

**FUNCTIONAL SERVICING &
STORMWATER MANAGEMENT REPORT**

**50 HIGH STREET EAST
RESIDENTIAL DEVELOPMENT**

**CITY OF MISSISSAUGA
REGION OF PEEL**

**PREPARED FOR:
MOHAGANY MANAGEMENT**

**PREPARED BY:
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TORONTO, ON M5B 1M4**

DECEMBER 2025

CFCA FILE NO. 2880-7436

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Revision Number	Date	Comments
Rev.0	August 1, 2025	Issued for First Submission (ZBA)
Rev.1	December 12, 2025	Issued for Second Submission (ZBA)

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1.0 Introduction

1.1 Purpose

C.F. Crozier & Associates Inc. was retained by Mahogany Management (the Client) to prepare a Functional Servicing and Stormwater Management Report in support of the Zoning By-Law Amendment (ZBA) for the property located at 50 High Street East in the City of Mississauga. This report demonstrates the proposed site can be developed in accordance with City of Mississauga and Region of Peel design guidelines from a functional servicing and stormwater management perspective.

2.0 Site Description

2.1 Existing Conditions

The existing property covers an area of 1022.21 m² (0.10 ha) and is bound by residential apartment buildings to the north, east and west, and High Street East to the south. The site lies within a residential land use area. The existing site contains a 3-storey residential building with at-grade parking located at the rear of the building. The unit count of the existing 3-storey residential building has been confirmed by the Client via email correspondence, which is included in **Appendix A** for reference. The existing unit count was used to calculate the existing population of the subject site.

Table 1 below summarizes the existing population of the subject site.

Table 1: Existing Population Density

Unit Type	Number of Units	Equivalent Population Density	Population
1 Bedroom	11	1.7 (person/hectare)	19
Total Existing Residential Population			19

KRCMAR Surveyor Ltd. was retained by the Client to prepare a topographic survey of the subject site. A copy of the topographic survey is included in **Appendix A** for reference.

Additionally, records drawings obtained from the City of Mississauga and the Region of Peel have been included in **Appendix A** for reference.

2.2 Proposed Development Concept

The proposed residential development includes the construction of an 11-storey residential building. The building is proposed to have an at-grade accessible parking stall within the covered at-grade vehicular access area. The development is proposed to have a total of 96 residential units and vehicular access to the site is provided via High Street East.

The proposed population for the subject site was calculated using the equivalent population density from the Region of Peel Linear Wastewater Standards dated March 29th, 2023, and residential unit information was obtained from the latest site plan and statistics provided by Chamberlain Architect

Services Limited, which is included in **Appendix A** for reference. **Table 2** below summarizes the proposed population for the subject property.

Table 2: Proposed Population Density

Unit Type	Number of Units	Equivalent Population Density	Population
1 Bedroom	60	2.7 (person/unit)	162
2 Bedroom	35		95
3 Bedroom	1		3
Total Proposed Residential Population			259

The proposed population equivalent was calculated to be greater than 475 person/hectare. Therefore, the population equivalent used for the design is based on a density of 2.7 person per unit using the equation below:

$$(2.7 \text{ ppu} \times \text{No. Units}) \div \text{Area} = \text{person/hectare}$$

$$(2.7 \times 96) \div 0.1 = 2592 \text{ person/hectare}$$

As a result, the total proposed population of the subject site is calculated to be 259 persons.

2.3 Reference Information

The following documents were referred to in preparation of this report, and offer background information regarding the existing infrastructure surrounding the proposed development:

- Region of Peel – Linear Wasterwater Standards, dated March 29th, 2023
- Region of Peel – Public Works Design, Specifications & Procedures Manual, Watermain Design Criteria, dated Revised June 2010
- Region of Peel – Public Works Stormwater Design Criteria and Procedural Manual, dated June 2019 (Version 2.1)
- City of Mississauga – Transportation & Works Department, Development Requirements Manual, Section 8 – Storm Drainage Design Requirements, dated November 2020
- Fire Underwriters' Survey – Water Supply for Public Fire Protection, dated 2020

3.0 Water Servicing

The following section of the report analyses the existing and proposed water servicing demands for the subject site. The Region of Peel – Linear Wastewater Standards (March 29, 2023) and Region of Peel – Public Works Design, Specifications & Procedures Manual, Watermain Design Criteria, dated (Revised June 2010) was referenced to calculate the domestic and fire flow demands for the subject site.

3.1 Existing Water Servicing

According to the as-built records provided by the City of Mississauga and the Region of Peel, the following water services exist in proximity to the subject site:

- 200 mm diameter watermain along High Street East

Based on the Region of Peel record drawing (No. 25842-D), it is determined that the existing residential building has a water service connection to the existing 200 mm diameter watermain along High Street East. The location of the existing water services is shown on the **Servicing Plan – C102**.

As per the Region of Peel Water Pressure Zones Map, the site is located within Pressure Zone 1 (PZ 1). The Water Pressure Zones Map is included in **Appendix B** for reference.

Based on pre-development conditions, a summary of the results is presented in **Table 3**, with detailed calculations provided in **Appendix B**.

Table 3: Existing Domestic Water Demand

Type of Use	Average Daily Demand (L/s)	Maximum Day Demand (L/s)	Peak Hourly Demand (L/s)
Residential	0.06	0.12	0.18

3.2 Proposed Water Servicing

The proposed water servicing strategy for the development consists of one (1) connection to the existing 200 mm diameter watermain along High Street East and will consist of a 100 mm diameter PVC domestic and 150 mm diameter PVC fire line. Each unit will be serviced internally to the building through mechanical design, which will be completed at the time of detailed design by a mechanical engineer.

Considering the height of the building is less than 84 meters, the building will not require to be serviced by two (2) separate watermains adhering to the Ontario Building Code (OBC) Section 3.2.9.7.

The proposed water services will be equipped with a property line valve and box per Region of Peel standards. The proposed water meter, backflow preventer, and internal building water servicing will be installed per the mechanical details and specifications. The site is proposed to be serviced by a private hydrant near the building entrance facing High Street East, which is located 5.72 meters from the proposed siamese connection. Refer to the **Servicing Plan – C102** for further details.

The domestic water demand for the subject site was calculated with reference to the Region of Peel – Linear Wastewater Standards (March 29, 2023) and Region of Peel – Public Works Design, Specifications & Procedures Manual, Watermain Design Criteria, dated (Revised June 2010). An average residential daily water demand of 280 L/capita/day was used in conjunction with the occupancy densities described in **Table 2**.

A summary of the results is presented in **Table 4**, with detailed calculations provided in **Appendix B**.

Table 4: Proposed Domestic Water Demand

Type of Use	Average Daily Demand (L/s)	Maximum Day Demand (L/s)	Peak Hourly Demand (L/s)
Residential	0.84	1.68	2.52

3.3 Fire Flow Demand

The fire flow requirements for the proposed development were calculated based on the methodology identified in the current version of the *Water Supply for Public Fire Protection: A Guide to Recommended Practice in Canada (2020)* prepared by the Fire Underwriters' Survey (FUS).

Fire Flow requirements were calculated based on the following parameters:

- (Type 1) Fire Resistive Construction materials with a construction coefficient of 0.6, where all structural elements, walls, columns, arches, floors, and roofs are constructed with a minimum 2-hour fire resistance rating, and all materials used in the construction of the structural elements, walls, columns, arches, floors and roofs are constructed with non-combustible materials.
- For a building classified with a construction coefficient below 1.0, with vertical opening properly protected in accordance with the National Building Code, the Total Effective Area was calculated to be 909.95 m², applying 100% of the single largest floor plus 25% of each of the two immediately adjoining floors, based on floors 6, 7 and 8 from the latest site statistics prepared by Chamberlain Architect Services Limited.
- An Occupancy and Contents Adjustment Factor of -15% for Limited Combustible contents, falling under a Group C Residential occupancy (Table 3 of the FUS)
- An automatic fully supervised sprinkler protection system designed and installed in accordance with NFPA 13 (50% reduction factor).
- Exposure charges were included in the calculations to account for various existing residential properties in proximity to the subject site.

As a result, the fire flow demand is calculated to be 50 L/s (3,000 L/min). In accordance with the FUS guidelines, the fire flow for residential areas shall not be less than 80 L/s (4,800 L/min). Therefore, the fire flow demand of the proposed development is increased to 80 L/s (4,800 L/min) in adherence to the FUS guidelines. Detailed calculations are included in **Appendix B**. Additionally, an email from the architect confirming the construction type, occupancy category and the sprinkler system is included in **Appendix B** for reference.

3.4 Hydrant Flow Test

One (1) hydrant flow test was performed by Watermark Solutions on June 11th, 2025, on the existing 200 mm diameter watermain along High Street East. The results indicate that at 20 psi residual pressure, a maximum of 567 L/s (8,983 USGPM) projected flow is available within the existing 200 mm diameter watermain along High Street East.

Based on the estimated maximum day plus fire flow demand of 81.68 L/s and the hydrant test report, the existing municipal water supply can support the proposed development without the need of external upgrades or retrofit. A detailed report of the hydrant flow test is provided in **Appendix B** for reference.

4.0 Sanitary Servicing

The following section of the report analyses the existing and proposed sanitary servicing conditions for the subject site. The Region of Peel – Linear Wastewater Standards (March 29, 2023) was referenced to calculate the existing and proposed sanitary demands for the subject site.

4.1 Existing Sanitary Servicing

According to the as-built records provided by the City of Mississauga and the Region of Peel, the following water services exist in proximity to the subject site:

- 375 mm diameter sewer along High Street East

Based on the Region of Peel record drawing (No. 25842-D), it is determined that the existing residential building has a sanitary service connection to the existing 375 mm diameter sewer along High Street East. The location of the existing sanitary service is shown on the **Servicing Plan – C102**.

The existing sanitary flows were calculated based on the Region of Peel - Linear Wastewater Standards (March 29, 2023) in conjunction with the existing occupancy densities described in **Table 1**. A summary of the results is shown in **Table 5**, with detailed calculations provided in **Appendix C**.

Table 5: Existing Sanitary Design Flows

Type of Use	Average Flow (L/s)	Peaking Factor (M)	Peak Flow (L/s)	Infiltration Flow (L/s)	Total Flow (L/s)
Residential	0.06	4.00	0.25	0.03	0.28

4.2 Proposed Sanitary Servicing

The subject site is proposed to be serviced by one (1) 150 mm diameter sanitary service connection to the existing 375 mm diameter sanitary sewer along High Street East. The proposed 150 mm diameter sanitary sewer connection includes a control manhole located at the property line fronting High Street East.

Refer to the **Servicing Plan – C102** for further details.

4.3 Sanitary Design Flows

The sanitary design flow for the subject site was calculated with reference to the Region of Peel – Linear Wastewater Standards (March 29, 2023). An average residential wastewater flow of 290 L/capita/day was used in conjunction with the occupancy densities described in **Table 2**. Peaking

factors were applied to the residential sewage flows to obtain the total estimated design sewage flow.

Table 6 below summarizes the results and **Appendix C** contains detailed calculations of the sanitary flow for the proposed development.

Table 6: Proposed Sanitary Design Flows

Type of Use	Average Flow (L/s)	Peaking Factor (M)	Peak Flow (L/s)	Infiltration Flow (L/s)	Total Peak Flow (L/s)
Residential	0.87	4.00	3.48	0.03	3.51

5.0 Groundwater Drainage Conditions

A Geotechnical Investigation for the subject site was completed by Toronto Inspection Ltd. dated July 28th, 2025, which detailed the site's subsurface and groundwater conditions. The major conclusions of the geotechnical report are summarized in the bullets below:

- The field work for the investigation consisted of drilling four (4) sampled boreholes (25BH-1 to 25BH-4), extending to depths of 3.8m to 5.2m from grade.
- Groundwater observations were made in the open boreholes during and upon the completion of drilling. Boreholes 25BH-1 and 25BH-3 were completed as monitoring wells for the determination of groundwater conditions.

Further investigation is to be completed to determine the short-term and long-term groundwater dewatering rates as well as the quality of the groundwater for discharge purposes. Refer to the Geotechnical Investigation prepared by Toronto Inspection Ltd. under a separate cover for more details.

Note that a site visit was completed by Toronto Inspection Ltd. on November 25th, 2025, to confirm the groundwater level measurements. The results indicate that at boreholes 25BH-1 and 25BH-3, the groundwater levels were recorded at 75.52 masl and 73.43 masl, respectively. It was noted that an additional 1 meter should be added to the recorded groundwater levels to estimate the seasonal high groundwater level at these borehole locations. Email correspondence with Toronto Inspection Ltd. is included in **Appendix D** for reference.

6.0 Drainage Conditions

6.1 Existing Drainage Conditions

According to the as-built records provided by the City of Mississauga and the Region of Peel, the following is existing stormwater infrastructure surrounding the subject site:

- 825 mm diameter sewer along High Street East

Based on the topographical survey, the subject site generally slopes from northwest to southeast draining overland runoff to the High Street East right-of-way, which is then captured by curbside catch basins. The catch basins are connected to the existing 825 mm diameter storm sewer along High Street East. Refer to **Appendix E** for the calculated pre-development catchment area and associated weighted runoff coefficient.

6.2 Proposed Drainage Conditions

Storm flows from the building will be directed to roof drains and an on-site catch basin, which will capture a majority of the overland flows. This flow will then ultimately discharge to an oil and grit separator prior to discharging into the proposed stormwater management tank located downstream.

It is proposed to connect to the existing 825 mm diameter storm sewer along High Street East. The proposed connection includes a control manhole located at the property line within the vehicular access drive aisle.

Due to the existing low point located at the southern corner of the site, it is proposed to have uncontrolled flows draining to the High Street East right-of-way. The uncontrolled release rate to High Street East is calculated to be 3.47 L/s with a weighted runoff coefficient of 0.84 (including a 100-year adjustment factor). More details about the total release rate to the existing 825 mm diameter sewer along High Street East are included in **Section 7.1**.

Refer to **Appendix E** for the calculated post-development catchment areas and associated weighted runoff coefficients.

7.0 Stormwater Management

7.1 Stormwater Quantity Control

Method of Analysis

The Modified Rational Method was used to calculate the runoff rates from all drainage catchments and to quantify the detention storage required for quantity control measures in keeping within the requirements of the City of Mississauga guidelines.

Allowable Release Rate

Using the City of Mississauga's current IDF parameters and referring to Table 1 of Section 8 – Storm Drainage Design Requirements of the City of Mississauga dated November 2020, the allowable release rate from the site to High Street East has been established as 21.96 L/s, with a weighted runoff coefficient of 0.78 (including 10-year adjustment factor). This rate is equal to the runoff generated from a 10-year storm event for the entire existing site area at a time of concentration 15 minutes. Refer to **Appendix E** for detailed stormwater management calculations.

Orifice & Post-Development Release Rates

Stormwater attenuation for the post-development site area, with a calculated runoff coefficient of 0.77 (including 100-year adjustment factor), will be by a 75 mm orifice tube at the downstream invert of the proposed stormwater management tank. The orifice tube has been designed to control flows from a 100-year storm event to a release rate of 15.12 L/s (including a 100-year adjustment factor). Therefore, the total release under a 100-year storm event is determined to be 18.83 L/s, which is less than the 10-year allowable release rate. As a result, this conforms with the City of Mississauga stormwater guidelines.

Proposed Stormwater Management Tank

A stormwater management tank is proposed within the subject site. **Table 7** summarizes the design parameters of the stormwater management tank, detailed calculations can be found in **Appendix E** and on the **Servicing Plan – C102**.

Table 7: Stormwater Management Tank Design Parameters

Tank Elevations	Bottom = 75.36 m Outlet = 75.36 m 100-Year High-Water Level (HWL) = 76.33 m Top = 76.43 m Minimum Freeboard = 0.10 m
Orifice Tube Details (CTRL MH)	Diameter = 75 mm Invert = 75.36 m
Tank Area	21.0 m ²
Tank Active Storage Volumes	Required: 20.3 m ³ Provided: 20.4 m ³ (to HWL)

7.2 Stormwater Quality Control

An enhanced level of stormwater quality treatment of 80% Total Suspended Solids (TSS) removal is to be provided based on 100% of the runoff leaving the subject site for all storm events that occur in an average year. An oil and grit separator unit is proposed upstream of the proposed stormwater management tank, which will be designed to provide greater or equal to 80% TSS removal. Specifications of the oil and grit separator unit will be provided during the detailed design stage.

7.3 Water Balance

Based on the City of Mississauga guidelines, runoff from the 5 mm rainfall event is to be retained on-site through infiltration, evapotranspiration, and/or water reuse measures. Water balance will be achieved through an infiltration gallery along the private driveway, upstream of the proposed stormwater management tank. Based on a required average annual precipitation depth of 5 mm to be retained on-site, the required retention volume is calculated to be 5.1 m³. Infiltration gallery calculations can be referenced in **Appendix E**.

As per the Geotechnical Investigation prepared by Toronto Inspection Ltd. dated July 28th, 2025, the boreholes revealed that the subsoil, below the topsoil and asphalt pavement, consisted of a layer of

fill, overlaying a native sandy silt till deposit. Probable shale was encountered at the termination depths of the boreholes. However, the depth of the shale will not impede on the infiltration gallery design as it is found to be at a depth of roughly 3.5 m. The native sandy silt till is desirable to promote infiltration.

As described in **Section 5.0**, Toronto Inspection Ltd. recently confirmed the high groundwater level at 25BH-1 and 25BH-3, which they then applied a meter to estimate the seasonal high groundwater level for each borehole location. The infiltration gallery has been designed to be a minimum of 1.0m above the estimated seasonally high groundwater level of 74.43 m to avoid water table encroachment.

The infiltration rate was provided by Toronto Inspection Ltd. via email correspondence and is determined to be 13 mm/hr based on the grain size distribution table appended to the Geotechnical Investigation – refer to **Appendix E** for the email from Toronto Inspection Ltd. A drawdown time of 70 hours was then calculated using the infiltration rate, which the proposed infiltration area can infiltrate a volume of 5.24 m³. Therefore, the infiltration gallery design does achieve full water balance for the development.

8.0 Conclusions & Recommendations

We recommend the approval of the Zoning By-Law Amendment application for the proposed development from a functional site servicing and stormwater management perspective.

Based on the information contained within this summary report, we offer the following conclusions:

1. Water servicing will be provided via one (1) connection to the existing 200 mm watermain along High Street East. It is determined that the existing watermain has sufficient capacity to service the proposed development's maximum day plus fire flow demand of 81.68 L/s. A private hydrant is proposed near the building entrance facing High Street East.
2. Sanitary servicing will be provided via one (1) connection to the existing 375 mm diameter sanitary sewer along High Street East. Based on post-development conditions, it was determined that sanitary demands would reach a total peak flow rate of 3.51 L/s.
3. Stormwater quantity control for the subject site will be provided via a stormwater management tank. Flows will be controlled by a 75 mm orifice tube downstream of the stormwater management tank.
4. Stormwater quality control for the subject site will be provided through an oil and grit separator unit, which will be sized to remove 80% of the TSS. The oil and grit separator is proposed to be located upstream of the stormwater management tank to promote clean water entering the stormwater management tank.
5. Water balance for the site will be achieved through an infiltration gallery along the private driveway upstream of the proposed stormwater management tank.

Based on the conclusions and recommendations, we suggest the approval of the applications from the perspective of functional servicing and stormwater management.

Respectfully submitted,

C.F. CROZIER & ASSOCIATES INC.

JP Labonte

J.P. Labonte, P.Eng.
Project Engineer

C.F. CROZIER & ASSOCIATES INC.



Julie Scott, P.Eng.
Manager, Land Development

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APPENDIX A

Background Information

JP Labonte

From: Tim Neeb <tim@mahoganymanagement.com>
Sent: May 26, 2025 1:25 PM
To: JP Labonte
Cc: Julie Scott
Subject: Re: CFC 2880-7436: 50 High Street East, Mississauga - Existing Building Unit Count Statistic Request

Follow Up Flag: Follow up
Flag Status: Flagged

current building has 11 one bedroom units.

planned building has 60 one bedroom, 35 two bedroom and 1 three bedroom total 96 units

On Mon, May 26, 2025 at 12:21 PM JP Labonte <jplabonte@cfcrozier.ca> wrote:

Thank you for providing the total unit count Tim.

We would also need the type of unit associated to that number (ie 1 bed, 2 bed, etc.)

Best,

JP Labonte

Engineering Intern, Land Development
Office: 905.876.7158
Collingwood | Milton | Toronto | Bradford | Guelph

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our vision for growth. [Learn how, here.](#)



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From: Tim Neeb <tim@mahoganymanagement.com>
Sent: May 26, 2025 12:02 PM
To: JP Labonte <jplabonte@cfcrozier.ca>; Christina Borowiec <christina@sajeckiplanning.com>; Tony De Franco <tony@sajeckiplanning.com>; Julie Scott <jscott@cfcrozier.ca>; Adrian Mauro <amauro@chamberlainipd.com>
Subject: Re: CFC 2880-7436: 50 High Street East, Mississauga - Existing Building Unit Count Statistic Request

existing building count is 11 units. new building should be 95 units.

Tim

On Mon, May 26, 2025 at 10:03 AM JP Labonte <jplabonte@cfcrozier.ca> wrote:

Hi Tim,

Hope you had a nice weekend.

I am requesting the existing building unit count for our existing sanitary and water demand calculations for the functional servicing report. The report must touch on the existing demands and how they compare to the proposed demands.

Let me know if you have any questions and/or concerns.

Thanks.

JP Labonte

Engineering Intern, Land Development

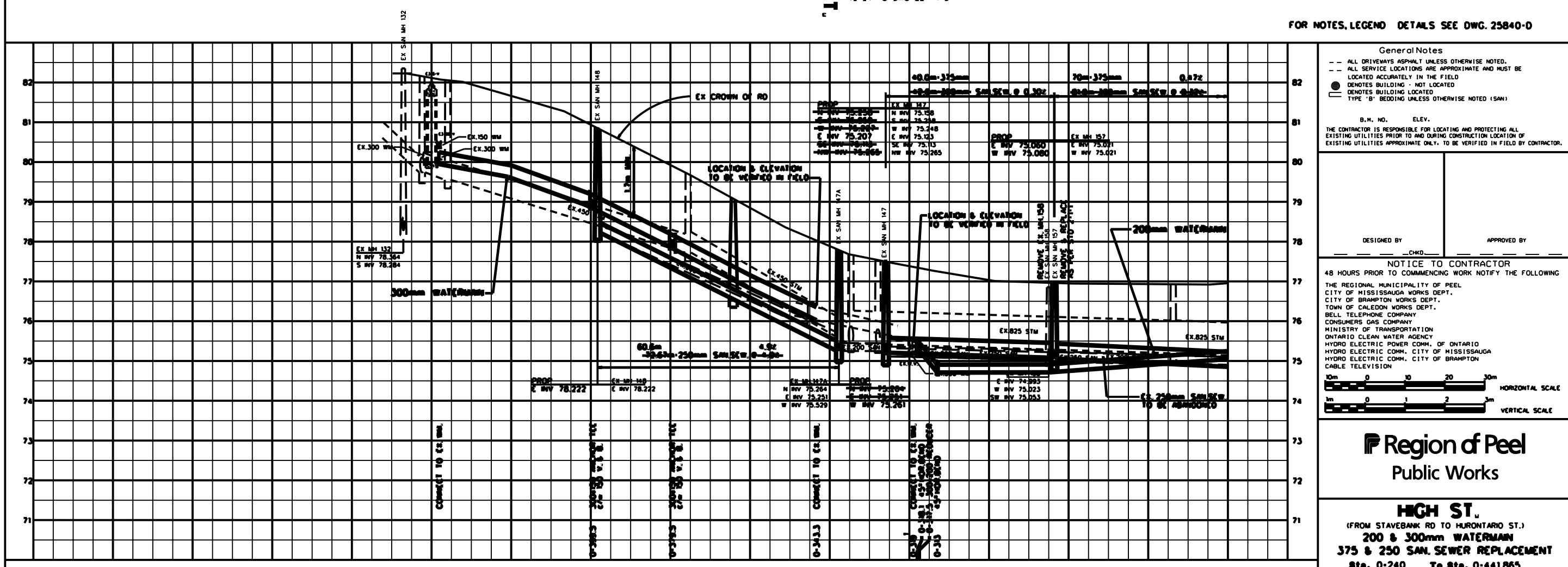
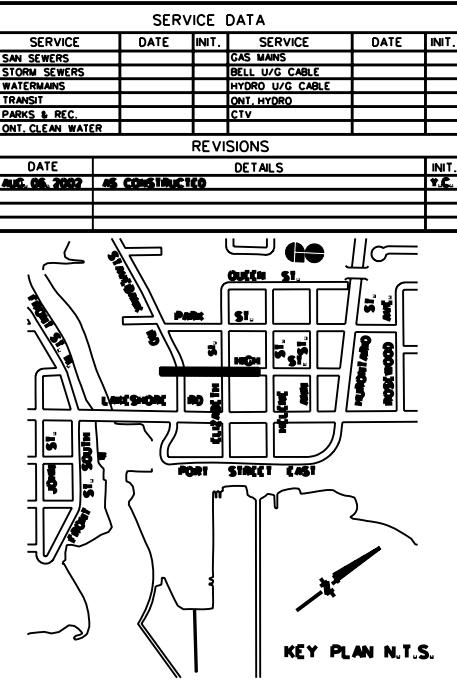
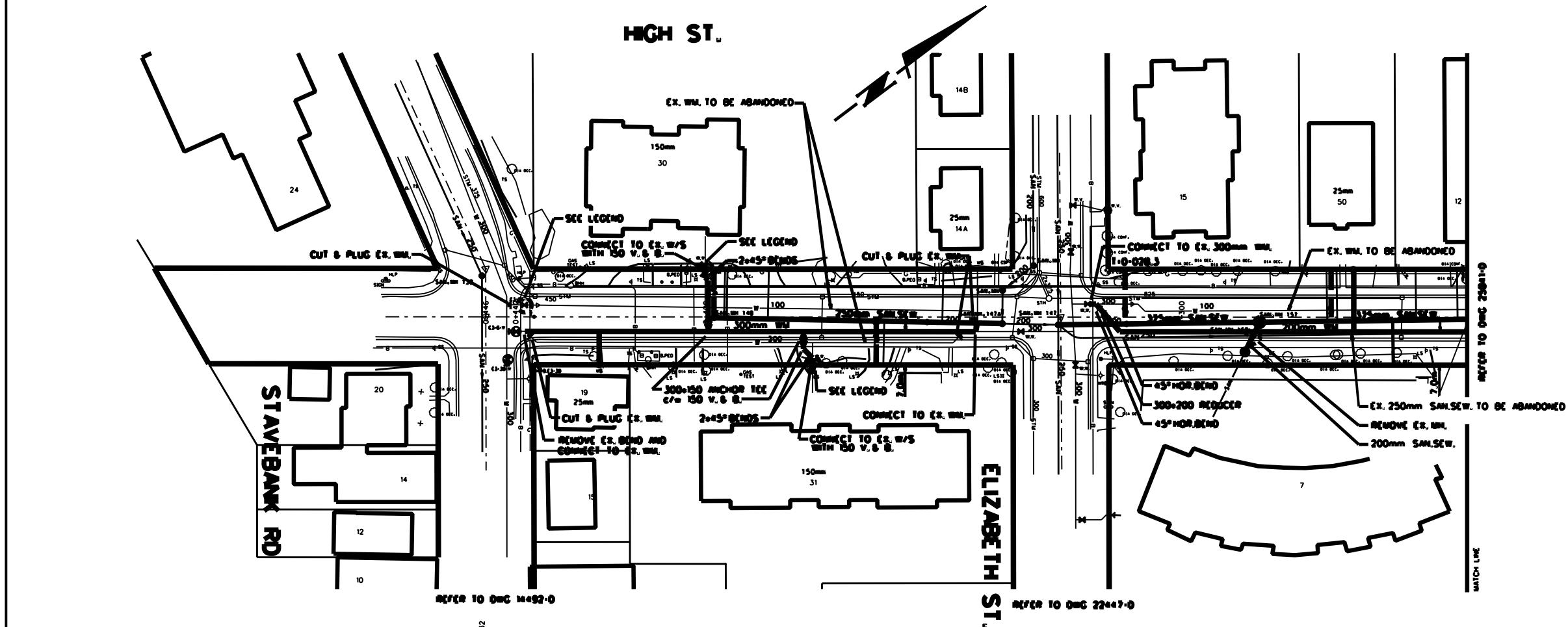
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our vision for growth. [Learn how, here.](#)**

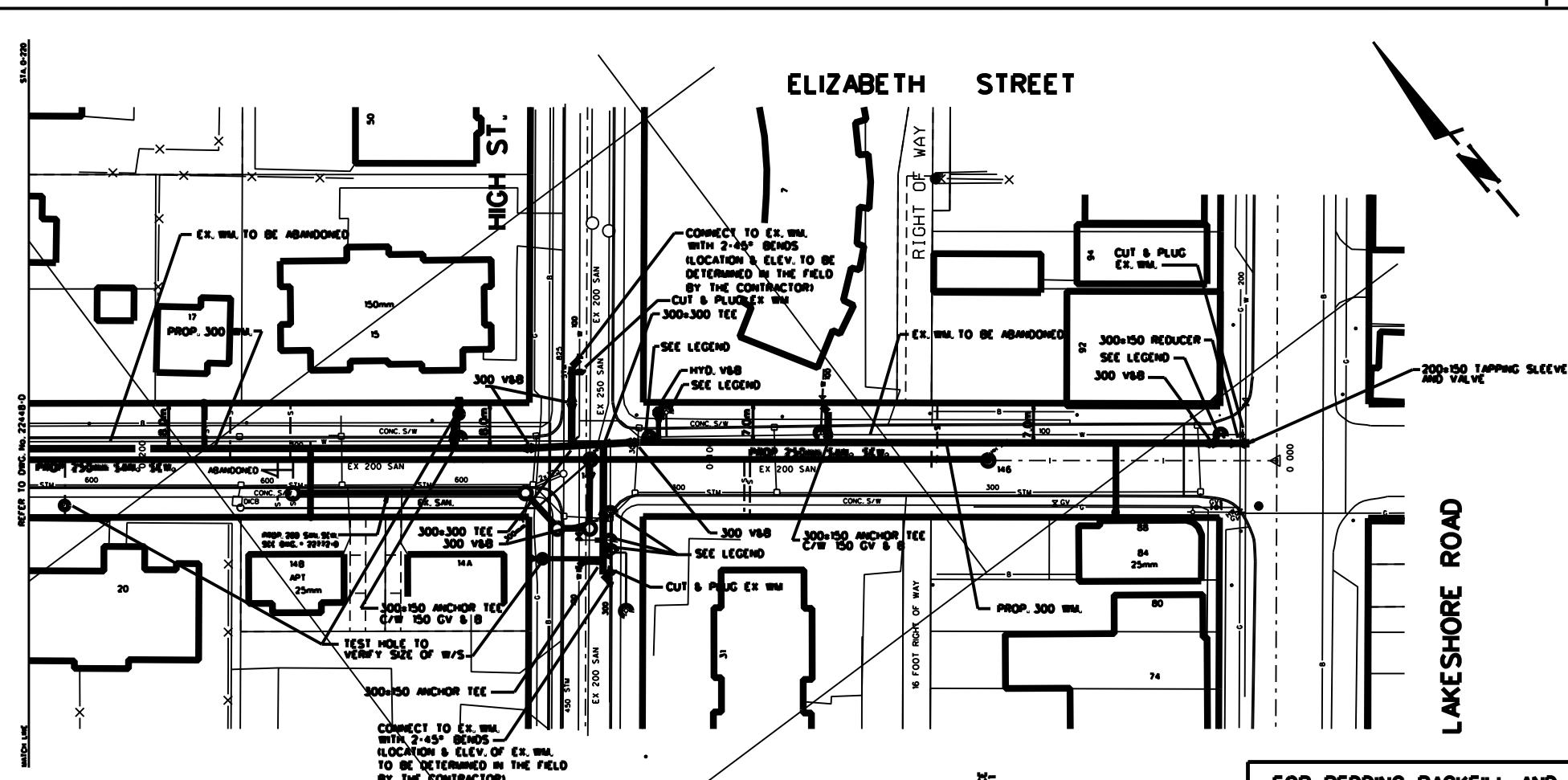


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LOTS	AREA	00-2210
		PROJECT NO. 00-1310
0-460	0-440	0-420
0-400	0-380	0-360
0-340	0-320	0-300
0-280	0-260	0-240
ROAD CHAINAGE		

DATE MARCH 03, 00 SHEET 2 OF 2 PLAN NO. 25842-D



SERVICE DATA			
SERVICE	DATE INIT.	SERVICE	DATE INIT.
SAN SEWERS	MAY 1996	EWK GAS LINES	JUNE 1996 A.S.
STORM SEWERS	EWK	CELL. LINE, GABLE	JUNE 1996 A.S.
WATERMANS	MAY 1996	EWK HYDRO U/G CABLE	
TRANSIT		CTV, HYDRO	A.S.
PARKS & REC.		CTV	A.S.
ONT. CLEAN WATER			

REVISIONS	DATE	DETAILS	INIT.
	JULY 98	AS CONSTRUCTED	EWK

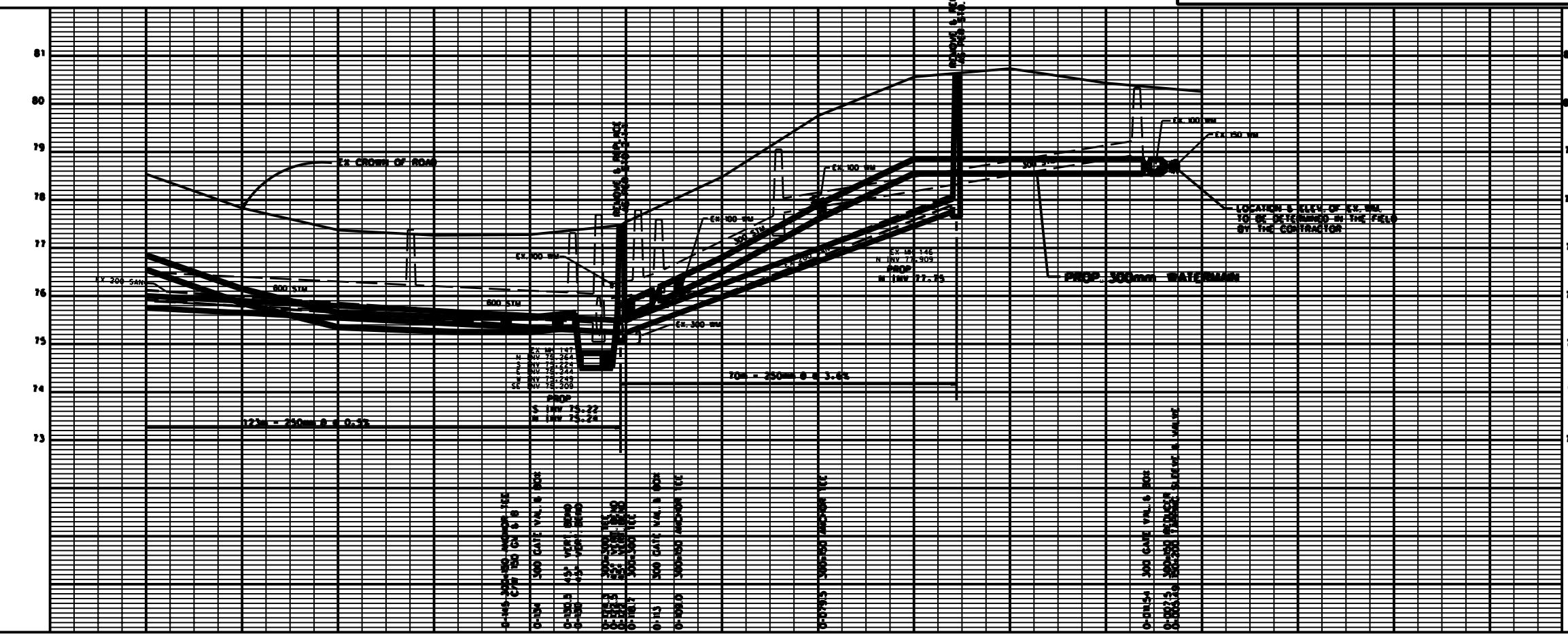
GENERAL NOTES:

- ALL COPPER (LESS THAN 20mm), GALVANIZED & LEAD WATER SERVICES ARE TO BE REPLACED WITH 20mm TYPE 'K' COPPER FROM THE NEW WM. TO THE STREET LINE COMPLETE WITH A NEW SERVICE BOX AT STREET LINE. ALL W/S MUST HAVE A MIN. OF 1.7m COVER IF W/S CONFLICTS WITH SEWERS AND/OR EX. WM. W/S HAS TO BE INSTALLED UNDER SEWER WITH A MIN. OF 300mm CLEARANCE. REMOVE & DISPOSE OF EXISTING WATER SERVICE BOXES.
- PLUG THE ENDS OF THE ABANDONED WM. WITH CONCRETE.
- 50mm TEMP. BLOW-OFF AND/OR RISER PIPE FOR SWABBING OF THE WM. IS TO BE LOCATED IN THE BLVD.
- NEW HYDRANT OFFSET AT 3.5m OR AS SHOWN ON PLANS.
- INSTALL TEMP. PLUG & B.O. AT END OF EACH PIPE FOR TEST.
- INSTALL W/S UNDER PAVEMENT, TREES AND/OR SHRUBS BY BORING.
- REMOVE AND DISPOSE OF EX. MANHOLES AND REINSTALL NEW 1200mm DIA. PRECAST SANITARY MANHOLE AS PER REGION STD. DWG. 2-1-1, 2-1-4 AND 2-2-2.
- ALL SANITARY SEWER LATERALS ARE TO BE REPLACED FROM MAIN TO STREET LINE UNLESS DIRECTED OTHERWISE BY THE PROJECT ENGINEER.
- THE EXACT LOCATION AND ELEVATION OF EX. WATERMAIN HAS TO BE DETERMINED IN THE FIELD BY THE CONTRACTOR.

LEGEND:

- EX. 25mm & LARGER COPPER W/S TO BE CUT AND TRANSFERRED OR EXTENDED TO THE NEW WM.
- REPLACE EX. W/S WITH 25mm COPPER
- EX. HYD. V. & B. TO BE REMOVED AND HYD. TO BE RETURNED TO REGION YARD AT 3515 WOLFDEALE RD. VALVES TO BE DISPOSED OF OFF SITE.
- REPLACE EX. SANITARY LATERALS.

FOR BEDDING, BACKFILL AND REINSTATEMENT DETAIL SEE DWG. NO. 22448-D



General Notes

- ALL DRIVEWAYS ASPHALT UNLESS OTHERWISE NOTED.
- ALL SERVICE LOCATIONS ARE APPROXIMATE AND MUST BE LOCATED ACCURATELY IN THE FIELD.
- DENOTES BUILDING - NOT LOCATED
- DENOTES BUILDING LOCATED
- TYPE 'B' BEDDING UNLESS OTHERWISE NOTED (SAN)

B.M. NO. ELEV.
THE CONTRACTOR IS RESPONSIBLE FOR LOCATING AND PROTECTING ALL EXISTING UTILITIES PRIOR TO AND DURING CONSTRUCTION LOCATION OF EXISTING UTILITIES APPROXIMATE ONLY. TO BE VERIFIED IN FIELD BY CONTRACTOR.

DESIGNED BY CHKD APPROVED BY

NOTICE TO CONTRACTOR
48 HOURS PRIOR TO COMMENCING WORK NOTIFY THE FOLLOWING

THE REGIONAL MUNICIPALITY OF PEEL
CITY OF MISSISSAUGA WORKS DEPT.
CITY OF BRAMPTON WORKS DEPT.
TOWN OF CALEDON WORKS DEPT.
BELL TELEPHONE COMPANY
CONSUMERS GAS COMPANY
MINISTRY OF TRANSPORTATION
ONTARIO CLEAN WATER AGENCY
HYDRO ELECTRIC POWER COMM. OF ONTARIO
HYDRO ELECTRIC COMM. CITY OF MISSISSAUGA
HYDRO ELECTRIC COMM. CITY OF BRAMPTON
CABLE TELEVISION

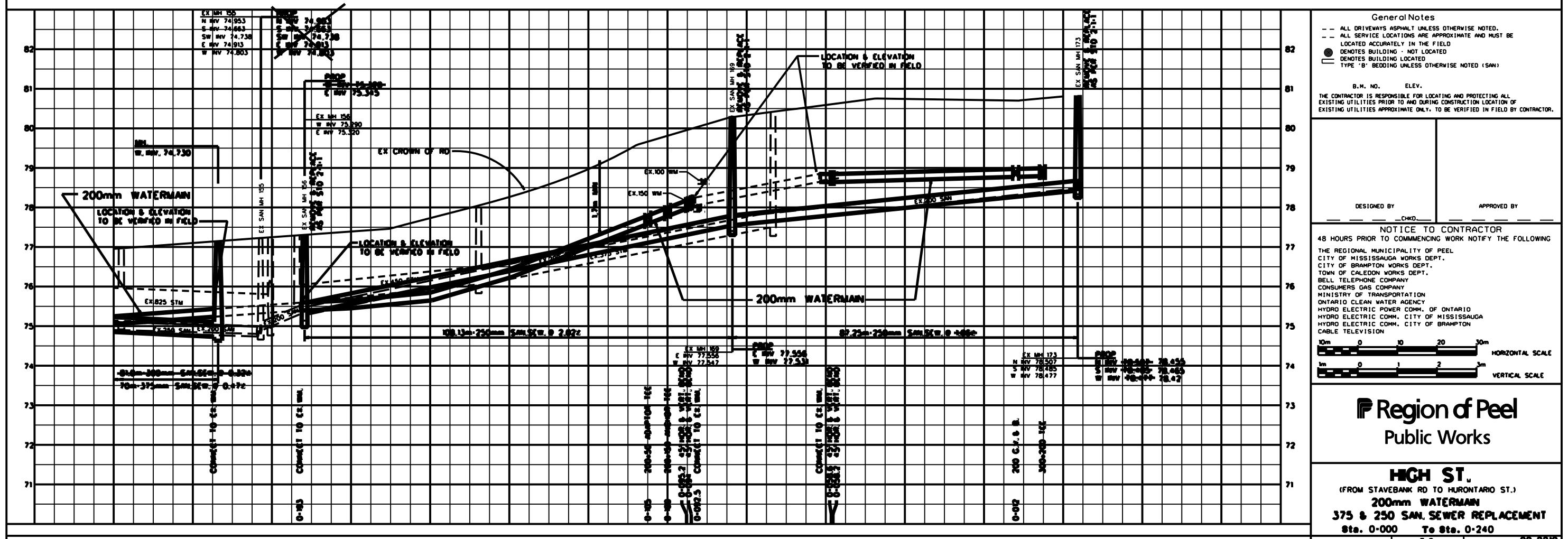
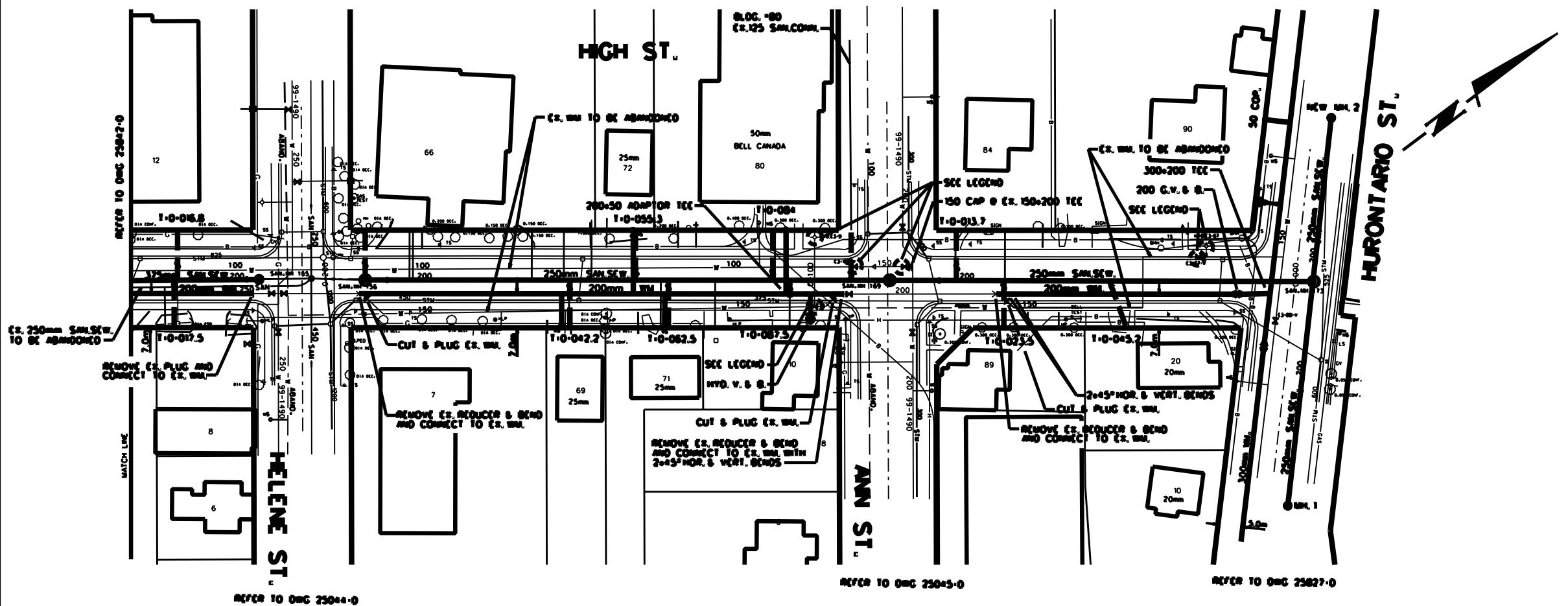
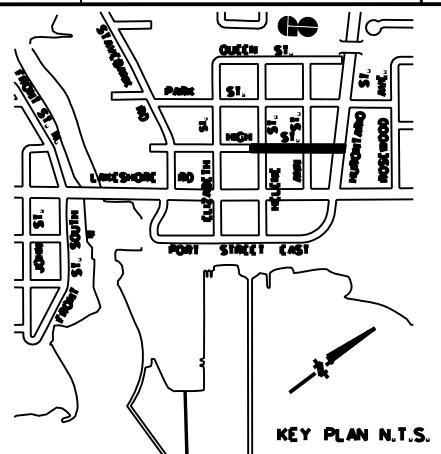
10m 0 10 20 30m HORIZONTAL SCALE
1m 0 1 2 3m VERTICAL SCALE

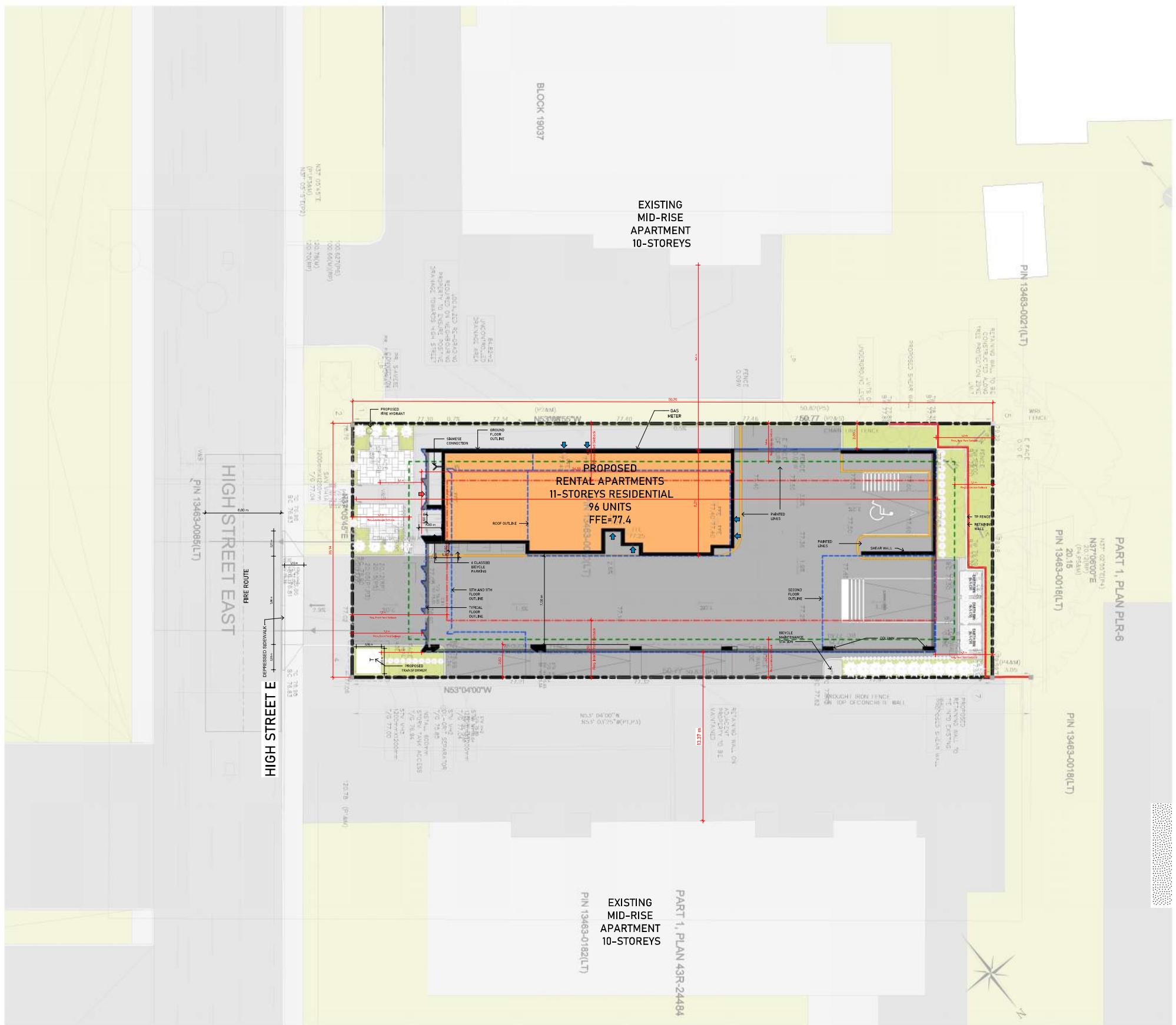
P Region of Peel
Public Works

ELIZABETH STREET
PROP. 300mm WATERMAIN REPLACEMENT
PROP. 250mm SANITARY REPLACEMENT
Sta. 0-000 To Sta. 0-220

LOTS AREA Z-8 PROJECT NO. 97-1440
DRAWN BY 48445 DRAWN BY 48445
CHECKED BY 48445 CHECKED BY 48445
DATE MAY 98 SHEET 1 OF 3 PLAN NO. 22447-D

SERVICE DATA	
SERVICE	DATE
SAN SEWERS	INIT.
STORM SEWERS	GAS MAINS
WATERMANS	BELL U/C CABLE
TRANSIT	HYDRO U/C CABLE
PARKS & REC	ONT. HYDRO
ONT. CLEAN WATER	CTV
REVISIONS	
DATE	DETAILS
AUG 06, 2002	AS CONSTRUCTED
	INIT.
	T.C.





CAR PARKING

ZONING INFO

DIMENSIONS:

STANDARD (90°)	2.60 x 5.20 m
PARALLEL	2.60 x 6.7 m
BARRIER-FREE TYPE (A)	3.40 x 5.20 m
BARRIER-FREE TYPE (B)	2.40 x 5.20 m
WIDTH OF DRIVEWAYS:	
ONE-WAY ASLE	5.50 m
TWO-WAY ASLE	7.00 m

REQUIRED PARKING SPACES:

Refer to the WSP transportation study for parking rationale.

PROPOSED PARKING SPACES:

PROVIDED PARKING SPACES		
TYPE	DESCRIPTION	COUNT
ACCESSIBLE PARKING	5.20m x 3.40m	1
ONE-WAY SPACE	9.00m x 3.50 m	
MASTER PARKING	6.2m x 5.8m	4
Grand total		6

LOADING SPACES:

One loading space per apartment building containing a minimum of 30 dwelling units.

Required loading spaces shall have an unobstructed rectangular area with a minimum width of 3.5 m and a minimum length of 9.0 m.

REQUIRED LOADING SPACES:

BUILDING CONTAINS 96 DWELLING UNITS

REQUIRED LOADING SPACES = 1

SITE STATISTICS

SITE STATISTICS OVERALL			
DESCRIPTION	AREA (m ²)	AREA (ft ²)	AREA (HA)
	PERCENTAGE (%)		
OVERALL SITE	10221 m ²	11003 ft ²	0.102 hectare
			100.0%

SITE STATISTICS

DESCRIPTION	AREA (SM)	AREA (SF)	PERCENTAGE
BUILDINGS			
PROPOSED BUILDING	185.14 m ²	1,971 ft ²	17.92%
	183.14 m ²	1,971 ft ²	17.92%
HARD LANDSCAPE			
ASPHALT	589.14 m ²	6,341 ft ²	57.64%
CURB	7.64 m ²	82 ft ²	0.75%
PAVER	24.30 m ²	262 ft ²	2.38%
SIDEWALK	91.63 m ²	986 ft ²	8.96%
	712.71 m ²	7,672 ft ²	69.73%
SOFT LANDSCAPE			
LANDSCAPE	126.32 m ²	1,360 ft ²	12.38%
	126.32 m ²	1,360 ft ²	12.30%
	1,022.16 m ²	11,002 ft ²	100%

GFA & FSI

GFA / FSI		
Level	Area (m ²)	Area (ft ²)
Ground	6095.88 m ²	65,000 ft ²
BASEMENT	0.00 m ²	0 ft ²
LVL 1	0.00 m ²	0 ft ²
LVL 2	498.31 m ²	5,301.4 ft ²
LVL 3	500.00 m ²	5,300.0 ft ²
LVL 4	600.63 m ²	6,529.7 ft ²
LVL 5	603.38 m ²	6,500.1 ft ²
LVL 6	600.83 m ²	6,529.7 ft ²
LVL 7	600.00 m ²	6,500.0 ft ²
LVL 8	600.63 m ²	6,529.7 ft ²
LVL 9	567.49 m ²	6,108.4 ft ²
LVL 10	430.00 m ²	4,645.5 ft ²
LVL 11	545.05 m ²	5,850.8 ft ²
T/O ROOF DECK	0.00 m ²	0 ft ²
Grand total	5657.88 m ²	60985.6 ft ²
		5.515362

BICYCLE PARKING

PROVIDED BICYCLE PARKING		
DESCRIPTION	COUNT	
BIKE PARKING - CLASS (A)	58	
BIKE PARKING - CLASS (B)	6	
Grand total	64	

REQUIRED LOADING SPACES:

BUILDING CONTAINS 96 UNITS

CLASS (A) = 0.6 * 96 UNITS= 58 SPACES

CLASS (B) = 0.05 * 96 UNITS = 5 SPACES

GROSS FLOOR AREA/APARTMENT ZONE)
 MEASUREMENT OF THE AREAS OF EACH STOREY OF A BUILDING ABOVE OR BELOW
 ESTABLISHED GRADE, MEASURED FROM THE EXTERIOR OF OUTSIDE
 WALLS OF THE BUILDING INCLUDING FLOOR AREA OCCUPIED BY
 REAR EXTERIOR WALLS, EXCEPT FOR AREAS OF THE BUILDING USED
 FOR MECHANICAL, FLOOR AREA, STAIRWELLS, ELEVATORS, MOTOR
 VEHICLE PARKING, BICYCLE PARKING, STORAGE LOCKERS, BELOW-
 GRADE STORAGE, ANY ENCLOSED AREA USED FOR THE COLLECTION
 AND DISCHARGE OF WASTE, AND AREAS OF THE BUILDING LOCATED
 WITHIN THE BUILDING, COMMON FACILITIES FOR THE USE OF THE
 RESIDENTS OF THE BUILDING, A DAY CARE AND AMENITY AREA.
 (0174-2017)

ZONING INFO

GDI: City of Mississauga

ADDRESS: 50 High Street E, Mississauga

LOT AREA: 1,022.21 m²

ZONE CODE: RA-1-6

ZONE DESCRIPTION: Apartment, Long-Term Care, Retirement

BUILDING: 1

ZONE CATEGORY: Residential

BY-LAW: 0225-2007

DESIGNATION: Residential High Density

Z-Area: Z08

	REQUIRED	PROPOSED
LOT AREA (M)		1,022.21 m ²
LOT FRONTAGE (M)	30.00 m	20.00 m
LOT COVERAGE (MAX)	-	16.00 %
** BUILDING HEIGHT		
MINIMUM	-	40.80m - 11 Storeys
MAXIMUM	13.00 m - 4 Storeys	
** LANDSCAPE BUFFER		
LANDSCAPING BUFFER ABUTTING A STREET	4.50 m	4.80 m
LANDSCAPING BUFFER ALONG LOT LINE	3.00 m	0.00 m
LANDSCAPED AREA	40% OF LOT AREA	32.74%
** REQUIRED YARDS (MIN.)		
FRONT YARD SETBACK (MIN.)	7.50 m	5.50 m
REAR YARD SETBACK (MIN.)	4.50 m	4.50 m
INTERIOR SIDE YARD SETBACK (MIN.)	4.50 m	4.00 m
EXTIOR SIDE YARD SETBACK (MIN.)	-	-
EXTIOR SIDE YARD SETBACK (MAX.)	-	-
AMENITY SPACES		
TOTAL AMENITY SPACES AREA	The greater of 3.8% of gross floor area or 10% of the site area + 476 m ²	580.86 m ²
AMENITY OUTDOOR AREA	Min. 55 m ²	73.9 m ²

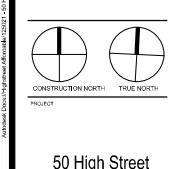
KEY PLAN

SETBACK PLAN

SETBACK PLAN

1:300

KEY LEGEND	
SITE PLAN LEGEND	
▲ ↑	ENTRANCE / EXIT
—	PROPERTY LINE
—	BUILDING SETBACK LINE
—	LANDSCAPE SETBACK LINE
—	EASEMENT AREA
■	PROPOSED BUILDING
■	EXISTING BUILDING
—	ASPHALT
—	LANDSCAPE / SOD AREA
—	CONCRETE SIDEWALK / CURB
—	PEDESTRIAN CROSSWALK
—	MANHOLE
—	CATCH-BASIN
—	DEBARRIED BARRELS/TREE
—	PARKING SPACE
—	6m WIDE FIRE ROUTE WITH HEAVY DUTY ASPHALT
—	SWIMMING CONNECTION
—	PROPOSED FIRE HYDRANT
—	LIGHT STANDARD
1	PROPOSED PAD MOUNTED TRANSFORMER LOCATED TO ELECTRICAL DRAWINGS
—	DEPRESSED CURB
○	PARKING COUNT



50 High Street
Affordable

50 High Street E, Mississauga

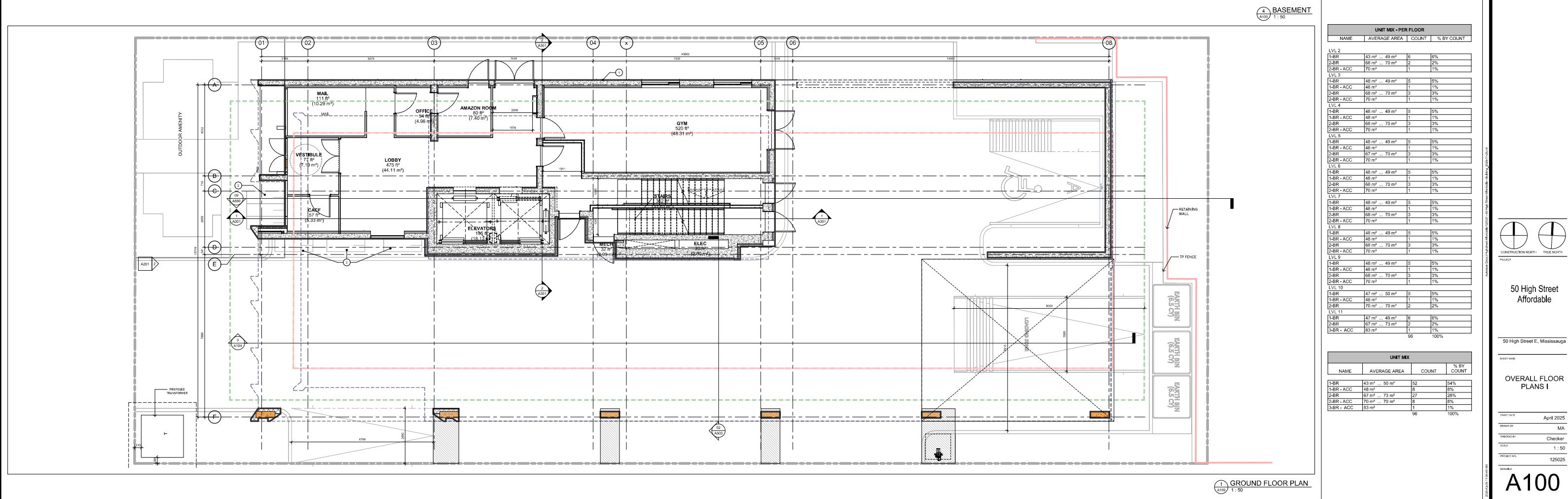
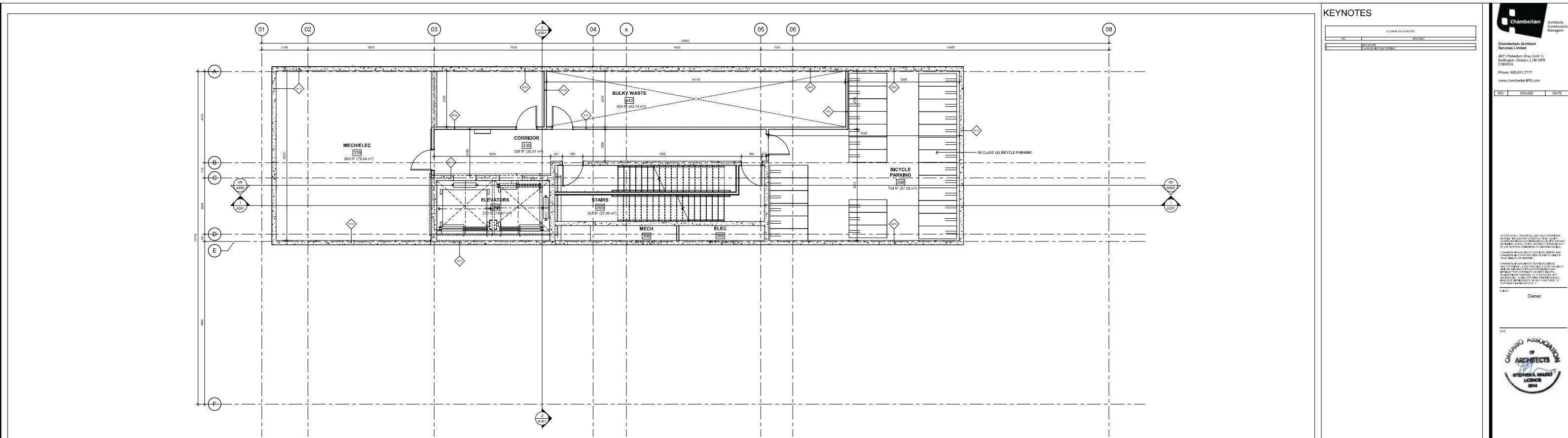
ANSWER

START DATE April 2025

SEARCHED BY

125021

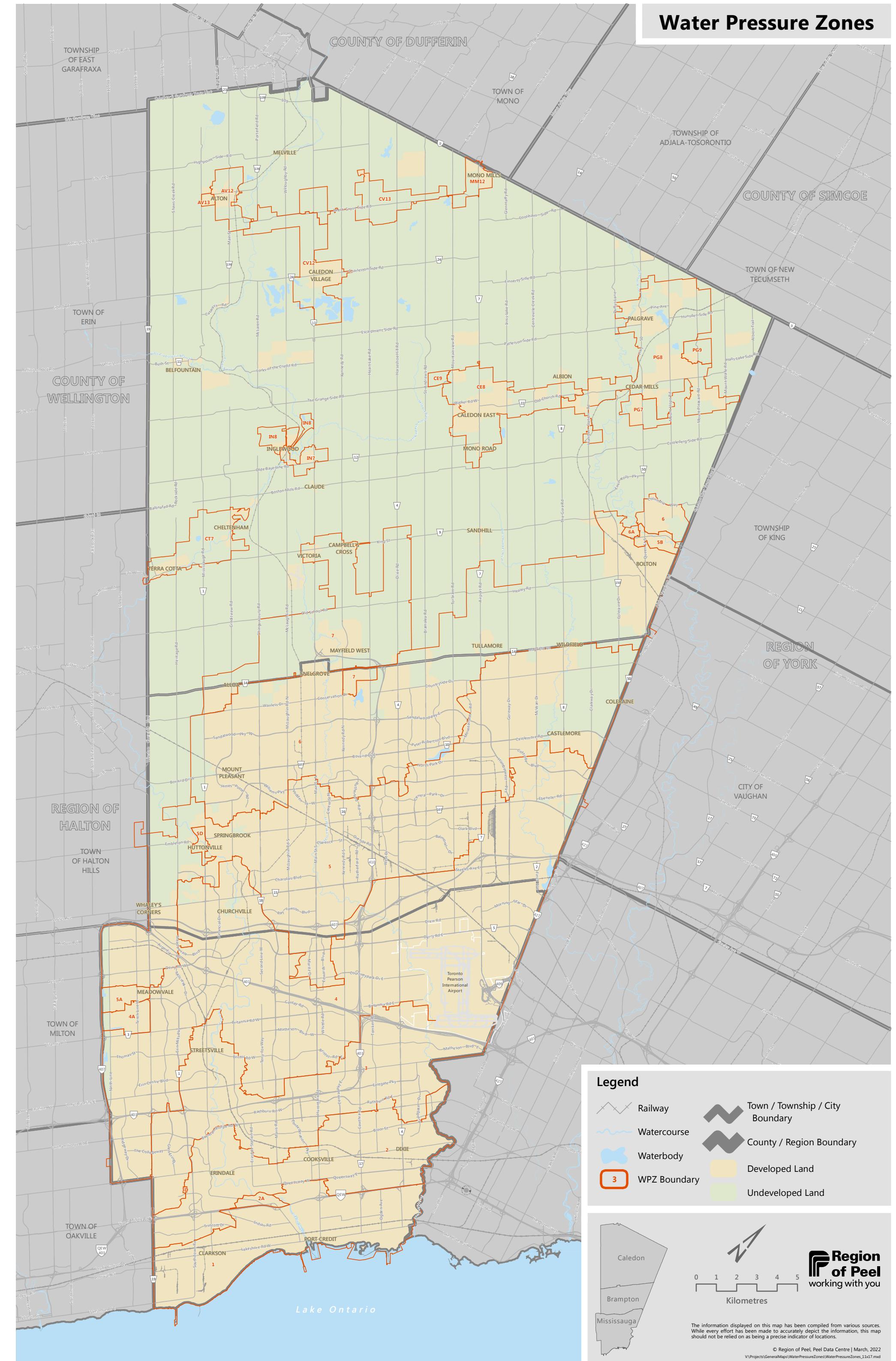
A.001



APPENDIX B

Water Servicing Calculations

Water Pressure Zones





Project: 50 High Street East
Project No.: 2880-7436
Created By: JPL
Checked By: JS
Date: 2025-08-01

Existing Water Demand

Site Area (m²) : 1022.21

Site Area (ha): 0.10

Notes & References

Residential

Residential: Small Apartments			
Housing Type	No. of Units	Population Density	Population
1 Bedroom	11	1.7	19

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Check:

If the proposed population equivalent for apartments is greater than 475 person/hectare, then the population equivalent used for design shall be calculated based on a density of 2.7 persons per unit using the equation below:

$$\frac{2.7 \text{ppu} \times \text{No. Units}}{\text{Area}} = \text{persons/hectare}$$

$$\frac{2.7 \times 11}{0.1} = 297 \text{ persons/hectare}$$

Therefore, use a proposed population equivalence of 1.7 persons/unit.

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Design Parameters

Residential Average Demand (L/capita/d)	
280	

Region of Peel - Linear Infrastructure - Watermain Design Criteria - (Rev. June 2010)

Average Daily Demand = 5236.00 L/day

Average Daily Demand = 0.06 L/s

Peaking Factors

Max. Day = 2.00
 Peak Hour = 3.00

Type of Use	Average Daily Water Demand (L/s)	Maximum Day Demand (L/s)	Peak Hourly Demand (L/s)
Residential	0.06	0.12	0.18
Total	0.06	0.12	0.18



Project: 50 High Street East
Project No.: 2880-7436
Created By: JPL
Checked By: JS
Date: 2025-08-01

Proposed Water Demand

Site Area (m²) : 1022.21

Site Area (ha): 0.10

Notes & References

Residential

Residential			
Housing Type	No. of Units	Population Density	Population
1 Bedroom	60	2.7	162
2 Bedroom	35	2.7	95
3 Bedroom	1	2.7	3
Total	96		259

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Check:

If the proposed population equivalent for apartments is greater than 475 person/hectare, then the population equivalent used for design shall be calculated based on a density of 2.7 persons per unit using the equation below:

$$\frac{2.7 \text{ppu} \times \text{No. Units}}{\text{Area}} = \text{persons/hectare}$$

$$\frac{2.7 \times 96}{0.1} = 2592 \text{ persons/hectare}$$

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Therefore, use a proposed population equivalence of 2.7 persons per unit.

Design Parameters

Residential Average Demand (L/capita/d)
280

Region of Peel - Linear Infrastructure - Watermain Design Criteria - (Rev. June 2010)

Average Daily Demand = 72576.00 L/day
 Average Daily Demand = 0.84 L/s

Peaking Factors

Max. Day = 2.00
 Peak Hour = 3.00

Type of Use	Average Daily Water Demand (L/s)	Maximum Day Demand (L/s)	Peak Hour Demand (L/s)
Residential	0.84	1.68	2.52
Total	0.84	1.68	2.52



Project: 50 High Street East
 Project No.: 2880-7436
 Created By: JPL
 Checked By: JS
 Date: 2025-12-10

Water Supply for Public Fire Protection - 2020
Fire Underwriters' Survey
Part II - Guide for Determination of Required Fire Flow

1. An estimate of fire flow required for a given area may be determined by the formula:

$$F = 220 * C * \text{sqrt } A$$

where

F = the required fire flow in litres per minute

C = coefficient related to the type of construction:

=	1.5	for wood frame construction (structure essentially all combustible)
=	1.0	for ordinary construction (brick or other masonry walls, combustible floor and interior)
=	0.8	for non-combustible construction (unprotected metal structural components)
=	0.6	for fire-resistant construction (fully protected frame, floors, roof)

A = The total floor area in square metres (including all storeys, but excluding basements at least 50 percent below grade) in the building considered.

Proposed Buildings

SIXTH FLOOR	606.63 sq.m
SEVENTH FLOOR	606.63 sq.m
EIGHTH FLOOR	606.63 sq.m

Area = 909.95 sq.m Area of the largest floor plus 25% of each of the two immediately adjoining floors.

C = 0.6

Therefore F = 3,982 L/min

Rounded to nearest 1000 L/min: 4,000 L/min

2. Values obtained in No. 1 may be reduced by as much as 25% for occupancies having low contents fire hazard or may be increased by up to 25% surcharge for occupancies having a high fire hazard.

Credits	Charges
Non-Combustible	-25%
Limited Combustible	-15%
Combustible	0%
Occupancy Category:	-15%
	-600 L/min Reduction
	3,400 L/min

Note: Fire flow shall not be less than 2,000 L/min

3. Sprinklers - The value obtained in No. 2 above may be reduced by up to 50% for complete automatic sprinkler protection. The credit for the system will be a maximum of 30% for an adequately designed system conforming to NFPA 13 and other NFPA sprinkler standards.

Automatic Sprinkler Protection:	50% (Credit)
NFPA 13 or Equivalent:	30% (Credit)
No sprinkler protection	0% (Null)
-1,700 L/min Reduction	

4. Exposure - To the value obtained in No. 2, a percentage should be added for structures exposed within 45 metres by the fire area under consideration. The percentage shall depend upon the height, area, and construction of the building(s) being exposed, the separation, openings in the exposed building(s), the length and height of exposure, the provision of automatic sprinklers and/or outside sprinklers in the building(s) exposed, the occupancy of the exposed building(s) and the effect of hillside locations on the possible spread of fire.

Separation	Charge
0 to 3 m	25%
3.1 to 10 m	20%
10.1 to 20 m	15%
20.1 to 30 m	10%
Greater than 30 m	0%

Direction	Distance (m)	Charge (%)	Surcharge (L/s)
E	11.5	15%	510
W	14.5	15%	510
N	>30	0%	-
S	>30	0%	-
1,020 L/min surcharge			

Determine the required fire flow for the proposed development:

No. 1	3,982
No. 2	-600 reduction
No. 3	-1,700 reduction
No. 4	1,020 surcharge

Required Fire Flow:	2,702 L/min
Rounded to nearest 1000 L/min:	3,000 L/min
Minimum Required Fire Flow:	4,800 L/min
Convert to L/s:	80.0 L/s

JP Labonte

From: Hosam Asem <hasem@chamberlainipd.com>
Sent: July 31, 2025 2:47 PM
To: JP Labonte
Cc: Menna Ali; Steve Mauro; Adrian Mauro; Tony De Franco; Christina Borowiec; Tim Neeb; Julie Scott
Subject: Re: CFC 2880-7436: 50 High Street East - FUS Confirmation Letter

Hi Labonte,

Please find below the requested information for the FUS categories :

- **Construction Type:** Fire-Resistive Construction (a)

A building design where all structural elements, walls, arches, floors, and roofs are constructed with a minimum 2-hour fire resistance rating, and all materials used in the construction of the structural elements are non-combustible.

- **Occupancy Category:** Limited Combustible Content

- **Sprinkler Type:** Fully Supervised Automatic Sprinkler System

Please let me know if you need any additional details

Kind regards,

Hossam Asem,

Designer

CHAMBERLAIN ARCHITECT SERVICES LIMITED

shaping your world

✉: hasem@chamberlainipd.com

🌐: www.chamberlainIPD.com

From: Menna Ali <mali@chamberlainipd.com>
Sent: July 30, 2025 10:13 AM
To: Hosam Asem <hasem@chamberlainipd.com>
Subject: Fw: CFC 2880-7436: 50 High Street East - FUS Confirmation Letter

Menna Ali,

Designer

CHAMBERLAIN ARCHITECT SERVICES LIMITED
shaping your world

✉: mali@chamberlainipd.com

🌐: www.chamberlainIPD.com

From: JP Labonte <jplabonte@cfcrozier.ca>

Sent: Wednesday, July 30, 2025 9:58 AM

To: Adrian Mauro <amauro@chamberlainIPD.com>; Steve Mauro <SMauro@chamberlainipd.com>; Menna Ali <mali@chamberlainipd.com>

Cc: Tony De Franco <tony@sajeckiplanning.com>; Christina Borowiec <christina@sajeckiplanning.com>; Tim Neeb <tim@mahoganymanagement.com>; Julie Scott <jscott@cfcrozier.ca>

Subject: CFC 2880-7436: 50 High Street East - FUS Confirmation Letter

Hi all,

Can you please provide us a letter confirming the FUS categories used for the design of the building? Please see below for what we'll require on the letter:

1. Confirm the construction type of the building: Fire-Resistive Construction (a) or Non-Combustible Construction (b)
 - a. A building design where all structural elements, walls, arches, floors, and roofs are constructed with a min. 2-hr fire resistance rating, and all materials used in the construction of the structural elements etc. are constructed with non-combustible materials.
 - b. A building design where all structural elements, walls, arches, floors, and roofs are constructed with a min. 1-hr fire resistance rating and are constructed with non-combustible materials.
2. Confirm the occupancy category: Non-Combustible Content or Limited Combustible Content
3. Confirm the sprinkler type: Fully Supervised Automatic Sprinkler System, NFPA 13 or equivalent, or no sprinkler system

Please note that we'll need this letter asap before the expected submission date for this Friday to include in our FSSWM report.

Let me know if you have any questions and/or concerns with the above.

Thank you!

JP Labonte

Engineering Intern, Land Development
Office: 905.876.7158

Collingwood | Milton | Toronto | Bradford | Guelph

**Learn how we've strengthened our
position as a total build partner.**



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Hydrant Flow Test Report

Residual Hydrant Number _____

Date: 11-Jun-25 Time: 10:15 AM Operator: Colin Powell

Witness: Region of Peel

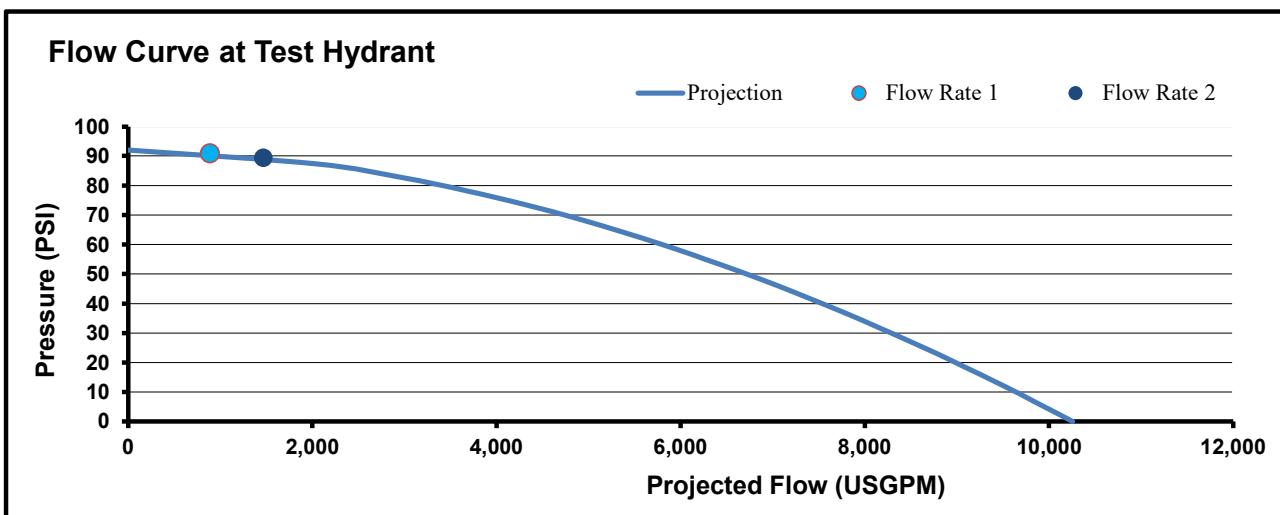
Residual Test Hydrant:	7 Helene Street North (at High St E)	
Hydrant Number:		NFPA Colour Code: CLASS AA - BLUE
Owner:	Region of Peel	

STATIC PRESSURE:	92 psi	634 kPa	Pressure Drop
RESIDUAL PRESSURE 1:	91 psi	627 kPa	
RESIDUAL PRESSURE 2:	89.5 psi	617 kPa	2.7%

Flow Hydrants:	Hydrant Number	
	A	80 High Street East (on Ann Street)
	B	
C		

Hydrant No.	Flow Device	Outlet Dia. (in.)	Flow Rate 1		Flow Rate 2	
			Reading (psi)	(USGPM)	Reading (psi)	(USGPM)
A	Pitot	2.5	32	882	22	732
A	Pitot			0	22	732
A	HoseMonster		4"	0		
Total Flow (USGPM)			882		1463	
Total Flow (L/second)			56		92	
Available Flow At Test Hydrant at 20 ps			8,885	USGPM	8,983	USGPM
			561	L/second	567	L/second

Average Projection at 20 PSI **8,934** USGPM



Comments/Discrepancies/Diagram:

APPENDIX C

Sanitary Servicing Calculations



Project: 50 High Street East
Project No.: 2880-7436
Created By: JPL
Checked By: JS
Date: 2025-08-01

Existing Sanitary Design Flow

Site Area (m²) : 1022.21

Site Area (ha): 0.10

Residential

Residential: Small Apartments

Housing Type	No. of Units	Population Density	Population
1 Bedroom	11	1.7	19

Notes & References

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Check:

If the proposed population equivalent for apartments is greater than 475 person/hectare, then the population equivalent used for design shall be calculated based on a density of 2.7 persons per unit using the equation below:

$$\frac{2.7 \text{ppu} \times \text{No. Units}}{\text{Area}} = \text{persons/hectare}$$

$$\frac{2.7 \times 11}{0.1} = 297 \text{ persons/hectare}$$

Therefore, use a proposed population equivalence of 1.7 persons/unit.

Design Parameters

Average Residential Flow (L/capita/d)

290

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Infiltration Flow (L/ha/s):

0.26

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Equations:

Harmon Peaking Factor
$M = 1 + (14 / (4 + (P/1000)^{0.5})). \text{Min}=2, \text{Max}=4$

Harmon Peaking Factor

$$M = 1 + (14 / (4 + (P/1000)^{0.5})). \text{Min}=2, \text{Max}=4$$



Project: 50 High Street East
Project No.: 2880-7436
Created By: JPL
Checked By: JS
Date: 2025-08-01

Proposed Sanitary Design Flow

Site Area (m²) : 1022.21

Site Area (ha): 0.10

Notes & References

Residential

Residential			
Housing Type	No. of Units	Population Density	Population
1 Bedroom	60	2.7	162
2 Bedroom	35	2.7	95
3 Bedroom	1	2.7	3
Total	96		259

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Check:

If the proposed population equivalent for apartments is greater than 475 person/hectare, then the population equivalent used for design shall be calculated based on a density of 2.7 persons per unit using the equation below:

$$\frac{2.7 \text{ppu} \times \text{No. Units}}{\text{Area}} = \text{persons/hectare}$$

$$\frac{2.7 \times 96}{0.1} = 2592 \text{ persons/hectare}$$

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Therefore, use a proposed population equivalence of 2.7 persons per unit.

Design Parameters

Average Residential Flow (L/capita/d)

290

Region of Peel - Linear Wastewater Standards, Chapter 2 - (R 1.0, 2023/03/29)

Infiltration Flow (L/ha/s): 0.26

Type of Use	Average Daily Flow (L/s)	Harmon Peaking Factor	Peak Flow (L/s)	Infiltration Flow (L/s)	Total Peak Flow (L/s)
Residential	0.87	4.00	3.48	0.03	3.51
Total					3.51

Equations:

Harmon Peaking Factor
 $M = 1 + (14 / (4 + (P/1000)^{0.5})), \text{Min}=2, \text{Max}=4$

APPENDIX D

Groundwater Drainage Conditions

J.P. Labonte

From: Yourong Li (Toronto Inspection Ltd.) <yourong@torontoinspection.com>
Sent: November 26, 2025 2:36 PM
To: J.P. Labonte
Cc: Julie Scott; Isabelle Forsyth; Matt Coleridge
Subject: Re: PN6857 - 50 High St E, Mississauga, LTM November 2025

Hi J.P.,

That sounds like a reasonable assumption for now. We just need to confirm this with long-term monitoring.

Many thanks,

Yourong Li M.Eng., G.I.T., E.P.t.

Project Manager, Hydrogeology and Environmental Services



110 Konrad Crescent, Unit 16

Markham, Ontario, L3R 9X2

T: 905-940-8509 ext.230

F: 905-940-8192

W: torontoinspection.com

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On Wednesday, November 26, 2025 at 02:33:08 PM EST, J.P. Labonte <jplabonte@cfcrozier.ca> wrote:

Hi Yourong,

After discussing internally, we would like to move the infiltration gallery to the back of the building where the results showed a lower HWL at BH-3.

Can you please confirm the use of a HWL elevation of **74.43m** (73.43m + 1.0m) is feasible at the back of the site?

Thank you.

J.P. Labonte, P.Eng.
Project Engineer, Land Development
Office: 905.876.7158
Collingwood | Milton | Toronto | Bradford | Guelph

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From: J.P. Labonte <jplabonte@cfcrozier.ca>
Sent: November 26, 2025 12:11 PM
To: Yourong Li (Toronto Inspection Ltd.) <yourong@torontoinspection.com>
Cc: Julie Scott <jscott@cfcrozier.ca>; Isabelle Forsyth <iforsyth@cfcrozier.ca>; Matt Coleridge <mcoleridge@cfcrozier.ca>
Subject: RE: PN6857 - 50 High St E, Mississauga, LTM November 2025

Hi Yourong,

Thank you for providing this information to us.

We will take this back internally and reach out if we have any questions.

Kind regards,

J.P. Labonte, P.Eng.
Project Engineer, Land Development
Office: 905.876.7158
Collingwood | Milton | Toronto | Bradford | Guelph

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From: Yourong Li (Toronto Inspection Ltd.) <yourong@torontoinspection.com>

Sent: November 26, 2025 10:55 AM

To: J.P. Labonte <jplabonte@cfcrozier.ca>

Cc: Julie Scott <jscott@cfcrozier.ca>

Subject: Fw: PN6857 - 50 High St E, Mississauga, LTM November 2025

Hello JP,

Please kindly see below.

As of the moment, I would use 76.52 as the seasonal high GWL for design purpose. This estimation may change as we carry out our long term GWL monitoring.

Many thanks,

Yourong Li M.Eng., G.I.T., E.P.t.

Project Manager, Hydrogeology and Environmental Services



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----- Forwarded Message -----

From: Kevin Nankisore (Toronto Inspection Ltd.) <kevin@torontoinspection.com>

To: Yourong Li (Toronto Inspection Ltd.) <yourong@torontoinspection.com>

Sent: Wednesday, November 26, 2025 at 10:46:16 AM EST

Subject: PN6857 - 50 High St E, Mississauga, LTM November 2025

Hi Yourong,

A site visit for long-term monitoring at 50 High St E, Mississauga, was completed on November 25, 2025. Please see the table below for the recorded groundwater level measurements (in mbgs and masl).

Water Level Measurements November 25, 2025

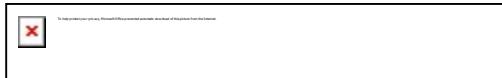
Well ID	mbgs	masl
25BH-1 (MW)	1.35	75.52
25BH-3 (MW)	4.39	73.43

Please note that, as these measurements were taken in late November (typically a lower groundwater period), an additional metre should be added to estimate the potential seasonal high groundwater level at this site. This estimate may be refined as the long-term monitoring period progresses and additional data becomes available.

Best regards,

Kevin Nankisore M.Eng., G.I.T., E.P.t.

Project Coordinator, Hydrogeological Services



110 Konrad Crescent, Unit 16

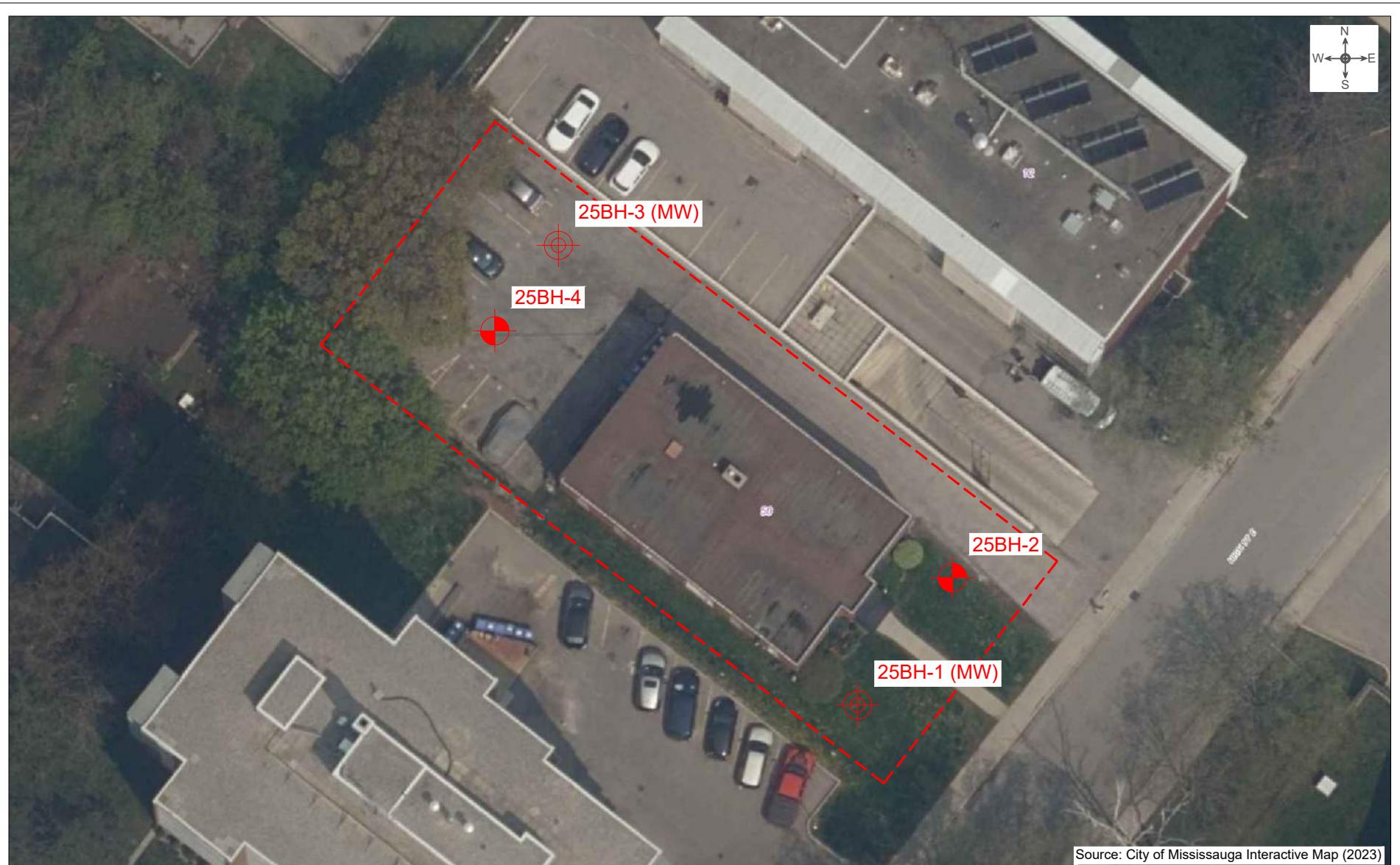
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LEGEND:



Borehole and Monitoring Well Location



Site Boundary

NOT TO SCALE

TorontoInspection
GEO-ENVIRONMENTAL CONSULTANTS

Tel: 905-940 8509

Fax: 905-940 8192

Email : TIL@torontoinspection.com

110 Konrad Crescent,
Unit 16
Markham, Ontario
L3R 9X2

TITLE:		Borehole and Monitoring Well Location Plan		
LOCATION:		50 High Street East, Mississauga, Ontario		
PROJECT NO.	6857-25-GB	DATE :	April 2025	DRAWING NO.
				1

APPENDIX E

Stormwater Management Calculations



CROZIER
CONSULTING ENGINEERS

Project: 50 High Street East
Project No.: 2880-7436
Created By: JPL
Checked By: JS
Date: 2025-12-12

Modified Rational Calculations - Input Parameters

Time of Concentration: $T_c = 15.00$ mins

Storm Data: City of Mississauga

Return Period	A	B	C	I (mm/hr)
10-Yr	1010.0	4.6	0.780	99.166
100-Yr	1450.0	4.9	0.780	140.690

Pre-Development Conditions

Land Type	Area (ha)	Area (m ²)	C	Weighted Average C
Catchment 100 to Storm Sewer along High Street East				
Pervious	0.02	190.00	0.25	0.05
Impervious	0.05	542.21	0.90	0.48
Roof	0.03	290.00	0.90	0.26
Total Subcatchment	0.10	1022.21	-	0.78
Total Site	0.10	1022.21		

Post-Development Conditions

Land Type	Area (ha)	Area (m ²)	C	Weighted Average C
Catchment 200 to Stormwater Management Tank - Controlled to High Street East				
Pervious	0.01	101.40	0.25	0.03
Roof Pervious	0.01	86.70	0.25	0.02
Impervious	0.07	747.71	0.90	0.72
Total Subcatchment	0.09	935.81	-	0.77
Total Site	0.10	1022.21		
Land Type	Area (ha)	Area (m ²)	C	Weighted Average C
Catchment 201 - Uncontrolled to High Street East				
Pervious	0.00	7.00	0.25	0.02
Impervious	0.01	79.40	0.90	0.83
Total Subcatchment	0.01	86.40	-	0.85
Total Site	0.10	1022.21		

Equations:

$$\text{Intensity} \\ I = A/(T_c + B)^C$$

$$\text{Peak Flow} \\ Q = 0.0028 \cdot C \cdot I \cdot A$$



Project: 50 High Street East

Project No.: 2880-7436

Created By: JPL

Checked By: JS

Date: 2025-12-12

Modified Rational Method Calculations - Release Rates

Pre-Development

Catchment 100 to Storm Sewer along High Street East

Storm Event	C	I (mm/hr)	A (ha)	Adjustment Factor	Q _{pre100} (m ³ /s)	Q _{pre100} (L/s)
10-Yr	0.78	99.166	0.102	1.0	0.02	21.96

Allowable Release Rate to High Street East - 10 Year (L/s) = **21.96**

Post-Development

Catchment 200 to Stormwater Management Tank - Controlled to High Street East

Storm Event	C	I (mm/hr)	A (ha)	Adjustment Factor	Q _{post200} (m ³ /s)	Q _{post200} (L/s)
100-Yr	0.77	140.690	0.094	1.25	0.04	35.20

Catchment 201 - Uncontrolled to High Street East

Storm Event	C	I (mm/hr)	A (ha)	Adjustment Factor	Q _{post201} (m ³ /s)	Q _{post201} (L/s)
100-Yr	0.85	140.690	0.009	1.25	0.004	3.58

Peak Flows (L/s)

Storm Event	Pre-Development to High Street East	Post-Development to High Street East				
		Q _{pre100}	Q _{target} (10-Yr)	Q _{post200} (100-Yr)	Q _{post201} (100-Yr)	Q _{c.post}
10-Yr	21.96	21.96	35.20	3.58	15.12	18.70

Equations:

Total Post-Development Flow (100-Year)

$$Q_{total} = Q_{post200} + Q_{post201}$$



Modified Rational Method Calculations - Control Orifice

Orifice Type =	tube
Invert Elevation =	75.36 m
Diameter of Orifice =	75 mm
Area of Orifice (A) =	0.0044 sq.m
Orifice Coefficient (Cd) =	0.80

Calculation of Head

Centroid Elevation =	75.40 m
Water Elevation =	76.33 m
Upstream Head*, (h) =	0.93 m

Controlled Discharge, $Q_{c,post}$ =	$(Cd)(A)(2gh)^{0.5}$
=	0.01512 m ³
=	15.12 L/s



Modified Rational Method Calculations - 100-Year Detention Volume

Rainfall IDF Coefficients	100-Year	
	A =	1450.0
	B =	4.90
	C =	0.78

Rational Method Calculation		
Area =	0.09	ha
Runoff Coefficient, C =	0.77	
C*A =	0.07	
Adjustment Factor	1.25	
Time of Concentration, t_c =	15.0	min
Storm Duration Increment =	10.0	min
Constant Inflow (Infiltrated Stormwater) =	0.00	L/s
Uncontrolled Outflow =	0.00	L/s
Release Rate =	15.12	L/s

Storm Duration (min)	Rainfall Intensity (mm/hr)	Max. Runoff Flow (L/s)	Runoff Volume (m ³)	Released Volume (m ³)	Storage Volume (m ³)	Max. Storage Volume Required (m ³)
15.0	140.690	35.17	31.65	13.61	18.05	
25.0	102.410	25.60	38.40	18.14	20.26	20.3
35.0	81.773	20.44	42.93	22.68	20.25	
45.0	68.683	17.17	46.36	27.21	19.15	
55.0	59.563	14.89	49.14	31.75	17.39	
65.0	52.805	13.20	51.48	36.28	15.20	
75.0	47.575	11.89	53.52	40.82	12.70	
85.0	43.395	10.85	55.33	45.35	9.97	
95.0	39.967	9.99	56.95	49.89	7.06	
105.0	37.101	9.27	58.43	54.42	4.01	
115.0	34.665	8.67	59.79	58.96	0.84	
125.0	32.565	8.14	61.06	63.49	0.00	
135.0	30.735	7.68	62.23	68.03	0.00	
145.0	29.123	7.28	63.34	72.56	0.00	
155.0	27.693	6.92	64.38	77.10	0.00	



CROZIER
CONSULTING ENGINEERS

Project: 50 High Street East
Project No: 2880-7436
Created By: JPL
Checked By: JS
Date: 2025-12-12

(100-Year) Tank Sizing

Tank Sizing

Required Active Detention Storage	20.3	m ³
Top of Tank Elevation	76.43	masl
Tank Outlet Elevation	75.36	masl
Bottom of Tank Elevation	75.36	masl
100-Year HWL Elevation	76.33	masl
100-Year HWL Depth	0.97	m
SWM Tank Dimensions		
Tank Area	21.0	m ²
Provided 100-Year Detention Storage	20.4	m ³



Project: 50 High Street East

Project No.: 2880-7436

Created By: JPL

Checked By: JS

Date: 2025-12-12

Water Quality Calculation - TSS Removal

Catchment 200 - Upstream of Stormwater Management Tank

Land Type	Area (m ²)	Water Quality Target (%)	% of Total Development Area	TSS Removal Credit (%)	Total TSS Removal (%)
Pervious	101.40	80.0%	9.9%	80.0%	7.9%
Roof Pervious	86.70		8.5%	80.0%	6.8%
Impervious - treated by OGS	747.71		73.1%	80.0%	58.5%
Sub-Total	935.81	-	91.5%	-	73.2%

Catchment 201 - Uncontrolled to High Street East

Land Type	Area (m ²)	Water Quality Target (%)	% of Total Development Area	TSS Removal Credit (%)	Total TSS Removal (%)
Pervious	7.00	80.0%	0.7%	80.0%	0.5%
Impervious	79.40		7.8%	80.0%	6.2%
Sub-Total	86.40	-	8.5%	-	6.8%
Total	1,022.21	-	100.0%	-	80.0%



CROZIER
CONSULTING ENGINEERS

Project: 50 High Street East
Project No.: 2880-7436
Created By: JPL
Checked By: JS
Date: 2025-12-12

Water Balance Calculation

Site Area = 1,022.21 m²

Required Average Annual Rainfall Depth = 5 mm

Total Required 5mm Retention Volume = 5.1 m³



Project: 50 High Street East
Project No.: 2880-7436
Created By: JPL
Checked By: JS
Date: 2025-12-12

INFILTRATION GALLERY

Type: Clearstone Wrapped in Geotextile Fabric

Bed Size: 28.0 m²
Total Active Retention Volume: 5.1 m³

Note: Total active retention volume represents the retention volume from bottom to top of gallery elevation

Infiltration Gallery Profile

Top of Grade:	77.1		
Bottom Elevation of Pavement Structure:	76.69	masl	dated 2025.06.04
System Obvert Elevation:	75.72	masl	
System Invert Elevation:	75.43	masl	
Bottom Elevation of Clearstone:	75.43	masl	
High Groundwater Table Elevation:	74.43	masl	Note: Groundwater elevation at 25BH-3 (73.43 masl + 1.0m)

Runoff Volume: 5.1 m³

Infiltration Rate: 13 mm/hr As per Toronto Inspection Ltd. via email correspondence - refer to **Appendix E** in the FSSWM Report.

Safety Factor: 2 -

Effective Infiltration Rate 6.5 mm/hr

Void Ratio: 0.4 m³/m³ Note: Clearstone assumed to have a void space of 0.4

Infiltration Area: 28.00 m²

Drawdown Time: 70 hr

Infiltrated Volume in 72 hrs: 5.24 m³

Equations:

Drawdown Time (hr)

DD_{TIME} = 1000 • Runoff Volume / Infiltration Rate • Void Ratio • Infiltration Area

J.P. Labonte

From: Yourong Li (Toronto Inspection Ltd.) <yourong@torontoinspection.com>
Sent: December 9, 2025 1:16 PM
To: Julie Scott
Cc: J.P. Labonte; Shan Goel
Subject: Re: PN6857 - 50 High St E, Mississauga, LTM November 2025
Attachments: Hydrometer Analysis.pdf

Hi Julie,

As discussed, please kindly see attached for our grain size analysis from 2.3 mbgs at 25BH-2. Unfortunately, when we drilled this spring, we did not run any hydrometer samples from the back of the site.

Based on one grain size sample from the front of the site, K value is estimated as 9.3×10^{-9} m/sec, which is equivalent to an unfactored infiltration rate of 13 mm/hr. Please note this rate estimation was generated using one single sample from a different part of the site. Although currently there is no reason to believe the rest of the site will be significantly different, in-situ infiltration test should be carried out to verify the infiltration rate at the proposed LID location.

Many thanks,

Yourong Li M.Eng., G.I.T., E.P.t.

Project Manager, Hydrogeology and Environmental Services



110 Konrad Crescent, Unit 16

Markham, Ontario, L3R 9X2

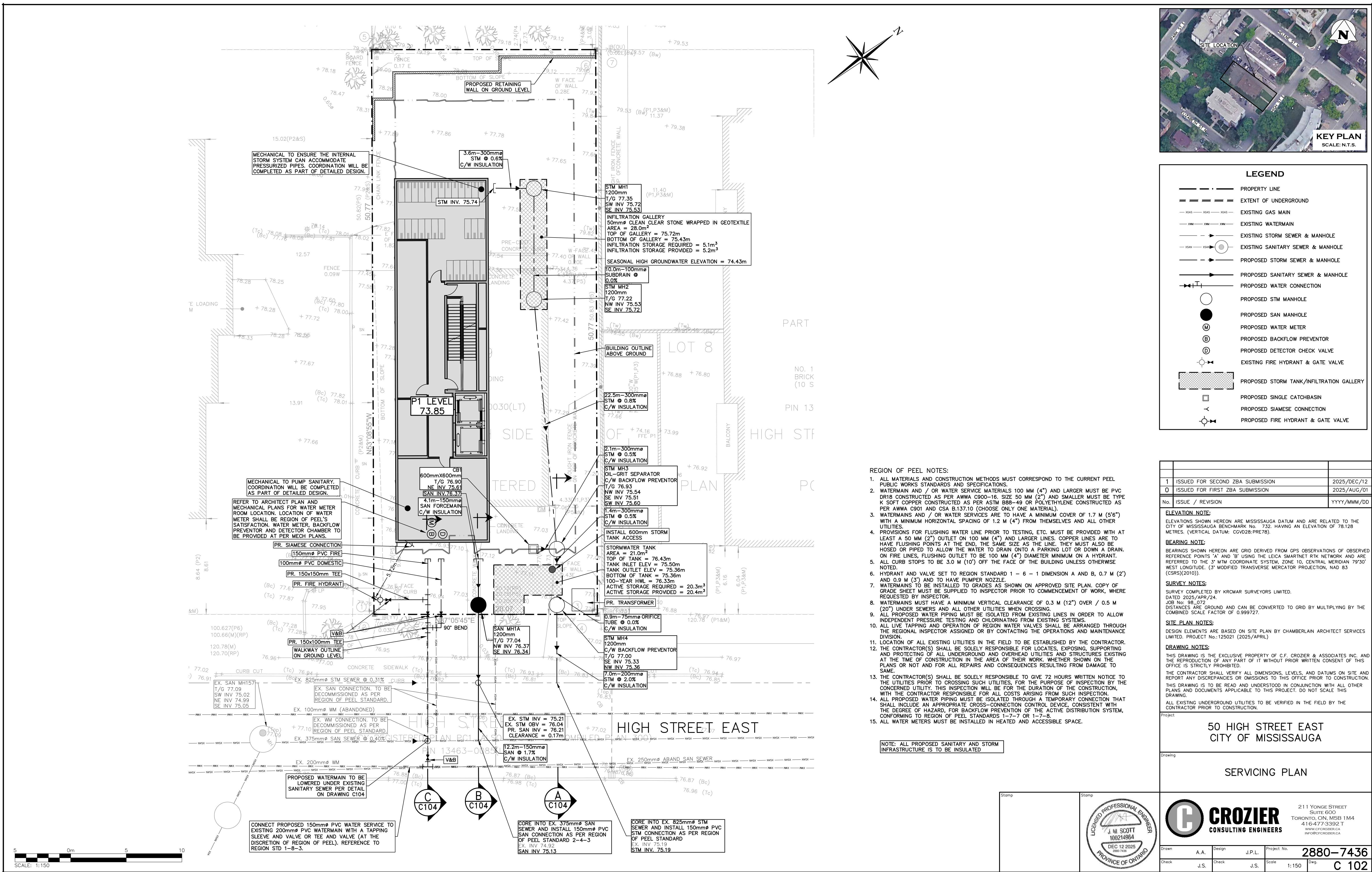
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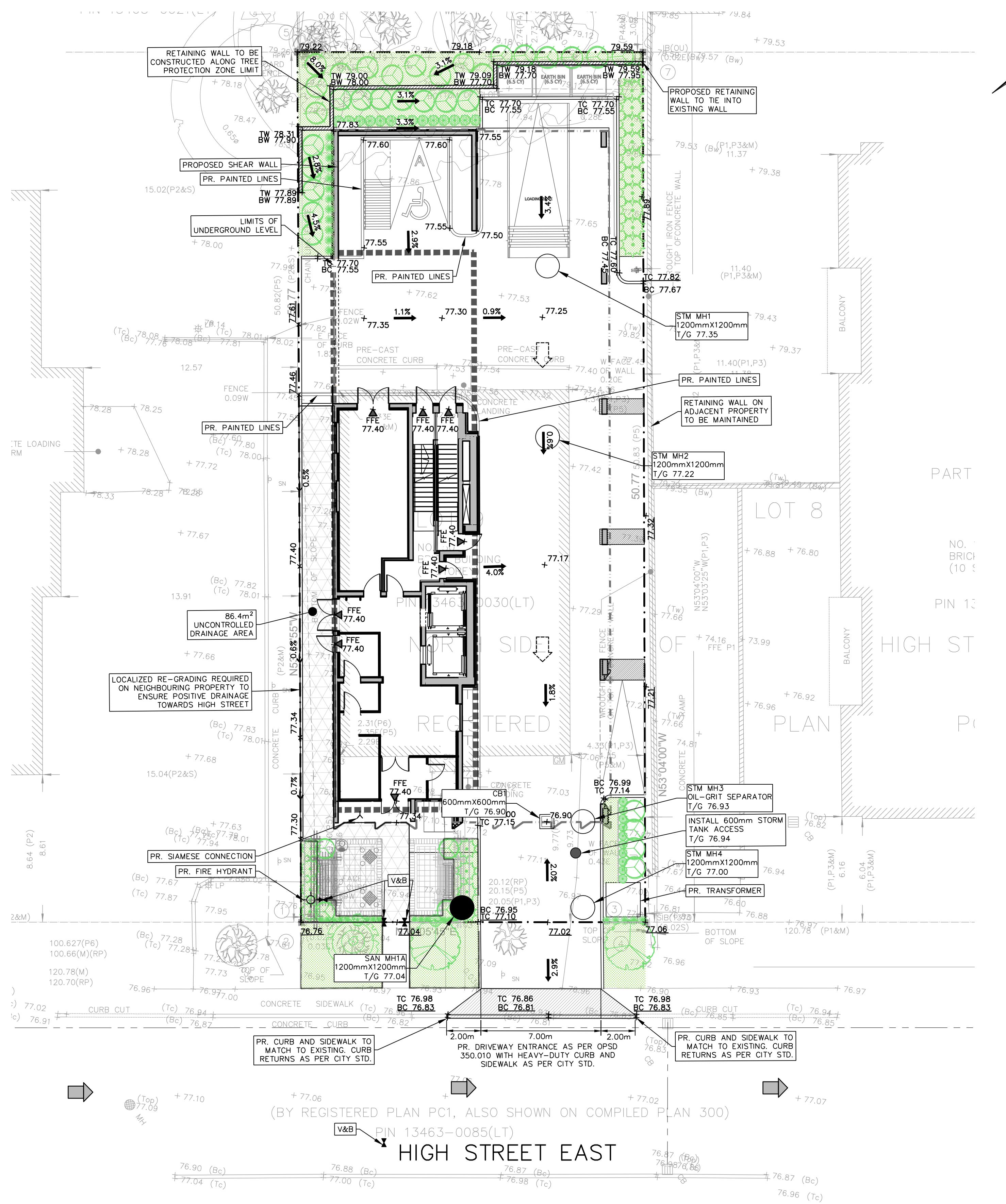
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DRAWINGS





LEGEND

	PROPERTY LINE
	EXTENT OF UNDERGROUND
	PROPOSED SWALE SLOPE
	EXTENT OF ABOVE GROUND
	TREE PROTECTION FENCE
	EXISTING GRADE
	PROPOSED GRADE
	PROPOSED GRADE (TO MATCH EXISTING)
	PROPOSED MINOR FLOW DIRECTION
	EXISTING FIRE HYDRANT & GATE VALVE
	EXISTING SANITARY MANHOLE
	PROPOSED STORM MANHOLE
	PROPOSED SANITARY MANHOLE
	EXISTING SINGLE / DOUBLE CATCHBASIN
	BUILDING ENTRANCE (PERSONNEL DOOR)
	PROPOSED OVERLAND FLOW DIRECTION
	EXISTING OVERLAND FLOW DIRECTION
	PROPOSED SINGLE CATCHBASIN
	PROPOSED FIRE HYDRANT & GATE VALVE
	UNCONTROLLED DRAINAGE AREA

1	ISSUED FOR SECOND ZBA SUBMISSION	2025/DEC/12
0	ISSUED FOR FIRST ZBA SUBMISSION	2025/AUG/01

ELEVATION NOTE:
ELEVATIONS SHOWN HEREON ARE MISSISSAUGA DATUM AND ARE RELATED TO THE CITY OF MISSISSAUGA BENCHMARK No. 732. HAVING AN ELEVATION OF 78.128 METRES. (VERTICAL DATUM: CGVD28: PRE78).

BEARING NOTE:
BEARINGS SHOWN HEREON ARE GRID DERIVED FROM GPS OBSERVATIONS OF OBSERVED REFERENCE POINTS 'A' AND 'B' USING THE LEICA SMARTNET RTK NETWORK AND ARE REFERRED TO THE 3° MTM COORDINATE SYSTEM, ZONE 10, CENTRAL MERIDIAN 79°30' WEST LONGITUDE. (3° MODIFIED TRANSVERSE MERCATOR PROJECTION, NAD 83 (CSRS)(2010)).

SURVEY NOTES:
SURVEY COMPLETED BY KRCMAR SURVEYORS LIMITED.
DATED 2025/APR/24.

JOB NO: 98_072
DISTANCES ARE GROUND AND CAN BE CONVERTED TO GRID BY MULTIPLYING BY THE
COMBINED SCALE FACTOR OF 0.999727.

SITE PLAN NOTES:

DESIGN ELEMENTS ARE BASED ON SITE PLAN BY CHAMBERLAIN ARCHITECT SERVICES

LIMITED. PROJECT No.:125021 (2025/APRIL)

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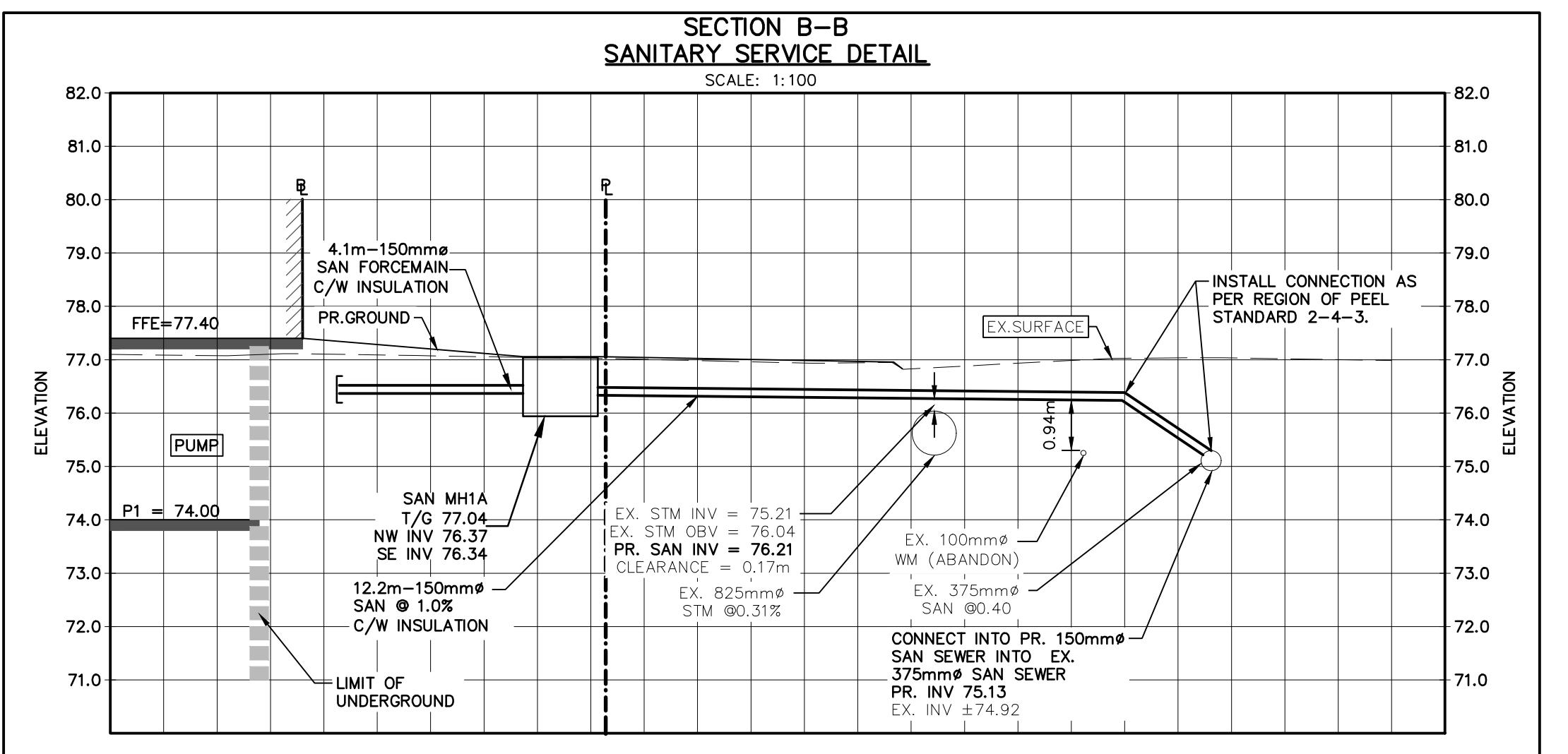
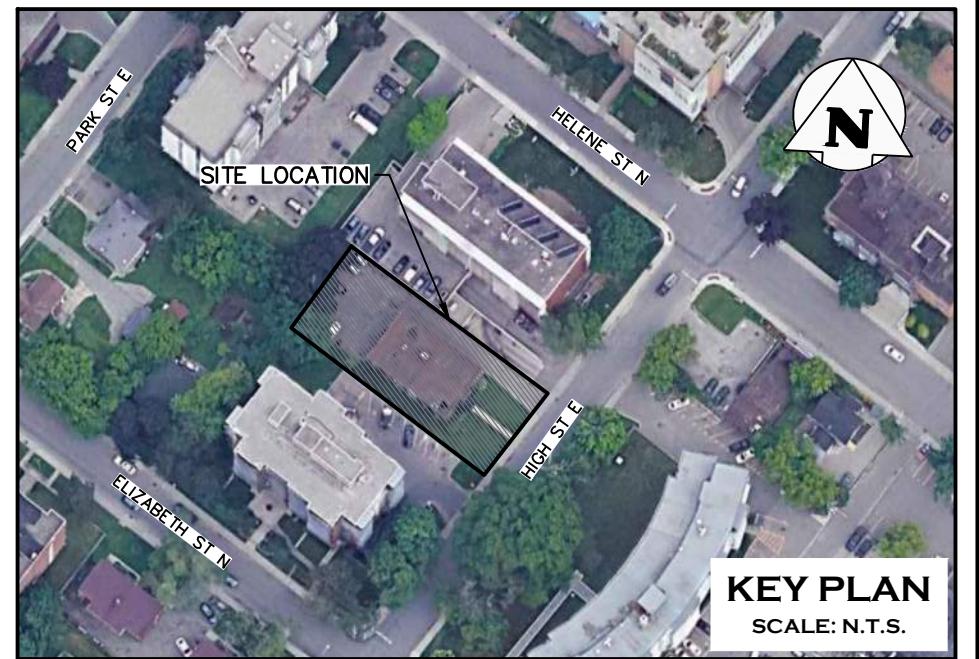
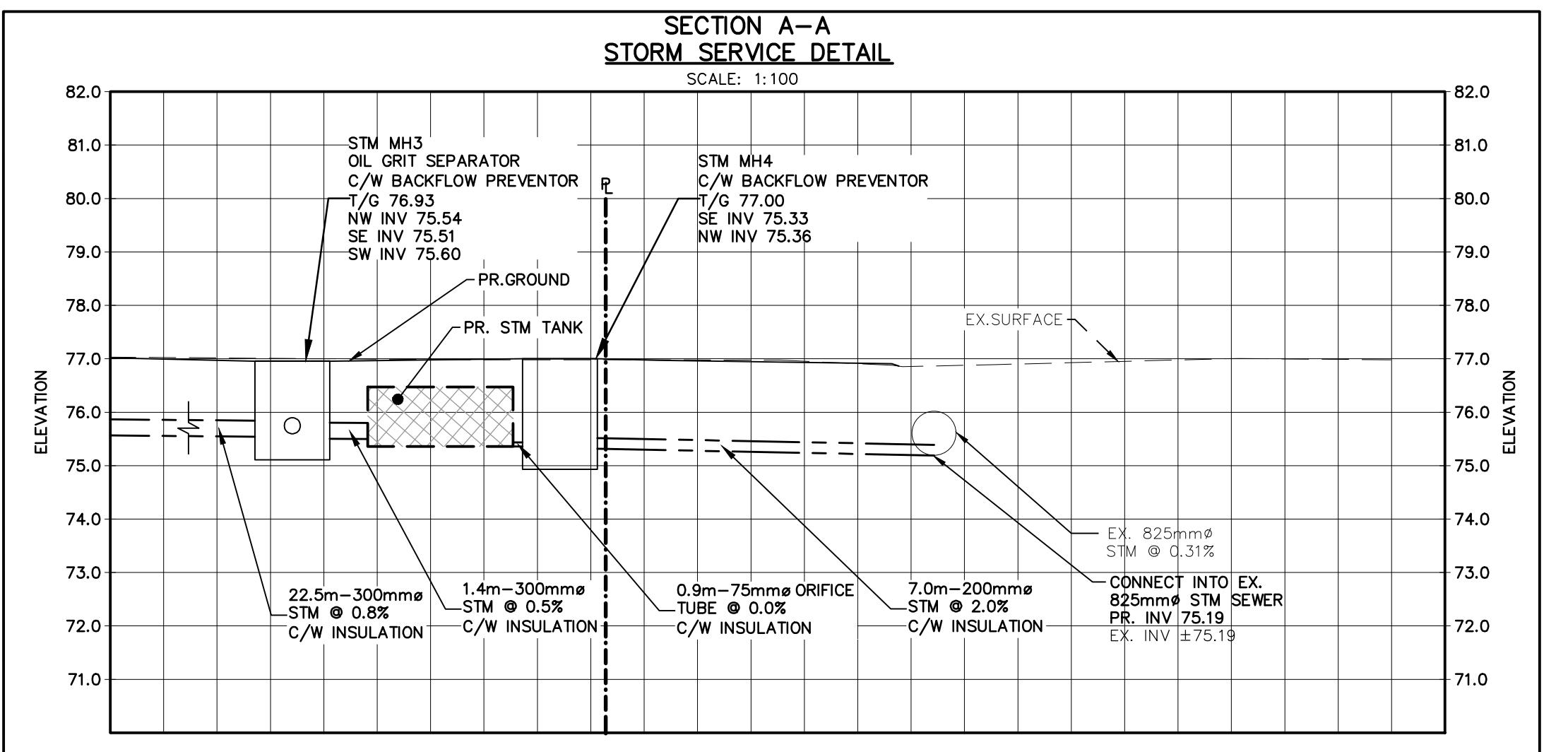
Project

50 HIGH STREET EAST
CITY OF MISSISSAUGA

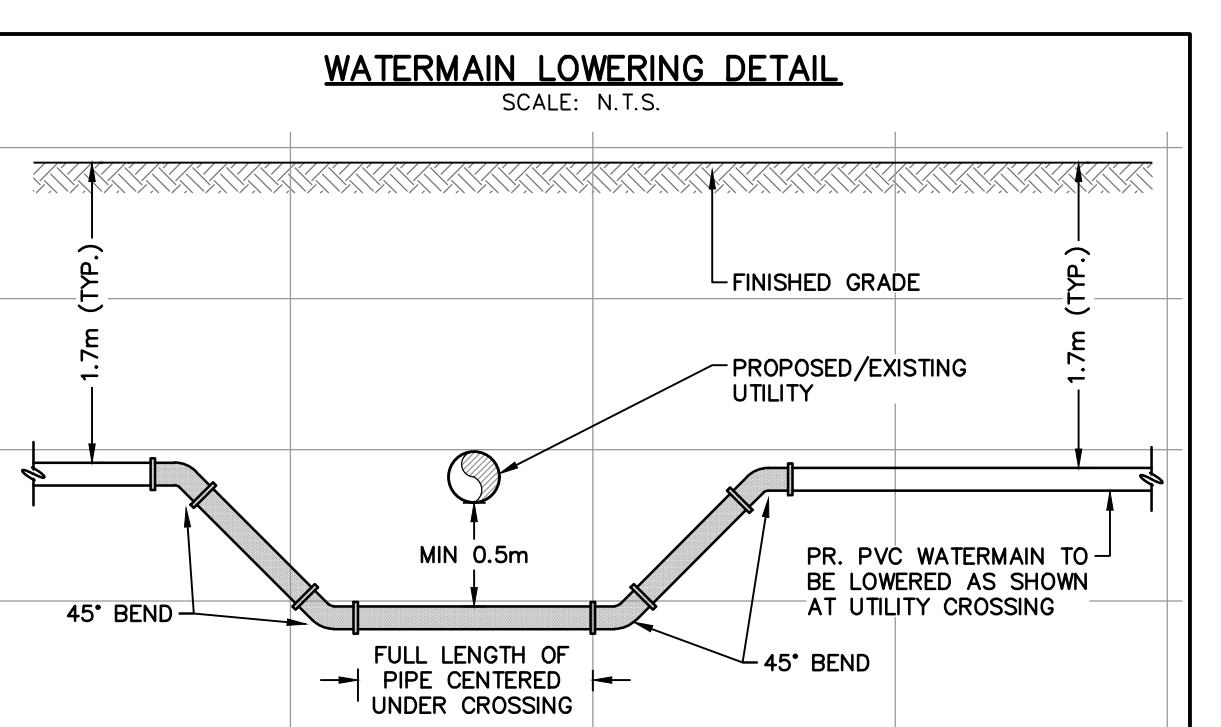
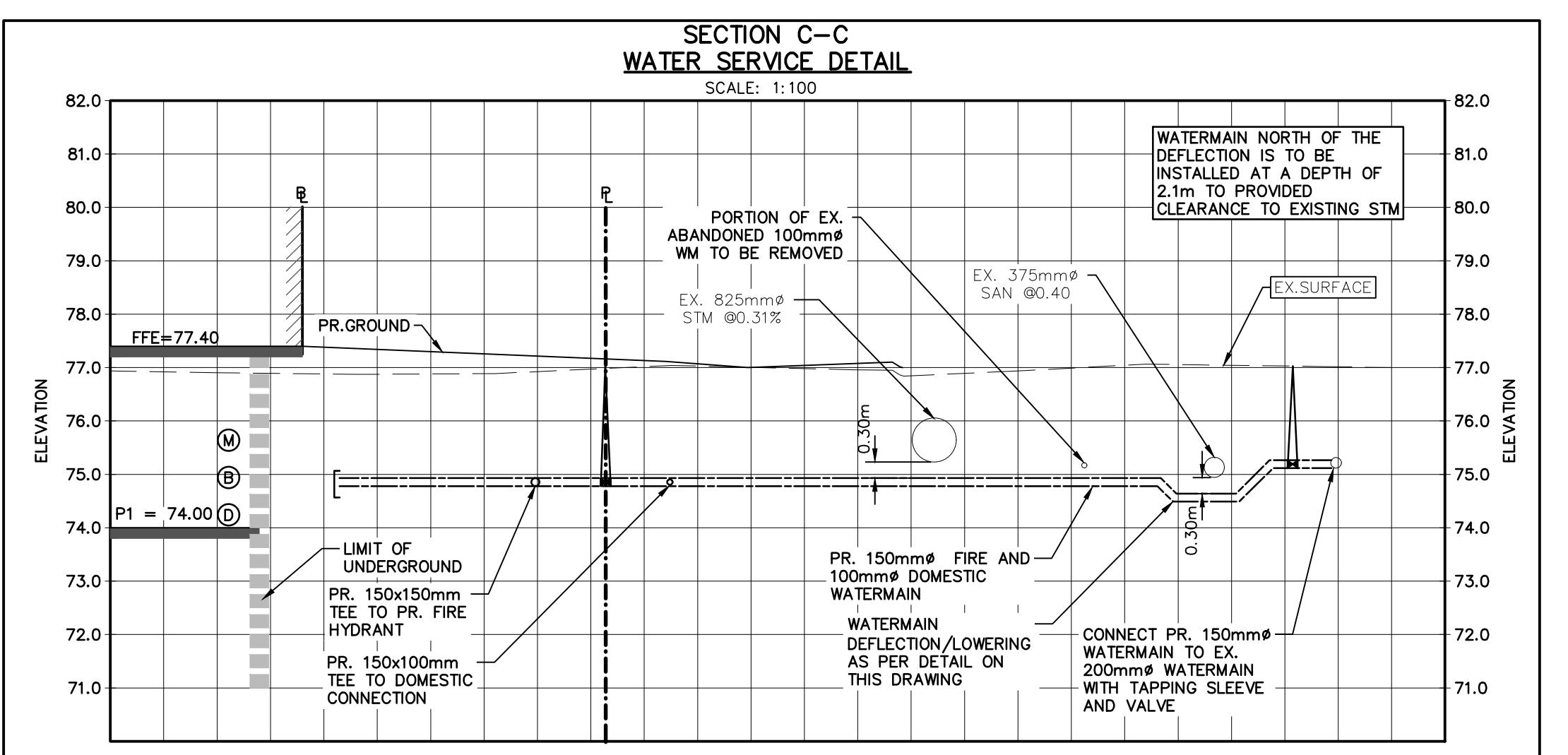
GRADING PLAN

CFCROZIER
CONSULTING ENGINEERS

211 YONGE STREET
SUITE 600
TORONTO, ON, M5B 1M4
416-477-3392 T
WWW.CFCROZIER.CA
INFO@CFCROZIER.CA



2	0m	2	4	6	8
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0 ISSUED FOR FIRST ZBA SUBMISSION 2025/AUG/01					
No. ISSUE / REVISION YYYY/MMM/DD					



Stamp	Stamp
211 YONGE STREET SUITE 600 TORONTO, ON, M5B 1M4 416-477-3392 T INFO@CROZIER.CA	PROVINCE OF ONTARIO J. M. SCOTT 100214964 DEC 12 2025 2025/12/12
Drawn A.A. Design J.P.L. Project No. 2880-7436 Check J.S. Check J.S. Scale 1:100 Dwg. C 104	