THORNY BRAE TOWNHOUSE DEVELOPMENT 1775 Thorny Brae Place Mississauga, Ontario

Functional Servicing & Stormwater Management Report

Prepared for:

KINGRIDE DEVELOPMENTS

Prepared by:



MGM Consulting Inc. 555 Industrial Drive, Suite 201 Milton, Ontario L9T 5E1

File No. 2025-004

Date: June 24, 2025

1st Revision October 16, 2025

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#### 1 Introduction

MGM Consulting Inc. has been retained by Kingridge Developments to prepare a Functional Servicing & Stormwater Management Report in support of a Site Plan Approval submission for the proposed Thorny Brae Townhouse Development, located at 1775 Thorny Brae Place, Mississauga Ontario.

The proposed development will consist of 9 stacked townhouse blocks and 2 traditional townhouse blocks, providing a total of 95 residential units with an anticipated population of 323 residents. A new asphalt access road will connect the site to Mississauga Road, with sidewalks, parking spaces, and landscaped amenity areas. The primary fire route access for the development will be provided from Mississauga Road.

The objective of this report is to provide details on the required site servicing, grading and drainage and stormwater management features as required meet the objectives of the City and Region's design criteria.

The site is identified in the location plan in Figure 1.

#### 2 Existing Conditions

The total site area is 1.53 ha with four vacant one-story residential buildings. The existing topography gradually slopes from west to east with steeper slopes in the east portion of the site. Elevations range from approximately 147.9m in the northwest, down to approximately 144.9 m in the east, approximately mid-lot.

The existing site is identified in Figure 2.

### 3 Proposed Site Grading

The proposed site grading will consider the existing topography, perimeter grades, the proposed vehicular access from Mississauga Road, provide sufficient frost cover for site servicing, and as required to meet the stormwater management and servicing objectives of the City and Municipal design criteria.

The proposed Grading Plan is indicated on the appended Drawing CV-2.

#### 4 Existing Municipal Servicing

The existing municipal servicing include:

- A storm sewer located within the storm sewer easement bisecting the site, ranging in size from 675
  to 750mm with and outlet invert of 140.28m,
- A 250mm sanitary sewer with an outlet invert of 143.52, located adjacent to the existing storm sewer easement within the site,
- A 400mm watermain located within the Mississauga Road right of way.

#### 5 Proposed Storm Design

5.1 Minor Storm Servicing

Fax: (905) 875-1339

Tel: (905) 567-8678



Storm flows from the site will be conveyed to the existing storm sewer system located within the storm sewer easement which bisects the site. Site storm sewers are designed to convey the 10-year storm flows, without surcharging, using the City of Mississauga Intensity-Duration Frequency (IDF) curves. The internal storm system will consist of a series of underground storm sewers, manholes and catch basins as indicated on the appended Site Servicing Plan, Drawing CV-3.

The minor system is designed based on the Rational Method using a time of concentration of 10 minutes and the City of Mississauga's IDF curve with a 10-year return period.

The storm sewer design sheet has been included in Appendix A.

#### 4.2 Major Storm Servicing

In the event of a major storm or the storm system becoming blocked, the proposed grading will be designed to ensure emergency overland flow is directed towards the Mississauga Road right of way, on the southwest side of the site.

The proposed overland spill elevation of 147.09 is 3.22m below the proposed lowest finished-floor elevation of the Townhouse Units.

#### 5. Stormwater Management

#### 5.1 Proposed Rate Controls

According to the City of Mississauga's Transportation and Works Development Requirements Manual, Section 8, the subject site is located in the Credit River Subwatershed. Per Section 8, sites located within the Credit River Subwatershed between Norval and Port Credit, no quantity stormwater management control is required. Therefore, no rate controls are to be implemented for this site.

However, despite no rate control imposed directly on the site, Low Impact Development (LID) measures such as 300mm deep topsoil layer will be implemented to reduce surface runoff and promote infiltration and rooftop rainwater leaders of the rear-draining building areas will be collectively directed to rear yard infiltration facilities.

#### 5.2 Proposed Quality Control

Tel: (905) 567-8678

Options for stormwater quality controls include wet ponds, wetlands, bio-treatment areas, flatly graded grass swales, and package treatment units. Given the nature of the development, the limited available areas for a quality control feature and the impact that a quality control feature would have on the use of the property, the required stormwater quality objectives will be achieved using a "treatment train" approach which includes the installation of catch basin shields installed in all catch basins and double catch basins and the installation of a HydroDome model HD 8 treatment unit, located at the downstream limit of the proposed internal storm system.

2

Fax: (905) 875-1339



The proposed treatment unit will be installed at the outlet from the internal storm system, and as such, it will provide the required stormwater quality treatment for runoff from all areas of the site.

The combined treatment train consisting of catch basin shields and the OGS unit will provide an anticipated combined TSS removal of 80%.

Refer to Appendix B for the treatment unit sizing and for projected treatment train TSS removal calculation. Additionally, Appendix B includes the proposed OGS unit and Catch Basin Shield design specifications.

#### 5.3 Proposed Runoff Volume Reduction

Current objectives are to retain 100% of runoff generated from a minimum 5 mm depth of rainfall from all impervious site surfaces through infiltration, evapotranspiration, water harvesting and reuse. Based on a proposed impervious area of 1.047 Ha, the required volume for infiltration is approximately 53.0 m<sup>3</sup>.

The runoff volume will be provided by three GreenStorm Stormwater Crates which will collect roof runoff from Blocks 3,4,7,8,9 & 10.

Runoff volume reduction calculations are provided in Appendix C.

#### 6. Sediment and Erosion Controls During Construction

In 2006, The Greater Golden Horseshoe Area Conservation Authorities prepared a guideline entitled "Erosion & Sediment Control Guideline for Urban Construction". Based on the guideline, all projects involving the removal of topsoil or site alteration requires an ESC (Erosion and Sediment Control) Plan in place prior to commencing construction. Failure to adhere to the plan could lead to the potential for prosecution under the various pieces of environmental legislation.

The following principles assist in creating an effective ESC Plan. (Ref. Erosion and Sediment Control Guidelines for Urban Construction)

Adopt a multi-barrier approach to provide erosion and sediment control through erosion controls first.

- Retain existing ground cover and stabilize exposed soils with vegetation where possible.
- Limit the duration of soil exposure and phase construction where possible.
- Limit the size of disturbed areas by minimizing nonessential clearing and grading.
- Minimize slope length and gradient of disturbed areas.
- Maintain overland sheet flow and avoid concentrated flows.
- Store/stockpile soil away (e.g. greater than 15 meters) from watercourses, drainage features and top
  of steep slopes.
- Ensure contractors and all involved in the ESC practices are trained in ESC Plan, implementation, inspections, maintenance, and repairs.
- Adjust ESC Plan at construction site to adapt to site features.
- Assess all ESC practices before and after all rainfall and significant snowmelt events.



Sediment and erosion controls proposed for the subject development include:

- Construction of a mud mat at the construction entrance, which will assist in the removal of mud from construction vehicle tires before they exist the site,
- The installation of catchbasin sediment protection on any existing catchbasins in the vicinity of the site,
- The installation of silt control fencing around the perimeter of the site
   The proposed Erosion & Sediment Control Plan Plan is indicated on the appended Drawing CV-1.

#### 7. Sanitary Servicing

Sanitary servicing for the proposed development will be provided by a proposed 250mm PVC sanitary sewer connecting to the existing sanitary manhole on the west side of the site which outlets to the existing 250mm sanitary sewer located withing the Mississauga Road right-of-way. Based on the available outlet elevation of 143.52, a gravity-based sanitary system that provides drainage from the proposed residential development can be provided.

The maximum sanitary flow, including infiltration allowance & peaking factor is 4.7 L/s.

Sanitary flow calculations are provided in Appendix D. The proposed sanitary servicing is indicated on Drawing CV-3.

#### 8. Water Servicing

Water servicing for the proposed development will include a 150mm PVC watermain which will provide firefighting protection and domestic use to Blocks 6 & 7. Four looped 50mm copper watermain services will also provide will provide domestic water supply to Blocks 1,2,3,4,5,8,9,10 & 11. The water service connection for the site is to be made to the existing 400mm watermain, east of the site within the Mississauga Road right of way.

In accordance with Peel Region's Municipal Design Criteria, the peak hour demand is 3.16 l/sec. Fire Flow Calculations, included in Appendix E, indicate a minimum flow of 17000 L/minute, 283 l/sec is required to meet the fire flow demand.

Based on the above, the total water demand, peak water demand per day plus fire flow for the site is 286.0 l/sec.

On June 14, 2024, hydrant flow testing has been conducted at the neighboring property, 4601 Mississauga Road which is included in Appendix F. Based on the test, the watermain has a theoretical flow of 383 L/s at 20 psi, therefore adequate water supply is available to meet the water demand of 286.6 l/sec.

The proposed water servicing for the site is indicated on Drawing CV-3.



#### 9. Summary

The following summarizes the findings and recommendations based on the preceding analyses;

- An internal underground storm sewer system, designed to convey the 10-year storm without surcharging, is proposed, which will convey storm flows to the existing 750mm storm sewer within the storm sewer easement which bisects the site,
- Emergency storm flows are directed towards the Mississauga Road right of way at an elevation of 147.09,
- The proposed runoff volume reduction quantity will be provided by three GreenStorm Stormwater Crates which will collect roof runoff from Blocks 3,4,7,8,9 & 10,
- Sanitary servicing can be provided by connecting to the existing sanitary manhole, located at the west side of the site, adjacent to Mississauga Road,
- Water servicing as required for fire protection and domestic water supply can be provided from the existing 400 mm municipal watermain within the Mississauga Road right of way,
- Sediment and erosion controls as indicated on the Removals/Sediment and Erosion Control Plan are to be implemented prior to construction and maintained until the site is stabilized,

Prepared	b١	<b>/</b> :
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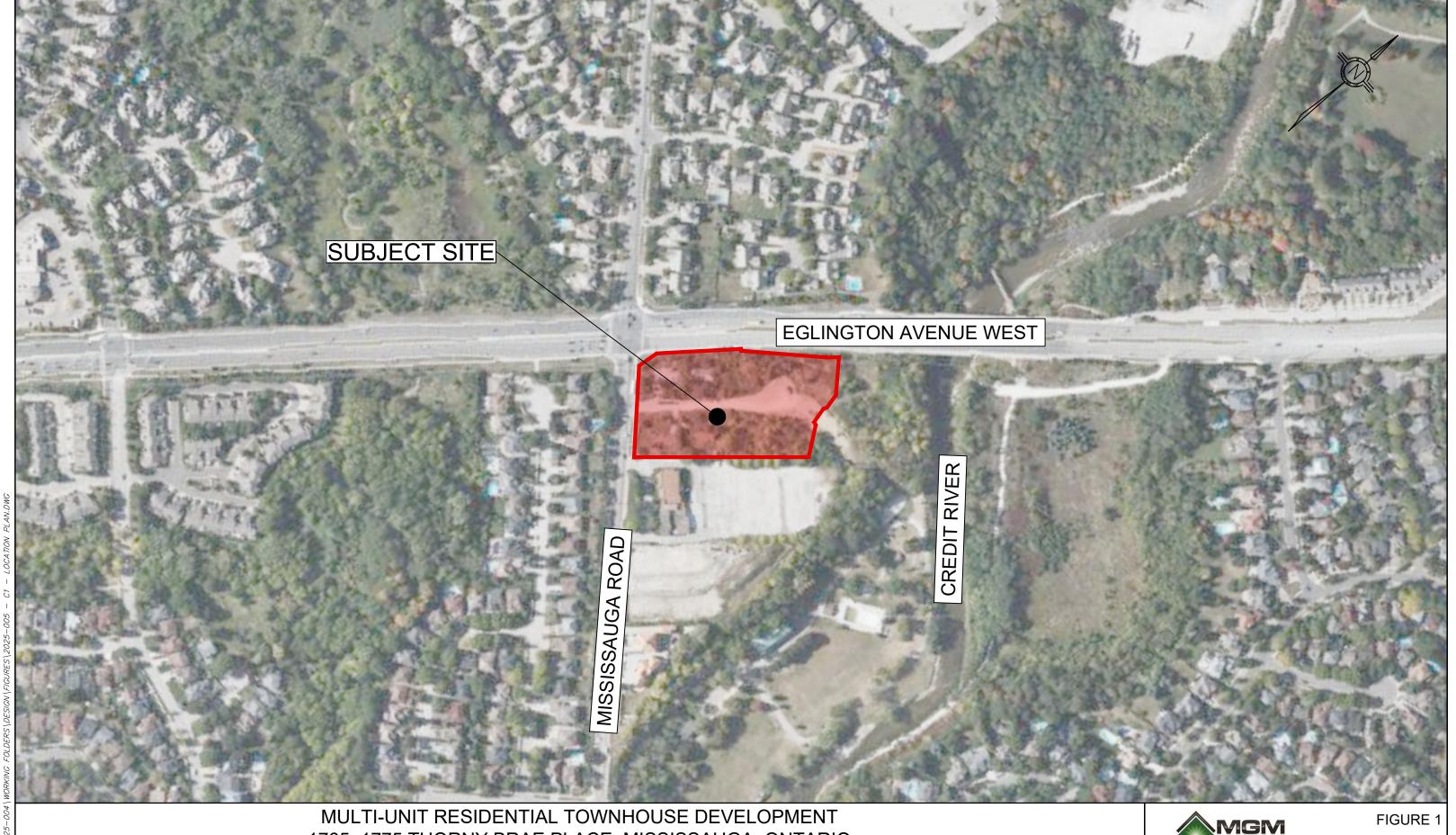
MGM CONSULTING INC.

A. J. KOZYM TO 100517316

Blair Nock, CET



Figures



1765, 1775 THORNY BRAE PLACE, MISSISSAUGA, ONTARIO

**LOCATION PLAN** 



DATE: JUNE 23, 2025 SCALE: 1:3000 DWG#: 2025-004



MULTI-UNIT RESIDENTIAL TOWNHOUSE DEVELOPMENT 1765, 1775 THORNY BRAE PLACE, MISSISSAUGA, ONTARIO

MGM CONSULTING INC.

FIGURE 2

DATE: JUNE 23, 2025 SCALE: 1:750 DWG#: 2025-004

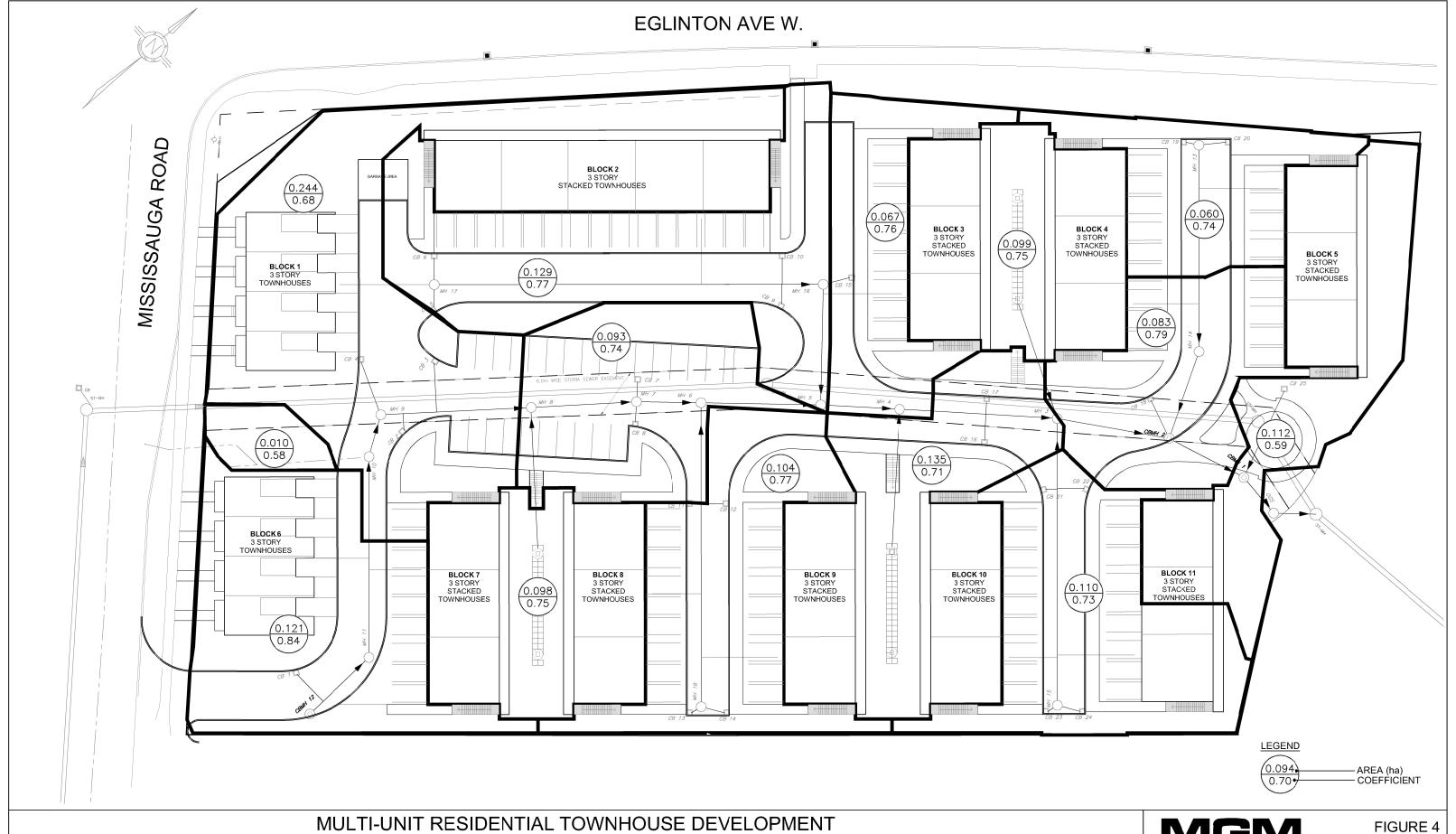


MULTI-UNIT RESIDENTIAL TOWNHOUSE DEVELOPMENT 1765, 1775 THORNY BRAE PLACE, MISSISSAUGA, ONTARIO PROPOSED SITE PLAN



FIGURE 3

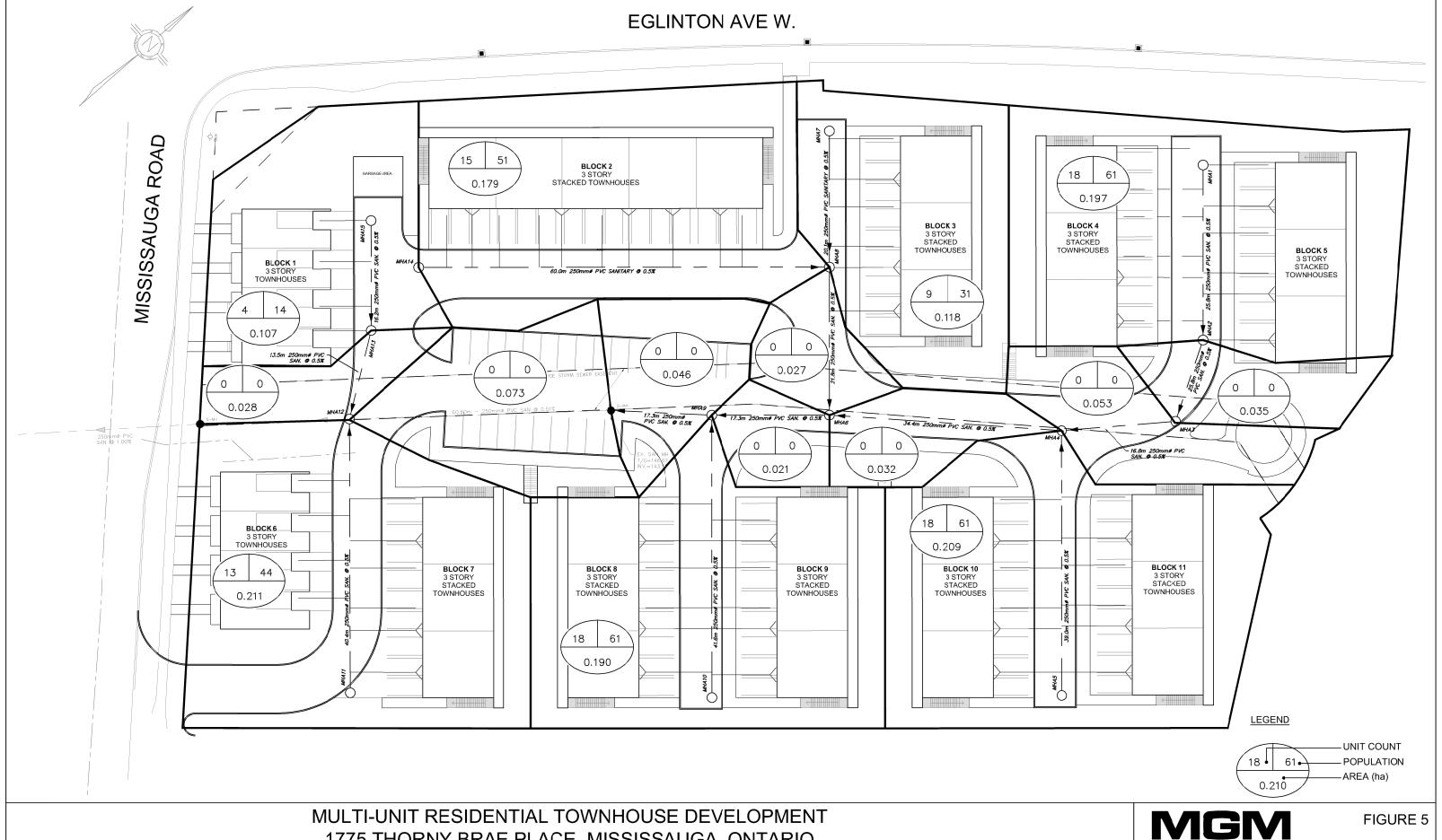
DATE: JUNE 23, 2025 SCALE: NTS DWG#: 2025-004



MULTI-UNIT RESIDENTIAL TOWNHOUSE DEVELOPMENT 1775 THORNY BRAE PLACE, MISSISSAUGA, ONTARIO STORM DRAINAGE AREAS



DATE: OCT.15, 2025 SCALE: 1:500 DWG#: 2025-004 C1



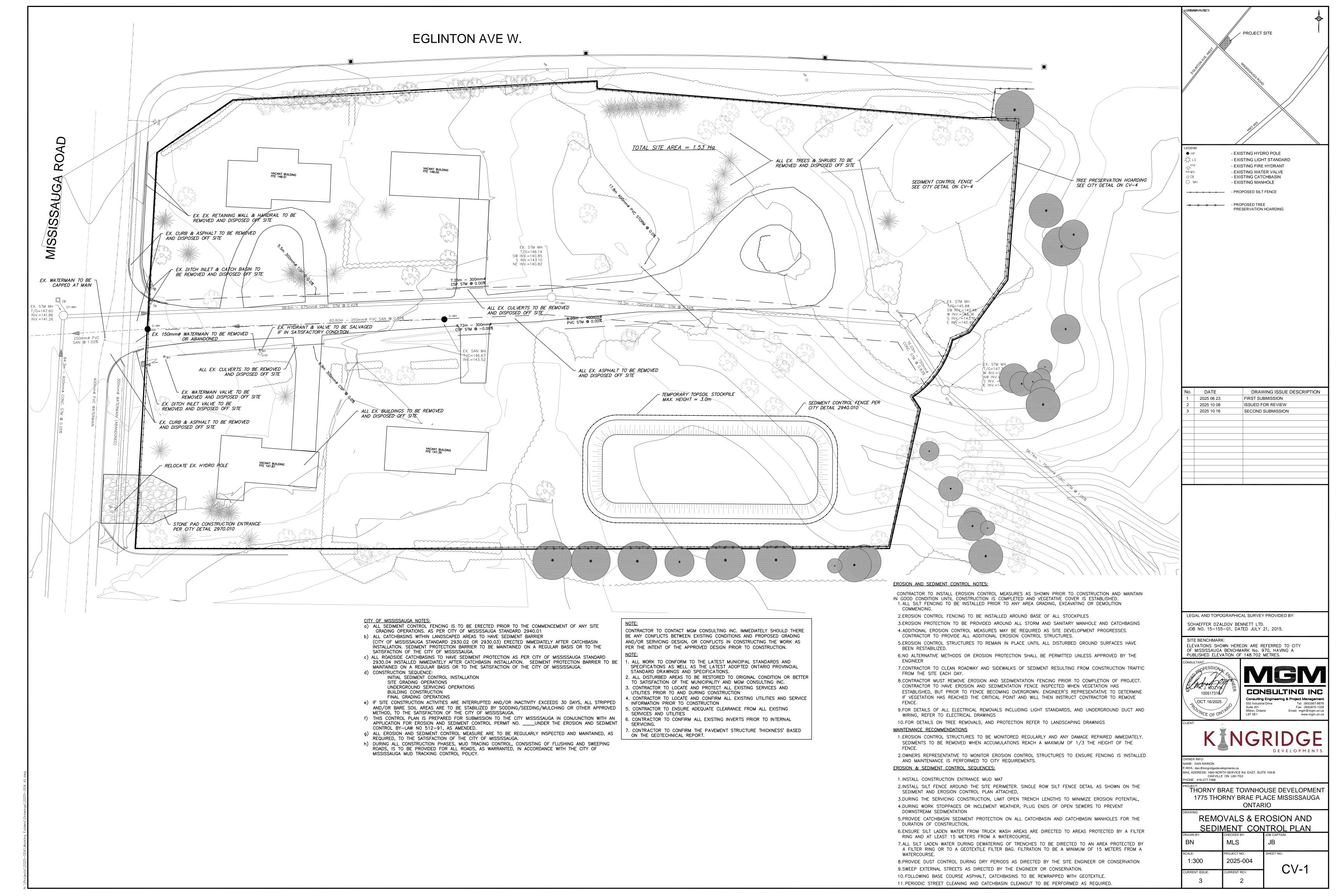
1775 THORNY BRAE PLACE, MISSISSAUGA, ONTARIO SANITARY DRAINAGE AREAS

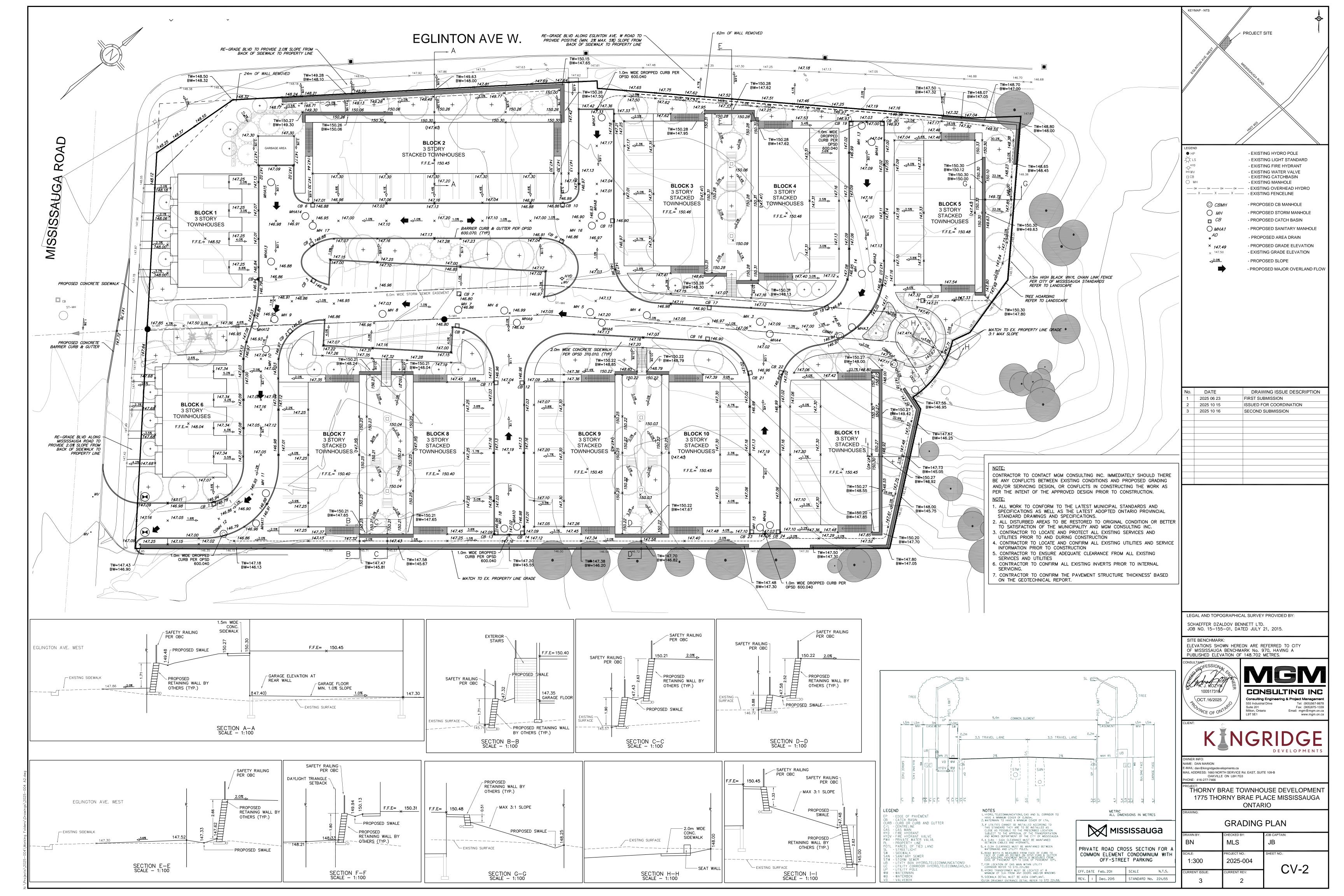


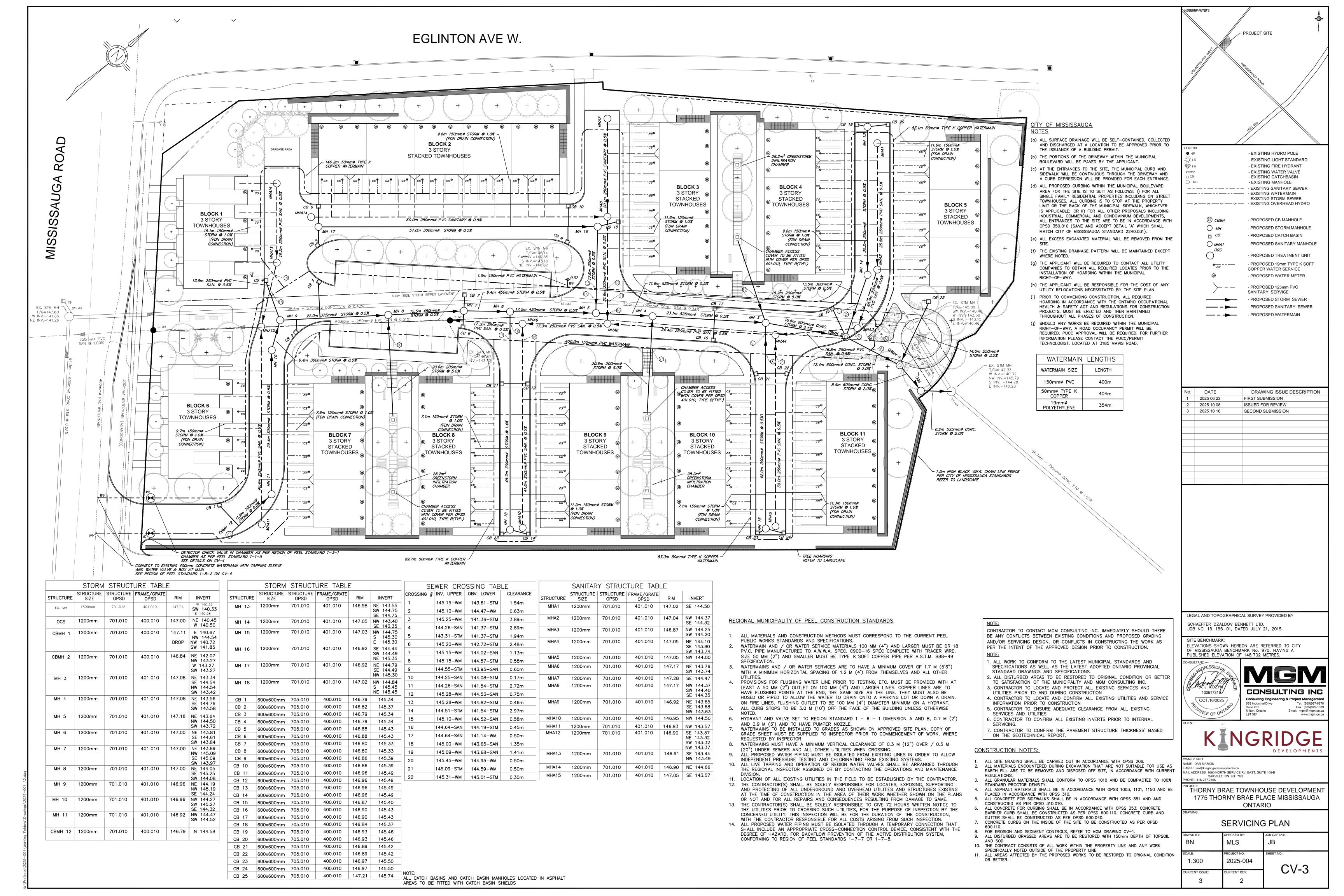
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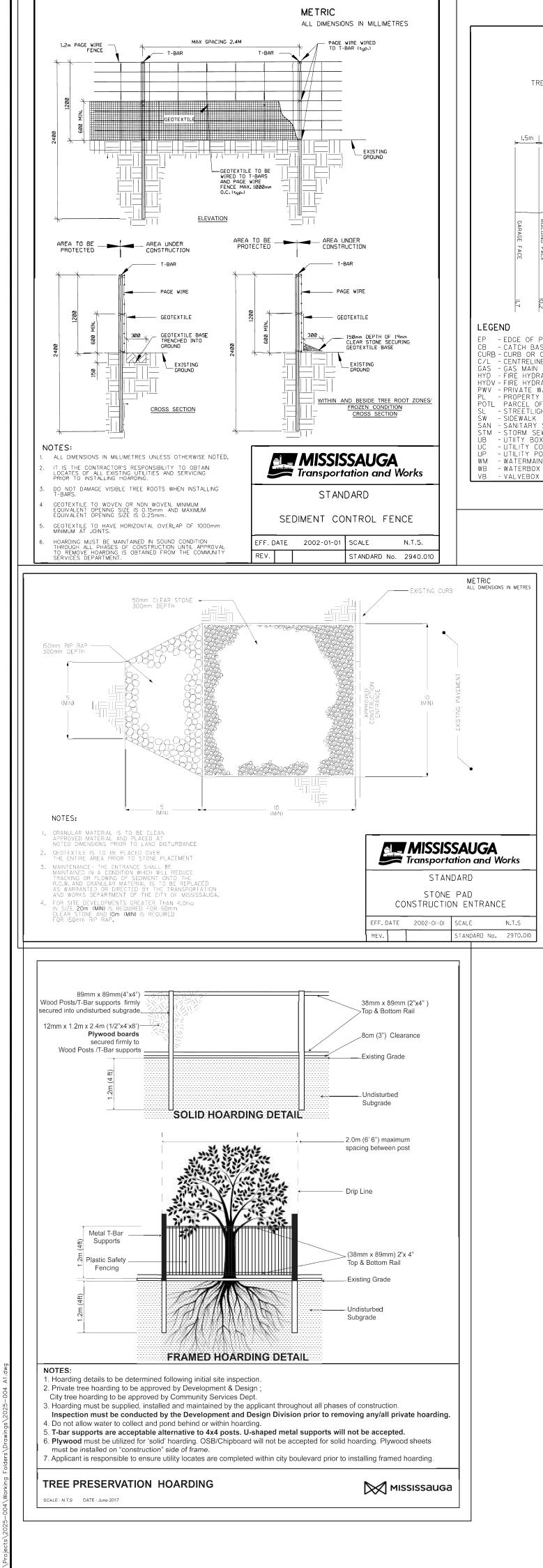


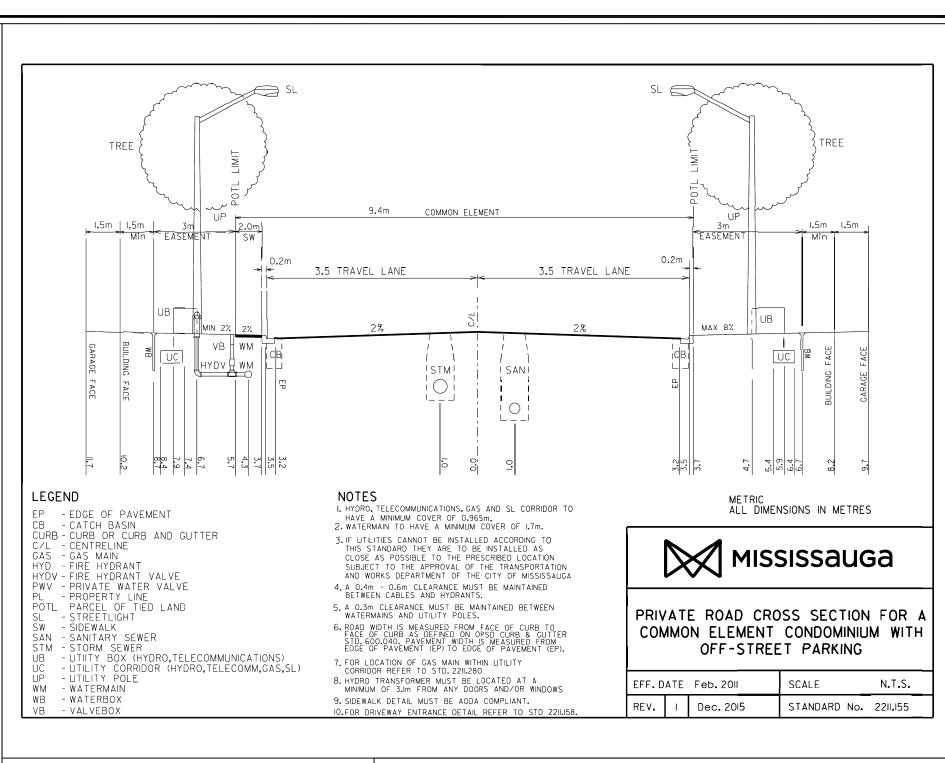
Civil Drawings

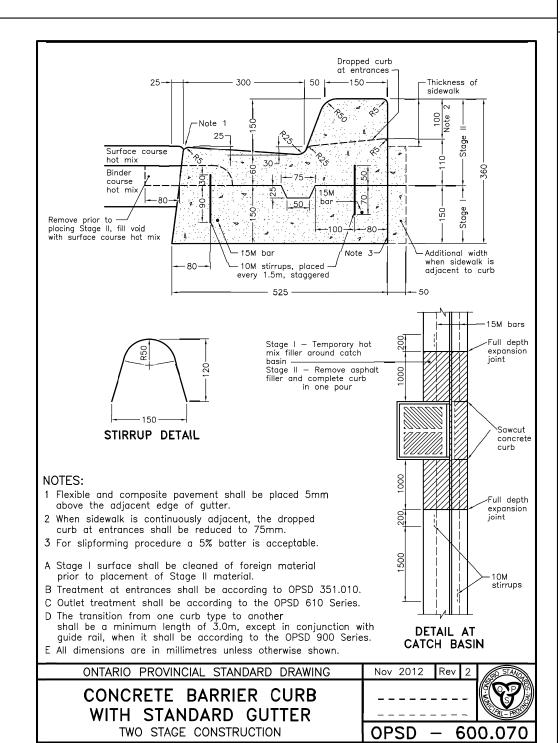


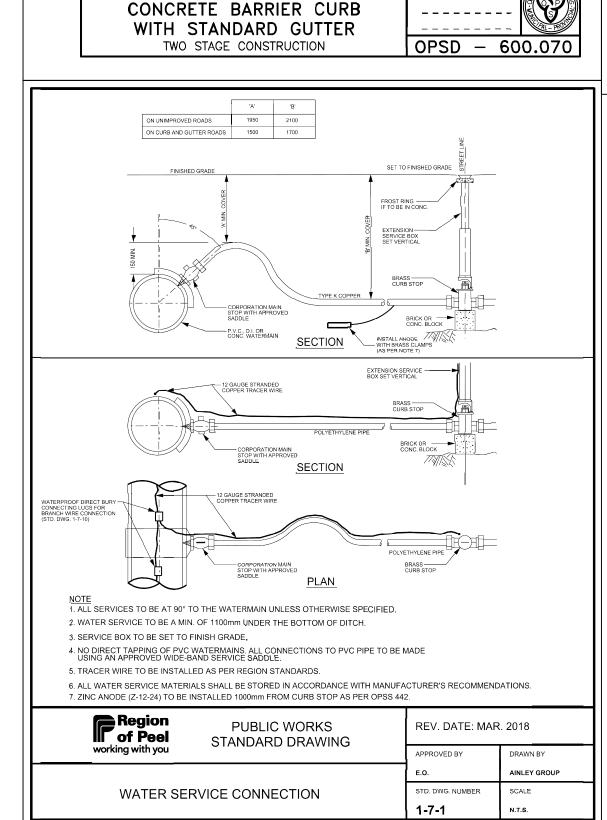


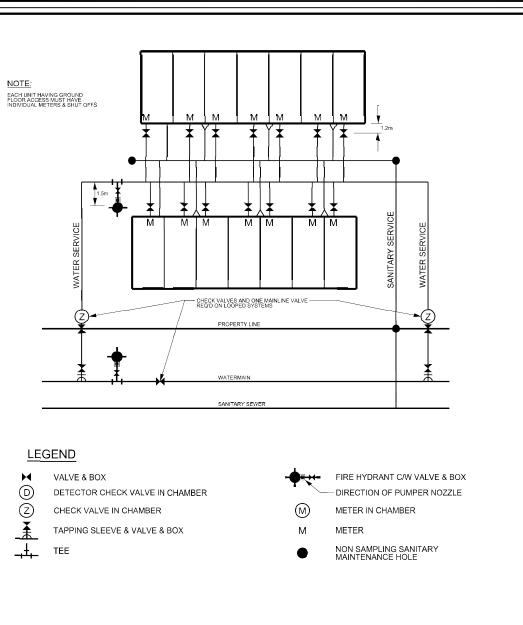




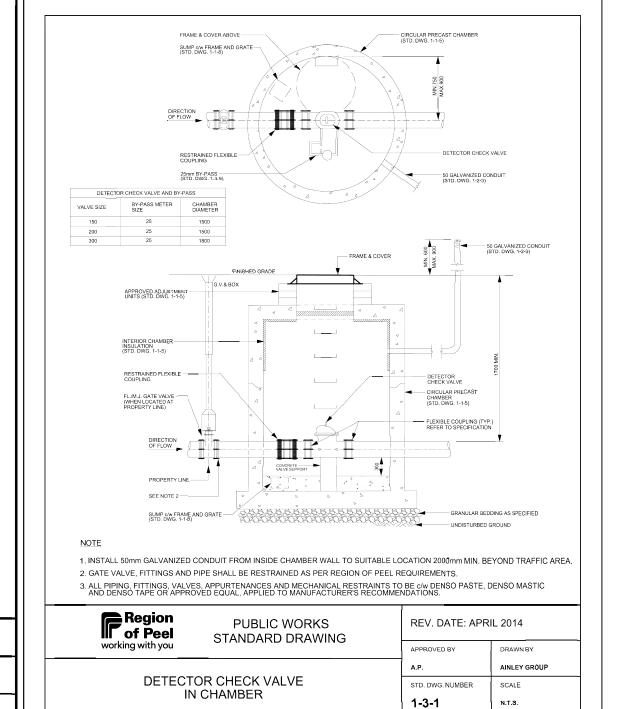


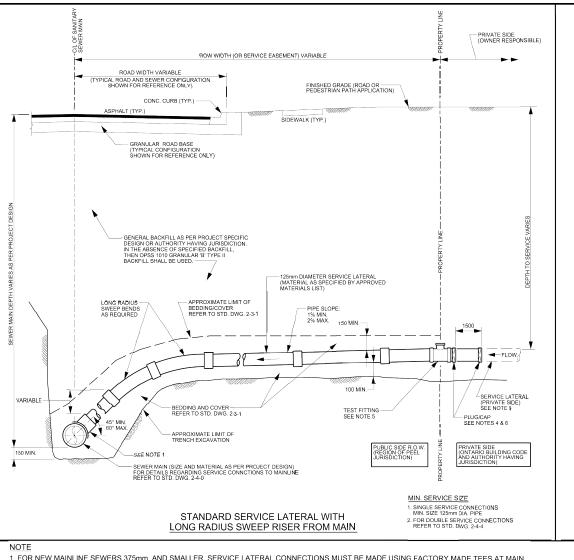


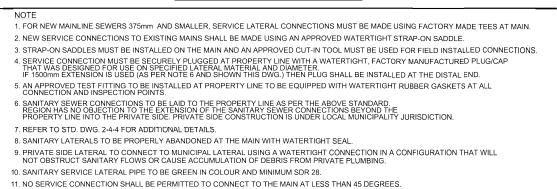




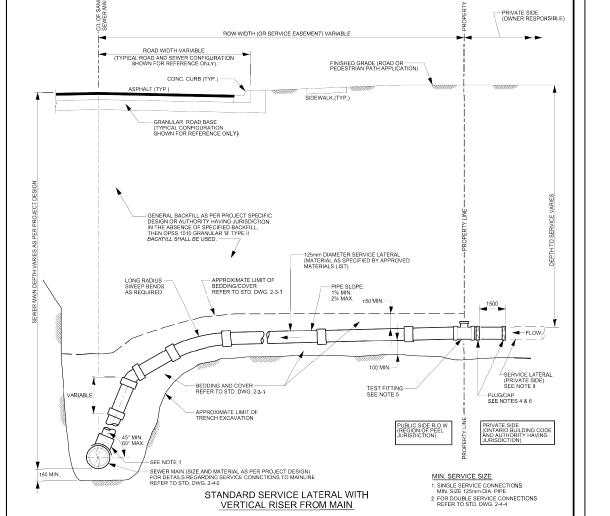
PUBLIC WORKS Working for you STANDARD DRAWING	REV. DATE: NOVEMBER 2011				
Working for you	APPROVED BY	DRAWN BY			
	A.P.	AINLEY GROUP			
SERVICING FOR TOWNHOUSE COMPLEX	STD. DWG. NUMBER	SCALE			
	1-8-2	N.T.S.			



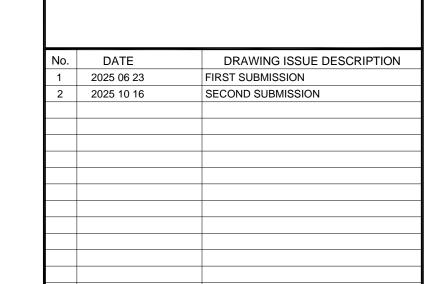




12. LATERAL CONNECTIONS UNLESS OTHERWISE SPECIFIED BY PROJECT ENGINEER SHALL BE MADE WITH INVERT OF LATERAL TO ENTER MAINLINE SEWER ABOVE SPRINGLINE AND BELOW TOP DEAD CENTRE.



Region PUBLIC WORKS		REV. DATE: AUGUST 2020			
of Peel STANDARD DRAWING	STANDARD DRAWING				
vorking with you					
SERVICE CONNECTIONS FOR FLEXIBLE PIPE		A.P.	AINLEY GROUP		
(SINGLE RESIDENTIAL DWELLING	STD. DWG. NUMBER	SCALE			
NCLUDING SEMI-DETACHED)	2-4-2	N.T.S.			



PROJECT SITE

LEGAL AND TOPOGRAPHICAL SURVEY PROVIDED BY:

SCHAEFFER DZALDOV BENNETT LTD.

JOB NO. 15–155–01, DATED JULY 21, 2015.

SITE BENCHMARK: ELEVATIONS SHOWN HEREON ARE REFERRED TO CITY OF MISSISSAUGA BENCHMARK No. 970, HAVING A





# KINGRIDGE

OWNER INFO:
NAME: DAN MARION
E-MAIL: dan@kingridgedevelopments.ca
MAIL ADDRESS: 1660 NORTH SERVICE Rd. EAST, SUITE 10
OAKVILLE ON L6H 7G3

MAIL ADDRESS: 1660 NORTH SERVICE Rd. EAST, SUITE 109-B
OAKVILLE ON L6H 7G3
PHONE: 416-277-7466

PROJECT:
THORNY BRAE TOWNHOUSE DEVELOPMENT

DETAILS PLAN

1775 THORNY BRAE PLACE MISSISSAUGA

ONTARIO

DRAWN BY:	CHECKED BY:	JOB CAPTAIN:
BN	MLS	JB
SCALE:	PROJECT NO.:	SHEET NO.:
-	2025-004	
CURRENT ISSUE:	CURRENT REV:	-  CV-4
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Appendix A

Storm Sewer Design Sheet



#### MGM CONSULTING Inc. STORM SEWER DESIGN SHEET

#### 1775 Thorny Brae Place, Mississauga, ON.

By: AB Date: October 2025

Location				Areas A * C					Rain	fall	Flow	Sewer Design						
Manhole	Invert	Manhole	Invert	Area	Cumulative	Weighted	Incremental	Cumulative	Time	Intensity		Pipe	Slope	Max. Flow	Max Velocity	Length	Time in	Pipe
from		to			Area	Coefficent	A * C	A * C		l10	Q	Size		Q max	V max		Section	Capacity
	m.		m.	ha	ha	С			min	mm/hr.	cms	mm.	%	cms	m./sec.	m.	min.	% full
CBMH12		MH11		0.121	0.121	0.83	0.101	0.101	10.0	124.8	0.035	300	0.50	0.068	0.97	11.9	0.20	51
MH11		MH10		0.000	0.121		0.000	0.101	10.2	123.4	0.035	300	0.50	0.068	0.97	29.4	0.51	50
MH10		MH9		0.010	0.131	0.58	0.006	0.106	10.7	120.2	0.036	300	0.50	0.068	0.97	6.4	0.11	52
MH9		MH8		0.244	0.375	0.68	0.166	0.272	10.8	119.6	0.091	375	0.50	0.124	1.12	22.0	0.33	73
MH8		MH7		0.093	0.468	0.74	0.069	0.341	11.1	117.6	0.112	450	0.50	0.202	1.27	15.5	0.20	55
MH7		MH6		0.096	0.564	0.69	0.067	0.408	11.4	116.5	0.132	450	0.50	0.202	1.27	9.4	0.12	65
MH18		MH6		0.104	0.104	0.77	0.081	0.081	10.0	124.8	0.028	300	0.50	0.068	0.97	45.7	0.79	41
MH6		MH5		0.000	0.668	0.00	0.000	0.488	11.5	115.8	0.157	450	0.50	0.202	1.27	17.5	0.23	78
MH17		MH16		0.131	0.131	0.77	0.100	0.100	10.0	124.8	0.035	300	0.50	0.068	0.97	57.0	0.98	51
MH16		MH5		0.067	0.198	0.76	0.051	0.151	11.0	118.6	0.050	300	0.50	0.068	0.97	17.6	0.30	73
IVIITIO		IVII IJ		0.007	0.190	0.70	0.031	0.131	11.0	110.0	0.030	300	0.50	0.008	0.57	17.0	0.30	10
MH5		MH4		0.000	0.866	0.00	0.000	0.640	11.7	114.5	0.204	525	0.50	0.305	1.41	11.6	0.14	67
MH4		MH3		0.135	1.001	0.71	0.096	0.736	11.8	113.7	0.233	525	0.50	0.305	1.41	23.1	0.27	76
MH15		MH3		0.110	0.110	0.73	0.080	0.080	10.0	124.8	0.028	300	0.50	0.068	0.97	42.0	0.72	41
МНЗ		CBMH2		0.099	1.210	0.75	0.074	0.890	10.7	120.2	0.297	600	0.50	0.435	1.54	16.6	0.18	68
MH13		MH14		0.060	0.060	0.74	0.044	0.044	10.9	119.1	0.015	300	0.50	0.068	0.97	30.2	0.52	21
MH14		CBMH2		0.000	0.060	0.00	0.000	0.044	11.4	116.1	0.014	300	0.50	0.068	0.97	13.5	0.23	21
СВМН2		CBMH1		0.083	1.354	0.79	0.065	1.000	10.9	119.1	0.331	600	2.00	0.869	3.08	11.2	0.06	38
СВМН1		OGS		0.112	1.526	0.28	0.032	1.076	11.4	116.1	0.347	600	2.00	0.869	3.08	8.5	0.05	40
OGS		EX. MH		0.000	1.526	0.00	0.000	1.076	11.7	114.8	0.343	600	2.00	0.869	3.08	6.2	0.03	39

n = 0.013

Note: Calculated as per City's 10yr storm IDF curve.



Appendix B

Oil and Grit Separator and Treatment Train Calculations



## **Hydroworks Sizing Summary**

# Thorny Brae Townhouse Development Mississauga

06-19-2025

Recommended Size: HydroDome HD 8

**Hydroworks Sizing Program Version 5.8.5** 

A HydroDome HD 8 is recommended to provide 80 % annual TSS removal based on a drainage area of 1.526 (ha) with an imperviousness of 69 % and Toronto Central, Ontario rainfall for the ETV particle size distribution.

The recommended HydroDome HD 8 treats 100 % of the annual runoff and provides 80 % annual TSS removal for the Toronto Central rainfall records and ETV particle size distribution.

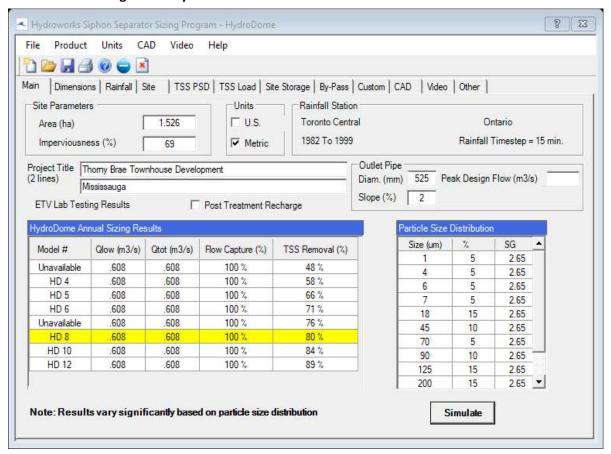
The HydroDome has a siphon which creates a discontinuity in headloss. Since a peak flow was not specified, headloss was calculated using the full pipe flow of .61 (m3/s) for the given 525 (mm) pipe diameter at 2% slope. The headloss was calculated to be 494 (mm) above the crown of the 525 (mm) outlet pipe.

This summary report provides the main parameters that were used for sizing. These parameters are shown on the summary tables and graphs provided in this report.

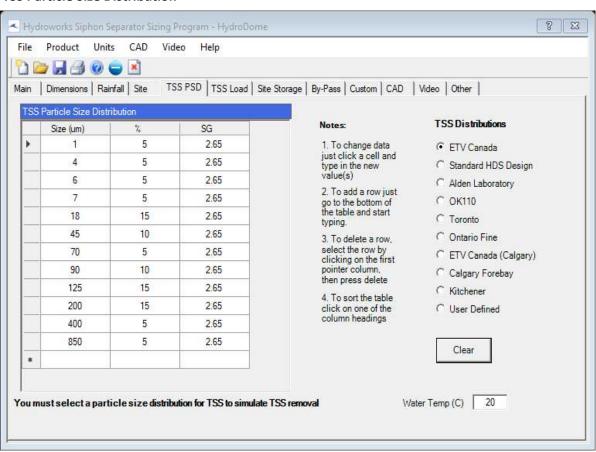
If you have any questions regarding this sizing summary please do not hesitate to contact Hydroworks at 888-290-7900 or email us at support@hydroworks.com.

The sizing program is for sizing purposes only and does not address any site specific parameters such as hydraulic gradeline, tailwater submergence, groundwater, soils bearing capacity, etc. Headloss calculations are not a hydraulic gradeline calculation since this requires a starting water level and an analysis of the entire system downstream of the HydroDome.

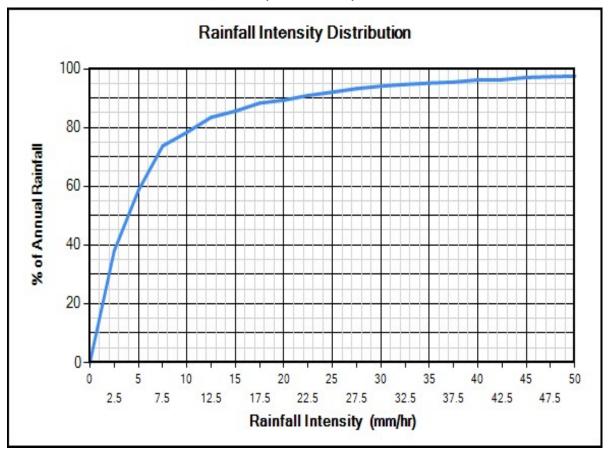
#### **TSS Removal Sizing Summary**



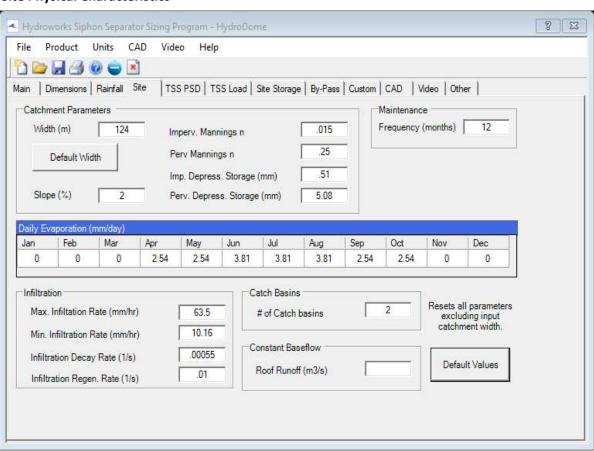
#### **TSS Particle Size Distribution**



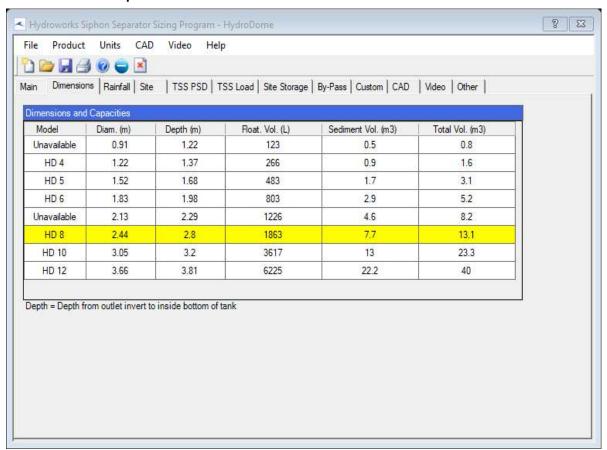
#### Rainfall Station - Toronto Central, Ontario (1982 To 1999)



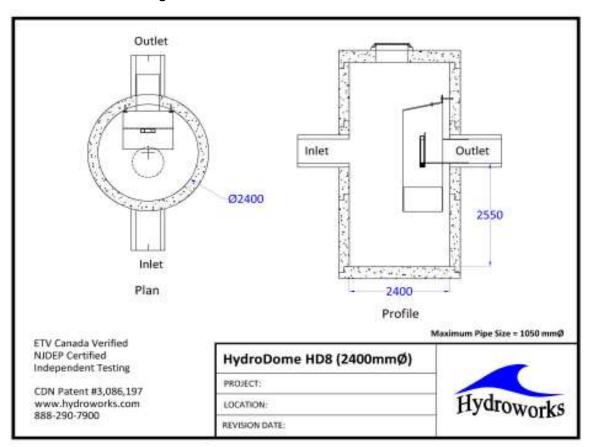
#### **Site Physical Characteristics**



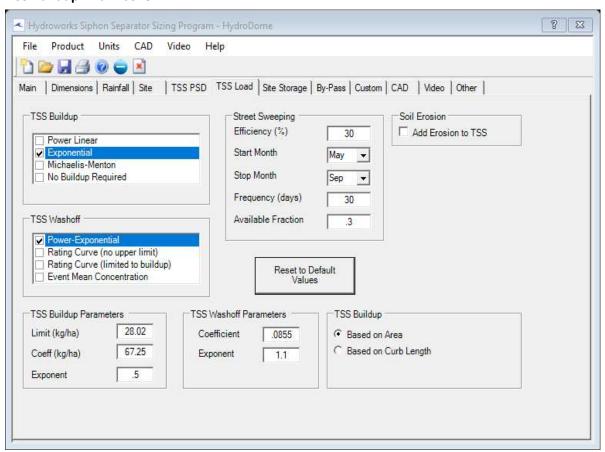
#### **Dimensions And Capacities**



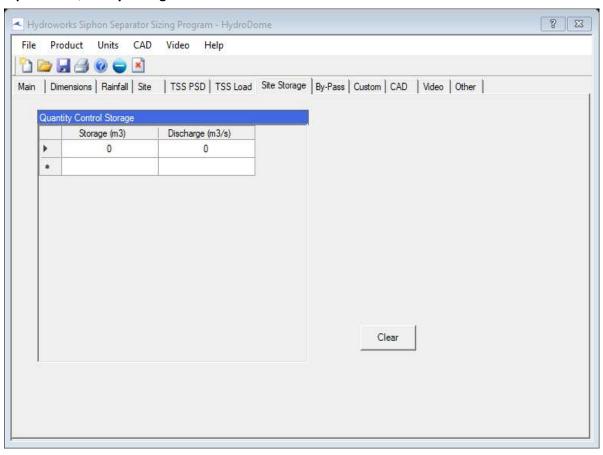
#### **Generic HD 8 CAD Drawing**



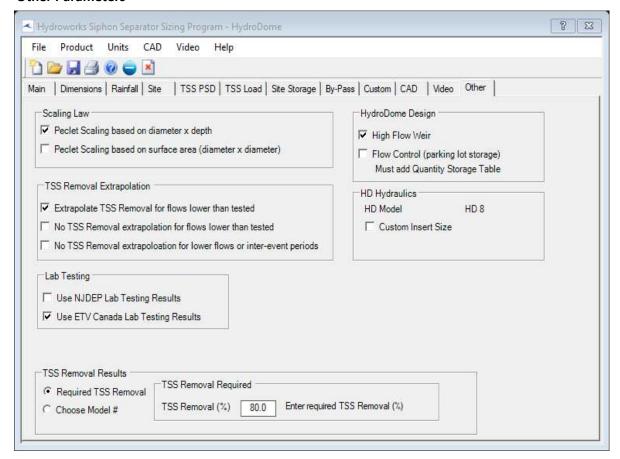
#### **TSS Buildup And Washoff**



#### **Upstream Quantity Storage**



#### **Other Parameters**



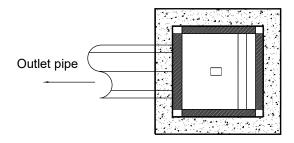
#### **Flagged Issues**

If there is underground detention storage upstream of the HydroDome please contact Hydroworks to ensure it has been modeled correctly.

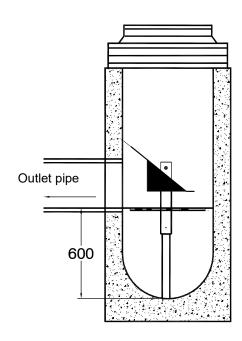
Hydroworks Sizing Program - Version 5.8.5 Copyright Hydroworks, LLC, 2024 1-800-290-7900 www.hydroworks.com

### **Notes**

- 1 Recommended depth t/g invert = 1.2m Maximum depth t/g - invert = 2.4m
- 1. CB Shield to be installed in non frozen conditions.
- 2. The frame and cover should be well aligned with the catchbasin.
- 3. The sump must be clean before installation
- 4. The grate is at the same elevation as pipe invert.
- 5. Pipes must be cut flush with inside walls



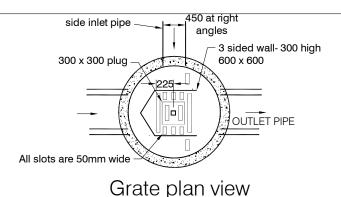
Top view

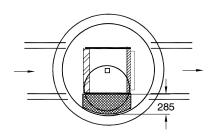


Profile view

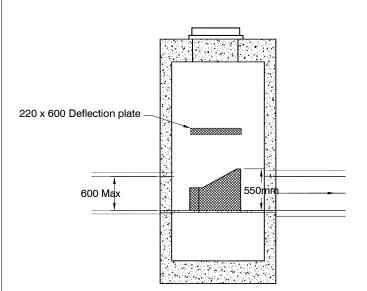


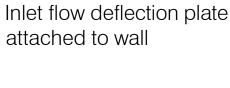
600 x 600 CB CB Shield (600mm Sump)





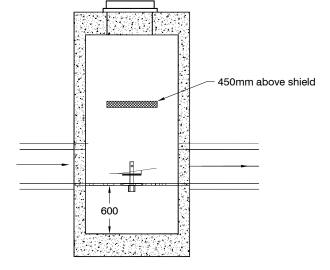
Standard Flat Cap







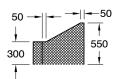
Shallow Sloped plate with flexible skirt.



600

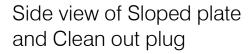


Deflection plate Detail



Deflection wall dimensions

Side view of Deflection wall and Deflection Plate (above)





CBMH Shield-1200mm -Generic Drawing



Date: June 24, 2025

Project Number: 2025-004

#### **Treatment Train Performance Calculation**

#### **Combined TSS Removal Calculations for Treatment Options in Series (Point Source Inlet Flows)**

R= A + B - [(AxB)/100] A= OGS HydroDome

B= CB Shield

R= Total TSS Removal Rate

A= First Removal (upstream)

B= Second Removal (downstream)

A = 50 %

B = 60 %

Total TSS Removal

Rate = 80 %



Appendix C

**Runoff Volume Reduction Calculations** 

#### **Water Balance**

### **Runoff Volume Reduction**

On-site stormwater retention is achieved equivelant to capturing 5mm over the impervious site area.

Description	Area (m²)	Ruired Depth (m)	Volume (m³)	
Impervious Surfaces Total	10470 10470	5	52.4 52.4	_
Equivalent Depth of the Site A	Area =		5.0	mm.
Infiltration Rate (mm/hr) Depth of Tank (mm)	15 660	(assumed	d for native soils)	
Infiltration Time (hours)	44.0			
Infiltration Trench Storage	Sizing			
Area of Infiltration Tank Depth of Tank Porosity		84.5 660.0 97.0	m² mm -	
Available Volume for Infiltration	on	54.1	$m^3$	



Appendix D

Sanitary Sewer Design Sheet



# THE REGIONAL MUNICIPALITY OF PEEL SANITARY SEWER DESIGN SHEET

Project No.			2025-004	
Subdivision	Thony Brae Place			
Date:			15-Oct-25	
Des. By:	BN	Chk. By:	AK	

Development Type	Persons/Unit	Daily per Capita Flow (l/cap/day)	Infiltration (l/s/Ha)
Residenttial (Townhouse)	3.4	290	0.26

		Tr	ributary A	rea Hec	tare	Pop	oulation T	ributary		Average	Average							SEW	ER			PIPE		·
			Increment	t	Total	In	crement		Total	Increment	Total	Peaking	Max.	Infiltration	Max. Flow			Q	Capacity	V m/S				l '
		Res.	Comm.	Ind.		Res. Units	Comm.	Ind.																1
		ha	ha	ha	ha					L/s	L/s	Factor	L/s	L/s	L/s	mm.	%	L/s	%	Full Flow	71	n	Class	REMARKS
MHA 1	MHA 2	0.197			0.197	18			61	0.205	0.205	4.000	0.822	0.051	0.873	250	0.50	42.067	2.1	0.86	PVC	0.013	SDR35	
MHA 2	MHA 3	0.035			0.232	0					0.205	4.000	0.000	0.060	0.933	250	0.50	42.067	2.2	0.86	PVC	0.013	SDR35	Conveyance
MHA 3	MHA 4	0.053			0.285	0					0.205	4.000	0.000	0.074	1.007	250	0.50	42.067	2.4	0.86	PVC	0.013	SDR35	Conveyance
MHA 5	MHA 4	0.209			0.209	18			61	0.205	0.205	4.000	0.822	0.054	0.876	250	0.50	42.067	2.1	0.86	PVC	0.013	SDR35	
MHA 4	MHA 6	0.032			0.526	0			122		0.411	4.000	1.643	0.137	1.883	250	0.50	42.067	4.5	0.86	PVC	0.013	SDR35	Conveyance
MHA 7	MHA 8	0.118			0.118	9			31	0.103	0.103	4.000	0.411	0.031	0.442	250	0.50	42.067	1.0	0.86	PVC	0.013	SDR35	<b></b>
V 47 4 4 4	MHA 8	0.170			0.207	1.5	-			0.171	0.171	4.000	0.505	0.077	0.762	250	0.50	12.067	1.0	0.86	PVC	0.010	appas	
MHA 14	MHA 8	0.179			0.297	15			51	0.171	0.171	4.000	0.685	0.077	0.762	250	0.50	42.067	1.8	0.86	PVC	0.013	SDR35	<del></del>
MHA 8	MHA 6	0.027			0.324	24	-		82		0.274	4.000	1.096	0.084	1.203	250	0.50	42.067	2.9	0.86	PVC	0.013	SDR35	Conveyance
WITA 6	WITA	0.027			0.324	24			62		0.274	4.000	1.090	0.084	1.203	230	0.50	42.007	2.7	0.80	1 VC	0.013	SDKJJ	Conveyance
MHA 6	MHA 9	0.021			1.156	60			204		0.685	4.000	2.739	0.301	3.039	250	0.50	42.067	7.2	0.86	PVC	0.013	SDR35	Conveyance
		0.021			1.150	- 00			201		0.005	1.000	2.757	0.501	5.057	250	0.50	12.007	7.2	0.00	.,.	0.015	DDICOS	conveyance
MHA 10	MHA 9	0.190			0.190	18			61	0.205	0.205	4.000	0.822	0.049	0.871	250	0.50	42.067	2.1	0.86	PVC	0.013	SDR35	
MHA 9	EX. SAN. MH	0.046			1.392	78			265		0.890	4.000	3.561	0.362	4.272	250	0.50	42.067	10.2	0.86	PVC	0.013	SDR35	Conveyance
EX. SAN. MH	MHA 12	0.073			1.465	78			265		0.890	4.000	3.561	0.381	4.653	250	0.50	42.067	11.1	0.86	PVC	0.013	SDR35	Conveyance
																								,
MHA 11	MHA 12	0.211			0.211	13			44	0.148	0.148	4.000	0.593	0.055	0.648	250	0.50	42.067	1.5	0.86	PVC	0.013	SDR35	
MHA 15	MHA 13	0.107			0.107	4			14	0.046	0.046	4.000	0.822	0.028	0.849	250	0.50	42.067	2.0	0.86	PVC	0.013	SDR35	
MHA 13	MHA 12	0.028			0.135				14		0.046	4.000	0.822	0.035	0.885	250	0.50	42.067	2.1	0.86	PVC	0.013	SDR35	Conveyance
MHA 12	EX SAN MH				1.53	95			323		1.084	4.000	4.337	0.397	4.733	250	0.51	42.485	11.1	0.87	PVC	0.013	SDR35	Conveyance



Appendix E

Fire Flow and Water Demand Calculations

### Thorny Brae Townhouse Development 1775 Thorny Brae Place, Mississauga Ontario

Date: September 2025 Project No.: 2025-004

#### Fire Flow Calculation

Thorny Brae Townhouse Development

The FUS requires that a minimum water supply source 'F' be provided at 140 kPa The min flow 'F' can be calculated as such:

F=220C√A

where:

F- Required fire flow in L/min

C- Coefficient related to construction

A- Total area in sq.m

C = 1.5 (Wood frame construction)

For non-combustible construction, the area shall be a total of all floors (excluding basements at least 50 percent below grade) in the building being considered.

 $A = 2051.7 \text{ m}^2$  (Block 2, Largest Townhouse Block in Development)

Therefore,

F= 14947.58 L/min

= 15000 L/min (rounded to nearest 1000)

Reduction Factors:

F'=F\*f1\*f2

where:

f1- Occupancy factor

Limited combustion, f1 = 15%

Therefore, the reduction due to low hazard occupancy = 2250 I/min.

and F = 12750 I/min

f2- Sprinkler protection factor

Based on fully automated sprinkler system, maximum reduction = 0%

Reduction 0 L/min

Exposure Factors:

F'' = F'\*f3

### Thorny Brae Townhouse Development 1775 Thorny Brae Place, Mississauga Ontario

Date: September 2025 Project No.: 2025-004

#### where:

f3- Exposure factor not to exceed 75%

Separation between subject building and other structures, and associated charges are as follows:

	Distance (m)	Charge	_
North Side	>30	0%	
South Side	>30	0%	
East Side	20	15%	
West Side	15	15%	
Total		30%	
The total increase for e	exposures is	30%	
and the increase due to	•	3825	
The resulting required	minimum flow, F =	16575	l/min

Therefore a minimum flow of approximately 17000 I/min (283 I/sec) must be available at the nearest hydrant with a minimum pressue of 140 kPa.



Appendix F

Hydrant Flow Test



Kingridge Developments

# 1786 Polaris Way, City of Mississauga

Functional Servicing and Stormwater Management Report (FSR/SWM)

March 26, 2025

**ARCADIS** 

NOTE: Hydrants tested according to NFPA 291: Recommended Practice for Fire Flow Testing and Marking of Hydrants

 Date of Testing
 14-Jun-2024

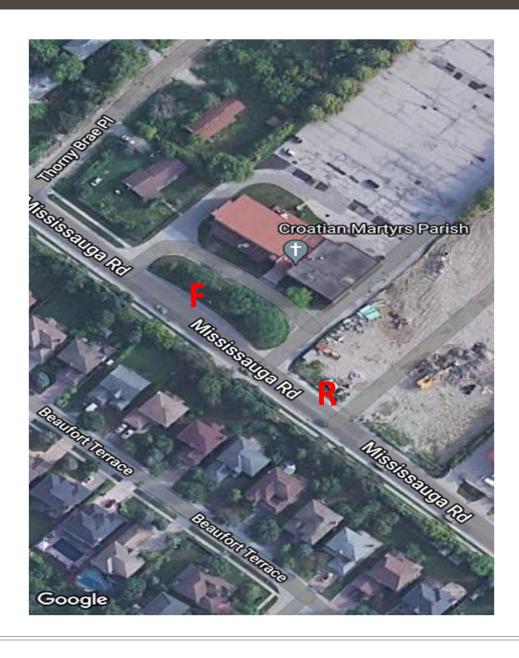
 Project Number:
 145121

 Test ID
 H2024-028

Site Location / Address: 1786 Polaris Rd, Miss

Region / MunicipalityPeel RegionHydrants Opened By:Peel RegionTested by:James W

# HYDRANT TEST LOCATION - RESIDUAL HYDRANT=R, FLOW HYDRANT=F (NORTH AT TOP)



#### **Test Data**

Time of Test 11:11 AM

Pipe Size (mm) -

Flow Hydrant Test Location (description) 4601 Mississauga Rd Residual Hydrant Test Location (description) 4587 Mississauga Rd

Static Pressure (PSIG) 9

### Q1 Test Data (1 Orifice)

# OUTLETS	ORIFICE SIZE(IN)	PITOT PRESSURE(PSIG)	FLOW(USGPM)	RESIDUAL PRESSURE(PSIG)
1	2.5	60	1300	88

### QT Test Data (2 Orifices)

# OUTLETS	ORIFICE SIZE(IN)	PITOT PRESSURE(PSIG)	FLOW(USGPM)	RESIDUAL PRESSURE(PSIG)
2	2.5	40	2122	86

#### Calculations

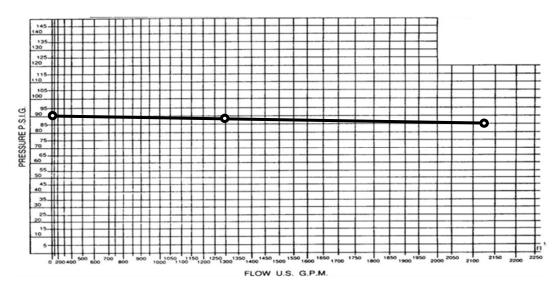
......p- pitot reading (psig)

**Q1 - 1 Orifice(s)** Q1=  $(29.83)(0.9)(2.5)^2 \sqrt{60}=1300$ 

**QT - 2 Orifice(s)** QT=  $2(29.83)(0.9)(2.5)^2 \sqrt{40}=2122$ 

Static Pressure (PSIG) 90

#### **Test Results Plot**



2024-06-14 - H2024-028 PAGE 2 OF 2

#### Appendix D.2 Estimated Available Pressure at Water Service Connection on Mississauga Road

ARCADIS

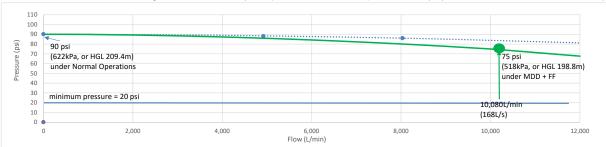
Project:	1786 Polaris Way, Mississauga	Proj.#	145121
Date:		2024-06-26	
Calc'ed by:		SK	

Hydrant Flow Test Results	
Flow Hydrant Test Location:	4587 Mississauga Rd
Residual Hydrant Test Location:	4601 Mississauga Rd
Main Size:	300mm Diameter Test Time: 11:11 AM
Test Date:	2024-06-14
Tested By:	Peel Region

Elev.(m) 146.0

**Number of Outlets Pilot Pressure Residual Pressure** Flow Flow **Estimated** Residual **Estimated** (US GPM) ressure\* (p 0 0 0 0 90 90 209.4 1 x 2.5" 60 1,300 4,921 88 88 208.0 2 x 2.5" 40 2,122 8,033 86 80 206.6

\*Estimated Residual Pressure: For a conservative design, it assumed that the residual pressure (at the maximum tested flow rate) would be reduced by 10 psi, which was used to estimate the available flow at 20 psi.



 $\textit{Where,} \qquad \textit{Q}_{\textit{R}} = \textit{Q}_{\textrm{T}} \bigg( \frac{\textit{P}_{\textrm{S}} - \textit{Pr}}{\textit{P}_{\textrm{S}} - \textit{Pt}} \bigg) ^{\texttt{A}} 0.54$ 

 $Q_r$  = Projected Flow Rate

 $Q_t$  = Flow Rate from Flow Test = 8033 L/min

P<sub>s</sub> = Static Pressure = 90 psi

P<sub>r</sub> = Desired System Pressure

 $P_t$  = Residual Presure inTest = 80 psi

Pressure Under Fire Suppression (P <sub>r1</sub> ) =	20.0	psi	
Calculated Flow Rate $(Q_{r1}) =$	22,974	L/min	
Pressure Under Normal Operation (P <sub>r2</sub> ) =	40.0	psi	
Calculated Flow Rate $(Q_{r2})$ =	19,157	L/min	

6,069 USGPM

383 L/s

5,061 USGPM 319 L/s