED ELEVATION OF 110.955 METERS.
- NO EXTERNAL DRAINAGE OR GRADING PERMITTED INTO PARK BLOCKS
- VEGETATION CLEARING, AND TREE REMOVAL ACTIVITIES SHOULD BE AVOIDED BETWEEN APRIL-OCTOBER OF EACH YEAR TO PROTECT THE BREEDING SEASONS OF MIGRATORY BIRDS AND BATS.
- REFER TO DWG C-108 "STREETSCAPE CROSS SECTIONS" FOR CROSS SECTION H & J-J

No.	Revision	Date	By	App
4	ISSUED FOR 3RD ZBA SUBMISSION	2023-11-07	P.R.	F.M.
3	ISSUED FOR ZBA RE-SUBMISSION	2023-09-15	P.R.	F.M.
2	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	P.R.	F.M.
1	ISSUED FOR ZBA SUBMISSION	2021-03-19	M.N.	B.H.

625 Cochrane Drive, Suite 900
Markham, Ontario
L3R 9R9, Canada
Tel: (905)470-0015
Fax: (905)470-0030

Owner/Client:

DVB REAL ESTATE INVESTMENTS INC.

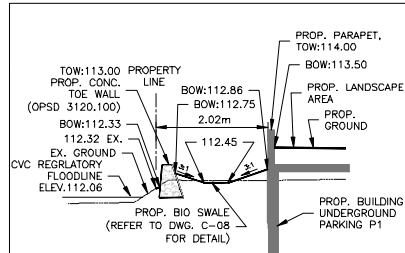
Location:

3031 LITTLE JOHN & 3016-3032 KIRWIN AVE DEVELOPMENT

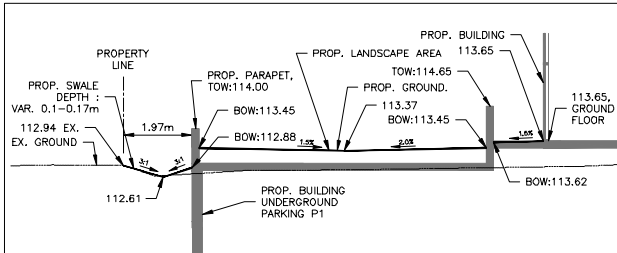
Title:

PRELIMINARY SITE GRADING PLAN

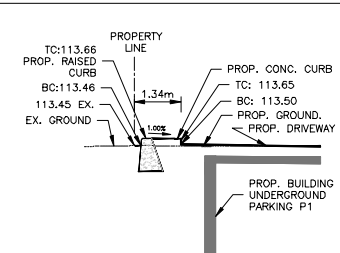
Designed By:	F.M.	Drawn By:	J.W.J.	Checked By:	F.M.
Scale:	1:250	Date:	FEB., 2021	Drawing No.:	C-01
Project No.:	21111				



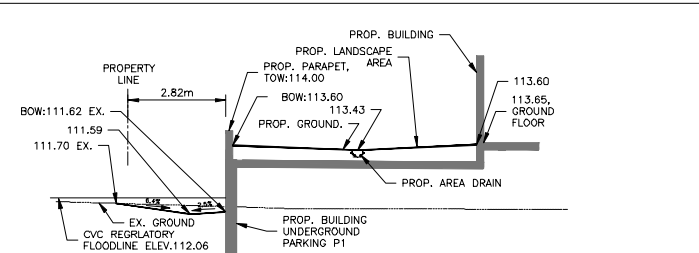
SECTION D-D



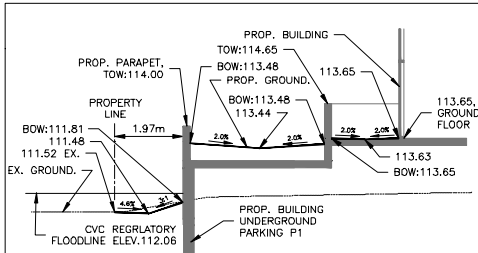
SECTION E-E



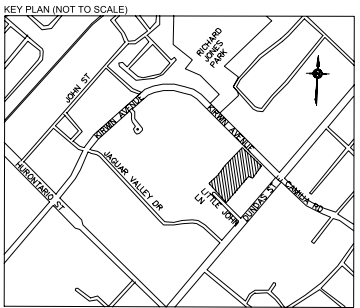
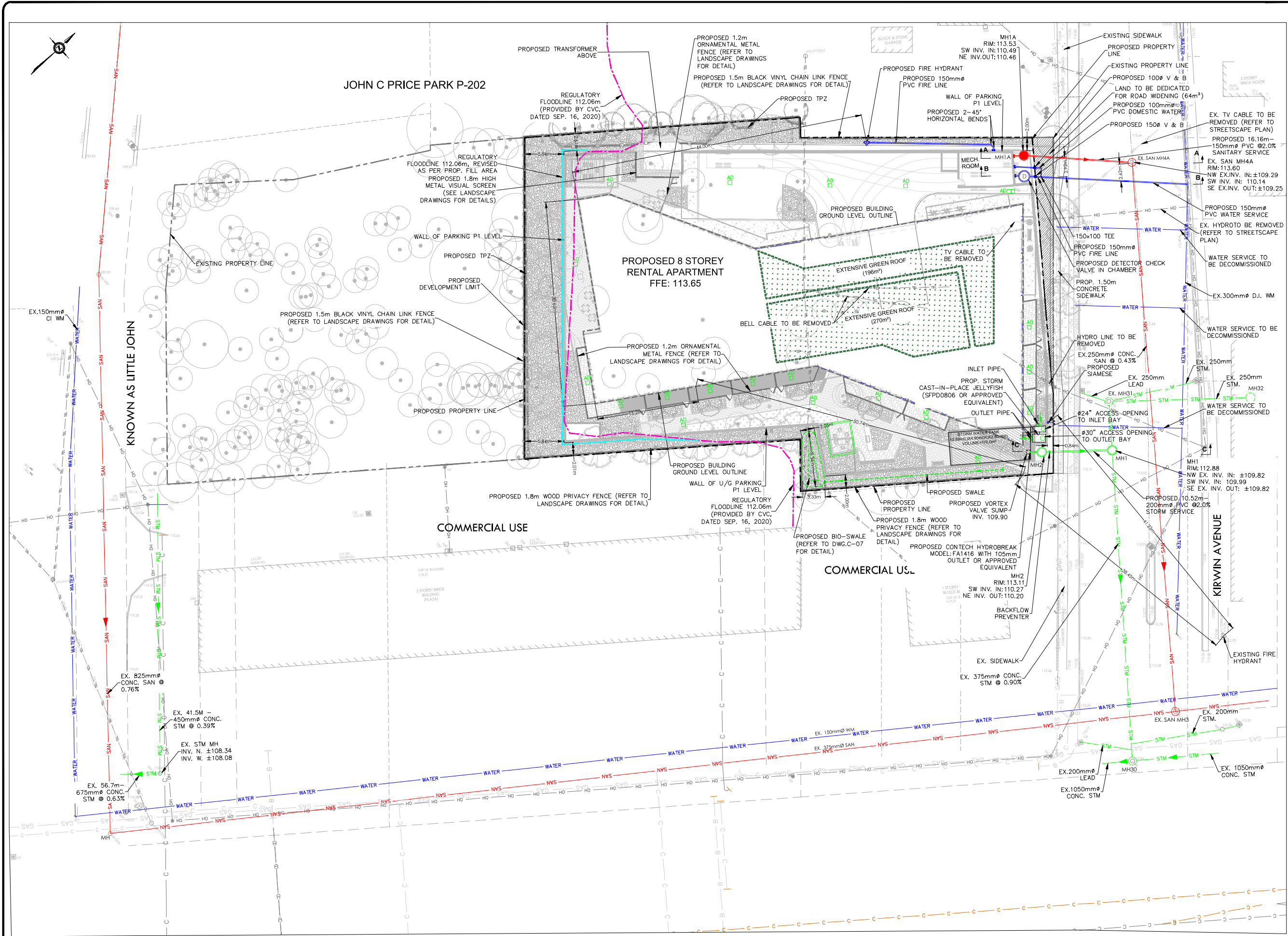
SECTION F-F



SECTION G-G



SECTION H-H



- LEGEND:**
- PROPOSED STORM MANHOLE
 - PROPOSED SANITARY MANHOLE
 - PROPOSED OIL GRIT SEPARATOR
 - PROPOSED V & B
 - PROPOSED DETECTOR CHECK VALVE CHAMBER
 - PROPOSED CATCHBASIN
 - PROPOSED AREA DRAIN
 - PROPERTY LINE
 - BUILDING OUTLINE ABOVE
 - EXISTING CATCHBASIN
 - EXISTING SANITARY MANHOLE
 - EXISTING STORM MANHOLE
 - EXISTING FIRE HYDRANT
 - EXISTING FIRE HYDRANT
 - EXISTING HYDRO POLE
 - EXISTING WATERMAIN
 - EXISTING SANITARY SEWER
 - EXISTING STORM SEWER
 - EXISTING GAS MAIN
 - EXISTING HYDRO
 - EXISTING TEL CABLE
 - EXISTING TV CABLE
 - EXISTING BELL CONDUIT
 - EXISTING BURIED BELL CABLE
 - EXISTING AERIAL ROGERS CABLE
 - 1.5m BLACK VINYL CHAIN LINK FENCE
 - 1.8m WOOD PRIVACY FENCE
 - TREE PROTECTION FENCING

- GENERAL NOTES:**
- ELEVATIONS ARE REFERRED TO THE CANADIAN GEODETIC DATUM, 1928 AND WERE DERIVED FROM THE CITY OF MISSISSAUGA BENCHMARK NO. 793 LOCATED ON THE NORTH FACE AT THE EAST CORNER OF CONCRETE END POST OF BOX CULVERT UNDER DUNDAS STREET EAST ON SOUTH SIDE OF DUNDAS STREET EAST, 15M EAST OF JAGUAR VALLEY DRIVE; HAVING A PUBLISHED ELEVATION OF 110.955 METERS.
 - REFER TO DWG C-108 "SITE SERVICING CROSS SECTIONS" FOR SERVICING CROSS SECTIONS.
 - NO EXTERNAL DRAINAGE OR GRADING IS PERMITTED INTO PARK BLOCKS.
 - ALL AREA DRAINS TO BE CONNECTED TO INTERNAL BUILDING PLUMBING. THE ENTIRE MECHANICAL STORM PIPING BELOW FINISHED FLOOR TO BE JOINT RESTRAINED AND WATERTIGHT.
 - VEGETATION CLEARING, AND TREE REMOVAL ACTIVITIES SHOULD BE AVOIDED BETWEEN APRIL-OCTOBER OF EACH YEAR TO PROTECT THE BREEDING SEASONS OF MIGRATORY BIRDS AND BATS.

No.	Revision	Date	By	App.
4	ISSUED FOR 3RD ZBA SUBMISSION	2023-11-07	F.M.	
3	ISSUED FOR ZBA RE-SUBMISSION	2023-09-15	F.M.	
2	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	F.M.	
1	ISSUED FOR ZBA SUBMISSION	2021-03-19	F.M.	B.H.

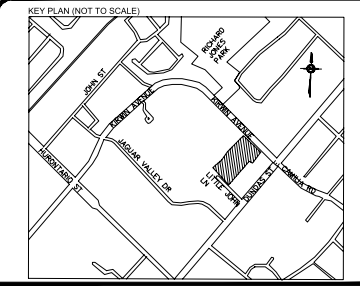
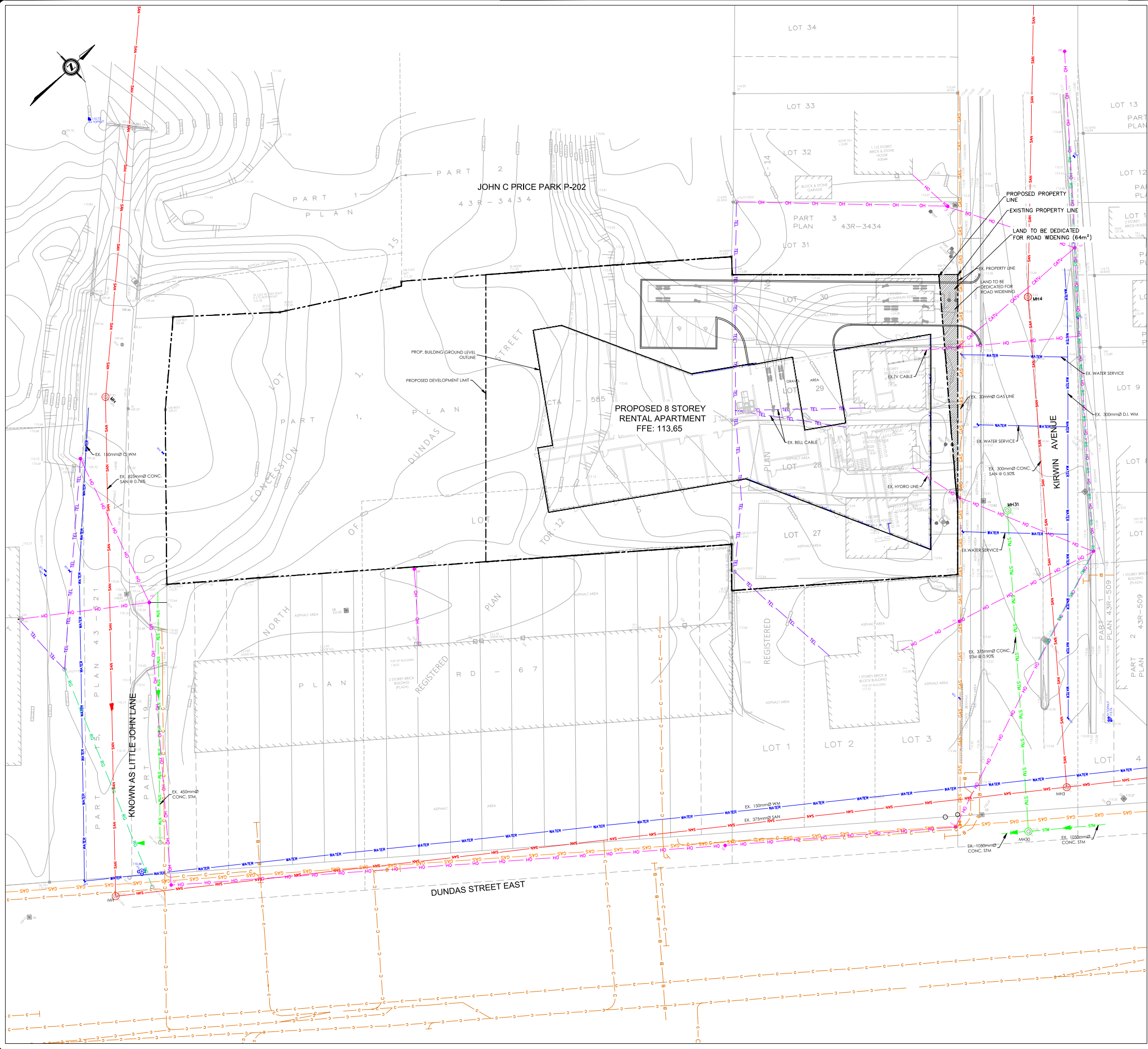
625 Cochrane Drive, Suite 900 Markham, Ontario L3R 9R9, Canada Tel: (905)470-0015 Fax: (905)470-0030	
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Owner/Cliet:
DVB REAL ESTATE INVESTMENTS INC.

Location:
3031 LITTLE JOHN & 3016-3032 KIRWIN AVE DEVELOPMENT

Title:
PRELIMINARY SITE SERVICING PLAN

Designed By: F.M.	Drawn By: J.W.	Checked By: F.M.
Scale: 1/250	Date: FEB., 2021	Drawing No.: C-02
Project No.: 21111		



- LEGEND:**
- PROPOSED STORM MANHOLE
 - PROPOSED SANITARY MANHOLE
 - PROPOSED OIL GREASE SEPARATOR
 - PROPOSED V & B
 - PROPOSED VALVE CHAMBER
 - PROPERTY LINE
 - EXISTING CATCHBASIN
 - EXISTING SANITARY MANHOLE
 - EXISTING STORM MANHOLE
 - EXISTING FIRE HYDRANT
 - EXISTING FIRE HYDRANT
 - EXISTING HYDRO POLE
 - EXISTING WATERMAIN
 - EXISTING SANITARY SEWER
 - EXISTING STORM SEWER
 - EXISTING GAS MAIN
 - EXISTING HYDRO
 - EXISTING BELL CABLE
 - EXISTING TV CABLE
 - EXISTING BELL CONDUIT
 - EXISTING BURIED BELL LABEL
 - EXISTING AERIAL ROGERS CABLE
 - EXISTING TREE

GENERAL NOTES:

- ELEVATIONS ARE REFERRED TO THE CANADIAN GEODETIC DATUM, 1928 AND WERE DERIVED FROM THE CITY OF MISSISSAUGA BENCHMARK NO. 793 LOCATED ON THE NORTH FACE AT THE EAST CORNER OF CONCRETE END POST OF BOX CULVERT UNDER DUNDAS STREET EAST ON SOUTH SIDE OF DUNDAS STREET EAST, 10M EAST OF JAGUAR VALLEY DRIVE HAVING A PUBLISHED ELEVATION OF 110.955 METERS.
- REFER TO DWG C-05 AND C-06 FOR CROSS SECTIONS.
- I HEREBY CERTIFY THAT THE INFORMATION FOR GAS AND WATERMAIN LINES ALONG THE DEVELOPMENT SITE ON KIRWIN AVE. ON THIS PLAN IS COMPLETE, ACCURATE AND BASED ON TEST PILES AS PROVIDED BY T2 UTILITY ENGINEERS, ON OCTOBER 23, 2019.

Engineer's Signature _____

No.	Revision	Date	By	Appr.
4	ISSUED FOR 3RD ZBA SUBMISSION	2023-11-07	P.R.	F.M.
3	ISSUED FOR ZBA RE-SUBMISSION	2023-09-15	P.R.	F.M.
2	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	P.R.	F.M.
1	ISSUED FOR ZBA SUBMISSION	2022-10-19	F.M.	B.H.

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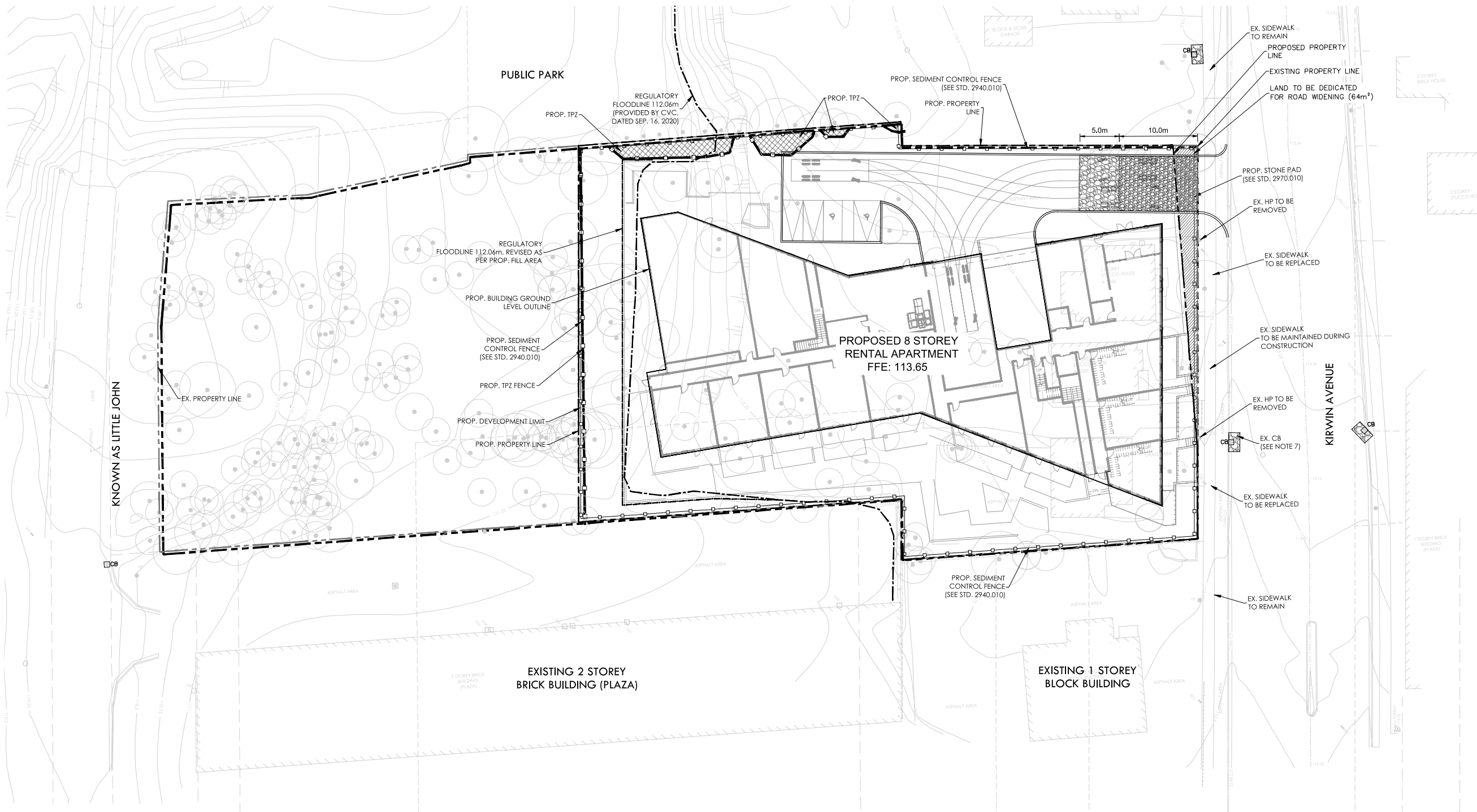


Owner/Client:
DVB REAL ESTATE INVESTMENTS INC.

Location:
**3031 LITTLE JOHN & 3016-3032
KIRWIN AVE DEVELOPMENT**

Title:
COMPOSITE UTILITY PLAN

Designed By: F.M.	Drawn By: L.W.	Checked By: F.M.
Scale: 1:200	Date: FEB., 2021	Drawing No.: C-03
Project No.: 21111		



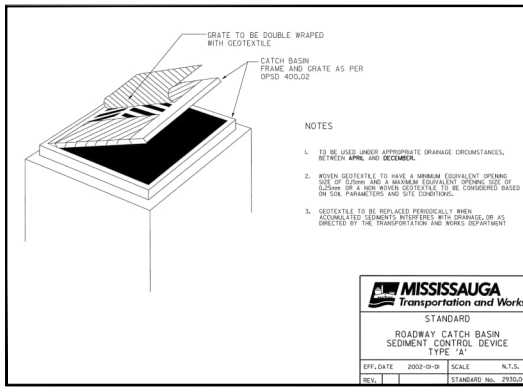
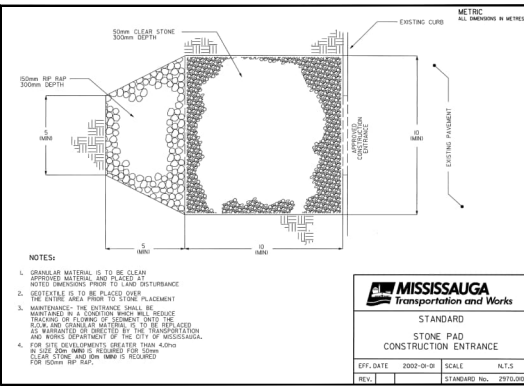
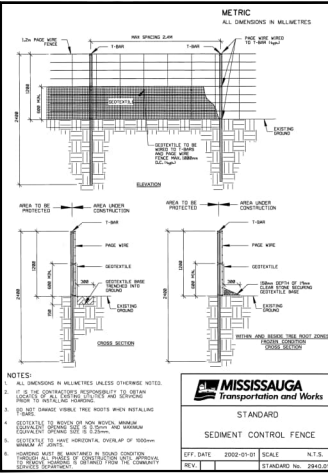
KEY PLAN (NOT TO SCALE)

LEGEND:

- CATCHBASIN TO BE COVERED (SEE NOTE 7)
- STONE PAD
- PROPOSED SEDIMENT CONTROL FENCE
- EXISTING CURB
- PROPOSED PROPERTY LINE
- EXISTING CONTOUR LINE
- EXISTING CATCHBASIN
- EXISTING HYDRO POLE
- EXISTING FIRE HYDRANT
- EXISTING MANHOLE
- EXISTING TREE
- TREE PROTECTION FENCING

- GENERAL NOTES:**
- CONTRACTOR MUST CHECK & VERIFY ALL DIMENSIONS ON THE JOB.
 - DO NOT SCALE DRAWINGS.
 - ALL DRAWINGS, SPECIFICATIONS AND RELATED DOCUMENTS ARE THE COPYRIGHT PROPERTY OF THE ARCHITECT AND MUST BE RETURNED UPON REQUEST. REPRODUCTION OF DRAWINGS, SPECIFICATIONS AND RELATED DOCUMENTS IN PART OR IN WHOLE IS FORBIDDEN WITHOUT THE WRITTEN PERMISSION OF THE ARCHITECT.
 - THIS DRAWING IS NOT TO BE USED FOR CONSTRUCTION UNLESS SIGNED BY THE ARCHITECT.
- TEMPORARY EROSION AND SEDIMENT CONTROL NOTES:**
- ALL SEDIMENT CONTROL DEVICES TO BE INSTALLED PRIOR TO THE BEGINNING OF CONSTRUCTION.
 - SEEDING AND EROSION CONTROL MEASURES WILL BE IMPLEMENTED PRIOR TO AND MAINTAINED DURING CONSTRUCTION TO PREVENT ENTRY OF SEDIMENT INTO PERMANENT STORM DRAINAGE SYSTEMS. CONTRACTOR SHALL PERFORM ROUTINE INSPECTION OF ALL SEDIMENTATION AND EROSION CONTROL MEASURES WEEKLY AND AFTER MAINTENANCE MEETING AND SHALL SUBMIT EROSION AND SEDIMENT CONTROL PLAN TO THE CITY OF MISSISSAUGA.
 - ALL MAINTENANCE TO SEDIMENT AND EROSION CONTROLS TO BE COMPLETED WITHIN 48 HOURS OF INSPECTION.
 - CONTRACTOR SHALL CONSTRUCT & MAINTAIN STONE PAD AT ALL CORNERS AND ENDS.
 - ALL EROSION AND SEDIMENT CONTROLS TO REMAIN IN PLACE UNTIL SEE IS COMPLETELY STABILIZED.
 - THE MINIMUM EROSION AND SEDIMENT CONTROLS ARE SHOWN ON THE PLAN. THE CONTRACTOR IS RESPONSIBLE FOR ADAPTING THE PLAN AS REQUIRED TO COMPLY WITH THE SEDIMENT AND EROSION CONTROL NOTES SHOWN ON THE DRAWING AND AS PER EROSION AND SEDIMENT CONTROL GUIDELINES FOR URBAN CONSTRUCTION BY THE TCA DURING ALL CONSTRUCTION PHASES OF THE PROJECT. THE CONTRACTOR SHALL PROVIDE UPDATED PLANS TO THE CITY PRIOR TO ANY MODIFICATION TO THE PLAN.
 - ALL EXISTING CATCH BASINS SHALL HAVE GEOTEXTILE FILTER CLOTH PLACED ON THEM TO CONTROL ANY SILT THAT MAY ENTER THE STORM SEWER. ALL FILTERS ARE TO BE MAINTAINED BY THE CONTRACTOR, AND TO BE REMOVED UPON COMPLETION OF THE PROJECT.
 - ELEVATIONS ARE REFERRED TO THE CANADIAN GEODETIC DATUM 1928 AND WERE DERIVED FROM THE CITY OF MISSISSAUGA BENCHMARK AND THE LOCATED ON THE NORTH FACE AT THE EAST CORNER OF CONCRETE END POST OF BOX CULVERT UNDER DUNDAS STREET EAST ON SOUTH SIDE OF DUNDAS STREET EAST 1.5M EAST OF JAGUARY VALLEY DRIVE HAVING A FINISHED ELEVATION OF 110.955 METERS.
 - ALL SNOW FENCING AND SEDIMENT CONTROL FENCING TO BE ERECTED AROUND PERIMETER OF DISTURBED AREA PRIOR COMMENCEMENT OF ANY GRADING OPERATIONS (AS PER CITY STD. 2940.011).
 - ALL ROADSIDE CATCHBASINS TO HAVE SEDIMENT PROTECTION AS PER CITY STD. 2930.04 INSTALLED IMMEDIATELY AFTER CURB INSTALLATION. SEDIMENT PROTECTION TO BE MAINTAINED ON A REGULAR BASIS UNTIL NO LONGER REQUIRED.
 - UNDER THE EROSION AND SEDIMENT CONTROL BYLAW NO. 53.01, AS AMENDED IF THE CONSTRUCTION IS INTENSIFIED AND/OR INACTIVITY EXCEEDS 30 DAYS ALL STOPPED AND/OR BARE AREAS WILL BE STABILIZED BY SEEDING.
 - EXISTING SIDEWALKS TO BE MAINTAINED DURING CONSTRUCTION.
 - VEGETATION CLEARING AND TREE REMOVAL ACTIVITIES MUST BE AVOIDED BETWEEN APRIL 1 - OCTOBER OF EACH YEAR TO PROTECT THE BREEDING SEASONS OF MIGRATORY BIRDS AND BATS.
 - EROSION AND SEDIMENT CONTROL METHODS ARE TO BE CONTINUOUSLY EVALUATED AND UPGRADES ARE TO BE IMPLEMENTED, WHEN NECESSARY.
 - ADDITIONAL EROSION AND SEDIMENT CONTROL MATERIALS (IE: SALT FENCE, STRAW BALES, CLEAR STONES ETC) ARE TO BE KEPT ON SITE FOR EMERGENCIES AND REPAIRS.
 - IF THE CONTRACTOR IS ULTIMATELY RESPONSIBLE FOR CONTROLLING SEDIMENT & EROSION WITHIN THE CONSTRUCTION SITE FOR THE DURATION OF THE CONSTRUCTION, THE SEDIMENT LADEN WATER WILL NOT BE ALLOWED TO DISCHARGE TO THE CREEK.
 - IF AN AFTER HOURS CONTACT NUMBER IS TO BE KEPT POSTED ON SITE FOR EMERGENCIES.
 - IF ANY SEDIMENT SPILL FROM THE SITE MUST BE REPORTED TO MINISTRY OF ENVIRONMENT AND CLIMATE CHANGE (CALL SPILL ACTION CENTER AT 1 800 268 6560).

No.	Revision	Date	By	App
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2	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	P.R.	F.M.
1	ISSUED FOR ZBA SUBMISSION	2021-03-19	F.M.	B.H.



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Owner/Client:

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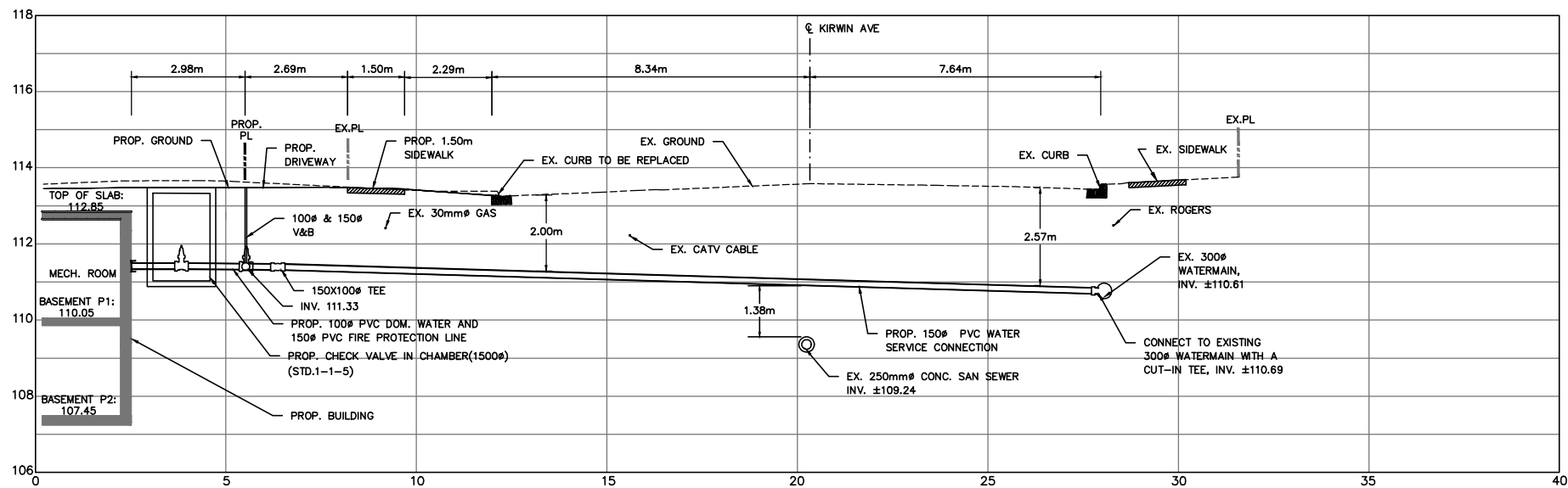
Location:

3031 LITTLE JOHN & 3016-3032 KIRWIN AVE DEVELOPMENT

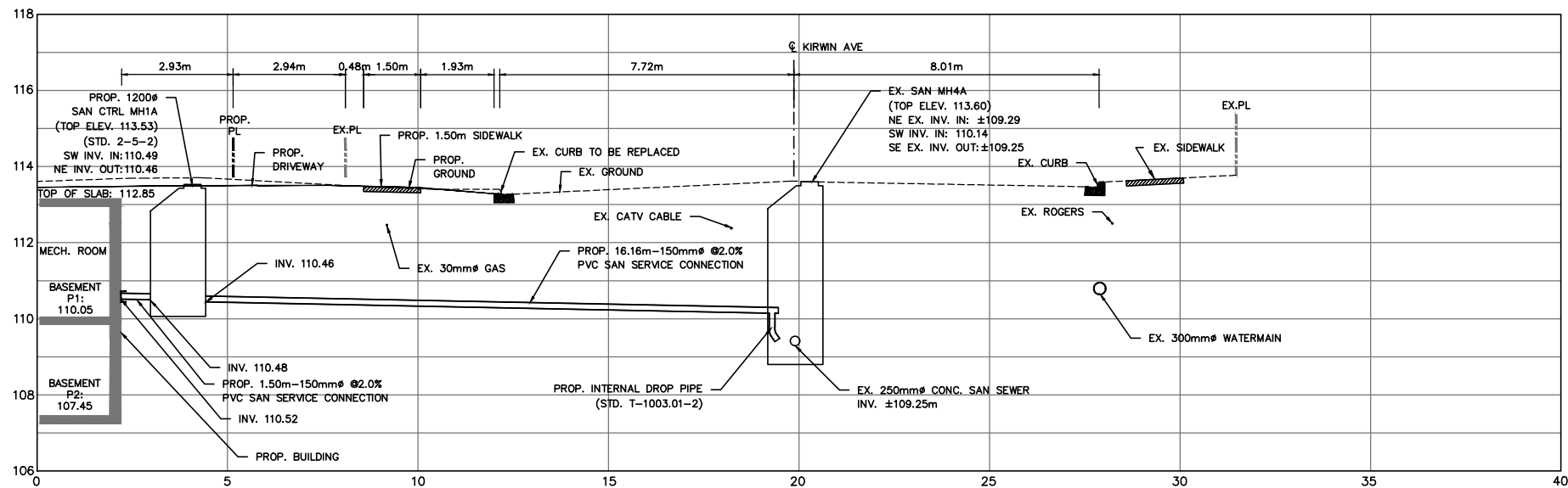
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TEMPORARY EROSION AND SEDIMENT CONTROL PLAN

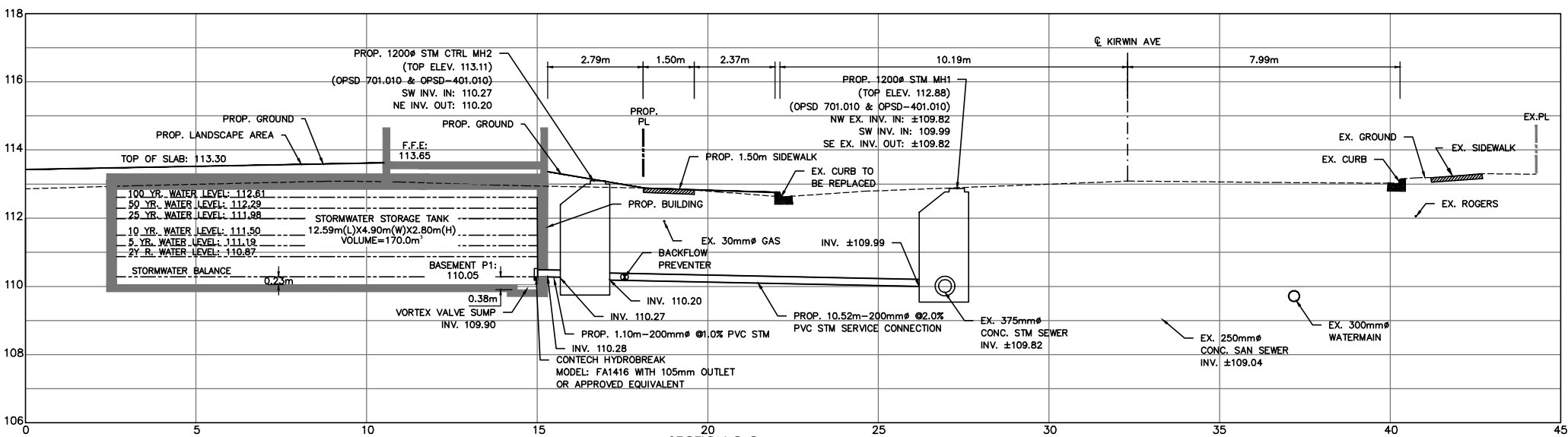
Designed By:	F.M.	Drawn By:	J.W.	Checked By:	F.M.
Scale:	1:250	Date:	FEB., 2021	Drawing No.:	C-04
Project No.:	21111				



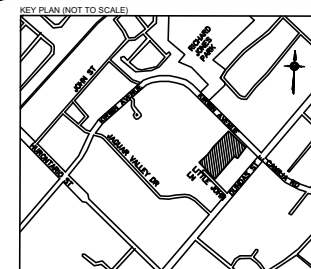
SECTION B-B
WATER SERVICE CONNECTION
SC 1:50



SECTION A-A
SANITARY SERVICE CONNECTION
SC 1:50



SECTION C-C
STORM SERVICE CONNECTION
SC 1:50



GENERAL NOTES:

- ELEVATIONS ARE REFERRED TO THE CANADIAN GEODETIC DATUM, 1928 AND WERE DERIVED FROM THE CITY OF MISSISSAUGA. BENCHMARK NO. 793 LOCATED ON THE NORTH FACE AT THE EAST CORNER OF CONCRETE END POST OF BOX CULVERT UNDER DUNDAS STREET EAST ON SOUTH SIDE OF DUNDAS STREET EAST, 15M EAST OF JAGUAR VALLEY DRIVE, HAVING A PUBLISHED ELEVATION OF 110.955 METERS.
- REFER TO DWG C-02 "SITE SERVICING PLAN" AND C-03 "COMPOSITE UTILITY PLAN" FOR LOCATION OF CROSS SECTIONS

No.	Revision	Date	By	App.
4	ISSUED FOR 3RD ZBA SUBMISSION	2023-11-07	P.R.	F.A.A.
3	ISSUED FOR ZBA RE-SUBMISSION	2023-09-15	P.R.	F.A.A.
2	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	P.R.	F.A.A.
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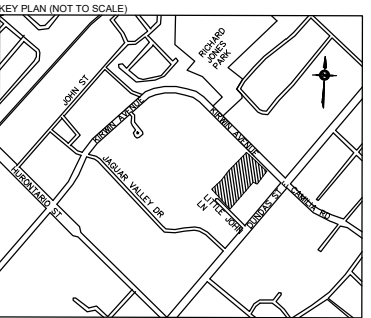
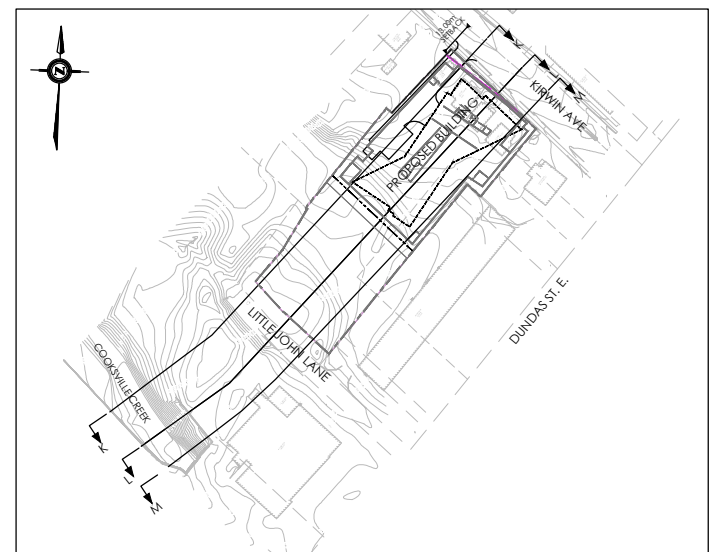
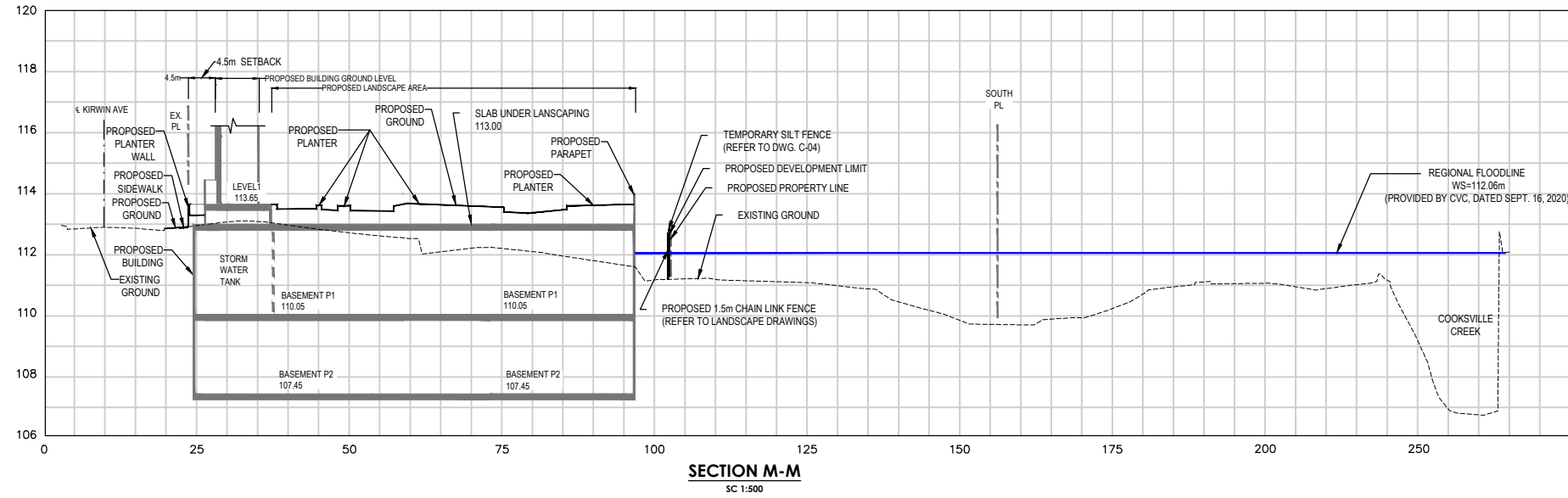
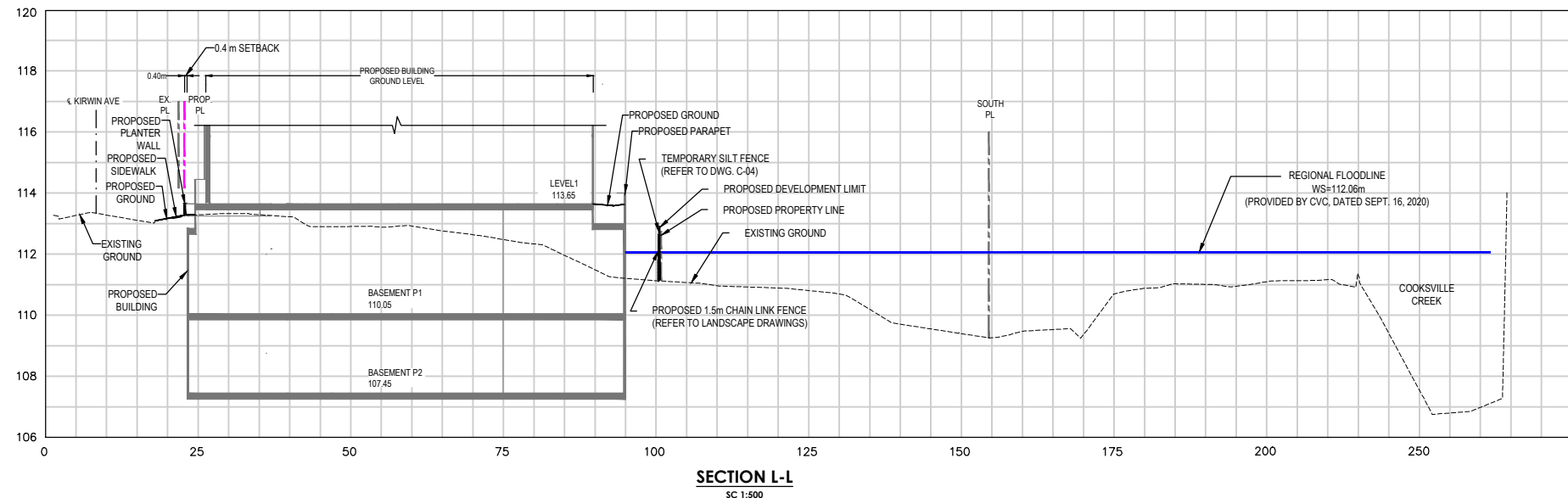
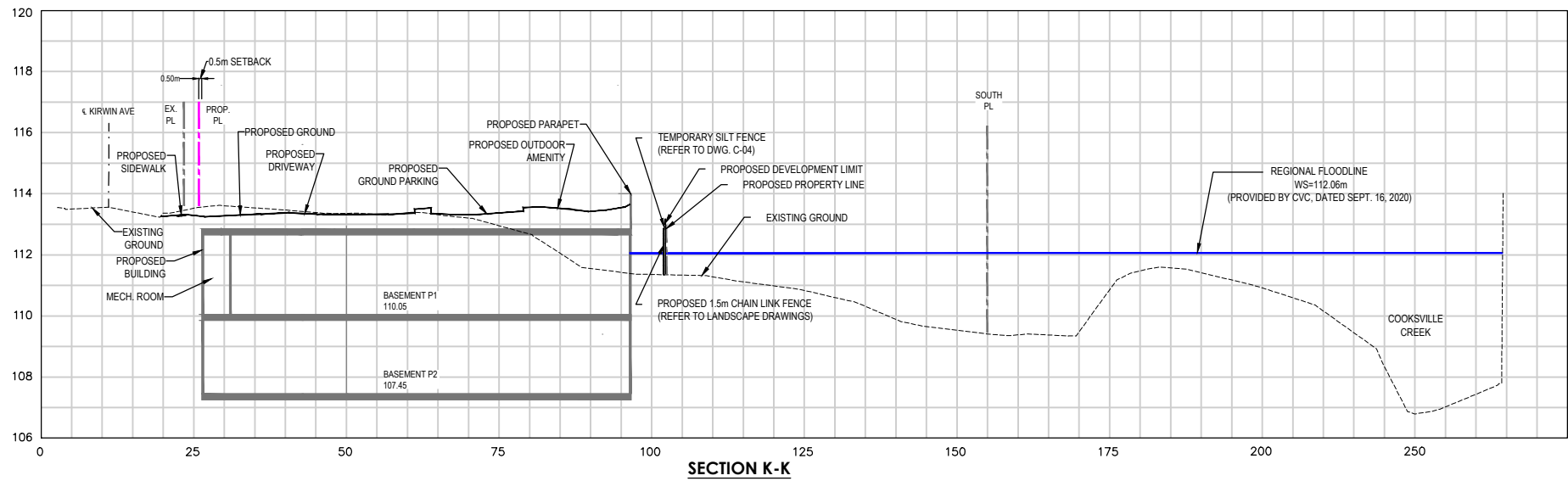
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Owner/Client:
DVB REAL ESTATE INVESTMENTS INC.

Location:
**3031 LITTLE JOHN & 3016-3032
KIRWIN AVE DEVELOPMENT**

Title:
SERVICING CROSS SECTIONS

Designed By: F.A.M.	Drawn By: J.W.	Checked By: F.A.M.
Scale: 1:50	Date: FEB., 2021	Drawing No.: C-05
Project No.: 21111		



LEGEND:

- EX. PROPERTY LINE
- PROP. PROPERTY LINE
- REGIONAL FLOODLINE (PROVIDED BY CVC, DATED SEPT. 16, 2020)
- REGIONAL FLOODLINE (PROVIDES BY AMEC, DATED FEB. 11, 2011)
- EXISTING GROUND
- PROPOSED GROUND

GENERAL NOTES:

- ELEVATIONS ARE REFERRED TO THE CANADIAN GEODETIC DATUM, 1928 AND WERE DERIVED FROM THE CITY OF MISSISSAUGA BENCHMARK NO. 793 LOCATED ON THE NORTH FACE AT THE EAST CORNER OF CONCRETE END POST OF BOX CULVERT UNDER DUNDAS STREET EAST ON SOUTH SIDE OF DUNDAS STREET EAST, 15M EAST OF JAGUAR VALLEY DRIVE; HAVING A PUBLISHED ELEVATION OF 110.955 METERS.
- REFER TO DWG C-01 "SITE GRADING PLAN" FOR LOCATION OF CROSS SECTIONS

No.	Revision	Date	By	App.
4	ISSUED FOR 3RD ZBA SUBMISSION	2023-11-07	P.R.	F.M.
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Fax: (905)470-0030



Owner/Client:

DVB REAL ESTATE INVESTMENTS INC.

Location:

3031 LITTLE JOHN & 3016-3032
KIRWIN AVE DEVELOPMENT

Title:

LONGITUDINAL CROSS SECTIONS

Designed By:	F.M.	Drawn By:	J.W.	Checked By:	F.M.
Scale:	1:500	Date:	FEB., 2021	Drawing No.:	C-06
Project No.:	21111				

GENERAL NOTES

- ALL SITE LAYOUT INFORMATION, INCLUDING BUILDING DIMENSIONS, SETBACKS, CURBS, DEPRESSED CURB LOCATIONS, SIDEWALKS, PARKING AND LANDSCAPE FEATURES MUST BE REFERENCED FROM THE ARCHITECT'S PLANS.
- PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR MUST VERIFY ALL DIMENSIONS AND LAYOUT INFORMATION. ANY DISCREPANCIES MUST BE REPORTED TO THE CONSULTANT BEFORE RESUMING CONSTRUCTION OPERATIONS.
- ALL SERVICES MUST BE INSTALLED TO THE CURRENT CITY OF MISSISSAUGA STANDARDS, REGION OF PEEL STANDARDS, ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD), ONTARIO PROVINCIAL STANDARD SPECIFICATION (OPSS), AND ONTARIO BUILDING CODE (OBC) UNLESS OTHERWISE SPECIFIED, TO THE SPECIFICATION OF THE CITY AND CONSULTANT.
- THE REGION OF PEEL AND CITY OF MISSISSAUGA STANDARD DRAWINGS, MATERIAL SPECIFICATIONS AND CONSTRUCTION SPECIFICATIONS, ONTARIO PROVINCIAL STANDARD DRAWINGS (OPSD) AND ONTARIO PROVINCIAL STANDARD SPECIFICATION (OPSS) SHALL FORM PART OF THE CONTRACT DOCUMENTS.
- THE POSITION OF EXISTING POLE LINES, CONDUITS, WATERMAINS, SEWERS AND OTHER UNDERGROUND AND ABOVEGROUND UTILITIES, STRUCTURES AND APPURTENANCES IS NOT NECESSARILY SHOWN ON THE DRAWING, AND WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. PRIOR TO CONSTRUCTION, THE CONTRACTOR SHALL SATISFY HIMSELF OF THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES, AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO THEM DURING THE COURSE OF CONSTRUCTION. THIS MAY REQUIRE EXCAVATION TO EXPOSE UTILITIES AS REQUIRED BY CONTRACTORS.
- ALL TRENCHING TO BE IN ACCORDANCE WITH THE LATEST REVISIONS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS.
- ALL TRENCHES SHALL BE BACKFILLED TO THE CITY'S OF STANDARDS AND IN ACCORDANCE WITH THE GEOTECHNICAL REPORT OR AS OTHERWISE NOTED ON THE DRAWINGS.
- ALL DIMENSIONS ARE IN METRES(m) AND ALL DIAMETERS ARE IN MILLIMETERS (mm) UNLESS OTHERWISE NOTED.
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TRAFFIC CONTROL AND SAFETY MEASURES DURING THE CONSTRUCTION PERIOD, INCLUDING THE SUPPLY, INSTALLATION AND REMOVAL OF ALL NECESSARY SIGNAGE, DELINEATORS, MARKERS AND BARRIERS. ALL SIGNS, ETC. SHALL CONFORM TO THE STANDARDS AND SPECIFICATIONS FOR THE CITY AND ONTARIO TRAFFIC MANUAL FOR TEMPORARY CONDITIONS AND MTO MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES.
- THE CONTRACTOR SHALL RECTIFY ALL DISTURBED AREAS TO THE ORIGINAL CONDITION OR BETTER AND TO THE SATISFACTION OF THE CITY.
- EXISTING STRUCTURES ARE NOT TO BE DISTURBED, NOR ENCROACHMENT ON ADJACENT PROPERTIES UNLESS INSTRUCTED BY THE ENGINEER.
- DEWATERING, IF REQUIRED, SHALL BE THE RESPONSIBILITY AND SOLE EXPENSE OF THE CONTRACTOR. REFER TO THE GEOTECHNICAL REPORT FOR EXISTING SITE CONDITIONS.
- CONTRACTOR TO EXPOSE AND VERIFY LOCATION, ELEVATION, AND SIZE OF ALL SERVICE CONNECTIONS PRIOR TO CONSTRUCTION. THE OWNER SHALL BE NOTIFIED IMMEDIATELY OF ANY CONFLICTS WITH EXISTING SERVICES
- CONTRACTOR SHALL RED-LINE ALL AS CONSTRUCTED INFORMATION ON A SET OF DRAWINGS AND PROVIDE TO THE OWNER AT THE END OF CONSTRUCTION, SEALED BY AN OLS OR P.ENG.
- CONTRACTOR SHALL SUPPORT AND PROTECT ALL EXISTING UTILITIES DURING CONSTRUCTION AS PER OPSD AND CITY OF MISSISSAUGA STANDARDS AND SPECIFICATIONS.
- THE APPROVAL OF THIS PLAN DOES NOT EXEMPT THE OWNERS CONTRACTOR FROM OBTAINING AND PAYING FOR, BUT NOT LIMITED TO THE FOLLOWING PERMITS, ROAD CUTS, SEWER PERMITS, RELOCATION OF SERVICES, ENCROACHMENT AGREEMENTS, APPROACH APPROVAL PERMITS, ETC. ALL RESTORATION AS PER CITY STANDARDS.
- THE CONTRACTOR SHALL ENDEAVOR TO PREVENT MUD TRACKING ONTO EXISTING RIGHT-OF-WAYS AND SHALL PROVIDE FOR CLEANUP AT HIS OWN EXPENSE AS DIRECTED BY THE CITY. THE CONTRACTOR SHALL ALSO BE RESPONSIBLE TO CONTROL DUST ON THE PROJECT AND HE SHALL PROVIDE AT HIS OWN EXPENSE, CONTROLLING MEASURES AS DIRECTED BY THE CITY.
- FOR ELECTRICAL, ARCHITECTURAL AND MECHANICAL DETAILS BY OTHERS, SEE RESPECTIVE DRAWINGS. WORKS SHOWN ON THESE DRAWINGS ARE TO BE READ IN CONJUNCTION WITH ALL OTHER PLANS.
- ALL EXISTING SERVICES ARE TO REMAIN IN SERVICE AT ALL TIMES DURING CONSTRUCTION.
- ITEMS DESIGNATED TO BE REMOVED SHALL BE DISPOSED OFF-SITE.
- CONSTRUCTION LAYOUT SHALL BE UNDERTAKEN BY CONTRACTOR'S SURVEYOR AT THE CONTRACTOR'S EXPENSE.
- CONTRACTOR SHALL REVIEW THE GEOTECHNICAL REPORT FOR THE SITE TO CONFIRM EXISTING SOIL CONDITIONS AND TO CONFIRM RECOMMENDED GEOTECHNICAL PROCEDURES FOR THE ADDITION.

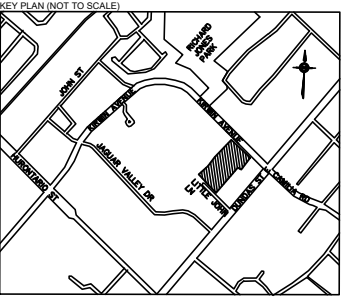
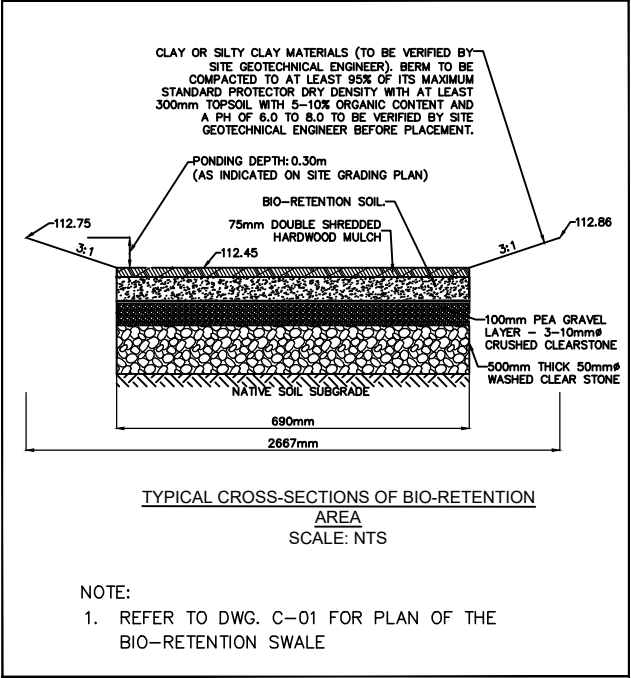
REGION OF PEEL STANDARD NOTES

- ALL MATERIALS AND CONSTRUCTION METHODS MUST CORRESPOND TO THE CURRENT PEEL PUBLIC WORKS STANDARDS AND SPECIFICATIONS.
- WATERMAIN AND/OR WATER SERVICES MATERIALS 100MM (4") AND LARGER MUST BE DR18 P.V.C. PIPE MANUFACTURED TO A.W.W.A. SPEC. C900-16 SPEC COMPLETE WITH TRACER WIRE. SIZE 50MM (2") AND SMALLER MUST BE TYPE 'K' SOFT COPPER PIPE PER A.S.T.M. B88-49 SPECIFICATION.
- WATERMAINS AND/OR WATER SERVICES ARE TO HAVE A MINIMUM COVER OF 1.7M (5'6") WITH A MINIMUM HORIZONTAL SPACING OF 1.2M (4') FROM THEMSELVES AND ALL OTHER UTILITIES.
- PROVISIONS FOR FLUSHING WATER LINE PRIOR TO TESTING, ETC. MUST BE PROVIDED WITH AT LEAST A 50MM (2") OUTLET ON 100MM (4") AND LARGER LINES. COPPER LINES ARE TO HAVE FLUSHING POINTS AT THE END, THE SAME SIZE AS THE LINE. THEY MUST ALSO BE HOSED OR PIPED TO ALLOW THE WATER TO DRAIN ONTO A PARKING LOT OR DOWN A DRAIN. ON FIRE LINES FLUSHING OUTLET TO BE 100MM (4") DIAMETER MINIMUM ON A HYDRANT.
- ALL CURB STOPS TO BE 3.0M OFF THE FACE OFF THE BUILDING UNLESS OTHERWISE NOTED.
- HYDRANT AND VALVE SET TO REGION STANDARDS 1-6-1 DIMENSION A AND B, 0.7M (2') AND 0.9M (3') AND TO HAVE PUMPER NOZZLE.
- WATERMAINS TO BE INSTALLED TO GRADES AS SHOWN ON APPROVED SITE PLAN. COPY OF GRADE SHEET MUST BE SUPPLIED TO INSPECTOR PRIOR TO COMMENCEMENT OF WORK, WHERE REQUESTED BY INSPECTOR.
- WATERMAINS MUST HAVE MINIMUM VERTICAL CLEARANCE OF 0.3M (12") OVER/0.5M (20") UNDER SEWERS AND ALL OTHER UTILITIES WHEN CROSSING.
- ALL PROPOSED WATER PIPING MUST BE ISOLATED FROM EXISTING LINES IN ORDER TO ALLOW INDEPENDENT PRESSURE TESTING AND CHLORINATING FROM EXISTING SYSTEMS.
- ALL LIVE TAPPING AND OPERATION OF REGION WATER VALVES SHALL BE ARRANGED THROUGH THE REGIONAL INSPECTOR ASSIGNED OR BY CONTACTING THE OPERATIONS AND MAINTENANCE DIVISION.
- LOCATION OF ALL EXISTING UTILITIES IN THE FIELD TO BE ESTABLISHED BY THE CONTRACTOR.
- THE CONTRACTOR(S) SHALL BE SOLELY RESPONSIBLE FOR LOCATES, EXPOSING, SUPPORTING AND PROTECTING OF ALL UNDERGROUND AND OVERHEAD UTILITIES AND STRUCTURES EXISTING AT THE TIME OF CONSTRUCTION IN THE AREA OF THEIR WORK WHETHER SHOWN ON THE PLANS OR NOT AND FOR ALL REPAIRS AND CONSEQUENCES RESULTING FROM DAMAGE TO SAME.
- THE CONTRACTORS(S) SHALL BE SOLELY RESPONSIBLE TO GIVE 72 HOURS WRITTEN NOTICE TO UTILITIES PRIOR TO CROSSING SUCH UTILITIES, FOR THE PURPOSE OF INSPECTION BY THE CONCERNED UTILITY. THIS INSPECTION WILL BE FOR THE DURATION OF THE CONSTRUCTION, WITH THE CONTRACTOR RESPONSIBLE FOR ALL COSTS ARISING FROM SUCH INSPECTIONS.
- ALL PROPOSED WATER PIPING MUST BE ISOLATED THROUGH A TEMPORARY CONNECTION THAT SHALL INCLUDE AN APPROPRIATE CROSS-CONNECTION CONTROL DEVICE, CONSISTENT WITH THE DEGREE OF HAZARD, FOR BACKFLOW PREVENTION OF THE ACTIVE DISTRIBUTION SYSTEM, CONFORMING TO REGION OF PEEL STANDARDS 1-7-7 OR 1-7-8.

SANITARY, STORM AND WATERMAIN NOTES

- FULL LENGTH PERFORATED SUB-DRAIN PIPES OF 150mm DIA. TO BE INSTALLED AROUND THE PERIMETER OF PARKING LOT.
- ALL UTILITY COMPANIES WILL BE NOTIFIED BY CONTRACTOR FOR LOCATES PRIOR TO THE INSTALLATION OF PROPOSED SERVICE CONNECTIONS.
- ALL PIPE MATERIALS SHALL BE IN ACCORDANCE WITH THE CURRENT MANUFACTURERS APPROVED PRODUCT LIST, SANITARY SEWER AND APPURTENANCES.
- ALL SANITARY MAINTENANCE HOLES SHALL CONFORM TO THE CURRENT MANUFACTURER'S APPROVED PRODUCT LIST, SANITARY SEWER AND APPURTENANCES, REGIONAL STANDARD DRAWING 2-1-1 WHICH MUST BE MODIFIED IN THE FIELD TO PREVENT INFLOW AND INFILTRATION.
- SANITARY SERVICE CONNECTION MATERIAL MUST BE PVC SDR28.
- STORM SERVICE CONNECTION MATERIAL MUST BE PVC DR35.
- ALL MAINTENANCE HOLE ARE TO BE SUPPLIED OR CONSTRUCTED IN ACCORDANCE WITH OPSD 701 SERIES.
- CATCH BASINS SHALL BE PRECAST AS PER OPSD 705 SERIES.
- SANITARY SEWERS SHALL BE INSTALLED WITH BEDDING AS PER REGIONAL STANDARD DRAWING 2-3-1.
- BEDDING FOR PVC STORM SEWER PIPE SHALL BE IN ACCORDANCE WITH CITY OF MISSISSAUGA STANDARD DRAWING NO. 2112.080.
- SEWER BEDDING SHALL CONFORM WITH OPSS 1010 FOR GRANULAR "A" OR CITY STANDARD DRAWING NO. 2112.100 OR 2112.140.

- ALL GRANULAR BEDDING AND BACKFILL MATERIAL SHALL CONFORM TO THE REQUIREMENTS OF OPSS 1010 AND MUST NOT CONTAIN RCM/RAP.
- ALL VALVE 300MM DIAMETER AND SMALLER SHALL BE EQUIPPED WITH VALVE BOXES AND RESTRAINED AND VALVE FITTING WRAPPED IN CORROSION PROTECTION TAPE.
- ALL APPROVED NATIVE MATERIAL SHALL BE FREE OF FROZEN LUMPS, CINDERS, ASHES, ASPHALT REFUSE, ORGANIC MATTER, ROCKS AND BOULDERS OR OTHER DELETERIOUS MATERIALS.
- ALL WATERMAIN FITTINGS SHALL BE MECHANICALLY RESTRAINED. DETAILS OF RESTRAINTS SHALL BE DESIGNED, STAMPED AND SIGNED BY A PROFESSIONAL ENGINEER AS PART OF SHOP DRAWINGS BY THE CONTRACTOR.
- THE CONTRACTOR SHALL RETAIN THE SERVICES OF A MOECC LICENSED CONTRACTOR SPECIALIZING IN THE PROVISION OF DISINFECTION SERVICES FOR ALL WATERMAIN TESTING REQUIRED IN THIS CONTRACT.
- TRACER WIRE IS TO BE INSTALLED ON ALL NEW PVC WATERMAIN PIPES.
- THE TOP OF VALVE BOX AND CHAMBER COVERS SHALL BE SET FLUSH WITH FINISHED GRADE AND REMAIN ACCESSIBLE AT ALL TIMES.
- WATER SERVICES, A 12-GAUGE TWU STANDARD COPPER, LIGHT COLORED, PLASTIC COATED TRACER WIRE MUST BE INSTALLED WITH AND ALONG THE PIPE AND BROUGHT TO THE SURFACE AT EACH SERVICE BOX. TRACER WIRE IS TO BE ATTACHED TO THE PIPE AND OUTSIDE OF EACH SERVICE BOX BY MEANS OF TAPE OR RUBBER GROMMET.
- CHAMBER AS PER REGION STANDARD DRAWING NUMBER 1-1-5.
- DETECTOR CHECK VALVE AS PER REGION STANDARD DRAWING NUMBER 1-3-1.
- PROPOSED WATER CONNECTION AS PER REGION STANDARD NUMBER 1-6-4 AND 1-8-3
- FOR DETAILS OF THE PROPOSED TRENCH DRAIN, ROOF DRAIN, SERVICE CONNECTIONS, WATER METER AND BACKFLOW PREVENTER REFER TO MECHANICAL DRAWING.



4	ISSUED FOR 3RD ZBA SUBMISSION	2023-11-07	P.R.	F.M.
3	ISSUED FOR ZBA RE-SUBMISSION	2023-09-15	P.R.	F.M.
2	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	P.R.	F.M.
1	ISSUED FOR ZBA SUBMISSION	2021-03-19	F.M.	B.H.
No.	Revision	Date	By	App

625 Cochrane Drive, Suite 900
Markham, Ontario
L3R 9R9, Canada
Tel: (905)470-0015
Fax: (905)470-0030



Owner/Client:

DVB REAL ESTATE INVESTMENTS INC.

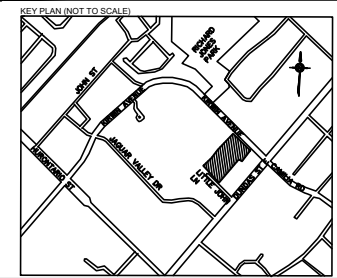
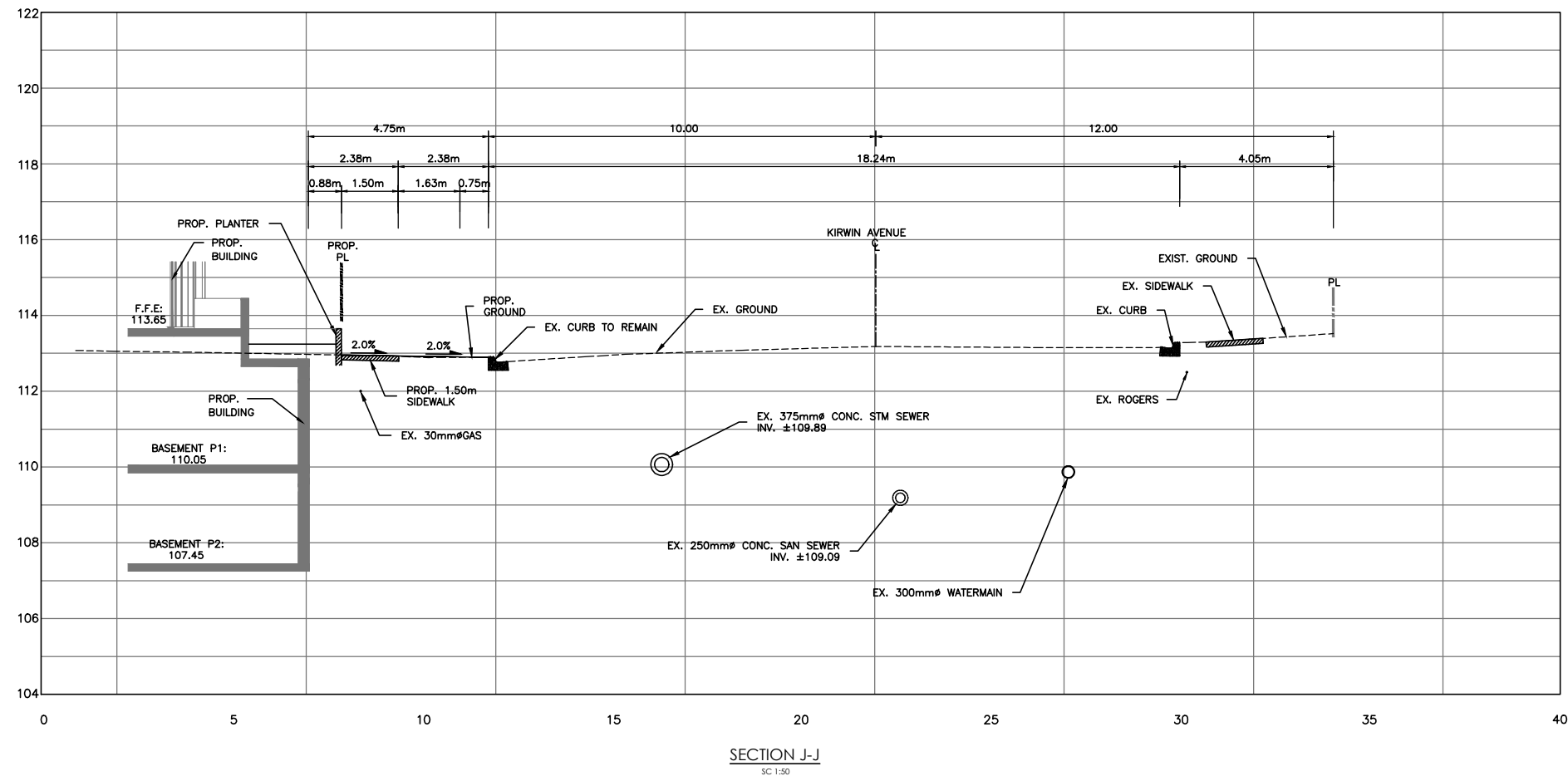
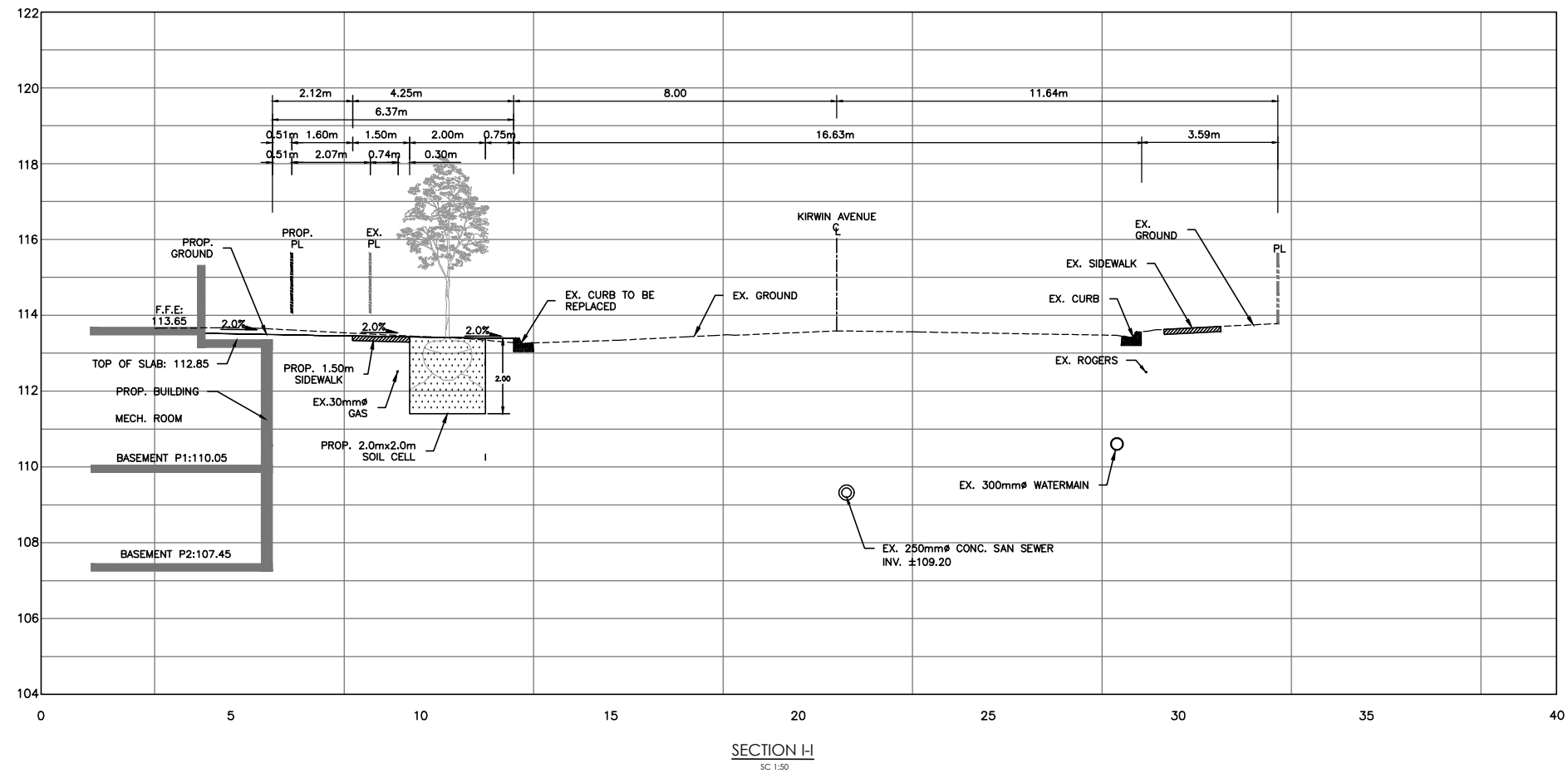
Location:

3031 LITTLE JOHN & 3016-3032
KIRWIN AVE DEVELOPMENT

Title:

GENERAL NOTES

Designed By:	F.M.	Drawn By:	J.W.	Checked By:	F.M.
Scale:	NTS	Date:	FEB., 2021	Drawing No.:	C-07
Project No.:	21111				



- GENERAL NOTES:**
- ELEVATIONS ARE REFERRED TO THE CANADIAN GEODETIC DATUM, 1928 AND WERE DERIVED FROM THE CITY OF MISSISSAUGA BENCHMARK NO. 793 LOCATED ON THE NORTH FACE AT THE EAST CORNER OF CONCRETE END POST OF BOX CULVERT UNDER DUNDAS STREET EAST ON SOUTH SIDE OF DUNDAS STREET EAST, 1.5M EAST OF JAGUAR VALLEY DRIVE, HAVING A PUBLISHED ELEVATION OF 110.955 METERS.
 - REFER TO DWG C101 "SITE GRADING PLAN" FOR LOCATION OF CROSS SECTIONS

No.	Revision	Date	By	App.
3	ISSUED FOR 3RD ZBA SUBMISSION	2023-11-07	P.R.	F.M.
2	ISSUED FOR ZBA RE-SUBMISSION	2023-09-15	P.R.	F.M.
1	ISSUED FOR ZBA RE-SUBMISSION	2022-12-19	P.R.	F.M.

625 Cochrane Drive, Suite 900
Markham, Ontario
L3R 9R9, Canada
Tel: (905) 470-0015
Fax: (905) 470-0030



Owner/Client:

DVB REAL ESTATE INVESTMENTS INC.

Location:
3031 LITTLE JOHN & 3016-3032
KIRWIN AVE DEVELOPMENT

Title:
STREETSCAPE CROSS SECTIONS

Designed By: F.M. Drawn By: J.W. Checked By: F.M.
Scale: 1:50 Date: FEB., 2021 Drawing No.: C-08
Project No.: 21111

APPENDIX H

Watertight Foundation Letter and
Hydrogeological Report



CANADA | INDIA | AFRICA | MIDDLE EAST

APPENDIX H-01

Watertight Foundation Letter



DVB Real Estate Investments Inc.
4918 King St., P.O. Box 1194
Beamsville Ont.
L0R 1B0

29/Nov/2022

Attention: Executive Director, Engineering and Construction Services
c/o Manager, Development Engineering

Dear Sir or Madam,

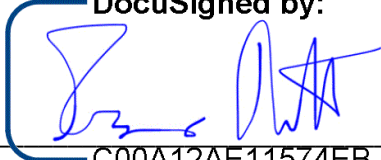
I Francesco Bertola, confirm and undertake that I will construct and maintain all building(s) on the subject lands at 3016, 3020, 3026, 3032 Kirwin Avenue & 3031 Little John Lane in Mississauga in a manner which shall be completely water-tight below grade and resistant to hydrostatic pressure without any necessity for Private Water Drainage System (subsurface drainage system) consisting but not limited to weeping tile(s), foundation drain(s), private water collection sumps(s), private water pump or any combination thereof for the disposal of private water on the surface of the ground or to a private sewer connection directly or indirectly or drainage system for disposal directly or indirectly in a municipal sewer.

A letter from a Professional Engineer confirming the design and implementation of a water-tight structure shall be provided as part of the site plan approval application.

Francesco Bertola - President
Name (printed) and Title

francescob@fbhgroup.ca

Email

DocuSigned by:

Signature C00A12AE11574EB...

I Francesco Bertola, have the authority to bind the corporation

APPENDIX H-02

Hydrogeological Report





October 24, 2022

Project No. 2202-001

Page 1 of 2

Weston Consulting
201 Millway Avenue #19, Concord
ON, L4K 5K8

Attention: Mr. Kaveh Wahdat - Planner

**Re: Hydrogeological Assessment
3016-3032 Kirwin Avenue & 3031 Little John Lane
Mississauga, Ontario**

Dear Sir:

Azure Group Inc. (Azure) was retained by Weston Consulting (The Client) to conduct a Hydrogeological Assessment at the property located at 3016-3032 Kirwin Avenue & 3031 Little John Lane in Mississauga, Ontario (The Subject Property). Azure thereby retained in partnership Azimuth Environmental Consulting, Inc. (Azimuth) to complete the Hydrogeological Assessment. As indicated in the completed report, the purpose of the Hydrogeological Assessment was to characterize the existing hydrogeological conditions at and in the vicinity of the Site, assess the need for, and options for, groundwater control in association with the proposed construction, evaluate potential impacts to the local groundwater regime resulting from the proposed construction, and identify appropriate mitigative measures, as warranted.

At the time of the site visit(s), the Site was vacant land covered with bushes, shrubs and trees. Vehicular access to the Site was from a gravel paved driveway off of Kirwin Avenue and Little John Lane, located on the northern and southern boundaries of the property. The Site had a total area of approximately 6,609 m² (1.6 acres). Azure retained Altech Drilling & Investigative Services Ltd., Ontario to complete the drilling program and Azure's representatives were on-site from April 6th, 2022 to April 8th, 2022 to conduct the field work. The scope of work consisted of the drilling of ten (10) boreholes (BH1 to BH10) to a maximum depth of approximately 9.0 metres (m) below grade or until refusal. Boreholes BH1, BH2, BH3, BH101 and BH106 were completed as groundwater monitoring wells. Representative soil samples were retrieved from each borehole and submitted for analyses of moisture content and grain size analysis. All figures showing the approximate location of the boreholes are included in the following report completed by Azimuth.

Azure Group Inc.

6751 Professional Court, Suites 201 & 202, Mississauga, Ontario, Canada

T: 905 673 2694 F: 416 907 2694 C: 416 779 2694 E: info@azuregroup.ca www.azuregroup.ca



CLOSURE

This report has been prepared for the benefit of Weston Consulting (The Client), and their clients.

Any other person or entity without the express written consent of Azure Group Inc. (Azure) and the client may not rely upon the report. Any use that a party makes of this report, or any reliance on decisions made based on it, are the responsibility of such parties. Azure accepts no liability and no responsibility whatsoever for damages, if any, suffered by any party as a result of decisions made or actions based on this report.

An environmental site characterization is a limited sampling of a site. The conclusions given herein are based on information gathered at the specific locations and can only be extrapolated to an undefined limited area around these locations. The extent of the limited area depends on the soil and groundwater conditions, as well as the history of the subject property reflecting natural, construction, and other activities. In addition, analyses have been carried out for a limited number of chemical parameters, and it should not be inferred that other chemical species are not present.

Due to the nature of the investigation and the limited data available, Azure cannot warrant against undiscovered environmental liabilities. No other warranty or representation, either expressed or implied, is included or intended in this report. Should any conditions at the site be encountered, which differ from those at the sampling locations and/or additional site information become available, Azure requests that this information be brought to our attention so that we may re-assess the conclusions presented herein. It should also be noted that current environmental Regulations, Guidelines, Policies, Standards, Protocols and Objectives are subject to change, and such changes, when put into effect, could alter the conclusions and recommendations noted throughout this report.

We trust this is satisfactory. Should any queries arise, please feel free to contact this office.

Yours truly,

AZURE GROUP INC.



Preliminary Hydrogeological Assessment
3016 – 3032 Kirwin Ave., Mississauga, Ontario

Prepared for:
Azure Group

Prepared by:
Azimuth Environmental
Consulting, Inc.

October, 2022

AEC 22-056

October 24, 2022

AEC 22-056

Azure Group
6751 Professional Court, Suite 201
Mississauga, Ontario
L4V 1Y3
Attention: Samantha Desgrosseilliers

Re: **Preliminary Hydrogeological Assessment:
3016 – 3032 Kirwin Ave., Mississauga, Ontario**


Dear Samantha,

Azimuth Environmental Consulting, Inc. (Azimuth) is pleased to provide our Preliminary Hydrogeological Assessment for the property 3016 – 3032 Kirwin Ave., within the City of Mississauga (the “Site”). This evaluation focused on the existing soil and ground water regime underlying the Site and the potential for the proposed eight (8) story residential building and associated parking development to impact the existing conditions.


Should you have any questions or wish to discuss the report in greater detail, please do not hesitate to contact the undersigned.

Yours truly,

AZIMUTH ENVIRONMENTAL CONSULTING, INC.



Brendan MacNaughton, B.Sc (Hons), EP.
Environmental Scientist



Colin Ross, B.Sc, P.Geo.
Senior Hydrogeologist

M:\Projects\22 Projects\22-056 Kirwin Ave. Hydrog Assessment\05.0 - Reporting\05.2 - Draft\220406- 22-056- Kirwin Ave
Hydrogeologic Report -FINAL.docx



Table of Contents

	page
1.0 INTRODUCTION.....	1
1.1 Background	1
2.0 ENVIRONMENTAL SETTING	1
2.1 Soil	1
2.2 Physiography	2
2.3 Topography and Drainage	2
2.4 Bedrock Geology	2
2.5 Quaternary Geology	2
2.6 Hydrogeology.....	3
3.0 SOURCE WATER PROTECTION.....	5
4.0 MONITORING	5
4.1 Previous Site Investigations	5
4.1.1 Site Drilling & Monitoring Well Installations.....	5
4.2 Ground Water Level Monitoring	5
4.3 Hydraulic Conductivity Testing	6
4.4 Water Quality.....	7
5.0 WATER BALANCE	7
5.1 Land Use	8
5.1.1 Pre-Development	8
5.1.2 Post-Development	8
5.2 Infiltration	9
5.2.1 Pre-Development Infiltration.....	9
5.2.2 Post-Development Infiltration	10
5.3 Water Balance Summary	10
6.0 DEWATERING ASSESSMENT.....	10
6.1 Drawdown Conditions.....	10
6.2 Approximate Dewatering Volumes	11
6.3 Impact Assessment.....	13
7.0 SUMMARY AND CONCLUSIONS	13
8.0 REFERENCES.....	16



List of In-Text Tables

	page
Table 1: MECP Water Well Database Summary (500 m radius from Site).....	4
Table 2: Ground Water Elevation Data	6
Table 3: Hydraulic Testing Results	7
Table 4: Pre-Development Area Classification	8
Table 5: Post-Development Area Classification.....	8
Table 6: Summary of Pervious Land Infiltration Factor.....	9

List of Figures

Figure 1	Property Location
Figure 2	Site Layout
Figure 3	Natural Features and Surrounding Well Records
Figure 4	Monitoring Well Locations and Ground Water Flow

List of Appendices

Appendix A:	Figures
Appendix B:	Proposed Development Plan
Appendix C:	MECP Well Records & Site Borehole Logs
Appendix D:	Water Balance Summary Tables
Appendix E:	Hydraulic Conductivity Testing
Appendix F:	Water Quality Data



1.0 INTRODUCTION

Azimuth Environmental Consulting Inc. (Azimuth) has been retained by the Azure Group to conduct a Preliminary Hydrogeological Assessment for the property 3016-3032 Kirwin Avenue within the City of Mississauga (the “Site”) (Figure 1).

The purpose of this assessment is to characterize the existing hydrogeological conditions at the Site, and determine any potential constraints to the proposed development plan. This assessment also addresses Source Water Protection policies developed under the *Clean Water Act* as they pertain to water quantity and quality issues.

1.1 Background

The Site is rectangular in shape, 6,385 m² (0.6 hectares (ha)) in size and is to be redeveloped as an 8 storey residential building with Underground parking. The Site is located on the south side of Kirwin Avenue; a small cleared area remains from the historical residential dwellings at the Site along the east of the site. As per the proposed development plans provided, the development will be accessed from Kirwin Avenue and will include two (2) below grade parking levels extending approximately 7 m below grade. The proposed Site development plans are provided in Appendix B.

The purpose of this assessment is to characterize the existing physical geological and hydrogeological conditions at the Site and the potential for the proposed development to impact the existing environmental / hydrogeological conditions. The report follows a standard format addressing typical requirements of both the City of Mississauga and Credit Valley Conservation Authority for hydrogeological submissions within the Credit Valley source water protection zone.

2.0 ENVIRONMENTAL SETTING

2.1 Soil

The Soil Map of Peel County (Report No. 18) (Hoffman, et al., 1953) defines the surficial soil for the Site as part of the Cooksville Series; however the Site sits just north of the divide between the Fox Series which uses the location of Dundas Street in the 1950’s as the divide. Based on the mapping, the region is also crosscut with Alluvial fans (Alluvial Series) spreading north from the Lake Ontario shoreline. For the purposes of this investigation we will assume that the location of Dundas Road has not significantly moved and the Site sits within the Cooksville Series. The Cooksville Series is described as shallow or very shallow surficial dark grey clay laden loams overtop of shallow grey shale. Cooksville clay Loams are classified within Soil Group D. Group D soils represent material with very high runoff potential and restricted to highly restrictive



infiltration rates. Of note Soils within Group D can have high shrink/swell potentials. This soils description is line with the physical investigation done onsite.

2.2 Physiography

The Ontario Geologic Survey (Chapman and Putnam 1984) describes the Site area as being located within the Iroquois Plain physiographic region. This region extends from the Trent River approximately 300 km to the Niagara River. The Iroquois Plain is subdivided into 8 regions; the Subject Site sits within the Hamilton to Toronto region, a thin region defined by the current and ancient shoreline of Lake Iroquois. This section is represented by multiple sand and gravel alluvial outwash sections and the flat, smoothed historic fine grained bedding of Lake Iroquois.

2.3 Topography and Drainage

The topographic relief at the Site is quite limited with elevations ranging from approximately 113 masl in the north along Kirwin Avenue to a low of 110 masl in the south west along Little John Lane. The current Site drainage is expected to follow the local topographic dip to the southwest towards Cooksville Creek, located approximately 70 m west of the Site, although any surface runoff exiting the Site is expected to be captured by the municipal drainage system in the area. Run on to the Site is not expected from the surrounding developments based on the topographic setting and curb and gutters present along the upslope side of the Site.

2.4 Bedrock Geology

The underlying bedrock geology has been described by the Ontario Geologic Survey (OGS) as being composed of grey calcareous shale of the Georgian Bay Formation of (Ontario Geologic Survey , 2011). The formation is Upper Ordovician in age. Based on the thickness mapping surrounding the site the Site, bedrock can be expected somewhere between 3 and 8 mbgs (Gao, et al., 2006), which is in agreement with the results of the boreholes advanced on Site. Shallow bedrock was identified in BH1, 2 and 3, all having weathered shale identified within the soil samples in the lower section of each log.

2.5 Quaternary Geology

The Quaternary Soil Map of Ontario (Onatrio Geological Survey, 2003) defines the local surficial soils in the vicinity of the Site as Paleozoic in age comprised of undifferentiated carbonate and clastic sedimentary rock, which is exposed at surface or covered by a discontinuous, thin layer of drift. This area also borders on an area characterized as the Halton Till, which consists predominantly of a silt to silty clay matrix. The Halton Till is texturally variable but is generally a sandy silt to clayey silt till interbedded with silt, clay, sand and gravel. In some areas it is very clay-rich where the Ontario Ice Lobe has



overridden glaciolacustrine deposits of the Lake Ontario basin. The Halton Till is typically 3 to 6 m thick but locally it can exceed 15 to 30 m in thickness in the western part of the study area.

Based on the Site specific soils data provided by the Azure Group subsurface investigation the Site is underlain by a thin topsoil layer (10 cm) overtop of a fill mixture consisting of sand, silt and clay of different compositional percentages to a depth of around 3.5 mbgs. Below this level the boreholes intersect a native Silty-Clay layer to the upper contact of the underlain Weathered Shale bedrock which was encountered in five (5) of the advanced boreholes below 7 mbgs, all of the boreholes all indicate a content of weathered Shale fragments below ~6.5 mbgs. The inclusion of the fragments indicate that the bedrock interface is very close to this depth, which is in agreement with both afore mentioned mapped Quaternary description and the drift thickness mapping results. Based on the observed Site soils, it is likely these material represent Halton Till.

For reference, the borehole locations are illustrated on Figure 2, while the borehole logs are provided in Appendix C.

2.6 Hydrogeology

The Ontario Ministry of Environment, Conservation, and Parks (MECP) Water Well Records were referenced for any recorded well information within the vicinity of the Site (500 m) (MECP, 2021). The Site and surrounding area is likely to be serviced with water and sewer utilities; however well records can be used to gain subsurface information which can provide insight into shallow geological formation within the area. The well records found in the vicinity of the Site that are pertinent to this assessment are summarized in Table 1 and are shown on Figure 3. The thirty-six (36) surrounding wells in the MECP well record database indicate that one (1) was a decommission record, one was completed in 1952 and is the only record of a potable water supply well (No. 4902211). The remaining thirty-four (34) well records were for advanced as test holes in the area. The wells were drilled to depths between 3 and 15 m. Nine of the well records were not available online. The remaining records have been included in Appendix C. The well records indicate that the grey /blue shale bedrock surface is quite limited, between 2 and 5 mbgs in fourteen of the well records. The overburden soils identified in these records were primarily clay and silt with some sand and or gravel, which matches the geological literature outlined above, as well as the Site specific soils identified the drilling program. Given the age of the wells and the fact the area has been municipally serviced for many years, it is unlikely that the supply well is still in use.



Table 1: MECP Water Well Database Summary (500 m radius from Site)

Well ID	Date Completed	Depth (m)	Depth to Bedrock (m)	Distance to Site (m)	Direction to Site
4902211	1958-11-12	15.5	5.2	201	N
4909841	2005-06-30	7.6	7.6	201	NNE
7107988	2008-06-02	6.1		215	SW
7140001	2010-01-20	6.7	6.1	233	E
7144432	2010-03-22	3.7		201	E
7145320	2010-04-28	4.8	2.5	467	NE
7148379	2010-06-21	3.1		262	NW
7148380	2010-06-21	3.4		260	NW
7148381	2010-06-21	0		415	NW
7196498	2012-10-09	7.6		115	SW
7202168	2012-11-20	6.09		200	SE
7210777	2013-10-11	5.5		60	S
7210806	2013-10-11	4.9		61	S
7210807	2013-10-11	4.7		62	S
7263541	2016-04-11	5.2	4.3	260	W
7263542	2016-04-11	5.2	3.7	265	W
7263543	2016-04-11	5.2	4.3	280	W
7263544	2016-04-24	1.4		285	W
7277547	2016-11-18	3		290	W
7277548	2016-11-17	3	3.0	430	SW
7278591	2016-11-25	5.3	2.5	360	NW
7296547	2017-09-12	4		425	SSW
7296548	2017-09-12	4		430	SSW
7296549	2017-09-12	4.3	3.0	420	SSW
7306688	2017-09-13	7.6		0	Onsite
7330071	2018-12-17	4		445	S
7332231	2019-04-08	4.5	2.1	350	NW
7345861	2019-07-03	3.7		326	NW
7345862	2019-07-03	3.7		325	NW
7358771	2020-04-24	0		410	SW
7358772	2020-04-24	0		400	SW
7358773	2020-04-24	0		400	SSW
7361501	2020-03-12	0		351	NW
7378766	2020-12-09	6.7	4.6	0	Onsite
7378767	2020-12-09	6.7	4.6	0	Onsite
7378768	2020-12-09	6.7	4.6	0	Onsite



3.0 SOURCE WATER PROTECTION

A review of the Source Water Protection Areas as identified on the MECP Source Protection Information Atlas website indicates the Site is contained within South Peel Drinking Water Intake Protection Zone (IPZ) 2, as well as within a Highly Vulnerable Aquifer Area (HVA). However, it is not within a Significant Ground Water Recharge Area (SGRA), Wellhead Protection Area (WHPA-D), WHPA-Q2, Issues Contributing Area (ICA). Given the IPZ, consideration may need to be given for stormwater control measures at the Site.

4.0 MONITORING

4.1 Previous Site Investigations

Azure Group Inc. completed a geotechnical drilling program at the Site in 2022 and it is also understood that a previous Phase II Environmental Site Assessment (ESA) as completed which included drilling and installation of monitoring wells on Site. These reports were not available at the time of report issuance: however, the borehole logs for the current monitoring wells on Site were provided and utilized in this assessment. The details of which are summarized in subsequent sections.

4.1.1 Site Drilling & Monitoring Well Installations

A drilling program was undertaken by Azure as part of the above mentioned geotechnical between April 1st and April 8th 2022. Ten (10) boreholes were advanced across the site, three (3) were then completed as ground water monitoring wells for the Site as illustrated on Figure 4, with borehole logs and a location plan included in Appendix D. It is noted that a collection of 3 additional historic wells are present at the Site from an Azure site investigation in December 2020 as well as two (2) additional wells, the history and construction details are not known, these are assumed to be related to the wells installed in 2017 (Appendix C record number 7306688). The onsite wells are summarized Table 2 below.

4.2 Ground Water Level Monitoring

As part of assessment, ground water levels were monitored on the May 11th 2022 by Azimuth staff. The ground water measurements have been included within Table 2 below and used to create Figure 4 with the inferred groundwater flow direction.

Currently the base of the underground parking level has been established at 6.7 mbgs such that the building foundation will encroach into the water table by up to ~1.5 m. As such, these seasonally high ground water elevations need to be considered in the building design such that proper waterproofing is being incorporated within the basement level.



The inferred ground water flow direction is illustrated on Figure 4, which shows a south flow pattern, which matches the direction of a buried section of the Cooksville Creek.

Table 2: Ground Water Elevation Data

Ground Water Elevation Table												
Azimuth Project Number			22-056									
Project Site			Kirwin Ave									
Town/Region			Mississauga, Peel									
			GPS (Zone 17)									
Well ID	Easting	Northing	Elevation (MRD)	Stick Up	Elevation of Screen Bottom (mASL)	Elevation of Screen Top (mASL)	Date	Depth to Water (mBTOP)	Depth to Bottom (mBTOP)	Depth to Water (mBGS)	Depth to Bottom (mBGS)	Groundwater Elevation (mASL)
BH1	612103	4826454	113.31	0.85	106.69	109.74	05-11-2022	5.06	7.47	4.21	6.62	109.10
BH2	612080	4826562	112.56	0.65	104.97	108.02	05-11-2022	5.94	8.24	5.29	7.59	107.27
BH3	612091	4826465	113.31	1.10	106.68	109.73	05-11-2022	5.36	7.73	4.26	6.63	109.05
BH101	612090	4826483	113.39	1.04	107.11	110.16	05-11-2022	5.75	7.32	4.71	6.28	108.68
BH106	612033	4826412	110.78	0.92	105.28	108.33	05-11-2022	3.87	6.42	2.95	5.50	107.83
Unknown 1*	612108	4826460	113.0*	0.79	105.34	108.39	05-11-2022	4.96	8.45	4.17	7.66	108.83
Unknown 2*	612101	4826439	112.5*	0.68	104.97	108.02	05-11-2022	4.75	8.21	4.07	7.53	108.43

GPS Location based on hand held device and is not a Surveyed location.
Elevations are in metres above sea level (mASL) Provided by Azure
*BH with unknown origin on site close to locations of BH 102 and 103, no known elevation was surveyed

4.3 Hydraulic Conductivity Testing

In order to understand the hydraulic characteristics of the underlying overburden, transient hydraulic tests were performed on the Site monitoring wells following the 2022 drilling program. The transient test involves the instantaneous injection or withdrawal of a volume or slug of water or solid cylinder of known volume. This is accomplished by adding or displacing a known volume to/from a well and measuring water level response time to return to equilibrium. Water level measurements were recorded both manually and with automatic dataloggers, which were programmed to record the pressure of water above the data logger every second. Data was analyzed using the Hvorslev Method (1976) for unconfined aquifers, which assumes a homogeneous, isotropic medium in which soil and water are incompressible. Hydraulic testing results are summarized in Table 3 (below).

The soil transmissivity for the Site is varied by an order of magnitude. Based on the local geology reported from both the borehole logs and from the surrounding water well records this is what was expected. The result of the slug test is included in Appendix E. The measured hydraulic conductivity is within the published range for a silty clay material (Freeze & Cherry, 1979).



Table 3: Hydraulic Testing Results

Hydraulic Test Results				
Azimuth Project Number		22-056		
Project Site		Kirwin Avenue		
Town/Region		Mississauga, Peel Region		
Well	Test Date	Screen Interval (MRD)	Screen Material	Hydraulic Conductivity (m/sec)
BH/MW106	2022-04-08	108.3-105.2	Clay/Silt	5.56E-09
BH/MW2	2022-04-08	108.2-104.9	Clay/Silt	2.28E-08
Site Average				1.42E-08
Site Max				2.28E-08

4.4 Water Quality

A water quality sample was taken from one onsite well location to provide some insight to the requirements of dewatering water treatments. The results of which are included in Appendix F. The results are compared to the Provincial Water Quality Standards as the discharge point is unknown at this time; the City of Mississauga has both storm and sanitary sewers in the area, as well as a watercourse to the south (Cooksville Creek). The PWQO Standards were chosen as they are more stringent than that of the sewer bylaw standards. Of the tested parameters Total Phosphorous exceeded the PWQO standard. The total phosphorus concentrations are significantly elevated, but this along with the metal constituents are interpreted to be sourced from the elevated sediment load in the sample; this is evidenced by the elevated turbidity at these locations (181 NTU). The nutrient analysis was completed on water that was unfiltered, and therefore contained high concentration of sediment particles. The increased phosphorus is therefore likely attributed to the excess nutrients that are bound to the sediment grains in suspension and dissolved within the acidified nutrients bottle. As such, discharge of any potential dewatering effluent into storm sewer or natural environment would not likely represent any impact assuming proper sediment controls are in place for any dewatering discharge. To confirm the effluent discharge into the storm sewer system, a secondary sample meeting all of the requirements of The City By-Law would need to be collected, which can be confirmed ahead of any potential construction dewatering.

5.0 WATER BALANCE

In order to determine the potential changes to the natural ground water recharge conditions, a pre- and post-development water balance assessment has been completed using the Thornthwaite and Mather method (1957). This method evaluates evapotranspiration based on precipitation and temperature. Residual soil saturation is a function of topography and soil type. Monthly data are tabulated from daily average



temperature and precipitation, and the water budget is a continuous calculation over the period of record. To clarify, the method and the approach used by many individuals in examining infiltration resets annual conditions (moisture deficit, snow storage, etc) over the winter months because of the general lack of infiltration during the frost period. However, we maintain those records and carry them forward from month to month during the entire period of record.

Values were determined on a monthly basis, compiled from daily Environment Canada meteorological data station located in Toronto Leaster B. Pearson International Airport (Station 6158733), Ontario between 1950 and 2021. The calculations are based on the average conditions during this period; the average precipitation was 779 mm, rainfall was 632 mm, evapotranspiration was 490 mm and the surplus was 289 mm.

5.1 Land Use

5.1.1 Pre-Development

The pre-development Site area was classified according to land use/vegetation type. Approximate pre-development land use classification areas are provided in Table 4.

Table 4: Pre-Development Area Classification

Land Use	Land Area (m ²)
Forest	4,300
Landscaped Grass	2,085
TOTAL	6,385

Land within the pre-development scenario is considered 0% impervious

5.1.2 Post-Development

The land classification in the post-development scenario was classified based on the Site Development Plans (Appendix B). Post-development land use classification areas are provided in Table 5:

Table 5: Post-Development Area Classification

Land Use	Land Area (m ²)
Impervious(building/driveway)	3,433
Pervious (landscaped/undeveloped)	502
Parkland Dedication	2,450
TOTAL	6,385

Land within the post-development scenario is considered 54% impervious. The post-development areas are illustrated in Appendix B.



It is noted that impervious areas included landscaped areas atop the below grade parking structure and any infiltration in these areas will likely be required to be drained to sewer or discharged to surface via a sump pump such that no infiltration would be expected.

5.2 Infiltration

Infiltration is generated one of two ways: (1) directly from rainfall impact or snowmelt on pervious surfaces; and (2) indirectly when runoff from impervious surfaces is diverted into adjacent naturalized areas.

Infiltration factors for the Site were estimated based on the underlying soil, local topography, and ground cover as per Table 2 of the Ministry of Environment and Energy (MOEE) Hydrogeological Technical Information Requirements for Land Development Applications (1995).

The soil variable factor was determined by taking into account information obtained from the regional geologic mapping and the field work programs completed for the Site. This information suggests that the surficial material at the Site is primarily composed of a silty clay. The infiltration factors utilized in the water balance assessment are summarized in Table 6 below.

Table 6: Summary of Pervious Land Infiltration Factor

Scenario	Land Use	Infiltration Factor	Assumption
Pre-Development	Landscaped Grass	0.4	Flat Land (0.2), Clay/silt (0.1), Maintained Grass Cover (0.1)
	Forest	0.5	Flat Land (0.2), Clay/silt (0.1), Woodland cover (0.2)
Post-Development	Landscaped Grass	0.4	Flat Land (0.2), Clay/silt (0.1), Maintained Grasses (0.1)
	Dedicated Parkland	0.5	Flat Land (0.2), Clay/Silt (0.1), Woodland Cover ¹ (0.2)

1- Dedicated Parkland surficial cover is assumed to be a mix of treed space to match the John C. Price Parkland existing adjacent to the dedication lands.

5.2.1 Pre-Development Infiltration

Pre-development direct infiltration was determined by multiplying the annual average surplus amount, the area of each land use, and the infiltration factor for each land use. The pre-development annual infiltration is therefore 862 m³/year (Appendix D).



5.2.2 Post-Development Infiltration

Post-development infiltration (without mitigation) was determined by multiplying the annual average surplus amount, the area of each land use, and the infiltration factor for each land use. The post-development annual direct infiltration is therefore 412 m³/year. There is therefore a decrease in infiltration of 450 m³/year from pre- to post-development without mitigation measures employed.

5.3 Water Balance Summary

Using the climate model data and calculations mentioned above, the water balance was completed for pre-development and post-development without mitigation (Appendix D) as no stormwater drainage plans were available at the time of reporting.

The pre-development infiltration volume is 862 m³/year. This assumes the Site is vacant as it sits today. The post-development without mitigation infiltration volume is 412 m³/year, which is a deficit of 450 m³/year. This is based on the proposed development as described in Section 1.0 of this report and illustrated in Appendix B (Site Development Plans).

6.0 DEWATERING ASSESSMENT

As noted above, the proposed development and associated underground parking and servicing, have been shown to be positioned below the water table. In this area, ground water elevations are represented by the installed monitoring wells. Based on the monitoring completed on the wells, the high ground table sits at 109.10 mASL, and the estimated base of the two (2) level underground parking slab proposed to be at 6.7 mbgs (107.45 mASL). Given these elevations place the foundation approximately 3.6 m into the water table (approximately 2m below the slab), for a dry working area at the base of the excavation, a construction dewatering plan will be needed.

Since the required drawdown is greater than 1.5 m, the use of shallow well points or educator systems may be required. The exact dewatering methodology will depend on site-specific conditions and will be determined by the dewatering contractor.

Dewatering discharge is assumed to be handled on-site with discharge ultimately being into either the municipal stormwater or sanitary infrastructure assumed to run along Kirwin Avenue.

6.1 Drawdown Conditions

The details utilized for this assessment are derived from the KEA design drawings (Appendix B). These details including location, width, length and base elevations for the



proposed building were utilized to determine the maximum drawdown required for construction in relation to the water table conditions for the Site as illustrated in Figure 4 appended.

Although the water table contouring illustrated on Figure 4 shows a decline to the south, for the purposes of the dewatering assessment, it has been assumed a high water table elevation of 109.10 mASL (BH/MW1) extends across the entire site area. In reality, there is a likely decline as illustrated in the contours toward the southeast which could limit the drawdown requirements for the south section of the excavation; however, this conservancy is utilized to address the limited ground water elevation points in this area as monitoring well coverage is limited on the Site. Regardless, based on the measured high ground water table (109.10 mASL) and the excavation base elevations (105.45), ground water lowering during construction will be approximately 3.6 m. This is based on the following assumptions:

- Construction ground water lowering will target a depth of 2 m below the base of the P2 slab to ensure dry working conditions within the utility trenching needed below the slab and footings;
- To be conservative, the hydraulic conductivity value referenced (2.28×10^{-7} m/sec) in this assessment has been increased from the high-end estimate of the overburden aquifer single well response testing (SWRT) included in Appendix G a order of magnitude. This was done to account for potential higher permeable horizons than what was tested;
- The most elevated ground water elevation / depth of ground water was assumed to apply to the area; and
- The entire proposed building is assumed to be constructed as single dewatering undertaking installed at one time. If the dewatering was done in sections, then the volumes and Zone of Influence would be reduced;

The actual drawdown will depend on construction timing.

6.2 Approximate Dewatering Volumes

For the dewatering a rectangular configuration where the relationship of length/width is greater than 1.5, calculations for the dewatering rate / volume were completed using the steady state method from Powers, *et al.* (1992) for estimating radial flow to an excavation in an unconfined aquifer.



The following equation was used:

$$Q = \frac{\pi K (H^2 - h^2)}{\ln\left(\frac{R_o}{R_s}\right)} + 2\left(\frac{LK(H^2 - h^2)}{2L}\right)$$

Based on Equation 6.12 in systems where $l/w > 1.5$ (Powers, P.E., 1992) Where:

Q (m³/Day)
 K - Hydraulic Conductivity (m/Day)
 H - Distance from Static water level to bottom of Aquifer (m)
 h - lowest water level needed from static (m)
 R_o - Radius of conical depression (m) (Taken from Equation 6.14(Powers, P.E., 1992))

$$R_o = 3(H - h)\sqrt{k}$$

Where
 K - Hydraulic Conductivity (m/Sec)
 R_s - Equivalent Radius (m)

$$R_s = \frac{l + w}{\pi}$$

l - Length of excavation/trench
 w - width of trench
in systems where $l/w > 1.5$

The full dewatering assessment can be found in Appendix G

Based on the information provided, the dewatering required for construction is 27,720 L/day. A 3x safety factor can then be applied to each of the above volumes for a conservative estimate (83,160 L/day). These values are based on worst case spring season ground high ground water table depths. The dewatering volume could be lower during the summer and fall months.

Any construction dewatering between 50,000 L/day and 400,000 L/day can be completed after registration under the Environmental Activity and Sector Registry (EASR). Any active construction dewatering above 400,000 L/day requires a Permit To Take Water (PTTW). As noted above, the magnitude of dewatering required will vary on the timing of construction and less dewatering could be needed in the summer drought conditions. Peak ground water elevation typically occurs between mid April and the end of May. Based on the calculations, it is likely that construction dewatering would be above the 50,000 L/day but below the threshold of 400,000 L for a PTTW, as such an EASR will be required. Potential dewatering requirements can be minimized if work is completed during the drier summer months.

Not included in the calculations above is the influx of stormwater from single 24 hour storm events. These numbers are estimated based on the Ministry of Transportation (Ministry) Intensity Duration Frequency (IDF) curves. Using the numbers provided by the Ministry, if the Site experiences a five (5) year storm event (56 mm across 24 hours) during the excavation an additional 289 m³ (219,000 L) into the excavation, in this event, pumping could continue under the registered EASR. Any of the larger less frequent (10



yr, 25 yr, 100 yr) storm events would require a staged approach where the excavation could be pumped at the 400,000 L/day over two (2) days to facilitate the removal of the storm water without exceeding the threshold of requiring a PTTW registration.

6.3 Post Construction Dewatering

It is our understanding that although the finished floor elevation of the building foundation encroaches into the water table by approximately 1.6 m, the planned waterproofing of the foundation will limit potential concerns with respect to the ground water at the Site with regards to permanent dewatering of the Site.

However, if the foundation is not waterproofed and the same assumptions as above are used, substituting the final floor elevation would be utilized for the dewatering depth (107.45 mASL) establishing a dewatering requirement of approximately 18 m³/day. A 3x safety factor can then be applied to the above volumes for a conservative estimate of 54 m³/day (54,000 L/day). This volume will make the registration of PTTW required for the permanent dewatering of the foundation.

6.4 Impact Assessment

Based on the information calculated, the largest zone of influence is 60 m from the edge of the dewatering zone; however this is the maximum distance where any measurable water table decline would be observed. However, more significant decline in ground water levels (2 m) will be contained within approximately 57 m of the Site

As the area is municipally serviced, there are not anticipated to be any private wells located within the radius of influence. There is a creek located approximately 70 m south west of the Site; however this is located at the very extent of the zone of influence, and is not expected to be affected by the dewatering process. Further to this if the creek was used as the discharge point, any minimal drawdown would be negated by the discharge.

The site is located within the Intake Protection Zone 2 for the South Peel Drinking Water intake which identifies that the site is within approximately two (2) hours surface water travel time to the point of the intake. This will have to be taken into account when considering the design of the dewatering discharge treatment.

7.0 SUMMARY AND CONCLUSIONS

Azimuth was retained by the Azure Group to conduct a Preliminary Hydrogeological Assessment for the property located along Kirwin Avenue inclusive of 3016-3032 within the City of Mississauga. The purpose of this assessment is to characterize the existing preliminary hydrogeological conditions at the Site and the potential for the proposed



development to impact the existing environmental / hydrogeological conditions. The report also addresses many of the CVC and Source Water Protection policy requirements.

The Site is rectangular in shape, 6,385 m² (0.6 hectares (ha)) in size and is to be redeveloped as an 8 storey residential building with underground parking. The Site is located on the south side of Kirwin Avenue; a gravel driveway and small paved area in the south side of the property remain from historical residential dwellings at the Site. As per the proposed development plans, the development will be accessed from Kirwin Avenue and will include two (2) below grade parking levels extending approximately 7 m below grade.

The Site is found at an elevation ranging between approximately 110 masl to 113 masl at with a slight southern slope. The existing Site drains via overland flow towards the existing City of Mississauga infrastructure along Little John Lane. Site native soils are composed of mostly silts and clays.

The inferred ground water flow direction is shown to be in a southern direction, which matches the direction of a buried section of the Cooksville Creek. Water table conditions fluctuated across the area ranging between 2.9 and 5.2 mbgs, this fluctuation is assumed to be based on the elevation of the bedrock in the area, which consists of a shallow weathered shale.

Hydraulic conductivity testing was completed at a number of the Site monitoring wells indicating the hydraulic conductivity of the site is ranging between 5×10^{-9} to 2×10^{-8} m/s.

The pre-development infiltration volume is 862 m³/year. This assumes the Site is currently not landscaped and vacant. The post-development without mitigation infiltration volume is 412 m³/year, which is a deficit of 450 m³/year.

At the time of report issuance, no formal storm water plans were developed, such that it is uncertain as to whether any LID's will be included in the development plan to mitigate any of the ground water infiltration loss. However, given the limited size of the Site and presence of underground parking structure, there will not likely be sufficient area to implement such measures.

The overall deficit is considered large; however, the area is municipally serviced such that there is unlikely any private supply wells in the area, while surface water features are limited to a creek approximately 70 m southeast of the Site. The limited permeability of



the soils would also indicate that the Site likely has little ground water infiltration capacity such that influence on the adjacent creek will not likely be impacted.

The proposed development will include the construction underground car parking with associated underground servicing (water, sewer, storm water). It is assumed that new service connections to Kirwin Avenue will be established as part of the proposed development. Based on the current development plan, dewatering will be required across the entire site due to the underground parking area. The assessment is based on the measured water table depths during the May, 2022 monitoring event; however water table conditions could vary seasonally. However, it is noted that the dewatering volumes are quite low such that even an increase in water table will not have a significant impact on water taking volumes. Consideration needs to be given to the quality of the dewatering discharge, which may require treatment prior to discharge city's storm water network or the local surface water creek. It is assumed that this will require obtaining a discharge permit from the city prior to initiation of any dewatering activities at the Site. Additional water quality samples may be required to confirm dewatering discharge quality.

As per Ontario Regulation 903 requirements, all existing monitoring wells which are no longer utilized at the Site will need to be properly decommissioned as per O.Reg. 903 (Wells Regulation) prior to commencement of building construction.

As the building foundation encroaches well into the water table, the planned waterproofing of the foundation will limit potential concerns with respect to the ground water at the Site. Dewatering will be required to facilitate construction; however, the dewatering assessment would indicate that the radius of influence does not extend to the closest natural feature which is a creek located 60 m south east of the Site. Similarly, the area is municipally serviced for water such that there is no expectation that any private wells exist within the area of influence.



8.0 REFERENCES

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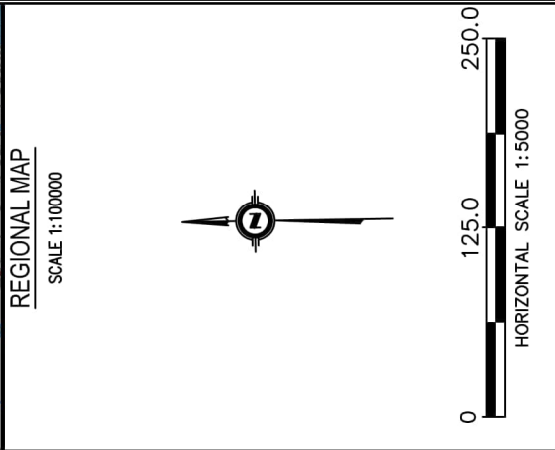
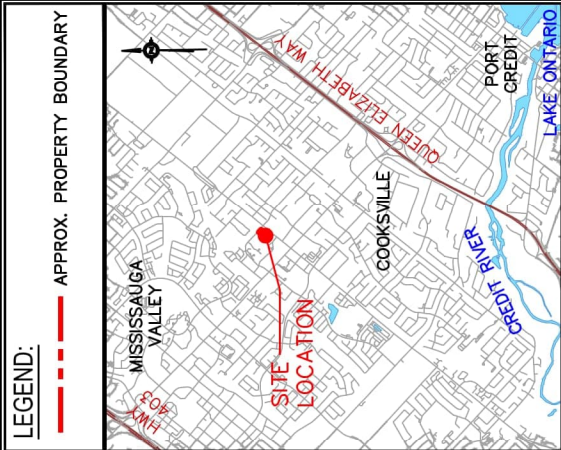
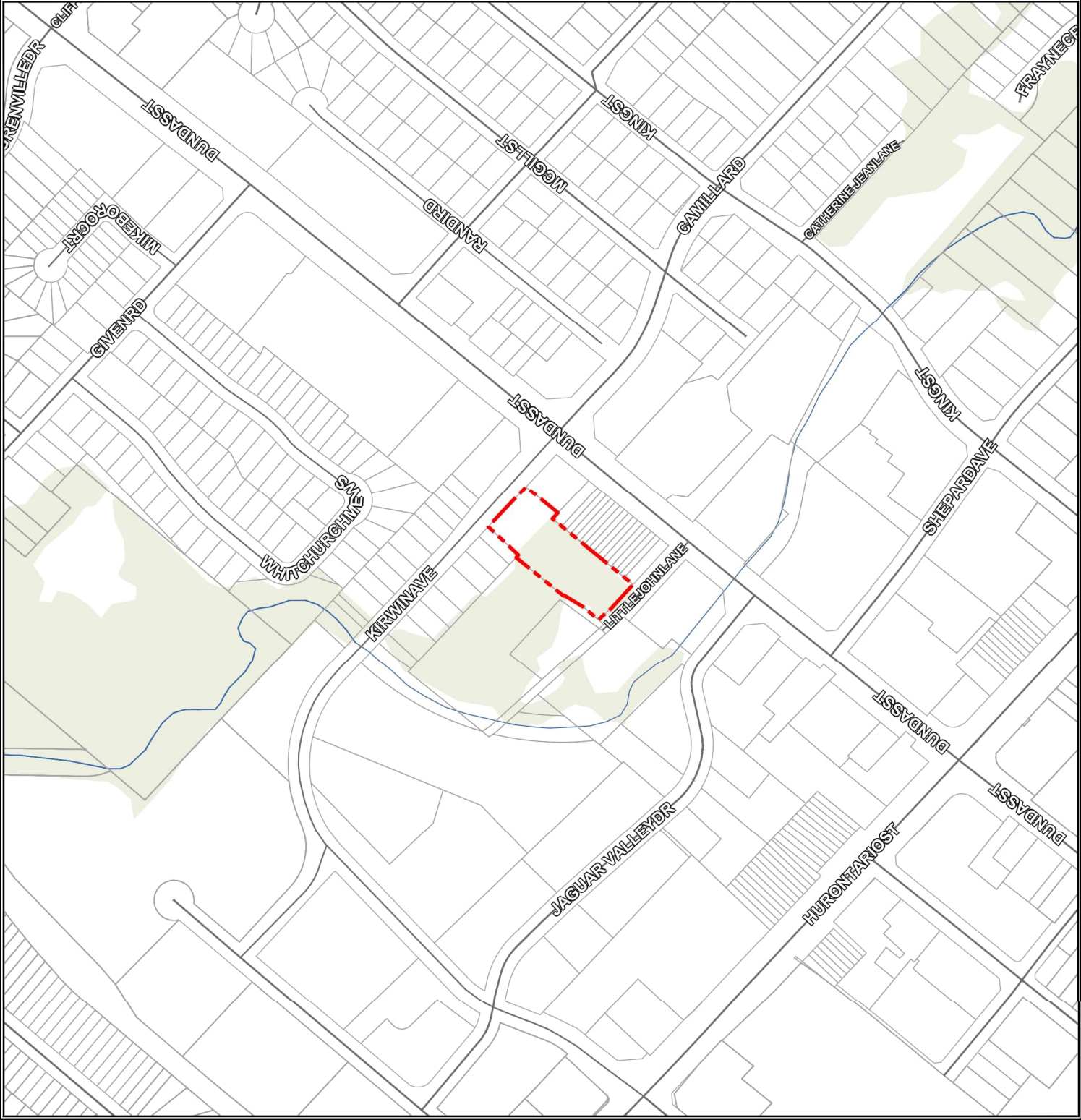
APPENDICES


- Appendix A: Figures**
 - Appendix B: Proposed Development Plan**
 - Appendix C: MECP Well Records & Site Borehole Logs**
 - Appendix D: Water Balance Summary Tables**
 - Appendix E: Hydraulic Conductivity Testing**
 - Appendix F: Water Quality Data**
 - Appendix G: Dewatering Calculations**
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APPENDIX A

Figures



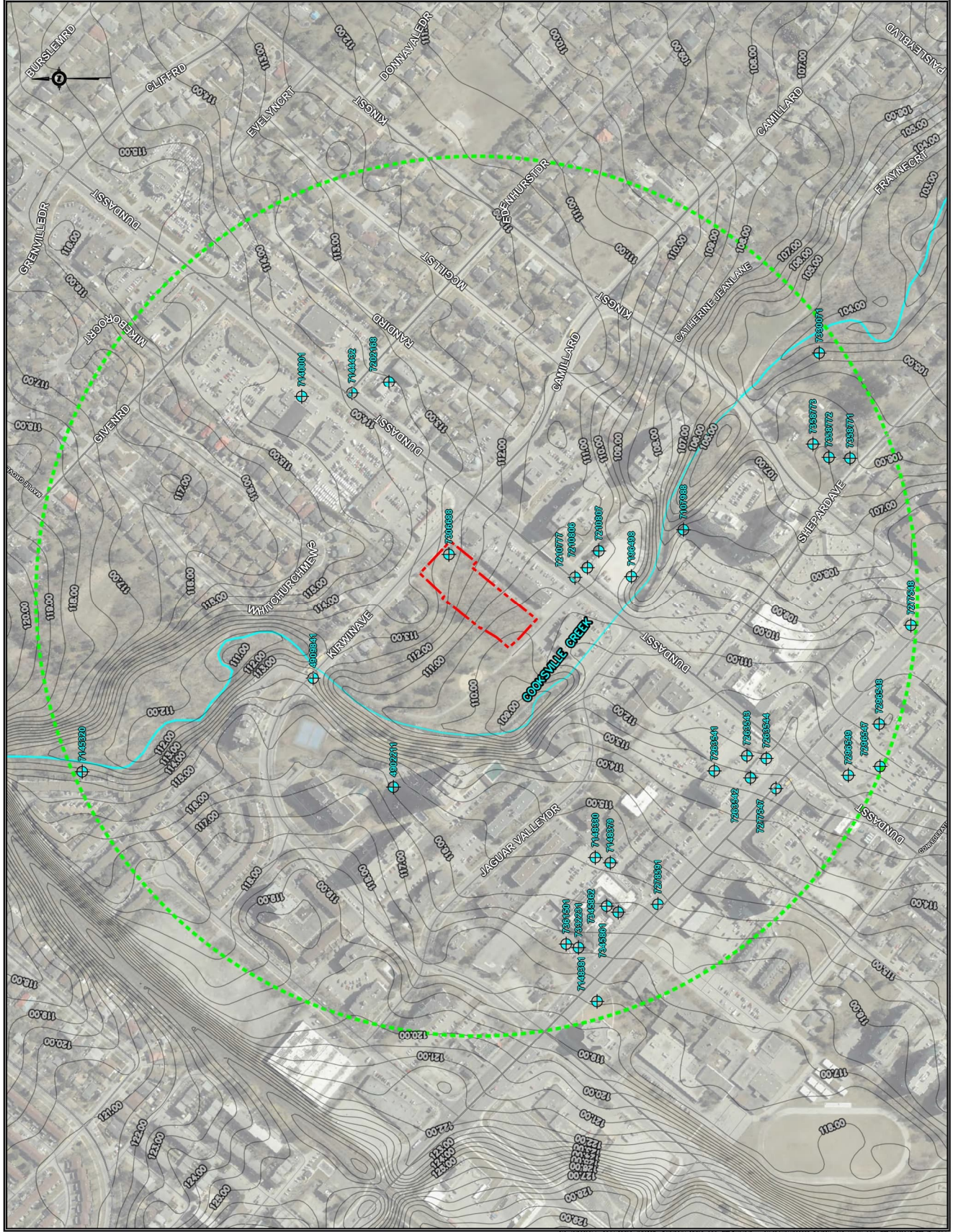


ENVIRONMENTAL ASSESSMENTS & APPROVALS

SITE LOCATION

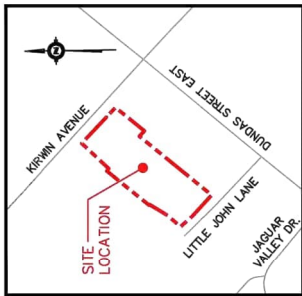
3016-3032 KIRWIN AVE.
MISSISSAUGA, ON

DATE ISSUED: JUNE 2022	Figure No.
CREATED BY: A.L.	1
PROJECT NO.: 22-056	
REFERENCE: CITY OF MISSISSAUGA	

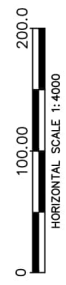


LEGEND:

- APPROX. PROPERTY BOUNDARY
- 500m RADIUS STUDY AREA
- WATERCOURSE (NDMNF, 2021)
- 0.5m CONTOUR (most: GTA DEM 2002)
- WATER WELL LOCATIONS / I.D.



LOCATION PLAN

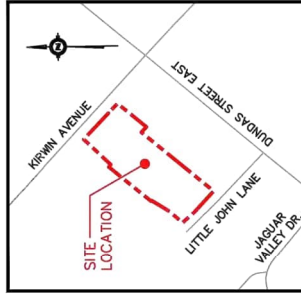


NATURAL FEATURES AND SURROUNDING WELLS	
3016-3032 KIRWIN AVE. MISSISSAUGA, ON	
DATE ISSUED: JUNE 2022	Figure No. 3
CREATED BY: A.L.	
PROJECT NO.: 22-056	
REFERENCE: CITY OF MISSISSAUGA	

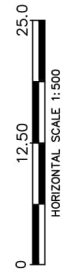


LEGEND:

- APPROX. PROPERTY BOUNDARY
- 100.00 0.5m CONTOURS (mmsl)
- INFERRED DIRECTION OF GROUND WATER FLOW



LOCATION PLAN



GROUND WATER CONTOURS

3016-3032 KIRWIN AVE.
MISSISSAUGA, ON

DATE ISSUED:	JUNE 2022	Figure No.	4
CREATED BY:	A.L.		
PROJECT NO.:	22-066		
REFERENCE:	CITY OF MISSISSAUGA		



APPENDIX B

Proposed Development Plan

PROPOSED 8 STOREY RENTAL BUILDING

3016 -3022 KIRWIN AVE, MISSISSAUGA, ON, CANADA

3016
KIRWIN AVE
3016-3022 Kirwin Avenue
Mississauga - ON - Canada

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DRAWING LIST:

Sheet Number	Sheet Name
A000	COVER PAGE
A001	SITE PLAN & STATS
A101	PARKING GARAGE LEVEL 2
A102	PARKING GARAGE LEVEL 1
A103	GROUND FLOOR
A104	2ND FLOOR PLAN
A105	3RD FLOOR PLAN
A106	4TH FLOOR PLAN
A107	5TH FLOOR PLAN
A108	6TH FLOOR PLAN
A109	7TH FLOOR PLAN
A110	8TH FLOOR PLAN
A111	MECHANICAL FLOOR PLAN
A112	ROOF PLAN
A201	EAST ELEVATION
A202	WEST ELEVATION
A203	NORTH ELEVATION
A204	SOUTH ELEVATION
A205	SECTION 1 E-W
A206	SECTION 2 N-S



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PROJECT NORTH

STAMP

CLIENT

DVB Real Estate
Investments Inc.



PROJECT NO:	20099
SCALE:	
DATE:	Feb. 14, 2020
DRAWN BY:	PCL
DRAWING TITLE:	

COVER PAGE

DRAWING NO

A000



TOPOGRAPHIC SURVEY OF
ALL OF LOTS 27 TO 30
REGISTERED PLAN NO. C-14
AND
PART OF LOT 5
REGISTERED PLAN TOR-12
CONCESSION 1,
HORNBY AVENUE STREET
RECONSTRUCTION (IN THE DISTRICT OF PEEL)
CITY OF MISSISSAUGA
REGIONAL MUNICIPALITY OF PEEL
SCALE 1:200
VAN HARTEN SURVEYING INC.

SURVEYOR'S CERTIFICATE

DATE OF SURVEY: 2018

REMARKS:

PROPERTY INFORMATION:

UNITARY:

LEGEND:

BEARING AND COORDINATE NOTE:

BEARING CONVERSIONS:

LEGEND:

CALL BEFORE YOU DIG

METRIC:

REGISTERED PLAN:

Van Harten
SURVEYING INC.
1000 SHEPPARD AVENUE EAST
SUITE 100
MISSISSAUGA, ONTARIO L4X 1L3
TEL: 905.276.1111
WWW.VANHARTENSURVEYING.COM



2 TOROCCADILIC ACIDIAL VIOLE



A001

KIRWIN AVE
3016-3022 Kirwin Avenue
Mississauga - ON - Canada

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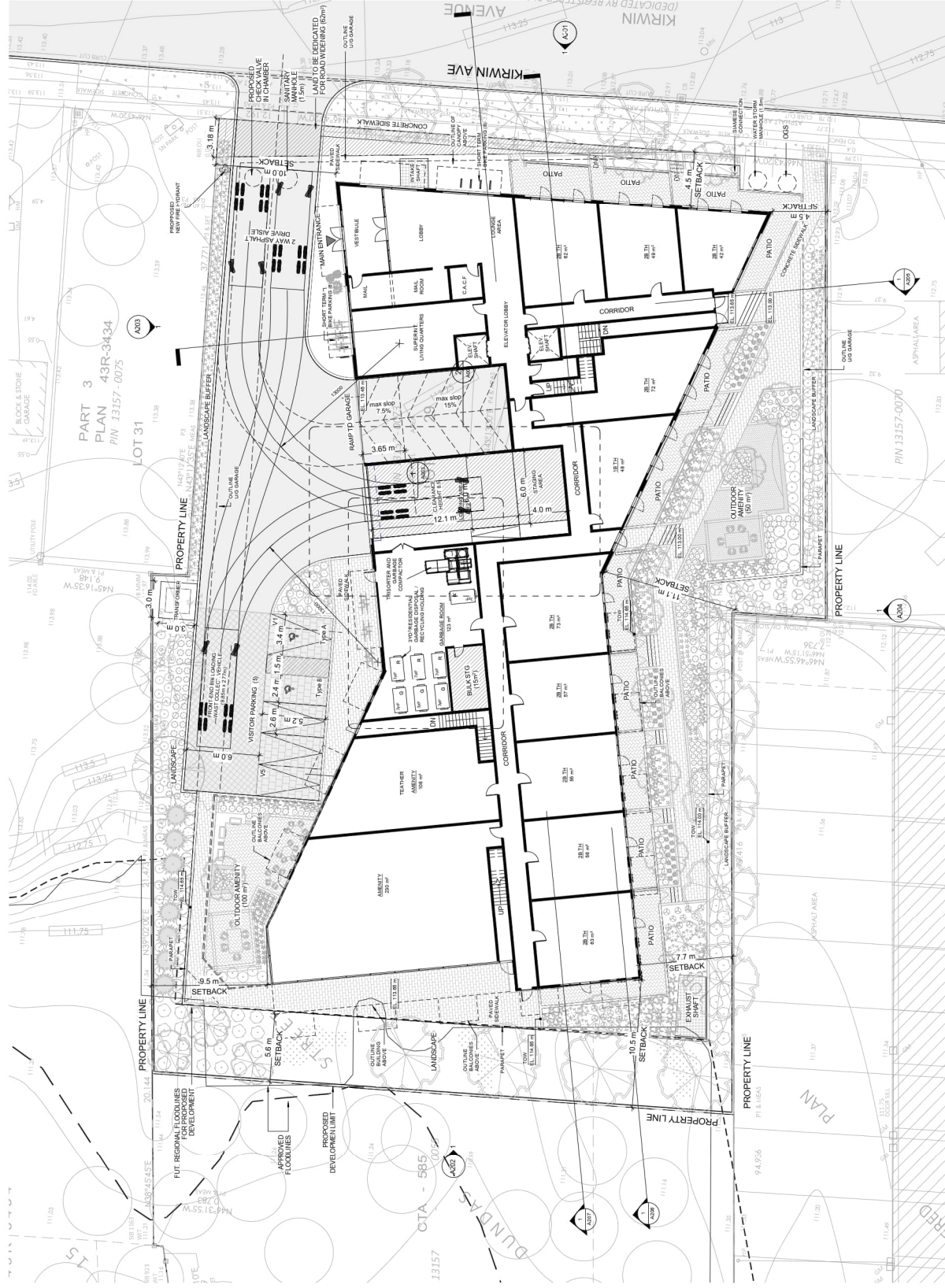
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Date:	Feb. 04, 2020
Drawn by:	FC
Drawing Title	

GROUND FLOOR

Drawing Number

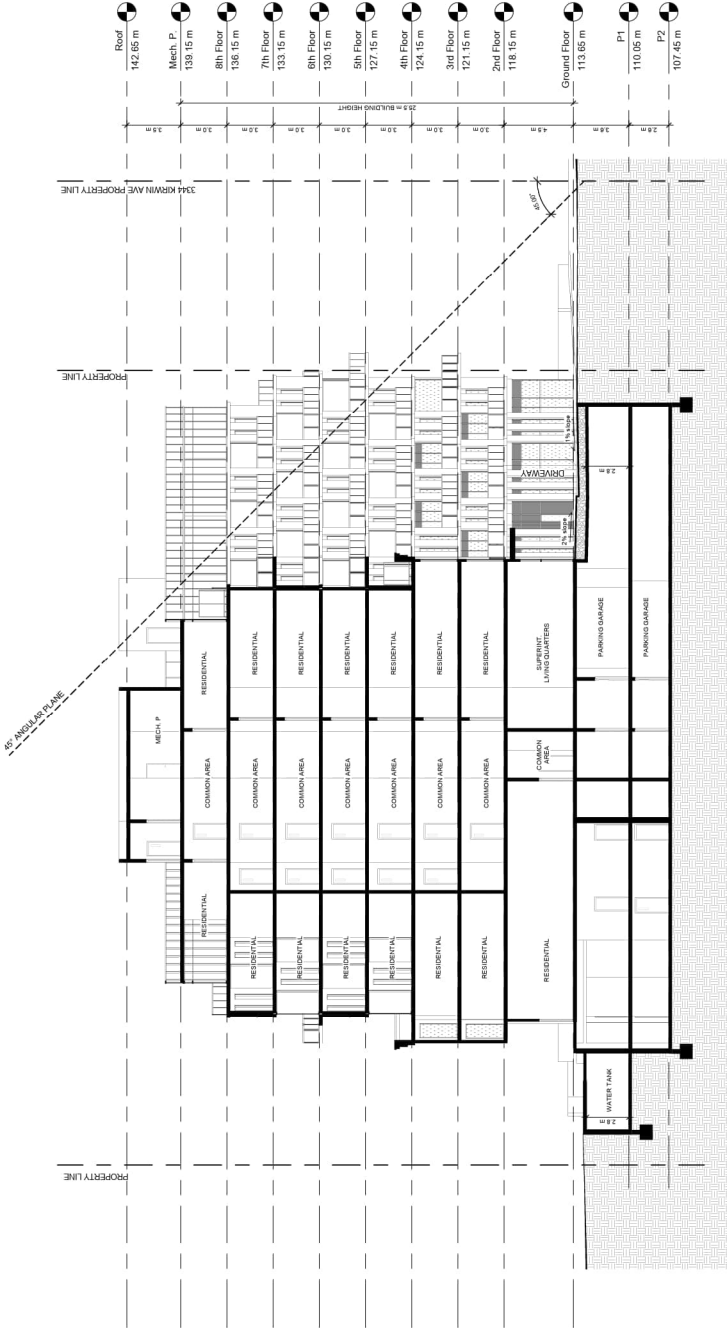
A103



3016
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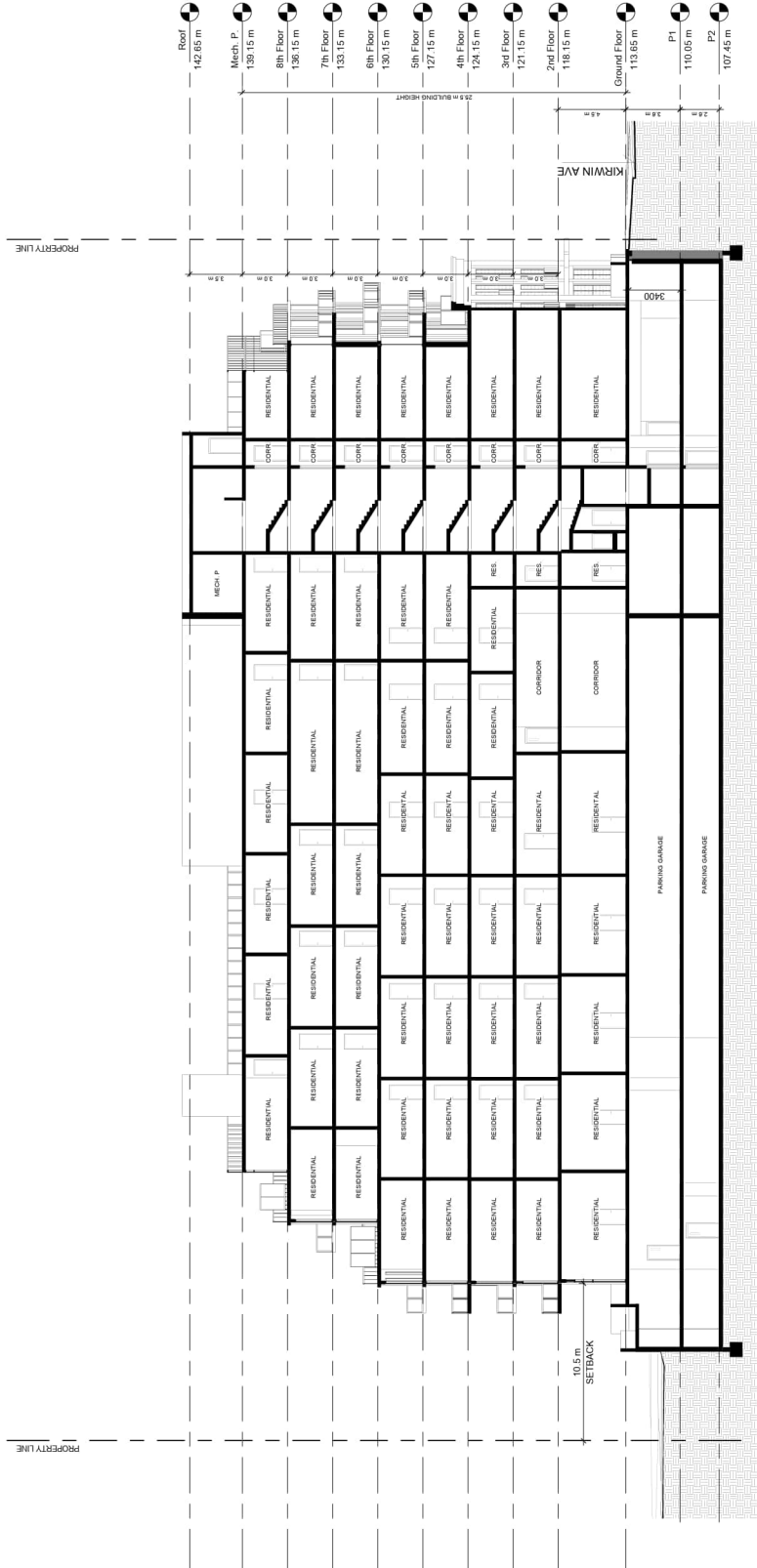
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Date Feb. 04, 2020
Drawn by FC
Drawing Title SECTION 1 E/W

Drawing Number
A205

3016
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Project No.	2009
Scale	1:150
Date	Feb. 04, 2009
Drawn by	FC
Drawing Title	

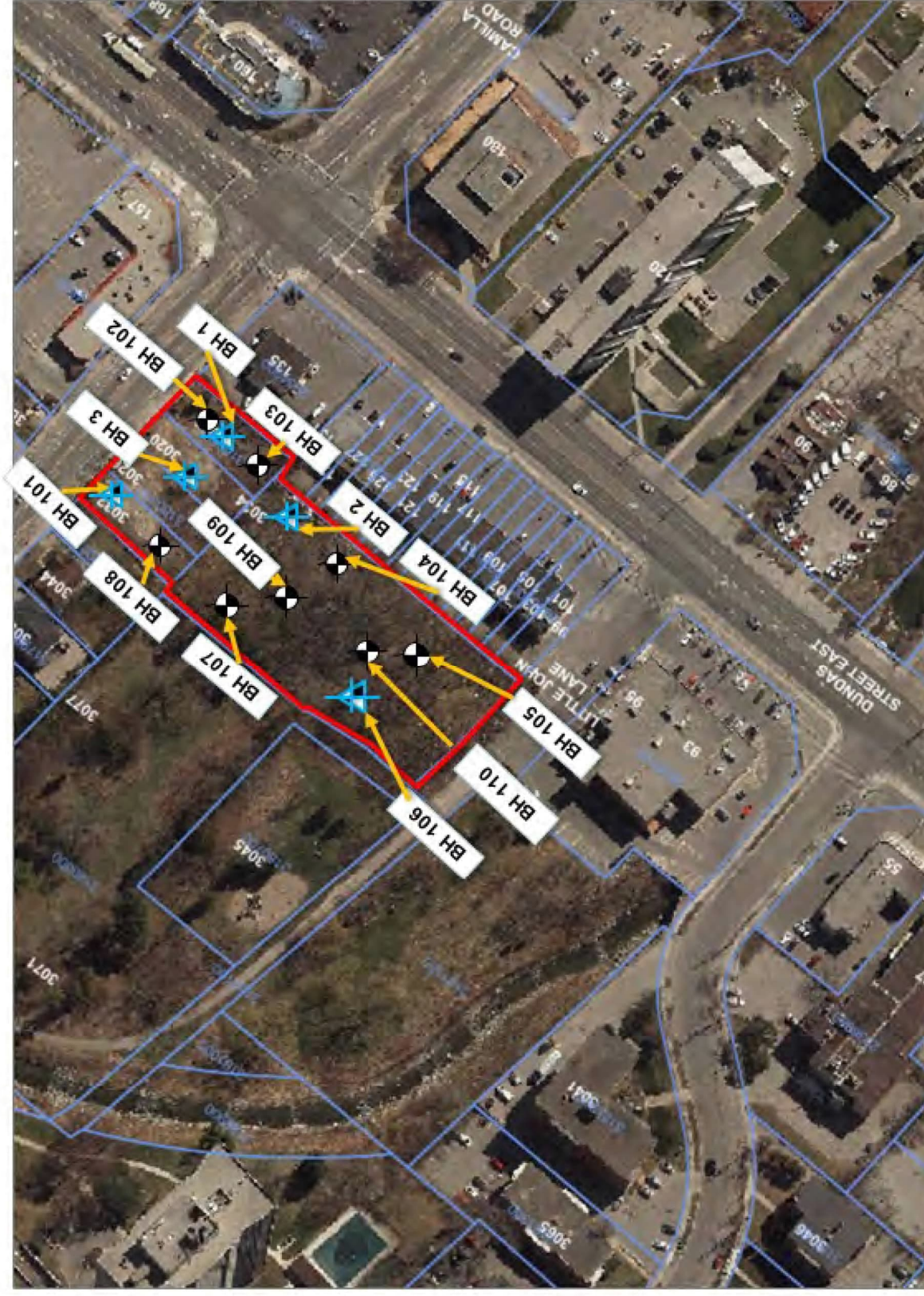
SECTION 2 N/S

A206



APPENDIX C

MECP Well Records & Site Borehole Logs



Approximate Location of Monitoring Well



Approximate location of Subject Property



Approximate location of Boreholes



Source: City of Mississauga Interactive Maps
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Title	Borehole Location Plan	Project No.	2202-001	Scale:	As drawn	Date:	April, 2022	Figure No.	4
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BH1

PROJECT NUMBER: 2012-001

PROJECT NAME: Phase Two ESA

CLIENT: DBV Real Estate Investments Inc.

ADDRESS: 3031 Littlejohn Ln and 3016, 3020, 3026, 3032 & 3034 Kirwin Av, Mississauga

UTM COORD. (m) 17 T611938 m E 4826562 m N **TOTAL WELL DEPTH:** 6.8 mbgs

HOLE SIZE/SAMPLING METHOD: 50 mm /SS **SURFACE ELEVATION:** 113.13 masl

RIG MODEL: Diedrich D-120

WELL SCREEN: 3.05 m; #10 Slot Screen

DRILLING METHOD: Spilt Spoon, Hollow Stem A **WATER LEVEL:** 4.46 mbgs

SAMPLING LENGTH: 0.762 m

COMMENTS : masl: meter above sea level - SS: Split-Spoon

LOGGED BY ST

CHECKED BY AT

Elevation (masl)	Depth (m)	Soil Sample ID	Sample Type	% Recovery	Soil Lab Analyses	Graphic Log	Material Description	HSVC as Isobutylene (ppm)	HSVC as Hexane (ppm)	Well Diagram
113	0	1	SS	0			100 mm Topsoil	0	0.0	
112.5	0.5						SILTY CLAY FILL, brown, some gravel, moist-wet, no odours & stains	0	0.0	
112	1	2	SS		PAHs, M&I			0	0.0	
111.5	1.5	3	SS				SILTY SAND FILL, brown, some gravel & cobbles, dry, no odours & stains	0	0.0	
111	2							0	0.0	
110.5	2.5	4	SS					0	0.0	
110	3	5	SS					0	0.0	
109.5	3.5							0	0.0	
109	4	6	SS		PHC, VOC, DUP-S1		SILTY CLAY, brown-grey, moist, some gravel & rocks, firm - stiff	0	0.0	
108.5	4.5	7A	SS					0	0.0	
108	5	7B						0	0.0	
107.5	5.5	8	SS				- grey, stiff to hard, weathered shale fragments	0	0.0	
107	6							0	0.0	
106.5	6.5	9	SS					0	0.0	
106	7							0	0.0	



BH2

PROJECT NUMBER: 2012-001

PROJECT NAME: Phase Two ESA

CLIENT: DBV Real Estate Investments Inc.

ADDRESS: 3031 Littlejohn Ln and 3016, 3020, 3026, 3032 & 3034 Kirwin Av, Mississauga

UTM COORD. (m) 17 T611938 m E 4826562 m N **TOTAL WELL DEPTH:** 6.06 mbgs

HOLE SIZE/SAMPLING METHOD: 50 mm /SS **SURFACE ELEVATION:** 112.56 masl

RIG MODEL: Diedrich D-120

WELL SCREEN: 3.05 m; #10 Slot Screen

DRILLING METHOD: Spilt Spoon, Hollow Stem A **WATER LEVEL:** 4.86 mbgs

SAMPLING LENGTH: 0.762 m

COMMENTS : masl: meter above sea level - SS: Split-Spoon

LOGGED BY ST

CHECKED BY AT

Elevation (masl)	Depth (m)	Soil Sample ID	Sample Type	% Recovery	Soil Lab Analyses	Graphic Log	Material Description	HSVC as Isobutylene (ppm)	HSVC as Hexane (ppm)	Well Diagram
112.5		1	SS				Topsoil and Asphalt			
	0.5						SILTY SAND FILL, brown, some gravel & cobbles, dry, no odours & stains	0	0.0	
112										
	1	2	SS		M&I			0	0.0	
111.5										
	1.5	3	SS					0	0.0	
111										
	2	4	SS					0	0.0	
110.5										
	2.5	5A	SS					0	0.0	
110										
	3	5B	SS					0	0.0	
109.5										
	3.5	6	SS		PHC, VOC		SILTY CLAY, grey, some organic, moist, soft-firm	0	0.0	
109										
	4	7	SS				- stiff to hard	0	0.0	
108.5							- weathered shale fragments	0	0.0	
	4.5	8	SS					0	0.0	
108										
	5									
107.5										
	5.5									
107										
	6									
106.5										
	6.5									
106										
	7									
105.5										



BH3

PROJECT NUMBER: 2012-001

PROJECT NAME: Phase Two ESA

CLIENT: DBV Real Estate Investments Inc.

ADDRESS: 3031 Littlejohn Ln and 3016, 3020, 3026, 3032 & 3034 Kirwin Av, Mississauga

UTM COORD. (m) 17 T611938 m E 4826562 m N **TOTAL WELL DEPTH:** 6.57 mbgs

HOLE SIZE/SAMPLING METHOD: 50 mm /SS **SURFACE ELEVATION:** 113.31 masl

RIG MODEL: Diedrich D-120

WELL SCREEN: 3.05 m; #10 Slot Screen

DRILLING METHOD: Spilt Spoon, Hollow Stem A **WATER LEVEL:** 4.48 mbgs

SAMPLING LENGTH: 0.762 m

COMMENTS : masl: meter above sea level - SS: Split-Spoon

LOGGED BY ST

CHECKED BY AT

Elevation (masl)	Depth (m)	Soil Sample ID	Sample Type	% Recovery	Soil Lab Analyses	Graphic Log	Material Description	HSVC as Isobutylene (ppm)	HSVC as Hexane (ppm)	Well Diagram
113	0.5	1	SS				100 mm Topsoil	0	0.0	
112.5	1	2	SS		M&I		SILTY SAND FILL, brown, some gravel & cobbles, dry, no odours & stains	0	0.0	
112	1.5	3	SS					0	0.0	
111.5	2	4	SS					0	0.0	
111	2.5	5	SS					0	0.0	
110.5	3	6	SS					0	0.0	
110	3.5	7A	SS					0	0.0	
109.5	4	7B	SS					0	0.0	
109	4.5	8	SS					0	0.0	
108.5	5	9	SS					0	0.0	
108	5.5							0	0.0	
107.5	6							0	0.0	
107	6.5							0	0.0	
106.5	7							0	0.0	
106										

AZURE GROUP DRAWING NO. 2

JOB NUMBER 2202-001BH101

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

C_u = Shear Strength (kPa) G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 1, 2022 Time: 8:55 am Sheet 1 of 1

Finished/Date April 1, 2022 Time: 5:30 pm

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 113.399 m G.W. Depth: 5.4 m G.W. Elevation: 107.13 m April 13, 2022 Time: 1 pm

Depth/Elev. (m)		Soil Description	Type/No	N	C_u (kPa)	G.W.T	Remark
0	113.4	250 mm Topsoil	SS	1	6		
		Soft to firm dark brown silty clay/clayey silt					
		trace sand, gravel, and organics					
.75	112.7		SS	2	5		
1.5	111.9		SS	3	5		
2.25	111.2	Compact SILTY SAND/SANDY SILT trace gravel, moist below 2.2 m	SS	4	37		
3.0	110.4		SS	5	36		
		Loose below 3.0 m, wet					
4.6	108.8	Stiff to very grayish brown stiff SILTY CLAY/CLAYEY SILT trace sand and gravel, wet below 4.0 m	SS	6	19		
						5.4 m	
6.1	107.9		SS	7	55		
		Hard grey CLAYEY SILT trace to some shale fragments below 6.0 m					
7.6	105.8		SS	8	>80		
8.2	105.2	Refusal at 8.2 m			>80		

EOB

AZURE GROUP DRAWING NO. 3

JOB NUMBER 2202-001BH102

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

C_u = Shear Strength (kPa) | G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 8, 2022 Time: 8:55 am Sheet 1 of 1

Finished/Date April 8, 2022 Time: 5:30 pm

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 113.094 m G.W. Depth: G.W. Elevation: Time:

Depth/Elev. (m)		Soil Description	Type/No	N	C_u (kPa)	G.W.T	Remark
0	113.1	250 mm Topsoil Soft to firm dark brown silty clay/clayey silt trace sand, gravel, and organics, moist	SS 1	8			
.75	112.4	Trace gravel, possible cobbles, moist below 0.7 m	SS 2	8			
1.5	111.6		SS 3	15			
		Compact SILTY SAND/SANDY SILT trace gravel, moist below 1.8 m					
2.25	110.9	Very dense SAND & GRAVEL below 2.2 m, moist (possible boulder)	SS 4	>80			
3.0	110.1	Very dense SAND & GRAVEL, moist below 3.0 m, possible cobbles	SS 5	66			
4.6	108.5	Compact SAND & GRAVEL trace clay, wet below 4.0 m	SS 6	22			
6.1	105.5	Hard grey SILTY CLAY/CLAYEY SILT trace shale fragments, wet below 6.0 m	SS 7	52			
7.6	105.5	Hard grey SILTY CLAY/CLAYEY SILT with SHALE fragments below 7.0 m	SS 8	>80			
		Hard weathered shale Below 9.0 M					
9.8	103.3	Refusal at 9.8 m	SS 9.8	>80			

EOB

AZURE GROUP DRAWING NO. 4

JOB NUMBER 2202-001BH103

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

C_u = Shear Strength (kPa) G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 8, 2022 Time: 4:45 am Sheet 1 of 1

Finished/Date April 8, 2022 Time: 6:30 pm

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 112.5 m G.W. Depth: G.W. Elevation: Time:

Depth/Elev. (m)		Soil Description	Type/No		N	C_u (kPa)	G.W.T	Remark
0	112.5	250 mm Topsoil	AS	1				
		Dark brown silty clay/clayey silt trace sand, gravel, and organics						
.75	111.8		AS	2				
1.5	111.0		AS	3				
2.25	110.3	SILTY SAND/SANDY SILT trace gravel, moist below 2.2 m	AS	4				
3.0	109.5		AS	5				
4.6	107.9	Stiff to very stiff SILTY CLAY/CLAYEY SILT trace sand and gravel, wet below 4.0 m	SS	6				
6.1	106.4	Hard CLAYEY SILT/SILTY CLAY trace gravel, wet below 6.0 m	SS	7	50			
7.6	104.9	Hard CLAYEY SILT/SILT below 7.0 m	SS	8	>80			
9.2	103.3	Refusal at 8.2 m	SS	9	>80			

EOB

AZURE GROUP DRAWING NO. 5

JOB NUMBER 2202-001BH104

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

C_u = Shear Strength (kPa) G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 7, 2022 Time: 3:10 am Sheet 1 of 1

Finished/Date April 7, 2022 Time: 6:30 pm

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 112.1 m G.W. Depth: G.W. Elevation: Time:

Depth/Elev. (m)		Soil Description	Type/No		N	C_u (kPa)	G.W.T	Remark
0	112.1	250 mm Topsoil Dark brown silty sand/sandy silt trace clay, gravel, and organics	AS	1				
.75	111.4	Dark brown SILTY CLAY trace gravel and organics below 0.7 m	AS	2				
1.5	110.6	Light brown CLAYEY SILT trace gravel below 1.5 m	AS	3				
2.25	109.9	SILTY CLAY/CLAYEY SILT, trace gravel, wet below 2.2 m	AS	4				
3.0	109.1	Hard CLAYEY SILT/SILTY CLAY below 3.0 m	AS	5				
4.6	107.5		AS	6				
6.1	106.0		SS	7	>80			
		Hard grey CLAYEY SILT/SILTY trace sand and gravel, wet below 6.0 m						
7.6	104.5		SS	7	>80			
9.2	102.9		SS	8	>80			
		Hard CLAYEY SILT with SHALE trace gravel below 9. M						
9.8	102.3	Refusal at 9.8 m	SS	9	>80			

EOB

AZURE GROUP DRAWING NO. 6

JOB NUMBER 2202-001BH105

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

C_u = Shear Strength (kPa) | G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 8, 2022 Time: Sheet 1 of 1

Finished/Date April 8, 2022 Time:

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 110.8 m G.W. Depth: G.W. Elevation: Time:

Depth/Elev. (m)		Soil Description	Type/No			C_u (kPa)	G.W.T	Remark
0	110.8	250 mm Topsoil Dark brown silty sand/sandy silt trace clay, gravel, and organics	AS	1				
.75	110.1	Sand trace clay and gravel below 0.75 m, moist to wet	AS	2				
1.5	109.3	SAND/SILTY SAND trace clay & GRAVEL, Wet below 1.5 m	AS	3				
2.25	108.6		AS	4				
3.0	107.8		AS	5				
4.6	106.2	Grey CLAYEY SILT, SILT trace sands below 4.6 m, wet	AS	6				
6.1	104.7	Very dense SILTY SAND/SANDY SILT trace Gravel and clay, wet below 6.0 m	SS	7	>80			
7.6	103.2		SS	8	>80			
9.2	101.6	Hard CLAYEY SILT with weathered SHALE below 9.0 m	SS	9	>80			
9.8	101.0	Refusal at 9.8 m	SS	10	>80			

EOB

AZURE GROUP DRAWING NO. 7

JOB NUMBER 2202-001BH(MW)106

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

C_u = Shear Strength (kPa) G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 8, 2022 Time: Sheet 1 of 1

Finished/Date April 8, 2022 Time:

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 110.78 m G.W. Depth: 2.69 m G.W. Elevation: 108.09 m Time:

Depth/Elev. (m)		Soil Description	Type/No	N	C_u (kPa)	G.W.T	Remark
0	110.8	250 mm Topsoil	SS	1			
		Dark brown SILTY SAND/SANDY SILT trace clay, gravel, and organics					
.75	110.1		SS	2			
1.5	109.3	CLAYEY SILT trace clay & GRAVEL, Wet below 1.5 m	SS	3			
2.25	108.6		SS	4			
3.0	107.8		SS	5		2.7 m	
4.6	106.2	Grey CLAYEY SILT trace gravel below, wet below 4.6 m	SS	6	225.0		
6.1	104.7	Hard grey CLAYEY SILT trace to some shale fragments, wet below 6.0 m	SS	7	>80	225.0	
7.6	103.2		SS	8	>80	225.0	
9.2	101.6	Hard grey CLAYEY SILT with weathered SHALE below 9.0 m, wet	SS	9	>80		
9.8	101.0	Refusal at 9.8 m	SS	10	>80		

EOB

AZURE GROUPDRAWING NO. 8**JOB NUMBER 2202-001BH(MW)107**

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

 C_u = Shear Strength (kPa) G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 8, 2022 Time: 11:45 Sheet 1 of 1

Finished/Date April 8, 2022 Time:

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 113.26 m G.W. Depth: G.W. Elevation: Time:

Depth/Elev. (m)		Soil Description	Type/No	N	C_u (kPa)	G.W.T	Remark
0	113.3	50 mm Asphalt	SS	1	5		
		Loose to very loose dark brown silty sand/sandy silt trace to some organics, gravel, and clay, moist					
.75	112.6		SS	2	7		
1.5	111.8	Compact below 1.5 m	SS	3	18		
2.25	111.1	Very dense below 2.2 m, possible boulders	SS	4	80		
3.0	110.3	Dense below 3.0 m, wet	SS	5	43		
4.6	108.7	Dense SILTY SAND/SAND possible boulders, wet below 4.0 m	SS	6	47		
6.1	107.2	Hard grey SILTY CLAY/CLAYEY SILT trace gravel, wet below 5.0 m	SS	7	47		
7.6	105.7	Hard grey weathered SHALE with hard SILTY CLAY	SS	8	>80		
9.2	104.1	Grey Weathered SHALE below 9.2 m	SS	9	>80		
10.7	102.6		SS	10	>80		
11.0	102.3	Refusal at 7.8 m	SS	11	>80		

EOB

AZURE GROUPDRAWING NO. 9**JOB NUMBER 2202-001BH108**

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

 C_u = Shear Strength (kPa) G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 8, 2022 Time: 8:00 am Sheet 1 of 1

Finished/Date April 8, 2022 Time:

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 113.28 m G.W. Depth: G.W. Elevation: Time:

Depth/Elev. (m)		Soil Description	Type/No		N	C_u (kPa)	G.W.T	Remark
0	113.3	250 mm Topsoil	AS	1				
		Dark brown SILTY SAND/SANDY SILT trace clay, gravel, and organics						
.75	112.6		AS	2				
1.5	111.8	Light brown SILTY SAND, trace clay and gravel, moist below 1.5 m,	AS	3	7			
2.25	111.1		AS	4				
3.0	110.3	Brown SILTY SAND with GRAVEL, moist below 3.0 m	AS	5	28			
4.6	108.7	Light brown SILTY SANDY/SANDY SILT trace to some clay and gravel, moist below 4.0 m	AS	6	25			
6.1	107.2	Hard CLAYEY SILT SILTY CLAY trace to some shale fragments, wet below 6.0 m	SS	7	45			
7.6	105.7	Grey weathered SHALE with SILTY CLAY trace gravel, moist below 7.0 m	SS	8	75			
9.2	104.1	Grey weathered SHALE with SILTY CLAY trace gravel, moist below 9.0 m	SS	9	>80			
10.7	102.6		SS	10	>80			
11.3	102.0	Refusal at 11.3 m	SS	11	>80			

EOB

AZURE GROUP DRAWING NO. 10

JOB NUMBER 2202-001BH109

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

C_u = Shear Strength (kPa) G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 8, 2022 Time: 8:50 am Sheet 1 of 1

Finished/Date April 8, 2022 Time:

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 112.5 m G.W. Depth: G.W. Elevation: Time:

Depth/Elev. (m)		Soil Description	Type/No	N	C_u (kPa)	G.W.T	Remark
0	112.5	250 mm Topsoil Dark brown SILTY SAND/SANDY SILT trace clay, gravel, and organics	AS				
.75	111.8		AS				
1.5	111.0	CLAYEY SILT trace clay & gravel, wet below 1.5 m	AS				
2.25	110.3		AS				
3.0	109.5		AS				
4.6	109.5	Grey CLAYEY SILT trace gravel below 4.6 m, wet below 4.0 m	AS				
6.1	106.4	Hard CLAYEY SILT/SILTY CLAY trace shale fragments, wet below 6.0 m	SS	>80			
7.6	104.9		SS	>80			
9.2	103.3	Hard CLAYEY SILT with weathered SHALE below 9.0 m, wet	SS	>80			
9.8	102.7	Refusal at 9.8 m	SS	>80			

EOB

AZURE GROUPDRAWING NO. 11**JOB NUMBER 2202-001BH110**

PROJECT LOCATION: 3016 – 3032 Kirwin Avenue & 3031 Little John Lane, Mississauga, Ontario

Client: Black Creek Group

 C_u = Shear Strength (kPa) G% = Gravel, S% = Sand, F% = Fines (Silt and Clay), M = Moisture Content

Temperature: 5°C

Started/Date April 8, 2022 Time: Sheet 1 of 1

Finished/Date April 8, 2022 Time:

Azure Rep: Amit Pal Auger Type: 150 mm Open

G. S. El: 110.88 m G.W. Depth: G.W. Elevation: Time:

Depth/Elev. (m)		Soil Description	Type/No		N	C_u (kPa)	G.W.T	Remark
0	110.9	250 mm Topsoil Dark brown SILTY SAND/SANDY SILT trace clay, gravel, and organics	AS	1				
.75	110.2		AS	2				
1.5	109.4	CLAYEY SILT trace sand & gravel, wet below 1.5 m	AS	3				
2.25	108.7		AS	4				
3.0	107.9	SILTY SAND/SANDY SILT, wet below 3.0 m	AS	5				
4.6	106.3	Grey CLAYEY SILT trace gravel below 4.6 m, wet below 4.0 m	AS	6		225.0		
6.1	104.8	Hard CLAYEY SILT trace to some gravels, wet below 6.0 m	SS	7	>80	225.0		
7.6	103.3	Hard grey CLAYEY SILT trace shale fragments below 7.5 m	SS	8	>80			
9.2	101.7	Hard grey CLAYEY SILT with weathered SHALE below 9.0 m, wet	SS	9	>80			
9.8	101.1	Refusal at 9.8 m	SS	10	>80			

EOB



A199313

Tag #: A199313

ROYAL BANK OF CANADA

Address of Well Location (Street Number/Name) 2 Dundas Street West		Township Mississauga	Lot	Concession
County/District/Municipality		City/Town/Village	Province Ontario	Postal Code
UTM Coordinates Zone - Easting NAD 83 11 17 011 692 482 61 27		Municipal Plan and Sublot Number		Other WKQ-010354 A 0 - A 02

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft) From To
Black	asphalt			0 3"
Brown	clay	silt		3' 10'
Grey	shale			10' 14'

Annular Space			Results of Well Yield Testing			
Depth Set at (m/ft) From To	Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)	After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify	Draw Down Time (min) Water Level (m/ft)	Recovery Time (min) Water Level (m/ft)	Static Level
0 6"	Concrete			1	1	
6" 3'	Grout			2	2	
3' 14'	Sand			3	3	
				4	4	
				5	5	
				10	10	
				15	15	
				20	20	
				25	25	
				30	30	
				40	40	
				50	50	
				60	60	

Method of Construction	Well Use
<input type="checkbox"/> Cable Tool <input checked="" type="checkbox"/> Rotary (Conventional) <input type="checkbox"/> Rotary (Reverse) <input type="checkbox"/> Boring <input type="checkbox"/> Air percussion <input checked="" type="checkbox"/> Other, specify Direct Push	<input type="checkbox"/> Public <input type="checkbox"/> Commercial <input type="checkbox"/> Not used <input type="checkbox"/> Domestic <input type="checkbox"/> Municipal <input type="checkbox"/> Dewatering <input type="checkbox"/> Livestock <input type="checkbox"/> Test Hole <input type="checkbox"/> Monitoring <input type="checkbox"/> Irrigation <input type="checkbox"/> Cooling & Air Conditioning <input type="checkbox"/> Industrial <input type="checkbox"/> Other, specify

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft) From To		
2"	PVC	2.25	0 4'	<input type="checkbox"/> Water Supply <input type="checkbox"/> Replacement Well <input type="checkbox"/> Test Hole <input type="checkbox"/> Recharge Well <input type="checkbox"/> Dewatering Well <input type="checkbox"/> Observation and/or Monitoring Hole <input type="checkbox"/> Alteration (Construction) <input type="checkbox"/> Abandoned, Insufficient Supply <input type="checkbox"/> Abandoned, Poor Water Quality <input type="checkbox"/> Abandoned, other, specify <input type="checkbox"/> Other, specify	

Construction Record - Screen				Status of Well	
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft) From To		
2.25	PVC	10	4' 14'	<input type="checkbox"/> Water Supply <input type="checkbox"/> Replacement Well <input type="checkbox"/> Test Hole <input type="checkbox"/> Recharge Well <input type="checkbox"/> Dewatering Well <input type="checkbox"/> Observation and/or Monitoring Hole <input type="checkbox"/> Alteration (Construction) <input type="checkbox"/> Abandoned, Insufficient Supply <input type="checkbox"/> Abandoned, Poor Water Quality <input type="checkbox"/> Abandoned, other, specify <input type="checkbox"/> Other, specify	

Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft) From To	Diameter (cm/in)
		0 14'	6"

Business Name of Well Contractor Strata Soil Sampling Inc.		Well Contractor's Licence No. 7 2 4 1	
Business Address (Street Number/Name) 165 Shields Court		Municipality Markham	
Province Ontario	Postal Code L3R 8V2	Business E-mail Address wrecords@stratasoil.com	
Bus. Telephone No. (inc. area code) 905-764-9304		Name of Well Technician (Last Name, First Name) Vanderhoof, Andrew	
Well Technician's Licence No. 36124		Signature of Technician and/or Contractor Andrew Vanderhoof	
Date Submitted 20170929		Date Package Delivered 20170912	

Map of Well Location

Please provide a map below following instructions on the back.

See Map

"C"

Comments: General contractor:
Pinchin Environmental

Well owner's information package delivered <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	Date Package Delivered 20170912	Ministry Use Only Audit No. 2270105 OCT 11 5 2017
Date Work Completed 20170912	Received	

S - 20827



*03-C "WP03-C"
added
17 T 611692 4826127
43.57974°N -79.61661°E
Elevation= 112.4m

*02-B "WP02-B"
added
17 T 611750 4826092
43.57942°N -79.61590°E
Elevation= 111.1m

*01-A "WP01-A"
added
17 T 611702 4826091
43.57942°N -79.61650°E
Elevation= 112.0m

**all waypoints removed...

C-7241
7270105

OCT 05 2017

Map data ©2017 Google Imagery ©2017, DigitalGlobe, First Base Solutions

<https://www.geoplaner.com/>

13/09/2017



Ontario

Ministry of the Environment
and Climate ChangeMeasurements recorded in: ☐ Metric ☒ Imperial

SOIL ON 4 IN 1709-5004

Well Tag No. (Place Sticker and/or Print Below)

A 223241

Well Record

Regulation 903 Ontario Water Resources Act

Page 1 of 1

Well Owner's Information

First Name	Last Name Organization NYX CAPITAL CORP.	E-mail Address	<input type="checkbox"/> Well Constructed by Well Owner
Mailing Address (Street Number/Name)	Municipality	Province	Postal Code
1131A LESLIE ST., Ste. 201	Toronto	Ontario	M3C 3L8
Telephone No. (inc. area code)		416 548 5590	

Well Location

Address of Well Location (Street Number/Name)	Township	Lot	Concession
3032 KIRWIN DR.			
County/District/Municipality	City/Town/Village	Province	Postal Code
	MISSISSAUGA	Ontario	
UTM Coordinates Zone	Easting	Northing	Municipal Plan and Sublot Number
NAD 83	176111	9434826580	
Other			

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m)
Brown	Earth Fill, silty clay and sand	Some Silt	Loose - Compact	0 12.5
Brown	Fine-Medium Sand	Tr. Silt, Some Grav	Compact	12.5 15
Grey	Silty Clay, Till	Some Sand, Tr. Gravel, Occ. Silt layers, cobbles/Boulders	Hard	15 25

Annular Space			Results of Well Yield Testing				
Depth Set at (m)	Type of Sealant Used (Material and Type)	Volume Placed (m ³)	After test of well yield, water was:	Draw Down		Recovery	
0 13	Bentonite	2.31	<input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify	Time (min)	Water Level (m)	Time (min)	Water Level (m)
			If pumping discontinued, give reason:	Static Level			
			Pump intake set at (m)	1		1	
			Pumping rate (l/min / GPM)	2		2	
			Duration of pumping hrs + min	3		3	
			Final water level end of pumping (m)	4		4	
			If flowing give rate (l/min / GPM)	5		5	
			Recommended pump depth (m)	10		10	
			Recommended pump rate (l/min / GPM)	15		15	
			Well production (l/min / GPM)	20		20	
			Disinfected?	25		25	
			<input type="checkbox"/> Yes <input type="checkbox"/> No	30		30	
				40		40	
				50		50	
				60		60	

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool <input checked="" type="checkbox"/> Rotary (Conventional) <input type="checkbox"/> Rotary (Reverse) <input type="checkbox"/> Boring <input type="checkbox"/> Air percussion <input type="checkbox"/> Other, specify	<input type="checkbox"/> Diamond <input type="checkbox"/> Jetting <input type="checkbox"/> Driving <input type="checkbox"/> Digging	<input type="checkbox"/> Public <input type="checkbox"/> Domestic <input type="checkbox"/> Livestock <input type="checkbox"/> Irrigation <input type="checkbox"/> Industrial <input type="checkbox"/> Other, specify	<input type="checkbox"/> Commercial <input type="checkbox"/> Municipal <input checked="" type="checkbox"/> Test Hole <input type="checkbox"/> Cooling & Air Conditioning <input type="checkbox"/> Not used <input type="checkbox"/> Dewatering <input type="checkbox"/> Monitoring

Construction Record - Casing				Status of Well	
Inside Diameter (cm)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm)	Depth (m)		
2	PVC	1/8	0 15	<input type="checkbox"/> Water Supply <input type="checkbox"/> Replacement Well <input checked="" type="checkbox"/> Test Hole <input type="checkbox"/> Recharge Well <input type="checkbox"/> Dewatering Well <input checked="" type="checkbox"/> Observation and/or Monitoring Hole <input type="checkbox"/> Alteration (Construction) <input type="checkbox"/> Abandoned, Insufficient Supply <input type="checkbox"/> Abandoned, Poor Water Quality <input type="checkbox"/> Abandoned, other, specify <input type="checkbox"/> Other, specify	

Construction Record - Screen			
Outside Diameter (cm)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m)
2 1/8	PVC	10	15 25

Water Details		Hole Diameter	
Water found at Depth (m)	Kind of Water: <input type="checkbox"/> Fresh <input checked="" type="checkbox"/> Untested	Depth (m)	Diameter (cm)
12.5	<input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	0 25	6
Water found at Depth (m)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested		
(m)	<input type="checkbox"/> Gas <input type="checkbox"/> Other, specify		
Water found at Depth (m)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested		
(m)	<input type="checkbox"/> Gas <input type="checkbox"/> Other, specify		

Well Contractor and Well Technician Information			
Business Name of Well Contractor	Well Contractor's Licence No.		
Strongly Soil Search Inc.	71 247		
Business Address (Street Number/Name)	Municipality		
5265 SIOUXE 16	CLAREMONT		
Province	Postal Code	Business E-mail Address	
Ontario	L1Y 1A1	strongsoilsearchinc@bell.net.ca	

Bus. Telephone No. (inc. area code)	Name of Well Technician (Last Name, First Name)	Well owner's information package delivered	Date Package Delivered	Ministry Use Only	
905 649 1115	NETO, NELSON	<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	Y Y Y Y M M D D	Audit No.	2272465
Well Technician's Licence No.	Signature of Technician and/or Contractor	Date Work Completed	20170903	MAR 02 2018	
3 174	[Signature]			Received	

Map of Well Location

Please provide a map below following instructions on the back.

N ←

KIRWIN DR.

← DUNDAS ST.

61074 LOT / PARCELS

Comments: 3 well clusters

230002

Geoplaner V2.8 - [in English | auf Deutsch]
dd.ddd44°



MAR 15 20:9

230002

Notice of Collection of Personal Information

Personal information contained on this form is collected pursuant to sections 35-50 and 75(2) of the *Ontario Water Resources Act* and section 16.3 of the Wells Regulation. This information will be used for the purpose of maintaining a public record of wells in Ontario. This form and the information contained on the form will be stored in the Ministry's well record database and made publicly available. Questions about this collection should be directed to the Water Well Customer Service Representative at the Wells Help Desk, 125 Resources Road, Toronto Ontario M9P 3V6, at 1-888-396-9355 or wellshelpdesk@ontario.ca.

Fields marked with an asterisk (*) are mandatory.

Well Tag Number *

A246265

Type *

☒ Construction ☐ Abandonment

Measurement recorded in: *

☒ Metric ☐ Imperial

1. Well Owner's Information

Last Name and First Name, or Organization is mandatory. *

Last Name First Name

Organization Email Address

EQUITY THREE HOLDINGS INC./EOB LTD.

Current Address

Unit Number Street Number * Street Name * City/Town/Village

Country Province Postal Code Telephone Number

CANADA

ONTARIO

2. Well Location

Address of Well Location

Unit Number Street Number * Street Name * Township

3085 HURONTARIO ST.

Lot Concession County/District/Municipality

PEEL

City/Town Province Postal Code

MISSISSAUGA

Ontario

L5A 4E4

UTM Coordinates Zone * Easting * Northing * Municipal Plan and Sublot Number

NAD 83

17

611496

4826433

Test UTM in Map

Other

BH 2

3. Overburden and Bedrock Material *

Well Depth * 4.5 (m)

General Colour	Most Common Material	Other Materials	General Description	Depth From (m)	Depth To (m)
Black		Asphalt		0	0.1
Grey	Gravel			0.1	0.3

Brown	Sand			0.3	1.5
Brown	Silt	Clay		1.5	2.1
Grey	Shale		Weathered	2.1	4.5

4. Annular Space *

Depth From (m)	Depth To (m)	Type of Sealant Used (Material and Type)	Volume Placed (cubic metres)
0	0.3	CONCRETE	0.01
0.3	2.7	BENTONITE CHIPS	0.08

5. Method of Construction *

- ☐ Cable Tool ☐ Rotary (Conventional) ☐ Rotary (Reverse) ☒ Boring ☐ Air percussion ☐ Diamond
☐ Jetting ☐ Driving ☐ Digging ☐ Rotary (Air) ☐ Augering ☐ Direct Push
☐ Other (specify) _____

6. Well Use *

- ☐ Public ☐ Industrial ☐ Cooling & Air Conditioning
☐ Domestic ☐ Commercial ☐ Not Used
☐ Livestock ☐ Municipal ☒ Monitoring
☐ Irrigation ☒ Test Hole ☐ Dewatering
☐ Other (specify) _____

7. Status of Well *

- ☐ Water Supply ☐ Replacement Well ☐ Test Hole
☐ Recharge Well ☐ Dewatering Well ☒ Observation and/or Monitoring Hole
☐ Alteration (Construction) ☐ Abandoned, Insufficient Supply ☐ Abandoned, Poor Water Quality
☐ Abandoned, other (specify) _____
☐ Other (specify) _____

8. Construction Record - Casing * (use negative number(s) to indicate depth above ground surface)

Inside Diameter (cm)	Open Hole or Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness	Depth From (m)	Depth To (m)
5.1	Plastic	0.65	0	3

9. Construction Record - Screen

Outside Diameter (cm)	Material (Plastic, Galvanized, Steel)	Slot Number	Depth From (m)	Depth To (m)
6.4	Plastic	10	3	4.5

10. Water Details

Water found at Depth (m) ☐ Gas Kind of Water ☐ Fresh ☒ Untested ☐ Other (specify)

11. Hole Diameter

Depth From (m)	Depth To (m)	Diameter (cm)
0	4.5	21

12. Results of Well Yield Testing

☐ Pumping Discontinued

Explain _____

If flowing give rate

☐ Flowing _____ (L/min)

Draw down *

Time (min)	Static Level	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (m)														

Recovery *

Time (min)	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (m)													

After test of well yield, water was

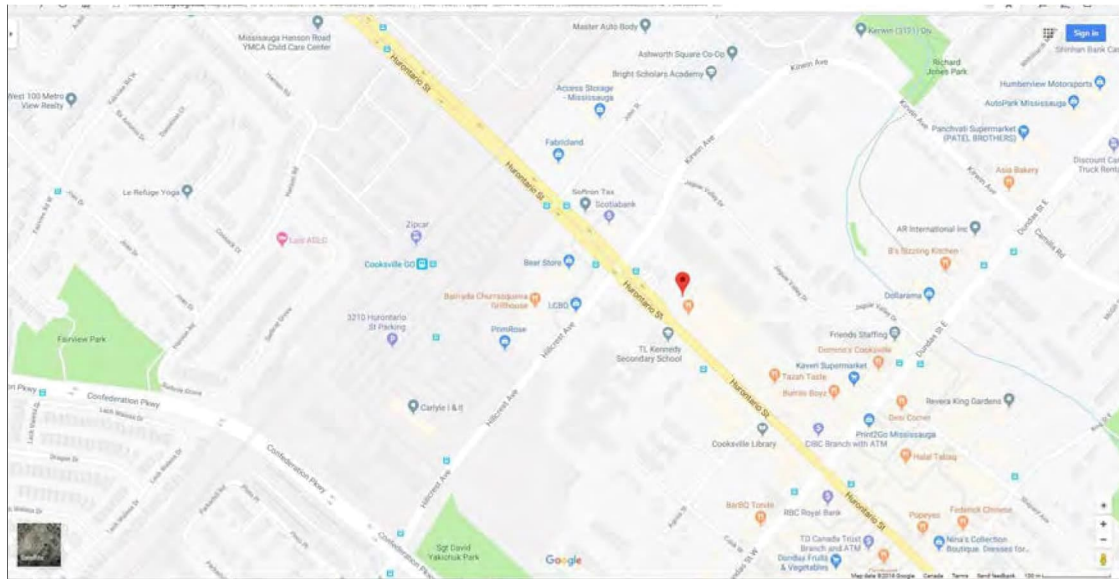
☐ Clear and sand free ☐ Other (specify)

Pump intake set at (m)	Pumping rate (L/min)	Duration of pumping hrs + min	Final water level end of pumping (m)	Disinfected? * <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
Recommended pump depth (m)	Recommended pump rate (L/min)	Well production (L/min)		

13. Map of Well Location *

Map 1. Please Click the map area below to import an image file to use as the map.

☐ Make map area bigger



14. Information

Well owner's information package delivered <input type="checkbox"/> Yes <input type="checkbox"/> No	Date Package Delivered (yyyy/mm/dd)	Date Work Completed (yyyy/mm/dd) *
		2019/04/08
Comments		

15. Well Contractor and Well Technician Information

Business Name of Well Contractor *		Well Contractor's License Number *	
Geo-Environmental Drilling Inc.		6607	
Business Address			
Unit Number	Street Number	Street Name *	
	1	Mansewood Court	
City/Town/Village *		Province	Postal Code *
Halton Hills		Ontario	L7J 0A1
Business Telephone Number		Business Email Address	
905-876-3388		dgunn@geo-environmentaldrilling.com	
Last Name of Well Technician *		First Name of Well Technician *	Well Technician's License Number *
PAQUETTE		JEFF	2386

16. Declaration *

☒ I hereby confirm that I am the person who constructed the well and I hereby confirm that the information on the form is correct and accurate.

Last Name	First Name	Email Address
PAQUETTE	JEFF	romana@geo-environmentaldrilling.com
Signature		Date Submitted (yyyy/mm/dd)
Jeff Paquette Digitally signed by Jeff Paquette Date: 2019.05.09 14:56:02 -04'00'		2019/05/09

17. Ministry Use Only

Audit Number
BALY VF8S

Measurements recorded in: ☐ Metric ☒ Imperial

A291838 Tag#:A291838

Page of

Well Owner's Information

First Name	Last Name / Organization		E-mail Address		<input type="checkbox"/> Well Constructed by Well Owner	
	City of Mississauga					
Mailing Address (Street Number/Name)		Municipality	Province	Postal Code	Telephone No. (inc. area code)	
300 City Centre Dr		Miss	ON	L5B3C1		

Well Location

Address of Well Location (Street Number/Name) 2515 Shepard Ave						Township	Lot	Concession
County/District/Municipality						City/Town/Village M ^c Ssenga	Province Ontario	Postal Code L5A2H7
UTM Coordinates		Zone	Easting	Northing	Municipal Plan and Sublot Number	Other		
NAD 83		17	120618	4836167				

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft)	
				From	To
Brown	Sand			0	3
Brown	Silt	Sand		3'	14'
Grey	Silt	Sand		14'	18

Annular Space

Depth Set at (m/ft) From	To	Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)
0	5'	concrete	
5'	7'	hole plug	
7'	18'	sand	

Method of Construction

<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial	<input type="checkbox"/> Not used
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input checked="" type="checkbox"/> Municipal	<input type="checkbox"/> Dewatering
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input checked="" type="checkbox"/> Test Hole	<input checked="" type="checkbox"/> Monitoring
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning	
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial		
<input checked="" type="checkbox"/> Other, specify <i>Dist. Prod.</i>		<input type="checkbox"/> Other, specify _____		

Well Use

☐ Public ☐ Commercial ☐ Not used
☐ Domestic ☐ Municipal ☐ Dewatering
☐ Livestock ☒ Test Hole ☒ Monitoring
☐ Irrigation ☐ Cooling & Air Conditioning
☐ Industrial
☐ Other, *specify* _____

Construction Record - Casing

Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft)		<input type="checkbox"/> Water Supply <input type="checkbox"/> Replacement Well <input checked="" type="checkbox"/> Test Hole <input type="checkbox"/> Recharge Well <input type="checkbox"/> Dewatering Well <input checked="" type="checkbox"/> Observation and/or Monitoring Hole <input type="checkbox"/> Alteration (Construction) <input type="checkbox"/> Abandoned, Insufficient Supply
			From	To	
2"	PVC	.125	0	8'	

Status of Well

☐ Water Supply
☐ Replacement Well
☒ Test Hole
☐ Recharge Well
☐ Dewatering Well
☒ Observation and/or Monitoring Hole
☐ Alteration (Construction)
☐ Abandoned, Insufficient Supply
☐ Abandoned, Poor Water Quality
☐ Abandoned, other *specify*
☐ Other, *specify*

Construction Record - Screen

Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft)	
			From	To
2.25"	PVC	10	8'	18'

Water Details

Water found at Depth _____ (m/ft) <input type="checkbox"/> Gas	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Other, specify _____
Water found at Depth _____ (m/ft) <input type="checkbox"/> Gas	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Other, specify _____
Water found at Depth _____ (m/ft) <input type="checkbox"/> Gas	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Other, specify _____

Hole Diameter

Depth (m/ft)		Diameter (cm/in)
From	To	
0	18'	6"

Well Contractor and Well Technician Information

Business Name of Well Contractor Strata Soil Sampling		Well Contractor Licence No. 7241
Business Address (Street Number/Name) 129 Ringwood Drive		Municipality Stouffville
Province ON	Postal Code L4A8C1	Business E-mail Address wrecord@stratasoil.com
Bus. Telephone No. (For use only) 9059407919		Name of Well Technician (Last Name, First Name) Kyle R. L.
Well Technician's Licence No. Signature of Technician and/or Contractor 3459		Date Submitted 20200130

Results of Well Yield Testing

After test of well yield, water was:	Draw Down		Recovery	
	Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
<input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify _____	Static Level			
If pumping discontinued, give reason:	1		1	
Pump intake set at (m/ft)	2		2	
Pumping rate (l/min / GPM)	3		3	
Duration of pumping _____ hrs + _____ min	4		4	
Final water level end of pumping (m/ft)	5		5	
If flowing give rate (l/min / GPM)	10		10	
Recommended pump depth (m/ft)	15		15	
Recommended pump rate (l/min / GPM)	20		20	
Well production (l/min / GPM)	25		25	
Disinfected?	30		30	
<input type="checkbox"/> Yes <input type="checkbox"/> No	40		40	
	50		50	
	60		60	

Map of Well Location

Please provide a map below following instructions on the back.

See Map
MWC

Comments:

Well owner's
information
package
delivered

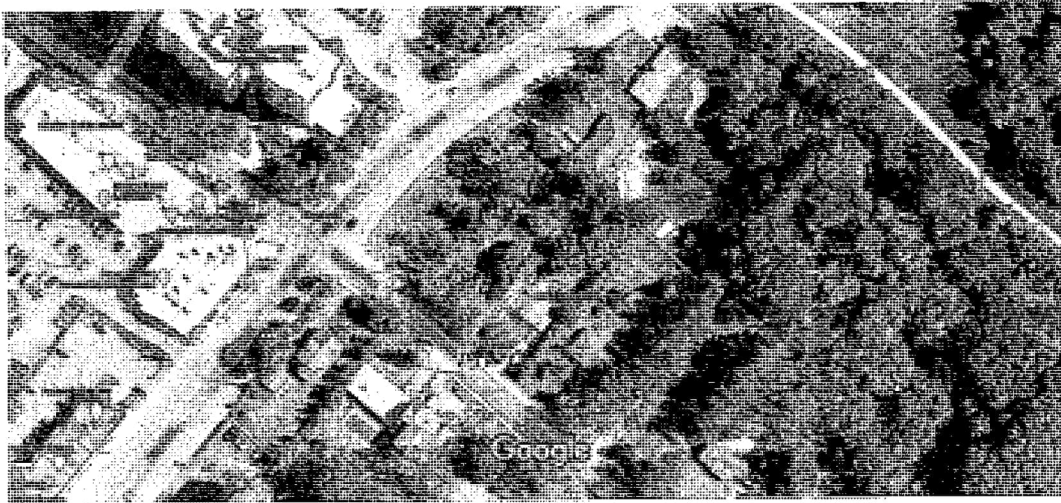
Date Package Delivered									
Y	Y	Y	Y	M	M	D	D		

Ministry Use Only

Audit No. **Z334740**

MAY 20 2020
Received

Google Maps 2515 Shepard Ave



Imagery ©2020 First Base Solutions, Maxar Technologies, Map data ©2020 20 m

C-7241
733740

MAY 20 2020

<https://www.google.ca/maps/place/2515+Shepard+Ave,+Mississauga,+ON+L5A+2H7/@...> 29/04/2020

Notice of Collection of Personal Information

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Fields marked with an asterisk (*) are mandatory.

Well Tag Number *

A 308294

Type *

☒ Construction ☐ Abandonment

Measurement recorded in: *

☐ Metric ☒ Imperial

1. Well Owner's Information

Last Name and First Name, or Organization is mandatory. *

Last Name | First Name

Organization | Email Address

Emblem Developments

Current Address

Unit Number | Street Number * | Street Name * | City/Town/Village

Country | Province | Postal Code | Telephone Number

2. Well Location

Address of Well Location

Unit Number | Street Number * | Street Name * | Township

90 | Dundas Street East

Lot | Concession | County/District/Municipality

City/Town | Province | Postal Code

Mississauga

UTM Coordinates | Zone * | Easting * | Northing * | Municipal Plan and Sublot Number

NAD 83 | 17 | 611907 | 4826370 | Test UTM in Map

Other

3. Overburden and Bedrock Material *

Well Depth * | 20 | (ft)

General Colour | Most Common Material | Other Materials | General Description | Depth From | Depth To

				(ft)	(ft)
Brown	Fill		Loose	0	15
Grey	Clay	Till	Packed	15	20

4. Annular Space *

Depth From (ft)	Depth To (ft)	Type of Sealant Used (Material and Type)	Volume Placed (cubic feet)
0	9	Bentonite	1.5
9	20	Sand Pack	1.8

5. Method of Construction *

- ☐ Cable Tool ☐ Rotary (Conventional) ☐ Rotary (Reverse) ☐ Boring ☐ Air percussion ☐ Diamond
☐ Jetting ☐ Driving ☐ Digging ☐ Rotary (Air) ☒ Augering ☐ Direct Push
☐ Other (specify) _____

6. Well Use *

- ☐ Public ☐ Industrial ☐ Cooling & Air Conditioning
☐ Domestic ☐ Commercial ☐ Not Used
☐ Livestock ☐ Municipal ☒ Monitoring
☐ Irrigation ☐ Test Hole ☐ Dewatering
☐ Other (specify) _____

7. Status of Well *

- ☐ Water Supply ☐ Replacement Well ☐ Test Hole
☐ Recharge Well ☐ Dewatering Well ☒ Observation and/or Monitoring Hole
☐ Alteration (Construction) ☐ Abandoned, Insufficient Supply ☐ Abandoned, Poor Water Quality
☐ Abandoned, other (specify) _____
☐ Other (specify) _____

8. Construction Record - Casing * (use negative number(s) to indicate depth above ground surface)

Inside Diameter (in)	Open Hole or Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness	Depth From (ft)	Depth To (ft)
2	Plastic	0.2	0	10

9. Construction Record - Screen

Outside Diameter (in)	Material (Plastic, Galvanized, Steel)	Slot Number	Depth From (ft)	Depth To (ft)
2.5	Plastic	10	10	20

10. Water Details

Water found at Depth (ft) ☐ Gas Kind of water ☐ Fresh ☐ Untested ☐ Other

11. Hole Diameter

Depth From (ft)	Depth To (ft)	Diameter (in)
0	20	7.5

12. Results of Well Yield Testing

☐ Pumping Discontinued

Explain _____

If flowing give rate

☐ Flowing _____ (GPM)

Draw down

Time (min)	Static Level	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (ft)														

Recovery

Time (min)	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (ft)													

After test of well yield, water was

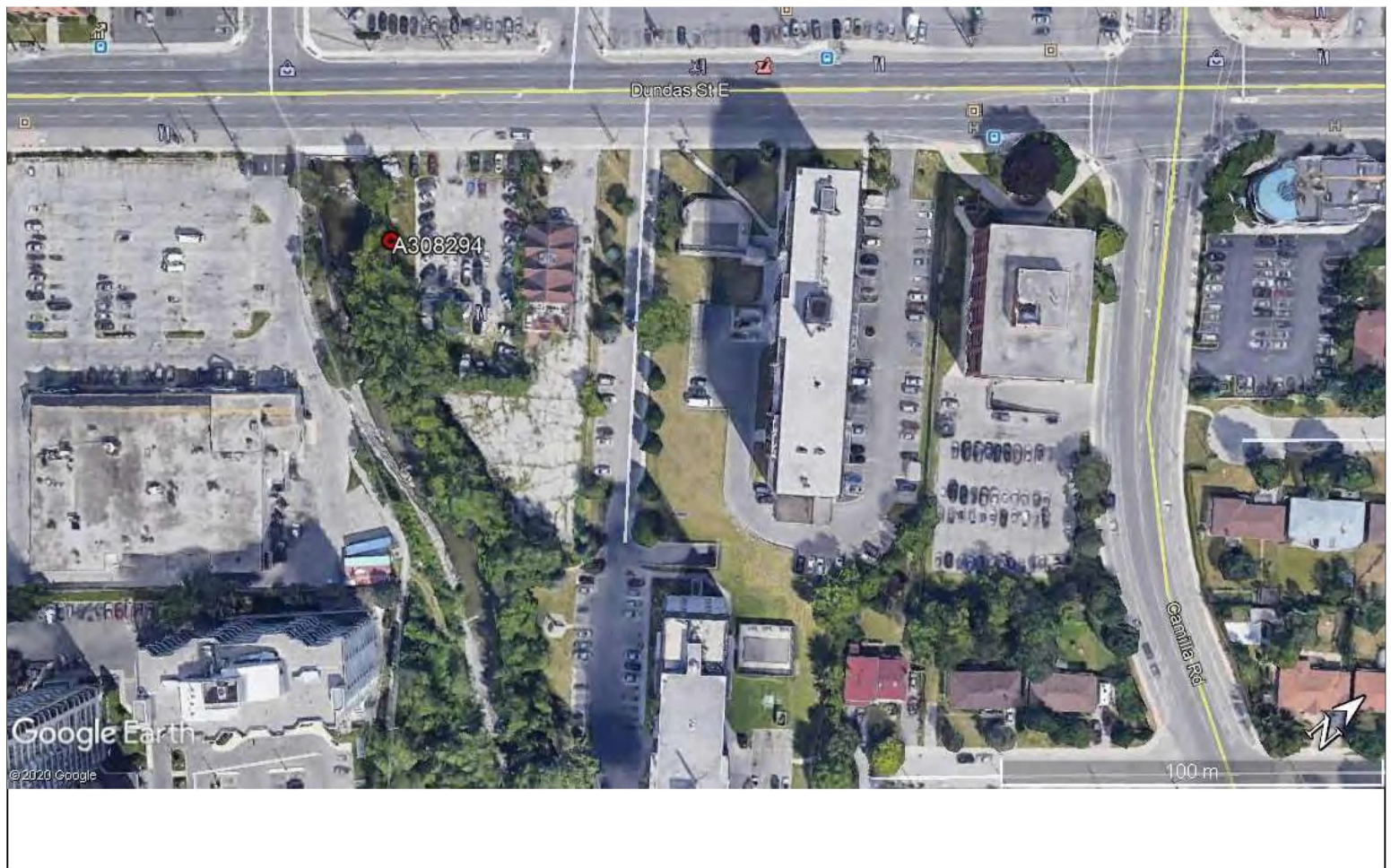
☐ Clear and sand free ☐ Other (specify)

Pump intake set at (ft)	Pumping rate (GPM)	Duration of pumping hrs + min	Final water level end of pumping (ft)	Disinfected? * <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
Recommended pump depth (ft)	Recommended pump rate (GPM)	Well production (GPM)		

13. Map of Well Location *

Map 1. Please Click the map area below to import an image file to use as the map.

☒ Make map area bigger



14. Information

Well owner's information package delivered <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	Date Package Delivered (yyyy/mm/dd)	Date Work Completed (yyyy/mm/dd) * 2020/10/22
Comments		

15. Well Contractor and Well Technician Information

Business Name of Well Contractor * Davis Drilling Ltd		Well Contractor's License Number * 7472	
Business Address			
Unit Number	Street Number 873	Street Name * Nipissing Rd	
City/Town/Village * Milton		Province ON	Postal Code * L9T 4Z4
Business Telephone Number 905-299-6915	Business Email Address davisdrilling@bellnet.ca		
Last Name of Well Technician * Borsellino	First Name of Well Technician * Nicholas	Well Technician's License Number * 3579	

16. Declaration *

☒ I hereby confirm that I am the person who constructed the well and I hereby confirm that the information on the form is correct and accurate.

Last Name Borsellino	First Name Nicholas	Email Address davisdrilling@bellnet.ca
Signature Nicholas Borsellino  Digitally signed by Nicholas Borsellino Date: 2020.11.23 08:27:50 -05'00'		Date Submitted (yyyy/mm/dd) 2020/11/23

17. Ministry Use Only

Audit Number

OTWW PHOK

Notice of Collection of Personal Information

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Fields marked with an asterisk (*) are mandatory.

Well Tag Number *

A307705

Type *

☒ Construction ☐ Abandonment

Measurement recorded in: *

☐ Metric ☒ Imperial

1. Well Owner's Information

Last Name and First Name, or Organization is mandatory. *

Last Name | First Name

Organization | Email Address

DBV Real Estate Investments Inc.

Current Address

Unit Number | Street Number * | Street Name * | City/Town/Village

Country | Province | Postal Code | Telephone Number

Ontario

2. Well Location

Address of Well Location

Unit Number | Street Number * | Street Name * | Township

3026 | Kirwin Ave

Lot | Concession | County/District/Municipality

City/Town | Province | Postal Code

Mississauga

UTM Coordinates | Zone * | Easting * | Northing * | Municipal Plan and Sublot Number

NAD 83 | 17 | 611938 | 4826579 | Test UTM in Map

Other

3. Overburden and Bedrock Material *

Well Depth * | 22 | (ft)

General Colour | Most Common Material | Other Materials | General Description | Depth From | Depth To

				(ft)	(ft)
Brown	Gravel	Sand		0	15
Blue	Shale		Weathered	15	22

4. Annular Space *

Depth From (ft)	Depth To (ft)	Type of Sealant Used (Material and Type)	Volume Placed (cubic feet)
0	11	Bentonite Chip	3.52
11	22	No. 2 Sand	3.52

5. Method of Construction *

- ☐ Cable Tool ☐ Rotary (Conventional) ☐ Rotary (Reverse) ☒ Boring ☐ Air percussion ☐ Diamond
☐ Jetting ☐ Driving ☐ Digging ☐ Rotary (Air) ☐ Augering ☐ Direct Push
☐ Other (specify) _____

6. Well Use *

- ☐ Public ☐ Industrial ☐ Cooling & Air Conditioning
☐ Domestic ☐ Commercial ☐ Not Used
☐ Livestock ☐ Municipal ☒ Monitoring
☐ Irrigation ☐ Test Hole ☐ Dewatering
☐ Other (specify) _____

7. Status of Well *

- ☐ Water Supply ☐ Replacement Well ☐ Test Hole
☐ Recharge Well ☐ Dewatering Well ☒ Observation and/or Monitoring Hole
☐ Alteration (Construction) ☐ Abandoned, Insufficient Supply ☐ Abandoned, Poor Water Quality
☐ Abandoned, other (specify) _____
☐ Other (specify) _____

8. Construction Record - Casing * (use negative number(s) to indicate depth above ground surface)

Inside Diameter (in)	Open Hole or Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness	Depth From (ft)	Depth To (ft)
2	Plastic	0.15	0	12

9. Construction Record - Screen

Outside Diameter (in)	Material (Plastic, Galvanized, Steel)	Slot Number	Depth From (ft)	Depth To (ft)
2.3	Plastic	10	12	22

10. Water Details

Water found at Depth **17.5** (ft) ☐ Gas Kind of water ☐ Fresh ☐ Untested ☐ Other

11. Hole Diameter

Depth From (ft)	Depth To (ft)	Diameter (in)
0	22	8

12. Results of Well Yield Testing

☐ Pumping Discontinued

Explain _____

If flowing give rate

☐ Flowing _____ (GPM)

Draw down

Time (min)	Static Level	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (ft)														

Recovery

Time (min)	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (ft)													

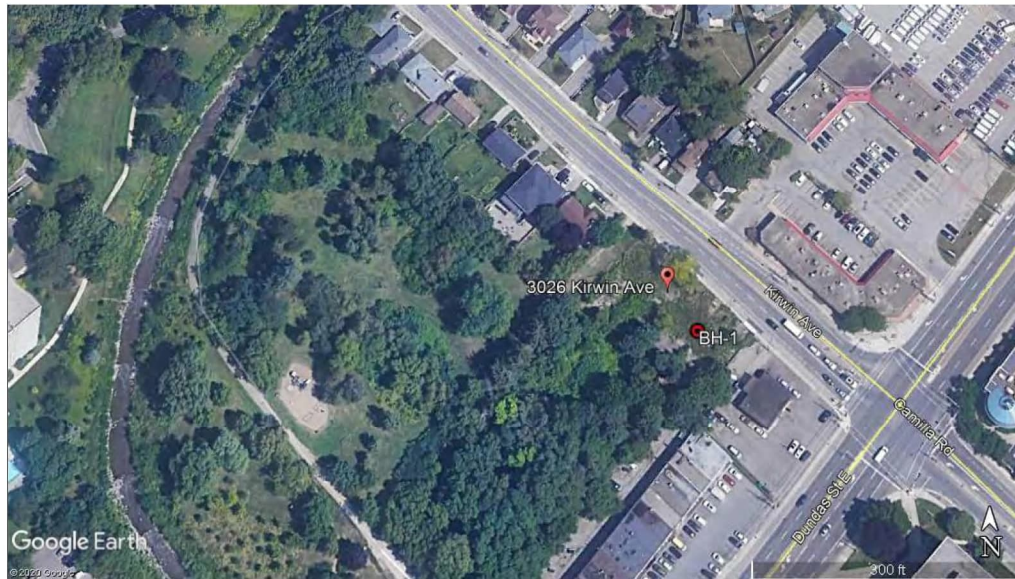
After test of well yield, water was

☐ Clear and sand free ☐ Other (specify)

Pump intake set at (ft)	Pumping rate (GPM)	Duration of pumping hrs + min	Final water level end of pumping (ft)	Disinfected? * <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
Recommended pump depth (ft)	Recommended pump rate (GPM)	Well production (GPM)		

13. Map of Well Location *

Map 1. Please Click the map area below to import an image file to use as the map. ☐ Make map area bigger



14. Information

Well owner's information package delivered <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	Date Package Delivered (yyyy/mm/dd) 2021/01/25	Date Work Completed (yyyy/mm/dd) * 2020/12/09
Comments 56946-bh1		

15. Well Contractor and Well Technician Information

Business Name of Well Contractor * Altech Drilling & Investigative Services		Well Contractor's License Number * 7282	
Business Address			
Unit Number	Street Number 410	Street Name * Pinebush Road	
City/Town/Village * Cambridge		Province Ontario	Postal Code * N1T 1Z6
Business Telephone Number 519-650-5557		Business Email Address	
Last Name of Well Technician * Stranz	First Name of Well Technician * Brandon	Well Technician's License Number * 4021	

16. Declaration *

☒ I hereby confirm that I am the person who constructed the well and I hereby confirm that the information on the form is correct and accurate.

Last Name Stranz	First Name Brandon	Email Address bstranz@altechworld.com
Signature Brandon Stranz Digitally signed by Brandon Stranz Date: 2021.01.25 08:12:40 -05'00'		Date Submitted (yyyy/mm/dd) 2021/01/25

17. Ministry Use Only

Audit Number
KCE2 XI4N

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Fields marked with an asterisk (*) are mandatory.

Well Tag Number *

A307718

Type *

☒ Construction ☐ Abandonment

Measurement recorded in: *

☐ Metric ☒ Imperial

1. Well Owner's Information

Last Name and First Name, or Organization is mandatory. *

Last Name | First Name

Organization | Email Address

DBV Real Estate Investments Inc.

Current Address

Unit Number | Street Number * | Street Name * | City/Town/Village

Country | Province | Postal Code | Telephone Number

Ontario

2. Well Location

Address of Well Location

Unit Number | Street Number * | Street Name * | Township

3026 | Kirwin Ave

Lot | Concession | County/District/Municipality

City/Town | Province | Postal Code

Mississauga

UTM Coordinates | Zone * | Easting * | Northing * | Municipal Plan and Sublot Number

NAD 83 | 17 | 611926 | 4826559 | Test UTM in Map

Other

3. Overburden and Bedrock Material *

Well Depth * | 19 | (ft)

General Colour | Most Common Material | Other Materials | General Description | Depth From | Depth To

				(ft)	(ft)
Brown	Gravel	Sand		0	15
Blue	Shale		Weathered	15	19

4. Annular Space *

Depth From (ft)	Depth To (ft)	Type of Sealant Used (Material and Type)	Volume Placed (cubic feet)
0	8	Bentonite Chip	2.56
8	19	No. 2 Sand	3.52

5. Method of Construction *

- ☐ Cable Tool ☐ Rotary (Conventional) ☐ Rotary (Reverse) ☒ Boring ☐ Air percussion ☐ Diamond
☐ Jetting ☐ Driving ☐ Digging ☐ Rotary (Air) ☐ Augering ☐ Direct Push
☐ Other (specify) _____

6. Well Use *

- ☐ Public ☐ Industrial ☐ Cooling & Air Conditioning
☐ Domestic ☐ Commercial ☐ Not Used
☐ Livestock ☐ Municipal ☒ Monitoring
☐ Irrigation ☐ Test Hole ☐ Dewatering
☐ Other (specify) _____

7. Status of Well *

- ☐ Water Supply ☐ Replacement Well ☐ Test Hole
☐ Recharge Well ☐ Dewatering Well ☒ Observation and/or Monitoring Hole
☐ Alteration (Construction) ☐ Abandoned, Insufficient Supply ☐ Abandoned, Poor Water Quality
☐ Abandoned, other (specify) _____
☐ Other (specify) _____

8. Construction Record - Casing * (use negative number(s) to indicate depth above ground surface)

Inside Diameter (in)	Open Hole or Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness	Depth From (ft)	Depth To (ft)
2	Plastic	0.15	0	9

9. Construction Record - Screen

Outside Diameter (in)	Material (Plastic, Galvanized, Steel)	Slot Number	Depth From (ft)	Depth To (ft)
2.3	Plastic	10	9	19

10. Water Details

Water found at Depth (ft) ☐ Gas Kind of water ☐ Fresh ☐ Untested ☐ Other

11. Hole Diameter

Depth From (ft)	Depth To (ft)	Diameter (in)
0	19	8

12. Results of Well Yield Testing

☐ Pumping Discontinued

Explain _____

If flowing give rate

☐ Flowing _____ (GPM)

Draw down

Time (min)	Static Level	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (ft)														

Recovery

Time (min)	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (ft)													

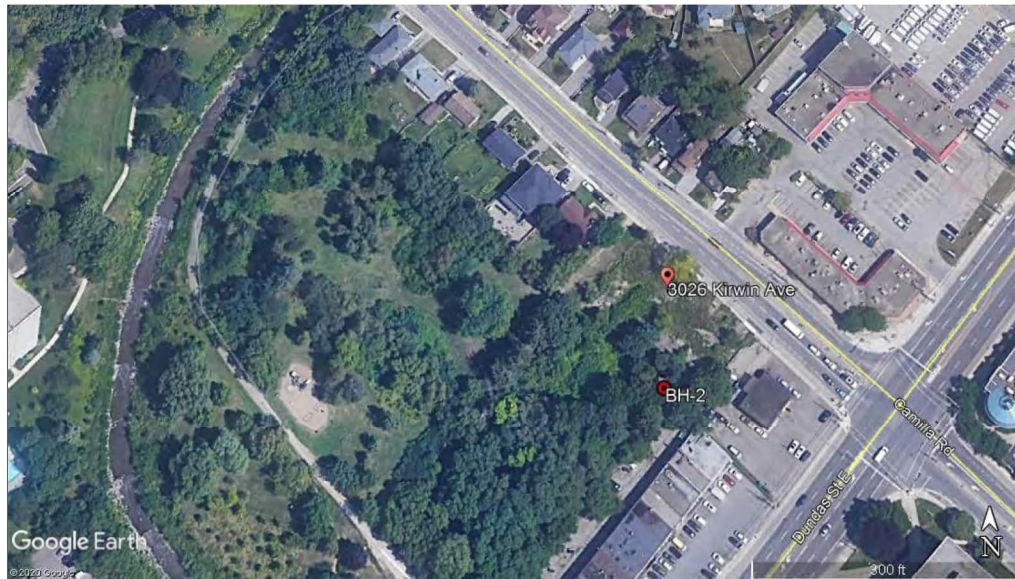
After test of well yield, water was

☐ Clear and sand free ☐ Other (specify)

Pump intake set at (ft)	Pumping rate (GPM)	Duration of pumping hrs + min	Final water level end of pumping (ft)	Disinfected? * <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
Recommended pump depth (ft)	Recommended pump rate (GPM)	Well production (GPM)		

13. Map of Well Location *

Map 1. Please Click the map area below to import an image file to use as the map. ☐ Make map area bigger



14. Information

Well owner's information package delivered <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	Date Package Delivered (yyyy/mm/dd) 2021/01/25	Date Work Completed (yyyy/mm/dd) * 2020/12/09
Comments 56946-bh2		

15. Well Contractor and Well Technician Information

Business Name of Well Contractor * Altech Drilling & Investigative Services		Well Contractor's License Number * 7282	
Business Address			
Unit Number	Street Number 410	Street Name * Pinebush Road	
City/Town/Village * Cambridge		Province Ontario	Postal Code * N1T 1Z6
Business Telephone Number 519-650-5557		Business Email Address	
Last Name of Well Technician * Stranz	First Name of Well Technician * Brandon	Well Technician's License Number * 4021	

16. Declaration *

☒ I hereby confirm that I am the person who constructed the well and I hereby confirm that the information on the form is correct and accurate.

Last Name Stranz	First Name Brandon	Email Address bstranz@altechworld.com
Signature Brandon Stranz Digitally signed by Brandon Stranz Date: 2021.01.25 08:11:31 -05'00'		Date Submitted (yyyy/mm/dd) 2021/01/25

17. Ministry Use Only

Audit Number
22K9 P6LU

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Fields marked with an asterisk (*) are mandatory.

Well Tag Number *

A307719

Type *

☒ Construction ☐ Abandonment

Measurement recorded in: *

☐ Metric ☒ Imperial

1. Well Owner's Information

Last Name and First Name, or Organization is mandatory. *

Last Name | First Name

Organization | Email Address

DBV Real Estate Investments Inc.

Current Address

Unit Number | Street Number * | Street Name * | City/Town/Village

Country | Province | Postal Code | Telephone Number

Ontario

2. Well Location

Address of Well Location

Unit Number | Street Number * | Street Name * | Township

3026 | Kirwin Ave

Lot | Concession | County/District/Municipality

City/Town | Province | Postal Code

Mississauga

UTM Coordinates | Zone * | Easting * | Northing * | Municipal Plan and Sublot Number

NAD 83 | 17 | 611933 | 4826568 | Test UTM in Map

Other

3. Overburden and Bedrock Material *

Well Depth * | 22 | (ft)

General Colour | Most Common Material | Other Materials | General Description | Depth From | Depth To

				(ft)	(ft)
Brown	Gravel	Sand		0	15
Blue	Shale		Weathered	15	22

4. Annular Space *

Depth From (ft)	Depth To (ft)	Type of Sealant Used (Material and Type)	Volume Placed (cubic feet)
0	11	Bentonite Chip	3.52
11	19	No. 2 Sand	3.52

5. Method of Construction *

- ☐ Cable Tool ☐ Rotary (Conventional) ☐ Rotary (Reverse) ☒ Boring ☐ Air percussion ☐ Diamond
☐ Jetting ☐ Driving ☐ Digging ☐ Rotary (Air) ☐ Augering ☐ Direct Push
☐ Other (specify) _____

6. Well Use *

- ☐ Public ☐ Industrial ☐ Cooling & Air Conditioning
☐ Domestic ☐ Commercial ☐ Not Used
☐ Livestock ☐ Municipal ☒ Monitoring
☐ Irrigation ☐ Test Hole ☐ Dewatering
☐ Other (specify) _____

7. Status of Well *

- ☐ Water Supply ☐ Replacement Well ☐ Test Hole
☐ Recharge Well ☐ Dewatering Well ☒ Observation and/or Monitoring Hole
☐ Alteration (Construction) ☐ Abandoned, Insufficient Supply ☐ Abandoned, Poor Water Quality
☐ Abandoned, other (specify) _____
☐ Other (specify) _____

8. Construction Record - Casing * (use negative number(s) to indicate depth above ground surface)

Inside Diameter (in)	Open Hole or Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness	Depth From (ft)	Depth To (ft)
2	Plastic	0.15	0	12

9. Construction Record - Screen

Outside Diameter (in)	Material (Plastic, Galvanized, Steel)	Slot Number	Depth From (ft)	Depth To (ft)
2.3	Plastic	10	12	22

10. Water Details

Water found at Depth (ft) ☐ Gas Kind of water ☐ Fresh ☐ Untested ☐ Other

11. Hole Diameter

Depth From (ft)	Depth To (ft)	Diameter (in)
0	22	8

12. Results of Well Yield Testing

☐ Pumping Discontinued

Explain _____

If flowing give rate

☐ Flowing _____ (GPM)

Draw down

Time (min)	Static Level	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (ft)														

Recovery

Time (min)	1	2	3	4	5	10	15	20	25	30	40	50	60
Water Level (ft)													

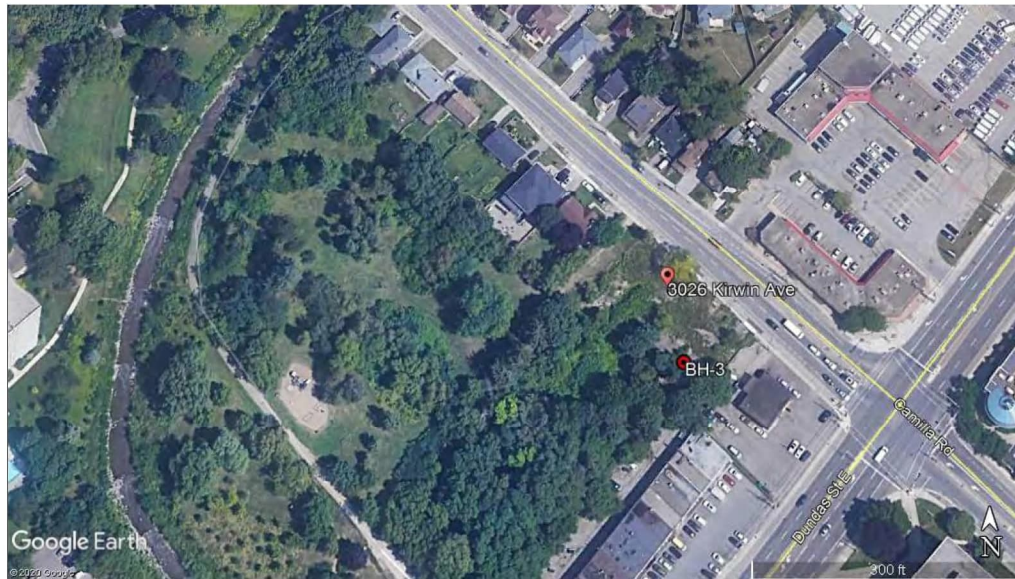
After test of well yield, water was

☐ Clear and sand free ☐ Other (specify)

Pump intake set at (ft)	Pumping rate (GPM)	Duration of pumping hrs + min	Final water level end of pumping (ft)	Disinfected? * <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
Recommended pump depth (ft)	Recommended pump rate (GPM)	Well production (GPM)		

13. Map of Well Location *

Map 1. Please Click the map area below to import an image file to use as the map. ☐ Make map area bigger



14. Information

Well owner's information package delivered <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No	Date Package Delivered (yyyy/mm/dd) 2021/01/25	Date Work Completed (yyyy/mm/dd) * 2020/12/09
Comments 56946-bh3		

15. Well Contractor and Well Technician Information

Business Name of Well Contractor * Altech Drilling & Investigative Services		Well Contractor's License Number * 7282	
Business Address			
Unit Number	Street Number 410	Street Name * Pinebush Road	
City/Town/Village * Cambridge		Province Ontario	Postal Code * N1T 1Z6
Business Telephone Number 519-650-5557		Business Email Address	
Last Name of Well Technician * Stranz	First Name of Well Technician * Brandon	Well Technician's License Number * 4021	

16. Declaration *

☒ I hereby confirm that I am the person who constructed the well and I hereby confirm that the information on the form is correct and accurate.

Last Name Stranz	First Name Brandon	Email Address bstranz@altechworld.com
Signature Brandon Stranz Digitally signed by Brandon Stranz Date: 2021.01.25 08:07:21 -05'00'		Date Submitted (yyyy/mm/dd) 2021/01/25

17. Ministry Use Only

Audit Number
KK5G 2P5X

CFM 17 6 11 6 6 4 E

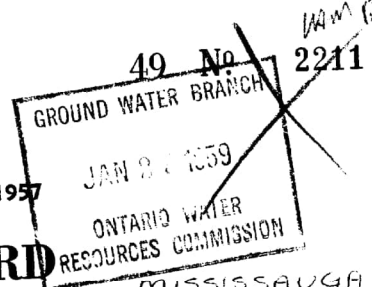
5 R 4 8 2 6 4 2 0 N

Elev. DUNDAS ST N.

Basin C94 LOT 15



The Ontario Water Resources Commission Act, 1957



WATER WELL RECORD

County or District PEEL Township, Village, Town or City TORONTO
 completed 12 NOV 58
 (day month year)



Casing and Screen Record

Inside diameter of casing 6"
 Total length of casing 22 FT
 Type of screen
 Length of screen
 Depth to top of screen
 Diameter of finished hole 6"

Pumping Test

Static level 10 FT
 Test-pumping rate 10 G.P.M.
 Pumping level 10
 Duration of test pumping 4 HRS
 Water clear or cloudy at end of test CLEAR
 Recommended pumping rate 10 G.P.M.
 with pumping level of 10

Well Log

Water Record

Overburden and Bedrock Record	From ft.	To ft.	Depth(s) at which water(s) found	No. of feet water rises	Kind of water (fresh, salty, sulphur)
<u>BROWN SAND & GRAVEL</u>	<u>0</u>	<u>17</u>			
<u>BLUE SHALE</u>	<u>17</u>	<u>51</u>	<u>40</u>	<u>41</u>	<u>FRESH</u>

For what purpose(s) is the water to be used?

HOUSE

Is well on upland, in valley, or on hillside?

UPLAND

Drilling Firm B. H. HARRISON & SONS

Address 494 LAKESHORE RD

MISSISSAUGA

Licence Number 113

Name of Driller J. B. HARRISON

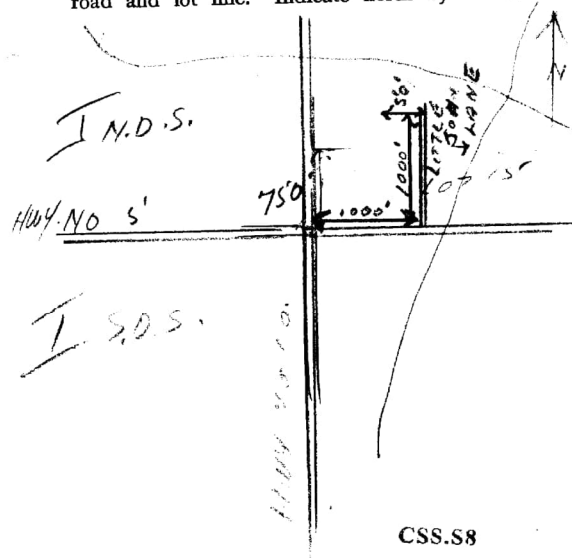
Address

Date JAN 20/59

J. B. Harrison
 (Signature of Licensed Drilling Contractor)

Location of Well

In diagram below show distances of well from road and lot line. Indicate north by arrow.



Instructions for Completing Form

- For use in the **Province of Ontario** only. This document is a permanent **legal** document. Please retain for future reference.
- All Sections **must** be completed in full to avoid delays in processing. Further instructions and explanations are available on the back of this form.
- Questions regarding completing this application can be directed to the Water Well Management Coordinator at 416-235-6203.
- **All metre measurements shall be reported to 1/10th of a metre.**
- Please print clearly in blue or black ink only.

All metre measurements shall be reported to 1/10 th or a metre. Please print clearly in blue or black ink only.						Ministry Use Only MUN [] [] [] [] [] [] [] [] [] [] [] [] [] [] [] [] CON [] [] [] [] [] [] [] [] [] [] [] [] LOT [] [] [] [] [] [] [] [] [] [] [] []							
Well Owner's Information and Location of Well Information													
First Name CITY OF MISSISSAUGA		Last Name		Mailing Address (Street Number/Name, RR, Lot, Concession) 300 CITY CENTRE DRIVE									
County/District/Municipality PEEL			Township/City/Town/Village MISSISSAUGA			Province Ontario		Postal Code L5B 3C1		Telephone Number (include area code) 905-896-5136			
Address of Well Location (County/District/Municipality) PEEL							Township			Lot		Concession	
RR#/Street Number/Name KIRWIN AVE							City/Town/Village MISSISSAUGA			Site/Compartment/Block/Tract etc.			
GPS Reading NAD 83		Zone 17		Easting 611802		Northing 4826734		Unit Make/Model MAGELLAN		Mode of Operation:		<input type="checkbox"/> Undifferentiated <input checked="" type="checkbox"/> Averaged <input type="checkbox"/> Differentiated, specify _____	

Log of Overburden and Bedrock Materials (see instructions)

[illegible][illegible][illegible]

Method of Construction			
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Rotary (air)	<input type="checkbox"/> Diamond	<input type="checkbox"/> Digging
<input type="checkbox"/> Rotary (conventional)	<input type="checkbox"/> Air percussion	<input type="checkbox"/> Jetting	<input type="checkbox"/> Other
<input type="checkbox"/> Rotary (reverse)	<input checked="" type="checkbox"/> Boring	<input type="checkbox"/> Driving	

Water Use			
<input type="checkbox"/> Domestic	<input type="checkbox"/> Industrial	<input type="checkbox"/> Public Supply	<input checked="" type="checkbox"/> Other
<input type="checkbox"/> Stock	<input type="checkbox"/> Commercial	<input type="checkbox"/> Not used	TEST
<input type="checkbox"/> Irrigation	<input type="checkbox"/> Municipal	<input type="checkbox"/> Cooling & air conditioning	

Final Status of Well			
<input type="checkbox"/> Water Supply	<input type="checkbox"/> Recharge well	<input type="checkbox"/> Unfinished	<input type="checkbox"/> Abandoned, (Other)
<input checked="" type="checkbox"/> Observation well	<input type="checkbox"/> Abandoned, insufficient supply	<input type="checkbox"/> Dewatering	
<input type="checkbox"/> Test Hole	<input type="checkbox"/> Abandoned, poor quality	<input type="checkbox"/> Replacement well	

Well Contractor/Technician Information			
Name of Well Contractor GEO ENVIRONMENTAL DRILLING		Well Contractor's Licence No. 6607	
Business Address (street name, number, city etc.) 340 MARKET DR. MILTON ON			
Name of Well Technician (last name, first name) BAILEY, RYAN		Well Technician's Licence No. T-3111	
Signature of Technician/Contractor [Signature]		Date Submitted yyyymmdd 05 06 30	
X [Signature]			

Location of Well

In diagram below show distances of well from road, lot line, and building. Indicate north by arrow.

Audit No. **Z 32255**

Date Well Completed **05** **MM** **06** **DD**

Was the well owner's information package delivered? ☐ Yes ☐ No

Date Delivered **YY** **MM** **DD**

Ministry Use Only			
Data Source	Contractor 8607		
Date Received JUL 22 2005 DD	Date of Inspection	YYYY	MM DD
Remarks	Well Record Number		

Well Owner's Information

60 DUNDAS STREET

County/District/Municipality

Peel

Mississauga

City/Town/Village

Mississauga

Province

Ontario

Postal Code

L5A1W4

UTM Coordinates Zone Easting Northing

NAD 83

17611971

4826314

GARMIN

ETREX

GPS Unit Make

Model

Mode of Operation:

☐ Undifferentiated

☒ Averaged

☐ Differentiated, specify

Overburden and Bedrock Materials (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (Metres) From To
black	asphalt		Packed	0 .05
brown	gravel	medium, coarse sand	Packed	.05 .25
grey	silt	fine sand, gravel	Dense	.25 6.10
wells GPS 2) 17/611981/4826271 3) 17/612170/4826252				
Consultant Construction Control				

Annular Space/Abandonment Sealing Record			
Depth Set at (Metres) From To	Type of Sealant Used (Material and Type)	Volume Placed (Cubic Metres)	
0 .30	concrete		
.30 1.50	bentonite		

Method of Construction		Water Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Test Hole
<input type="checkbox"/> Rotary (Air)	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning
<input type="checkbox"/> Air percussion	<input checked="" type="checkbox"/> Boring	<input type="checkbox"/> Industrial	<input checked="" type="checkbox"/> Monitoring
<input type="checkbox"/> Other, specify		<input type="checkbox"/> Other, specify	
Status of Well			
<input type="checkbox"/> Water Supply	<input type="checkbox"/> Dewatering Well	<input checked="" type="checkbox"/> Observation and/or Monitoring Hole	
<input type="checkbox"/> Replacement Well	<input type="checkbox"/> Abandoned, Insufficient Supply	<input type="checkbox"/> Alteration (Construction)	
<input type="checkbox"/> Test Hole	<input type="checkbox"/> Abandoned, Poor Water Quality	<input type="checkbox"/> Other, specify	
<input type="checkbox"/> Recharge Well	<input type="checkbox"/> Abandoned, other, specify		

Please provide a map below showing:

- all property boundaries, and measurements sufficient to locate the well in relation to fixed points
- an arrow indicating the North direction
- detailed drawings can be provided as attachments no larger than legal size (8.5" by 14")
- digital pictures of inside of well can also be provided

Well Tag

60 Dundas St. East

Dundas St. East

Results of Well Yield Testing			
Draw Down		Recovery	
Time (Min)	Water Level (Metres)	Time (Min)	Water Level (Metres)
Static Level		Static Level	
1		1	
2		2	
3		3	
4		4	
5		5	
10		10	
15		15	
20		20	
25		25	
30		30	
40		40	
50		50	
60		60	

Water Details	
Water found at Depth	Kind of Water
Metres	<input type="checkbox"/> Gas <input type="checkbox"/> Fresh <input type="checkbox"/> Salty <input type="checkbox"/> Sulphur <input type="checkbox"/> Minerals
Water found at Depth	Kind of Water
Metres	<input type="checkbox"/> Gas <input type="checkbox"/> Fresh <input type="checkbox"/> Salty <input type="checkbox"/> Sulphur <input type="checkbox"/> Minerals
Water found at Depth	Kind of Water
Metres	<input type="checkbox"/> Gas <input type="checkbox"/> Fresh <input type="checkbox"/> Salty <input type="checkbox"/> Sulphur <input type="checkbox"/> Minerals

Casing Used	Screen Used	Casing and Well Details
<input type="checkbox"/> Galvanized	<input type="checkbox"/> Galvanized	Diameter of the Hole (Centimetres)
<input type="checkbox"/> Steel	<input type="checkbox"/> Steel	10
<input type="checkbox"/> Fibreglass	<input type="checkbox"/> Fibreglass	Depth of the Hole (Metres)
<input checked="" type="checkbox"/> Plastic	<input checked="" type="checkbox"/> Plastic	6.10
<input type="checkbox"/> Concrete	<input type="checkbox"/> Concrete	Wall Thickness (Metres)
		Sch 40
No Casing and Screen Used		Inside Diameter of the Casing (Metres)
<input type="checkbox"/> Open Hole		.05
Disinfected?		Depth of the Casing (Metres)
<input type="checkbox"/> Yes <input type="checkbox"/> No		2.13

Ministry Use Only	
Audit No.	Well Contractor No.
z69137	
Date Received (yyyy/mm/dd)	Date of Inspection (yyyy/mm/dd)
JUL 11 2008	
Remarks	

Date Well Completed (yyyy/mm/dd)

2008/06/02

Was the well owner's information package delivered? ☐ Yes ☒ No

Date the Well Record and Package Delivered to Well Owner (yyyy/mm/dd)

Well Contractor and Well Technician Information

Business Name of Well Contractor

Atcost Soil Drilling

Well Contractor's Licence No.

61032

Business Address (Street No./Name, number, RR)

2160 Hwy 7

Municipality

Concord

Province

Ont

Postal Code

L4K1W6

Business E-mail Address

9056691253

Name of Well Technician (Last Name, First Name)

Green Wayne

Well Technician's Licence No.

Signature of Technician

Wayne Green

Date Submitted (yyyy/mm/dd)

2008/06/09



Ministry of
the Environment

Well Tag No. (Place Sticker and/or Print Below)

A006214

Well Record

Regulation 903 Ontario Water Resources Act

Well Location

Address of Well Location (Street Number/Name) 225 Dundas St. E.		Township	Lot	Concession
County/District/Municipality		City/Town/Village Mississauga	Province Ontario	Postal Code
UTM Coordinates Zone Easting NAD 83 1171611211224182617417		Municipal Plan and Sublot Number		Other

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft) From To
Brown	Fill	Rock, sand	moist	0' 5'
Brown	silt	sand	moist-dry	5' 18'
Gray	silt		moist	18' 20'
Gray	weathered shale		moist	20' 22'

Annular Space		
Depth Set at (m/ft) From To	Type of Sealant Used (Material and Type)	Volume Placed (m³/ft³)
22' 11'	Sand	
11' 1'	Bentonite	
1' 0'	Sand casing, concrete	

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input checked="" type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Dewatering
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input checked="" type="checkbox"/> Test Hole
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial	<input type="checkbox"/> Cooling & Air Conditioning
<input type="checkbox"/> Other, specify		<input type="checkbox"/> Other, specify	

Construction Record - Casing			Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Well Thickness (cm/in)	Depth (m/ft) From To	
2"	Plastic	Sch. 40	12' 0'	<input type="checkbox"/> Water Supply
				<input type="checkbox"/> Replacement Well
				<input checked="" type="checkbox"/> Test Hole
				<input type="checkbox"/> Recharge Well
				<input type="checkbox"/> Dewatering Well
				<input type="checkbox"/> Observation and/or Monitoring Hole
				<input type="checkbox"/> Alteration (Construction)
				<input type="checkbox"/> Abandoned, Insufficient Supply
				<input type="checkbox"/> Abandoned, Poor Water Quality
				<input type="checkbox"/> Abandoned, other, specify
				<input type="checkbox"/> Other, specify

Construction Record - Screen			
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft) From To
2"	Plastic	10	22' 12'

Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft) From To	Diameter (cm/in)
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	22' 0'	9"
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify		

Business Name of Well Contractor Profile Drilling Inc.		Well Contractor's Licence No. 72115	
Business Address (Street Number/Name) 149 North Finch Dr.		Municipality North York	
Province Ont.	Postal Code M3W1Y2	Business E-mail Address jason@profiledrilling.com	
Bus. Telephone No. (inc. area code) 416 615 0644		Name of Well Technician (Last Name, First Name) Slocki, Jason	
Well Technician's Licence No. 24718		Signature of Technician and/or Contractor [Signature]	
		Date Submitted 20100201	

Results of Well Yield Testing

After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify	Draw Down		Recovery	
	Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
If pumping discontinued, give reason:	Static Level			
	1		1	
Pump intake set at (m/ft)	2		2	
Pumping rate (l/min / GPM)	3		3	
Duration of pumping hrs + min	4		4	
Final water level end of pumping (m/ft)	5		5	
If flowing give rate (l/min / GPM)	10		10	
Recommended pump depth (m/ft)	15		15	
Recommended pump rate (l/min / GPM)	20		20	
Well production (l/min / GPM)	25		25	
Disinfected?	30		30	
<input type="checkbox"/> Yes <input type="checkbox"/> No	40		40	
	50		50	
	60		60	

Map of Well Location

Please provide a map below following instructions on the back.

See Attached.

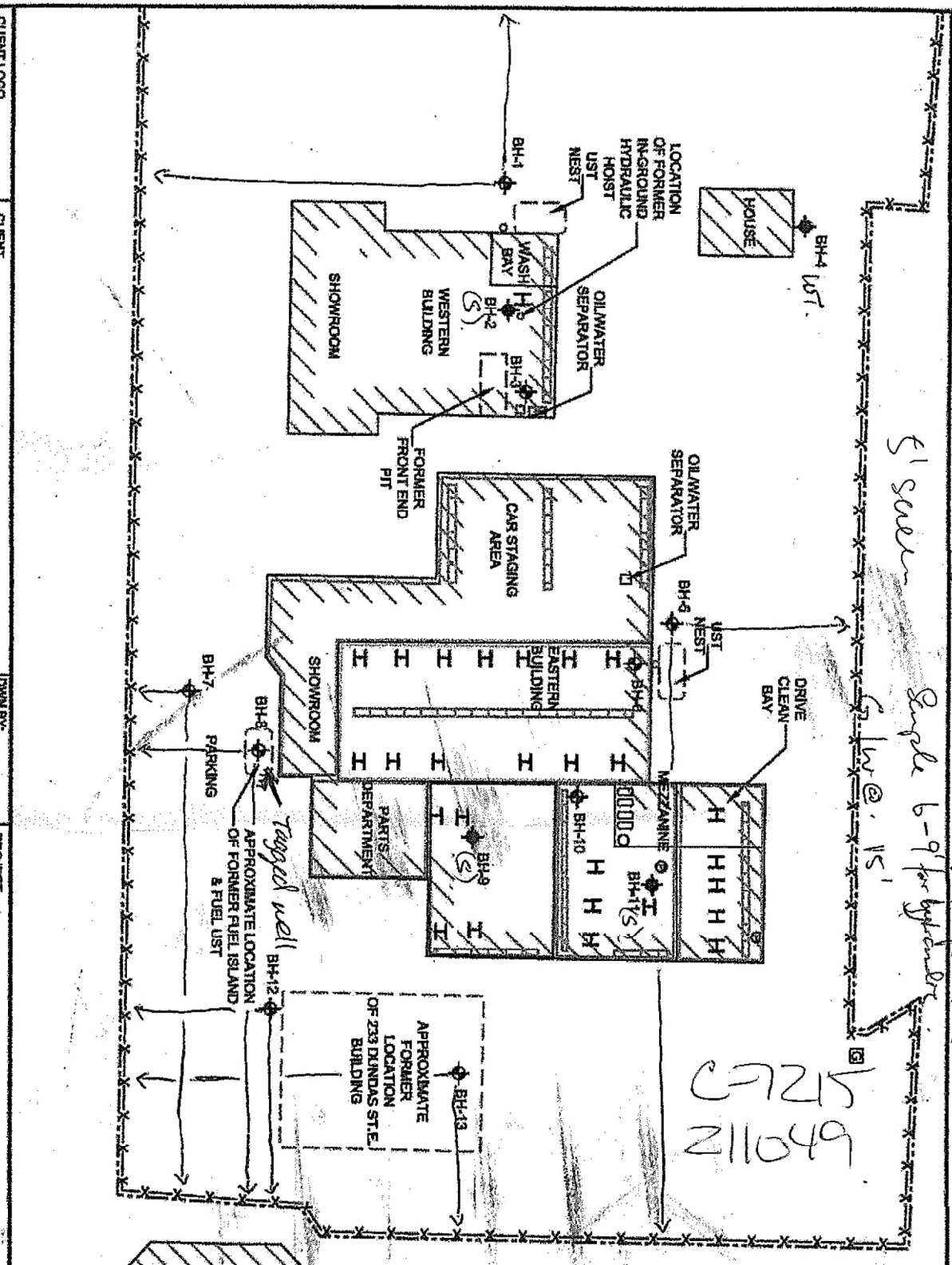
Comments:

Well owner's information package delivered <input type="checkbox"/> Yes <input type="checkbox"/> No	Date Package Delivered Y Y Y M M D D 20100120	Ministry Use Only Audit No. 2110049 FEB 16 2010
	Date Work Completed 20100120	

Shed 10' for WT for P.H.C.

5' Suen Sample 6-9 for hydrocarbon

C-725
211049

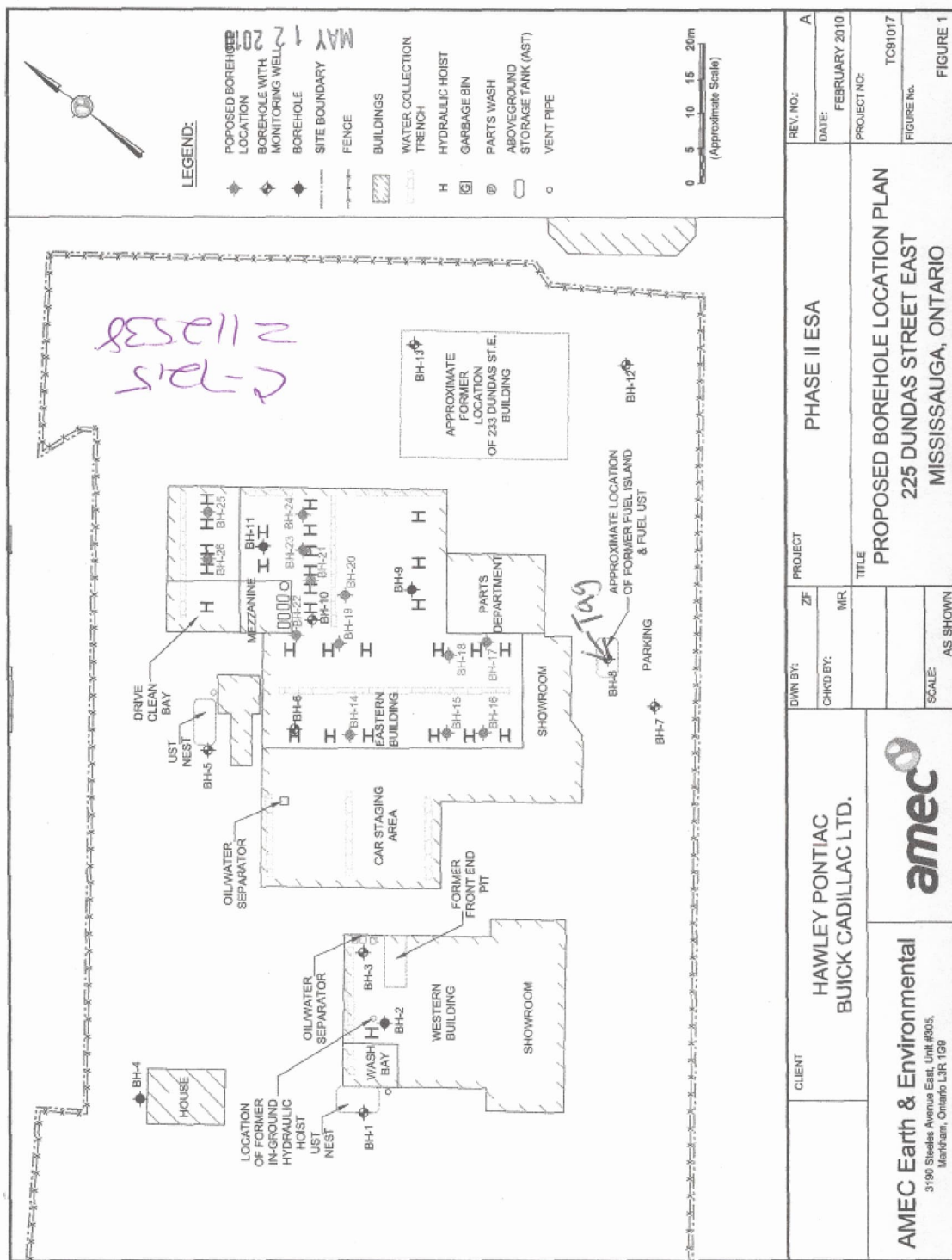


LEGEND:

- PROPOSED BOREHOLE WITH MONITORING WELL
- PROPOSED BOREHOLE
- ORIGINAL 1949 BUILDING
- EARLY 1950 ADDITION
- 1991 ADDITION
- 2006 ADDITION
- SITE BOUNDARY
- FENCE
- BUILDINGS
- WATER COLLECTION TRENCH
- HYDRAULIC HOIST
- GARBAGE BIN
- PARTS WASH
- ABOVEGROUND STORAGE TANK (AST)
- VENT PIPE

0 5 10 15 20m
(Approximate Scale)

CLIENT LOGO	CLIENT	DWN BY:	PROJECT	REV. NO.:
	HAWLEY PONTIAC BUICK CADILLAC LTD.	MM	PHASE II ESA	A
		CHK'D BY:	TITLE	DATE:
		MR	PROPOSED BOREHOLE LOCATION PLAN	DECEMBER 2009
AMEC Earth & Environmental		SCALE:	225 DUNDAS STREET EAST MISSISSAUGA, ONTARIO	PROJECT NO.:
180 Tradem Boulevard East Mississauga, Ontario L4Z 3K7		AS SHOWN		PROPOSAL 1216
				FIGURE NO.
				FIGURE 1



AMEC Earth & Environmental 3190 Steeles Avenue East, Unit #903, Markham, Ontario L3R 1G9	CLIENT HAWLEY PONTIAC BUICK CADILLAC LTD.		PROJECT PHASE II ESA		REV. NO.: A
	AMEC		DWN BY: ZF	CHKD BY: MR	DATE: FEBRUARY 2010
	SCALE: AS SHOWN		TITLE PROPOSED BOREHOLE LOCATION PLAN 225 DUNDAS STREET EAST MISSISSAUGA, ONTARIO		
			PROJECT NO.: TC91017		
		FIGURE NO.: FIGURE 1			



Ontario

Ministry of
the Environment

(Well Tag No. / Class / Status) (or Print Below)

A 096787

Ap96787

Well Record
Regulation 903 Ontario Water Resources ActMeasurements recorded in: ☒ Metric ☐ Imperial

Page 3 of 3

Well Location

Address of Well Location (Street Number/Name) 38-40 Dundas St. West Township Leamington Lot M.35135a Concession 002528

County/District/Municipality Leamington City/Town/Village Leamington Province Ontario Postal Code 002528

UTM Coordinates Zone 18 Easting 117611696 Northing 4826996 Municipal Plan and Sublot Number 002528 Other WKQ-002528

NAD 83 117611696 4826996 002528 002528

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft)
				From To
Black	Asphalt		soft	0 .1
brown	sand		soft	.1 2.7
grey	Shale	374	hard	2.7 4.8

Annular Space

Depth Set at (m/ft)	Type of Sealant Used	Volume Placed
From To	(Material and Type)	(m ³ /ft ³)
0 .31	Concrete	.0031
.31 3	Bentonite	.0126
3 4.8	Silica Sand	.0084

Method of Construction

☐ Cable Tool ☐ Diamond ☐ Public ☐ Commercial ☐ Not used

☐ Rotary (Conventional) ☐ Jetting ☐ Domestic ☐ Municipal ☐ Dewatering

☐ Rotary (Reverse) ☐ Driving ☐ Livestock ☒ Test Hole ☒ Monitoring

☐ Boring ☐ Digging ☐ Irrigation ☐ Cooling & Air Conditioning

☐ Air percussion ☐ Industrial

☒ Other, specify Direct Push ☐ Other, specify

Construction Record - Casing

Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Well Thickness (cm/in)	Depth (m/ft)
			From To
4.03	PVC	.36	0 3.3

Status of Well

☐ Water Supply ☐ Replacement Well ☒ Test Hole ☐ Recharge Well ☐ Dewatering Well ☐ Observation and/or Monitoring Hole ☐ Alteration (Construction) ☐ Abandoned, Insufficient Supply ☐ Abandoned, Poor Water Quality ☐ Abandoned, other, specify ☐ Other, specify

Construction Record - Screen

Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft)
			From To
4.82	PVC	10	3.3 4.8

Water Details

Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify
0 4.8	
4.8 10.9	

Hole Diameter

Depth (m/ft)	Diameter (cm/in)
From To	
0 4.8	10.9

Well Contractor and Well Technician Information

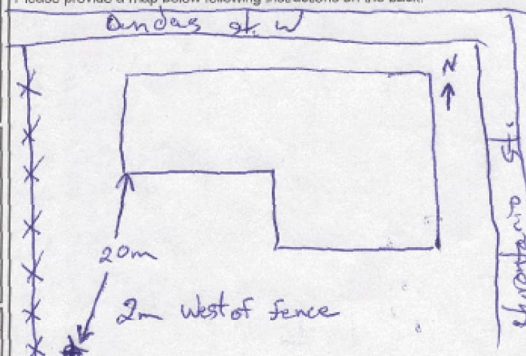
Business Name of Well Contractor Strata Soil Sampling Inc. Well Contractor's Licence No. 7241

Business Address (Street Number/Name) 147-2 West Beaver Creek Road Municipality Richmond Hill

Province Ontario Postal Code L4B 1C6 Business E-mail Address wrecords@stratasoil.com

Business Telephone No. (inc. area code) 905-764-9304 Name of Well Technician (Last Name, First Name) Robinson

Well Technician's Licence No. 31154 Signature of Technician and/or Contractor [Signature] Date Submitted 20100430



Comments: General contractor: [Signature]

Well owner's information package delivered ☐ Yes ☒ No

Date Package Delivered 20100428

Date Work Completed 20100428

Ministry Use Only

Audit No. z114336

Received MAY 21 2010



Ontario

Ministry of
the EnvironmentMeasurements recorded in: ☒ Metric ☒ Imperial

Well Tag No. (Place Sticker and/or Print Below)

A103044

Well Record

Regulation 903 Ontario Water Resources Act

Page 1 of 2

Address of Well Location (Street Number/Name) 120 Dundas street east		Township	Lot	Concession
County/District/Municipality		City/Town/Village Mississauga	Province Ontario	Postal Code
UTM Coordinates Zone	Easting	Northing	Municipal Plan and Sublot Number	
NAD 83	11611592	4026397	Other	

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft)	
				From	To
Brown	Sand	gravel	coarse	0	1.83
Brown	clay	silt	fine	1.83	3.1

Annular Space				Results of Well Yield Testing				
Depth Set at (m/ft)		Type of Sealant Used (Material and Type)	Volume Placed (m³/ft³)	After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify If pumping discontinued, give reason: Pump intake set at (m/ft)	Draw Down		Recovery	
From	To				Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
0	0.31	concrete	0.005		Static Level			
0.31	1.5	bentonite	0.025					
1.5	3.1	sand	0.0625					
					1		1	
					2		2	

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input checked="" type="checkbox"/> Test Hole
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial	
<input checked="" type="checkbox"/> Other, specify: Direct Push		<input type="checkbox"/> Other, specify	

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft)		
			From	To	
3.45	Plastic	0.356	0	1.5	<input checked="" type="checkbox"/> Water Supply
					<input type="checkbox"/> Replacement Well
					<input type="checkbox"/> Test Hole
					<input type="checkbox"/> Recharge Well
					<input type="checkbox"/> Dewatering Well
					<input type="checkbox"/> Observation and/or Monitoring Hole
					<input type="checkbox"/> Alteration (Construction)
					<input type="checkbox"/> Abandoned, Insufficient Supply
					<input type="checkbox"/> Abandoned, Poor Water Quality
					<input type="checkbox"/> Abandoned, other, specify
					<input type="checkbox"/> Other, specify

Construction Record - Screen				Status of Well	
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft)		
			From	To	
4.21	Plastic	10	1.5	3.1	<input type="checkbox"/> Water Supply
					<input type="checkbox"/> Replacement Well
					<input type="checkbox"/> Test Hole
					<input type="checkbox"/> Recharge Well
					<input type="checkbox"/> Dewatering Well
					<input type="checkbox"/> Observation and/or Monitoring Hole
					<input type="checkbox"/> Alteration (Construction)
					<input type="checkbox"/> Abandoned, Insufficient Supply
					<input type="checkbox"/> Abandoned, Poor Water Quality
					<input type="checkbox"/> Abandoned, other, specify
					<input type="checkbox"/> Other, specify

Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft)	Diameter (cm/in)
		From	To
		0	3.1

Well Contractor and Well Technician Information	
Business Name of Well Contractor State Soil Sampling	Well Contractor's Licence No. 7241
Business Address (Street Number/Name) 2-147 West Beaver Creek Dr Richmond Hill	Municipality
Province ON	Postal Code
Business E-mail Address k4B1c6w@state-soil.com	Business Telephone No. (inc. area code) 905 764 9304
Name of Well Technician (Last Name, First Name) Mike	Well Technician's Licence No. 3448
Signature of Technician and/or Contractor	Date Submitted 20100631

Results of Well Yield Testing			
After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify	Draw Down		Recovery
	Time (min)	Water Level (m/ft)	Time (min)
If pumping discontinued, give reason:	Static Level		
	1		1
	2		2
	3		3
	4		4
	5		5
Pump intake set at (m/ft)	10		10
Pumping rate (l/min / GPM)	15		15
Duration of pumping hrs + min	20		20
Final water level end of pumping (m/ft)	25		25
If flowing give rate (l/min / GPM)	30		30
Recommended pump depth (m/ft)	40		40
Recommended pump rate (l/min / GPM)	50		50
Well production (l/min / GPM)	60		60
Disinfected? <input type="checkbox"/> Yes <input type="checkbox"/> No			

Map of Well Location

Please provide a map below following instructions on the back.

See
attachment
mww
A103044

Comments:

Well owner's information package delivered <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	Date Package Delivered Y Y Y Y M M D D 2010 06 21	Ministry Use Only Audit No. z119050 JUL 16 2010
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Ontario

Ministry of
the EnvironmentMeasurements recorded in: ☒ Metric ☒ Imperial

A103036

Print Below)

Well Record

Regulation 903 Ontario Water Resources Act

Page 2 of 2

Address of Well Location (Street Number/Name) 120 Dundas Street East		Township Mississauga	Lot	Concession
County/District/Municipality		City/Town/Village Mississauga	Province Ontario	Postal Code
UTM Coordinates Zone Easting Northing NAD 83 17 41 59 84326414		Municipal Plan and Sublot Number		

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)					
General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft)	
				From	To
Brown Grey	Sand Clay	gravel soil	loose dense	0	1.83
				1.83	3.35

Annular Space				Results of Well Yield Testing			
Depth Set at (m/ft)		Type of Sealant Used (Material and Type)	Volume Placed (m³/ft³)	Draw Down		Recovery	
From	To			Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
0	0.31	concrete	0.0005	Static Level			
0.31	1.83	Bentonite	0.003	1		1	
1.83	3.35	sand	0.0025	2		2	
				3		3	
				4		4	
				5		5	
				10		10	
				15		15	
				20		20	
				25		25	
				30		30	
				40		40	
				50		50	
				60		60	

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Test Hole
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial	
<input checked="" type="checkbox"/> Other, specify Direct Push		<input type="checkbox"/> Other, specify	

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft)		
			From	To	
3.45	Plastic	0.345	0	1.83	<input checked="" type="checkbox"/> Water Supply
					<input type="checkbox"/> Replacement Well
					<input type="checkbox"/> Test Hole
					<input type="checkbox"/> Recharge Well
					<input type="checkbox"/> Dewatering Well
					<input checked="" type="checkbox"/> Observation and/or Monitoring Hole
					<input type="checkbox"/> Alteration (Construction)
					<input type="checkbox"/> Abandoned, Insufficient Supply
					<input type="checkbox"/> Abandoned, Poor Water Quality
					<input type="checkbox"/> Abandoned, other, specify
					<input type="checkbox"/> Other, specify

Construction Record - Screen			
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft)
			From To
4.21	Plastic	10	1.83 3.35

Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft)	Diameter (cm/in)
		From To	
		0 3.35	5.71

Well Contractor and Well Technician Information			
Business Name of Well Contractor State Soil Sampling		Well Contractor's Licence No. 722411	
Business Address (Street Number/Name) 2-147 West Beaver Creek Dr Richmond Hill		Municipality	
Province ON	Postal Code	Business E-mail Address 416166 wrecords@state-soil.com	
Bus. Telephone No. (inc. area code) 9057649304		Name of Well Technician (Last Name, First Name) Mgt Mike	
Well Technician's Licence No. 3448		Signature of Technician and/or Contractor [Signature]	
Date Submitted 20100631			

Comments:

Well owner's information package delivered	Date Package Delivered	Ministry Use Only
<input type="checkbox"/> Yes <input type="checkbox"/> No	Y Y Y Y M M D D 29/06/2010	Audit No. z119051
	Date Work Completed	Received JUL 16 2010

Measurements recorded in: ☐ Metric ☒ Imperial

Page 2 of 2

Address of Well Location (Street Number/Name)

Address or Web Location (Street Number/Name)
120 Dundas Street E

Township

City/Town/Village

Mississauga
Municipal Plan and Sublot Number

Lot

Concession

Province
Ontario

Postal Code

UTM Coordinates	Zone	Easting	Northing
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NAD 83 176114354826412

Other	
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Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

[illegible]

Annular Space				Results of Well Yield Testing				
Depth Set at (m/ft) From To		Type of Sealant Used (Material and Type)	Volume Placed (m³/ft³)	After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify _____	Draw Down		Recovery	
					Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
0'	0.5'	Cement		If pumping discontinued, give reason:	Static Level			
0.5'	5'	Bentonite			1		1	
5'	16'	Sand			2		2	
				Pump intake set at (m/ft)				

Method of Construction		Well Use		
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial	<input type="checkbox"/> Not used
<input checked="" type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal	<input type="checkbox"/> Dewatering
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Test Hole	<input checked="" type="checkbox"/> Monitoring
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning	
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial		
<input type="checkbox"/> Other, <i>specify</i>		<input type="checkbox"/> Other, <i>specify</i>		

Construction Record - Casing					Status of Well
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft)		<input type="checkbox"/> Water Supply <input type="checkbox"/> Replacement Well <input type="checkbox"/> Test Hole <input type="checkbox"/> Recharge Well <input type="checkbox"/> Dewatering Well <input checked="" type="checkbox"/> Observation and/or Monitoring Hole <input type="checkbox"/> Alteration (Construction) <input type="checkbox"/> Abandoned,
			From	To	
1.5"	Plastic	0.25"	0'	6'	

Construction Record - Screen					<input type="checkbox"/> Insufficient Supply <input type="checkbox"/> Abandoned, Poor Water Quality <input type="checkbox"/> Abandoned, other, specify _____ <input type="checkbox"/> Other, specify _____
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft) From To		
1.75"	Plastic	10	6'	16'	

Water Details		Hole Diameter	
Water found at Depth (<i>mf/t</i>) <input type="checkbox"/> Gas	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Other, <i>specify</i>	Depth (<i>mf/t</i>) From To	Diameter (<i>cm/in</i>)
Water found at Depth (<i>mf/t</i>) <input type="checkbox"/> Gas	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Other, <i>specify</i>	0' 16'	4.5"
Water found at Depth (<i>mf/t</i>) <input type="checkbox"/> Gas	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Other, <i>specify</i>		

Well Contractor and Well Technician Information				
Business Name of Well Contractor			Well Contractor's Licence No.	
Stata Soil Sampling			7 2 4 1	
Business Address (Street Number/Name)			Municipality	
2-147 West Beaver Creek Rd Richmond Hill				
Province	Postal Code	Business E-mail Address		
ON	L4B 1C6	wreard@statasoil.com		
Bus. Telephone No. (inc. area code)		Name of Well Technician (Last Name, First Name)		
905 764 9304		Ma N, Mike		
Well Technician's Licence No.	Signature of Technician and/or Contractor		Date Submitted	
3 4 4 8	[Signature]		20100631	

Results of Well Yield Testing				
After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, <u>specify</u>	Draw Down		Recovery	
	Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
If pumping discontinued, give reason:	Static Level			
	1		1	
Pump intake set at (m/ft)	2		2	
Pumping rate (l/min / GPM)	3		3	
	4		4	
Duration of pumping hrs + min	5		5	
Final water level end of pumping (m/ft)	10		10	
If flowing give rate (l/min / GPM)	15		15	
Recommended pump depth (m/ft)	20		20	
	25		25	
Recommended pump rate (l/min / GPM)	30		30	
Well production (l/min / GPM)	40		40	
	50		50	
Disinfected? <input type="checkbox"/> Yes <input type="checkbox"/> No	60		60	

Map of Well Location

Please provide a map below following instructions on the back.

see Map
MW 3-1

Well owner's information package Delivered <input type="checkbox"/> Yes <input type="checkbox"/> No	Date Package Delivered Y Y Y Y M M D D	Ministry Use Only Audit No. z119052 Rep'd On JUL 16 2010
	Date Work Completed 20100621	

Measurements recorded in: ☒ Metric ☐ Imperial

Well Owner's Information

First Name MATAS	Last Name / HOMES	E-mail Address		<input type="checkbox"/> Well Constructed by Well Owner
Mailing Address (Street Number/Name) 109 THOMAS ST		Municipality OAKVILLE	Province ON	Postal Code L6W 3A7

Well Location

Address of Well Location (Street Number/Name)				Township		Lot		Concession	
86 DUNDAS ST E				MISSISSAUGA					
County/District/Municipality				City/Town/Village				Province	
PEEL				MISSISSAUGA				Ontario	
UTM Coordinates		Zone		Easting		Northing		Municipal Plan and Sublot Number	
NAD 83		17		611918		4826373			
								Other	

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

[illegible]

Annular Space

Depth Set at (m/ft)		Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)
From	To		
0	1.3	CEMENT	
1.3	2.8	BENTONITE CHIPS	

Method of Construction

<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial	<input type="checkbox"/> Not used
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal	<input type="checkbox"/> Dewatering
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input checked="" type="checkbox"/> Test Hole	<input checked="" type="checkbox"/> Monitoring
<input checked="" type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning	
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial		
<input type="checkbox"/> Other, <i>specify</i>		<input type="checkbox"/> Other, <i>specify</i>		

Well Use

<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial	<input type="checkbox"/> Not used
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal	<input type="checkbox"/> Dewatering
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input checked="" type="checkbox"/> Test Hole	<input checked="" type="checkbox"/> Monitoring
<input checked="" type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning	
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial		
<input type="checkbox"/> Other, <i>specify</i>		<input type="checkbox"/> Other, <i>specify</i>		

Construction Record - Casing

[illegible]

Status of Well

[illegible]

Construction Record - Screen

Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft)	
			From	To
6	PLASTIC	100	3.0	7.6

Water Details

Water found at Depth 3 (mft) Kind of Water: ☐ Fresh ☒ Untested
☐ Gas ☐ Other, *specify* _____

Water found at Depth _____ Kind of Water: ☐ Fresh ☐ Untested
(mft) ☐ Gas ☐ Other, *specify* _____

Water found at Depth _____ Kind of Water: ☐ Fresh ☐ Untested
(mft) ☐ Gas ☐ Other, *specify* _____


Hole Diameter

Water found at Depth 3 (mft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, <i>specify</i>	Kind of Water: <input type="checkbox"/> Fresh <input checked="" type="checkbox"/> Untested	Depth (mft)	Diameter (cm/in)
Water found at Depth (mft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, <i>specify</i>	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested	From To	
Water found at Depth (mft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, <i>specify</i>	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested	0 7.6	12

Well Contractor and Well Technician Information

Business Name of Well Contractor ATCOST DRILLING		Well Contractor's Licence No. 61032
Business Address (Street Number/Name) 2160 HWY 75		Municipality YORK
Province ONT	Postal Code L4K 1W6	Business E-mail Address

Bus. Telephone No. (inc. area code) Name of Well Technician (Last Name, First Name)
1056691253 BARTZT, SEAN

Vell Technician's Licence No.	Signature of Technician and/or Contractor	Date Submitted
2519		20121015

Results of Well Yield Testing

Results of Well Yield Testing					
After test of well yield, water was:		Draw Down		Recovery	
<input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, <u>specify</u>		Time (min)	Water Level (m/fl)	Time (min)	Water Level (m/fl)
If pumping discontinued, give reason:		Static Level			
		1		1	
Pump intake set at (m/fl)		2		2	
Pumping rate (l/min / GPM)		3		3	
Duration of pumping hrs + min		4		4	
Final water level end of pumping (m/fl)		5		5	
If flowing give rate (l/min / GPM)		10		10	
Recommended pump depth (m/fl)		15		15	
Recommended pump rate (l/min / GPM)		20		20	
Well production (l/min / GPM)		25		25	
		30		30	
		40		40	
		50		50	
Disinfected?		60		60	
<input type="checkbox"/> Yes <input type="checkbox"/> No					

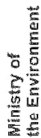
Map of Well Location

Please provide a map below following instructions on the back.

Comments:

12-A 187

Well owner's information package delivered	Date Package Delivered	Ministry Use Only Audit No. z 121323 JAN 31 2013
	Date Work Completed 20121009	



Well Record for Well Cluster - Part 1 of 3
(Only for Multiple Test Holes or Dewatering Wells)
Regulation 903 Ontario Water Resources Act

Well Tag No. of Deer: **Tag#: A139584**

Well # on Drawing of Leasehold: 113

Metric	Imperial
Weight	150 lbs
Height	5' 10"
Age	35
Gender	Male
Occupation	Software Engineer
Education	Master's Degree
Marital Status	Single
Religion	Christian
Political Affiliation	Democrat
Interests	Reading, Hiking, Music
Current Location	New York City
Current Residence	Manhattan
Current Employment	Google
Current Income	\$120,000
Current Assets	\$50,000
Current Liabilities	\$10,000
Current Net Worth	\$40,000
Current Credit Score	750
Current Debt-to-Income Ratio	15%
Current Savings Rate	10%
Current Retirement Savings Rate	5%
Current Insurance Coverage	Health, Life, Auto
Current Tax Status	Single
Current Filing Status	Single
Current Tax Rate	25%
Current Tax Bracket	25%
Current Tax Deductions	\$1,000
Current Tax Credits	\$500
Current Tax Liability	\$1,500
Current Tax Refund	\$500
Current Tax Payment	\$1,000
Current Tax Due	\$500
Current Tax Status Summary	Single, 25% Tax Rate, \$1,000 Deductions, \$500 Credits, \$1,500 Liability, \$500 Refund, \$1,000 Payment, \$500 Due

Follow instructions on the front and back of this form.

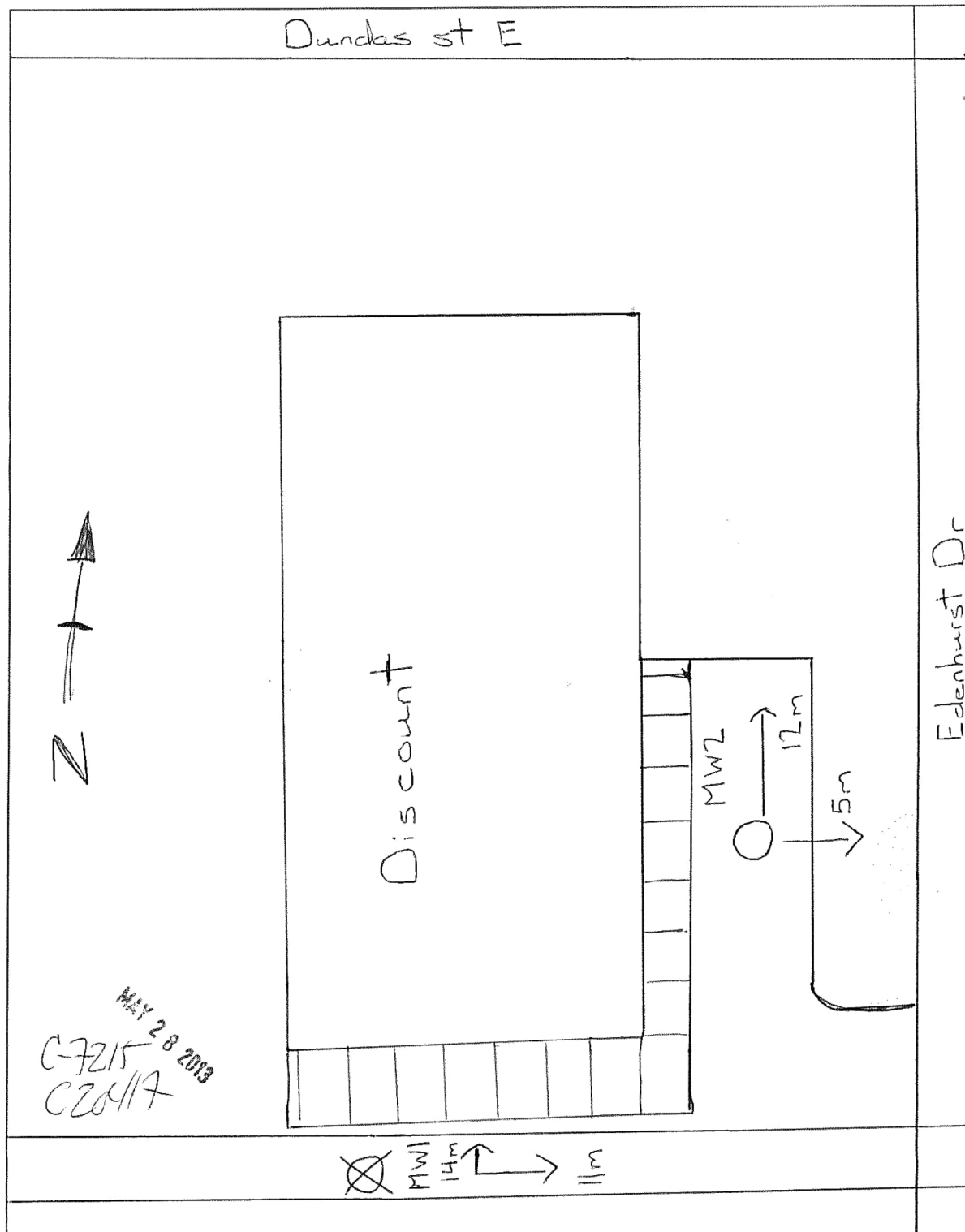
Page 1 of _____[illegible]



Note: This Well Record for Well Cluster Part 3 - Detailed Drawing of all Well Locations, must be attached to Parts 1 and 2. The drawing must include all property boundaries, an arrow indicating the North direction, all named roads and sufficient measurements to locate all wells in the cluster in relation to fixed points. The drawing must show the location of each well and each well must be numbered on the drawing to match number used for that well on the Well Record for Well Cluster Parts 1 and 2. The well with the well tag must be clearly identified on the Drawing. UTM coordinates should appear beside each well, if space permits. Additional comments on wells can be included on the drawing

Well Tag Number: # A139584

"Well Record for Well Cluster" Form Audit Number: # C 20417





Ministry of
the Environment

Well Tag No. (Place Sticker and/or Print Below)

Tag#: A156353

Regulation 903 Ontario Water Resources Act

Well Record

Measurements recorded in: ☐ Metric ☒ Imperial

Page _____ of _____

Well Owner's Information

First Name _____ Last Name / Organization Strata Soil Sampling Inc. E-mail Address _____
Mailing Address (Street Number/Name) 401 The West Mall Suite 100 Municipality Toronto Province ON Postal Code M9C5J5 Telephone No. (inc. area code) _____
☐ Well Constructed by Well Owner

Well Location

Address of Well Location (Street Number/Name) 100 Dundas Street East Township _____ Lot _____ Concession _____
County/District/Municipality _____ City/Town/Village Mississauga Province Ontario Postal Code _____
UTM Coordinates Zone 18N Easting 119174 Northing 836437 Municipal Plan and Sublot Number _____ Other WKQ-006380
NAD 83

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft)
Brown	Fill			0 3'
Brown	Silty	Sand		3' 10'
Grey	Silty	Clay		10' 18'

Annular Space		
Depth Set at (m/ft)	Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)
0.5'	FLUSHMOUNT/Concrete	
0.5' 7'	BENSEAL	
7' 18'	Sand	

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Test Hole
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial	
<input type="checkbox"/> Other, specify _____	Direct Push	<input type="checkbox"/> Other, specify _____	

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft)		
2"	PVC	0.25"	0 8'	<input type="checkbox"/> Water Supply	
				<input type="checkbox"/> Replacement Well	
				<input type="checkbox"/> Test Hole	
				<input type="checkbox"/> Recharge Well	
				<input type="checkbox"/> Dewatering Well	
				<input type="checkbox"/> Observation and/or Monitoring Hole	
				<input type="checkbox"/> Alteration (Construction)	
				<input type="checkbox"/> Abandoned, Insufficient Supply	
				<input type="checkbox"/> Abandoned, Poor Water Quality	
				<input type="checkbox"/> Abandoned, other, specify _____	
				<input type="checkbox"/> Other, specify _____	

Construction Record - Screen			
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft)
2.25"	PVC	10	8' 18'

Water Details		Hole Diameter	
Water found at Depth (m/ft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify _____	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested	Depth (m/ft)	Diameter (cm/in)
Water found at Depth (m/ft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify _____	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested	0 18'	6"
Water found at Depth (m/ft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify _____	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested		

Well Contractor and Well Technician Information
Business Name of Well Contractor Strata Soil Sampling Inc. Well Contractor's Licence No. 7 2 4 1
Business Address (Street Number/Name) 147-2 West Beaver Creek Road Municipality Richmond Hill
Province Ontario Postal Code L4B 1C6 Business E-mail Address wrecords@stratasoil.com
Bus. Telephone No. (inc. area code) 905-764-9304 Name of Well Technician (Last Name, First Name) CAROL MARR
Well Technician's Licence No. 3728 Signature of Technician and/or Contractor Date Submitted 2013/11/01

Results of Well Yield Testing

After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify _____ If pumping discontinued, give reason:	Draw Down		Recovery	
	Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
Pump intake set at (m/ft)	1	1		
Pumping rate (l/min / GPM)	2	2		
Duration of pumping hrs + min	3	3		
Final water level end of pumping (m/ft)	4	4		
If flowing give rate (l/min / GPM)	5	5		
Recommended pump depth (m/ft)	10	10		
Recommended pump rate (l/min / GPM)	15	15		
Well production (l/min / GPM)	20	20		
Disinfected? <input type="checkbox"/> Yes <input type="checkbox"/> No	25	25		
	30	30		
	40	40		
	50	50		
	60	60		

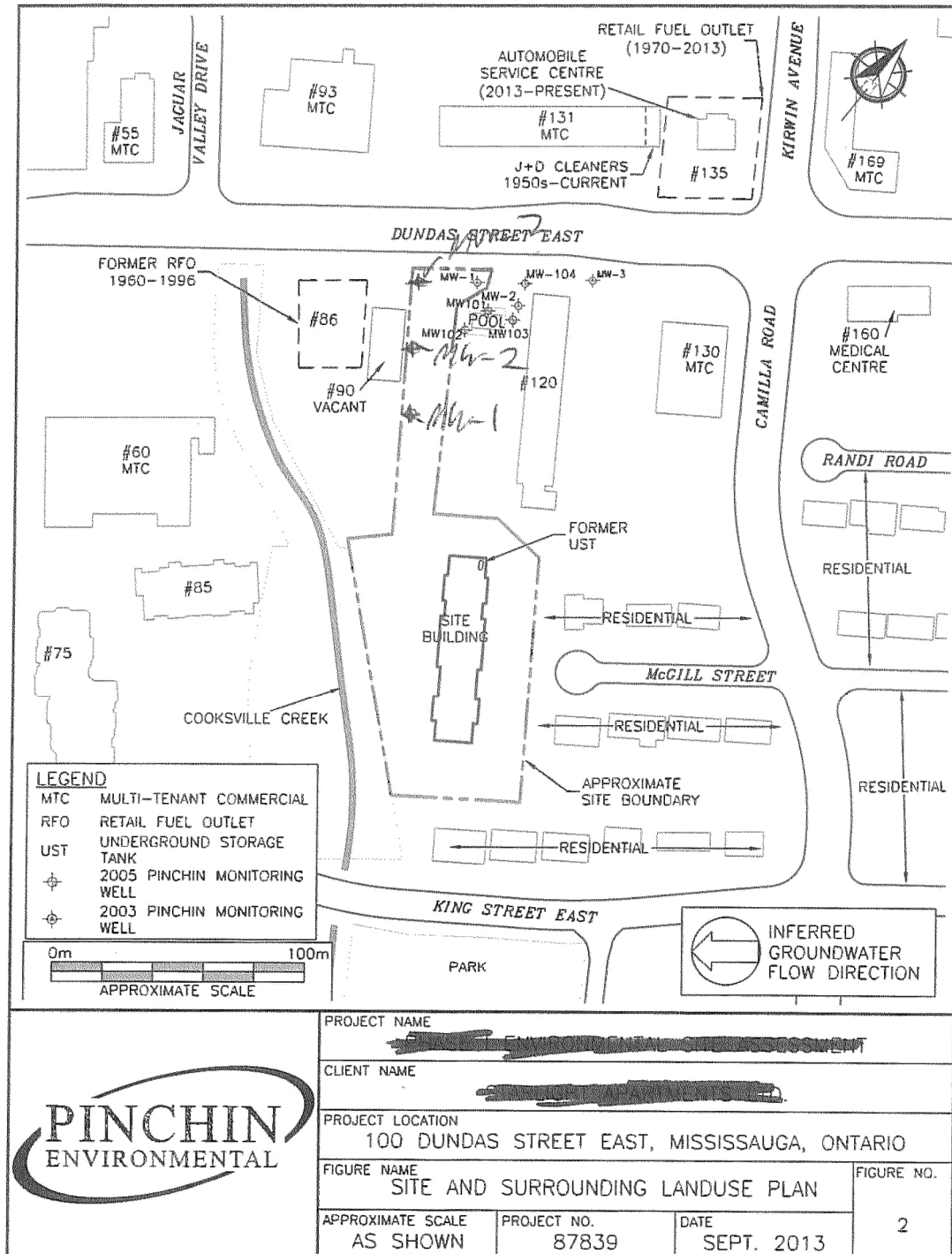
Map of Well Location

Please provide a map below following instructions on the back.

See map
MW-1

Comments: General contractor:
Pinchin Environmental

Well owner's information package delivered	Date Package Delivered	Ministry Use Only
<input type="checkbox"/> Yes <input type="checkbox"/> No	<u>2013/11/01</u>	Audit No. <u>Z 179768</u>
	Date Work Completed	Received <u>13</u>



NOV 12 2013

C-7241 2179768


 Ministry of
the Environment

Well Tag No. (Place Sticker and/or Print Below)

Tag#: A156350

S-14660

Well Record

Regulation 903 Ontario Water Resources Act

 Measurements recorded in: ☐ Metric ☒ Imperial

Page of

STARLIGHT APARTMENTS LTD.

Well Location

Address of Well Location (Street Number/Name) 100 Dundas Street East		Township	Lot	Concession
County/District/Municipality		City/Town/Village Mississauga	Province Ontario	Postal Code
UTM Coordinates NAD 83	Zone 17	Eastings 611938	Northings 438423	Municipal Plan and Sublot Number
		Other WKQ-006380 A 0 - A 02		

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft) From To
Black	Asphalt			0 4"
Brown	Silty	sand		4" 8"
Gray	Silty	clay		8 16"

Annular Space			Results of Well Yield Testing			
Depth Set at (m/ft) From To	Type of Sealant Used (Material and Type)	Volume Placed (m³/ft³)	After test of well yield, water was:		Draw Down	
0 0.5'	Flushment/concrete.		<input type="checkbox"/> Clear and sand free		Time (min)	Water Level (m/ft)
0.5' 5'	Water plug		<input type="checkbox"/> Other, specify		Static Level	
5' 16'	Sand		If pumping discontinued, give reason:			
			Pump intake set at (m/ft)		1	1
			Pumping rate (l/min / GPM)		2	2
			Duration of pumping hrs + min		3	3
			Final water level end of pumping (m/ft)		4	4
			If flowing give rate (l/min / GPM)		5	5
			Recommended pump depth (m/ft)		10	10
			Recommended pump rate (l/min / GPM)		15	15
			Well production (l/min / GPM)		20	20
			Disinfected?		25	25
			<input type="checkbox"/> Yes <input type="checkbox"/> No		30	30
					40	40
					50	50
					60	60

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Test Hole
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning
<input type="checkbox"/> Air percussion	<input type="checkbox"/> Direct Push	<input type="checkbox"/> Industrial	<input type="checkbox"/> Monitoring
<input type="checkbox"/> Other, specify		<input type="checkbox"/> Other, specify	

Construction Record - Casing			Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Well Thickness (cm/in)	Depth (m/ft) From To	
2"	PVC	0.25"	0 6'	<input type="checkbox"/> Water Supply
				<input type="checkbox"/> Replacement Well
				<input type="checkbox"/> Test Hole
				<input type="checkbox"/> Recharge Well
				<input type="checkbox"/> Dewatering Well
				<input type="checkbox"/> Observation and/or Monitoring Hole
				<input type="checkbox"/> Alteration (Construction)
				<input type="checkbox"/> Abandoned, Insufficient Supply
				<input type="checkbox"/> Abandoned, Poor Water Quality
				<input type="checkbox"/> Abandoned, other, specify
				<input type="checkbox"/> Other, specify

Construction Record - Screen			Status of Well	
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft) From To	
2.25"	PVC	10	6 16"	<input type="checkbox"/> Water Supply
				<input type="checkbox"/> Replacement Well
				<input type="checkbox"/> Test Hole
				<input type="checkbox"/> Recharge Well
				<input type="checkbox"/> Dewatering Well
				<input type="checkbox"/> Observation and/or Monitoring Hole
				<input type="checkbox"/> Alteration (Construction)
				<input type="checkbox"/> Abandoned, Insufficient Supply
				<input type="checkbox"/> Abandoned, Poor Water Quality
				<input type="checkbox"/> Abandoned, other, specify
				<input type="checkbox"/> Other, specify

Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft) From To	Diameter (cm/in)
		0 16	6"

Well Contractor and Well Technician Information			
Business Name of Well Contractor Strata Soil Sampling Inc.		Well Contractor's Licence No. 7241	
Business Address (Street Number/Name) 147-2 West Beaver Creek Road		Municipality Richmond Hill	
Province Ontario	Postal Code L4B 1G6	Business E-mail Address wrecords@stratasoil.co	
Bus. Telephone No. (inc. area code) 905-764-9304	Name of Well Technician (Last Name, First Name) CASHMAN MARK		
Well Technician's Licence No. 3708	Signature of Technician and/or Contractor Date Submitted 11/01/2013		

Map of Well Location

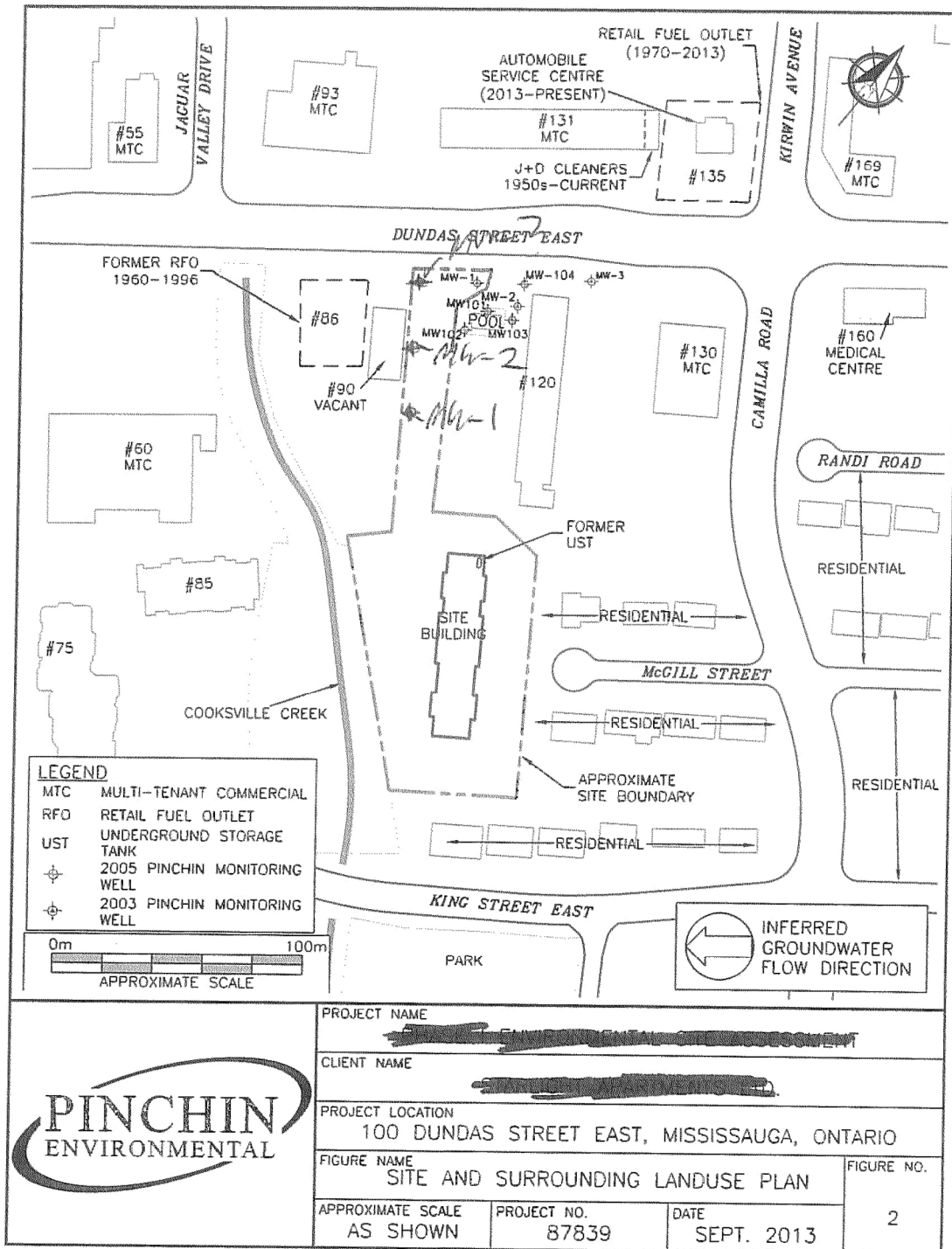
Please provide a map below following instructions on the back.

 See map
Mh-3

 Comments: General contractor:
Pinchin Environmental

Well owner's information package delivered	Date Package Delivered	Ministry Use Only
<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	2013/10/11	Audit No. 2179767
	Date Work Completed 2013/10/11	Received NOV 12 2013

S-14660



NOV 1 2013

C-2261 279767



Ontario

Ministry of
the EnvironmentMeasurements recorded in: ☐ Metric ☒ Imperial

Well Tag No. (Place Sticker and/or Print Below)

Tag#: A156352 A156352

5-14660
Well Record
Regulation 903 Ontario Water Resources Act

Page of

STARLIGHT APARTMENTS LTD.

Well Location

Address of Well Location (Street Number/Name) 100 Dundas Street East		Township	Lot	Concession
County/District/Municipality		City/Town/Village Mississauga	Province Ontario	Postal Code
UTM Coordinates NAD 83	Zone 17	Easting 611947	Northings 4826410	Municipal Plan and Sublot Number
				Other WKQ-006380 A 0 - A 02

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft) From	To
Brown	Fill			0	3'
Brown	Silty	Sand		3'	8'
Gray	Silty	Clay		8'	15.5'

Annular Space			
Depth Set at (m/ft) From	To	Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)
0	0.5'	Flash mortar/Concrete	
0.5'	4.5'	Hole Rag	
4.5'	15.5'	Sand	

Method of Construction	Well Use
<input type="checkbox"/> Cable Tool <input type="checkbox"/> Rotary (Conventional) <input type="checkbox"/> Rotary (Reverse) <input type="checkbox"/> Boring <input type="checkbox"/> Air percussion <input type="checkbox"/> Other, specify	<input type="checkbox"/> Diamond <input type="checkbox"/> Jetting <input type="checkbox"/> Driving <input type="checkbox"/> Digging <input type="checkbox"/> Direct Push <input type="checkbox"/> Public <input type="checkbox"/> Domestic <input type="checkbox"/> Livestock <input type="checkbox"/> Irrigation <input type="checkbox"/> Industrial <input type="checkbox"/> Other, specify

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fiberglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft) From	To	
2"	PVC	0.25"	0	5.5'	<input type="checkbox"/> Water Supply <input type="checkbox"/> Replacement Well <input type="checkbox"/> Test Hole <input type="checkbox"/> Recharge Well <input type="checkbox"/> Dewatering Well <input type="checkbox"/> Observation and/or Monitoring Hole <input type="checkbox"/> Alteration (Construction) <input type="checkbox"/> Abandoned, Insufficient Supply <input type="checkbox"/> Abandoned, Poor Water Quality <input type="checkbox"/> Abandoned, other, specify <input type="checkbox"/> Other, specify

Construction Record - Screen				Status of Well	
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft) From	To	
2.25"	PVC	10	5.5'	15.5'	<input type="checkbox"/> Water Supply <input type="checkbox"/> Replacement Well <input type="checkbox"/> Test Hole <input type="checkbox"/> Recharge Well <input type="checkbox"/> Dewatering Well <input type="checkbox"/> Observation and/or Monitoring Hole <input type="checkbox"/> Alteration (Construction) <input type="checkbox"/> Abandoned, Insufficient Supply <input type="checkbox"/> Abandoned, Poor Water Quality <input type="checkbox"/> Abandoned, other, specify <input type="checkbox"/> Other, specify

Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft) From	To
0		0	15.5'
15.5'			

Well Contractor and Well Technician Information			
Business Name of Well Contractor Strata Soil Sampling Inc.		Well Contractor's Licence No. 7 2 4 1	
Business Address (Street Number/Name) 147-2 West Beaver Creek Road		Municipality Richmond Hill	
Province Ontario	Postal Code L4B 1G6	Business E-mail Address wrecords@stratasoil.com	
Bus. Telephone No. (inc. area code) 905-764-9304		Name of Well Technician (Last Name, First Name) Casper Mark	
Well Technician's Licence No. 3708		Signature of Technician and/or Contractor Date Submitted 2013/11/01	

Results of Well Yield Testing

After test of well yield, water was:		Draw Down		Recovery	
<input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify		Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
If pumping discontinued, give reason:		Static Level			
Pump intake set at (m/ft)		1		1	
Pumping rate (l/min / GPM)		2		2	
Duration of pumping hrs + min		3		3	
Final water level end of pumping (m/ft)		4		4	
If flowing give rate (l/min / GPM)		5		5	
Recommended pump depth (m/ft)		10		10	
Recommended pump rate (l/min / GPM)		15		15	
Well production (l/min / GPM)		20		20	
Disinfected?		25		25	
<input type="checkbox"/> Yes <input type="checkbox"/> No		30		30	
		40		40	
		50		50	
		60		60	

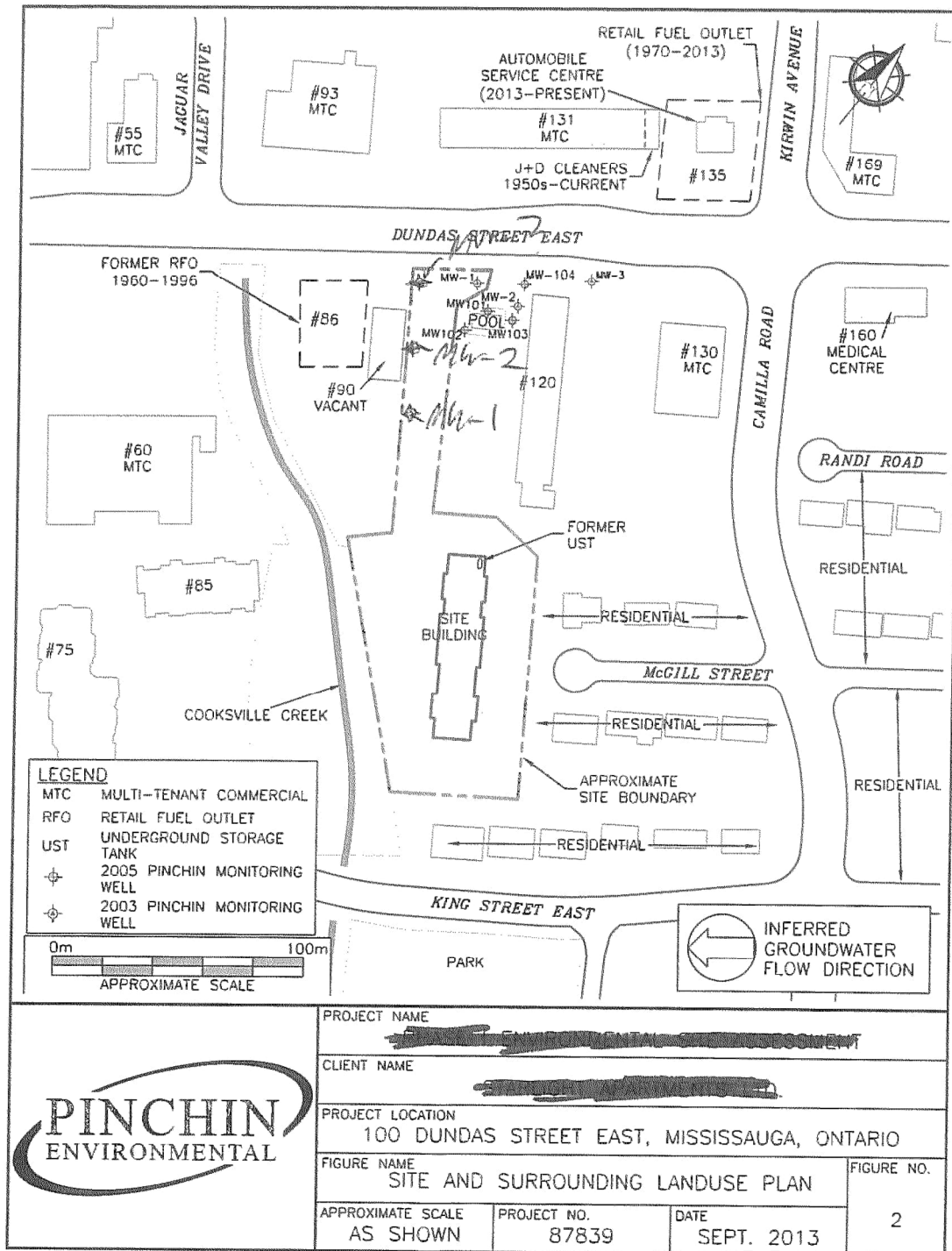
Map of Well Location

Please provide a map below following instructions on the back.

See Map
Mw-2.

Comments: General contractor:
Pinchin Environmental

Well owner's information package delivered	Date Package Delivered	Ministry Use Only	
<input type="checkbox"/> Yes <input type="checkbox"/> No	2013/11/01	Audit No. 2179766	NG
Date Work Completed	2013/11/01		



NO 7-19

C-7241 2779766



S-18471

Measurements recorded in: ☐ Metric ☒ Imperial

Page ____ of ____

Well Owner's Information

First Name	Last Name / Organization	E-mail Address	<input type="checkbox"/> Well Constructed by Well Owner
	CIBC Corporate Real Estate		
Mailing Address (Street Number/Name)	Municipality	Province	Postal Code
55 Yonge St. 4 th floor	Toronto	ON	M5E 1U9

Well Location

Address of Well Location (Street Number/Name)	Township	Lot	Concession
5 Dundas Street East			
County/District/Municipality	City/Town/Village	Province	Postal Code
	Mississauga	Ontario	
UTM Coordinates	Zone	Easting	Northing
NAD 83	17	611697	482627
Municipal Plan and Sublot Number	Other	WKQ-008852	
		A 0 - A 03	

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft)
Blk	Asphalt			0 3"
BRN	Sand	Silt		3" 5'
BRN/GRY	Silt	Clay/Sand		5' 14 1/2'
GRY	Shale	Weathered		14 1/2 17'

Annular Space			Results of Well Yield Testing					
Depth Set at (m/ft) From To		Type of Sealant Used (Material and Type)	Volume Placed (m³/ft³)	After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify	Draw Down		Recovery	
17'	6'	Sand		If pumping discontinued, give reason:	Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
6'	0	Grout plug			Static Level			
		Flowmeters			1		1	
				Pump intake set at (m/ft)	2		2	

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool <input type="checkbox"/> Rotary (Conventional) <input type="checkbox"/> Rotary (Reverse) <input type="checkbox"/> Boring <input type="checkbox"/> Air percussion <input type="checkbox"/> Other, specify	<input type="checkbox"/> Diamond <input type="checkbox"/> Jetting <input type="checkbox"/> Driving <input type="checkbox"/> Digging <input type="checkbox"/> Direct Push	<input type="checkbox"/> Public <input type="checkbox"/> Domestic <input type="checkbox"/> Livestock <input type="checkbox"/> Irrigation <input type="checkbox"/> Industrial <input type="checkbox"/> Other, specify	<input type="checkbox"/> Commercial <input type="checkbox"/> Municipal <input checked="" type="checkbox"/> Test Hole <input type="checkbox"/> Monitoring <input type="checkbox"/> Cooling & Air Conditioning

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft)	From	To
2"	PVC	.25	0	7'	

<input type="checkbox"/> Water Supply <input type="checkbox"/> Replacement Well <input checked="" type="checkbox"/> Test Hole <input type="checkbox"/> Recharge Well <input type="checkbox"/> Dewatering Well <input type="checkbox"/> Observation and/or Monitoring Hole <input type="checkbox"/> Alteration (Construction) <input type="checkbox"/> Abandoned, Insufficient Supply <input type="checkbox"/> Abandoned, Poor Water Quality <input type="checkbox"/> Abandoned, other, specify <input type="checkbox"/> Other, specify
--

Construction Record - Screen			
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft)
2.25	PVC	.10	7' 17'

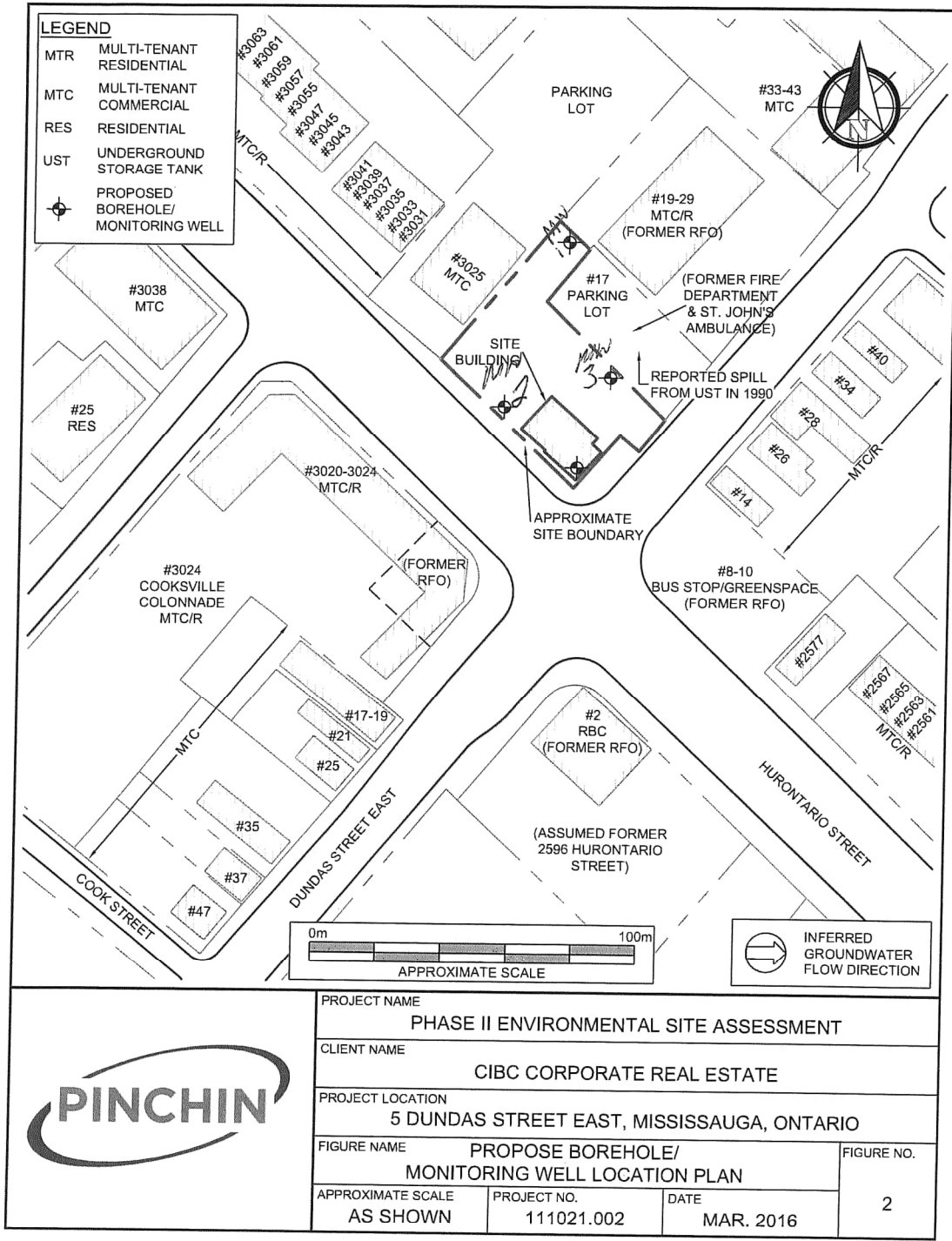
Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft)	Diameter (cm/in)
		From To	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	0	17' 6"
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify		

Business Name of Well Contractor		Well Contractor's Licence No.	
Strata Soil Sampling Inc.		7 2 4 1	
Business Address (Street Number/Name)		Municipality	
165 Shields Court		Markham	
Province	Postal Code	Business E-mail Address	
Ontario	L3R 8V2	wrecords@stratasoil.com	
Bus. Telephone No. (inc. area code)	Name of Well Technician (Last Name, First Name)		
905-764-9304	Lecien M. K.		
Well Technician's License No.	Signature of Technician and/or Contractor		
3816	[Signature]		
Date Submitted	20160911		

Map of Well Location	
Please provide a map below following instructions on the back.	
Mw1	

Comments:		General contractor: Pinchin Environmental	
Well owner's information package delivered	Date Package Delivered	Ministry Use Only	
<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	20160911	Audit No.	2231550
Date Work Completed	27 MAY 2016	Received	27 MAY 2016

5-18471



MAY 27 2016

C-724 223580



Ontario

Ministry of the Environment
and Climate Change

Well Tag

Tag #: A197938

A197938

Regulation 903 Ontario Water Resources Act

Page ____ of ____

Measurements recorded in: ☐ Metric ☒ Imperial

Well Owner's Information

First Name

Last Name / Organization

E-mail Address

☐ Well Constructed
by Well Owner

Mailing Address (Street Number/Name)

Municipality

Province

Postal Code

Telephone No. (inc. area code)

Well Location

Address of Well Location (Street Number/Name)

Township

Lot

Concession

County/District/Municipality

City/Town/Village

Province
Ontario

Postal Code

UTM Coordinates

Zone Easting

Northing

Municipal Plan and Sublot Number

Other WKQ-008852

A 0 - A 03

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft) From To
B/K	Asphalt			0 3'
BRN	Sand	S.H.		3' 5'
BRN/GRY	S.H.	Sand/Clay		5' 12 1/2'
GRY	Shale		Weathered	12 1/2' 17'

Annular Space			
Depth Set at (m/ft) From To	Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)	
17' 6"	Sand		
6' 0"	Grout		
	Flintman		

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Not used
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Municipal
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input checked="" type="checkbox"/> Test Hole
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial	<input type="checkbox"/> Cooling & Air Conditioning
<input checked="" type="checkbox"/> Other, specify Direct Push		<input type="checkbox"/> Other, specify	

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Well Thickness (cm/in)	Depth (m/ft) From To		
2"	PVC	.25	0 7'	<input type="checkbox"/> Water Supply	
				<input type="checkbox"/> Replacement Well	
				<input type="checkbox"/> Test Hole	
				<input type="checkbox"/> Recharge Well	
				<input type="checkbox"/> Dewatering Well	
				<input type="checkbox"/> Observation and/or Monitoring Hole	
				<input type="checkbox"/> Alteration (Construction)	
				<input type="checkbox"/> Abandoned, Insufficient Supply	
				<input type="checkbox"/> Abandoned, Poor Water Quality	
				<input type="checkbox"/> Abandoned, other, specify	
				<input type="checkbox"/> Other, specify	

Construction Record - Screen				Status of Well	
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft) From To		
2.25	PVC	.110	7' 14'	<input type="checkbox"/> Water Supply	
				<input type="checkbox"/> Replacement Well	
				<input type="checkbox"/> Test Hole	
				<input type="checkbox"/> Recharge Well	
				<input type="checkbox"/> Dewatering Well	
				<input type="checkbox"/> Observation and/or Monitoring Hole	
				<input type="checkbox"/> Alteration (Construction)	
				<input type="checkbox"/> Abandoned, Insufficient Supply	
				<input type="checkbox"/> Abandoned, Poor Water Quality	
				<input type="checkbox"/> Abandoned, other, specify	
				<input type="checkbox"/> Other, specify	

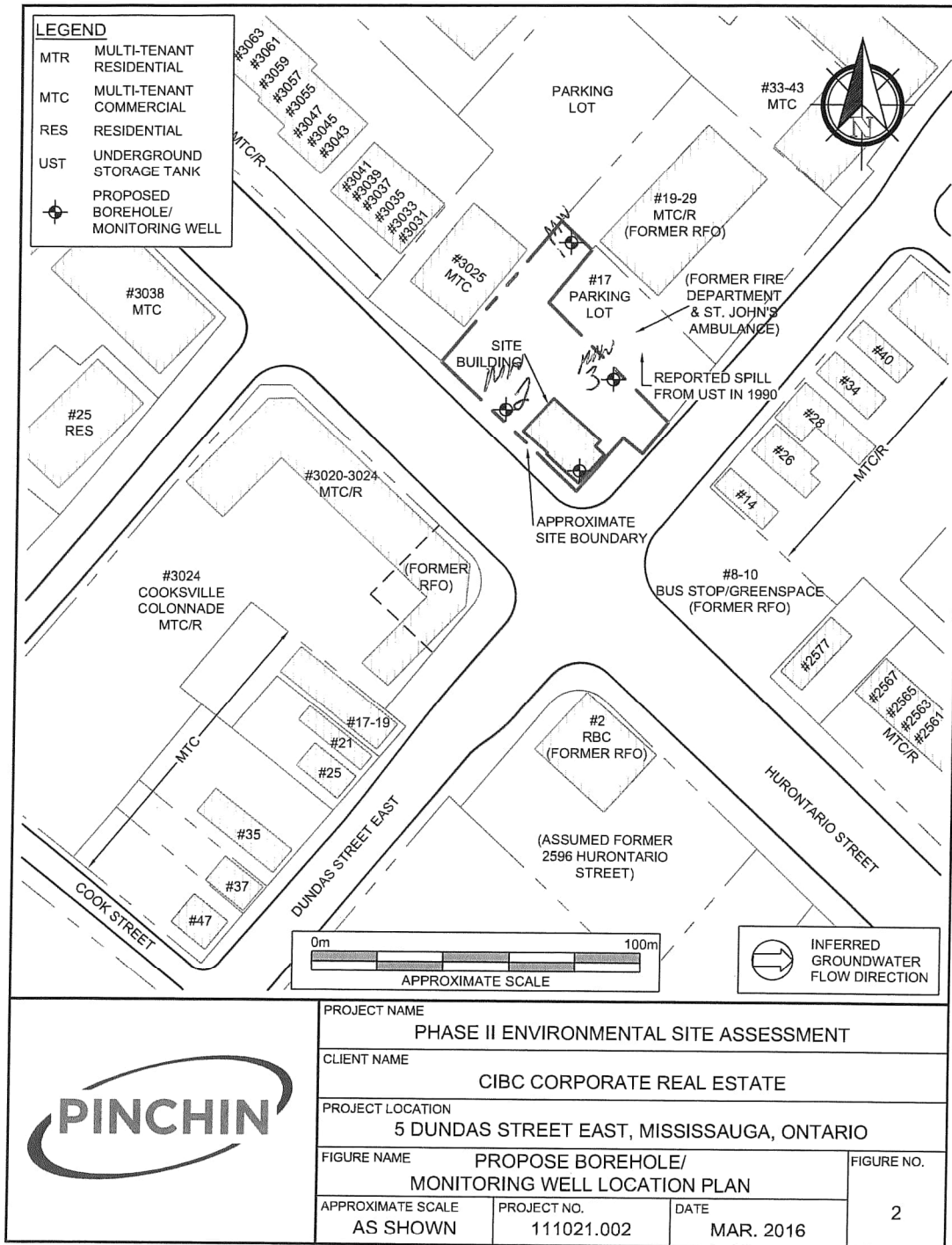
Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft) From To	Diameter (cm/in)
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	0 17' 6"	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify		

Well Contractor and Well Technician Information			
Business Name of Well Contractor	Well Contractor's Licence No.		
Strata Soil Sampling Inc.	7 2 4 1		
Business Address (Street Number/Name)	Municipality		
165 Shields Court	Markham		
Province	Postal Code	Business E-mail Address	
Ontario	L3R 8V2	wrecords@stratasoil.com	
Bus. Telephone No. (inc. area code)	Name of Well Technician (Last Name, First Name)		
905-764-9304	Leccese		
Well Technician's Licence No.	Signature of Technician and/or Contractor	Date Submitted	
13016		2010/09/11	

Results of Well Yield Testing			
After test of well yield, water was:		Draw Down	
<input type="checkbox"/> Clear and sand free		Time (min)	Water Level (m/ft)
<input type="checkbox"/> Other, specify		Time (min)	Water Level (m/ft)
If pumping discontinued, give reason:		Static Level	
Pump intake set at (m/ft)		1	1
Pumping rate (l/min / GPM)		2	2
Duration of pumping hrs + min		3	3
Final water level end of pumping (m/ft)		4	4
If flowing give rate (l/min / GPM)		5	5
Recommended pump depth (m/ft)		10	10
Recommended pump rate (l/min / GPM)		15	15
Well production (l/min / GPM)		20	20
Disinfected?		25	25
<input type="checkbox"/> Yes <input type="checkbox"/> No		30	30
		40	40
		50	50
		60	60

Map of Well Location	
Please provide a map below following instructions on the back.	
Mn 2	
Comments: General contractor: Pinchin Environmental	
Well owner's information package delivered	Date Package Delivered
<input type="checkbox"/> Yes <input type="checkbox"/> No	2010/09/11
Date Work Completed	2010/09/11
Ministry Use Only	
Audit No. 2231549	
AY 27 2010	
Received	

5-18471



MAY 27 2016

C-724 7281549

Ministry of the Environment
and Climate Change

Well Tag #: A197940

A197940

Regulation 903 Ontario Water Resources Act

Page of

Measurements recorded in: ☐ Metric ☒ Imperial

Well Owner's Information

First Name Last Name / Organization E-mail Address ☐ Well Constructed by Well Owner

Mailing Address (Street Number/Name) Municipality Province Postal Code Telephone No. (inc. area code)

55 Yonge St 4th Floor Toronto ON M5E 1B4

Well Location

Address of Well Location (Street Number/Name) Township Lot Concession

5 Dundas Street East

County/District/Municipality City/Town/Village Province Postal Code

Mississauga Ontario

UTM Coordinates Zone Easting Northing Other WKQ-008852

NAD 83 17 611 714 9220242 A0 - A03

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft)	
				From	To
BLK	Asphalt			0	3'
BRN	Sand	3:1		3'	5'
BRN/GRY	Silt	Clay		5'	14'
GRY	Shale		Weathered	14'	17'

Annular Space		
Depth Set at (m/ft)	Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)
From To		
17' 6"	Sand	
6' 0"	Hotpack	
	Flowmud	

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Test Hole
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial	
<input checked="" type="checkbox"/> Other, specify	Direct Push	<input type="checkbox"/> Other, specify	

Construction Record - Casing			Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft)	
			From To	
2"	PVC	.25	0	7'

<input type="checkbox"/> Water Supply	<input type="checkbox"/> Replacement Well	<input checked="" type="checkbox"/> Test Hole
<input type="checkbox"/> Recharge Well	<input type="checkbox"/> Dewatering Well	<input type="checkbox"/> Observation and/or Monitoring Hole
<input type="checkbox"/> Alteration (Construction)	<input type="checkbox"/> Abandoned, Insufficient Supply	<input type="checkbox"/> Abandoned, Poor Water Quality
<input type="checkbox"/> Abandoned, other, specify		
<input type="checkbox"/> Other, specify		

Construction Record - Screen			Depth (m/ft)	
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	From	To
2.25	PVC	.10	7'	17'

Water Details		Hole Diameter	
Water found at Depth (m/ft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested	Depth (m/ft) From To	Diameter (cm/in)
Water found at Depth (m/ft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested	0	17' 6"
Water found at Depth (m/ft) <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested		

Well Contractor and Well Technician Information			
Business Name of Well Contractor	Well Contractor's Licence No.		
Strata Soil Sampling Inc.	7 2 4 1		
Business Address (Street Number/Name)	Municipality		
165 Shields Court	Markham		
Province	Postal Code	Business E-mail Address	
Ontario	L3R 8V2	wrecords@stratasoil.com	
Bus. Telephone No. (inc. area code)	Name of Well Technician (Last Name, First Name)		
905-764-9304	Leccese, Nick		
Well Technician's Licence No.	Signature of Technician and/or Contractor	Date Submitted	
13816		20150411	

Results of Well Yield Testing

After test of well yield, water was:	Draw Down		Recovery	
	Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
<input type="checkbox"/> Clear and sand free				
<input type="checkbox"/> Other, specify				
If pumping discontinued, give reason:	Static Level			
	1		1	
	Pump intake set at (m/ft)	2	2	
	Pumping rate (l/min / GPM)	3	3	
	Duration of pumping hrs + min	4	4	
	Final water level end of pumping (m/ft)	5	5	
If flowing give rate (l/min / GPM)	10		10	
	15		15	
	20		20	
	25		25	
	30		30	
	40		40	
Recommended pump depth (m/ft)	50		50	
	60		60	
Recommended pump rate (l/min / GPM)				
Well production (l/min / GPM)				
Disinfected?				
<input type="checkbox"/> Yes <input type="checkbox"/> No				

Map of Well Location

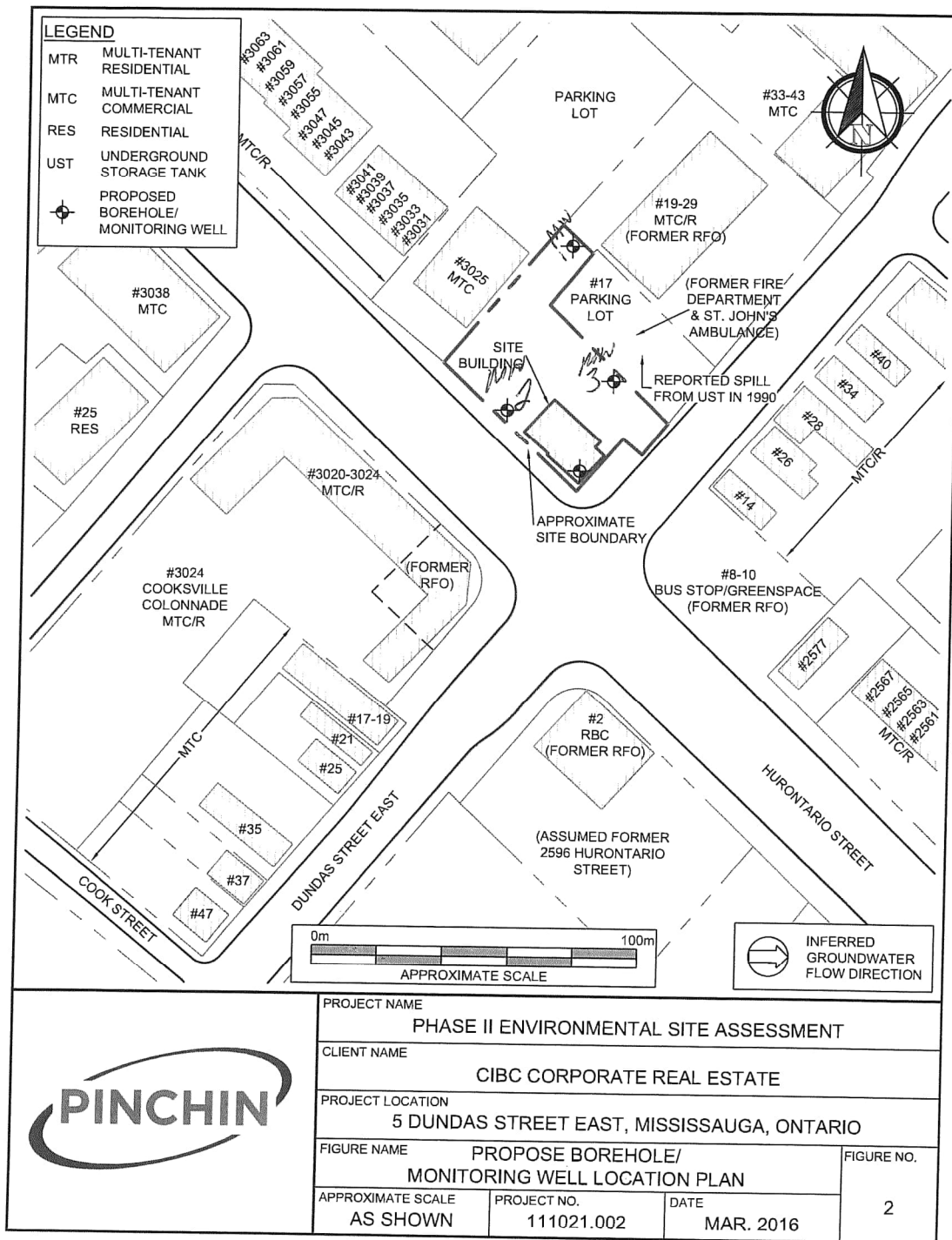
Please provide a map below following instructions on the back.

M13

Comments: General contractor:
Pinchin Environmental

Well owner's Information package delivered	Date Package Delivered		Ministry Use Only	
	Y	M	D	Audit No.
<input type="checkbox"/> Yes	Y	Y	Y	2231548
<input type="checkbox"/> No				
Date Work Completed				Received
20150411				MAY 27 2015

5-18471



MAY 27 2016

C-741 7231548



Ministry of the Environment
and Climate Change

Well Tag No. (Place Sticker and/or Print Below)

A197985

S-18471

Well Record

Regulation 903 Ontario Water Resources Act

Measurements recorded in: ☐ Metric ☒ Imperial

Page _____ of _____

Well Owner's Information

First Name	Last Name / Organization	E-mail Address	<input type="checkbox"/> Well Constructed by Well Owner
	CIBC Corporate Real Estate		
Mailing Address (Street Number/Name)	Municipality	Province	Postal Code
55 Yonge St, 4th floor	Toronto	ON	M5E1B4

Well Location

Address of Well Location (Street Number/Name)	Township	Lot	Concession
5 Dundas Street East			
County/District/Municipality	City/Town/Village	Province	Postal Code
	Mississauga	Ontario	
UTM Coordinates	Zone	Easting	Northing
NAD 83	17	761171	14826220
Municipal Plan and Sublot Number	Other	WKQ-008919	
		A 0 - A 00	

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft)
Grey	Concrete			From To
Brown	Fill			0 0.5'
Grey	clay			0.5' 2'
				2' 4.5'

Annular Space		
Depth Set at (m/ft)	Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)
From To		
0 0.5'	concrete/flash mount	
0.5' 1.5'	Benseal	
1.5' 4.5'	Sand	

Method of Construction		Well Use	
<input type="checkbox"/> Cable Tool	<input type="checkbox"/> Diamond	<input type="checkbox"/> Public	<input type="checkbox"/> Commercial
<input type="checkbox"/> Rotary (Conventional)	<input type="checkbox"/> Jetting	<input type="checkbox"/> Domestic	<input type="checkbox"/> Municipal
<input type="checkbox"/> Rotary (Reverse)	<input type="checkbox"/> Driving	<input type="checkbox"/> Livestock	<input type="checkbox"/> Test Hole
<input type="checkbox"/> Boring	<input type="checkbox"/> Digging	<input type="checkbox"/> Irrigation	<input type="checkbox"/> Cooling & Air Conditioning
<input type="checkbox"/> Air percussion		<input type="checkbox"/> Industrial	
<input checked="" type="checkbox"/> Other, specify	Direct Push	<input type="checkbox"/> Other, specify	

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fibreglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft)	<input type="checkbox"/> Water Supply	
From To				<input type="checkbox"/> Replacement Well	
1.25"	PVC	0.125"	0 2'	<input checked="" type="checkbox"/> Test Hole	
				<input type="checkbox"/> Recharge Well	
				<input type="checkbox"/> Dewatering Well	
				<input type="checkbox"/> Observation and/or Monitoring Hole	
				<input type="checkbox"/> Alteration (Construction)	
				<input type="checkbox"/> Abandoned, Insufficient Supply	
				<input type="checkbox"/> Abandoned, Poor Water Quality	
				<input type="checkbox"/> Abandoned, other, specify	
				<input type="checkbox"/> Other, specify	

Construction Record - Screen			
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft)
From To			
1.5"	PVC	10	2' 4.5'

Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Untested <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft)	Diameter (cm/in)
From To		From To	
		0 4.5'	2.25"

Business Name of Well Contractor		Well Contractor's Licence No.
Strata Soil Sampling Inc.		7 2 4 1
Business Address (Street Number/Name)		Municipality
165 Shields Court		Markham
Province	Postal Code	Business E-mail Address
Ontario	L3R 8V2	wrecords@stratasoil.com

Bus. Telephone No. (inc. area code)	Name of Well Technician (Last Name, First Name)
905-764-9304	Walker, Jonathan
Well Technician's Licence No.	Signature of Technician and/or Contractor
3 8 3 3	
Date Submitted	
Y Y Y Y M M D D	

Results of Well Yield Testing				
After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, <i>specify</i>	Draw Down		Recovery	
	Time (min)	Water Level (m/ft)	Time (min)	Water Level (m/ft)
If pumping discontinued, give reason:	Static Level			
	1		1	
Pump intake set at (m/ft)	2		2	
Pumping rate (l/min / GPM)	3		3	
Duration of pumping ____ hrs + ____ min	4		4	
	5		5	
Final water level end of pumping (m/ft)	10		10	
If flowing give rate (l/min / GPM)	15		15	
	20		20	
Recommended pump depth (m/ft)	25		25	
	30		30	
Recommended pump rate (l/min / GPM)	40		40	
	50		50	
Well production (l/min / GPM)	60		60	
Disinfected? <input type="checkbox"/> Yes <input type="checkbox"/> No				

Map of Well Location

Please provide a map below following instructions on the back.

See Map
mwl

Comments: General contractor:
Pinchin Environmental

Well owner's information package delivered <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	Date Package Delivered	Ministry Use Only Audit No. 231466 MAY 27 2016 MAY 27 2016
	Date Work Completed	
	20160424	

Measurements recorded in: ☐ Metric ☒ Imperial

Well Tag No. (Place Sticker and Print Below)

A199312

A199312

Tag#: A199312

Well Record

Regulation 903 Ontario Water Resources Act

S-20827 Page of

ROYAL BANK OF CANADA

Address of Well Location (Street Number/Name) 2 Dundas Street West		Township	Lot	Concession
County/District/Municipality		City/Town/Village Mississauga	Province Ontario	Postal Code
UTM Coordinates Zone Easting Northing NAD 83 17 611175P 4826092		Municipal Plan and Sublot Number		Other WKQ-010354 A 0 - A 02

Overburden and Bedrock Materials/Abandonment Sealing Record (see instructions on the back of this form)

General Colour	Most Common Material	Other Materials	General Description	Depth (m/ft) From To
Blk	Asphalt			0 3'
Brown	silt	clay		3' 10'
Grey	Shale			10' 13'

Annular Space			Results of Well Yield Testing			
Depth Set at (m/ft) From To	Type of Sealant Used (Material and Type)	Volume Placed (m ³ /ft ³)	After test of well yield, water was: <input type="checkbox"/> Clear and sand free <input type="checkbox"/> Other, specify	Draw Down Time (min) Water Level (m/ft)	Recovery Time (min) Water Level (m/ft)	Static Level
0 6'	Concrete					
6' 2'	Bentonite					
2' 13'	Sand					

Method of Construction	Well Use
<input type="checkbox"/> Cable Tool <input checked="" type="checkbox"/> Rotary (Conventional) <input type="checkbox"/> Rotary (Reverse) <input type="checkbox"/> Boring <input type="checkbox"/> Air percussion <input type="checkbox"/> Other, specify	<input type="checkbox"/> Diamond <input type="checkbox"/> Jetting <input type="checkbox"/> Driving <input type="checkbox"/> Digging <input type="checkbox"/> Industrial <input type="checkbox"/> Other, specify
<input type="checkbox"/> Public <input type="checkbox"/> Domestic <input type="checkbox"/> Livestock <input type="checkbox"/> Irrigation <input type="checkbox"/> Other, specify	<input type="checkbox"/> Commercial <input type="checkbox"/> Municipal <input type="checkbox"/> Test Hole <input type="checkbox"/> Cooling & Air Conditioning <input type="checkbox"/> Not used <input type="checkbox"/> Dewatering <input type="checkbox"/> Monitoring

Construction Record - Casing				Status of Well	
Inside Diameter (cm/in)	Open Hole OR Material (Galvanized, Fiberglass, Concrete, Plastic, Steel)	Wall Thickness (cm/in)	Depth (m/ft) From To		
2"	PVC	.225	0 3'		

Construction Record - Screen				Status of Well	
Outside Diameter (cm/in)	Material (Plastic, Galvanized, Steel)	Slot No.	Depth (m/ft) From To		
2.25	PVC	10	3' 13'		

Water Details		Hole Diameter	
Water found at Depth (m/ft)	Kind of Water: <input type="checkbox"/> Fresh <input type="checkbox"/> Gas <input type="checkbox"/> Other, specify	Depth (m/ft) From To	Diameter (cm/in)
		0 13	6"

Well Contractor and Well Technician Information	
Business Name of Well Contractor Strata Soil Sampling Inc.	Well Contractor's Licence No. 7 2 4 1
Business Address (Street Number/Name) 165 Shields Court	Municipality Markham
Province Ontario	Postal Code L3R 8V2
Business E-mail Address wrecords@stratasoil.com	
Bus. Telephone No. (inc. area code) 905-764-9304	Name of Well Technician (Last Name, First Name) Vanderboor, Andrew
Well Technician's Licence No. 3614	Signature of Technician and/or Contractor Andrew Vanderboor
Date Submitted 2017 09 29	

Map of Well Location

Please provide a map below following instructions on the back.

See Map

B"

Comments: General contractor:
Pinchin Environmental

Well owner's information package delivered <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	Date Package Delivered 24 1 7 2017	Ministry Use Only Audit No. 2270104 OCT 5 2017
Date Work Completed 24 1 7 2017	Received	



APPENDIX D

Water Balance Summary Tables

Table C: Water Balance Summary Table

Characteristic	Site			Change (Pre to Post)
	Pre-Development	Post-Development		
	Inputs (Volume)			
Precipitation (m ³ /yr)	4,974	4,974	0	0%
Run-On (m ³ /yr)	0	0	0	NA
Other Inputs (m ³ /yr)	0	0	0	NA
Total Inputs (m ³ /yr)	4,974	4,974	0	0%
	Outputs (Volume)			
Precipitation Surplus (m ³ /yr)	1,845	2,993	1,147	62%
Net Surplus (m ³ /yr)	1,845	2,993	1,147	62%
Evapotranspiration (m ³ /yr)	3,129	1,981	-1,147	-37%
Infiltration (m ³ /yr)	862	412	-450	-52%
Rooftop Infiltration (m ³ /yr)	0	0	0	NA
Total Infiltration (m³/yr)	862	412	-450	-52%
Run-Off Pervious Areas (m ³ /yr)	983	441	-542	-55%
Run-Off Impervious Areas (m ³ /yr)	0	2,139	2,139	NA
Total Run-Off (m ³ /yr)	983	2,581	1,598	163%
Total Outputs (m³/yr)	4,974	4,974	0	0%

Table A: Pre-Development

Catchment Designation	Forest	Landscaped Grass	Total
Area (m ²)	4,300	2,085	6,385
Pervious Area (m ²)	4,300	2,085	6,385
Impervious Area (m ²)	0	0	0
Infiltration Factors			
Topography Infiltration Factor	0.2	0.2	
Soil Infiltration Factor	0.1	0.1	
Land Cover Infiltration Factor	0.2	0.1	
Infiltration Factor	0.5	0.4	
Run-Off Coefficient	0.5	0.6	
Run-Off From Impervious Surfaces	0.8	0.8	
Inputs (Per Unit Area)			
Precipitation (mm/yr)	779	779	779
Rainfall (mm/yr)	632	632	632
Run-On (mm/yr)	0	0	0
Other Inputs (mm/yr)	0	0	0
Total Inputs (mm/yr)	779	779	779
Outputs (Per Unit Area)			
Precipitation Surplus (mm/yr)	289	289	289
Net Surplus (mm/yr)	289	289	289
Evapotranspiration (mm/yr)	490	490	490
Infiltration (mm/yr)	145	116	135
Surplus Infiltration (mm/yr)	0	0	0
Total Infiltration (mm/yr)	145	116	135
Run-Off Pervious Areas (mm/yr)	145	173	154
Run-Off Impervious Areas (mm/yr)	0	0	0
Total Run-Off (mm/yr)	145	173	154
Total Outputs (mm/yr)	779	779	779
Difference (Inputs - Outputs)			
Inputs (Volumes)			
Precipitation (m ³ /yr)	3,350	1,624	4,974
Run-On (m ³ /yr)	0	0	0
Other Inputs (m ³ /yr)	0	0	0
Total Inputs (m³/yr)	3,350	1,624	4,974
Outputs (Volumes)			
Precipitation Surplus (m ³ /yr)	1,243	603	1,845
Net Surplus (m ³ /yr)	1,243	603	1,845
Evapotranspiration (m ³ /yr)	2,107	1,022	3,129
Infiltration (m ³ /yr)	621	241	862
Surplus Infiltration (m ³ /yr)	0	0	0
Total Infiltration (m³/yr)	621	241	862
Run-Off Pervious Areas (m ³ /yr)	621	362	983
Run-Off Impervious Areas (m ³ /yr)	0	0	0
Total Run-Off (m ³ /yr)	621	362	983
Total Outputs (m³/yr)	3,350	1,624	4,974
Difference (Inputs - Outputs)			
	0	0	0

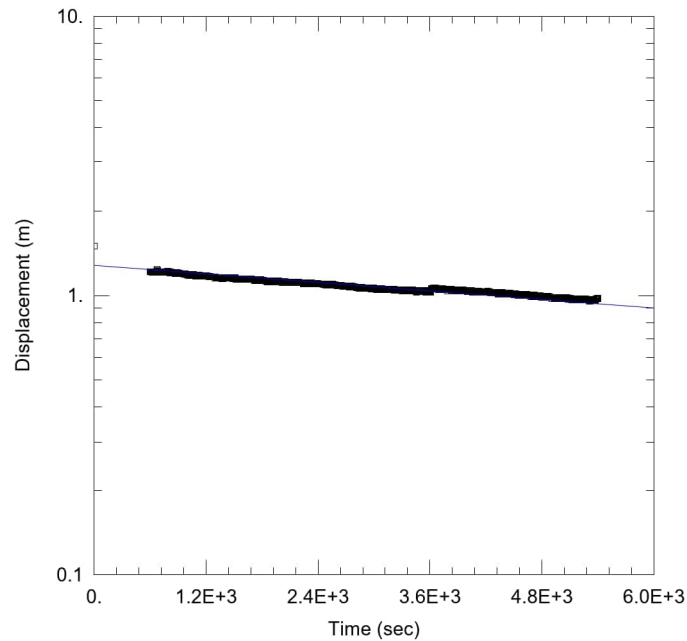
Table B: Post-Development (no mit)

Catchment Designation	Parkland Dedication	Landscaped Grass	Structure	Total
Area (m ²)	2,450	502	3,433	6,385
Pervious Area (m ²)	2,450	502	0	2,952
Impervious Area (m ²)	0	0	3,433	3,433
Infiltration Factors				
Topography Infiltration Factor	0.2	0.2	0	
Soil Infiltration Factor	0.1	0.1	0	
Land Cover Infiltration Factor	0.2	0.1	0	
Infiltration Factor	0.5	0.4	0	
Run-Off Coefficient	0.5	0.6	1	
Run-Off From Impervious Surfaces	0.8	0.8	0.8	
Inputs (Per Unit Area)				
Precipitation (mm/yr)	779	779	779	779
Rainfall (mm/yr)	632	632	632	632
Run-On (mm/yr)	0	0	0	0
Other Inputs (mm/yr)	0	0	0	0
Total Inputs (mm/yr)	779	779	779	779
Outputs (Per Unit Area)				
Precipitation Surplus (mm/yr)	289	289	623	469
Net Surplus (mm/yr)	289	289	623	469
Evapotranspiration (mm/yr)	490	490	156	310
Infiltration (mm/yr)	145	116	0	65
Surplus Infiltration (mm/yr)	0	0	0	0
Total Infiltration (mm/yr)	145	116	0	65
Run-Off Pervious Areas (mm/yr)	145	173	0	69
Run-Off Impervious Areas (mm/yr)	0	0	623	335
Total Run-Off (mm/yr)	145	173	623	404
Total Outputs (mm/yr)	779	779	779	779
Difference (Inputs - Outputs)	0	0	0	0
Inputs (Volumes)				
Precipitation (m ³ /yr)	1,909	391	2,674	4,974
Run-On (m ³ /yr)	0	0	0	0
Other Inputs (m ³ /yr)	0	0	0	0
Total Inputs (m³/yr)	1,909	391	2,674	4,974
Outputs (Volumes)				
Precipitation Surplus (m ³ /yr)	708	145	2,139	2,993
Net Surplus (m ³ /yr)	708	145	2,139	2,993
Evapotranspiration (m ³ /yr)	1,201	246	535	1,981
Infiltration (m ³ /yr)	354	58	0	412
Surplus Infiltration (m ³ /yr)	0	0	0	0
Total Infiltration (m³/yr)	354	58	0	412
Run-Off Pervious Areas (m ³ /yr)	354	87	0	441
Run-Off Impervious Areas (m ³ /yr)	0	0	2,139	2,139
Total Run-Off (m ³ /yr)	354	87	2,139	2,581
Total Outputs (m³/yr)	1,909	391	2,674	4,974
Difference (Inputs - Outputs)	0	0	0	0

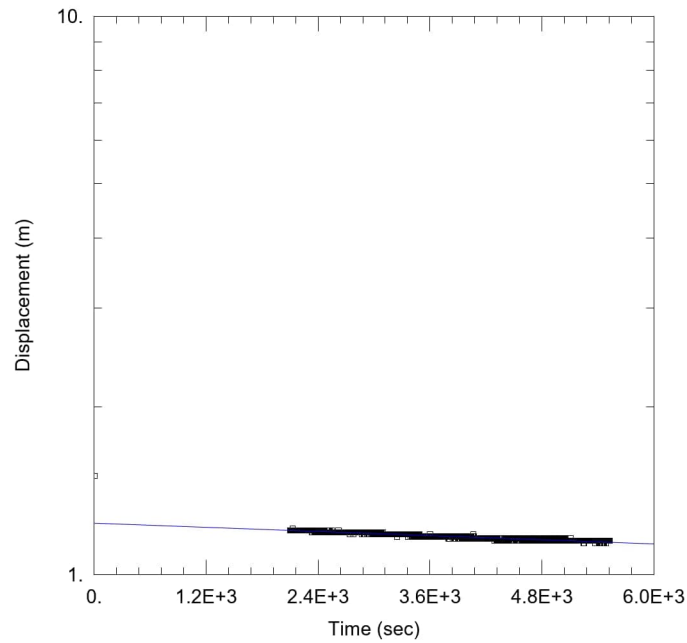


APPENDIX E

Hydraulic Conductivity Testing



WELL TEST ANALYSIS	
Data Set: <u>X:\...\BH2 Logger.aqt</u>	Time: <u>17:50:09</u>
Date: <u>06/02/22</u>	
PROJECT INFORMATION	
Company: <u>Azimuth Environmental</u>	
Client: <u>Azure Group</u>	
Project: <u>22-056</u>	
Location: <u>Mississauga</u>	
Test Date: <u>May 11th 2022</u>	
AQUIFER DATA	
Saturated Thickness: <u>3.34</u> m	Anisotropy Ratio (Kz/Kr): <u>1.</u>
WELL DATA (BH2)	
Initial Displacement: <u>1.5</u> m	Static Water Column Height: <u>4.9</u> m
Total Well Penetration Depth: <u>3.34</u> m	Screen Length: <u>3.05</u> m
Casing Radius: <u>0.0254</u> m	Wellbore Radius: <u>0.1524</u> m
SOLUTION	
Aquifer Model: <u>Unconfined</u>	Solution Method: <u>Hvorslev</u>
K = <u>2.278E-8</u> m/sec	y0 = <u>1.28</u> m



<u>WELL TEST ANALYSIS</u>	
Data Set: <u>X:\...\BH106 Logger.aqt</u>	Time: <u>17:49:51</u>
Date: <u>06/02/22</u>	
<u>PROJECT INFORMATION</u>	
Company: <u>Azimuth Environmental</u>	
<u>AQUIFER DATA</u>	
Saturated Thickness: <u>3.58 m</u>	Anisotropy Ratio (Kz/Kr): <u>1.</u>
<u>WELL DATA (BH106)</u>	
Initial Displacement: <u>1.5 m</u>	Static Water Column Height: <u>3.84 m</u>
Total Well Penetration Depth: <u>3.58 m</u>	Screen Length: <u>3.05 m</u>
Casing Radius: <u>0.0254 m</u>	Wellbore Radius: <u>0.1524 m</u>
<u>SOLUTION</u>	
Aquifer Model: <u>Unconfined</u>	Solution Method: <u>Hvorslev</u>
K = <u>5.564E-9 m/sec</u>	y0 = <u>1.236 m</u>



APPENDIX F

Water Quality Data

Results of Surface Water Chemical Analyses

			Provincial Water Quality Objectives (1994)	BH-3
				Sampled on:
				2022-05-11
				Sampled by:
			Objective	Azimuth
Parameter	Symbol	Units		Analyzed
				Caduceon
Saturation pH		N/A	-	6.73
pH		N/A	6.5-8.5	7.51
Langlier Index		N/A	-	0.777
Alkalinity (as CaCO3)		mg/L	262	244
Bicarbonate (as CaCO3)	HCO ₃ ⁻	mg/L	-	244
Carbonate (as CaCO3)	CO ₃ ⁻²	mg/L	-	< 5
Hydroxide		mg/L	-	< 5
Electrical Conductivity		uS/cm	-	3380
Fluoride	F	mg/L	-	< 1
Chloride	Cl ⁻	mg/L	-	777
Nitrate as N	NO ₃ -N	mg/L	-	5.47
Nitrite as N	NO ₂ -N	mg/L	-	< 0.5
Bromide	Br ⁻	mg/L	-	< 4
Sulphate	SO ₄ ⁻²	mg/L	-	83
Calcium	Ca	mg/L	-	247
Magnesium	Mg	mg/L	-	26.7
Sodium	Na	mg/L	-	393
Potassium	K	mg/L	-	4.9
Ammonia as N	NH ₃ -N	mg/L	-	0.02
Phosphate as P	PO ₄ ⁻³	mg/L	-	0.005
Total Phosphorus	P	mg/L	0.03	2.89
Reactive Silica	Si	mg/L	-	9.33
Total Organic Carbon	TOC	mg/L	-	1.1
Colour		Colour Units	-	< 2
Turbidity		NTU	-	181
Aluminum	Al	mg/L	0.075	0.29
Antimony	Sb	mg/L	0.02	0.0002
Arsenic	As	mg/L	0.005	< 0.0003
Barium	Ba	mg/L	-	0.265
Boron	B	mg/L	0.2	0.04
Cadmium	Cd	mg/L	0.0002	< 0.000029
Chromium	Cr	mg/L	0.0089	0.001
Copper	Cu	mg/L	0.005	0.0009
Iron	Fe	mg/L	0.3	0.259
Lead	Pb	mg/L	0.001	0.00024
Manganese	Mn	mg/L	-	0.032
Mercury	Hg	mg/L	0.0002	< 0.00002
Molybdenum	Mo	mg/L	0.04	0.0003
Nickel	Ni	mg/L	0.025	< 0.01
Selenium	Se	mg/L	0.1	0.004
Silver	Ag	mg/L	0.0001	0.0003
Strontium	Sr	mg/L	-	0.623
Thallium	Tl	mg/L	0.0003	< 0.00005
Tin	Sn	mg/L	-	< 0.05
Titanium	Ti	mg/L	-	0.008
Uranium	U	mg/L	0.005	0.0006
Vanadium	V	mg/L	0.006	0.0005
Zinc	Zn	mg/L	0.03	< 0.005
Total Dissolved Solids	TDS	mg/L	-	1678
Total Hardness (as CaCO3)		mg/L	-	727
% Difference/Ion Balance		%	-	4.69
Biochemical Oxygen Demand	BOD	mg/L	-	< 3
Total Kjeldahl Nitrogen	TKN	mg/L	-	5.9
Chemical Oxygen Demand	COD	mg/L	-	31
Phenols		mg/L	0.001	< 0.001
Total Suspended Solids	TSS	mg/L	-	
Conductivity (field)		µS/cm	-	
Temperature (field)		°C	-	
pH (field)			-	
Redox		mV	-	
Dissolved Oxygen		mg/L	-	

Bold and highlighted indicates PWQO exceedance
INS - Insufficient sample quantity to analyze for parameter



APPENDIX G

Dewatering Calculations

Pumping Rates Calculations

Project:	Kirwin Ave	Construction Phase
Project Number:	22-056	

Open Cut Calculations (Rectangular Excavation)

$$Q = -\frac{\pi K(H^2 - h^2)}{\ln(\frac{R_o}{R_e})} + 2\left(\frac{LK(H^2 - h^2)}{2L}\right)$$

Based on Equation 6.12 in systems where $(\omega \geq 1.5)$ (Powers, P.E., 1992) Where:

Q (m³/day)

K - Hydraulic Conductivity (m/Day)

H - Distance from Static water level to bottom of Aquifer (m)

h - lowest water level needed from static (m)

R_e - Radius of conical depression (m) (Taken from Equation 6.14 (Powers, P.E., 1992))

$$Ro = 3(H - h)\sqrt{k}$$

Where

K - Hydraulic Conductivity (m/Sec)

R_e - Equivalent Radius (m)

$$R_o = \frac{l + w}{\pi}$$

l - Length of excavation/trench

w - width of trench

In systems where $(\omega \geq 1.5)$

$\ell / \omega > 1.5$

K m/sec	2.28E-07	Fill in
K m/d calc	1.97E-02	Leave alone
		calculated number

Parameter	Units		Q_t
K	m/d	0.01968192	21.06 m ³ /d
H	m	7.10	2.44E-04 m ³ /Sec
h	m	3.65	
R	m	46.3	
ω		47	
ℓ		83	
R_o	m	41	21,065
$\ln(R_o/R_e)$		0.113	
Limit	400 m ³ /d		
EASR	50 m ³ /d		
		Expected Pumping Rate with contingency	63,194
		EASR Required	21,065

300.0% Contingency for the variability in hydraulic conductivity that could be experienced and to provide flexibility to address additional drainage needed as a result of precipitation events.

50.00% Porosity Table from Freeze and Cherry 1979

Table 2.4 Range of Values of Porosity

	$n(\%)$
Unconsolidated deposits	
Gravel	25-40
Sand	25-50
Silt	35-50
Clay	40-70
Rocks	
Fractured basalt	5-50
Karst Limestone	5-50
Sandstone	5-30
Limestone, dolomite	0-20
Shale	0-10
Fractured crystalline rock	0-10
Dense crystalline rock	0-5

W	L	L/W
47	83	1.76597

Note: Width and length of the excavation is assuming PL to PL

K Max used	2.28E-07 m/sec
Ground Surface from:	Finished Floor (Drawing) 113.65 mRD

High Water Table	BH/MW1
Bottom of excavation (mbigs)	Set to 2 mb finished P2 Slab
Bottom of lowest screen	Based on the lowest elevation of known screens
Dewatering Target (Construction)	105.45 3.65
Dewatering Target (Operations)	102.00 7.10
Aquifer depth	Based on assumed bedrock elevation in the area

Storage Volume			
Thickness (m)	m ³	L	30 day (m ³)
Clayey Silt	3.6	7119	7.12E+06
	0	0	0
Total	3.6	7119	7119325
			79
			40

Precipitation Event into excavation			
Storm Event	(mm)	Depth (m)	Area m2
2-yr 24-hr.	56.2	0.0562	3901
5-yr 24-hr.	74.2	0.0742	3901
25-yr 24-hr.	101.2	0.1012	3901
100-yr 24-hr.	123.6	0.1236	3901
Climate Normals (/Yr)	709	0.709	3901
Climate Normals (/Day Average 6 months)			
			17

Pumping Rates			
Time	m ³ /day	m ³ /hour	L/Min
Storage (30 day pre excavation)	142.3	6	99
Storage (60 day pre excavation)	103.7	4	71
Construction	63.19	2.6	44

EASR Required

EASR Required

EASR Required

Pumping Rates Calculations

Project:	Kirwin Ave. Development	Post Construction
Project Number:	22-056	

Open Cut Calculations (Rectangular Excavation)

$\ell / w > 1.5$

$$Q = \frac{\pi K (H^2 - h^2)}{\ln(R_o/R_s)} + 2 \left(\frac{LK(H^2 - h^2)}{2L} \right)$$

Based on Equation 6.12 in systems where $l/w > 1.5$ (Powers, P.E., 1992) Where:

Q (m³/Day)

K - Hydraulic Conductivity (m/Day)

H - Distance from Static water level to bottom of Aquifer (m)

h - lowest water level needed from static (m)

R_o - Radius of conical depression (m) (Taken from Equation 6.14 (Powers, P.E., 1992))

$$R_o = 3(H - h)\sqrt{k}$$

Where

K- Hydraulic Conductivity (m/Sec)

R_s - Equivalent Radius (m)

$$R_s = \frac{l + w}{\pi}$$

l- Length of excavation/trench

w- width of trench

in systems where $l/w > 1.5$

w - excavation width
ℓ - excavation length

Development footprint requiring dewatering

W	L	L/W
47	83	1.765957

Note: Width and length of the excavation is assuming PL to PL

K Max used	2.28E-07	m/sec
Ground Surface from:	Finished Floor (Drawing)	mASL
		113.65

High Water Table	
Bottom of excavation (mbgs)	6.7
Bottom of lowest screen	
Dewatering Target (Construction)	
Dewatering Target (Operations)	
Aquifer depth	

mASL	Water Column	BH/MW1
109.10		Set to 2 mb finished P2 Slab
107.45		Based on the lowest elevation of known screens
104.90		
107.45		1.65
107.45		1.65
102.00		7.10
		Based on assumed bedrock elevation in the area

Legend:

	Fill in
	Leave alone
	calculated number

K m/sec	2.28E-07
K m/d calc	1.97E-02

Parameter	Units		Q _o
K	m/d	0.01968192	18.01 m ³ /d
H	m	7.10	2.08E-04 m ³ /Sec
h	m	1.65	
R	m	49.2	
	w	47	
	ℓ	83	
R _s	m	41	
ln(R _o /R _s)		0.173	
			18.006
Limit	400 m ³ /d		
EASR	50 m ³ /d		
			54.02 m ³ /d
			Expected Pumping Rate with contingency
			EASR Required

300.0%

Contingency for the variability in hydraulic conductivity that could be experienced and to provide flexibility to address additional drainage needed as a result of precipitation events.

