## **Environmental Noise Update**

## **69 & 117 John Street**

### **Proposed Residential Development**

City of Mississauga

October 6, 2025 Project: 122-0393

Prepared for

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## **Version History**

Version #	Date	Comments	
1.0	April 19, 2024	Final – Issued to Client	
2.0	October 2, 2024	Final – Issued to Client	
3.0	October 6, 2025	Update – Revised Architectural Drawings	

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## **Environmental Noise Update**

## 69 & 117 John Street

## **Proposed Residential Development**

City of Mississauga

#### **EXECUTIVE SUMMARY**

Valcoustics Canada Ltd. (VCL) previously prepared an Environmental Noise Feasibility Study report dated April 19, 2024 and an Environmental Noise Feasibility Study Update report dated October 2, 2024 for the proposed residential development. This subsequent update has been prepared to address revisions to the architectural drawings.

The project will consist of three (3) towers that are 32, 31 and 24 storeys in height. An eight (8) storey podium with two (2) levels of underground parking will be used to connect the towers.

The main noise source with potential to impact the subject site is rail traffic on CPR Galt Subdivision and GO Transit Milton Line and road traffic on Hurontario Street and Kirwin Avenue.

To meet the applicable transportation noise source guideline limits:

- All residential units in the development require air conditioning to allow windows to remain closed for noise control purposes;
- Brick veneer exterior wall construction or masonry equivalent (STC 54) construction from the foundation to the rafters for the west, north and east facades of the entire development (including Buildings A, B and C), exposed to the railway noise; and
- Upgraded windows are also required:
  - North facade: Up to STC 49; and
  - West and east facades: Up to STC 46.
- Sound barriers are required for the 2<sup>nd</sup>-level patios and the parking rooftop outdoor amenity space on the north sides of the buildings. Additional sound barriers are required for terraces on levels 6 and 7 if the terrace depth is not modified to less than 4 m.

Requirements should be reviewed prior to site plan approval and confirmed when detailed building plans are finalized. This could be done as a condition for obtaining a building permit.

#### 1.0 INTRODUCTION

VCL previously prepared an Environmental Noise Feasibility Study report dated April 19, 2024 and an Environmental Noise Feasibility Study Update report dated October 2, 2024 for the proposed residential development. This subsequent update has been prepared to address revisions to the architectural drawings.

The predicted sound levels and noise mitigation measures needed for the proposed development to comply with noise guidelines of the Ministry of the Environment, Conservation and Parks (MECP) are outlined herein.

#### 1.1 THE SITE AND SURROUNDING AREA

The proposed development is located at 69 & 117 John Street in the City of Mississauga. The site is bounded by:

- CPR Galt Subdivision and GO Transit Milton Line, with existing residential dwellings beyond, to the north;
- Existing residential dwellings to the east;
- John Street, with existing residential dwelling beyond, to the south; and
- Existing storage facility, with existing commercial plaza and Hurontario Street beyond, to the west.

A Key Plan is included as Figure 1.

#### 1.2 THE PROPOSED DEVELOPMENT

The Project will consist of three (3) towers that are 31, 30 and 20 storeys in height, for Buildings A, B and C, respectively. A eight (8) storey podium with two (2) levels of underground parking will be used to connect the towers. The underground parking structure extends beyond the footprint of the podium, towards the rail ROW. The development will also include a safety berm along the north property line. The berm will be approximately 2.5 m in height relative to the rail track elevation.

This report is based on the architectural drawings prepared by Tregebov Cogan Architect, latest revised September 17, 2025 ("For Review"). Figures 2 to 6 show the site plan, ground floor plan, 2<sup>nd</sup> floor plan and 7<sup>th</sup> floor plan from the drawings respectively. Additional relevant plans from the drawings are included in Appendix A.

#### 2.0 NOISE SOURCES

#### 2.1 TRANSPORTATION SOURCES

The noise source with potential to impact the proposed development is rail traffic on CPR Galt Subdivision and GO Transit Milton Line and road traffic on Hurontario Street and Kirwin Avenue. The traffic data is shown in Appendix B.

The planned future rail traffic data for the GO Transit Milton Line was obtained from Metrolinx on October 2, 2025.

The data indicates that GO rail service on this subdivision will be comprised of diesel trains. There are no anti-whistling by-laws in affect near the subject site.

Note, as of November 2020, CPR is no longer supplying rail traffic data. This project is using the CPR rail data dated April 12, 2018 from our previous projects, and escalated to the Year 2035 design condition using the 2.5% annual growth rate.

The rail traffic data is summarized in Table 1A.

TADI	<b>E</b> 1 A	DAII	TRAFFIC	DATA
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Railway	Time Period	Volume	# Cars per Train	# Locos per Train	Speed (km/hr)
Milton GO Line (1)	Day (0700-2300)	20	10	1	105
	Night (2300-0700)	2	10		
CD Calt Subdivision (2)	Day (0700-2300)	9 (13.7)	151	4	90
CP Galt Subdivision (2)	Night (2300-0700)	8 (12.2)	131	4	80

#### Notes:

- (1) The future planned rail traffic data was provided by Metrolinx/GO Transit on October 2, 2025.
- (2) Obtained from CPR for the year 2018. Data shown in brackets was projected to the year 2035 design condition at a 2.5% growth rate, compounded annually. The data provided shows the maximum number of train cars and locomotives.

Ultimate (2041) road traffic data for Hurontario Street and Kirwin Avenue were obtained from the City of Mississauga on October 11, 2022. The traffic data indicates a proposed LRT line along Hurontario Street, and existing lanes may be converted from 6 lanes to 4 lanes with 2 LRT lines in the middle. Currently, traffic data and a timeline for the proposed LRT line is not available and thus was not included in the analysis. The road traffic data is summarized in Table 1B.

TABLE 1B ROAD TRAFFIC DATA

Bood	24-Hour Volume <sup>(1)</sup>	Day/Night Split (%)	Trucks (%)		Speed (km/hr)
Road	24-nour volume Day/Night Split (%)	Medium	Heavy		
Hurontario Street	53 200	90/10	2.2	1.8	50
Kirwin Avenue	12 500	90/10	1.1	0.9	50

#### Note:

(1) Ultimate traffic data (2041) obtained from the City of Mississauga.

#### 2.2 STATIONARY SOURCES

Based on a visit to the area by VCL staff on November 23, 2022, there are no stationary sources in the vicinity with the potential to significantly impact the subject site and therefore noise impact from stationary noise sources is not considered further in this report.

#### 3.0 ENVIRONMENTAL NOISE GUIDELINES

#### 3.1 MECP NPC-300 - TRANSPORTATION SOURCES

The applicable noise guidelines for new residential development are those in MECP Publication NPC-300, "Environmental Noise Guideline, Stationary, and Transportation Sources – Approval and Planning".

The environmental noise guidelines of the MECP, as provided in Publication NPC-300, are discussed briefly below and summarized in Appendix A.

#### 3.1.1 Architectural Elements

In the daytime, the indoor criterion for road noise is  $L_{eq\ Day}^{(1)}$  of 45 dBA for sensitive spaces such as living/dining rooms, dens and bedrooms. At night, the indoor criterion for road noise is  $L_{eq\ Night}^{(2)}$  of 45 dBA for sensitive spaces such as living/dining rooms and dens and 40 dBA for bedrooms. The indoor criteria for rail noise are 5 dBA more stringent (i.e. lower) than those for the road; that is 40 dBA for living/dining rooms, dens and bedrooms during the daytime and nighttime periods except for bedrooms where the nighttime indoor criterion is 35 dBA.

The architectural design of the building envelope (walls, windows, etc.) must provide adequate sound isolation to achieve these indoor sound level limits, based on the applicable outdoor sound level on the facades.

In addition, the MECP requires brick veneer exterior wall construction or masonry equivalent construction from the foundation to the rafters for the first row of dwellings provided they are within 100 m of the rail line and the  $L_{eq\,24}$  is greater than 60 dBA.

#### 3.1.2 Ventilation

In accordance with the MECP noise guideline for road traffic sources, if the daytime sound level,  $L_{\text{eq Day}}$ , at the exterior face of a noise sensitive window is greater than 65 dBA, means must be provided so that windows can be kept closed for noise control purposes and central air conditioning is required. For daytime sound levels between 56 dBA and 65 dBA inclusive, there need only be the provision for adding air conditioning at a later date. A warning clause advising the occupant of the potential interference with some activities is also required. At nighttime, air conditioning would be required when the sound level exceeds 60 dBA ( $L_{\text{eq Night}}$ ) at a noise sensitive window (provision for adding air conditioning is required when greater than 50 dBA).

- (1) 16-hour energy equivalent sound level (0700-2300 hours).
- (2) 8-hour energy equivalent sound level (2300-0700 hours).

#### 3.1.3 Outdoors

For outdoor amenity areas ("Outdoor Living Areas" - OLAs), the guideline is  $L_{eq}$  of 55 dBA, with an excess not exceeding 5 dBA considered acceptable if it is technically not practicable to achieve the 55 dBA objective, providing warning clauses are registered on title.

Note, a balcony or elevated terrace is not considered an OLA, unless it is:

- the only OLA for the occupant;
- at least 4 m in depth; and
- unenclosed.

## 3.2 FEDERATION OF CANADIAN MUNICIPALITIES (FCM) AND RAILWAY ASSOCIATION OF CANADA (RAC)

The standard noise mitigation measures recommended jointly by the Federation of Canadian Municipalities and the Railway Association of Canada (FCM/RAC) in the guidelines of Reference 5 are:

- a minimum setback of 30 m from the edge of the railway right-of-way to the closest dwelling facade:
- a safety berm at least 2.5 m above grade at the property line;
- an approximately 3.0 m high acoustic fence atop the safety berm (to achieve a total height of 5.5 m above the top of the rail);
- upgraded exterior wall construction (such as brick veneer), where needed; and
- warning clauses specific to the railway for all dwellings within 300 m of the right-of-way.

Aside from the "standard" requirements regarding the setback of dwellings and safety berm/sound barrier configuration, the sound level design objectives of the FCM/RAC guidelines are similar to those of the MECP. See Appendix A. The FCM/RAC guidelines also permit modifications to their standard requirements where substantiated by a detailed noise impact assessment.

#### 4.0 NOISE IMPACT ASSESSMENT

#### 4.1 ANALYSIS METHOD

Using the rail and road traffic data in Tables 1A and 1B, the sound levels, in terms of  $L_{\text{eq Day}}$  and  $L_{\text{eq Night}}$ , were determined using STAMSON V5.04 – ORNAMENT/STEAM, the computerized road/rail traffic noise prediction models of the MECP.

The receptor locations used in the noise assessment are shown in Figures 2 to 6.

The worst-case facade receptors were assessed at the heights corresponding to windows on the highest floors for the Buildings.

The daytime sound levels at the grade-level private patios were assessed at a height of 1.5 m above grade, at the centre of each outdoor amenity area, in accordance with the NPC-300 requirements.

The daytime sound levels at elevated terraces were assessed at a height of 1.5 m above each terrace elevation, at the centre of the amenity space.

Inherent acoustical screening due to the orientation of the buildings relative to the noise sources was included in the assessment. Screening from off-site buildings was not included for the facade sound level calculations. However, screening from the safety berm and the off-site buildings was included for the OLA calculations.

#### 4.2 SOUND LEVEL PREDICTION

Table 2 summarises the predicted sound levels outdoors at the receptor locations.

The highest daytime/nighttime unmitigated sound levels of 72 dBA/74 dBA are predicted to occur at the north facade of Building A.

The highest daytime OLA sound level of 71 dBA is predicted to occur at the 6<sup>th</sup> and 7<sup>th</sup> floor terraces on north sides of the buildings.

Sample sound level calculation is included in Appendix D.

TABLE 2 PREDICTED SOUND LEVELS – TRANSPORTATION SOURCES

Location	Source Distance (m) <sup>(1)</sup>		L <sub>eq Day</sub> (dBA)	L <sub>eq Night</sub> (dBA)
A <sup>(2)</sup>	Milton GO Line/CP Galt Subdivision	43	72	74
Building A Northwest Corner	Hurontario Street	233	56	49
(North Facade)	TOTAL	-	72	74
A <sup>(2)</sup>	Milton GO Line/CP Galt Subdivision	43	69	71
Building A Northwest Corner	Hurontario Street	233	59	52
(West Facade)	TOTAL	-	69	71
	Milton GO Line/CP Galt Subdivision	81	66	68
B <sup>(2)</sup> Building A	Hurontario Street	231	59	52
Southwest Corner (West Facade)	Kirwin Avenue	145	50	43
	TOTAL	-	67	68

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TABLE 2 PREDICTED SOUND LEVELS – TRANSPORTATION SOURCES (continued)

Location	Source	Distance (m) <sup>(1)</sup>	L <sub>eq Day</sub> (dBA)	L <sub>eq Night</sub> (dBA)
B <sup>(2)</sup>	Hurontario Street	231	56	49
Building A Southwest Corner (South Facade)	Kirwin Avenue	145	53	46
(Sodil 1 acade)	TOTAL	_	58	51
C <sup>(2)</sup> Buildings B & C 8-storey Podium Amenity Terrace (OLA)	Milton GO Line/CP Galt Subdivision	60	59	-
D <sup>(3)</sup> Building A Outdoor Amenity on Grade (OLA)	Milton GO Line/CP Galt Subdivision	47	49	_
E <sup>(3)</sup> Building A West Side Ground Patio (OLA)	Milton GO Line/CP Galt Subdivision	69	49	_
F <sup>(3)</sup> Building C Outdoor Amenity on Grade (OLA)	Milton GO Line/CP Galt Subdivision	49	54	_
G <sup>(3)</sup> Building C North Side Ground Patio (OLA)	Milton GO Line/CP Galt Subdivision	74	55	_
H <sup>(4)</sup> Building A North Side Level 2 Patio (OLA)	Milton GO Line/CP Galt Subdivision	41	63	-
I <sup>(4)</sup> Building A Outdoor Amenity Parking Rooftop (OLA)	Milton GO Line/CP Galt Subdivision	39	63	-
J <sup>(5)</sup> Building B-C North Side Level 6 Terrace (OLA)	Milton GO Line/CP Galt Subdivision	51	71	_

.../cont'd

#### TABLE 2 PREDICTED SOUND LEVELS – TRANSPORTATION SOURCES (continued)

K <sup>(6)</sup> Building A West Side Level 7 Terrace (OLA)	Milton GO Line/CP Galt Subdivision	68	67	-
L <sup>(6)</sup> Building C North Side Level 7 Terrace (OLA)	Milton GO Line/CP Galt Subdivision	53	71	

#### Notes:

- (1) Distance is from the centreline of the roadway/railway.
- (2) Locations A to C are shown on Figure 2.
- (3) Locations D to G are shown on Figure 3.
- (4) Locations H and I are shown on Figure 4.
- (5) Location J is shown on Figure 5.
- (6) Locations K and L is shown on Figure 6.

#### 4.3 NOISE CONTROL MEASURES

The noise control measures can generally be classified into two categories which are interrelated, but which can be treated separately for the most part:

- a) Architectural elements to achieve acceptable indoor noise guidelines for transportation sources; and
- b) Design features to protect the OLAs.

Noise abatement requirements are summarised in Table 3 and notes to Table 3.

#### 4.3.1 Indoors

#### 4.3.1.1 Exterior Wall and Window Construction

Floor plans showing the suite layouts have not yet been developed. The STC requirements were therefore calculated assuming exterior walls and windows to have surface areas equalling 20% and 80% of the associated floor area, respectively, on the facade of a top-floor bedroom (worst case) exposed directly to or at an angle to the road or rail traffic noise sources.

Our analysis indicates that exterior wall construction meeting STC 54 (e.g., brick veneer) or higher is required. Moreover, the MECP/FCM requires brick veneer exterior wall construction or masonry equivalent construction for the first row of dwellings (i.e. all the development including proposed Buildings A, B and C) as they are within 100 m of the rail line and the  $L_{eq 24}$  is greater than 60 dBA.

Upgraded windows are also required:

- North facade: Up to STC 49; and
- West and east facades: Up to STC 46.

For south facade, the analysis shows that exterior wall and window construction meeting the minimum non-acoustical requirements of the Ontario Building Code will be sufficient to meet the indoor noise criteria.

Note, the required window STC ratings can be up to 3 points higher at corner locations if windows are provided on both facades.

The window STC requirements outlined above are quite stringent and may be reduced through proper space design. Consideration should be given to:

- Reducing the size of the windows or ensuring that the exterior window area is small relative to the floor area of the associated space.
- Designing the spaces so that the rooms at the corners of the building have windows on only one facade.
- Having non-noise sensitive spaces, such as walk-in closets or washrooms, at the corners of the building.
- Upgrade the exterior wall construction to have an STC rating greater than STC 54.

Note, the window frames themselves must also be designed to ensure that the overall sound isolation performance for the entire window assembly meets the sound isolation requirement. This must be confirmed by the window manufacturer through the submission of acoustical test data.

The assessment should be updated, and the sound isolation requirements confirmed once more detailed plans, suite layout drawings and elevation drawings become available.

#### 4.3.1.2 Ventilation Requirements

All dwelling units in the development require central air conditioning to allow windows to be closed for noise control purposes.

#### 4.3.2 Outdoors

The unmitigated daytime OLA sound levels at the Level 2 patios and the parking rooftop outdoor amenity space on the north side of the buildings, as well as the Level 6 and Level 7 roof terraces, are predicted to exceed the 60 dBA upper limit of the MECP noise guidelines. Therefore, sound barriers are typically required.

To reduce the OLA sound levels to 60 dBA, following sound barriers would be required:

- For Level 2 patios and the parking rooftop outdoor amenity space on the north side of the buildings, a 1.8 m high sound barrier is required along the perimeter of the proposed underground parking structure. The location of the sound barrier is shown on Figures 2 and 4.
- For two of the Level 6 roof terraces on the north side of the podium, each requires a minimum 2.3 m high sound barrier. The locations of the sound barriers are shown on Figure 5.
- For Level 7 roof terrace on the west side of Building A, a minimum 1.7 m high sound barrier is required. The location of the sound barrier is shown on Figure 6.
- For Level 7 roof terrace on the north side of Building C, a minimum 2.2 m high sound barrier is required. The location of the sound barrier is shown on Figure 6.

Alternatively, if the elevated terraces on Level 6 and Level 7 can be re-designed to have depths less than 4 m, they would not be considered as OLA's and noise mitigation would not be required. Note that there are common amenity areas on the building rooftops meeting the MECP noise guidelines and thus, these elevated terraces are not the only OLAs provided for the units. Permanent planters are often used when terrace depths need to be reduced by a small amount.

The unmitigated daytime OLA sound levels at all other OLAs are all below the 60 dBA upper limit of the MECP noise guidelines. Therefore, sound barriers are not required for these OLAs. Note that there are a number of common OLA areas with sound levels well below 55 dBA where occupants can pursue quiet outdoor enjoyment. Therefore, it is acceptable to exercise the 60 dBA upper limit for some OLAs.

The sound barriers must be of solid construction with no gaps, cracks or holes (except for small openings required for water drainage) and must have a minimum surface weight of 20 kg/m². A variety of materials may be used, including concrete, masonry, glass, wood, specialty composite materials, or a combination of these.

Sound barrier requirements should be reviewed once grading plans and cross-sections are finalized.

In addition to the sound barrier requirements, a safety berm/crash wall has been provided along the rail right-of-way. Note that rail safety is outside the purview of our expertise and safety berm/crash wall design is not within the scope of the noise study.

#### 4.3.3 Warning clauses

Warning clauses are a tool to inform prospective owners/occupants of potential annoyance due to existing noise sources. Where the guideline sound level limits are exceeded, appropriate warning clauses should be registered on title or included in the development agreement that is registered on title. The warning clauses should also be included in agreements of Offers of

Purchase and Sale and lease/rental agreements to make future occupants aware of the potential noise situation.

Table 3 and the notes to Table 3 summarize the warning clauses for the site.

TABLE 3 MINIMUM NOISE ABATEMENT MEASURES

Location	Air Conditioning <sup>(1)</sup>	Exterior Wall <sup>(2)</sup>	Window STC Rating <sup>(2)</sup>	Sound Barrier <sup>(3)</sup>	Warning Clauses <sup>(4)</sup>
Units along north facade of development including Buildings A, B and C	Mandatory	brick veneer or masonry equivalent (STC 54)	STC 49	See Section 4.3.2	A + B + C
Units along west and east facades of development including Buildings A, B and C	Mandatory	brick veneer or masonry equivalent (STC 54)	STC 46	See Section 4.3.2	A + B + C
Units along south facade of development including Buildings A, B and C	Mandatory	No specifical acoustical requirement		A + B + C	

#### Notes:

- (1) Where methods must be provided to allow windows to remain closed for noise control purposes, a commonly used technique for is the use of air conditioning. Provision for adding air conditioning typically takes the form of a ducted ventilation system suitably sized to permit the addition of central air conditioning by the occupant.
- (2) STC Sound Transmission Class Rating (Reference ASTM-E413). Analyses were based upon the assumption that wall and window areas are as indicated in Section 4.3.1.1 of this report. Requirements should be checked once floor plans have been finalized and exterior wall construction details are defined.
- (3) Sound barriers must be of solid construction with no gaps, cracks, or holes, and must meet a minimum surface density of 20 kg/m². Suitable material can include wood, concrete metal sandwich panel, glazing or a combination of these.
- (4) The warning clauses to be registered on title and be included in Offers of Purchase and Sale for designated lots:
  - A. "Purchasers/tenants are advised that despite the inclusion of noise control features in the development and within the building units, sound levels due to increasing road and rail traffic may on occasions interfere with some activities of the dwelling occupants as the sound levels exceed the sound level limits of the Municipality and the Ministry of the Environment, Conservation and Parks."
  - B. "This dwelling has been supplied with a central air conditioning system which will allow windows and exterior doors to remain closed, thereby ensuring that the indoor sound levels are within the noise criteria of the municipality and the Ministry of the Environment."
  - C. "Purchasers/occupants are advised Canadian Pacific Limited (CP)/Metrolinx or its affiliated railway companies has or have a railway right-of-way within 300 m from this dwelling unit. There may be alterations to or expansions of the railway facilities of such right-of-way in the future, including the possibility that CP/Metrolinx or its affiliated railway companies as aforesaid, or their assigns or successors may expand their business operations. Such expansion may affect the living and business environment of the residents, tenants and their visitors, employees, customers and patients in the vicinity, notwithstanding the inclusion of any noise and vibration attenuating features in the design of the development. CP/Metrolinx, its affiliated railway companies and their successors and assigns will not be responsible or any complaints or claims arising from use of such facilities and/or operations on, over or under the aforesaid right of-way."
- (5) All exterior doors shall be fully weather-stripped.

#### 5.0 THE EFFECT OF THE PROJECT ON THE NEIGHBOURHOOD

The main source of noise associated with this development, with the potential for significant impact on surrounding buildings, is the mechanical equipment.

Mechanical equipment interfacing to the outdoors must comply with the MECP noise guideline limits in NPC-300. By proper engineering design, all requirements can be met, and no significant noise impact would be created for surrounding uses. Appropriate choice of location, equipment type, and noise control features should be considered during detailed design for such items as rooftop equipment and air intakes and exhausts, including underground parking garage ventilation systems. The noise emissions from parking garage air shafts located immediately adjacent to residential uses can be designed to comply with the noise guideline limits by acoustically lining the shaft and/or providing silencers.

For any emergency generators, appropriate steps should be taken to ensure that the equipment placement, treatment, and the routine testing schedule will not generate significant noise impact on neighbouring properties. The generator will require silencers on the intake and exhaust cooling air paths, as well as a muffler on the combustion exhaust.

The additional road traffic generated by this project will be small relative to existing traffic volumes within the general area and is not expected to create significant additional noise impact.

The noise impact of the project on the neighbourhood should be reviewed as design progresses and mechanical details are known. This typically occurs prior to the issuance of building permit.

#### 6.0 CONCLUSIONS

With the incorporation of the recommended noise mitigation measures, the indoor and outdoor transportation noise guidelines can be met. Future occupants will be made aware of potential noise situation through warning clauses, as per MECP guidelines.

The approvals and administrative procedures are available to ensure that the noise requirements are implemented.

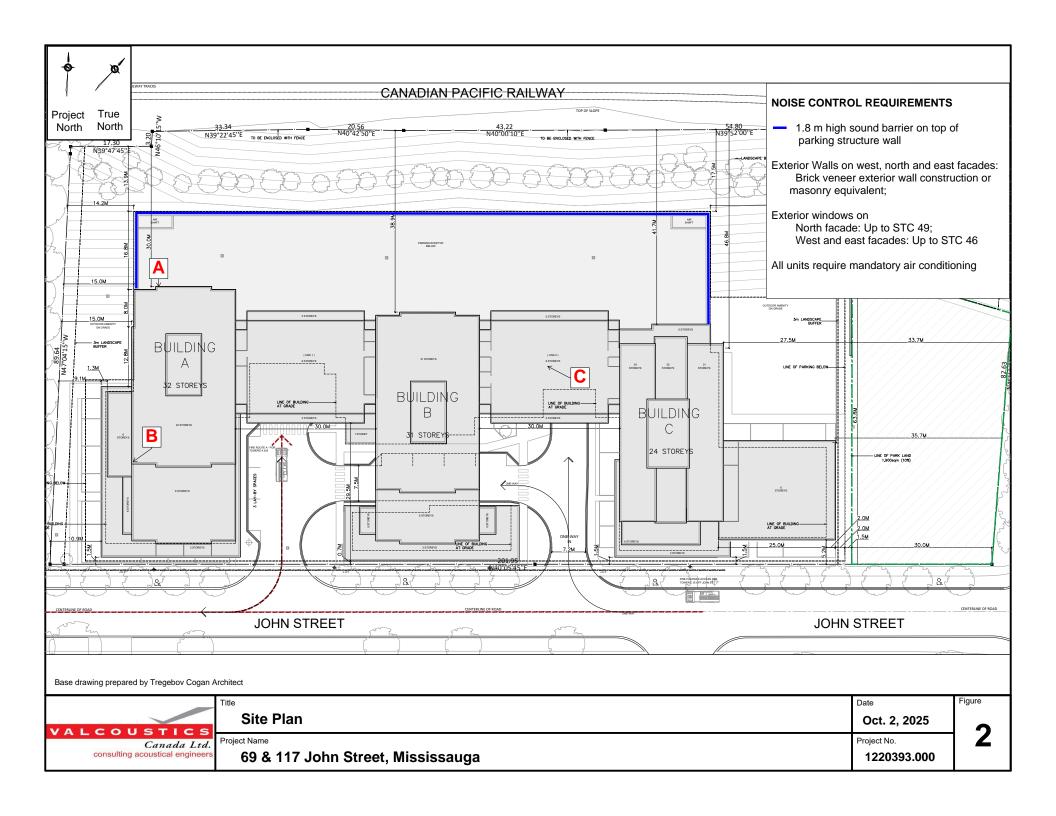
#### 7.0 REFERENCES

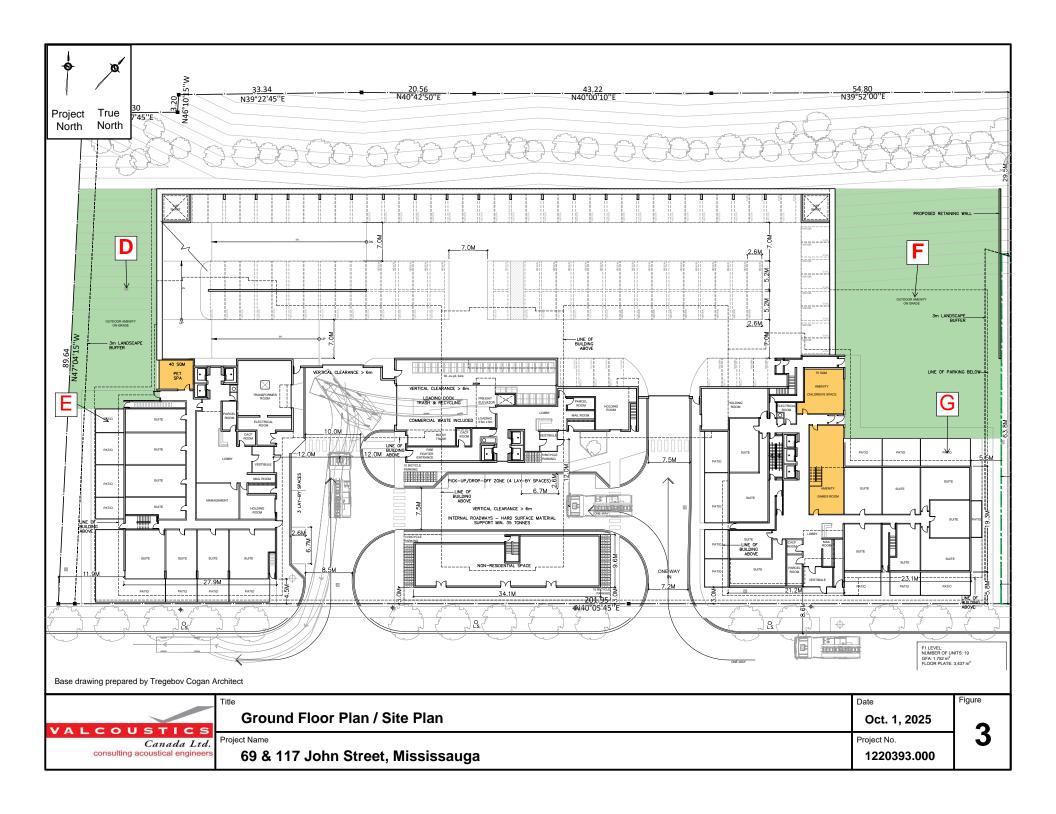
- 1. PC STAMSON 5.04, "Computer Program for Road Traffic Noise Assessment", Ontario Ministry of the Environment.
- 2. Building Practice Note No. 56: "Controlling Sound Transmission into Buildings", by J. D. Quirt, Division of Building Research, National Council of Canada, September 1985.
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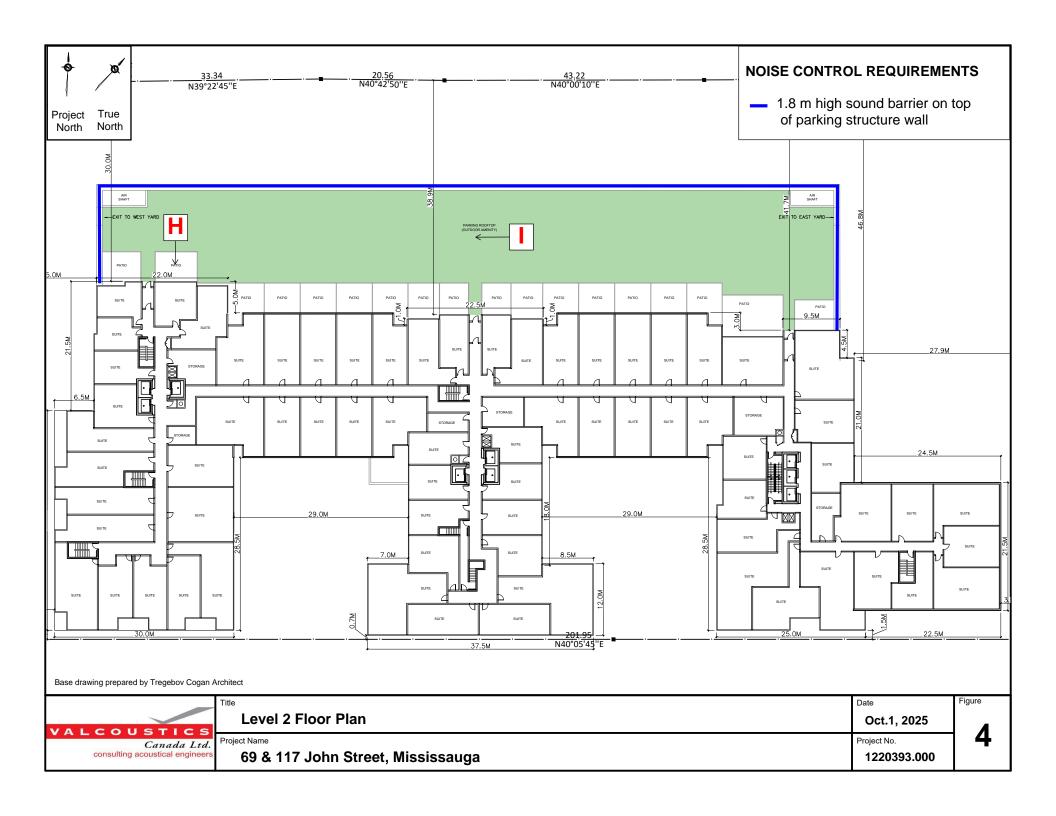
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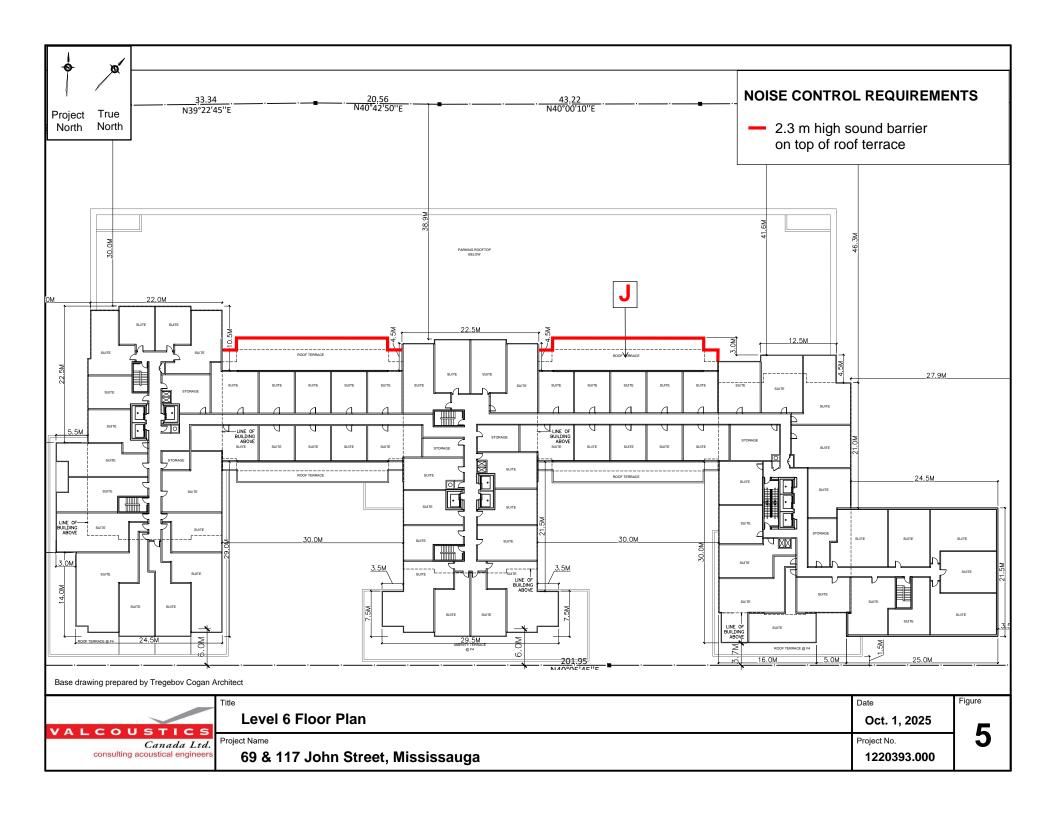
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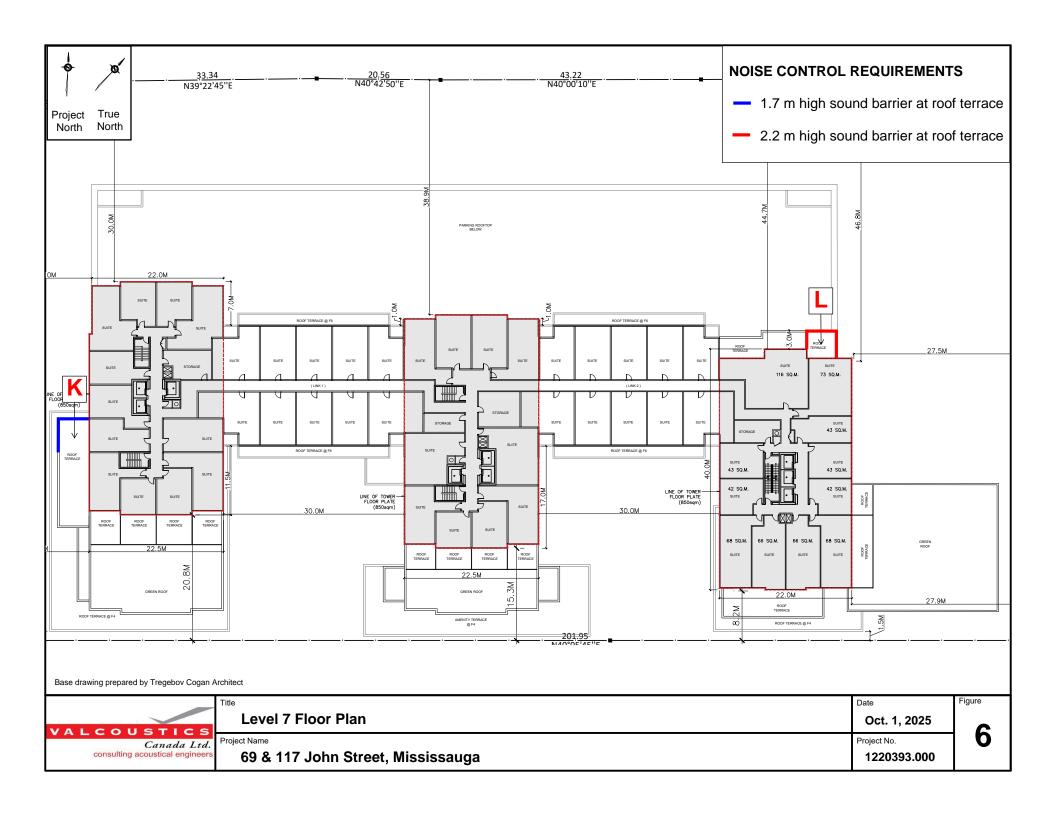




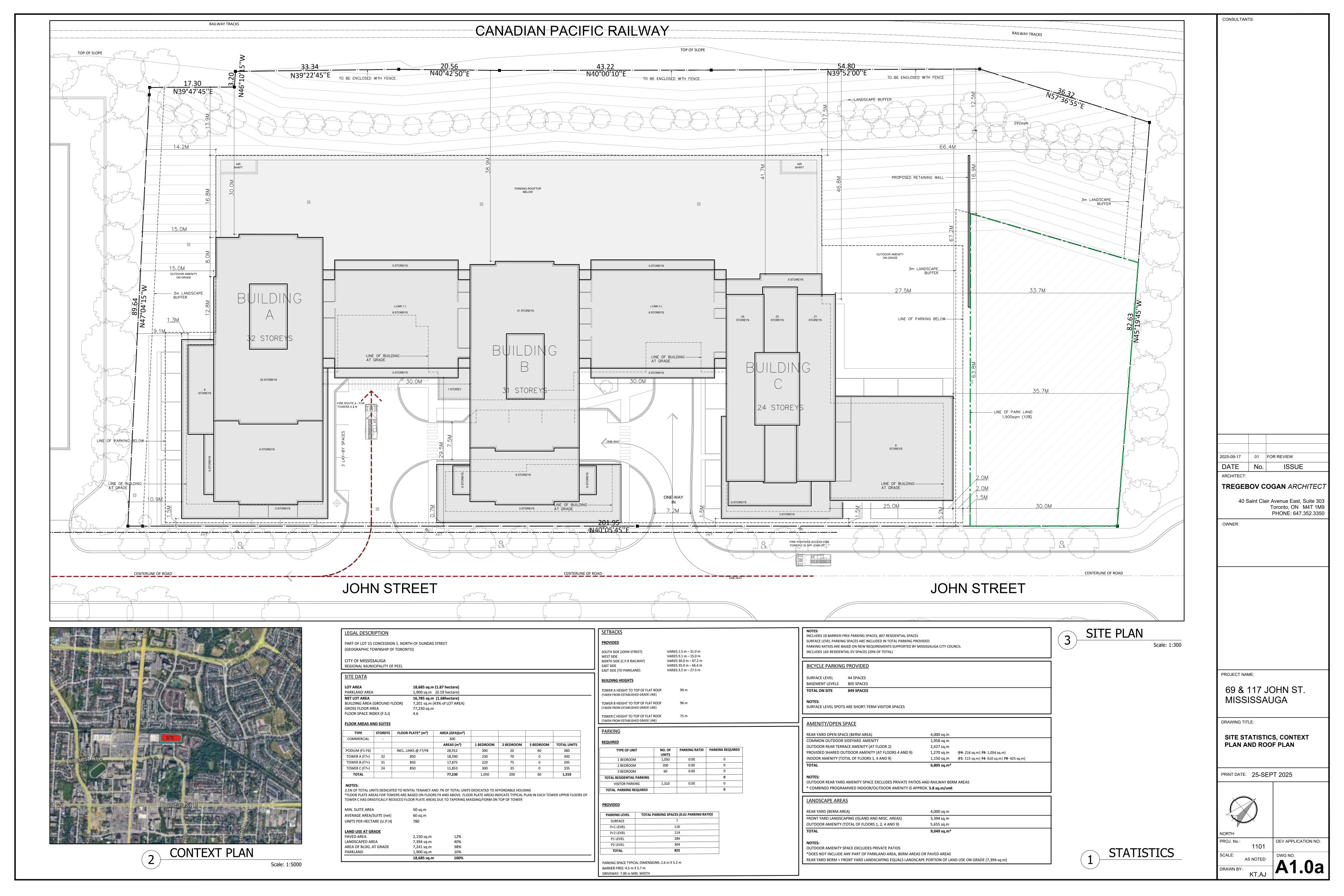


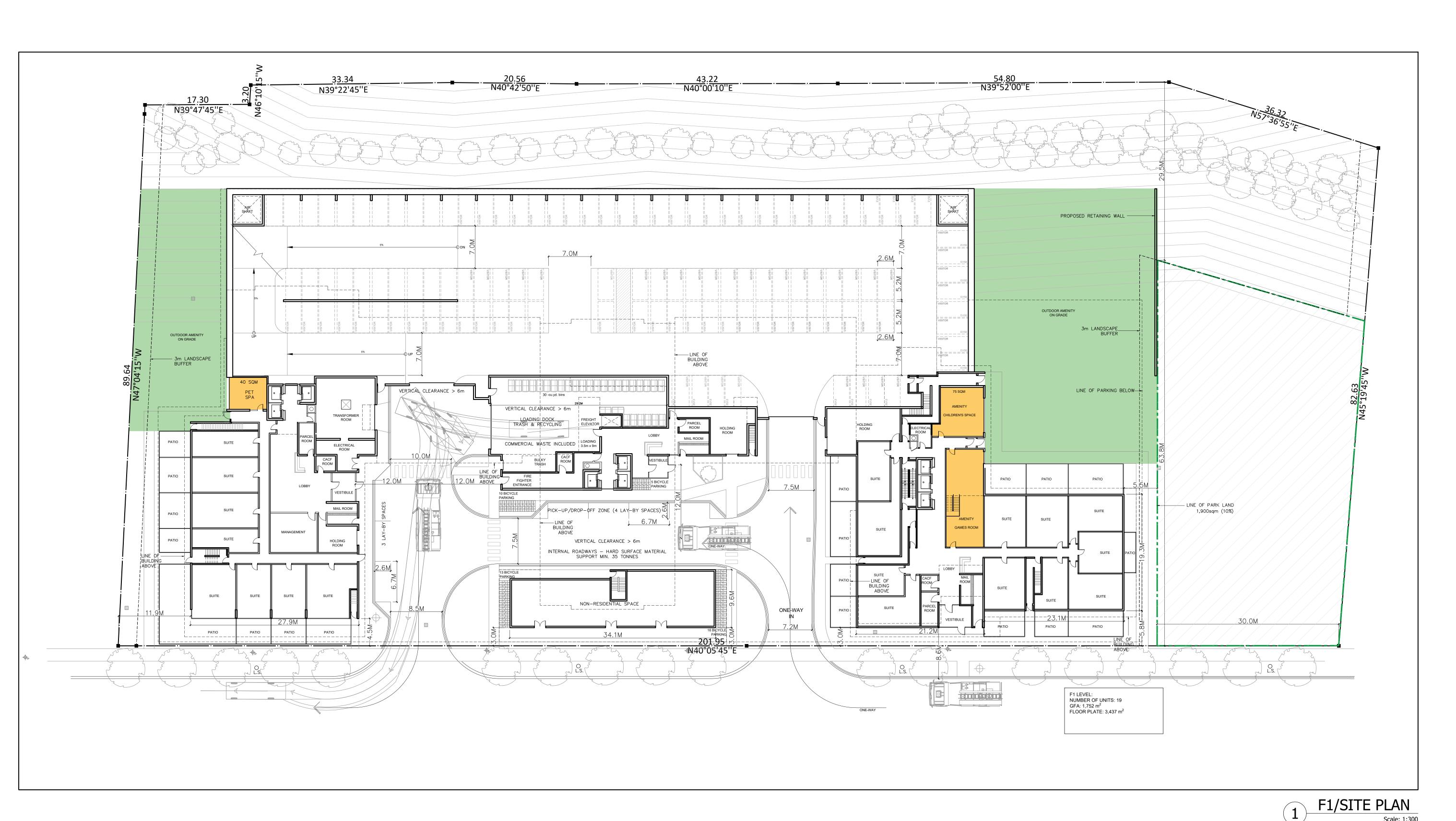






# APPENDIX A ARCHITECTURAL PLANS





40 Saint Clair Avenue East, Suite 303 Toronto, ON M4T 1M9 PHONE: 647.352.3350

OWNER:

CONSULTANTS:

PROJECT NAME:

69 & 117 JOHN ST. MISSISSAUGA

DRAWING TITLE:

F1/SITE PLAN

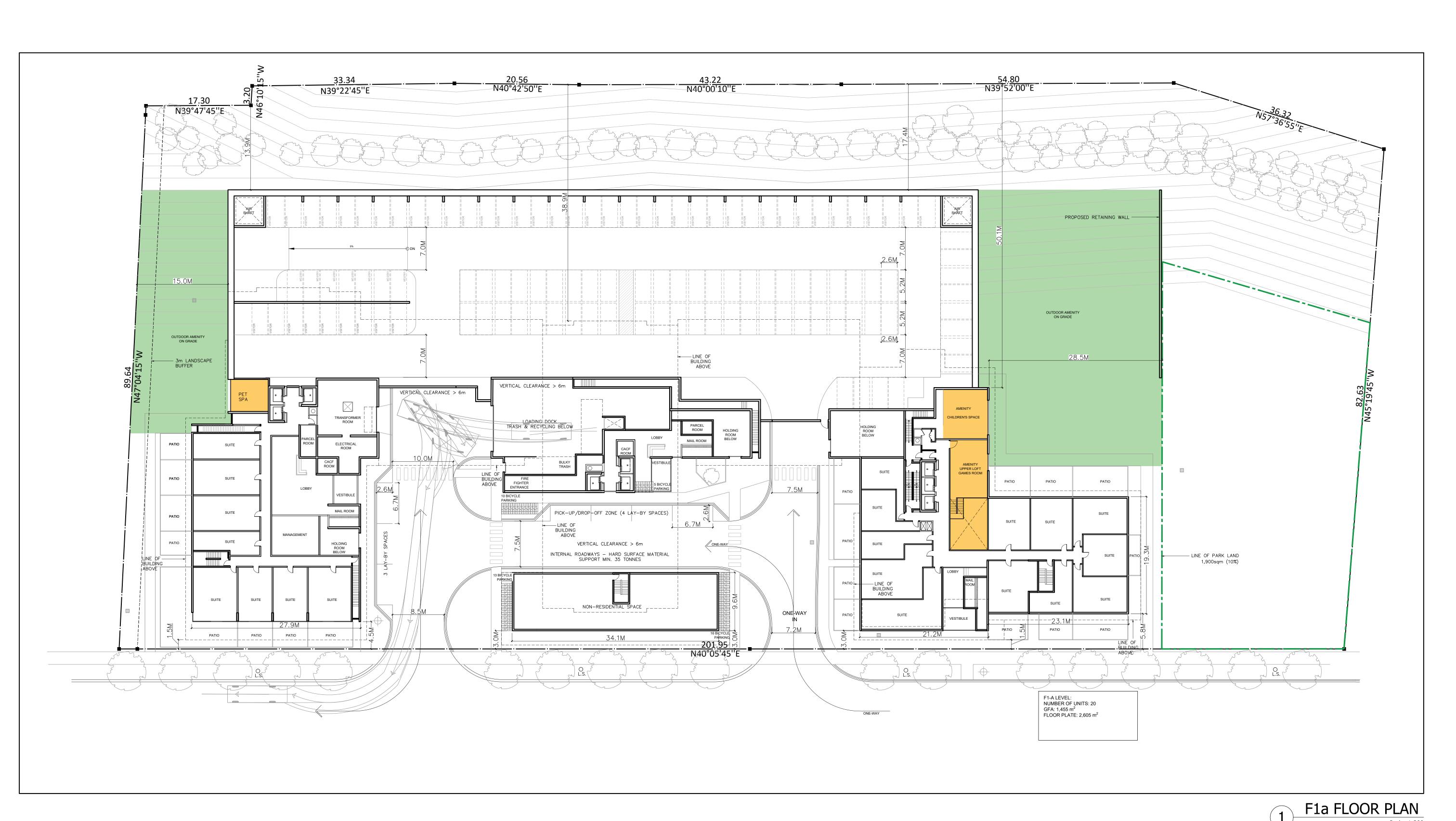
PRINT DATE: 25-SEPT 2025

NORTH
PROJ. No.:
1101
SCALE:
AS NOTED
DRAWN BY:

AS NOTED DWG NO.

KT,AJ

DEV APPLICATION NO:



40 Saint Clair Avenue East, Suite 303 Toronto, ON M4T 1M9 PHONE: 647.352.3350

OWNER:

CONSULTANTS:

PROJECT NAME:

69 & 117 JOHN ST. MISSISSAUGA

DRAWING TITLE:

PRINT DATE: 25-SEPT 2025

F1a FLOOR PLAN

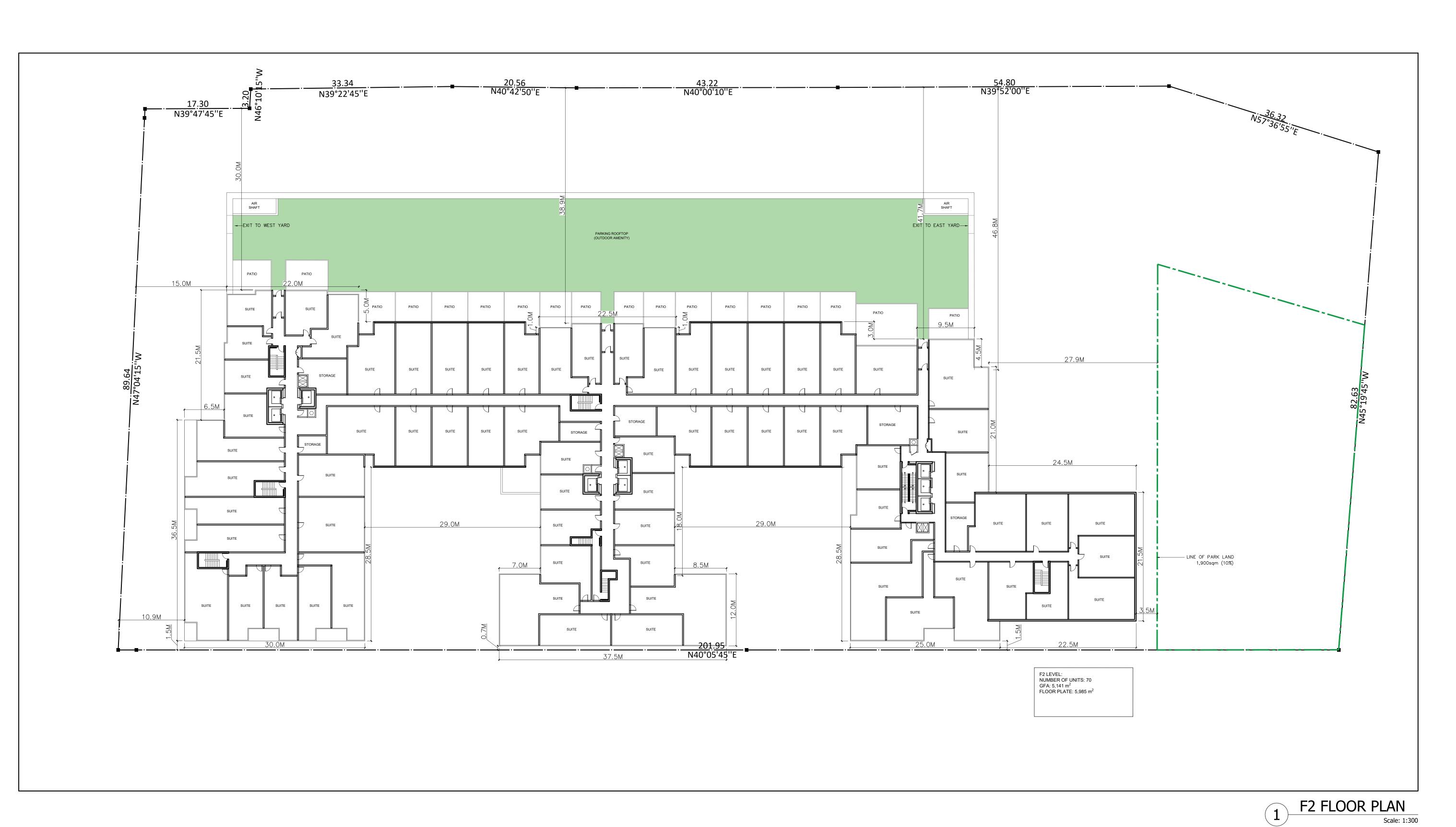
DRAWN BY:

NORTH
PROJ. No.:
1101
SCALE:
AS NOTED

AS NOTED DWG NO.

KT,AJ

DEV APPLICATION NO:



40 Saint Clair Avenue East, Suite 303 Toronto, ON M4T 1M9 PHONE: 647.352.3350

OWNER:

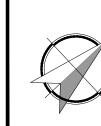
CONSULTANTS:

PROJECT NAME:

69 & 117 JOHN ST. MISSISSAUGA

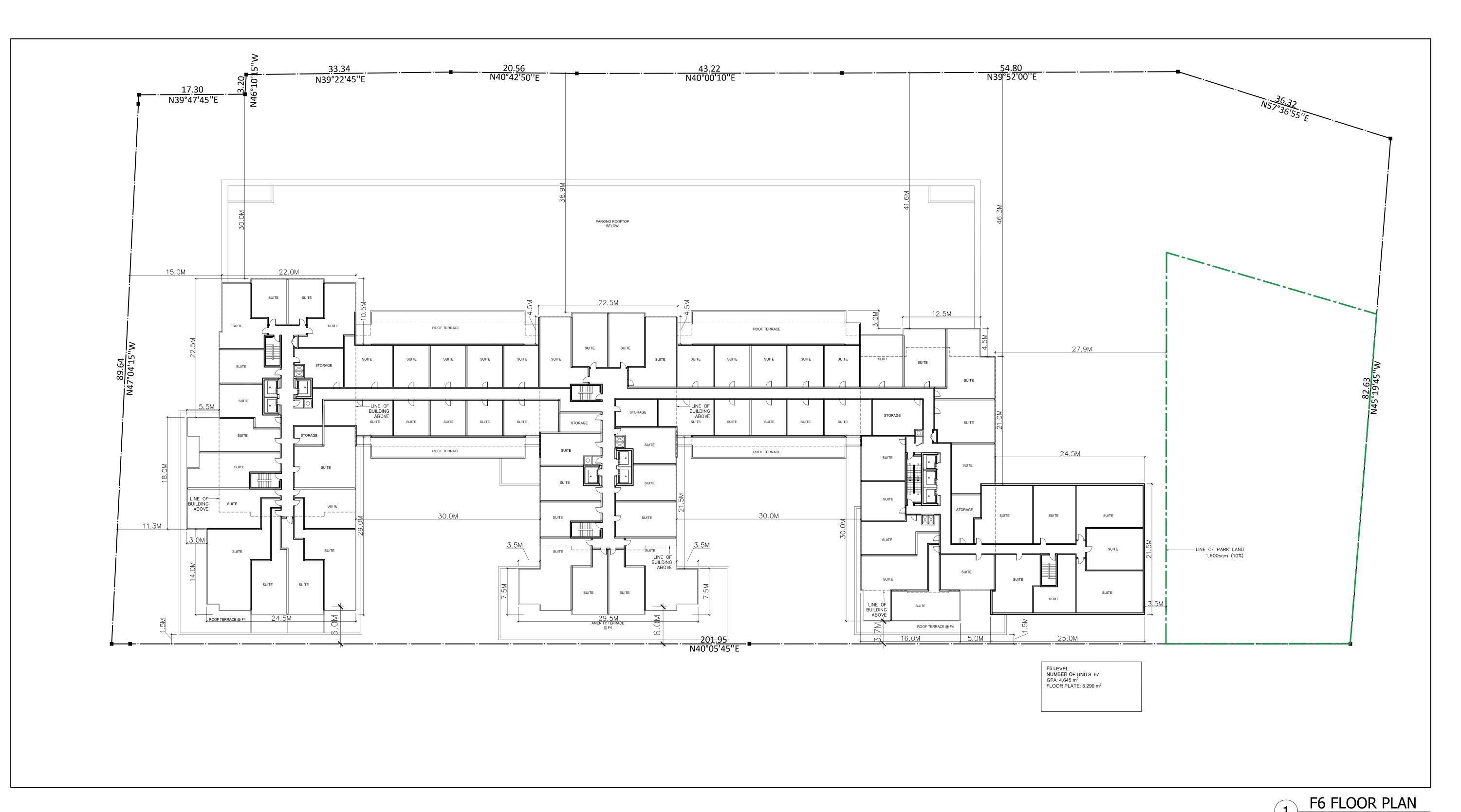
DRAWING TITLE: **F2 FLOOR PLAN** 

PRINT DATE: 25-SEPT 2025



PROJ. No.: DEV APPLICATION NO: 1101 SCALE: DRAWN BY:

KT,AJ



DATE No. ISSUE

ARCHITECT: TREGEBOV COGAN ARCHITECT

40 Saint Clair Avenue East, Suite 303 Toronto, ON M4T 1M9 PHONE: 647.352.3350

OWNER:

CONSULTANTS:

PROJECT NAME:

69 & 117 JOHN ST. MISSISSAUGA

DRAWING TITLE:

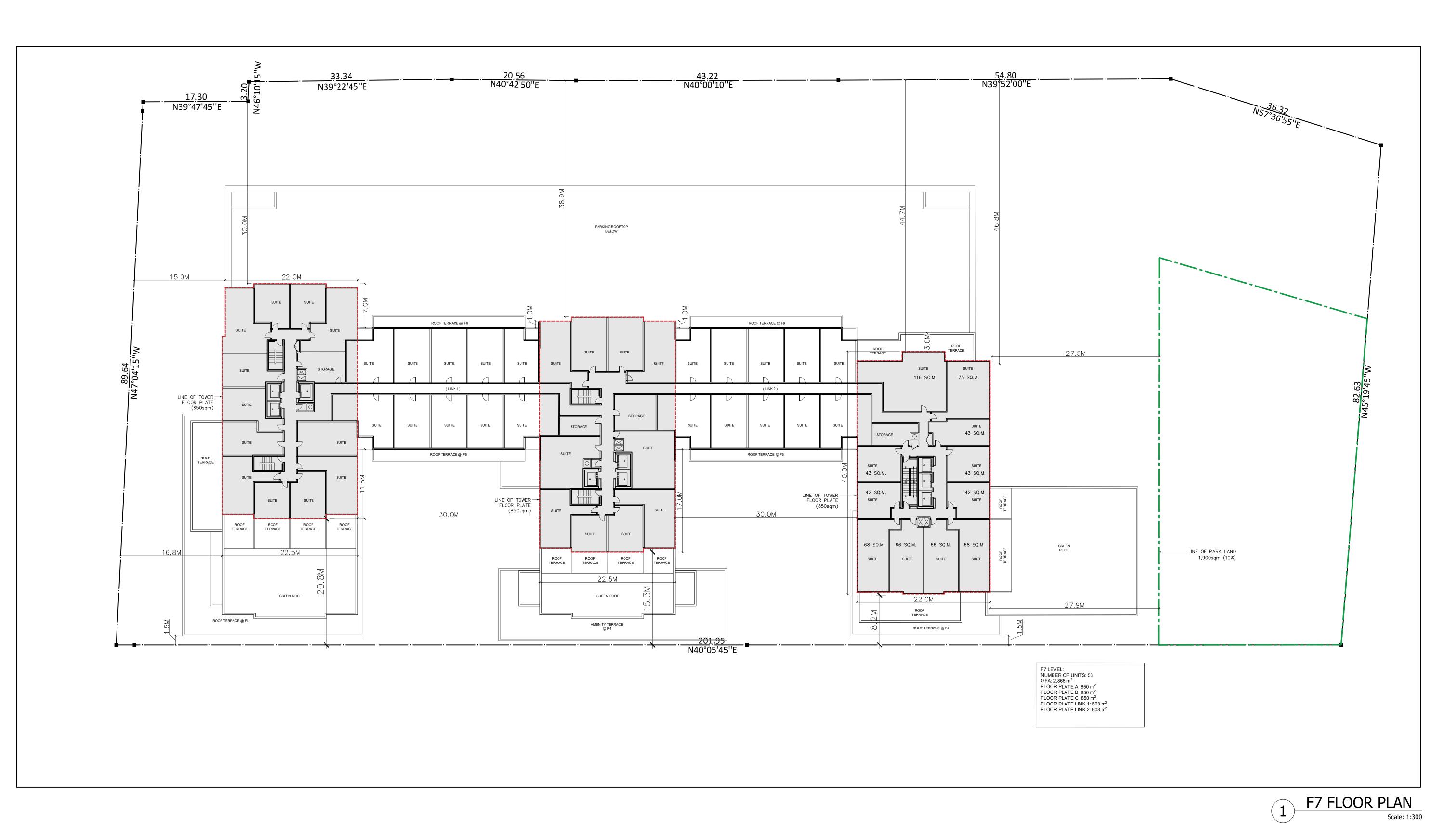
**F6 FLOOR PLAN** 

PRINT DATE: 25-SEPT 2025



PROJ. No.: DEV APPLICATION NO: 1101 SCALE: DRAWN BY:

KT,AJ



DATE No. ISSUE

ARCHITECT: TREGEBOV COGAN ARCHITECT

40 Saint Clair Avenue East, Suite 303 Toronto, ON M4T 1M9 PHONE: 647.352.3350

OWNER:

CONSULTANTS:

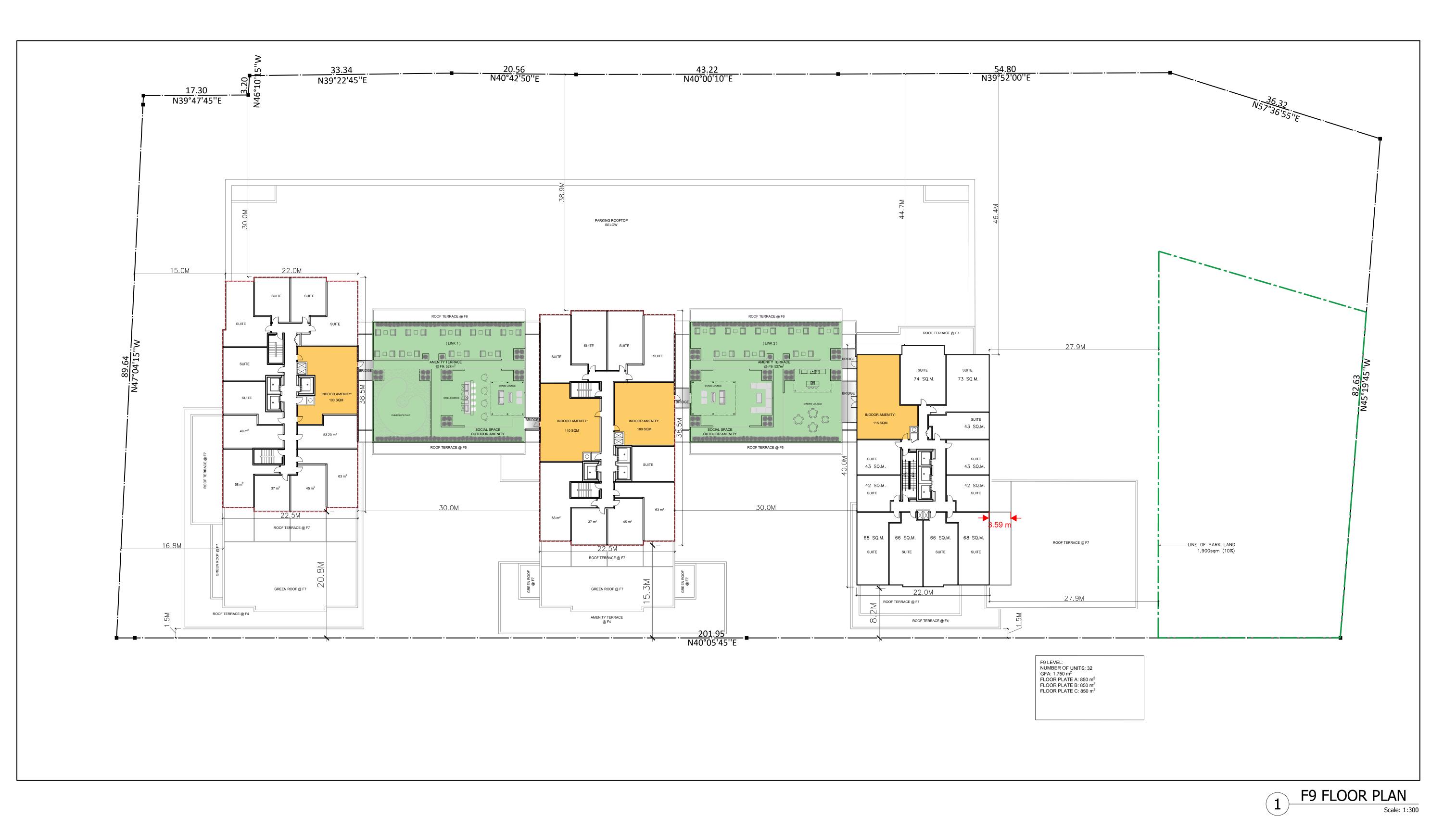
PROJECT NAME:

69 & 117 JOHN ST. MISSISSAUGA

DRAWING TITLE: **F7 FLOOR PLAN** 

PRINT DATE: 25-SEPT 2025

PROJ. No.: DEV APPLICATION NO: 1101 SCALE: DRAWN BY:



DATE No. ISSUE

ARCHITECT:

TREGEBOV COGAN ARCHITECT

40 Saint Clair Avenue East, Suite 303 Toronto, ON M4T 1M9 PHONE: 647.352.3350

OWNER:

CONSULTANTS:

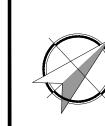
PROJECT NAME:

69 & 117 JOHN ST. MISSISSAUGA

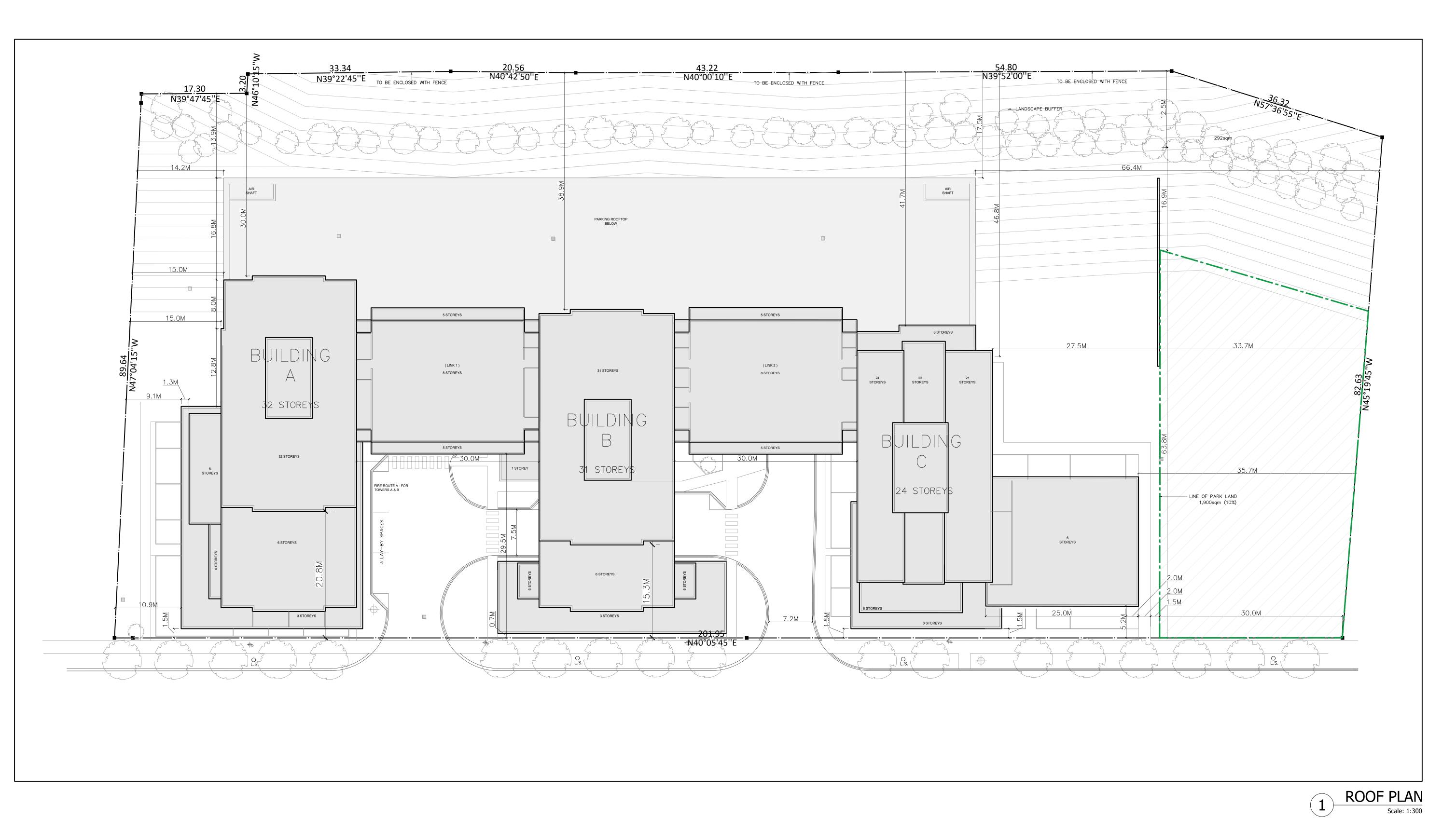
DRAWING TITLE:

**F9 FLOOR PLAN** 

PRINT DATE: 25-SEPT 2025



PROJ. No.: DEV APPLICATION NO: 1101 SCALE: DRAWN BY:



40 Saint Clair Avenue East, Suite 303
Toronto, ON M4T 1M9
PHONE: 647.352.3350

OWNER:

CONSULTANTS:

PROJECT NAME:

69 & 117 JOHN ST. MISSISSAUGA

DRAWING TITLE:

ROOF PLAN

PRINT DATE: 25-SEPT 2025



NORTH
PROJ. No.:
1101
SCALE:
AS NOTED
DRAWN BY:

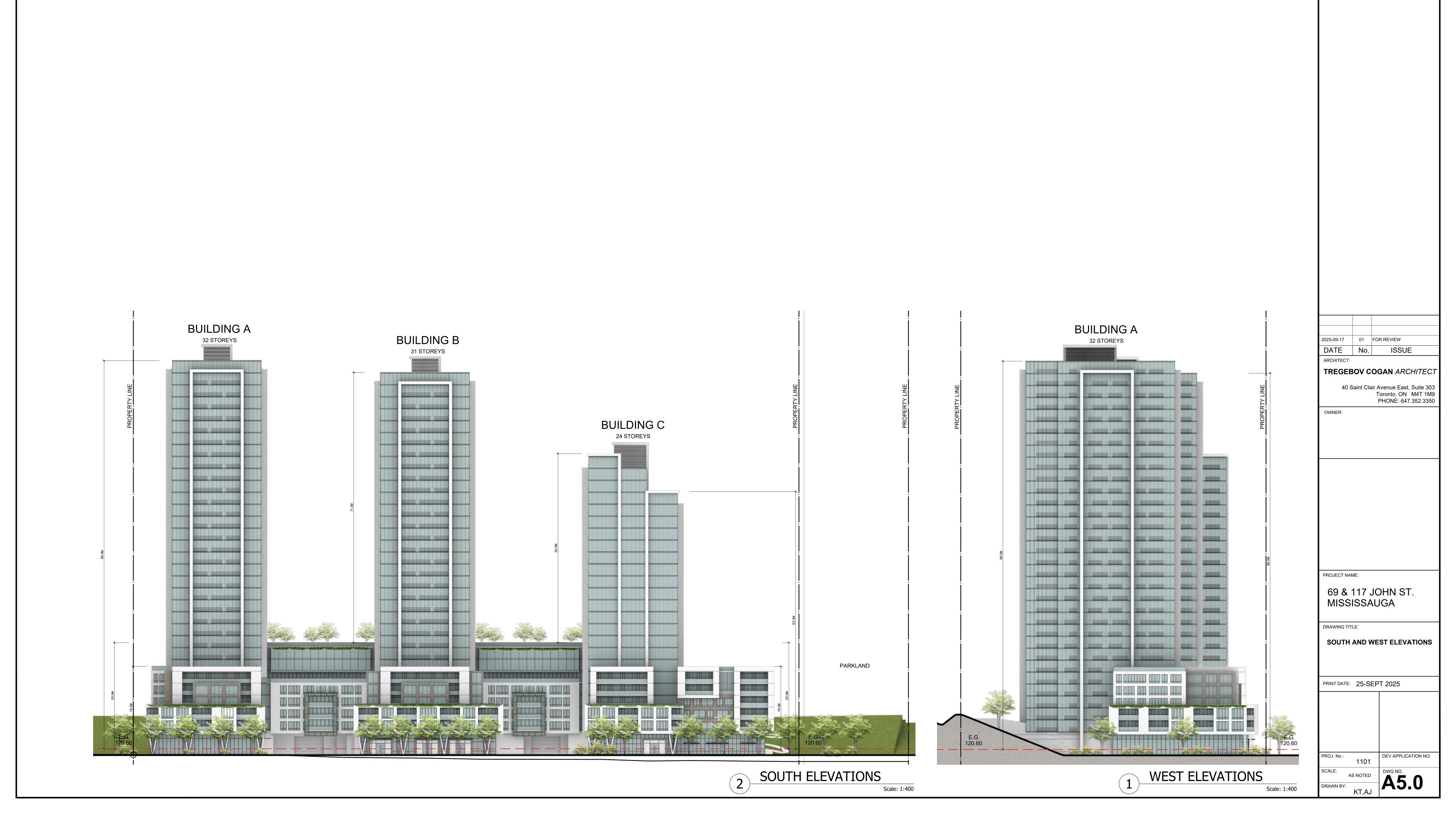
1101 DEV APPLICATION NO:

AS NOTED

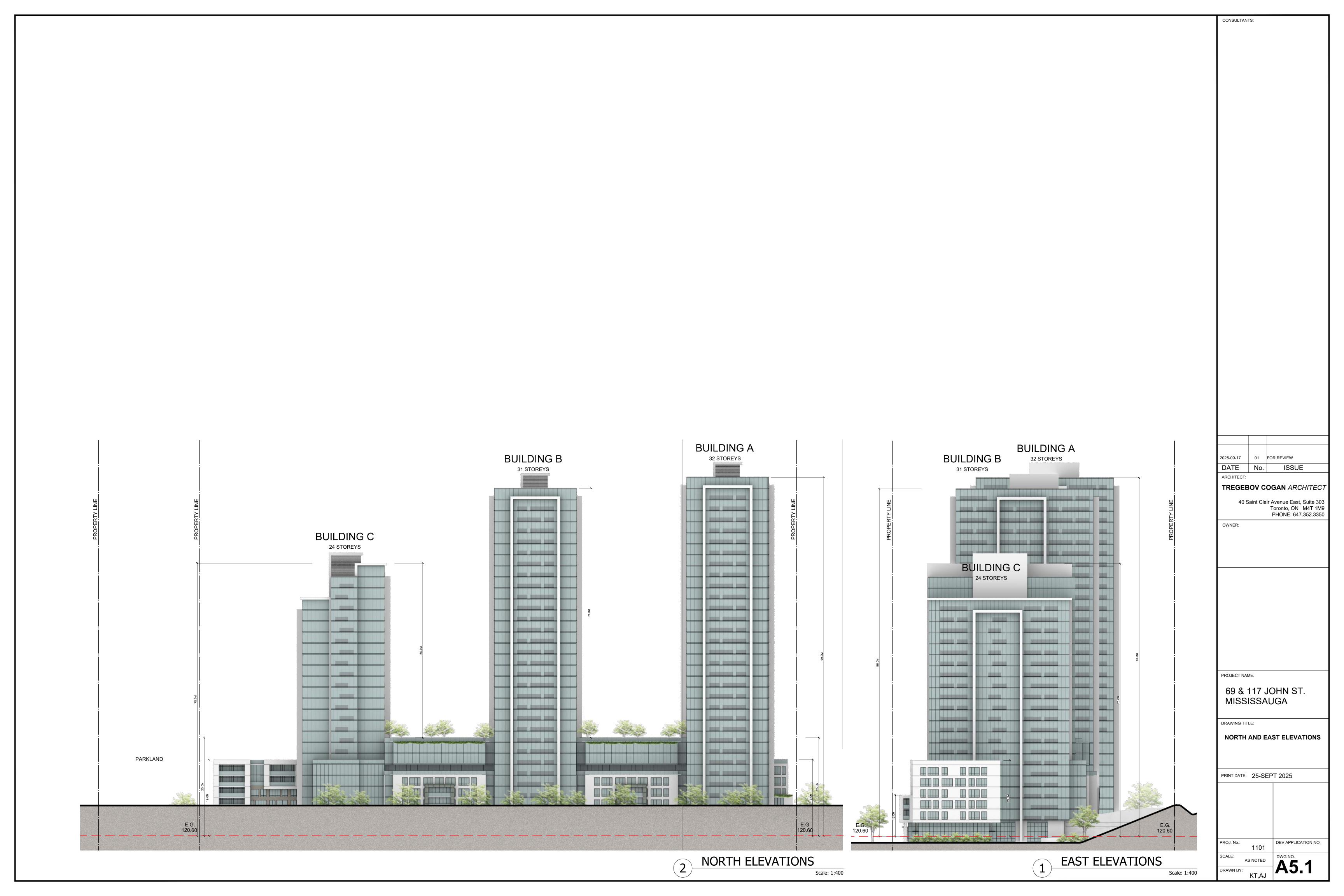
KT,AJ

DWG NO.

A2.18



CONSULTANTS:



## APPENDIX B TRAFFIC DATA

#### **Richard Li**

From: Rail Data Requests < RailDataRequests@metrolinx.com>

**Sent:** October 2, 2025 12:18 PM

To: Richard Li

**Cc:** Kathy Katsiroumpas

Subject: RE: GO Traffic Data Request: 69 & 117 John St, Mississauga (VCL#1220393.000)

#### Good afternoon,

Further to your request dated September 22, 2025, the subject lands (69 & 117 John Street, Mississauga) are located within 300 metres of the Canadian Pacific Galt Subdivision (which carries Milton GO rail service).

It's anticipated that GO rail service on this Subdivision will be comprised of diesel trains only. The GO rail fleet combination on this Subdivision will consist of up to 1 locomotive and 10 passenger cars. The typical GO rail weekday train volume forecast near the subject lands, including both revenue and equipment trips is in the order of 22 trains. The planned detailed trip breakdown is listed below:

	1 Diesel Locomotive		1 Diesel Locomotive
Day (0700- 2300)	20	Night (2300- 0700)	2

The current track design speed near the subject lands is 65 mph (105 km/h).

There are anti-whistling by-laws in affect near the subject lands at Haines Road at railway crossing.

Operational information is subject to change and may be influenced by, among other factors, service planning priorities, operational considerations, funding availability and passenger demand.

It should be noted that this information only pertains to Metrolinx rail service. It would be prudent to contact other rail operators in the area directly for rail traffic information pertaining to non-Metrolinx rail service.

I trust this information is useful. Should you have any questions or concerns, please do not hesitate to contact me.

Best Regards,

#### Jenna Auger (She/Her)

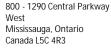
Project Analyst, Adjacent Construction Review (ACR)
Development & Real Estate Management
T: (416)-881-0579
20 Bay Street | Toronto | Ontario | M5J 2W3





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April 12, 2018

Via email: seema@valcoustics.com

Seema Nagaraj Valcoustics 30 Wertheim Court Unit 25 Richmond Hill, ON L4B 1B9

Dear Sir/Madam:

Re: Rail Traffic Volumes, CP Mileage 14.15, Galt Subdivision,

473 Hensall Circle

This is in reference to your request for rail traffic data in the vicinity of 473 Hensall Circle in the City of Mississauga. The study area is located at mile 14.15 of our Galt Subdivision, which is classified as a Prinicipal Main line.

The information requested is as follows:

Number of freight trains between 0700 & 2300:
 Number of freight trains between 2300 & 0700:

Average number of cars per train: 67Maximum cars per train freight: 151

3. Number of locomotives per train: 2 (4 max)

4. Maximum permissible train speed: 50 mph freight

- 5. The whistle signal is prohibited approaching public grade crossings through the study area, however, the whistle may be sounded if deemed necessary by the train crew for safety reasons at any time.
- 6. There are 2 mainline tracks with continuously welded rail at this location along with a cross connection between these rails which may cause more than normal noise.

The information provided is based on recent rail traffic. Variations of the above may exist on a day-to-day basis. Specific measurements may also vary significantly depending on customer needs.

Yours truly,

Josie Tomei SR/WA

Specialist Real Estate Sales & Acquisitions – Ontario

	11-Oct-22	NOISE REPORT FOR PROPOSED DEVELOPMENT		
REQUESTED	BY:			
Name: Richard Li		Location:	Hurontario Street from Dundas Street to CPR	
Company: Valcoustics Canad				
PREPARED E	BY:			
Name Loudel Uy				
Tel#: (905) 615- 3200	= 50			
MISSISSAU	<u>iga</u>	ID#	564	

ON SITE TRAFFIC DATA					
Specific	Street Names				
	Hurontario Street	Kirwin Avenue	ACC STATE OF THE PARTY OF THE P	ATTENDO CONTRACTOR	
AADT:	53,200	12,500	- Series of	The same of the sa	
# of Lanes:	4 lanes	2 lanes		The state of the s	
% Trucks:	4%	2%			
Medium/Heavy Trucks Ratio:	55/45	55/45			
Day/Night Split:	90/10	90/10	At an interest and a principle of the state		
Posted Speed Limit:	50km/h	50km/h		70	
Gradient Of Road:	<2%	<2%			
Ultimate R.O.W:	35m	26m		No.	
Lilltimate Traffic Data O	hhv (2041)	4	Talen s Malenda Malenda Market (1975)	74	

ON SITE TRAFFIC DATA

#### **Comments:**

Ultimate Traffic Data Only (2041)

-There is a proposed LRT line along Hurontario Street. Existing lanes may be converted from 6 lanes to 4 lanes with 2 LRT lines in the middle.

Please contact Farhad Shala @ (905) 615-3200 ext. 3377 or farhad.shala@mississauga.ca for more info regarding LRT.

- There's no available Ultimate AADT for John Street.

## APPENDIX C ENVIRONMENTAL NOISE GUIDELINES

# APPENDIX C ENVIRONMENTAL NOISE GUIDELINES MINISTRY OF THE ENVIRONMENT, CONSERVATION AND PARKS (MECP)

Reference: MECP Publication NPC-300, October 2013: "Environmental Noise Guideline, Stationary and Transportation Source – Approval and Planning".

SPACE	SOURCE	TIME PERIOD	CRITERION
Living/dining, den areas of residences, hospitals, nursing homes, schools, daycare centres, etc.	Road Rail Aircraft	07:00 to 23:00 07:00 to 23:00 24-hour period	45 dBA 40 dBA NEF/NEP 5
Living/dining, den areas of residences, hospitals, nursing homes, etc. (except schools or daycare centres)	Road Rail Aircraft	23:00 to 07:00 23:00 to 07:00 24-hour period	45 dBA 40 dBA NEF/NEP 5
Sleeping quarters	Road Rail Aircraft	07:00 to 23:00 07:00 to 23:00 24-hour period	45 dBA 40 dBA NEF/NEP 0
Sleeping quarters	Road Rail Aircraft	23:00 to 07:00 23:00 to 07:00 24-hour period	40 dBA 35 dBA NEF/NEP 0
Outdoor Living Areas	Road and Rail	07:00 to 23:00	55 dBA
Outdoor Point of Reception	Aircraft	24-hour period	NEF/NEP 30#
	Stationary Source Class 1 Area	07:00 to 19:00 <sup>(1)</sup> 19:00 to 23:00 <sup>(1)</sup>	50* dBA 50* dBA
	Class 2 Area	07:00 to 19:00 <sup>(2)</sup> 19:00 to 23:00 <sup>(2)</sup>	50* dBA 45* dBA
	Class 3 Area	07:00 to 19:00 <sup>(3)</sup> 19:00 to 23:00 <sup>(3)</sup>	45* dBA 40* dBA
	Class 4 Area	07:00 to 19:00 <sup>(4)</sup> 19:00 to 23:00 <sup>(4)</sup>	55* dBA 55* dBA

..../cont'd

SOURCE	TIME PERIOD	CRITERION
Stationary Source		
Class 1 Area		50* dBA
		50* dBA
	23:00 to 07:00 <sup>(1)</sup>	45* dBA
Class 2 Area	07:00 to 19:00 <sup>(2)</sup>	50* dBA
	19:00 to 23:00 <sup>(2)</sup>	50* dBA
	23:00 to 07:00 <sup>(2)</sup>	45* dBA
Class 3 Area	07:00 to 19:00 <sup>(3)</sup>	45* dBA
	19:00 to 23:00 <sup>(3)</sup>	45* dBA
	23:00 to 07:00 <sup>(3)</sup>	40* dBA
Class 4 Area	07:00 to 19:00 <sup>(4)</sup>	60* dBA
	19:00 to 23:00 <sup>(4)</sup>	60* dBA
	23:00 to 07:00 <sup>(4)</sup>	55* dBA
	Stationary Source Class 1 Area Class 2 Area Class 3 Area	Stationary Source Class 1 Area  07:00 to 19:00 <sup>(1)</sup> 19:00 to 23:00 <sup>(1)</sup> 23:00 to 07:00 <sup>(1)</sup> Class 2 Area  07:00 to 19:00 <sup>(2)</sup> 19:00 to 23:00 <sup>(2)</sup> 23:00 to 07:00 <sup>(2)</sup> 23:00 to 07:00 <sup>(2)</sup> 07:00 to 19:00 <sup>(3)</sup> 19:00 to 23:00 <sup>(3)</sup> 23:00 to 07:00 <sup>(3)</sup> Class 4 Area  07:00 to 19:00 <sup>(4)</sup> 19:00 to 23:00 <sup>(4)</sup>

Reference: MECP Publication ISBN 0-7729-2804-5, 1987: "Environmental Noise Assessment in Land-Use Planning".

EXCESS ABOVE RECOMMENDED SOUND LEVEL LIMITS (dBA)	CHANGE IN SUBJECTIVE LOUDNESS ABOVE	MAGNITUDE OF THE NOISE PROBLEM	NOISE CONTROL MEASURES (OR ACTION TO BE TAKEN)
No excess (<55 dBA)	_	No expected noise problem	None
1 to 5 inclusive (56 to 60 dBA)	Noticeably louder	Slight noise impact	If no physical measures are taken, then prospective purchasers or tenants should be made aware by suitable warning clauses.
6 to 10 inclusive (61 - 65 dBA)	Almost twice as loud	Definite noise impact	Recommended.
11 to 15 inclusive (66 - 70 dBA)	Almost three times as loud	Serious noise impact	Strongly Recommended.
16 and over (>70 dBA)	Almost four times as loud	Very serious noise impact	Strongly Recommended (may be mandatory).

may not apply to in-fill or re-development. or the minimum hourly background sound exposure  $L_{\text{eq}(1)}$ , due to road traffic, if higher.

<sup>(1)</sup> Class 1 Area: Urban.

Class 2 Area: Urban during day; rural-like evening and night.

<sup>(2)</sup> (3) (4)

Class 3 Area: Rural.
Class 4 Area: Subject to land use planning authority's approval.

## APPENDIX D SAMPLE SOUND LEVEL CALCULATION

STAMSON 5.04 NORMAL REPORT Date: 02-10-2025 20:34:38 MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT Filename: a nf.te Time Period: Day/Night 16/8 hours Description: Predicted Sound Levels - Building A, North Facade Rail data, segment # 1: CPR&GO (day/night) ! Trains ! Speed !# loc !# Cars! Eng !Cont ! (km/h) !/Train!/Train! type !weld Train \* 1. CPR ! 13.7/12.2 ! 80.0 ! 4.0 !151.0 !Diesel! Yes \* 2. GO ! 20.0/2.0 ! 105.0 ! 1.0 ! 10.0 !Diesel! Yes \* 2. GO \* The identified number of trains have been adjusted for future growth using the following parameters: Train type: ! Unadj. ! Annual % ! Years of !
No Name ! Trains ! Trains Train type: 1. CPR ! 9.0/8.0 ! 2.50 ! 17.00 ! ! 20.0/2.0 ! 0.00 ! 10.00 ! Data for Segment # 1: CPR&GO (day/night) Angle1 Angle2 : -90.00 deg 90.00 deg

Wood depth : 0 (No woods
No of house rows : 0 / 0

Surface : 1 (Absorptive (No woods.) (Absorptive ground surface) Receiver source distance : 43.00 / 43.00 m Receiver height : 90.00 / 90.00 m
Topography : 1 (Flat (Flat/gentle slope; no barrier) No Whistle Reference angle : 0.00 Results segment # 1: CPR&GO (day) LOCOMOTIVE (0.00 + 70.93 + 0.00) = 70.93 dBA Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq -90 90 0.00 75.50 **-**4.57 0.00 0.00 0.00 0.00 70.93 \_\_\_\_\_\_ WHEEL (0.00 + 64.08 + 0.00) = 64.08 dBAAngle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq -90 90 0.00 68.65 -4.57 0.00 0.00 0.00 0.00 64.08

\_\_\_\_\_\_

Segment Leq: 71.75 dBA

Total Leq All Segments: 71.75 dBA

File: 122-0393

```
Results segment # 1: CPR&GO (night)
_____
LOCOMOTIVE (0.00 + 72.73 + 0.00) = 72.73 \text{ dBA}
Angle1 Angle2 Alpha RefLeg D.Adj F.Adj W.Adj H.Adj B.Adj SubLeg
  -90 90 0.00 77.31 -4.57 0.00 0.00 0.00 0.00 72.73
WHEEL (0.00 + 66.02 + 0.00) = 66.02 \text{ dBA}
Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
  -90 90 0.00 70.59 -4.57 0.00 0.00 0.00 0.00 66.02
______
Segment Leq: 73.57 dBA
Total Leg All Segments: 73.57 dBA
Road data, segment # 1: Hurontario (day/night)
______
Car traffic volume : 45965/5107 veh/TimePeriod *
Medium truck volume : 1053/117 veh/TimePeriod
Heavy truck volume : 862/96 veh/TimePeriod *
Posted speed limit : 50 km/h
Road gradient : 0 \% Road pavement : 1 (Typical asphalt or concrete)
* Refers to calculated road volumes based on the following input:
   24 hr Traffic Volume (AADT or SADT): 53200
   Percentage of Annual Growth :
Number of Years of Growth :
                                  : 10.00
   Medium Truck % of Total Volume : 2.20 Heavy Truck % of Total Volume : 1.80
   Day (16 hrs) % of Total Volume : 90.00
Data for Segment # 1: Hurontario (day/night)
_____
Angle1 Angle2 : 0.00 deg 90.00 deg Wood depth : 0 (No woods
Wood depth : 0
No of house rows : 0 / 0
Surface : 1
                                     (No woods.)
                                     (Absorptive ground surface)
Receiver source distance : 233.00 / 233.00 m
Receiver height : 90.00 / 90.00 m
Topography : 1 (Flat/gentle slope; no barrier)
```

Reference angle : 0.00

Results segment # 1: Hurontario (day)

Source height = 1.16 m

ROAD (0.00 + 55.76 + 0.00) = 55.76 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
0 90 0.00 70.68 0.00 -11.91 -3.01 0.00 0.00 0.00 55.76

Segment Leq : 55.76 dBA

Total Leq All Segments: 55.76 dBA

Results segment # 1: Hurontario (night)

Source height = 1.16 m

ROAD (0.00 + 49.23 + 0.00) = 49.23 dBA

Angle1 Angle2 Alpha RefLeq P.Adj D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

0 90 0.00 64.15 0.00 -11.91 -3.01 0.00 0.00 0.00 49.23

Segment Leq: 49.23 dBA

Total Leq All Segments: 49.23 dBA

TOTAL Leq FROM ALL SOURCES (DAY): 71.86 (NIGHT): 73.59

File: 122-0393

STAMSON 5.04 NORMAL REPORT Date: 02-10-2025 20:23:20

MINISTRY OF ENVIRONMENT AND ENERGY / NOISE ASSESSMENT

Filename: 1 cl7 o.te Time Period: Day/Night 16/8 hours Description: Predicted Sound Levels - Building C, L7 Terrace

#### Rail data, segment # 1: CPR&GO (day/night) \_\_\_\_\_

Train ! Trains ! Speed !# loc !# Cars! Eng !Cont Type ! (km/h) !/Train!/Train! type !weld \* 1. CPR ! 13.7/12.2 ! 80.0 ! 4.0 !151.0 !Diesel! Yes \* 2. GO ! 20.0/2.0 ! 105.0 ! 1.0 ! 10.0 !Diesel! Yes

\* The identified number of trains have been adjusted for future growth using the following parameters:

Train type: ! Unadj. ! Annual % ! Years of ! No Name ! Trains ! Increase ! Growth ! ----+ 1. CPR ! 9.0/8.0 ! 2.50 ! 17.00 ! 2. GO ! 20.0/2.0 ! 0.00 ! 10.00 !

### Data for Segment # 1: CPR&GO (day/night)

Angle1 Angle2 : -82.00 deg 90.00 deg
Wood depth : 0 (No woods No of house rows : 0 / 0
Surface : 1 (Absorptive (No woods.)

(Absorptive ground surface)

Receiver source distance : 53.00 / 53.00 m Receiver height : 1.50 / 87.00 m
Topography : 4 (Elev

(Elevated; with barrier)

No Whistle

No whistle

Barrier angle1 : -82.00 deg Angle2 : 90.00 deg

Barrier height : 0.00 m

Elevation : 23.00 m

Barrier receiver distance : 2.80 / 2.80 m

Source elevation : 8.40 m
Receiver elevation : 23.00 m
Barrier elevation : 23.00 m
Reference angle : 0.00

Results segment # 1: CPR&GO (day)

```
Barrier height for grazing incidence
Source ! Receiver ! Barrier ! Elevation of
Height (m) ! Height (m) ! Height (m) ! Barrier Top (m)
      4.00! 1.50! 0.86! 23.86
      0.50 !
                   1.50 !
                                 0.68 !
LOCOMOTIVE (0.00 + 69.82 + 0.00) = 69.82 \text{ dBA}
Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
  -82 90 0.00 75.50 -5.48 -0.20 0.00 0.00 -0.65 69.17*
  -82
         90 0.00 75.50 -5.48 -0.20 0.00 0.00 0.00 69.82
* Bright Zone !
WHEEL (0.00 + 62.97 + 0.00) = 62.97 \text{ dBA}
Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

    -82
    90
    0.00
    68.65
    -5.48
    -0.20
    0.00
    0.00
    -1.45
    61.52*

    -82
    90
    0.00
    68.65
    -5.48
    -0.20
    0.00
    0.00
    0.00
    62.97

* Bright Zone !
Segment Leq: 70.64 dBA
Total Leq All Segments: 70.64 dBA
Results segment # 1: CPR&GO (night)
Barrier height for grazing incidence
Source ! Receiver ! Barrier ! Elevation of
Height (m) ! Height (m) ! Barrier Top (m)
     4.00! 87.00! 81.84! 104.84
      0.50 !
                 87.00 !
                               81.66 !
LOCOMOTIVE (0.00 + 71.63 + 0.00) = 71.63 \text{ dBA}
Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq

    -82
    90
    0.00
    77.31
    -5.48
    -0.20
    0.00
    0.00
    -0.00
    71.63*

    -82
    90
    0.00
    77.31
    -5.48
    -0.20
    0.00
    0.00
    0.00
    71.63*

______
* Bright Zone !
WHEEL (0.00 + 64.91 + 0.00) = 64.91 \text{ dBA}
Angle1 Angle2 Alpha RefLeq D.Adj F.Adj W.Adj H.Adj B.Adj SubLeq
______
  -82 90 0.00 70.59 -5.48 -0.20 0.00 0.00 -0.00 64.91*
  -82
        90 0.00 70.59 -5.48 -0.20 0.00 0.00 0.00 64.91
______
* Bright Zone !
Segment Leq: 72.47 dBA
Total Leg All Segments: 72.47 dBA
TOTAL Leq FROM ALL SOURCES (DAY): 70.64
```

(NIGHT): 72.47