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RIP-RAP SIZING FOR EMERGENCY SPILLWAY OF TEMPORARY SEDIMENT BASIN 1

Project # 60549-001  
Date June 23, 2025  
Rip-rap sizing calculations based on procedures outlined in Chapter 5 of the MTO Drainage Manual.  
Outlet Channel Characteristics  
Flow Through Rip Rap Channel  $Q = 0.136 \text{ m}^3/\text{s}$   
Manning's  $n$  (rock rip rap  $D_{50}=300$ ) = 0.078  
NOTE: obtained using Rational Method with an intensity equal to a 5-yr Design Distribution of a 25mm storm.  
(As described in MOE-SWM Manual 4.)

RIP-RAP APRON HYDRAULIC CHARACTERISTICS

Consider a cross-section through the rip-rap apron immediately downstream of the overflow weir:  
Bottom width (m) = 5.0  
Long Slope (%) = 25.00%  
Side slope (H:V) = 3:1  
Manning's  $n$  = 0.078  
Flow rate (m<sup>3</sup>/s) = 0.136  
Analysis results from Flowmaster:  
Depth of flow (m) = 0.038  
Flow velocity (m/s) = 0.716  
Area of flow (m<sup>2</sup>) = 0.20  
Wetted Perim. (m) = 5.10  
Hydraulic Radius (m) = 0.037

DETERMINE SHEAR STRESS ON CHANNEL BED AND BANK

Unit weight of water ( $\gamma$ ) N/m<sup>3</sup> = 9810  
Mean boundary shear stress ( $\tau_b$ ):  
 $\tau_b = \gamma \cdot R \cdot S = 9810 \times 0.037 \times (25.00/100) = 91 \text{ N/m}^2$   
Shear stress on channel bottom ( $\tau_b$ ):  
 $\tau_b = K_b \cdot \tau_b = 1.30 \times 91 = 118 \text{ N/m}^2$  (governs)  
Shear stress on channel bank ( $\tau_s$ ):  
 $\tau_s = K_s \cdot \tau_b = 1.15 \times 91 = 104 \text{ N/m}^2$   
Note:  $K_b$  &  $K_s$  from Design Charts 2.11 and 2.12 of the MTO Drainage Manual

DETERMINE RIP-RAP SIZING

Based on Equation 5.31 (MTO drainage manual), the critical shear stress on a particle on the channel bed can be determined by:  
 $\tau_{bc} = 0.0642 \times D_{50} \times 9.81$   
For  $D_{50} = 300 \text{ mm} \rightarrow \tau_{bc} = 0.0642 \times 300 \times 9.81 = 189 \text{ N/m}^2$  OK  
Based on Equation 5.31 (MTO drainage manual), the critical shear stress on a particle on the channel sides can be determined by:  
 $\tau_{sc} = K_{sc} \cdot \tau_{bc}$   
 $K_{sc} =$  (Design Chart 2.14)  
Angle of Repose = 42.5 degrees (per Design Chart 2.13)  
Degree of Side Slope = 3:1  
= 18.4 degrees  
 $K_{sc} = 0.90$  (per Design Chart 2.14)  
For  $D_{50} = 150 \text{ mm} \rightarrow \tau_{sc} = 0.90 \times 189 = 170 \text{ N/m}^2$  OK  
Therefore, use  $D_{50} = 300 \text{ mm}$  (Rip Rap size to be 300mm)

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RIP-RAP SIZING FOR EMERGENCY SPILLWAY OF TEMPORARY SEDIMENT BASIN 2

Project # 60549-001  
Date June 23, 2025  
Rip-rap sizing calculations based on procedures outlined in Chapter 5 of the MTO Drainage Manual.  
Outlet Channel Characteristics  
Flow Through Rip Rap Channel  $Q = 0.261 \text{ m}^3/\text{s}$  100-yr ex. Flow (2.65 ha, Rational Method)  
Manning's  $n$  (rock rip rap  $D_{50}=300$ ) = 0.078

RIP-RAP APRON HYDRAULIC CHARACTERISTICS

Consider a cross-section through the rip-rap apron immediately downstream of the overflow weir:  
Bottom width (m) = 5.0  
Long Slope (%) = 25.00%  
Side slope (H:V) = 3:1  
Manning's  $n$  = 0.078  
Flow rate (m<sup>3</sup>/s) = 0.261  
Analysis results from Flowmaster:  
Depth of flow (m) = 0.056  
Flow velocity (m/s) = 0.927  
Area of flow (m<sup>2</sup>) = 0.30  
Wetted Perim. (m) = 5.10  
Hydraulic Radius (m) = 0.055

DETERMINE SHEAR STRESS ON CHANNEL BED AND BANK

Unit weight of water ( $\gamma$ ) N/m<sup>3</sup> = 9810  
Mean boundary shear stress ( $\tau_b$ ):  
 $\tau_b = \gamma \cdot R \cdot S = 9810 \times 0.055 \times (25.00/100) = 135 \text{ N/m}^2$   
Shear stress on channel bottom ( $\tau_b$ ):  
 $\tau_b = K_b \cdot \tau_b = 1.30 \times 135 = 175 \text{ N/m}^2$  (governs)  
Shear stress on channel bank ( $\tau_s$ ):  
 $\tau_s = K_s \cdot \tau_b = 1.15 \times 135 = 155 \text{ N/m}^2$   
Note:  $K_b$  &  $K_s$  from Design Charts 2.11 and 2.12 of the MTO Drainage Manual

DETERMINE RIP-RAP SIZING

Based on Equation 5.31 (MTO drainage manual), the critical shear stress on a particle on the channel bed can be determined by:  
 $\tau_{bc} = 0.0642 \times D_{50} \times 9.81$   
For  $D_{50} = 300 \text{ mm} \rightarrow \tau_{bc} = 0.0642 \times 300 \times 9.81 = 189 \text{ N/m}^2$  OK  
Based on Equation 5.31 (MTO drainage manual), the critical shear stress on a particle on the channel sides can be determined by:  
 $\tau_{sc} = K_{sc} \cdot \tau_{bc}$   
 $K_{sc} =$  (Design Chart 2.14)  
Angle of Repose = 42.5 degrees (per Design Chart 2.13)  
Degree of Side Slope = 3:1  
= 18.4 degrees  
 $K_{sc} = 0.90$  (per Design Chart 2.14)  
For  $D_{50} = 150 \text{ mm} \rightarrow \tau_{sc} = 0.90 \times 189 = 170 \text{ N/m}^2$  OK  
Therefore, use  $D_{50} = 300 \text{ mm}$  (Rip Rap size to be 300mm)

Worksheet for Trapezoidal Channel -SB-1

Project Description  
Friction Method Manning  
Solve For Formula  
Normal Depth  
Input Data  
Roughness Coefficient 0.078  
Channel Slope 0.250 m/m  
Left Side Slope 0.330 H:V  
Right Side Slope 0.330 H:V  
Bottom Width 5.000 m  
Discharge 0.136 m<sup>3</sup>/s  
Results  
Normal Depth 0.038 m  
Flow Area 0.2 m<sup>2</sup>  
Wetted Perimeter 5.1 m  
Hydraulic Radius 0.037 m  
Top Width 5.025 m  
Critical Depth 0.042 m  
Critical Slope 0.174 m/m  
Velocity 0.716 m/s  
Flow Head 0.026 m  
Specific Energy 0.084 m  
Froude Number 1.177  
Flow Type Supercritical  
GVF Input Data  
Downstream Depth 0.000 m  
Length 0.0 m  
Number Of Steps 0  
GVF Output Data  
Upstream Depth 0.000 m  
Profile Description  
Profile Headloss 0.000 ft  
Downstream Velocity Infinity m/s  
Upstream Velocity Infinity m/s  
Normal Depth 0.056 m  
Critical Depth 0.042 m  
Channel Slope 0.250 m/m  
Critical Slope 0.174 m/m  
sediment basin spillway fnb 6/23/2025 Bentley Systems, Inc. Haestad Methods Solution Center 37 Simon Company Drive Suite 200 W Watertown, CT 06095 USA +1-203-755-1666 FlowMaster 10/03/2025 Page 1 of 1

Worksheet for Trapezoidal Channel -SB-2

Project Description  
Friction Method Manning  
Solve For Formula  
Normal Depth  
Input Data  
Roughness Coefficient 0.078  
Channel Slope 0.250 m/m  
Left Side Slope 0.330 H:V  
Right Side Slope 0.330 H:V  
Bottom Width 5.000 m  
Discharge 0.261 m<sup>3</sup>/s  
Results  
Normal Depth 0.056 m  
Flow Area 0.3 m<sup>2</sup>  
Wetted Perimeter 5.1 m  
Hydraulic Radius 0.055 m  
Top Width 5.037 m  
Critical Depth 0.045 m  
Critical Slope 0.152 m/m  
Velocity 0.927 m/s  
Flow Head 0.044 m  
Specific Energy 0.100 m  
Froude Number 1.253  
Flow Type Supercritical  
GVF Input Data  
Downstream Depth 0.000 m  
Length 0.0 m  
Number Of Steps 0  
GVF Output Data  
Upstream Depth 0.000 m  
Profile Description  
Profile Headloss 0.000 ft  
Downstream Velocity Infinity m/s  
Upstream Velocity Infinity m/s  
Normal Depth 0.056 m  
Critical Depth 0.045 m  
Channel Slope 0.250 m/m  
Critical Slope 0.152 m/m  
sediment basin spillway fnb 6/23/2025 Bentley Systems, Inc. Haestad Methods Solution Center 37 Simon Company Drive Suite 200 W Watertown, CT 06095 USA +1-203-755-1666 FlowMaster 10/03/2025 Page 1 of 1

CITY OF MISSISSAUGA

KEY PLAN N.T.S.

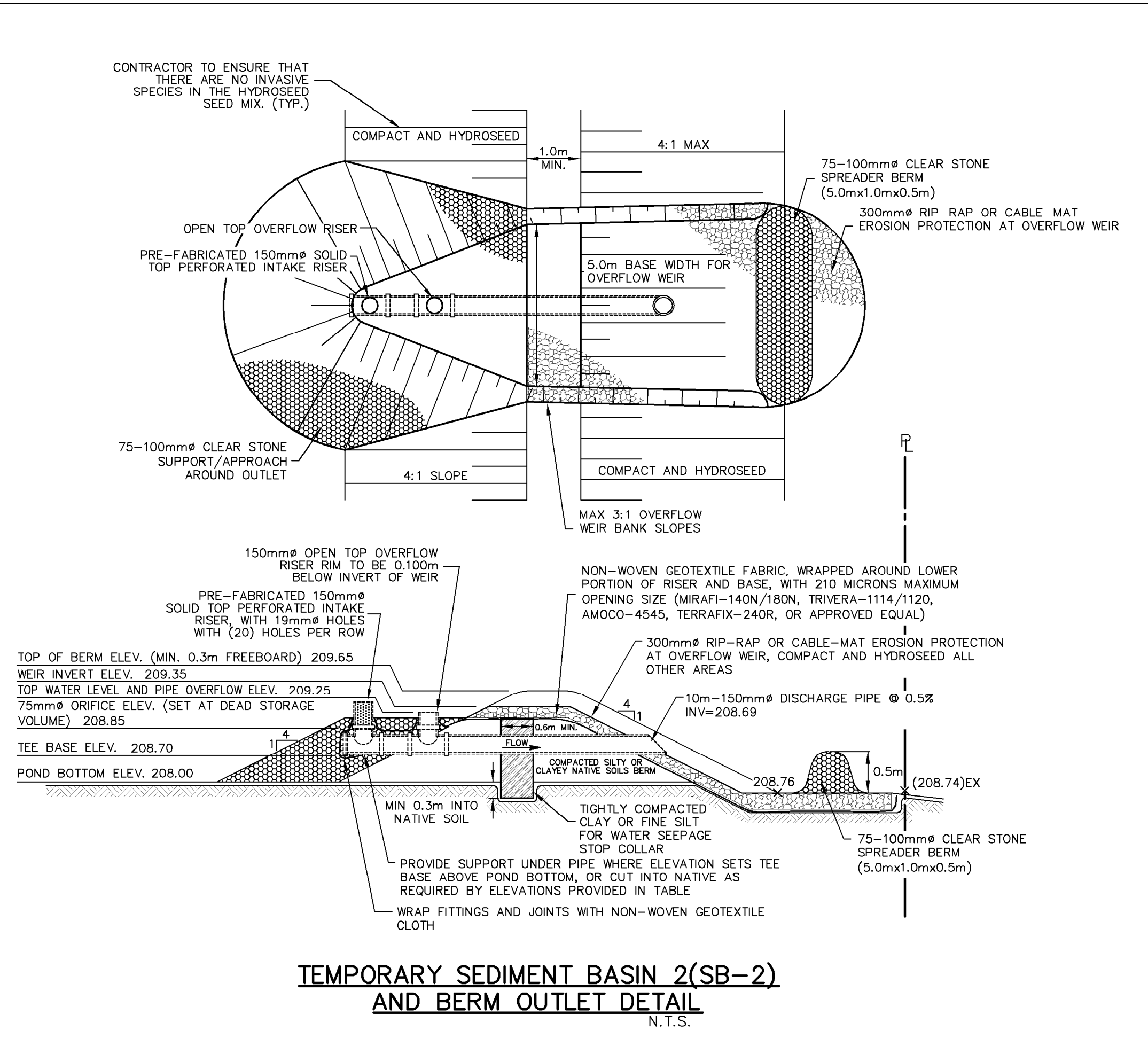
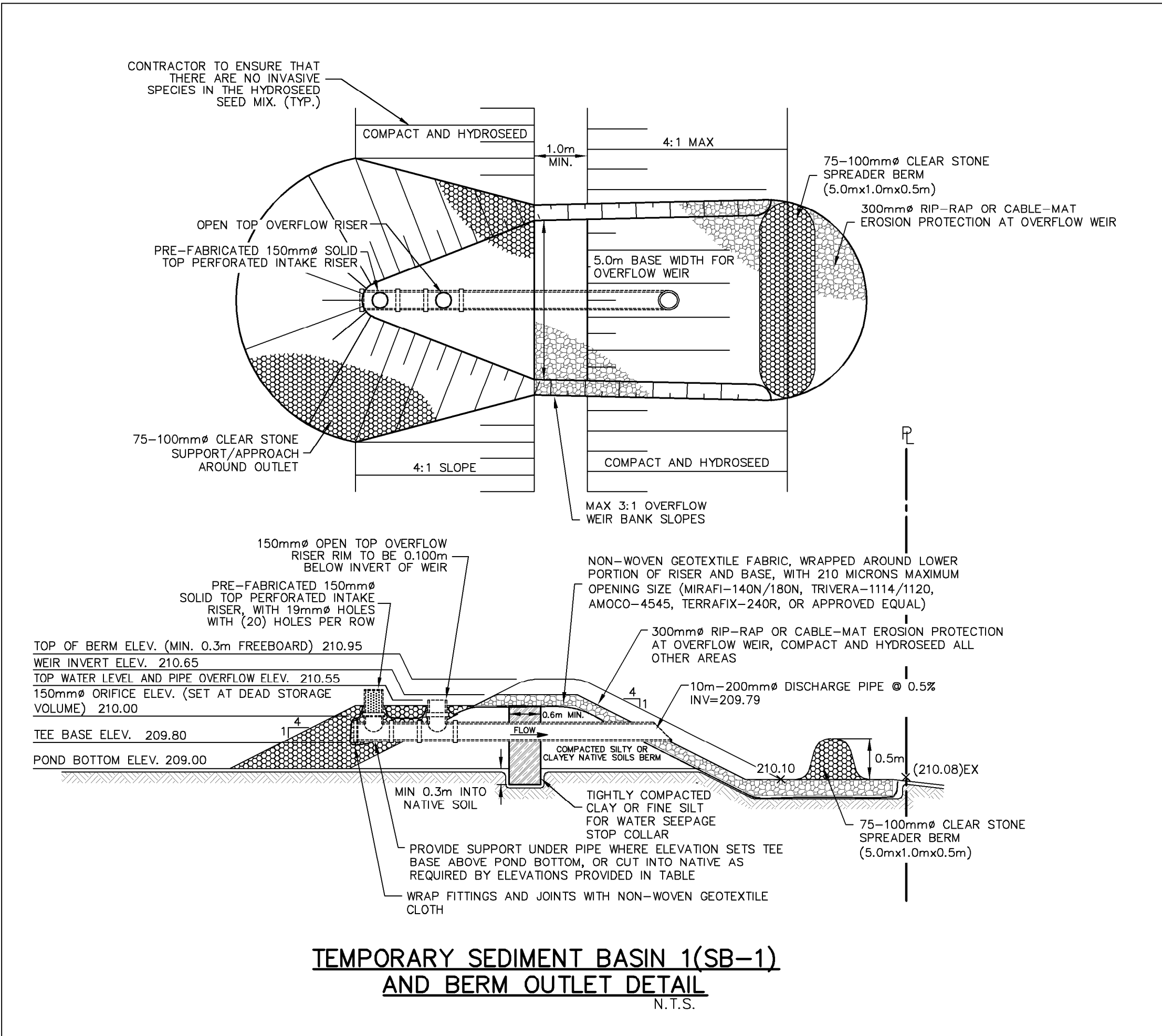
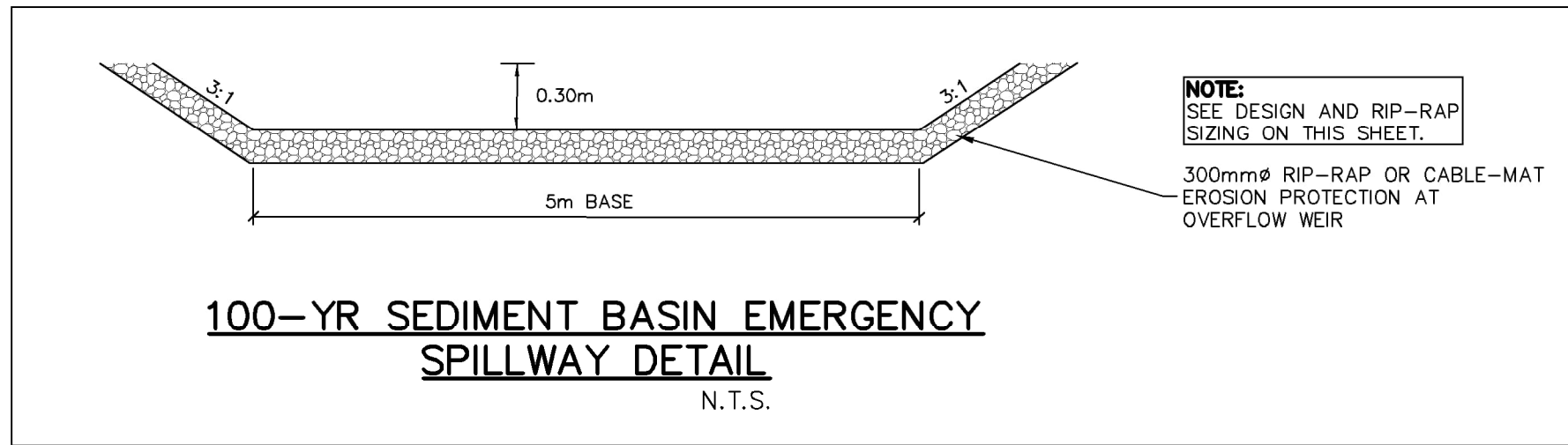
GEODETIC BENCHMARK ELEV. = 208.076m  
BENCHMARK No. 1045, LOCATED AT THE BASE OF A 750mm CONCRETE TRAFFIC POLE AT THE SOUTH-WEST CORNER OF ARGENTA ROAD AND PLAZA ENTRANCE (WILMART), HAVING A PUBLISHED ELEVATION OF 208.076 METRES.

SITE BENCHMARK ELEV. = m  
SEE GEODETIC BENCHMARK

NOTE TO CONTRACTOR :  
DO NOT SCALE DRAWINGS.  
CONTRACTORS MUST CHECK AND VERIFY ALL DIMENSIONS AND REPORT ANY DISCREPANCIES TO THE ENGINEER BEFORE PROCEEDING WITH THE WORK.  
ALL DRAWINGS REMAIN THE PROPERTY OF THE ENGINEER AND SHALL NOT BE REPRODUCED OR REUSED WITHOUT THE ENGINEER'S WRITTEN PERMISSION.  
THE OWNER/ARCHITECT/CONTRACTOR IS ADVISED THAT M.T.E. CONSULTANTS INC. CANNOT GUARANTEE ANY COMPONENT OF THE SITE WORKS NOT INSPECTED DURING CONSTRUCTION. IT IS THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO NOTIFY M.T.E. CONSULTANTS INC. PRIOR TO COMMENCEMENT OF CONSTRUCTION TO ARRANGE FOR INSPECTION.

| EROSION & SEDIMENT CONTROL<br>SEDIMENT BASIN SIZING & CONSTRUCTION INFORMATION |            |                                  |                |                |               |             |                 |                  |                    | Prologis Meadowvale Distribution Centre<br>Mississauga, Ontario |        |                                           |             |                    | Date: June 23, 2025<br>Project Number: 60549-001<br>Design By: NZR |                 |                |               |  |
|--------------------------------------------------------------------------------|------------|----------------------------------|----------------|----------------|---------------|-------------|-----------------|------------------|--------------------|-----------------------------------------------------------------|--------|-------------------------------------------|-------------|--------------------|--------------------------------------------------------------------|-----------------|----------------|---------------|--|
| ID Tag                                                                         | Basin Area | Sediment Basin Design Volume (V) |                |                |               | Bottom Area | Bottom of Basin | Bottom Elevation | Toe Base Elevation | Orifice Plate                                                   |        | Top Water Level & Overflow Pipe Elevation | Weir Invert | Top Berm Elevation | Orifice Diameter                                                   | Maximum Storage | Live Storage   | Drawdown Time |  |
|                                                                                |            | Dead                             | Live           | Total          | Orifice Plate |             |                 |                  |                    | Dead Volume                                                     |        |                                           |             |                    |                                                                    |                 |                |               |  |
|                                                                                |            | m <sup>3</sup>                   | m <sup>3</sup> | m <sup>3</sup> | Elevation     |             |                 |                  |                    | m <sup>3</sup>                                                  |        |                                           |             |                    |                                                                    |                 |                |               |  |
| na                                                                             | na         | m <sup>2</sup>                   | m <sup>2</sup> | m <sup>2</sup> | na            | na          | na              | na               | na                 | na                                                              | na     | m                                         | m           | m                  | m                                                                  | m <sup>3</sup>  | m <sup>3</sup> | h             |  |
| SB-1                                                                           | 13.40      | 2.479                            | 1.675          | 4.154          | 2198          | 430         | 209.9           | 209.80           | 210.0              | 209.1                                                           | 210.55 | 4.303                                     | 210.65      | 210.65             | 150                                                                | 0.0340          | 41.5           | 29.5          |  |
| SB-2                                                                           | 2.65       | 490                              | 331            | 822            | 430           | ft          | 208.0           | 208.70           | 208.9              | 208.9                                                           | 209.25 | 877                                       | 209.35      | 209.65             | 75                                                                 | 0.0074          |                |               |  |

(1) Dead Storage is based upon minimum 185 m<sup>3</sup> volume per ha drainage area due to drawdown time being less than 48 hours; Live Storage is based upon minimum 125 m<sup>3</sup> volume per ha drainage area.



|                      |                           |                |
|----------------------|---------------------------|----------------|
| 8.                   |                           |                |
| 7.                   |                           |                |
| 6.                   |                           |                |
| 5.                   |                           |                |
| 4.                   |                           |                |
| 3.                   |                           |                |
| 2.                   | ISSUED FOR SPA            | RDZ 2025-08-08 |
| 1.                   | ISSUED FOR DRIVING PERMIT | RDZ 2025-08-30 |
| NOT FOR CONSTRUCTION |                           | DT 1999-08-05  |

MTE  
Engineers, Scientists, Surveyors  
906-639-2552

2025-08-08  
R.D. ZHOU  
100561167  
PROFESSIONAL ENGINEER  
PROVINCE OF ONTARIO

NOT FOR CONSTRUCTION

CLIENT  
PETROFF PARTNERSHIP ARCHITECTS  
10 AVIVA WAY SUITE 400 MARKHAM

PROJECT  
PROLOGIS MEADOWVALE DISTRIBUTION CENTRE  
7564 TENTH LINE WEST MISSISSAUGA

DRAWING  
ESC DETAILS PLAN

Project Manager R.ZHOU Job No. 60549\_001  
Design By NZR Checked By RDZ  
Drawn By AXG Checked By NZR  
Surveyed By Others  
Date Apr.15/25  
Scale AS NOTES Sheet 3 of 9