

**PEDESTRIAN LEVEL  
WIND STUDY**

4100 Ponytail Drive  
Mississauga, Ontario

REPORT: GWE14-118-WTPLW-B4-B6



January 9, 2026

PREPARED FOR

**Chelsea on the Green I Limited Partnership**

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## **EXECUTIVE SUMMARY**

This report describes a wind tunnel pedestrian level wind study undertaken to assess wind conditions for the full build-out of the proposed development located at 4100 Ponytail Drive and 1850 Rathburn Road East in Mississauga, Ontario. Two configurations were studied: (i) *existing conditions*, including all surrounding developments and B3 from first phase of the development and excluding the future B4-B6, and (ii) *future conditions* with the full build-out of the proposed development in place. The study involves wind tunnel measurements of pedestrian wind speeds using a physical scale model, combined with meteorological data integration, to assess pedestrian comfort at key areas within and surrounding the study site. Grade-level areas investigated include sidewalks, walkways, laneways, transit stops, parking areas, outdoor amenity areas, landscaped spaces, and building access points. Wind comfort is also evaluated over the Building 3 Level 6 amenity terrace. The results and recommendations derived from these considerations are summarized in the following paragraphs and detailed in the subsequent report.

Our work is based on industry standard wind tunnel testing and data analysis procedures, City of Mississauga wind criteria, architectural drawings provided by 4 Architecture Inc. in October 2025 and updated in December 2025, surrounding street layouts, as well as existing and approved future building massing information and recent site imagery.

A complete summary of the predicted wind conditions is provided in Section 5 of this report and is also illustrated in Figures 2A through 3B, as well as Tables A1-A2 and B1-B4 in the appendices. Based on wind tunnel test results, meteorological data analysis, and experience with similar developments in Mississauga, we conclude that the future wind conditions over most grade-level pedestrian wind-sensitive areas within and surrounding the study site will be acceptable for the intended uses on a seasonal basis. An exception is the primary lobby entrance for B5, for which mitigation is recommended as described in Section 5.2. Optional targeted mitigation is also discussed for the remaining outdoor amenity spaces, depending on their programming.

Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no areas over the study site were found to experience conditions that could be considered unsafe.



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## **1. INTRODUCTION**

This report describes a pedestrian level wind study undertaken to assess wind conditions for the full build-out of the proposed development located at 4100 Ponytail Drive and 1850 Rathburn Road East in Mississauga, Ontario. The development comprises Building 3 as part of Phase 1 and Buildings 4 through 6 as part of Phase 2. Two configurations were studied: (i) *existing conditions*, including all surrounding developments and B3 from first phase of the development and excluding the future B4-B6, and (ii) *future conditions* with the full build-out of the proposed development in place. The study was performed in accordance with industry standard wind tunnel testing techniques, City of Mississauga wind criteria, architectural drawings provided by 4 Architecture Inc. in October 2025 and updated in December 2025, surrounding street layouts and existing and approved future building massing information, as well as recent site imagery.

## **2. TERMS OF REFERENCE**

The focus of this pedestrian wind study is Phase 2 the proposed development located at 4100 Ponytail Drive and 1850 Rathburn Road East in Mississauga, Ontario. The study site is situated to the immediate southwest of the intersection of Rathburn Road East and Ponytail Drive and further bordered by the Chechalk Trail/hydro transmission corridor to the southwest. Buildings 4-6 (Phase 2) of the proposed development, arranged west to east, are located to the immediate south of the two existing Forest Park Circle 18-storey towers and Building 3 (Phase 1).

Each building within Phase 2 comprises a 20-storey rectangular tower rising from a 5-storey podium. At grade, a proposed driveway surrounding a central outdoor amenity connects each of the buildings to the existing driveway and provides access to drop-off areas fronting primary lobbies at the northeast corner of Building 4, the northwest corner of Building 5, and the west elevation of Building 6. Three levels of shared underground parking are accessed via a parking ramp connecting to existing surface-level parking to the northeast of Building 6. Additional outdoor amenity spaces at grade separate each of the buildings while the remainder of the ground floors within each building comprise indoor amenities, residential space, and building support services. Above, each podium rises with uniform residential floorplans, to Level 6 where the floorplate set back from each elevation to the base of the tower. The typical tower floorplates begin at Level 7 and rise to Level 20, with small setbacks at Levels 17 and 19 accommodating



private terraces on Buildings 4 and 5, and Level 20 on Building 6. Each tower is completed with a central mechanical penthouse.

Regarding wind exposures, the near-field surroundings of the development (defined as an area falling within a 200-metre radius of the site) are characterized by a primarily low-rise massing and greenspace in all directions, with the two existing Forest Park Circle 18-storey towers at 4100 Ponytrail Drive and 1850 Rathburn Road East to the southeast and southwest, respectively. The far-field surroundings (defined as the area beyond the near-field and within a two-kilometer radius) reflect a continuation of the low-rise and greenspace exposure, with isolated clusters of taller residential developments, in all directions.

Grade-level areas investigated include sidewalks, walkways, laneways, transit stops, parking areas, outdoor amenity areas, landscaped spaces, and building access points. Wind comfort is also evaluated over the Building 3 Level 6 amenity terrace. Figures 1A and 1B illustrate the *existing* and *future* study site and surrounding context, respectively, and Photographs 1 through 6 depict the wind tunnel model used to conduct the study.

### **3. OBJECTIVES**

The principal objectives of this study are to (i) determine pedestrian level wind comfort and safety conditions at key areas within and surrounding the development site; (ii) identify areas where wind conditions may interfere with the intended uses of outdoor spaces; (iii) recommend suitable mitigation measures, where required; and (iv) evaluate the influence of the proposed development and of surrounding approved future developments, on the existing wind conditions.

### **4. METHODOLOGY**

The approach followed to quantify pedestrian wind conditions over the site is based on wind tunnel measurements of wind speeds at selected locations on a reduced-scale physical model, meteorological analysis of the Mississauga area wind climate and synthesis of wind tunnel data with industry-accepted guidelines. The following sections describe the analysis procedures, including a discussion of the pedestrian comfort and safety guidelines.



## 4.1 Wind Tunnel Context Modelling

A detailed PLW study is performed to determine the influence of local winds at the pedestrian level for a proposed development. The physical model of the proposed development and relevant surroundings, illustrated in Photographs 1 through 6 following the main text, was constructed at a scale of 1:400. The wind tunnel model includes all existing buildings and approved future developments within a full-scale diameter of approximately 840 metres. The general concept and approach to wind tunnel modelling is to provide building and topographic detail in the immediate vicinity of the study site on the surrounding model, and to rely on a length of wind tunnel upwind of the model to develop wind properties consistent with known turbulent intensity profiles that represent the surrounding terrain.

An industry standard practice is to omit trees, vegetation, and other existing and planned landscape elements from the wind tunnel model due to the difficulty of providing accurate seasonal representation of vegetation. The omission of trees and other landscaping elements produces slightly more conservative wind speed values.

## 4.2 Wind Speed Measurements

The PLW study was performed by testing a total of 107 sensor locations on the scale model in Gradient Wind's wind tunnel. Of these 107 sensors, 105 were located at grade and the remaining two sensors were located over the Building 3 Level 6 amenity terrace. Wind speed measurements were performed for each of the 107 sensors for 36 wind directions at 10° intervals. Figures 1A and 1B illustrate the existing and proposed study site and surrounding context, while sensor locations used to investigate wind conditions are illustrated in Figures 2A through 3B.

Mean and peak wind speed values for each location and wind direction were calculated from real-time pressure measurements, recorded at a sample rate of 500 samples per second, and taken over a 60-second time period. This period at model-scale corresponds approximately to one hour in full-scale, which matches the time frame of full-scale meteorological observations. Measured mean and gust wind speeds at grade were referenced to the wind speed measured near the ceiling of the wind tunnel to generate mean and peak wind speed ratios. Ceiling height in the wind tunnel represents the depth of the boundary layer of wind flowing over the earth's surface, referred to as the gradient height. Within this boundary layer, mean wind speed increases up to the gradient height and remains constant thereafter. Appendices



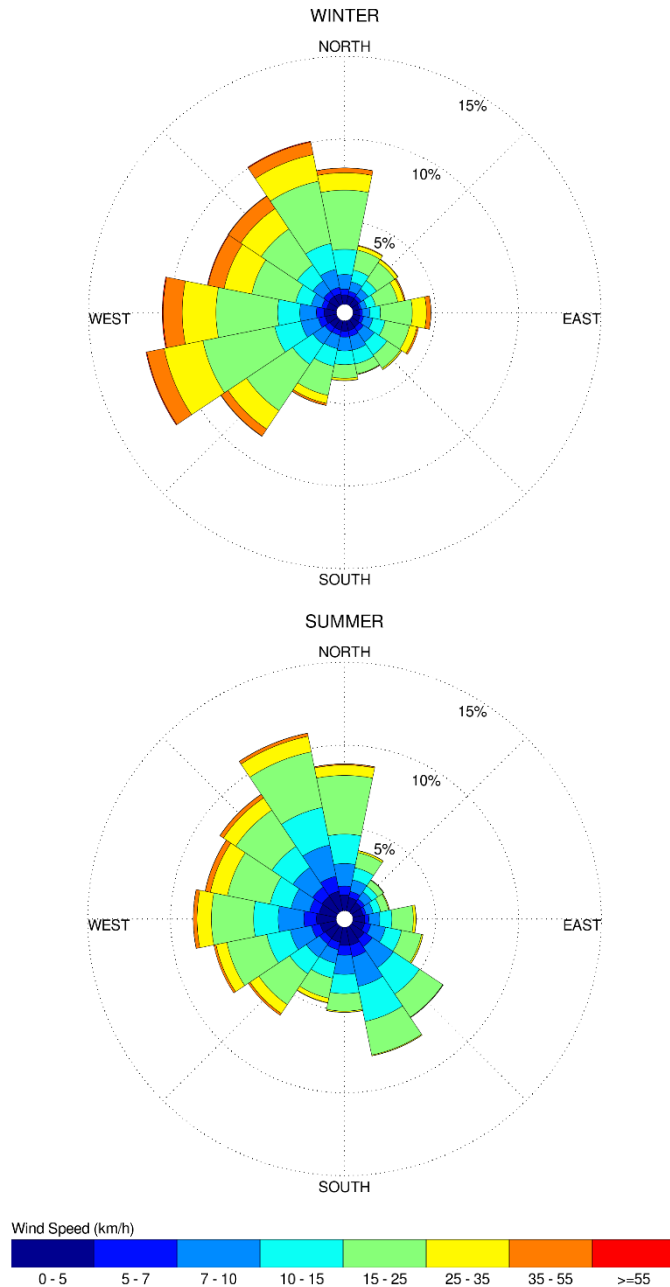
C and D provide greater detail of the theory behind wind speed measurements. Wind tunnel measurements for this project, conducted in Gradient Wind's wind tunnel facility, meet or exceed guidelines found in the National Building Code of Canada 2015 and of 'Wind Tunnel Studies of Buildings and Structures', ASCE Manual 7 Reports on Engineering Practice No 67.

### 4.3 Meteorological Data Analysis

A statistical model for winds in Mississauga was developed from over 50 years of hourly meteorological wind data recorded at Pearson International Airport. Wind speed and direction data were analyzed for each month of the year in order to determine the statistically prominent wind directions and corresponding speeds, and to characterize similarities between monthly weather patterns. Based on this portion of the analysis, the four seasons are represented by grouping data from consecutive months based on similarity of weather patterns, and not according to the traditional calendar method.

The statistical model of the Mississauga area wind climate, which indicates the directional character of local winds on a seasonal basis, is illustrated on the following page. The plots illustrate seasonal distribution of measured wind speeds and directions in km/h. Probabilities of occurrence of different wind speeds are represented as stacked polar bars in sixteen azimuth divisions. The radial direction represents the percentage of time for various wind speed ranges per wind direction during the measurement period. The preferred wind speeds and directions can be identified by the longer length of the bars. For Pearson International Airport, the most common winds concerning pedestrian comfort occur from the southwest clockwise to the north, as well as those from the east. The directional preference and relative magnitude of the wind speed varies somewhat from season to season, with the summer months displaying the calmest winds relative to the remaining seasonal periods.

## SEASONAL DISTRIBUTION OF WINDS FOR VARIOUS PROBABILITIES PEARSON INTERNATIONAL AIRPORT, MISSISSAUGA, ONTARIO



### Notes:

1. Radial distances indicate percentage of time of wind events.
2. Wind speeds are mean hourly in km/h, measured at 10 m above the ground.



#### 4.4 Pedestrian Comfort and Safety Guidelines

Pedestrian comfort and safety guidelines are based on the mechanical effects of wind without consideration of other meteorological conditions (i.e. temperature, relative humidity). The comfort guidelines assume that pedestrians are appropriately dressed for a specified outdoor activity during any given season. Four pedestrian comfort classes are based on 80% non-exceedance Gust Equivalent Mean (GEM) wind speed ranges, which include (i) Sitting; (ii) Standing; (iii) Walking; and (iv) Uncomfortable. More specifically, the comfort classes and associated GEM wind speed ranges are summarized as follows:

- (i) **Sitting** – A wind speed below 10 km/h (i.e. 0 – 10 km/h) would be considered acceptable for sedentary activities, including sitting.
- (ii) **Standing** – A wind speed below 15 km/h (i.e. 10 km/h – 15 km/h) is acceptable for activities such as standing or leisurely strolling.
- (iii) **Walking** – A wind speed below 20 km/h (i.e. 15 km/h – 20 km/h) is acceptable for walking or more vigorous activities.
- (iv) **Uncomfortable** – A wind speed over 20 km/h is classified as uncomfortable from a pedestrian comfort standpoint. Brisk walking and exercise, such as jogging, would be acceptable for moderate excesses of this criterion.

The pedestrian safety wind speed guideline is based on the approximate threshold that would cause a vulnerable member of the population to fall. A 0.1% exceedance gust wind speed of greater than 90 km/h is classified as dangerous.

Experience and research on people’s perception of mechanical wind effects has shown that if the wind speed levels are exceeded for more than 20% of the time, the activity level would be judged to be uncomfortable by most people. For instance, if wind speeds of 10 km/h were exceeded for more than 20% of the time most pedestrians would judge that location to be too windy for sitting or more sedentary activities. Similarly, if 20 km/h at a location were exceeded for more than 20% of the time, walking or less vigorous activities would be considered uncomfortable. As most of these criteria are based on subjective reactions of a population to wind forces, their application is partly based on experience and judgment.

Once the pedestrian wind speed predictions have been established at tested locations, the assessment of pedestrian comfort involves determining the suitability of the predicted wind conditions for their associated spaces. This step involves comparing the predicted comfort class to the desired comfort class, which is dictated by the location type represented by the sensor (i.e. a sidewalk, building entrance, amenity space, or other). An overview of common pedestrian location types and their desired comfort classes are summarized below.

### DESIRED PEDESTRIAN COMFORT CLASSES FOR VARIOUS LOCATION TYPES

Location Types	Desired Comfort Classes
Primary Building Entrance	Standing
Secondary Building Access Point	Walking
Public Sidewalks / Pedestrian Walkways	Walking
Outdoor Amenity Spaces	Sitting / Standing
Cafés / Patios / Benches / Gardens	Sitting / Standing
Plazas	Standing / Walking
Transit Stops	Standing
Public Parks	Sitting / Walking
Garage / Service Entrances	Walking
Vehicular Drop-Off Zones	Walking
Laneways / Loading Zones	Walking

## 5. RESULTS AND DISCUSSION

Tables A1 through A2 in Appendix A provide a summary of seasonal comfort predictions for each sensor location under the *existing* massing scenario. Similarly, Tables B1 through B4 in Appendix B provide the seasonal comfort predictions for under the *future* massing scenario. The tables indicate the 80% non-exceedance GEM wind speeds and corresponding comfort classifications as defined in Section 4.4. In other words, a wind speed threshold of 19.1 for the summer season indicates that 80% of the measured data falls at or below 19.1 km/h during the summer months and conditions are therefore suitable for walking, as the 80% threshold value falls within the exceedance range of 15-20 km/h for walking. The tables include the predicted threshold values for each sensor location during each season, accompanied by the corresponding predicted comfort class (i.e. sitting, standing, walking, etc.).

The most significant findings of the PLW study are summarized in Sections 5.1 and 5.2. To assist with understanding and interpretation, predicted conditions for the proposed development are also illustrated in colour-coded format in Figures 2A through 3B. Conditions suitable for sitting are represented by the colour blue, while standing is represented by green, and walking by yellow. Conditions considered uncomfortable for walking are represented by the colour orange. For locations where the wind safety criterion is exceeded, the sensor is highlighted in red.

### 5.1 Pedestrian Comfort Suitability – Existing Scenario

Based on the analysis of the measured data, consideration of local climate data, and the suitability descriptors provided in Tables A1-A2 in Appendix A and illustrated in Figures 2A and 2B, this section summarizes the significant findings of the PLW study with respect to the *existing scenario*, as follows:

1. Most public sidewalks, walkways, laneways, landscaped spaces, and parking areas within and surrounding the proposed development are suitable for walking or better during each seasonal period, which is acceptable. Limited exceptions include portions of walkway to the east of B3 (Sensor 21), surface parking to the southwest (Sensor 53), and landscaped area/walkway at the southwest corner of B3 (Sensor 67), where conditions become uncomfortable for walking during the winter period.



2. The nearby transit stop along the south side of Rathburn Road East (Sensor 18) will be suitable for walking throughout each seasonal period. Notably, this stop is presently equipped with a pedestrian transit shelter.
3. The Phase 1 outdoor amenity areas to the east (Sensors 43 & 61-63), south (Sensors 40, 44, and 45), and west (Sensors 15, 54, & 55) of Building 3, will primarily be comfortable for standing throughout the summer months and walking or better during the winter.
4. The existing building access points serving the adjacent Forest Park Circle 18-storey towers to the southeast (Sensor 25) and southwest (Sensor 14) will be suitable for sitting throughout each seasonal period. The B3 primary lobby entrance along the south elevation (Sensor 64) will be comfortable for sitting throughout the summer period and standing throughout the winter.
5. Throughout the warmer months, the B3 Level 6 outdoor amenity terrace (Sensors 106 and 107) is comfortable for sitting towards the south edge of the space and walking towards the north.
6. Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no areas over the study site were found to experience wind conditions that are considered unsafe.

## 5.2 Pedestrian Comfort Suitability – *Future Conditions*

Based on the analysis of the measured data, consideration of local climate data, and the suitability descriptors provided in Tables B1-B4 in Appendix B and illustrated in Figures 3A and 3B, this section summarizes the most significant findings of the PLW study with respect to *future conditions*, as follows:

1. Most public sidewalks, walkways, laneways, landscaped spaces, and parking areas within and surrounding the proposed development will experience wind conditions suitable for walking or better during each seasonal period, which is acceptable. An exception is a portion of landscaped area/walkway at the southwest corner of B3 (Sensor 67), where conditions become uncomfortable for walking during the winter period. Under the full-build out, conditions are improved when compared to the *existing* massing and the exceedance of the walking criterion at this location is now marginal (< 0.6 km/hr – See Appendix B). Thus, the noted conditions are acceptable without the need for mitigation.



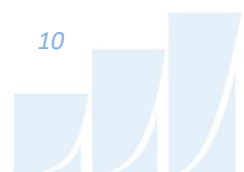
2. Most primary entrances serving B4, B5, and B6 will be comfortable for standing or better throughout each seasonal period, which is acceptable. Exceptions include the primary lobby entrances along the west elevation of B5 (Sensor 93) and B6 (Sensor 95), where conditions exceed the standing criterion and become intermittently suitable for walking throughout the winter period. Notably, the exceedance at the B6 entrance is marginal (0.5 km/h – See Appendix B) therefore mitigation is not considered to be necessary.

For the B5 primary lobby entrance (Sensor 93), it is recommended to either flank the entrance with wind barriers, recess within the façade, equip sliding doors, or provide a canopy overhead.

All secondary building access points (such as stairwell exits, loading areas, vehicle entrances, and mail access) serving the proposed development will be comfortable for walking or better throughout the year, which is acceptable.

3. The nearby transit stop along the south side of Rathburn Road East (Sensor 18) will be suitable for walking throughout the winter and standing throughout the summer period. As this stop is already equipped with a pedestrian transit shelter, additional mitigation is not necessary.
4. The Phase 1 outdoor amenity areas to the east (Sensors 43 & 61-63), south (Sensors 40, 44, and 45), and west (Sensors 54, 55, 67, & 68) of Building 3, will primarily remain comfortable for standing or better throughout the summer months and walking or better during the winter, which is acceptable depending on the programming of the space. An exception is the previously noted windy area at the southwest corner of Building 3 (Sensor 67), which will continue to experience walking conditions throughout the summer period. The area is currently programmed as a landscaped space, which is acceptable, but if calmer conditions are desired, it is recommended to introduce a cluster of wind barriers to the north along the west side of Building 3. Wind barriers may take the form of coniferous/marcescent plantings, high-solidity windscreens, raised planters, or a combination thereof and should measure at least 1.6-metres tall.

Regarding the Phase 2 spaces, the outdoor amenity areas to the west and southwest of B6 (Sensors 32, 36, & 39 and Sensors 85, 104, & 105, respectively) and to the west of B4 (Sensors 46-48 & 79-81) will be comfortable for standing or better during the summer and walking or better during the winter, which is acceptable depending on the programming of the space. Where calmer



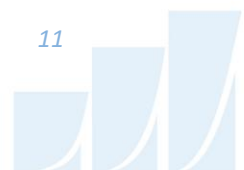
conditions are desired such as designated seating areas, targeted 1.6-metre-tall wind barriers to the immediate northwest and southeast may be considered.

5. The existing building access points serving the adjacent Forest Park Circle 18-storey towers to the southeast (Sensor 25) and southwest (Sensor 14) will remain suitable for sitting throughout each seasonal period. The B3 primary lobby entrance along the south elevation (Sensor 64) will remain comfortable for sitting throughout the summer period and standing throughout the winter. The noted conditions are acceptable.
6. Throughout the warmer months, the B3 (Phase 1) Level 6 outdoor amenity terrace (Sensors 106 and 107) will remain comfortable for sitting towards the south edge of the space and walking towards the north. Wind speeds will not be exacerbated with the introduction of Buildings 4 through 6 (Phase 2).
7. Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no areas over the study site were found to experience wind conditions that are considered unsafe.

## **6. CONCLUSIONS AND RECOMMENDATIONS**

This report describes a wind tunnel pedestrian level wind study undertaken to assess wind conditions for the full build-out of the proposed development located at 4100 Ponytail Drive and 1850 Rathburn Road East in Mississauga, Ontario. The study was performed in accordance with industry standard wind tunnel testing and data analysis procedures.

A complete summary of the predicted wind conditions is provided in Section 5 of this report and is also illustrated in Figures 2A through 3B, as well as Tables A1-A2 and B1-B4 in the appendices. Based on wind tunnel test results, meteorological data analysis, and experience with similar developments in Mississauga, we conclude that the proposed wind conditions over most grade-level pedestrian wind-sensitive areas within and surrounding the study site will be acceptable for the intended uses on a seasonal basis. An exception is the primary lobby entrance for B5, for which mitigation is recommended as described in Section 5.2. Optional targeted mitigation is also discussed for the remaining outdoor amenity spaces, depending on their programming.

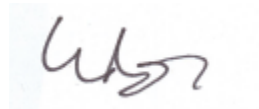


Within the context of typical weather patterns, which exclude anomalous localized storm events such as tornadoes and downbursts, no areas over the study site were found to experience conditions that could be considered unsafe.

This concludes our pedestrian level wind study and report. Please advise the undersigned of any questions or comments.

Sincerely,

***Gradient Wind Engineering Inc.***



William Knipe, B.E.Sc.,  
Junior Wind Scientist



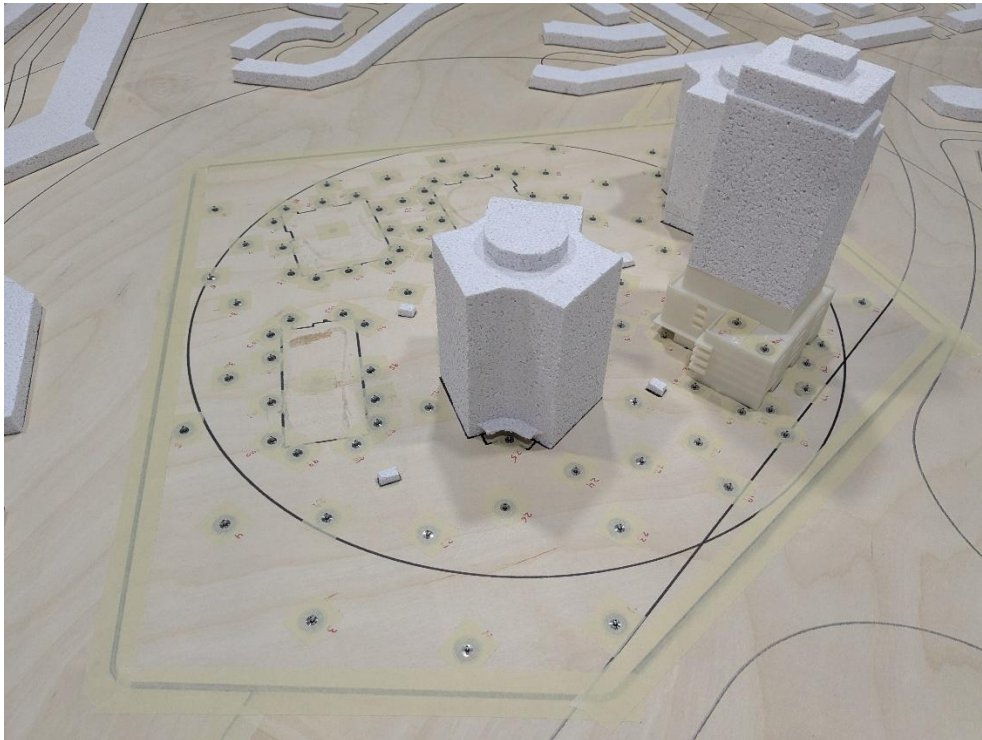
Nick Petersen, P.Eng.,  
Wind Engineer

*GWE14-118-WTPLW-B4-B6*





**PHOTOGRAPH 1: CLOSE-UP VIEW OF EXISTING CONTEXT MODEL LOOKING NORTH**



**PHOTOGRAPH 2: CLOSE-UP VIEW OF EXISTING CONTEXT MODEL LOOKING SOUTHWEST**



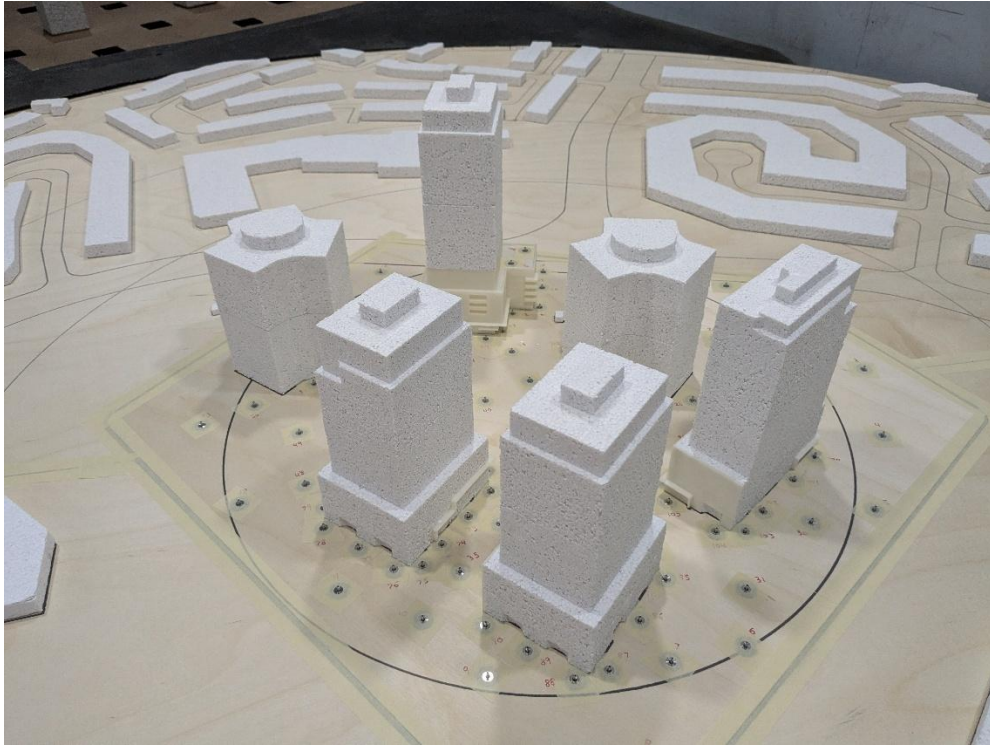


**PHOTOGRAPH 3: PROPOSED STUDY MODEL INSIDE THE GWE WIND TUNNEL LOOKING DOWNWIND**

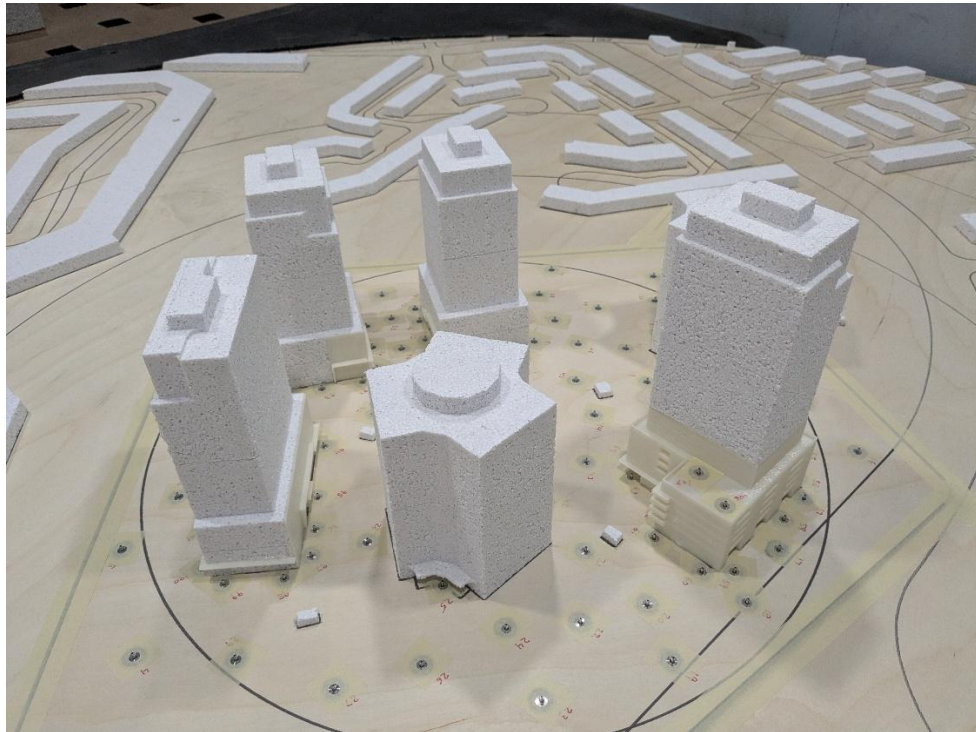


**PHOTOGRAPH 4: PROPOSED STUDY MODEL INSIDE THE GWE WIND TUNNEL LOOKING UPWIND**



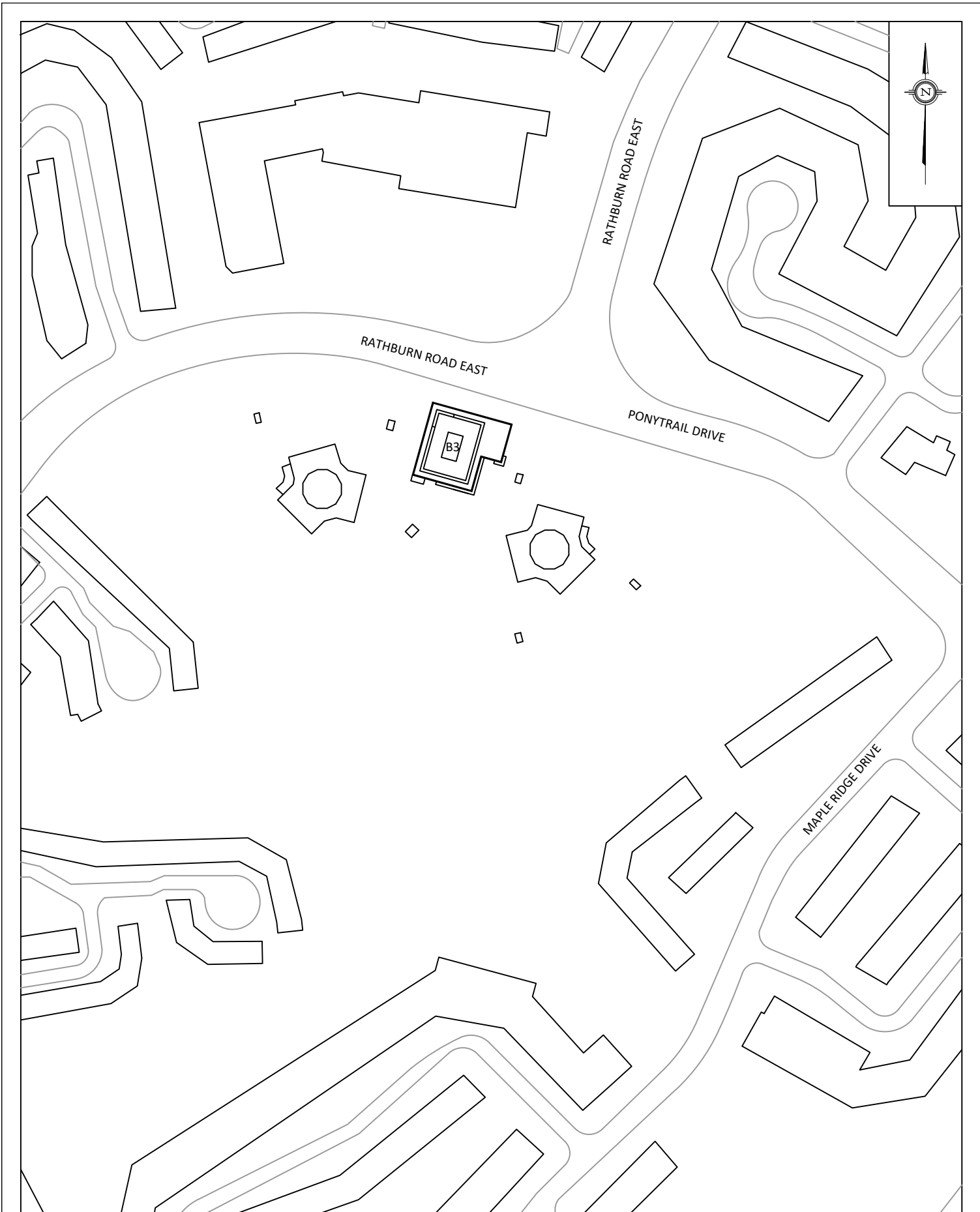


**PHOTOGRAPH 5: CLOSE-UP VIEW OF PROPOSED STUDY MODEL LOOKING NORTH**



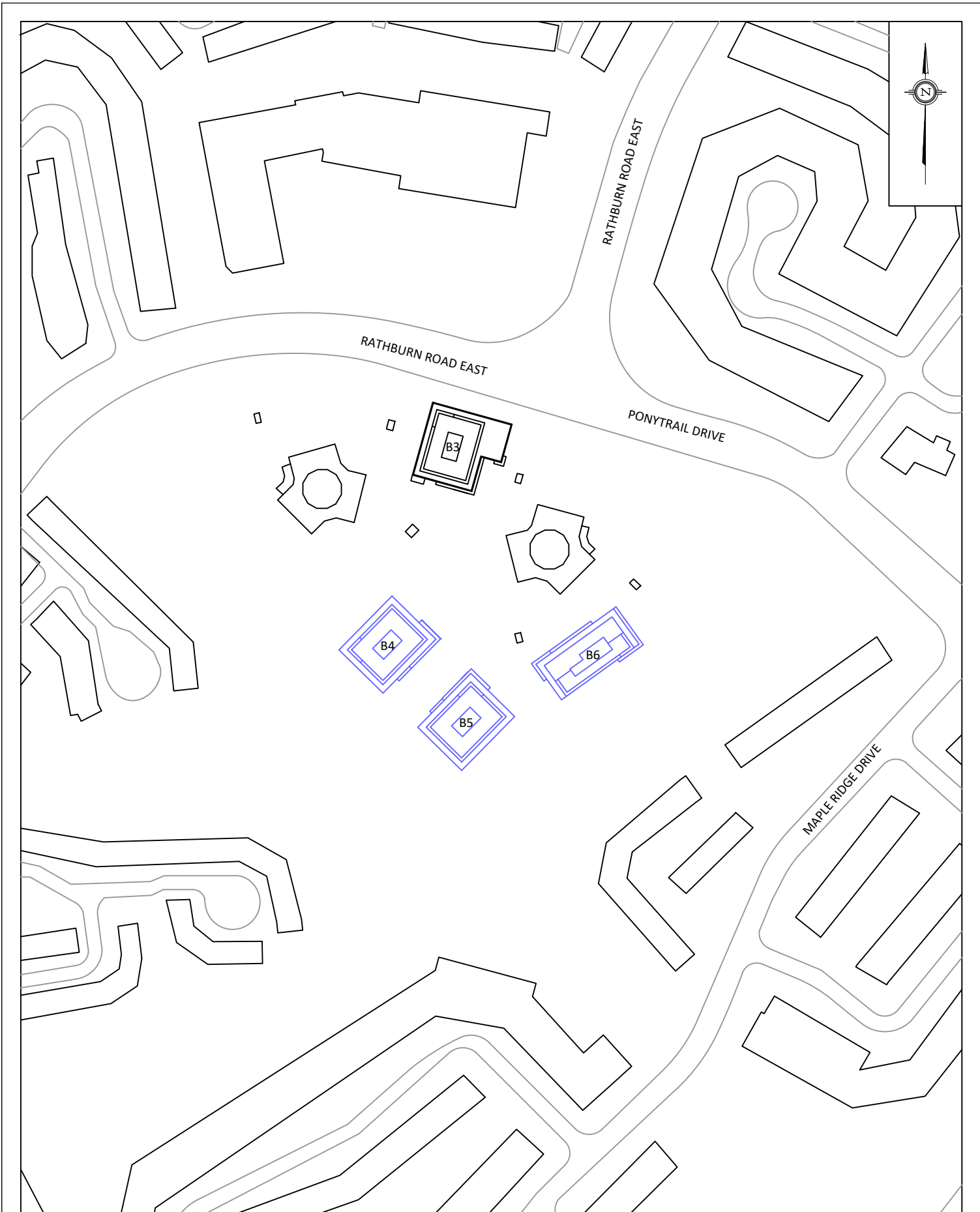
**PHOTOGRAPH 6: CLOSE-UP VIEW OF PROPOSED STUDY MODEL LOOKING SOUTHWEST**





PROJECT	B4-B6, FOREST PARK CIRCLE, MISSISSAUGA PEDESTRIAN LEVEL WIND STUDY	
SCALE	1:2500 (APPROX.)	DRAWING NO. GW14-118-PLW-B4/6-1A
DATE	JANUARY 9, 2026	DRAWN BY K.A.

DESCRIPTION	FIGURE 1A: EXISTING SCENARIO AND SURROUNDING CONTEXT
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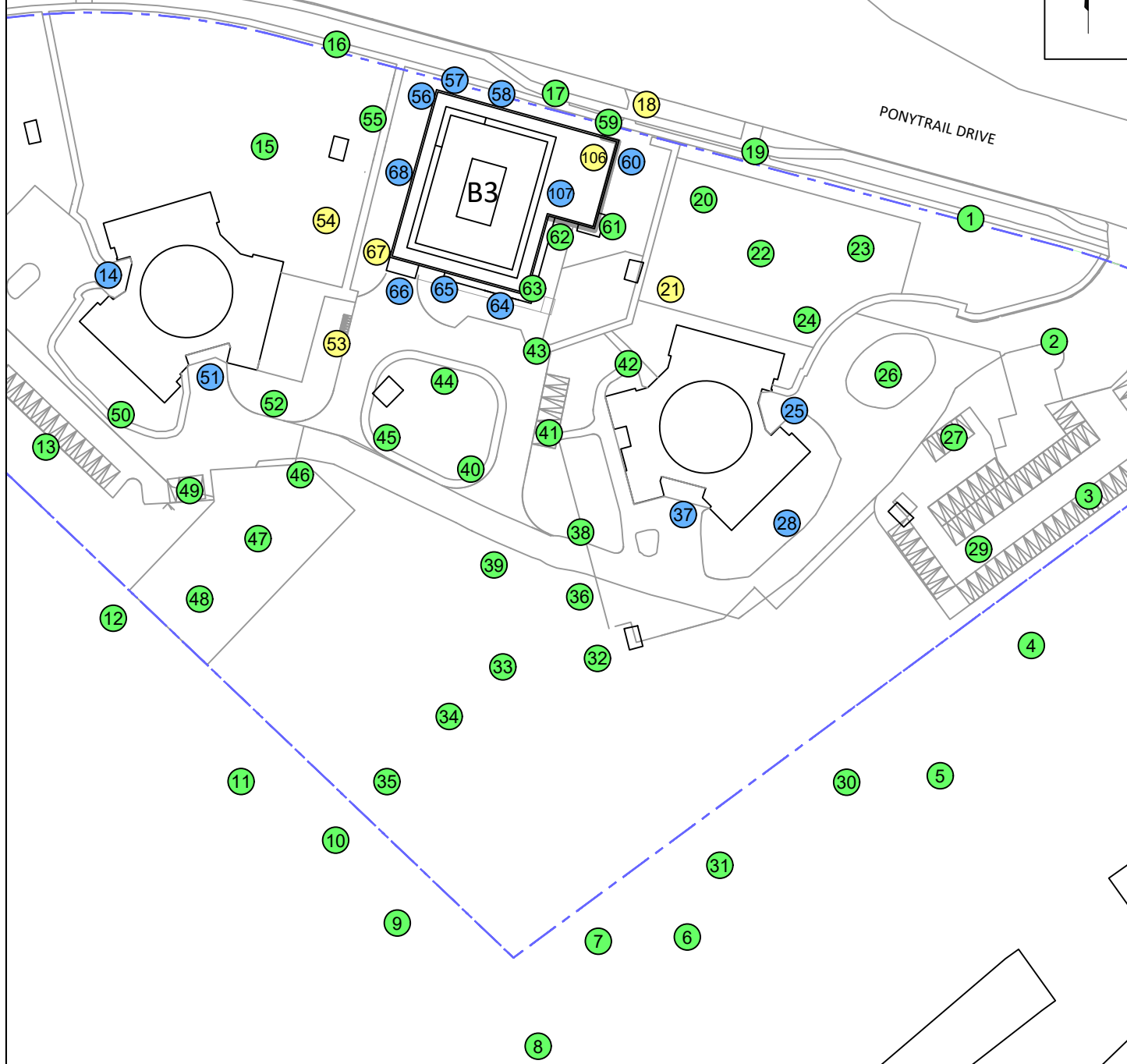
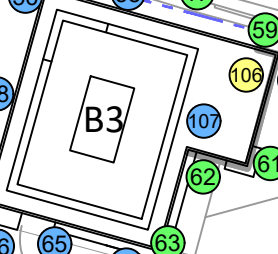
PROJECT	B4-B6, FOREST PARK CIRCLE, MISSISSAUGA PEDESTRIAN LEVEL WIND STUDY	
SCALE	1:2500 (APPROX.)	DRAWING NO. GW14-118-PLW-B4/6-1B
DATE	JANUARY 9, 2026	DRAWN BY K.A.

DESCRIPTION	FIGURE 1B: FUTURE SCENARIO AND SURROUNDING CONTEXT
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RATHBURN ROAD EAST

PONYTRAIL DRIVE



PREDICTED COMFORT CLASSES	<span style="color: blue;">#</span>	SITTING
	<span style="color: green;">#</span>	STANDING
	<span style="color: yellow;">#</span>	WALKING
	<span style="color: orange;">#</span>	UNCOMFORTABLE
WIND SAFETY CRITERION	<span style="border: 1px solid black; border-radius: 50%; padding: 2px;">#</span>	ACCEPTABLE
	<span style="border: 1px solid red; border-radius: 50%; padding: 2px;">#</span>	EXCEEDED

**NOTES:**

- SCALE IS APPROXIMATE.
- # PEDESTRIAN LEVEL WIND SENSOR LOCATION.

**GRADIENTWIND**  
ENGINEERS & SCIENTISTS  
127 WALGREEN ROAD, OTTAWA, ON  
613 836 0934 • GRADIENTWIND.COM

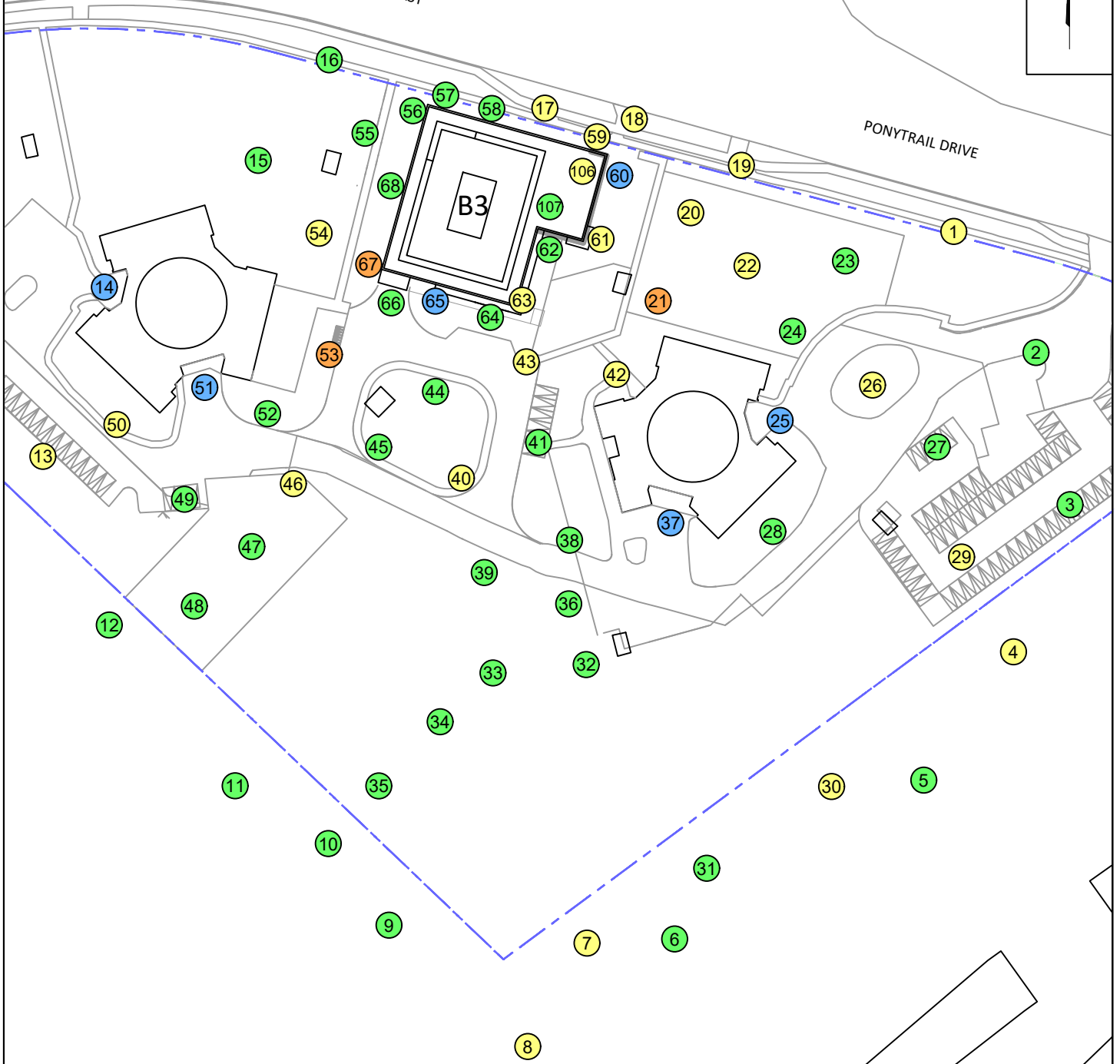
PROJECT	B3, FOREST PARK CIRCLE, MISSISSAUGA PEDESTRIAN LEVEL WIND STUDY	
SCALE	1:1300 (APPROX.)	DRAWING NO. GW14-118-PLW-B4/6-2A
DATE	JANUARY 9, 2026	DRAWN BY C.E.

DESCRIPTION  
**FIGURE 2A: SUMMER  
PROPOSED GRADE LEVEL PLW SENSOR LAYOUT  
PEDESTRIAN COMFORT PREDICTIONS**



RATHBURN ROAD EAST

PONYTRAIL DRIVE



PREDICTED COMFORT CLASSES	<span style="color: blue;">#</span>	SITTING
	<span style="color: green;">#</span>	STANDING
	<span style="color: yellow;">#</span>	WALKING
	<span style="color: orange;">#</span>	UNCOMFORTABLE
WIND SAFETY CRITERION	<span style="color: black;">#</span>	ACCEPTABLE
	<span style="color: red;">#</span>	EXCEEDED

**NOTES:**

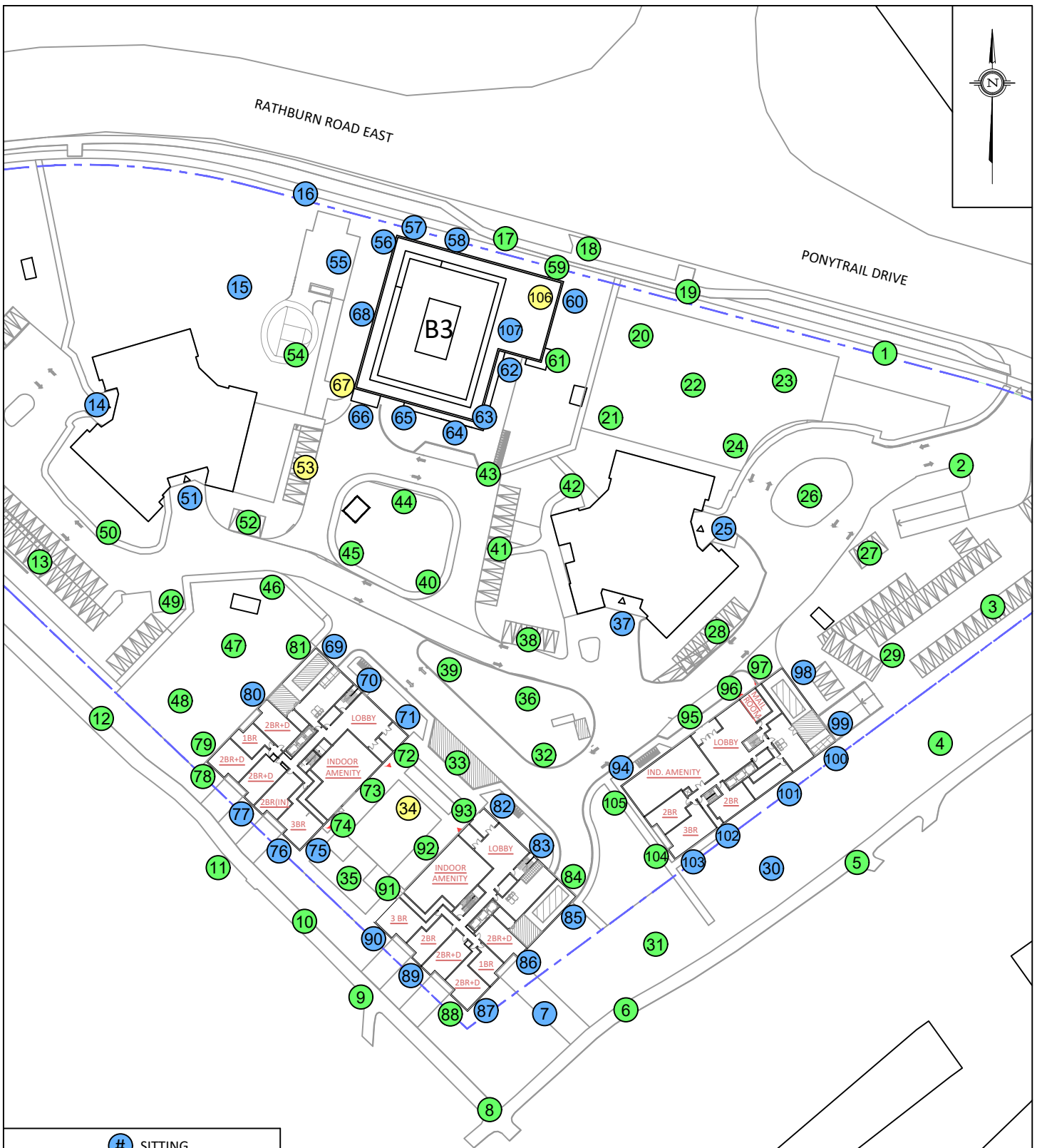
1. SCALE IS APPROXIMATE.
2. # PEDESTRIAN LEVEL WIND SENSOR LOCATION.

**GRADIENTWIND**  
ENGINEERS & SCIENTISTS

127 WALGREEN ROAD, OTTAWA, ON  
613 836 0934 • GRADIENTWIND.COM

PROJECT	B3, FOREST PARK CIRCLE, MISSISSAUGA PEDESTRIAN LEVEL WIND STUDY	
SCALE	1:1300 (APPROX.)	DRAWING NO. GW14-118-PLW-B4/6-2B
DATE	JANUARY 9, 2026	DRAWN BY C.E.

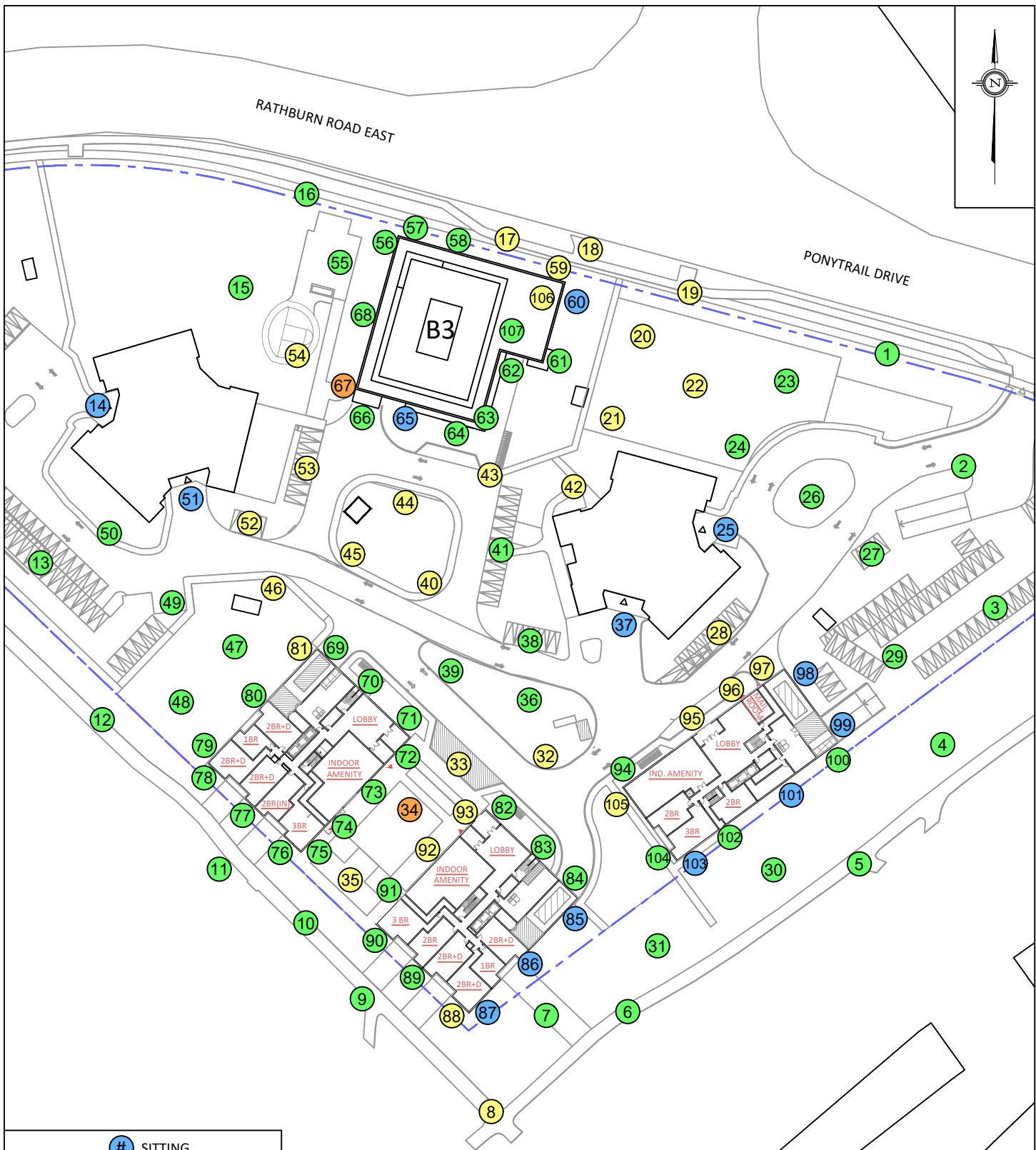
DESCRIPTION	FIGURE 2B: WINTER PROPOSED GRADE LEVEL PLW SENSOR LAYOUT PEDESTRIAN COMFORT PREDICTIONS
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PREDICTED COMFORT CLASSES	<span style="color: blue;">●</span> # SITTING
	<span style="color: green;">●</span> # STANDING
	<span style="color: yellow;">●</span> # WALKING
	<span style="color: orange;">●</span> # UNCOMFORTABLE
WIND SAFETY CRITERION	<span style="border: 1px solid black; border-radius: 50%; padding: 2px;">#</span> ACCEPTABLE
	<span style="border: 1px solid red; border-radius: 50%; padding: 2px;">#</span> EXCEEDED

**NOTES:**

1. SCALE IS APPROXIMATE.
2. # PEDESTRIAN LEVEL WIND SENSOR LOCATION.



PREDICTED COMFORT CLASSES	<span style="color: blue;">#</span>	SITTING
	<span style="color: green;">#</span>	STANDING
	<span style="color: yellow;">#</span>	WALKING
	<span style="color: orange;">#</span>	UNCOMFORTABLE
WIND SAFETY CRITERION	<span style="border: 1px solid black; border-radius: 50%; padding: 2px;">#</span>	ACCEPTABLE
	<span style="border: 1px solid red; border-radius: 50%; padding: 2px;">#</span>	EXCEEDED

**NOTES:**

1. SCALE IS APPROXIMATE.
2. # PEDESTRIAN LEVEL WIND SENSOR LOCATION.

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PROJECT	B4-B6, FOREST PARK CIRCLE, MISSISSAUGA PEDESTRIAN LEVEL WIND STUDY	
SCALE	1:1300 (APPROX.)	DRAWING NO. GW14-118-PLW-B4/6-3B
DATE	JANUARY 9, 2026	DRAWN BY K.A.

DESCRIPTION	FIGURE 3B: WINTER FUTURE GRADE LEVEL PLW SENSOR LAYOUT PEDESTRIAN COMFORT PREDICTIONS
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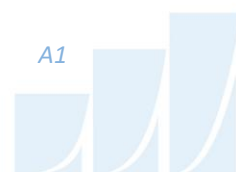
## APPENDIX A

### PEDESTRIAN COMFORT SUITABILITY, TABLES A1-A2 (EXISTING CONDITIONS)

Guidelines	
Pedestrian Comfort	<b>20% exceedance wind speed</b> 0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable
Pedestrian Safety	<b>0.1% exceedance wind speed</b> 0-90 km/h = Safe

**TABLE A1: SUMMARY OF PEDESTRIAN COMFORT (EXISTING CONDITIONS)**

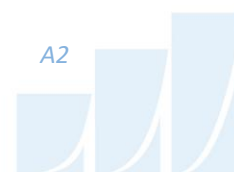
Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
1	12.9	Standing	15.4	Walking	58.6	Safe
2	12.2	Standing	14.6	Standing	54.3	Safe
3	12.1	Standing	14.7	Standing	56.4	Safe
4	12.4	Standing	15.7	Walking	59.6	Safe
5	11.6	Standing	14.9	Standing	52.0	Safe
6	11.1	Standing	14.9	Standing	51.6	Safe
7	11.2	Standing	15.1	Walking	53.2	Safe
8	11.3	Standing	15.3	Walking	53.8	Safe
9	11.0	Standing	14.4	Standing	50.7	Safe
10	11.3	Standing	14.8	Standing	52.8	Safe
11	11.3	Standing	14.6	Standing	53.2	Safe
12	10.8	Standing	13.8	Standing	58.3	Safe
13	13.8	Standing	16.9	Walking	70.5	Safe
14	6.5	Sitting	8.5	Sitting	34.1	Safe
15	11.5	Standing	14.0	Standing	55.9	Safe
16	11.5	Standing	14.1	Standing	54.9	Safe
17	11.9	Standing	15.6	Walking	58.9	Safe
18	15.1	Walking	18.4	Walking	69.1	Safe
19	14.6	Standing	18.4	Walking	68.9	Safe
20	14.4	Standing	17.8	Walking	71.8	Safe
21	15.5	Walking	20.1	Uncomfortable	71.7	Safe
22	12.2	Standing	15.9	Walking	62.4	Safe
23	12.4	Standing	14.8	Standing	61.0	Safe
24	12.5	Standing	14.8	Standing	60.6	Safe
25	6.6	Sitting	8.2	Sitting	31.2	Safe
26	13.7	Standing	15.4	Walking	62.4	Safe
27	12.4	Standing	14.7	Standing	61.4	Safe
28	9.0	Sitting	11.4	Standing	55.8	Safe
29	13.0	Standing	16.1	Walking	65.8	Safe
30	11.5	Standing	15.2	Walking	55.4	Safe
31	10.8	Standing	14.4	Standing	51.0	Safe
32	10.4	Standing	13.6	Standing	52.6	Safe
33	10.9	Standing	14.5	Standing	54.0	Safe
34	10.3	Standing	13.9	Standing	51.2	Safe
35	10.6	Standing	13.8	Standing	49.4	Safe



Guidelines	
Pedestrian Comfort	<b>20% exceedance wind speed</b> 0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable
Pedestrian Safety	<b>0.1% exceedance wind speed</b> 0-90 km/h = Safe

**TABLE A2: SUMMARY OF PEDESTRIAN COMFORT (EXISTING CONDITONS)**

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
36	10.6	Standing	14.1	Standing	55.6	Safe
37	6.7	Sitting	8.7	Sitting	40.0	Safe
38	11.0	Standing	13.1	Standing	53.6	Safe
39	10.9	Standing	13.9	Standing	55.8	Safe
40	12.1	Standing	15.3	Walking	59.9	Safe
41	12.6	Standing	14.9	Standing	56.1	Safe
42	13.8	Standing	18.0	Walking	75.9	Safe
43	14.4	Standing	18.2	Walking	65.6	Safe
44	11.2	Standing	14.5	Standing	58.4	Safe
45	10.8	Standing	13.9	Standing	51.8	Safe
46	12.4	Standing	15.9	Walking	62.8	Safe
47	11.6	Standing	14.9	Standing	55.9	Safe
48	11.0	Standing	14.3	Standing	55.3	Safe
49	11.2	Standing	14.8	Standing	57.0	Safe
50	14.9	Standing	17.9	Walking	68.1	Safe
51	6.9	Sitting	9.0	Sitting	42.8	Safe
52	11.7	Standing	14.7	Standing	62.8	Safe
53	16.8	Walking	20.9	Uncomfortable	75.0	Safe
54	16.0	Walking	19.0	Walking	64.0	Safe
55	11.6	Standing	13.9	Standing	54.7	Safe
56	9.3	Sitting	12.0	Standing	54.1	Safe
57	9.8	Sitting	13.8	Standing	64.4	Safe
58	8.5	Sitting	11.5	Standing	48.4	Safe
59	12.6	Standing	15.8	Walking	67.7	Safe
60	8.5	Sitting	10.0	Sitting	41.0	Safe
61	12.7	Standing	15.6	Walking	65.6	Safe
62	10.1	Standing	12.7	Standing	57.2	Safe
63	12.8	Standing	15.6	Walking	69.5	Safe
64	8.7	Sitting	11.5	Standing	47.8	Safe
65	7.6	Sitting	9.7	Sitting	49.2	Safe
66	9.5	Sitting	11.2	Standing	46.1	Safe
67	17.8	Walking	21.6	Uncomfortable	75.0	Safe
68	9.6	Sitting	11.6	Standing	47.7	Safe
106	15.7	Walking	19.1	Walking	82.9	Safe
107	8.4	Sitting	10.1	Standing	46.5	Safe





## APPENDIX B

### PEDESTRIAN COMFORT SUITABILITY, TABLES B1-B4 (FUTURE CONDITIONS)

Guidelines	
Pedestrian Comfort	<b>20% exceedance wind speed</b> (0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable)
Pedestrian Safety	<b>0.1% exceedance wind speed</b> 0-90 km/h = Safe

**TABLE B1: SUMMARY OF PEDESTRIAN COMFORT (FUTURE CONDITONS)**

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
1	12.3	Standing	14.5	Standing	58.8	Safe
2	12.1	Standing	13.7	Standing	54.1	Safe
3	13.1	Standing	14.8	Standing	55.9	Safe
4	12.9	Standing	14.3	Standing	55.2	Safe
5	11.5	Standing	13.9	Standing	53.8	Safe
6	10.8	Standing	14.0	Standing	61.3	Safe
7	9.5	Sitting	12.2	Standing	60.7	Safe
8	13.1	Standing	18.5	Walking	66.5	Safe
9	11.1	Standing	13.2	Standing	53.0	Safe
10	11.5	Standing	14.1	Standing	54.3	Safe
11	10.3	Standing	12.9	Standing	60.0	Safe
12	11.0	Standing	12.6	Standing	53.6	Safe
13	11.3	Standing	14.0	Standing	65.2	Safe
14	6.4	Sitting	8.2	Sitting	32.1	Safe
15	9.4	Sitting	12.2	Standing	51.6	Safe
16	9.9	Sitting	13.6	Standing	56.0	Safe
17	11.7	Standing	15.4	Walking	58.5	Safe
18	14.2	Standing	17.9	Walking	67.4	Safe
19	13.7	Standing	17.3	Walking	66.2	Safe
20	13.3	Standing	16.6	Walking	69.0	Safe
21	14.7	Standing	18.9	Walking	66.5	Safe
22	11.6	Standing	15.1	Walking	59.1	Safe
23	11.5	Standing	13.9	Standing	60.4	Safe
24	11.6	Standing	14.5	Standing	60.6	Safe
25	6.9	Sitting	8.4	Sitting	34.8	Safe
26	11.6	Standing	14.0	Standing	61.4	Safe
27	13.0	Standing	15.0	Standing	60.2	Safe
28	12.5	Standing	16.4	Walking	60.8	Safe
29	12.7	Standing	14.0	Standing	59.7	Safe
30	9.4	Sitting	11.3	Standing	46.7	Safe
31	12.0	Standing	14.9	Standing	55.8	Safe
32	13.3	Standing	16.8	Walking	67.7	Safe
33	13.8	Standing	18.2	Walking	71.8	Safe
34	15.9	Walking	20.6	Uncomfortable	77.3	Safe
35	14.2	Standing	18.1	Walking	66.9	Safe

Guidelines	
Pedestrian Comfort	<b>20% exceedance wind speed</b> (0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable)
Pedestrian Safety	<b>0.1% exceedance wind speed</b> 0-90 km/h = Safe

**TABLE B2: SUMMARY OF PEDESTRIAN COMFORT (FUTURE CONDITONS)**

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
36	11.6	Standing	14.1	Standing	54.4	Safe
37	8.0	Sitting	10.0	Sitting	49.5	Safe
38	11.0	Standing	13.3	Standing	52.5	Safe
39	11.8	Standing	14.5	Standing	63.6	Safe
40	13.0	Standing	17.0	Walking	65.6	Safe
41	11.9	Standing	14.2	Standing	53.4	Safe
42	12.6	Standing	16.3	Walking	63.0	Safe
43	14.7	Standing	18.6	Walking	63.8	Safe
44	11.9	Standing	15.4	Walking	58.7	Safe
45	12.5	Standing	16.3	Walking	58.5	Safe
46	14.2	Standing	18.0	Walking	59.0	Safe
47	12.9	Standing	16.2	Standing	55.7	Safe
48	11.2	Standing	14.1	Standing	53.7	Safe
49	11.5	Standing	14.4	Standing	51.9	Safe
50	10.8	Standing	14.4	Standing	59.6	Safe
51	7.2	Sitting	9.5	Sitting	45.3	Safe
52	13.6	Standing	17.2	Walking	64.7	Safe
53	15.6	Walking	19.2	Walking	70.4	Safe
54	12.4	Standing	15.6	Walking	58.6	Safe
55	9.7	Sitting	12.6	Standing	52.8	Safe
56	8.9	Sitting	11.7	Standing	53.9	Safe
57	9.7	Sitting	13.7	Standing	61.7	Safe
58	8.6	Sitting	11.5	Standing	47.2	Safe
59	12.2	Standing	15.3	Walking	64.8	Safe
60	8.0	Sitting	9.8	Sitting	41.7	Safe
61	11.2	Standing	14.0	Standing	56.5	Safe
62	9.3	Sitting	11.8	Standing	53.9	Safe
63	9.8	Sitting	12.6	Standing	62.0	Safe
64	9.8	Sitting	12.8	Standing	51.9	Safe
65	8.2	Sitting	9.9	Sitting	44.4	Safe
66	9.5	Sitting	11.5	Standing	47.8	Safe
67	16.2	Walking	20.2	Uncomfortable	72.3	Safe
68	8.5	Sitting	10.9	Standing	46.8	Safe
69	8.5	Sitting	10.3	Standing	45.2	Safe
70	8.8	Sitting	11.1	Standing	47.9	Safe

Guidelines	
Pedestrian Comfort	<b>20% exceedance wind speed</b> (0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable)
Pedestrian Safety	<b>0.1% exceedance wind speed</b> 0-90 km/h = Safe

**TABLE B3: SUMMARY OF PEDESTRIAN COMFORT (FUTURE CONDITONS)**

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
71	9.9	Sitting	12.4	Standing	54.1	Safe
72	11.2	Standing	13.5	Standing	52.6	Safe
73	12.3	Standing	14.6	Standing	56.4	Safe
74	10.9	Standing	12.5	Standing	53.5	Safe
75	8.8	Sitting	11.7	Standing	68.2	Safe
76	8.8	Sitting	11.6	Standing	53.9	Safe
77	9.1	Sitting	10.5	Standing	43.6	Safe
78	10.3	Standing	11.9	Standing	56.1	Safe
79	10.2	Standing	13.1	Standing	55.7	Safe
80	8.1	Sitting	10.5	Standing	45.5	Safe
81	13.9	Standing	18.2	Walking	64.5	Safe
82	9.7	Sitting	11.7	Standing	54.6	Safe
83	9.1	Sitting	11.4	Standing	46.7	Safe
84	10.7	Standing	13.3	Standing	48.8	Safe
85	7.8	Sitting	9.1	Sitting	35.5	Safe
86	7.0	Sitting	8.9	Sitting	39.9	Safe
87	8.0	Sitting	9.9	Sitting	53.0	Safe
88	12.4	Standing	16.8	Walking	69.6	Safe
89	8.0	Sitting	10.7	Standing	55.3	Safe
90	9.3	Sitting	11.1	Standing	48.8	Safe
91	11.2	Standing	14.9	Standing	58.2	Safe
92	11.8	Standing	16.8	Walking	75.3	Safe
93	12.6	Standing	18.0	Walking	83.7	Safe
94	9.3	Sitting	11.7	Standing	45.7	Safe
95	12.2	Standing	15.5	Walking	52.4	Safe
96	14.2	Standing	18.0	Walking	62.7	Safe
97	12.4	Standing	15.9	Walking	55.7	Safe
98	6.9	Sitting	8.4	Sitting	36.1	Safe
99	7.8	Sitting	9.6	Sitting	41.7	Safe
100	9.3	Sitting	10.3	Standing	45.0	Safe
101	7.8	Sitting	9.8	Sitting	40.2	Safe
102	8.2	Sitting	10.4	Standing	40.3	Safe
103	7.6	Sitting	9.4	Sitting	43.0	Safe
104	10.2	Standing	11.9	Standing	45.7	Safe
105	12.8	Standing	15.6	Walking	66.3	Safe

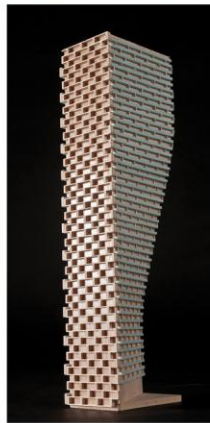
Guidelines	
Pedestrian Comfort	<b>20% exceedance wind speed</b> (0-10 km/h = Sitting, 10-15 km/h = Standing, 15-20 km/h = Walking, >20 km/h = Uncomfortable)
Pedestrian Safety	<b>0.1% exceedance wind speed</b> 0-90 km/h = Safe

**TABLE B4: SUMMARY OF PEDESTRIAN COMFORT (FUTURE CONDITONS)**

Sensor	Pedestrian Comfort				Pedestrian Safety	
	Summer		Winter		Annual	
	Wind Speed	Comfort Class	Wind Speed	Comfort Class	Wind Speed	Safety Class
<b>106</b>	15.2	Walking	18.7	Walking	79.7	Safe
<b>107</b>	8.6	Sitting	10.0	Standing	43.9	Safe

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## APPENDIX C

### WIND TUNNEL SIMULATION OF THE NATURAL WIND

## WIND TUNNEL SIMULATION OF THE NATURAL WIND

Wind flowing over the surface of the earth develops a boundary layer due to the drag produced by surface features such as vegetation and man-made structures. Within this boundary layer, the mean wind speed varies from zero at the surface to the gradient wind speed at the top of the layer. The height of the top of the boundary layer is referred to as the gradient height, above which the velocity remains more-or-less constant for a given synoptic weather system. The mean wind speed is taken to be the average value over one hour. Superimposed on the mean wind speed are fluctuating (or turbulent) components in the longitudinal (i.e. along wind), vertical and lateral directions. Although turbulence varies according to the roughness of the surface, the turbulence level generally increases from nearly zero (smooth flow) at gradient height to maximum values near the ground. While for a calm ocean the maximum could be 20%, the maximum for a very rough surface such as the center of a city could be 100%, or equal to the local mean wind speed. The height of the boundary layer varies in time and over different terrain roughness within the range of 400 metres (m) to 600 m.

Simulating real wind behaviour in a wind tunnel requires simulating the variation of mean wind speed with height, simulating the turbulence intensity, and matching the typical length scales of turbulence. It is the ratio between wind tunnel turbulence length scales and turbulence scales in the atmosphere that determines the geometric scales that models can assume in a wind tunnel. Hence, when a 1:200 scale model is quoted, this implies that the turbulence scales in the wind tunnel and the atmosphere have the same ratios. Some flexibility in this requirement has been shown to produce reasonable wind tunnel predictions compared to full scale. In model scale the mean and turbulence characteristics of the wind are obtained with the use of spires at one end of the tunnel and roughness elements along the floor of the tunnel. The fan is located at the model end and wind is pulled over the spires, roughness elements and model. It has been found that, to a good approximation, the mean wind profile can be represented by a power law relation, shown below, giving height above ground versus wind speed.

$$U = U_g \left( \frac{Z}{Z_g} \right)^\alpha$$

Where;  $U$  = mean wind speed,  $U_g$  = gradient wind speed,  $Z$  = height above ground,  $Z_g$  = depth of the boundary layer (gradient height) and  $\alpha$  is the power law exponent.

Figure C1 on the following page plots three velocity profiles for open country, and suburban and urban exposures.

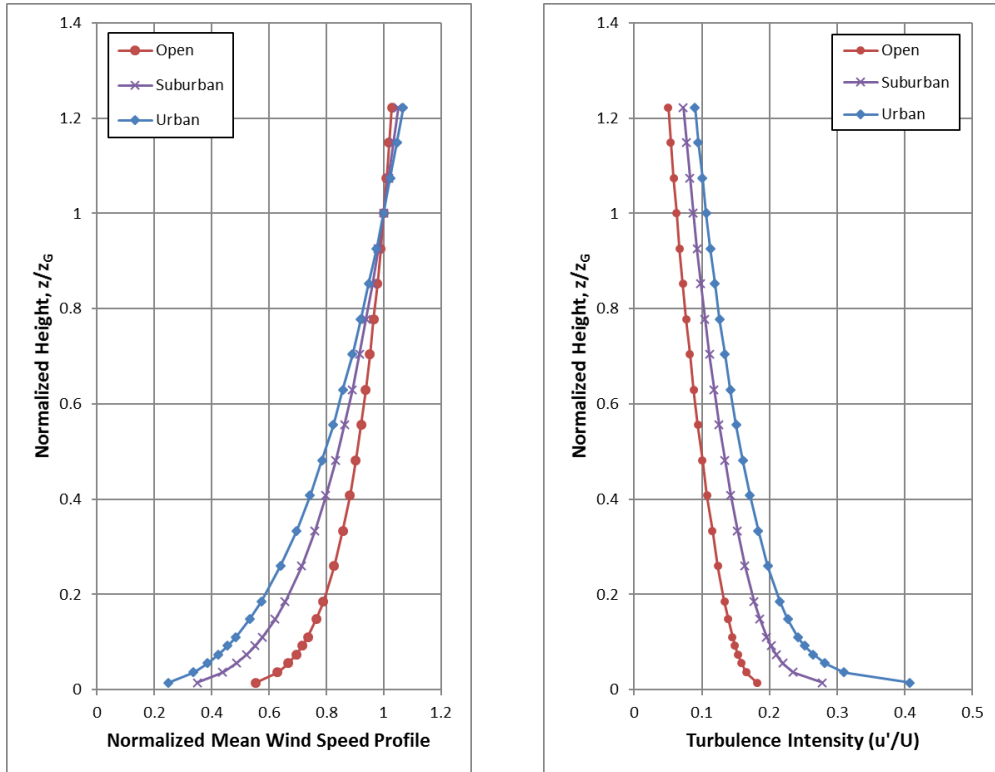
The exponent  $\alpha$  varies according to the type of upwind terrain;  $\alpha$  ranges from 0.14 for open country to 0.33 for an urban exposure. Figure C2 illustrates the theoretical variation of turbulence for open country, suburban and urban exposures.

The integral length scale of turbulence can be thought of as an average size of gust in the atmosphere. Although it varies with height and ground roughness, it has been found to generally be in the range of 100 m to 200 m in the upper half of the boundary layer. Thus, for a 1:300 scale, the model value should be between 1/3 and 2/3 of a metre. Integral length scales are derived from power spectra, which describe the energy content of wind as a function of frequency. There are several ways of determining integral length scales of turbulence. One way is by comparison of a measured power spectrum in model scale to a non-dimensional theoretical spectrum such as the Davenport spectrum of longitudinal turbulence. Using the Davenport spectrum, which agrees well with full-scale spectra, one can estimate the integral scale by plotting the theoretical spectrum with varying  $L$  until it matches as closely as possible the measured spectrum:

$$f \times S(f) = \frac{4(Lf)^2}{U_{10}^2} \left[ 1 + \frac{4(Lf)^2}{U_{10}^2} \right]^{-\frac{4}{3}}$$

Where,  $f$  is frequency,  $S(f)$  is the spectrum value at frequency  $f$ ,  $U_{10}$  is the wind speed 10 m above ground level, and  $L$  is the characteristic length of turbulence.

Once the wind simulation is correct, the model, constructed to a suitable scale, is installed at the center of the working section of the wind tunnel. Different wind directions are represented by rotating the model to align with the wind tunnel center-line axis.



**FIGURE C1 (LEFT): MEAN WIND SPEED PROFILES;  
FIGURE C2 (RIGHT): TURBULENCE INTENSITY PROFILES**

## REFERENCES

1. Teunissen, H.W., 'Characteristics of The Mean Wind And Turbulence In The Planetary Boundary Layer', Institute For Aerospace Studies, University Of Toronto, UTIAS # 32, Oct. 1970
2. Flay, R.G., Stevenson, D.C., 'Integral Length Scales in an Atmospheric Boundary Layer Near The Ground', 9th Australian Fluid Mechanics Conference, Auckland, Dec. 1966
3. ESDU, 'Characteristics of Atmospheric Turbulence Near the Ground', 74030
4. Bradley, E.F., Coppin, P.A., Katen, P.C., '*Turbulent Wind Structure Above Very Rugged Terrain*', 9<sup>th</sup> Australian Fluid Mechanics Conference, Auckland, Dec. 1966



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## APPENDIX D

### PEDESTRIAN LEVEL WIND MEASUREMENT METHODOLOGY

## **PEDESTRIAN LEVEL WIND MEASUREMENT METHODOLOGY**

Pedestrian level wind studies are performed in a wind tunnel on a physical model of the study buildings at a suitable scale. Instantaneous wind speed measurements are recorded at a model height corresponding to 1.5 m full scale using either a hot wire anemometer or a pressure-based transducer. Measurements are performed at any number of locations on the model and usually for 36 wind directions. For each wind direction, the roughness of the upwind terrain is matched in the wind tunnel to generate the correct mean and turbulent wind profiles approaching the model.

The hot wire anemometer is an instrument consisting of a thin metallic wire conducting an electric current. It is an omni-directional device equally sensitive to wind approaching from any direction in the horizontal plane. By compensating for the cooling effect of wind flowing over the wire, the associated electronics produce an analog voltage signal that can be calibrated against velocity of the air stream. For all measurements, the wire is oriented vertically so as to be sensitive to wind approaching from all directions in a horizontal plane.

The pressure sensor is a small cylindrical device that measures instantaneous pressure differences over a small area. The sensor is connected via tubing to a transducer that translates the pressure to a voltage signal that is recorded by computer. With appropriately designed tubing, the sensor is sensitive to a suitable range of fluctuating velocities.

For a given wind direction and location on the model, a time history of the wind speed is recorded for a period of time equal to one hour in full-scale. The analog signal produced by the hot wire or pressure sensor is digitized at a rate of 400 samples per second. A sample recording for several seconds is illustrated in Figure D1. This data is analyzed to extract the mean, root-mean-square (rms) and the peak of the signal. The peak value, or gust wind speed, is formed by averaging a number of peaks obtained from sub-intervals of the sampling period. The mean and gust speeds are then normalized by the wind tunnel gradient wind speed, which is the speed at the top of the model boundary layer, to obtain mean and gust ratios. At each location, the measurements are repeated for 36 wind directions to produce normalized polar plots, which will be provided upon request.



In order to determine the duration of various wind speeds at full scale for a given measurement location the gust ratios are combined with a statistical (mathematical) model of the wind climate for the project site. This mathematical model is based on hourly wind data obtained from one or more meteorological stations (usually airports) close to the project location. The probability model used to represent the data is the Weibull distribution expressed as:

$$P(>U_g) = A_\theta \cdot \exp\left[-\left(\frac{U_g}{C_\theta}\right)^{K_\theta}\right]$$

Where,

$P(>U_g)$  is the probability, fraction of time, that the gradient wind speed  $U_g$  is exceeded;  $\theta$  is the wind direction measured clockwise from true north,  $A$ ,  $C$ ,  $K$  are the Weibull coefficients, (Units:  $A$  - dimensionless,  $C$  - wind speed units [km/h] for instance,  $K$  - dimensionless).  $A_\theta$  is the fraction of time wind blows from a  $10^\circ$  sector centered on  $\theta$ .

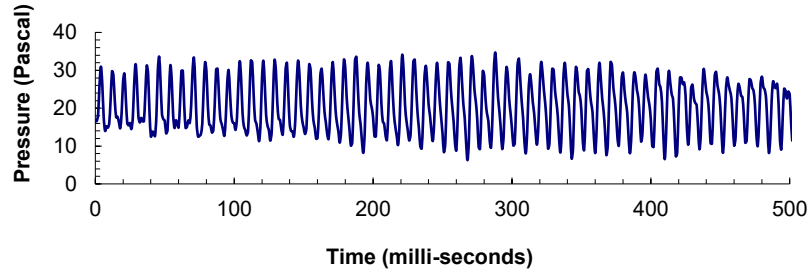
Analysis of the hourly wind data recorded for a length of time, on the order of 10 to 30 years, yields the  $A_\theta$ ,  $C_\theta$  and  $K_\theta$  values. The probability of exceeding a chosen wind speed level, say 20 km/h, at sensor  $N$  is given by the following expression:

$$P_N(>20) = \sum_\theta P\left[\frac{(>20)}{\left(\frac{U_N}{U_g}\right)}\right]$$

$$P_N(>20) = \sum_\theta P\{>20/(U_N/U_g)\}$$

Where,  $U_N/U_g$  is the gust velocity ratios, where the summation is taken over all 36 wind directions at  $10^\circ$  intervals.

If there are significant seasonal variations in the weather data, as determined by inspection of the  $C_{\theta}$  and  $K_{\theta}$  values, then the analysis is performed separately for two or more times corresponding to the groupings of seasonal wind data. Wind speed levels of interest for predicting pedestrian comfort are based on the comfort guidelines chosen to represent various pedestrian activity levels as discussed in the main text.



**FIGURE D1: TIME VERSUS VELOCITY TRACE FOR A TYPICAL WIND SENSOR**

## REFERENCES

1. Davenport, A.G., '*The Dependence of Wind Loading on Meteorological Parameters*', Proc. of Int. Res. Seminar, Wind Effects on Buildings & Structures, NRC, Ottawa, 1967, University of Toronto Press.
2. Wu, S., Bose, N., '*An Extended Power Law Model for the Calibration of Hot-wire/Hot-film Constant Temperature Probes*', Int. J. of Heat Mass Transfer, Vol.17, No.3, pp.437-442, Pergamon Press.